

FACTORIZATION OF THE $j = 7/2$ SHELL OF NEUTRONS AND PROTONS
Transformation Coefficients to States of Good Particle Number

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Complete tabulations are given, for the $j = 7/2$ nuclear shell, of the transformation coefficients to states of good particle number needed in a new method of nuclear spectroscopy based on a quasiparticle factorization of the j -shell. The method leads to a classification scheme in which total angular momentum and isospin are good quantum numbers and in which the calculation of matrix elements can be carried out simply by standard techniques of Racah algebra, without the use of coefficients of fractional parentage and with the use of only a very small number of reduced matrix elements. These reduced matrix elements also are tabulated. A few sample calculations show how matrix elements of one- and two-body operators, single nucleon and pair creation operators, . . . , can be calculated with this technique and the present tabulations.

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$$\sum_{J''_\mu T''_\mu} \frac{\langle J''_\mu T''_\mu \| [M \times M]^{J_o T_o} \| J_\mu T_\mu \rangle^2}{(2J_\mu + 1)(2T_\mu + 1)}$$

INTRODUCTION

The basic technical problem in nuclear-shell theory involves the calculation of matrix elements of the physically relevant operators such as one- and two-body operators, pair creation operators, etc., between definite states of an n -particle configuration. The standard technique for the evaluation of such matrix elements makes use of the fractional parentage expansion. Despite this fact tabulations of coefficients of fractional parentage (cfp) for configurations j^n are quite limited. For identical-particle configurations, $n \rightarrow n - 1$ cfp are available in tabulated form.¹⁻³ For identical-particle configurations tabulations also have been given for the expansion coefficients which express the n -particle matrix elements of a two-body interaction in terms of the 2-particle matrix elements (Band and Kharitonov⁴). For configurations of both protons and neutrons complete tabulations of $n \rightarrow n - 1$ and $n \rightarrow n - 2$ cfp in the isospin formalism are available only for $j = 3/2$ and $5/2$ shells (Towner and Hardy⁵). A similar tabulation for the full $j = 7/2$ shell would involve a prohibitively large number of cfp. It would be impractical to give such a tabulation in printed form; and for $j = 7/2$, tables of $n \rightarrow n - 1$ cfp in isospin formalism are available only for $n \leq 5$ (L. B. Hubbard⁶). Although nuclear shell-model computer codes^{7,8} have reduced such problems to efficient machine calculations, there are many instances

where a few specific matrix elements are needed and where a quick calculation from relatively simple tabulations (without the need of a computer code) may be of particular value. An alternate method of nuclear spectroscopy recently has been developed in terms of a factorization of the j -shell of both neutrons and protons in terms of a new type of quasiparticle operator.^{9,10} The method is a generalization of one developed by Armstrong and Judd¹¹ for the atomic l -shell. The new classification scheme is complete (requiring no arbitrary labels) for $j \leq 7/2$. The calculation of matrix elements in this scheme may be carried out simply without the use of fractional-parentage coefficients, with the use of only a very small number of reduced matrix elements and with standard techniques of Racah algebra. The total angular momentum J and isospin T are good quantum numbers in the new scheme. However, the particle number n is in general not a good quantum number. In order to calculate matrix elements between definite n -particle states it is necessary to calculate the transformation coefficients to states of good particle number. For the $j = 3/2$ and $5/2$ shells these have been tabulated in Ref. 10. These tabulations are extended here to the full $j = 7/2$ shell. The tabulation should be particularly useful in the calculation of matrix elements between states of large particle number ($n \geq 5$) and small isospin, where the cfp expansion becomes extremely cumbersome, and as a supplement to the cfp

tabulations of Ref. 6.

Since the new classification scheme may be somewhat unfamiliar, a brief review of the formalism is given in the following section where the notation also is established. The format of the tables is explained in USE OF TABLES which, in the first part, illustrates the use of the tables by means of a few examples and which, in the second part, makes a few sample calculations to illustrate fully the usefulness of the new technique.

QUASIPARTICLE FACTORIZATION OF THE j -SHELL

The method and notation follow Ref. 10, where details and derivations are given.

In terms of conventional nucleon creation (annihilation) operators $a_{m_i}^\dagger$ (a_{m_i}), with $m_i = \pm 1/2$ for neutron/proton, the new quasiparticle fermion operators are defined by:

$$\begin{aligned} \lambda_m^\dagger &= \frac{1}{\sqrt{2}} \{ a_{m, +\frac{1}{2}}^\dagger - (-1)^{j-m} a_{-m, -\frac{1}{2}} \} \\ \lambda_m &= (\lambda_m^\dagger)^\dagger \\ \mu_m^\dagger &= \frac{1}{\sqrt{2}} \{ a_{m, -\frac{1}{2}}^\dagger - (-1)^{j-m} a_{-m, +\frac{1}{2}} \} \\ \mu_m &= (\mu_m^\dagger)^\dagger \end{aligned} \tag{1}$$

where $m = j, \dots, -j$.

In terms of these two sets of anticommuting fermion operators, angular momentum and quasispin operators are defined for the λ and μ spaces:

$$\begin{aligned} (J_\lambda)_q &= \sum_m \langle jm \ 1q | j(m+q) \rangle [j(j+1)]^{\frac{1}{2}} \lambda_{m+q}^\dagger \lambda_m, \\ (J_\mu)_q &= \sum_m \langle jm \ 1q | j(m+q) \rangle [j(j+1)]^{\frac{1}{2}} \mu_{m+q}^\dagger \mu_m; \tag{2} \\ (T_\lambda)_+ &= \sum_{m>0} (-1)^{j-m} \lambda_m^\dagger \lambda_{-m}^\dagger, (T_\lambda)_- = (T_\lambda)_+^\dagger, \\ (T_\lambda)_0 &= \frac{1}{4} \sum_m (\lambda_m^\dagger \lambda_m - \lambda_m \lambda_m^\dagger); \\ (T_\mu)_+ &= \sum_{m>0} (-1)^{j-m} \mu_{-m} \mu_m, (T_\mu)_- = (T_\mu)_+^\dagger, \\ (T_\mu)_0 &= -\frac{1}{4} \sum_m (\mu_m^\dagger \mu_m - \mu_m \mu_m^\dagger). \end{aligned} \tag{3}$$

It follows that

$$\begin{aligned} \mathbf{J} &= \mathbf{J}_\lambda + \mathbf{J}_\mu \\ \mathbf{T} &= \mathbf{T}_\lambda + \mathbf{T}_\mu \end{aligned} \tag{4}$$

where \mathbf{J} and \mathbf{T} are the total angular momentum and isospin operators, respectively. The possible $J_\lambda T_\lambda$ (alternately $J_\mu T_\mu$) combinations (see Fig. 1) follow from the rules of identical particle spectroscopy (even though the λ and μ particles are not real particles and the J_λ and J_μ , for example, not physical angular momenta).

$T_\lambda (T_\mu)$	$J_\lambda (J_\mu)$				
0	2	4	5	8	
1/2	3/2	5/2	9/2	11/2	15/2
1	2	4	6		
3/2	7/2				
2	0				

Fig. 1. Possible $T_\lambda J_\lambda$ (alternately $T_\mu J_\mu$) combinations

In terms of angular momentum coupled-state vectors the basis

$$|(J_\lambda J_\mu) JM (T_\lambda T_\mu) TM_T\rangle \tag{5}$$

furnishes a complete classification scheme for shells with $j \leq 7/2$. Due to the transformation [Eq. (1)], however, the number operator is not diagonal in the basis [Eq. (5)].

It is useful to define coupled state vectors either symmetric (s) or antisymmetric (a), to an interchange of the λ and μ quantum numbers

$$\begin{aligned} &|(ab)J(cd)T\rangle_{(s)} \\ &= \sqrt{\frac{1}{2}} \{ |(ab)J(cd)T\rangle \\ &\quad \pm (-1)^{J-a-b+T-c-d} |(ba)J(dc)T\rangle \}. \end{aligned} \tag{6}$$

Quantum numbers M and M_T have been omitted for brevity but are quietly understood. Note that λ quantum numbers always precede μ quantum numbers in the order of the coupling; thus $J_\lambda = a$ in the first term of the right-hand side of Eq. (6), while $J_\lambda = b$ in the second term. Note also that the normalized state vector $|(aa)J(cc)T\rangle$, with both $J_\lambda = J_\mu$ and $T_\lambda = T_\mu$, is a state vector with $(\sigma) = (s)$ or (a) for $J - 2a + T - 2c = \text{even}$ or odd, respectively.

States of a definite nucleon number n must be linear combinations of either (s) or (a) states according to the rules:

$$\begin{aligned} \text{For } n = 2j + 1 \pm 4k, \text{ or } n = 2j \pm 4k: \\ (s) \text{ states only,} \\ \text{For } n = 2j + 3 \pm 4k, \text{ or } n = 2j + 2 \pm 4k: \\ (a) \text{ states only, } (7) \end{aligned}$$

where $k = \text{integer}$.

In making the transformation to states of good particle number n , one finds it is useful to employ the seniority classification scheme and the quantum numbers of the five-dimensional quasispin and symplectic groups: $R(5) \times Sp(2j + 1)$. In particular, it will be useful to use the particle-hole antisymmetric quantum number H_1 in place of the particle number n . States of good particle number are then defined by the transformation:

$$\begin{aligned} |(vt)H_1\beta T; \alpha J\rangle \\ = \sum_{T_\lambda T_\mu} C_{H_1\beta; T_\lambda T_\mu}^{(vt)T} \sum_{J_\lambda J_\mu} D_{(vt)\alpha; J_\lambda J_\mu}^{T_\lambda T_\mu} |(J_\lambda J_\mu)J(T_\lambda T_\mu)T\rangle_{(\sigma)} \quad (8) \end{aligned}$$

where $v = \text{seniority number}$; $t = \text{reduced isospin}$, $H_1 = \frac{1}{2}(n - 2j - 1) = \frac{1}{2}n - 4$; $\beta = \text{the label which distinguishes multiple occurrences of states with the same } n$, T in the representation (vt) , an $R(5)$ subgroup label; and $\alpha = \text{a similar label which distinguishes multiple occurrences of states with the same } J$ in the representation (vt) , a $Sp(2j + 1)$ subgroup label. The subscript (σ) refers to the symmetry label of Eq. (6) where, for each n , $(\sigma) = (s)$ or (a) according to the rules, Eq. (7).

The transformation coefficients in Eq. (8) have been factored into two parts. The C -coefficients come from the quasispin (or seniority) symmetry of the basis and have been calculated with the help of recursion formulae obtained from the known structure of the $R(5)$ group. The D -coefficients carry the dependence on the subgroup structure of $Sp(2j + 1)$ and have been calculated by numerical techniques as outlined in Ref. 10.

USE OF TABLES

Transformation to States of Good Particle Number

Example 1. $|(vt)H_1T; J\rangle = |(00)00; 0\rangle$
The state with $n = 8$, $v = 0$, $t = 0$, $T = 0$, $J = 0$. For $n = 8$, $H_1 = 0$. For this state the labels β and α are not needed (but are enumerated as $\beta = 1$ in Table I and $\alpha = 1$ in Table II). For this state of even- n , line 1 of Fig. 2 gives the allowed $(T_\lambda T_\mu)$ pairs as: $(T_\lambda T_\mu) = (00)$, (11) , (22) . The possible J_λ values for $T_\lambda = 0, 1, 2$ are given in Fig. 1 (similarly for J_μ). Note that $J_\lambda = J_\mu$ since $J = 0$. The three nonzero $C_{H_1\beta; T_\lambda T_\mu}^{(vt)T}$ coefficients are read from Table I as

$$\begin{aligned} C_{01;00}^{(00)0} = .4841229 \text{ with allowed } (J_\lambda J_\mu) \\ = (22), (44), (55), (88) \end{aligned}$$

$$\begin{aligned} C_{01;11}^{(00)0} = -.5229125 \text{ with allowed } (J_\lambda J_\mu) \\ = (22), (44), (66) \\ C_{01;22}^{(00)0} = .7015608 \text{ with allowed } (J_\lambda J_\mu) = (00). \end{aligned}$$

Hence there are eight $D_{(vt)J_\lambda J_\mu}^{T_\lambda T_\mu}$ coefficients needed in the construction of $|(vt)H_1T; J\rangle = |(00)00; 0\rangle$. These are read from Table II as:

$$\begin{aligned} D_{(00)22}^{000} = .345033 & \quad D_{(00)22}^{110} = .430332 \\ D_{(00)44}^{000} = .462910 & \quad D_{(00)44}^{110} = .577350 \\ D_{(00)55}^{000} = .511766 & \quad D_{(00)66}^{110} = .693889 \\ D_{(00)88}^{000} = .636209 & \quad D_{(00)00}^{220} = 1. \end{aligned}$$

The full-state vector then follows from Eq. (8),

$$\begin{aligned} |(vt)H_1T; J\rangle = |(00)00; 0\rangle \\ = .167038 |(22)0(00)0\rangle + .224105 |(44)0(00)0\rangle \\ + .247758 |(55)0(00)0\rangle + .308003 |(88)0(00)0\rangle \\ - .225026 |(22)0(11)0\rangle - .301904 |(44)0(11)0\rangle \\ - .362843 |(66)0(11)0\rangle + .701561 |(00)0(22)0\rangle. \end{aligned}$$

Note that the states $|(J_\lambda J_\mu)J(T_\lambda T_\mu)T\rangle$ of this equation are all automatically (s) states.

Example 2. The $n = 8$ state: $|(vt)H_1T; J\rangle = |(42)01; 4\rangle$
From Fig. 2 it can be seen that there is only one allowed $(T_\lambda T_\mu)$ pair, $(T_\lambda T_\mu) = (3/2 \ 1/2)$, and hence the C -coefficient = 1. For $(T_\lambda T_\mu) = (3/2 \ 1/2)$, the allowed $(J_\lambda J_\mu)$ -values, read from Fig. 1, and consistent with vector coupling to resultant $J = 4$, are $(J_\lambda J_\mu) = (7/2 \ 3/2)$, $(7/2 \ 5/2)$, $(7/2 \ 9/2)$, $(7/2 \ 11/2)$, $(7/2 \ 15/2)$. The five D -coefficients in the expansion of $|(42)01; 4\rangle$ in terms of $|(J_\lambda J_\mu)A(T_\lambda T_\mu)1\rangle_{(s)}$ are read from the $v = 4 \ t = 2$ entry of Table II and give

$$\begin{aligned} |(vt)H_1T; J\rangle = |(42)01; 4\rangle \\ = .175933 |(7/2 \ 3/2)A(3/2 \ 1/2)1\rangle_{(s)} \\ - .658281 |(7/2 \ 5/2)A(3/2 \ 1/2)1\rangle_{(s)} \\ - .128388 |(7/2 \ 9/2)A(3/2 \ 1/2)1\rangle_{(s)} \\ + .645497 |(7/2 \ 11/2)A(3/2 \ 1/2)1\rangle_{(s)} \\ - .320256 |(7/2 \ 15/2)A(3/2 \ 1/2)1\rangle_{(s)}. \end{aligned}$$

Note that the state vectors of the right-hand side of this equation are all of symmetry (s) as defined by Eq. (6). Note also that Fig. 2 gives only entries with $T_\lambda \geq T_\mu$; but for $T_\lambda \neq T_\mu$ the symmetrized state vectors (σ) of Eq. (8) always involve state vectors with both $T_\lambda > T_\mu$ and $T_\lambda < T_\mu$ (and, in this example, with both $J_\lambda = 7/2$ and $J_\mu = 7/2$), through Eq. (6).

Example 3. The $n = 7$ state:

$$|(vt)H_1T; J\rangle = |(1 \ 1/2) - 1/2 \ 5/2; 7/2\rangle$$

Figure 3 shows that the allowed $(T_\lambda T_\mu)$ pairs are $(2 \ 3/2)$ and $(1 \ 3/2)$, with $(J_\lambda J_\mu) = (0 \ 7/2)$ and $(J_\lambda J_\mu) = (2 \ 7/2)$, $(4 \ 7/2)$, $(6 \ 7/2)$, respectively. Tables I and II lead to

in the λ and μ spaces and apply standard techniques of Racah algebra.

In terms of double spherical tensor operators $\Lambda_{m m_i}^j, M_{m m_i}^j$, the quasiparticle operators of Eq. (1) have spherical tensor character given by

$$\begin{aligned} \lambda_m^\dagger &= \Lambda_{m, +\frac{1}{2}}^j & (-1)^{j-m} \lambda_{-m} &= \Lambda_{m, -\frac{1}{2}}^j \\ \mu_m^\dagger &= M_{m, -\frac{1}{2}}^j & (-1)^{j-m} \mu_{-m} &= M_{m, +\frac{1}{2}}^j \end{aligned} \quad (9)$$

where the operator $\Lambda_{m m_i}^j$ is a spherical tensor of rank j in the J -part of the λ space and of rank $\frac{1}{2}$ in the isospin (quasispin) part of the λ space, similarly for M in the μ space. From Eqs. (1) and (9),

$$\begin{aligned} a_{m \pm \frac{1}{2}}^\dagger &= \frac{1}{\sqrt{2}} (\Lambda_{m \pm \frac{1}{2}}^j + M_{m \pm \frac{1}{2}}^j); \\ (-1)^{j-m} a_{-m \mp \frac{1}{2}} &= \mp \frac{1}{\sqrt{2}} (\Lambda_{m \pm \frac{1}{2}}^j - M_{m \pm \frac{1}{2}}^j). \end{aligned} \quad (10)$$

Matrix elements of the operators Λ and M in the vector coupled $|(J_\lambda J_\mu)J(T_\lambda T_\mu)T\rangle$ basis are reduced to double-barred matrix elements $\langle \Delta' J'_\lambda T'_\lambda \| \Lambda \| \Delta J_\lambda T_\lambda \rangle$, $\langle \Delta' J'_\mu T'_\mu \| M \| \Delta J_\mu T_\mu \rangle$ by standard formulae of Racah algebra. The Δ and Δ' are quantum numbers common to both λ and μ spaces; [see Ref. 10; they characterize the irreducible representations $(\frac{1}{2} \frac{1}{2} \dots \pm \frac{1}{2})$ of $R(8j + 4)$ in which the direct product of λ and μ quasispin groups is imbedded]. These Δ 's have only two possible values and are characterized completely by the sign of $(-1)^{2T_\lambda + 2T_\mu}$ and are hence redundant when both T_λ and T_μ are given. Only the phase of the reduced matrix element of Λ is Δ -dependent; the reduced matrix element of M is independent of Δ . It is convenient to introduce Δ -independent reduced matrix elements, identical for λ and μ spaces, and symmetric to interchange of bra and ket labels, to be denoted by a double-barred matrix element with a prime superscript:

$$\begin{aligned} \langle \Delta' J'_\lambda T'_\lambda \| \Lambda \| \Delta J_\lambda T_\lambda \rangle &= (-1)^{T'_\lambda + T_\lambda + 2T_\mu + \frac{1}{2}} (-1)^{J'_\lambda - T'_\lambda + j + \frac{1}{2}} \langle J'_\lambda T'_\lambda \| \Lambda \| J_\lambda T_\lambda \rangle'; \\ \langle \Delta' J'_\mu T'_\mu \| M \| \Delta J_\mu T_\mu \rangle &= (-1)^{J'_\mu - T'_\mu + j} \langle J'_\mu T'_\mu \| M \| J_\mu T_\mu \rangle' \end{aligned} \quad (11)$$

where the primed reduced matrix elements satisfy

$$\begin{aligned} \langle a'b' \| \Lambda \| ab \rangle' &= \langle ab \| \Lambda \| a'b' \rangle' \\ &= \langle ab \| M \| a'b' \rangle' = \langle a'b' \| M \| ab \rangle'. \end{aligned} \quad (12)$$

The numerical values of these reduced matrix elements are related to those of identical nucleon cfp with $n = v$,

$$\begin{aligned} \langle J'T' = T - \frac{1}{2} \| M \| JT \rangle' &= (-1)^{J' + T + j} \left[\left(j + \frac{3}{2} - v \right) (v + 1) (2J' + 1) \right]^{\frac{1}{2}} \\ &\quad \times \langle j^v v J; j \rangle' j^{v+1} v + 1 J' \rangle \end{aligned} \quad (13)$$

with $v = j + \frac{1}{2} - 2T$. For easy reference the primed reduced matrix elements for $j = 7/2$ are given in Table III. Matrix elements of all physical operators can be related to these reduced matrix elements.

Single Nucleon Creation Operators

The basic reduced matrix element is obtained from Eq. (10) and standard Racah algebra:

$$\begin{aligned} &\langle (J'_\lambda J'_\mu)J'(T'_\lambda T'_\mu)T' \| a^\dagger \| (J_\lambda J_\mu)J(T_\lambda T_\mu)T \rangle \\ &= [\frac{1}{2}(2J + 1)(2J' + 1)(2T + 1)(2T' + 1)]^{\frac{1}{2}} \\ &\quad \times \left\{ \delta_{J'_\lambda J_\lambda} \delta_{T'_\lambda T_\lambda} \begin{Bmatrix} J_\lambda & J_\mu & J \\ J' & j & J'_\lambda \end{Bmatrix} \begin{Bmatrix} T_\lambda & T_\mu & T \\ T' & \frac{1}{2} & T'_\lambda \end{Bmatrix} \right\} \\ &\quad \times (-1)^{J + T + J_\mu - T_\lambda + T'_\lambda - T'_\mu - \frac{1}{2}} \langle J'_\lambda T'_\lambda \| \Lambda \| J_\lambda T_\lambda \rangle' \\ &\quad + \delta_{J'_\lambda J_\lambda} \delta_{T'_\lambda T_\lambda} \begin{Bmatrix} J_\lambda & J_\mu & J \\ j & J' & J'_\mu \end{Bmatrix} \begin{Bmatrix} T_\lambda & T_\mu & T \\ \frac{1}{2} & T' & T'_\mu \end{Bmatrix} \\ &\quad \times (-1)^{J' + T' + J_\lambda + T_\lambda + J_\mu + J'_\mu - \frac{1}{2}} \langle J'_\mu T'_\mu \| M \| J_\mu T_\mu \rangle' \end{aligned} \quad (14)$$

One-Body Operators, Pair Creation Operators

One-body operators can be expressed in terms of the basic tensors

$$\begin{aligned} [a^\dagger \times a]_{M_o M_{T_o}}^{J_o T_o} &= \sum_{m m_i} \langle j m j - m' | J_o M_o \rangle \langle \frac{1}{2} m_i \frac{1}{2} - m'_i | T_o M_{T_o} \rangle \\ &\quad \times a_{m m_i}^\dagger a_{m'_i m'_i} (-1)^{j - m' + \frac{1}{2} - m'_i} \end{aligned} \quad (15)$$

where

$$\begin{aligned} [a^\dagger \times a]_{M_o M_{T_o}}^{J_o T_o} &= -[\Lambda \times \Lambda]_{M_o M_{T_o}}^{J_o T_o} + [M \times M]_{M_o M_{T_o}}^{J_o T_o} \\ &\quad \text{for } J_o + T_o = \text{odd} \quad (16) \\ &= [\Lambda \times M]_{M_o M_{T_o}}^{J_o T_o} + [\frac{1}{2}(2j + 1)]^{\frac{1}{2}} \delta_{J_o 0} \delta_{T_o 0} \\ &\quad \text{for } J_o + T_o = \text{even.} \end{aligned}$$

Similarly,

$$\begin{aligned} [a^\dagger \times a^\dagger]_{M_o M_{T_o}}^{J_o T_o} &= \frac{1}{2} [\Lambda \times \Lambda]_{M_o M_{T_o}}^{J_o T_o} + \frac{1}{2} [M \times M]_{M_o M_{T_o}}^{J_o T_o} + [\Lambda \times M]_{M_o M_{T_o}}^{J_o T_o} \end{aligned} \quad (17)$$

with $J_o + T_o = \text{odd only}$.

For one-body operators with $J_o + T_o = \text{even}$, all matrix elements are related to the reduced matrix element

$$\begin{aligned} &\langle (J'_\lambda J'_\mu)J'(T'_\lambda T'_\mu)T' \| [\Lambda \times M]_{M_o M_{T_o}}^{J_o T_o} \| (J_\lambda J_\mu)J(T_\lambda T_\mu)T \rangle \\ &= [(2J + 1)(2J' + 1)(2J_o + 1)(2T + 1)(2T' + 1) \\ &\quad \times (2T_o + 1)]^{\frac{1}{2}} (-1)^{J'_\lambda + J'_\mu + T'_\lambda - T'_\mu + 2T_o} \\ &\quad \times \begin{Bmatrix} J_\lambda & j & J'_\lambda \\ J_\mu & j & J'_\mu \\ J & J_o & J' \end{Bmatrix} \begin{Bmatrix} T_\lambda & \frac{1}{2} & T'_\lambda \\ T_\mu & \frac{1}{2} & T'_\mu \\ T & T_o & T' \end{Bmatrix} \\ &\quad \times \langle J'_\lambda T'_\lambda \| \Lambda \| J_\lambda T_\lambda \rangle' \langle J'_\mu T'_\mu \| M \| J_\mu T_\mu \rangle'. \end{aligned} \quad (18)$$

The number operator, in particular, is given by

$$N_{\text{op.}} = (2j + 1) + [2(2j + 1)]^{\frac{1}{2}} [\Lambda \times M]_{00}^{00} \quad (19)$$

and has been used to check the entries in Tables I and II. Its matrix elements are given by

$$\begin{aligned} & \langle (J'_{\lambda} J'_{\mu}) JM(T'_{\lambda} T'_{\mu}) TM_T | N_{\text{op.}} | (J_{\lambda} J_{\mu}) JM(T_{\lambda} T_{\mu}) TM_T \rangle \\ &= (2j + 1) \delta_{J'_{\lambda} J_{\lambda}} \delta_{J'_{\mu} J_{\mu}} \delta_{T'_{\lambda} T_{\lambda}} \delta_{T'_{\mu} T_{\mu}} \\ &+ (-1)^{j + \frac{1}{2} + J + T + J_{\lambda} + J'_{\lambda} + 2J'_{\mu} + 2T'_{\lambda} - T_{\mu} - T'_{\mu}} \\ &\times \begin{Bmatrix} J_{\lambda} & J_{\mu} & J \\ J'_{\mu} & J'_{\lambda} & j \end{Bmatrix} \begin{Bmatrix} T_{\lambda} & T_{\mu} & T \\ T'_{\mu} & T'_{\lambda} & \frac{1}{2} \end{Bmatrix} \\ &\times \langle J'_{\lambda} T'_{\lambda} \| \Lambda \| J_{\lambda} T_{\lambda} \rangle \langle J'_{\mu} T'_{\mu} \| M \| J_{\mu} T_{\mu} \rangle. \quad (20) \end{aligned}$$

Specific Examples.—Note that for all states with $n = 8$ (Examples 1 and 2 above), T_{λ} and T_{μ} are either both all integral or both all half-integral. Hence the $[\Lambda \times M]$ operator of Eq. (19) has zero matrix elements between all components of the $n = 8$ state vectors, and the eigenvalue of $N_{\text{op.}}$ is $n = 2j + 1 = 8$ independent of the expansion coefficients C and D . In Example 3, the $[\Lambda \times M]$ -part of $N_{\text{op.}}$ makes contributions through four types of terms:

1. Matrix elements connecting the $| (07/2)7/2(23/2)5/2 \rangle$

and

$$| (7/20)7/2(3/22)5/2 \rangle$$

pieces of the (s) state vectors with $(T_{\lambda} T_{\mu}) = (23/2)$ contribute $-(3/4)^2(-3/4) = +27/64$.

2. Matrix elements connecting the

$| (07/2)7/2(23/2)5/2 \rangle$ piece to the $| (7/2J)7/2(3/21)5/2 \rangle$ pieces contribute.

$$\begin{aligned} & (3/4) \sum_J (-[7(2J + 1)/16 \cdot 27]^{\frac{1}{2}}) ([7(2J + 1)/16 \cdot 3]^{\frac{1}{2}}) \\ &= -63/64. \end{aligned}$$

3. Matrix elements connecting the

$$| (7/20)7/2(3/22)5/2 \rangle$$

piece to the

$$| (J7/2)7/2(13/2)5/2 \rangle$$

pieces contribute

$$\begin{aligned} & - (3/4) \sum_J (-[7(2J + 1)/16 \cdot 27]^{\frac{1}{2}}) \\ & \times (-[7(2J + 1)/16 \cdot 3]^{\frac{1}{2}}) = -63/64. \end{aligned}$$

4. Matrix elements connecting the

$$| (J7/2)7/2(13/2)5/2 \rangle$$

and

$$| (7/2J)7/2(3/21)5/2 \rangle$$

pieces of the (s) states with $(T_{\lambda} T_{\mu}) = (13/2)$ contribute $+35/64$, so that

$$n = 8 + (27 - 63 - 63 + 35)/64 = 7.$$

For the state with $n = 9$, and the same $(vt)TJ$, the replacement of (s) vectors with (a) vectors changes the signs of contributions 1-4, so that

$$n = 8 + (-27 + 63 + 63 - 35)/64 = 9.$$

Matrix elements of the operators $[\Lambda \times \Lambda]$ and $[M \times M]$, with $J_o + T_o = \text{odd}$, are again reduced to double-barred matrix elements by standard Racah algebra. The double-barred matrix element of $[M \times M]$ is independent of Δ (independent of whether $T_{\lambda} + T_{\mu} = \text{integer or half-integer}$) and is given by:

$$\begin{aligned} & \langle \Delta J'_{\mu} T'_{\mu} \| [M \times M]^{J_o T_o} \| \Delta J_{\mu} T_{\mu} \rangle = (-1)^{J_o + T_o + J_{\mu} + T'_{\mu}} \\ & \times \sum_{J''_{\mu} T''_{\mu}} (-1)^{J''_{\mu} + T''_{\mu}} [2J_o + 1](2T_o + 1)^{\frac{1}{2}} \\ & \times \begin{Bmatrix} J_{\mu} & j & J''_{\mu} \\ j & J'_{\mu} & J_o \end{Bmatrix} \begin{Bmatrix} T_{\mu} & \frac{1}{2} & T''_{\mu} \\ \frac{1}{2} & T'_{\mu} & T_o \end{Bmatrix} \\ & \times \langle J''_{\mu} T''_{\mu} \| M \| J'_{\mu} T'_{\mu} \rangle \langle J''_{\mu} T''_{\mu} \| M \| J_{\mu} T_{\mu} \rangle. \quad (21) \end{aligned}$$

These reduced matrix elements for $j = 7/2$ are given in Table IV. Only matrix elements with $J' \leq J$, $T' \leq T$ are tabulated since matrix elements with $J' > J$, $T' > T$ can be obtained from these by the symmetry property

$$\begin{aligned} & \langle J' T' \| [M \times M]^{J_o T_o} \| J T \rangle \\ &= (-1)^{J - J' + T - T'} \langle J T \| [M \times M]^{J_o T_o} \| J' T' \rangle. \quad (22) \end{aligned}$$

The reduced matrix elements

$$\langle \Delta J'_{\lambda} T'_{\lambda} \| [\Lambda \times \Lambda]^{J_o T_o} \| \Delta J_{\lambda} T_{\lambda} \rangle$$

gain an additional minus sign through their Δ -dependence:

$$\begin{aligned} & \langle \Delta a' b' \| [\Lambda \times \Lambda]^{J_o T_o} \| \Delta a b \rangle \\ &= - \langle a' b' \| [M \times M]^{J_o T_o} \| a b \rangle \quad (23) \end{aligned}$$

for both $T_{\lambda} + T_{\mu} = \text{integer or half-integer}$ (note that Δ' must $= \Delta$).

Two-Body Operators

Finally, the most general charge independent 2-body interaction acting within the j -shell can be expressed in terms of the 2-particle matrix elements

$$V_{JT} = \langle j^2 JM TM_T | V | j^2 JM TM_T \rangle \quad (24)$$

by

$$H_{2\text{-body}} = \left[\frac{1}{8} + \frac{(n - 2j - 1)}{2(2j + 1)} \right] V + \frac{1}{8} \sum_{J_o T_o} V_{J_o T_o} \times \{ ([\Lambda \times \Lambda]^{J_o T_o} : [\Lambda \times \Lambda]^{J_o T_o}) + ([M \times M]^{J_o T_o} : [M \times M]^{J_o T_o}) \} + \frac{1}{8} \sum_{J_o T_o} U_{J_o T_o} ([\Lambda \times \Lambda]^{J_o T_o} : [M \times M]^{J_o T_o}) \quad (25)$$

where the double-dot product is defined by

$$([\Lambda \times \Lambda]^{J_o T_o} : [\Lambda \times \Lambda]^{J_o T_o}) = -[(2J_o + 1)(2T_o + 1)]^{\frac{1}{2}} \times [[\Lambda \times \Lambda]^{J_o T_o} \times [\Lambda \times \Lambda]^{J_o T_o}]_{00}^{00} \quad (26)$$

and where

$$V = \sum_{JT} (2J + 1)(2T + 1) V_{JT} \quad (27)$$

$$U_{J_o T_o} = \sum_{JT} V_{JT} \left(2\delta_{J_o J} \delta_{T_o T} + 4(2J + 1)(2T + 1) \times \left\{ \begin{matrix} j & j & J \\ j & j & J_o \end{matrix} \right\} \left\{ \begin{matrix} \frac{1}{2} & \frac{1}{2} & T \\ \frac{1}{2} & \frac{1}{2} & T_o \end{matrix} \right\} \right). \quad (28)$$

The matrix elements of the operators in Eq. (25) are given by:

$$\langle (J_\lambda J_\mu) JM(T_\lambda T_\mu) TM_T | ([M \times M]^{J_o T_o} : [M \times M]^{J_o T_o}) \times (J_\lambda J_\mu) JM(T_\lambda T_\mu) TM_T \rangle = \sum_{J'_\mu T'_\mu} \frac{\langle J'_\mu T'_\mu || [M \times M]^{J_o T_o} || J_\mu T_\mu \rangle^2}{(2J_\mu + 1)(2T_\mu + 1)} \quad (29)$$

(similarly for the companion Λ operator). Note that these matrix elements must be diagonal in *all* λ and μ quantum numbers. For convenience, the sums of Eq. (29) are tabulated for each $J_\mu T_\mu$ ($J_o T_o$) in Table V.

$$\langle (J'_\lambda J'_\mu) JM(T'_\lambda T'_\mu) TM_T | ([\Lambda \times \Lambda]^{J_o T_o} : [M \times M]^{J_o T_o}) \times |(J_\lambda J_\mu) JM(T_\lambda T_\mu) TM_T \rangle = (-1)^{J+J_\lambda+J'_\mu+T+T_\lambda+T'_\mu} \left\{ \begin{matrix} J_\lambda & J_\mu & J \\ J'_\mu & J'_\lambda & J_o \end{matrix} \right\} \left\{ \begin{matrix} T_\lambda & T_\mu & T \\ T'_\mu & T'_\lambda & T_o \end{matrix} \right\} \times \langle \Delta J'_\lambda T'_\lambda || [\Lambda \times \Lambda]^{J_o T_o} || \Delta J_\lambda T_\lambda \rangle \langle \Delta J'_\mu T'_\mu || [M \times M]^{J_o T_o} || \Delta J_\mu T_\mu \rangle. \quad (30)$$

As a further test of the tabulations sample calculations of a few simple 2-body interactions with known eigenvalues have been carried out. These interactions are listed below

Interaction	Eigenvalue	$V_{J_o T_o}$	$U_{J_o T_o}$
$\sum_{i < k} 1$	$\frac{1}{2}n(n - 1)$	1	4
H_{pairing}	$\frac{1}{4}(n - v)(4j + 8 - n - v) + t(t + 1) - T(T + 1)$	$\delta_{J_o 0} \delta_{T_o 1} (2j + 1)$	$\delta_{J_o 0} \delta_{T_o 1} (4j + 2) + 6(-1)^{J_o+1} / (2T_o + 1)$
$\sum_{i < k} \mathbf{t}_i \cdot \mathbf{t}_k$	$\frac{1}{2}[T(T + 1) - \frac{3}{4}n]$	$+\frac{1}{4} T_o = 1$ $-\frac{3}{4} T_o = 0$	$-(2j + 1) \delta_{J_o 0} \delta_{T_o 1}$
$\sum_{i < k} \mathbf{j}_i \cdot \mathbf{j}_k$	$\frac{1}{2}[J(J + 1) - nj(j + 1)]$	$[\frac{1}{2}J_o(J_o + 1) - j(j + 1)]$ $= (-1)^{J_o+1} j(j + 1)(2j + 1) \left\{ \begin{matrix} j & j & J_o \\ j & j & 1 \end{matrix} \right\}$	$-\frac{4}{3}j(j + 1)(2j + 1) \delta_{J_o 1} \delta_{T_o 0}$

Sample Calculation.—For the $n = 8$ state with $(vt) = (00)$, $T = 0$, $J = 0$ (Example 1), the eigenvalues for the first three interactions above are found to be [with the aid of Tables IV and V and Eqs. (29) and (30)]

$$E = \frac{1}{8}V + \frac{1}{4}(6V_{01} + 54V_{e1})(.492188) + \frac{1}{4}(2V_{01} + 42V_{e1} + 16V_{o0})(.273438) + \frac{1}{4}(36V_{e1} + 24V_{o0})(.234375) + .369141U_{01} - 1.230469U_{e1} + [.068359U_{01} + .683595U_{e1} + .546876U_{o0}] + .703119U_{o0} - 1.640620U_{e1},$$

where $V_{e1} = V_{J1}$ for any even- J ($J \neq 0$), $V_{o0} = V_{J0}$ for any odd- J (similarly for U_{e1} and U_{o0})*; and where terms 2, 3, and 4 arise from matrix elements of $([\Lambda \times \Lambda]^{J_o T_o} : [\Lambda \times \Lambda]^{J_o T_o})$ and $([M \times M]^{J_o T_o} : [M \times M]^{J_o T_o})$.

The U_{JT} -dependent terms are grouped as follows:

The first term arises from matrix elements connecting the $|(00)0(22)0\rangle$ term to itself,

* The notation V_{e1}, V_{o0}, \dots , is convenient for the special test interactions above but has no general significance.

The second term from matrix elements connecting $|(00)0(22)0\rangle$ to $|(JJ)0(11)0\rangle$,

The third term from matrix elements connecting $|(JJ)0(11)0\rangle$ to $|(J'J')0(11)0\rangle$,

The fourth term from matrix elements connecting $|(JJ)0(00)0\rangle$ to $|(J'J')0(00)0\rangle$,

The fifth term from matrix elements connecting $|(JJ)0(11)0\rangle$ to $|(J'J')0(00)0\rangle$.

The sum gives

$$E = 0.125V + 0.875V_{01} + 11.625V_{e1} + 2.500V_{00} \\ + 0.4375U_{01} - 2.1875U_{e1} + 1.250U_{00},$$

so that $E = 28, 28, -3$ for the 2-body operators $\Sigma 1, H_{\text{pairing}}, \Sigma t_i \cdot t_k$, respectively.

For the matrix elements of the operator $\Sigma \mathbf{j}_i \cdot \mathbf{j}_k$ in the state of Example 1, ($n = 8, (vt) = (00), T = 0, J = 0$),

$$E = \frac{1}{8}(-126) + \frac{1}{4} \\ \times \{.492188(-189) + .050637(-165 - 24) \\ + .091146(-109 - 80) + .131655(-21 - 168) \\ + .027902(-165 - 24) + .050223(-109 - 80) \\ + .061384(-69 - 120) + .094866(+99 - 288)\},$$

where the decimal numbers are the squares of the expansion coefficients of the state vector, and the first numbers in () give the contributions of the

$$\Sigma V_{J,T_0} \{([\Lambda \times \Lambda]^{J_0 T_0} : [\Lambda \times \Lambda]^{J_0 T_0}) \\ + ([M \times M]^{J_0 T_0} : [M \times M]^{J_0 T_0})\}$$

term of H , while the second numbers give the contributions of the U_{10} term. The final result gives $E = -63$.

Although these test interactions are extremely simple, the degree of complexity of the calculation is no greater for a matrix element of the most general

2-body interaction V_{JT} . For states of low T and n near the half-filled shell, in particular, the new technique for the calculation of nuclear matrix elements has a great advantage over the conventional cfp technique, since the cfp expansion becomes extremely cumbersome for such values of n and T .

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References

1. B. F. Bayman and A. Lande, Nucl. Phys. **77**, 1 (1966)
2. I. M. Band, Yu. I. Kharitonov, and L. A. Sliv, Nucl. Phys. **54**, 369 (1964)
3. I. M. Band, Sov. Phys.—JETP **18**, 1056 (1964)
4. I. M. Band and Yu. I. Kharitonov, NUCLEAR DATA TABLES **10**, 107 (1971)
5. I. S. Towner and J. C. Hardy, NUCLEAR DATA TABLES **6**, 153 (1969)
6. L. B. Hubbard, NUCLEAR DATA TABLES **9**, 85 (1971)
7. J. B. French et al., in *Advances in Nuclear Physics*, p. 193, Vol. 3 (M. Baranger and E. Vogt, eds.) Plenum Press, New York (1969)
8. L. B. Hubbard, Comp. Phys. Commun. **1**, 225 (1970)
9. J. P. Elliott and J. A. Evans, Phys. Lett. **31B**, 157 (1970)
10. K. T. Hecht and S. Szpikowski, Nucl. Phys. A **158**, 449 (1970)
11. L. Armstrong and B. R. Judd, Proc. R. Soc. Lond. A **315**, 27 and 39 (1970)

EXPLANATION OF TABLES

Definitions of Symbols

C	The transformation coefficients $C_{H_1\beta;T_\lambda T_\mu}^{(vt)T}$ defined by Eq. (8) and listed in Table I
D	The transformation coefficients $D_{(vt)\alpha;J_\lambda J_\mu}^{T_\lambda T_\mu J}$ defined by Eq. (8) and listed in Table II
H_1	$H_1 = \frac{1}{2}(n - 2j - 1) = \frac{1}{2}(n - 8)$, $n =$ particle number
J	Total angular momentum
J_λ, J_μ	The quasiparticle quantum numbers defined by Eqs. (2) and (4)
T	Total isospin
t	Reduced isospin
T_λ, T_μ	The quasiparticle quantum numbers defined by Eqs. (3) and (4)
v	Seniority
α	The label which distinguishes multiple occurrences of states with the same J in the representation (vt)
β	The label which distinguishes multiple occurrences of states with the same n, T in the representation (vt)
Λ, M	Double spherical tensor operators for the λ -, μ -spaces defined by Eqs. (9) and (10)
$\langle \ \Lambda\ \rangle'$	The symmetrical <i>primed</i> reduced matrix elements defined by Eq. (11) and listed in Table III
$\langle \ [M \times M]\ \rangle$	The reduced matrix elements $\langle J'_\mu T'_\mu \ [M \times M]^{J_o T_o}\ J_\mu T_\mu \rangle$ defined by Eqs. (21)–(23) and listed in Table IV
JL TL	$J_L T_L \equiv J'_\mu T'_\mu$
JR TR	$J_R T_R \equiv J_\mu T_\mu$
JOTO	$[M \times M]^{J_o T_o} \equiv (M * M) J O T O$

TABLE I. The Transformation Coefficients $C_{H_1\beta; T_\lambda T_\mu}^{(vt)T}$

T	H_1	β	T_λ	T_μ	C	T	H_1	β	T_λ	T_μ	C
$v = 0 \quad \frac{1}{2} = 0$											
0	-4	1	0	0	.4050463	1	-3	1	2	2	-.2795085
			1/2	1/2	.6123724	1	-1	1	1/2	1/2	.5590170
			1	1	.5625000				1	1	.2795085
			3/2	3/2	.3535534				3/2	3/2	-.4330127
			2	2	.1397542				2	2	-.6495191
0	-2	1	0	0	-.4677072	1	1	1	1/2	1/2	-.5590170
			1/2	1/2	-.3535534				1	1	.2795085
			1	1	.2165064				3/2	3/2	.4330127
			3/2	3/2	.6123724				2	2	-.6495191
			2	2	.4841229	1	3	1	1/2	1/2	.4330127
0	0	1	0	0	.4841229				1	1	-.6495191
			1/2	1/2	.0000000				3/2	3/2	.5590170
			1	1	-.5229125				2	2	-.2795085
			3/2	3/2	.0000000	2	-2	1	1	1	.5303301
			2	2	.7015608				3/2	3/2	.7071068
0	2	1	0	0	-.4677072				2	2	.4677072
			1/2	1/2	.3535534	2	0	1	1	1	-.6614378
			1	1	.2165064				3/2	3/2	.0000000
			3/2	3/2	-.6123724				2	2	.7500000
			2	2	.4841229	2	2	1	1	1	.5303301
0	4	1	0	0	.4050463				3/2	3/2	-.7071068
			1/2	1/2	-.6123724				2	2	.4677072
			1	1	.5625000	3	-1	1	3/2	3/2	-.7071068
			3/2	3/2	-.3535534				2	2	-.7071068
			2	2	.1397542	3	1	1	3/2	3/2	.7071068
1	-3	1	1/2	1/2	-.4330127				2	2	-.7071068
			1	1	-.6495191	4	0	1	2	2	1.000000
			3/2	3/2	-.5590170						
$v = 1 \quad \frac{1}{2} = 1/2$											
1/2	-7/2	1	0	1/2	-.5728220	1/2	7/2	1	1	3/2	-.4592793
			1	1/2	.6495191				2	3/2	-.1976424
			1	3/2	.4592793	3/2	-5/2	1	1	1/2	-.6123724
			2	3/2	.1976424				1	3/2	-.6846532
1/2	-5/2	1	0	1/2	-.3307189				2	3/2	-.3952847
			1	1/2	-.6250000	3/2	-3/2	1	1	1/2	.4564355
			1	3/2	.6187184				1	3/2	-.7144345
			2	3/2	-.3423266				2	3/2	.5303301
1/2	-3/2	1	0	1/2	.5728220	3/2	-1/2	1	1	1/2	.6454972
			1	1/2	-.0721688				1	3/2	-.1443376
			1	3/2	.5613414				2	3/2	-.7500000
			2	3/2	.5929271	3/2	1/2	1	1	1/2	-.6454972
1/2	-1/2	1	0	1/2	.4841229				1	3/2	.1443376
			1	1/2	.4269563				2	3/2	.7500000
			1	3/2	.3019037	3/2	3/2	1	1	1/2	-.4564355
			2	3/2	-.7015608				1	3/2	.7144345
1/2	1/2	1	0	1/2	-.4841229				2	3/2	-.5303301
			1	1/2	-.4269563	3/2	5/2	1	1	1/2	.6123724
			1	3/2	-.3019037				1	3/2	.6846532
			2	3/2	.7015608				2	3/2	.3952847
1/2	3/2	1	0	1/2	-.5728220	5/2	-3/2	1	1	3/2	.7500000
			1	1/2	.0721688				2	3/2	.6614378
			1	3/2	-.5613414	5/2	-1/2	1	1	3/2	.6614378
			2	3/2	-.5929271				2	3/2	-.7500000
1/2	5/2	1	0	1/2	.3307189	5/2	1/2	1	1	3/2	-.6614378
			1	1/2	.6250000				2	3/2	.7500000
			1	3/2	-.6187184	5/2	3/2	1	1	3/2	-.7500000
			2	3/2	.3423266				2	3/2	-.6614378
1/2	7/2	1	0	1/2	.5728220	7/2	-1/2	1	2	3/2	-1.000000
			1	1/2	-.6495191						
$v = 2 \quad \frac{1}{2} = 0$											
0	-3	1	0	0	.4677072	0	-3	1	3/2	3/2	-.2500000
			1/2	1/2	-.6614378	0	-1	1	0	0	-.5303301
			1	1	.5303301				1/2	1/2	.2500000

See page 321 for Explanation of Tables

TABLE I. The Transformation Coefficients $C_{H_1\beta; T_\lambda T_\mu}^{(v)T}$

τ	H_1	β	T_λ	T_μ	C	τ	H_1	β	T_λ	T_μ	C
$v = 2 \quad \frac{1}{2} = 0$											
0	-1	1	1	1	.4677072	1	-2	1	3/2	3/2	.4564355
			3/2	3/2	-.6614378	1	0	1	1/2	1/2	-.6454972
0	1	1	0	0	.5303301				1	1	.0000000
			1/2	1/2	.2500000				3/2	3/2	.7637626
			1	1	-.4677072	1	2	1	1/2	1/2	.5400617
			3/2	3/2	-.6614378				1	1	.7071068
0	3	1	0	0	.4677072				3/2	3/2	.4564355
			1/2	1/2	-.6614378	2	-1	1	1	1	.7071068
			1	1	-.5303301				3/2	3/2	-.7071068
			3/2	3/2	.2500000	2	1	1	1	1	-.7071068
1	-2	1	1/2	1/2	.5400617				3/2	3/2	-.7071068
			1	1	-.7071068	3	0	1	3/2	3/2	1.0000000
$v = 2 \quad \frac{1}{2} = 1$											
0	-2	1	1/2	1/2	.5400617	1	1	1	3/2	3/2	-.6575959
			1	1	-.7071068				1	0	.3970613
			3/2	3/2	.4564355				1	1	-.5812382
0	0	1	1/2	1/2	-.6454972				2	1	-.0671156
			1	1	.0000000	1	2	1	1/2	1/2	.0000000
			3/2	3/2	.7637626				3/2	1/2	.7071068
0	2	1	1/2	1/2	.5400617				3/2	3/2	.0000000
			1	1	.7071068				1	0	-.5400617
			3/2	3/2	.4564355				1	1	.0000000
1	-3	1	1/2	1/2	-.4930066				2	1	.4564355
			3/2	1/2	.4714045	1	3	1	1/2	1/2	.4930066
			3/2	3/2	-.1863390				3/2	1/2	-.4714045
			1	0	.5400617				3/2	3/2	.1863390
			1	1	.3952847				1	0	.5400617
			2	1	-.2282177				1	1	.3952847
1	-2	1	1/2	1/2	.0000000				2	1	-.2282177
			3/2	1/2	-.7071068	2	-2	1	3/2	1/2	-.5773503
			3/2	3/2	.0000000				3/2	3/2	.4082483
			1	0	-.5400617				1	1	-.5590170
			1	1	.0000000				2	1	.4330127
			2	1	.4564355	2	-1	1	3/2	1/2	.7071068
1	-1	1	1/2	1/2	.5068969				3/2	3/2	.0000000
			3/2	1/2	.4584869				1	1	.0000000
			3/2	3/2	-.1812328				2	1	-.7071068
			1	0	-.2251126	2	0	1	3/2	1/2	.5773503
			1	1	-.0768906				3/2	3/2	.8164966
			2	1	-.6658920				1	1	.0000000
			1/2	1/2	.0000000				2	1	.0000000
			3/2	1/2	-.2599376				3/2	1/2	.0000000
			3/2	3/2	-.6575959				3/2	3/2	.0000000
			1	0	-.3970613				1	1	.6123724
			1	1	.5812382				2	1	.7905694
			2	1	.0671156	2	1	1	3/2	1/2	-.7071068
1	0	1	1/2	1/2	.0000000				3/2	1/2	.0000000
			3/2	1/2	.0000000				1	1	.0000000
			3/2	3/2	.0000000				2	1	-.7071068
			1	0	.6454972	2	2	1	3/2	1/2	.5773503
			1	1	.0000000				3/2	3/2	-.4082483
			2	1	.7637626				1	1	-.5590170
1	1	1	1/2	1/2	-.5068969				2	1	.4330127
			3/2	1/2	-.4584869	3	-1	1	3/2	3/2	-.7071068
			3/2	3/2	.1812328				2	1	-.7071068
			1	0	-.2251126	3	0	1	3/2	3/2	.0000000
			1	1	-.0768906				2	1	1.0000000
			2	1	-.6658920	3	1	1	3/2	3/2	.7071068
			1/2	1/2	.0000000				2	1	-.7071068
			3/2	1/2	-.2599376						
$v = 3 \quad \frac{1}{2} = 1/2$											
1/2	-5/2	1	0	1/2	.6614378	1/2	-5/2	1	1	3/2	.3535534
			1	1/2	-.6614378	1/2	-3/2	1	0	1/2	.4330127

See page 321 for Explanation of Tables

TABLE I. The Transformation Coefficients $C_{H_1\beta; T_\lambda T_\mu}^{(vt)T}$

T	H_1	β	T_λ	T_μ	C	T	H_1	β	T_λ	T_μ	C
$v = 3 \quad t = 1/2$											
1/2	-3/2	1	1	1/2	.7216878	1/2	5/2	1	1	1/2	-.6614378
			1	3/2	.5400617				1	3/2	.3535534
1/2	-1/2	1	0	1/2	-.6123724	3/2	-3/2	1	1	1/2	.7637626
			1	1/2	-.2041241				1	3/2	-.6454972
			1	3/2	.7637626	3/2	-1/2	1	1	1/2	-.6454972
1/2	1/2	1	0	1/2	-.6123724	3/2	1/2	1	1	1/2	-.7637626
			1	1/2	-.2041241				1	1/2	-.6454972
			1	3/2	.7637626	3/2	3/2	1	1	3/2	-.7637626
1/2	3/2	1	0	1/2	.4330127	3/2	3/2	1	1	1/2	.7637626
			1	1/2	.7216878				1	3/2	-.6454972
			1	3/2	.5400617	5/2	-1/2	1	1	3/2	1.000000
1/2	5/2	1	0	1/2	.6614378	5/2	1/2	1	1	3/2	1.000000
$v = 3 \quad t = 3/2$											
1/2	-3/2	1	1	1/2	.7637626	3/2	1/2	1	0	3/2	.3393104
			1	3/2	-.6454972				1	1/2	-.5364969
1/2	-1/2	1	1	1/2	-.6454972				1	3/2	-.0573539
			1	3/2	-.7637626				2	1/2	-.7705518
1/2	1/2	1	1	1/2	-.6454972				0	3/2	.4442617
			1	3/2	-.7637626				1	1/2	.1873172
1/2	3/2	1	1	1/2	.7637626				1	3/2	.8760958
			1	3/2	-.6454972				2	1/2	.0000000
3/2	-5/2	1	0	3/2	-.4677072	3/2	3/2	1	0	3/2	.6846532
			1	1/2	-.7395100				1	1/2	-.3608439
			1	3/2	.3952847				1	3/2	-.2700309
			2	1/2	.2795085				2	1/2	.5728220
3/2	-3/2	1	0	3/2	-.6846532	3/2	5/2	1	0	3/2	.4677072
			1	1/2	.3608439				1	1/2	.7395100
			1	3/2	.2700309				1	3/2	-.3952847
			2	1/2	-.5728220				2	1/2	-.2795085
3/2	-1/2	1	0	3/2	-.3393104	5/2	-3/2	1	1	3/2	-.8660254
			1	1/2	.5364969				2	1/2	-.5000000
			1	3/2	.0573539				1	3/2	-.5000000
			2	1/2	.7705518				2	1/2	.8660254
			0	3/2	.4442617	5/2	1/2	1	1	3/2	.5000000
			1	1/2	.1873172				2	1/2	-.8660254
			1	3/2	.8760958	5/2	3/2	1	1	3/2	.8660254
			2	1/2	.0000000				2	1/2	.5000000
$v = 4 \quad t = 0$											
0	-2	1	0	0	.5590170	0	2	1	1/2	1/2	.7071068
			1/2	1/2	-.7071068				1	1	.4330127
			1	1	.4330127	1	-1	1	1/2	1/2	.7071068
0	0	1	0	0	-.6123724				1	1	-.7071068
			1/2	1/2	.0000000	1	1	1	1/2	1/2	-.7071068
			1	1	.7905694				1	1	-.7071068
0	2	1	0	0	.5590170	2	0	1	1	1	1.000000
$v = 4 \quad t = 1$											
0	-1	1	1/2	1/2	-.7071068	1	0	1	1	1	.0000000
			1	1	.7071068				1/2	1/2	.0000000
0	1	1	1/2	1/2	.7071068				3/2	1/2	.0000000
			1	1	.7071068				1	0	.5000000
1	-2	1	1/2	1/2	.5773503				1	1	.8660254
			3/2	1/2	.4082483	1	1	1	1/2	1/2	.0000000
			1	0	-.6123724				3/2	1/2	-.7071068
			1	1	-.3535534				1	0	-.7071068
1	-1	1	1/2	1/2	.0000000				1	1	.0000000
			3/2	1/2	-.7071068	1	2	1	1/2	1/2	.5773503
			1	0	.7071068				3/2	1/2	.4082483
			1	1	.0000000				1	0	.6123724
1	0	1	1/2	1/2	.5773503				1	1	.3535534
			3/2	1/2	.8164966	2	-1	1	3/2	1/2	-.7071068
			1	0	.0000000				1	1	.7071068

See page 321 for Explanation of Tables

TABLE I. The Transformation Coefficients $C_{H_1\beta; T_\lambda T_\mu}^{(vt)T}$

T	H_1	β	T_λ	T_μ	C	T	H_1	β	T_λ	T_μ	C
$v = 4 \quad \bar{t} = 1$											
2	0	1	3/2	1/2	1.000000	2	1	1	3/2	1/2	-.7071068
			1	1	.0000000				1	1	-.7071068
$v = 4 \quad \bar{t} = 2$											
0	0	1	1	1	1.000000	2	-1	1	3/2	1/2	-.7071068
1	-1	1	1	1	-.7071068				2	0	-.7071068
			3/2	1/2	-.7071068	2	0	1	1	1	-.5000000
1	0	1	1	1	.0000000				3/2	1/2	.0000000
			3/2	1/2	1.000000				2	0	.8660254
1	1	1	1	1	.7071068	2	1	1	1	1	.0000000
			3/2	1/2	-.7071068				3/2	1/2	.7071068
2	-2	1	1	1	.6123724				2	0	-.7071068
			3/2	1/2	.7071068	2	2	1	1	1	.6123724
			2	0	.3535534				3/2	1/2	-.7071068
2	-1	1	1	1	.0000000				2	0	.3535534
$v = 5 \quad \bar{t} = 1/2$											
1/2	-3/2	1	0	1/2	.7905694	1/2	1/2	1	1	1/2	.7905694
			1	1/2	.6123724	1/2	3/2	1	0	1/2	-.7905694
1/2	-1/2	1	0	1/2	.6123724				1	1/2	-.6123724
			1	1/2	-.7905694	3/2	-1/2	1	1	1/2	-1.0000000
1/2	1/2	1	0	1/2	-.6123724	3/2	1/2	1	1	1/2	1.0000000
$v = 5 \quad \bar{t} = 3/2$											
1/2	-1/2	1	1	1/2	-1.000000	3/2	-1/2	1	1	1/2	-.5000000
1/2	1/2	1	1	1/2	1.000000	3/2	1/2	1	0	3/2	.8660254
3/2	-3/2	1	0	3/2	.5000000				1	1/2	-.5000000
			1	1/2	.8660254	3/2	3/2	1	0	3/2	.5000000
3/2	-1/2	1	0	3/2	.8660254				1	1/2	.254
$v = 6 \quad \bar{t} = 0$											
0	-1	1	0	0	.7071068	0	1	1	1/2	1/2	-.7071068
			1/2	1/2	-.7071068	1	0	1	1/2	1/2	1.0000000
0	1	1	0	0	-.7071068						
$v = 6 \quad \bar{t} = 1$											
0	0	1	1/2	1/2	1.000000	1	0	1	1	0	1.000000
1	-1	1	1/2	1/2	-.7071068	1	1	1	1/2	1/2	.7071068
			1	0	-.7071068				1	1	-.7071068
1	0	1	1/2	1/2	.0000000						
$v = 7 \quad \bar{t} = 1/2$											
1/2	1/2	1	0	1/2	1.000000						
$v = 8 \quad \bar{t} = 0$											
0	0	1	0	0	1.000000						

TABLE II. The Transformation Coefficients $D_{(v)l\alpha, J, J_\mu}^{T, T_\mu, J}$

J	α	T_λ	T_μ	J_λ	J_μ	D	J	α	T_λ	T_μ	J_λ	J_μ	D		
$v = 0 \quad \dagger = 0$															
0	1	0	0	2	2	.345033	0	1	1/2	1/2	11/2	11/2	-.500000		
		0	0	4	4	.462910			1/2	1/2	15/2	15/2	-.577350		
		0	0	5	5	.511766			1	1	2	2	.430332		
		0	0	8	8	.636209			1	1	4	4	.577350		
		1/2	1/2	3/2	3/2	-.288675			1	1	6	6	.693889		
		1/2	1/2	5/2	5/2	-.353553			3/2	3/2	7/2	7/2	-1.00000		
		1/2	1/2	9/2	9/2	-.456435			2	2	0	0	1.00000		
$v = 1 \quad \dagger = 1/2$															
7/2	1	0	1/2	2	3/2	-.193430	7/2	1	1	1/2	2	3/2	-.133631		
		0	1/2	2	5/2	-.054555			1	1/2	2	5/2	.276385		
		0	1/2	2	9/2	-.260449			1	1/2	2	9/2	.146611		
		0	1/2	2	11/2	.104031			1	1/2	2	11/2	.263523		
		0	1/2	4	3/2	.081441			1	1/2	4	3/2	.255883		
		0	1/2	4	5/2	.304725			1	1/2	4	5/2	.087039		
		0	1/2	4	9/2	.059432			1	1/2	4	9/2	-.367806		
		0	1/2	4	11/2	.298807			1	1/2	4	11/2	-.221906		
		0	1/2	4	15/2	-.148250			1	1/2	4	15/2	-.275241		
		0	1/2	5	3/2	.198206			1	1/2	6	5/2	-.202572		
		0	1/2	5	5/2	-.170783			1	1/2	6	9/2	.227062		
		0	1/2	5	9/2	-.283473			1	1/2	6	11/2	-.362372		
		0	1/2	5	11/2	.235100			1	1/2	6	15/2	.507519		
		0	1/2	5	15/2	.240464			1	3/2	2	7/2	-.430332		
		0	1/2	8	9/2	.237929			1	3/2	4	7/2	-.577350		
		0	1/2	8	11/2	.307603			1	3/2	6	7/2	-.693889		
0	1/2	8	15/2	.503520	2	3/2	0	7/2	-1.00000						
$v = 2 \quad \dagger = 0$															
1	1	0	0	2	2	.130410	3	1	1	1	2	4	.521641		
		0	0	4	4	.319438			1	1	4	4	-.390151		
		0	0	4	5	.000000			1	1	4	6	.708080		
		0	0	5	5	.432522			1	1	6	6	.109259		
		0	0	8	8	.832993			3/2	3/2	7/2	7/2	1.00000		
		1/2	1/2	3/2	3/2	.092214			5	1	0	0	2	4	-.172292
		1/2	1/2	3/2	5/2	.000000					0	0	2	5	-.301511
		1/2	1/2	5/2	5/2	.172516					0	0	4	4	-.418738
		1/2	1/2	9/2	9/2	.374575					0	0	4	5	.277350
		1/2	1/2	9/2	11/2	.000000					0	0	4	8	.573768
		1/2	1/2	11/2	11/2	.493150					0	0	5	5	.285714
		1/2	1/2	15/2	15/2	.760415					0	0	5	8	-.371874
		1	1	2	2	.199205					0	0	8	8	.279303
		1	1	4	4	.487950					1/2	1/2	3/2	9/2	-.258438
		1	1	6	6	.849837					1/2	1/2	3/2	11/2	-.213201
		3/2	3/2	7/2	7/2	1.00000					1/2	1/2	5/2	5/2	-.268226
3	1	0	0	2	2	.356679	1/2	1/2			5/2	9/2	.285955		
		0	0	2	4	-.275321	1/2	1/2			5/2	11/2	-.314918		
		0	0	2	5	.455842	1/2	1/2			5/2	15/2	.398663		
		0	0	4	4	-.029574	1/2	1/2			9/2	9/2	.020663		
		0	0	4	5	-.478091	1/2	1/2			9/2	11/2	.276202		
		0	0	5	5	.061564	1/2	1/2	9/2	15/2	-.157924				
		0	0	5	8	.519944	1/2	1/2	11/2	11/2	.196744				
		0	0	8	8	-.292589	1/2	1/2	11/2	15/2	.579007				
		1/2	1/2	3/2	3/2	.208073	1/2	1/2	15/2	15/2	.017954				
		1/2	1/2	3/2	5/2	.316228	1	1	2	4	-.530458				
		1/2	1/2	3/2	9/2	.412982	1	1	2	6	.594588				
		1/2	1/2	5/2	5/2	-.066205	1	1	4	4	.137442				
		1/2	1/2	5/2	9/2	.200722	1	1	4	6	.310514				
		1/2	1/2	5/2	11/2	-.248965	1	1	6	6	-.499770				
		1/2	1/2	9/2	9/2	-.213855	3/2	3/2	7/2	7/2	1.00000				
		1/2	1/2	9/2	11/2	-.470499	7	1	0	0	2	5	-.314561		
1/2	1/2	9/2	15/2	-.417578	0	0			2	8	-.355190				
1/2	1/2	11/2	11/2	.015327	0	0			4	4	.230256				
1/2	1/2	11/2	15/2	-.323821	0	0			4	5	.339544				
1/2	1/2	15/2	15/2	-.181456	0	0			4	8	-.216347				
1	1	2	2	-.249716	0	0			5	5	-.127242				

See page 321 for Explanation of Tables

TABLE II. The Transformation Coefficients $D_{(v)t\alpha; J_\lambda J_\mu}^{T_\lambda T_\mu J}$

J	∞	T_λ	T_μ	J_λ	J_μ	D	J	∞	T_λ	T_μ	J_λ	J_μ	D		
$v = 2 \quad t = 0$															
7	1	0	0	5	8	-.508077	7	1	1/2	1/2	9/2	15/2	-.457040		
		0	0	8	8	-.534271			1/2	1/2	11/2	11/2	.252106		
		1/2	1/2	3/2	11/2	-.234738			1/2	1/2	11/2	15/2	-.342545		
		1/2	1/2	3/2	15/2	-.304166			1/2	1/2	15/2	15/2	.436230		
		1/2	1/2	5/2	9/2	-.129181			1	1	2	6	-.471404		
		1/2	1/2	5/2	11/2	-.301642			1	1	4	4	-.259794		
		1/2	1/2	5/2	15/2	.164842			1	1	4	6	-.749656		
		1/2	1/2	9/2	9/2	-.266996			1	1	6	6	-.385099		
		1/2	1/2	9/2	11/2	-.257231			3/2	3/2	7/2	7/2	1.00000		
$v = 2 \quad t = 1$															
2	1	1/2	1/2	3/2	3/2	.232379	4	1	1	0	6	5	-.493150		
		1/2	1/2	3/2	5/2	-.254270			1	0	6	8	-.404270		
		1/2	1/2	5/2	5/2	-.329610			1	1	2	2	-.315869		
		1/2	1/2	5/2	9/2	.315420			1	1	2	4	.049737		
		1/2	1/2	9/2	9/2	.168550			1	1	2	6	-.362372		
		1/2	1/2	9/2	11/2	.467099			1	1	4	4	.335055		
		1/2	1/2	11/2	11/2	-.039376			1	1	4	6	-.756970		
		1/2	1/2	11/2	15/2	.579534			1	1	6	6	.284913		
		1/2	1/2	15/2	15/2	-.298685			3/2	1/2	7/2	3/2	-.443203		
		1	0	2	2	.268621			3/2	1/2	7/2	5/2	.150756		
		1	0	2	4	.376999			3/2	1/2	7/2	9/2	-.637059		
		1	0	4	2	.187044			3/2	1/2	7/2	11/2	.384353		
		1	0	4	4	.369382			3/2	1/2	7/2	15/2	.476731		
		1	0	4	5	.387298			3/2	3/2	7/2	7/2	-1.00000		
		1	0	6	4	-.414039			2	1	0	4	1.00000		
		1	0	6	5	.345525			6	1	1/2	1/2	3/2	9/2	-.293792
		1	0	6	8	.416497			1/2	1/2	3/2	11/2	-.091372		
		1	1	2	2	.295084			1/2	1/2	3/2	15/2	.184144		
		1	1	2	4	-.599319			1/2	1/2	5/2	9/2	.025836		
		1	1	4	4	.047184			1/2	1/2	5/2	11/2	.412325		
1	1	4	6	-.486172	1/2	1/2	5/2	15/2	.247263						
1	1	6	6	-.561384	1/2	1/2	9/2	9/2	-.310565						
3/2	1/2	7/2	3/2	.310530	1/2	1/2	9/2	11/2	.291023						
3/2	1/2	7/2	5/2	.642262	1/2	1/2	9/2	15/2	.076173						
3/2	1/2	7/2	9/2	.340693	1/2	1/2	11/2	11/2	.134402						
3/2	1/2	7/2	11/2	-.612372	1/2	1/2	11/2	15/2	-.459573						
3/2	3/2	7/2	7/2	-1.00000	1/2	1/2	15/2	15/2	-.472644						
2	1	0	2	1.00000	1	0	2	4	-.256776						
4	1	1/2	1/2	3/2	5/2	-.135526	1	0	2	5	-.214286				
		1/2	1/2	3/2	9/2	-.343776	1	0	2	8	.258300				
		1/2	1/2	3/2	11/2	.286039	1	0	4	2	-.188200				
		1/2	1/2	5/2	5/2	.216600	1	0	4	4	-.067049				
		1/2	1/2	5/2	9/2	-.125864	1	0	4	5	.410326				
		1/2	1/2	5/2	11/2	-.274238	1	0	4	8	-.536373				
		1/2	1/2	9/2	9/2	.107158	1	0	6	2	.115248				
		1/2	1/2	9/2	11/2	.064282	1	0	6	4	-.356893				
		1/2	1/2	9/2	15/2	.588078	1	0	6	5	.000000				
		1/2	1/2	11/2	11/2	-.341399	1	0	6	8	.599454				
		1/2	1/2	11/2	15/2	-.242866	1	1	2	4	-.301511				
		1/2	1/2	15/2	15/2	.326621	1	1	2	6	-.492366				
		1	0	2	2	.139414	1	1	4	4	-.445362				
		1	0	2	4	.275321	1	1	4	6	.535256				
		1	0	2	5	-.288675	1	1	6	6	.596593				
		1	0	4	2	-.395822	3/2	1/2	7/2	5/2	-.291937				
		1	0	4	4	-.157631	3/2	1/2	7/2	9/2	.327231				
		1	0	4	5	.000000	3/2	1/2	7/2	11/2	.522233				
		1	0	4	8	-.419070	3/2	1/2	7/2	15/2	-.731413				
		1	0	6	2	-.226188	3/2	3/2	7/2	7/2	-1.00000				
1	0	6	4	-.080582	2	1	0	6	1.00000						
$v = 3 \quad t = 1/2$															
1/2	1	0	1/2	2	3/2	.642857	1/2	1	0	1/2	5	9/2	.543557		
		0	1/2	2	5/2	.197386			0	1/2	5	11/2	.417053		
		0	1/2	4	9/2	.123718			0	1/2	8	15/2	.251157		

See page 321 for Explanation of Tables

TABLE II. The Transformation Coefficients $D_{(v) \alpha; J_N J_\mu}^{T_\lambda T_\mu J}$

J	α	T_λ	T_μ	J_λ	J_μ	D	J	α	T_λ	T_μ	J_λ	J_μ	D				
$v = 3 \quad t = 1/2$																	
1/2	1	1	1/2	2	3/2	-.410326	5/2	2	0	1/2	8	15/2	-.107103				
			1/2	2	5/2	.188982				1/2	2	3/2	.164686				
			1/2	4	9/2	-.868165				1/2	2	5/2	.143566				
			1/2	6	11/2	.205445				1/2	2	9/2	.485730				
3/2	1	1	3/2	4	7/2	-1.00000	7/2	1	0	1/2	4	3/2	.342594				
			0	1/2	2	3/2				.156492	1/2	4	5/2	-.347313			
			0	1/2	2	5/2				.327469	1/2	4	9/2	.087640			
			0	1/2	4	5/2				.407206	1/2	4	11/2	.546594			
			0	1/2	4	9/2				-.510784	1/2	6	9/2	.410584			
			0	1/2	4	11/2				.343776	1/2	6	11/2	.055709			
			0	1/2	5	9/2				.000000	1/2	6	15/2	.014446			
			0	1/2	5	11/2				-.540219	1	3/2	2	7/2	-.541186		
			0	1/2	8	15/2				.177595	1	3/2	4	7/2	.724326		
			1	1/2	2	3/2				-.449489	1	3/2	6	7/2	-.427165		
			1	1/2	2	5/2				.442627	5/2	2	0	1/2	2	3/2	.128022
			1	1/2	4	5/2				.501158				0	1/2	2	5/2
1	1/2	4	9/2	-.028675	0	1/2	2	9/2	.300006								
1	1/2	4	11/2	-.111340	0	1/2	2	11/2	-.321316								
1	1/2	6	9/2	.240523	0	1/2	4	3/2	.277457								
1	1/2	6	11/2	.512946	0	1/2	4	5/2	.071752								
1	1/2	6	15/2	-.129219	0	1/2	4	9/2	.173353								
1	3/2	2	7/2	.886405	0	1/2	4	11/2	.292846								
1	3/2	4	7/2	.462910	0	1/2	4	15/2	-.187119								
5/2	1	0	1/2	2	3/2	.052523	0	1/2	5	3/2				.229571			
			0	1/2	2	5/2	.022220	0	1/2	5				5/2	.343808		
			0	1/2	2	9/2	.117279	0	1/2	5				9/2	-.189422		
			0	1/2	4	3/2	-.030281	0	1/2	5	11/2	-.298236					
			0	1/2	4	5/2	-.177145	0	1/2	5	15/2	-.237198					
			0	1/2	4	9/2	-.050391	0	1/2	8	9/2	.392170					
			0	1/2	4	11/2	-.259238	0	1/2	8	11/2	-.088743					
			0	1/2	5	5/2	.089803	0	1/2	8	15/2	-.003204					
			0	1/2	5	9/2	.269408	1	1/2	2	3/2	-.367714					
			0	1/2	5	11/2	-.247246	1	1/2	2	5/2	-.233346					
			0	1/2	5	15/2	-.212836	1	1/2	2	9/2	.321970					
			0	1/2	8	11/2	-.293828	1	1/2	2	11/2	.000000					
			0	1/2	8	15/2	-.779450	1	1/2	4	3/2	.000000					
			1	1/2	2	3/2	.041144	1	1/2	4	5/2	-.225898					
			1	1/2	2	5/2	-.127646	1	1/2	4	9/2	-.163670					
			1	1/2	2	9/2	-.074857	1	1/2	4	11/2	.388579					
			1	1/2	4	3/2	-.107881	1	1/2	4	15/2	.393921					
			1	1/2	4	5/2	-.057373	1	1/2	6	5/2	.214880					
			1	1/2	4	9/2	.353609	1	1/2	6	9/2	.449493					
			1	1/2	4	11/2	.218298	1	1/2	6	11/2	.078447					
			1	1/2	6	9/2	-.247174	1	1/2	6	15/2	.052493					
			1	1/2	6	11/2	.473361	1	3/2	2	7/2	.391622					
			1	1/2	6	15/2	-.709663	1	3/2	4	7/2	-.812006					
			1	3/2	2	7/2	-.309849	1	3/2	6	7/2	.432757					
1	3/2	4	7/2	-.644008	7/2	2	0	1/2	2	3/2	.011460						
1	3/2	6	7/2	-.699462				0	1/2	2	5/2	.043633					
5/2	2	0	1/2	2				3/2	.398748	0	1/2	2	9/2	-.211397			
			0	1/2				2	5/2	-.344002	0	1/2	2	11/2	.077658		
			0	1/2				2	9/2	-.113403	0	1/2	4	3/2	.042460		
			0	1/2				4	3/2	-.305133	0	1/2	4	5/2	-.066798		
			0	1/2				4	5/2	.101422	0	1/2	4	9/2	.082745		
			0	1/2				4	9/2	-.368648	0	1/2	4	11/2	.396545		
			0	1/2				4	11/2	.037996	0	1/2	4	15/2	-.411928		
			0	1/2				5	5/2	.267359	0	1/2	5	3/2	-.131519		
			0	1/2				5	9/2	.377045	0	1/2	5	5/2	.239798		
			0	1/2				5	11/2	.211769	0	1/2	5	9/2	-.058781		
			0	1/2	5	15/2	.544065	0	1/2	5	11/2	.033429					
			0	1/2	8	11/2	.284117										

See page 321 for Explanation of Tables

TABLE II. The Transformation Coefficients $D_{(v) \alpha; J \lambda J \mu}^{T \lambda T \mu J}$

J	∞	T_λ	T_μ	J_λ	J_μ	D	J	∞	T_λ	T_μ	J_λ	J_μ	D		
$v = 3 \quad t = 1/2$															
7/2	2	0	1/2	5	15/2	.383228	9/2	2	0	1/2	8	15/2	.145861		
		0	1/2	8	9/2	-.365090			1	1/2	2	5/2	-.235100		
		0	1/2	8	11/2	-.492049			1	1/2	2	9/2	-.269039		
		0	1/2	8	15/2	-.074578			1	1/2	2	11/2	-.211380		
		1	1/2	7	3/2	-.032916			1	1/2	4	3/2	-.098222		
		1	1/2	2	5/2	-.164008			1	1/2	4	5/2	-.496050		
		1	1/2	2	9/2	.180893			1	1/2	4	9/2	.070042		
		1	1/2	2	11/2	.305670			1	1/2	4	11/2	-.404061		
		1	1/2	4	3/2	-.273889			1	1/2	4	15/2	.210028		
		1	1/2	4	5/2	-.166252			1	1/2	6	3/2	-.308957		
		1	1/2	4	9/2	.030474			1	1/2	6	5/2	-.230667		
		1	1/2	4	11/2	.034783			1	1/2	6	9/2	.345916		
		1	1/2	4	15/2	-.409864			1	1/2	6	11/2	-.240464		
		1	1/2	6	5/2	.536622			1	1/2	6	15/2	-.183098		
		1	1/2	6	9/2	-.186602			1	3/2	7	7/2	.908514		
		1	1/2	6	11/2	.324578			1	3/2	4	7/2	.113961		
		9/2	1	1	1/2	6			15/2	.380717	1	3/2	6	7/2	-.402015
				1	3/2	2			7/2	.813294	11/2	1	0	1/2	2
1	3/2			4	7/2	.085513	0	1/2	2	11/2			.275264		
1	3/2			6	7/2	-.575535	0	1/2	2	15/2			-.293815		
0	1/2			2	5/2	-.016052	0	1/2	4	3/2			-.220084		
0	1/2			2	9/2	-.121656	0	1/2	4	5/2			-.050316		
0	1/2			2	11/2	.044147	0	1/2	4	9/2			-.061863		
0	1/2			4	3/2	.029738	0	1/2	4	11/2			.197407		
0	1/2			4	5/2	.161395	0	1/2	4	15/2			.028174		
0	1/2			4	9/2	.046268	0	1/2	5	3/2			.102706		
0	1/2			4	11/2	.250232	0	1/2	5	5/2			-.303414		
0	1/2			4	15/2	-.101743	0	1/2	5	9/2			.345945		
0	1/2			5	3/2	.069985	0	1/2	5	11/2			-.044679		
0	1/2			5	5/2	-.095875	0	1/2	5	15/2			-.362606		
0	1/2			5	9/2	-.250232	0	1/2	8	5/2			.150241		
0	1/2			5	11/2	.231511	0	1/2	8	9/2			.474272		
0	1/2			5	15/2	.238268	0	1/2	8	11/2			-.075690		
0	1/2			8	9/2	.178215	0	1/2	8	15/2			.154091		
0	1/2	8	11/2	.330085	1	1/2	2	9/2	.326214						
0	1/2	8	15/2	.743748	1	1/2	2	11/2	.020273						
1	1/2	2	5/2	.092214	1	1/2	2	15/2	-.210980						
1	1/2	2	9/2	.077651	1	1/2	4	3/2	.333590						
1	1/2	2	11/2	.126804	1	1/2	4	5/2	-.094308						
1	1/2	4	3/2	.105946	1	1/2	4	9/2	-.288021						
1	1/2	4	5/2	.052272	1	1/2	4	11/2	.452304						
1	1/2	4	9/2	-.324675	1	1/2	4	15/2	-.296554						
1	1/2	4	11/2	-.210714	1	1/2	6	3/2	-.429092						
1	1/2	4	15/2	-.214187	1	1/2	6	5/2	-.060510						
1	1/2	6	3/2	.000000	1	1/2	6	9/2	-.277606						
1	1/2	6	5/2	-.113094	1	1/2	6	11/2	-.159393						
1	1/2	6	9/2	.240523	1	1/2	6	15/2	-.250506						
1	1/2	6	11/2	-.445866	1	3/2	2	7/2	.370312						
1	1/2	6	15/2	.700216	1	3/2	4	7/2	.887517						
1	3/2	2	7/2	.267261	1	3/2	6	7/2	-.274194						
1	3/2	4	7/2	.581087	11/2	2	0	1/2	2	9/2	-.052410				
1	3/2	6	7/2	.768706			0	1/2	2	11/2	.074978				
9/2	2	0	1/2	2			5/2	-.245554	0	1/2	2	15/2	-.058421		
		0	1/2	2			9/2	.143152	0	1/2	4	3/2	-.095467		
		0	1/2	2			11/2	.305195	0	1/2	4	5/2	.478764		
		0	1/2	4			3/2	-.279942	0	1/2	4	9/2	-.165035		
		0	1/2	4			5/2	.142434	0	1/2	4	11/2	-.140719		
		0	1/2	4			9/2	.421935	0	1/2	4	15/2	-.506220		
		0	1/2	4			11/2	-.039260	0	1/2	5	3/2	-.206845		
		0	1/2	4			15/2	.239440	0	1/2	5	5/2	.080579		
		0	1/2	5			3/2	.267643	0	1/2	5	9/2	.171774		
		0	1/2	5			5/2	.056408	0	1/2	5	11/2	.363385		
		0	1/2	5			9/2	.245373	0	1/2	5	15/2	-.037810		
		0	1/2	5			11/2	-.177072	0	1/2	8	5/2	-.346358		
		0	1/2	5			15/2	.373826	0	1/2	8	9/2	.012246		
		0	1/2	8			9/2	.110677	0	1/2	8	11/2	-.285002		
		0	1/2	8			11/2	-.388410	0	1/2	8	15/2	.181633		

See page 321 for Explanation of Tables

TABLE II. The Transformation Coefficients $D_{(v) \alpha, J, J_\mu}^{T_\lambda T_\mu J}$

J	α	T_λ	T_μ	J_λ	J_μ	D	J	α	T_λ	T_μ	J_λ	J_μ	D		
$v = 3 \quad t = 1/2$															
11/2	2	1	1/2	2	9/2	-.175625	13/2	2	1	1/2	4	5/2	.195629		
		1	1/2	2	11/2	.514445			1	1/2	4	9/2	-.314188		
		1	1/2	2	15/2	.294261			1	1/2	4	11/2	.222373		
		1	1/2	4	3/2	-.066992			1	1/2	4	15/2	-.178254		
		1	1/2	4	5/2	-.306319			1	1/2	6	3/2	-.444498		
		1	1/2	4	9/2	-.150553			1	1/2	6	5/2	.131167		
		1	1/2	4	11/2	.083774			1	1/2	6	9/2	.163348		
		1	1/2	4	15/2	.035550			1	1/2	6	11/2	-.436008		
		1	1/2	6	3/2	-.104856			1	1/2	6	15/2	-.276325		
		1	1/2	6	5/2	-.477637			1	3/2	4	7/2	-.915540		
		1	1/2	6	9/2	-.013390			1	3/2	6	7/2	.402228		
		1	1/2	6	11/2	.483572			15/2	1	0	1/2	2	11/2	.232526
		1	1/2	6	15/2	-.124385					0	1/2	2	15/2	.319023
		1	3/2	2	7/2	.764913					0	1/2	4	9/2	.203255
		1	3/2	4	7/2	-.123868					0	1/2	4	11/2	.262314
		1	3/2	6	7/2	.632112					0	1/2	4	15/2	.044347
13/2	1	0	1/2	2	9/2	-.331555	0	1/2			5	5/2	.243182		
		0	1/2	2	11/2	.120747	0	1/2			5	9/2	.145444		
		0	1/2	2	15/2	.265506	0	1/2			5	11/2	.000000		
		0	1/2	4	5/2	.038104	0	1/2			5	15/2	.446431		
		0	1/2	4	9/2	.244519	0	1/2			8	3/2	-.387298		
		0	1/2	4	11/2	-.179356	0	1/2			8	5/2	-.059372		
		0	1/2	4	15/2	-.222382	0	1/2			8	9/2	.123818		
		0	1/2	5	3/2	.359178	0	1/2			8	11/2	.407534		
		0	1/2	5	5/2	.215894	0	1/2			8	15/2	-.342836		
		0	1/2	5	9/2	.200518	1	1/2			2	11/2	-.222627		
		0	1/2	5	11/2	.302786	1	1/2			2	15/2	-.305441		
		0	1/2	5	15/2	.000000	1	1/2	4	9/2	.178287				
		0	1/2	8	3/2	-.301206	1	1/2	4	11/2	-.235614				
		0	1/2	8	5/2	.233245	1	1/2	4	15/2	-.466791				
		0	1/2	8	9/2	.242987	1	1/2	6	3/2	.228125				
		0	1/2	8	11/2	-.231726	1	1/2	6	5/2	-.234244				
0	1/2	8	15/2	-.311064	1	1/2	6	9/2	.638362						
1	1/2	2	9/2	-.133417	1	1/2	6	11/2	-.167452						
1	1/2	2	11/2	-.299619	1	1/2	6	15/2	.097419						
1	1/2	2	15/2	-.305043	1	3/2	4	7/2	.879049						
1	1/2	4	5/2	.252110	1	3/2	6	7/2	.476731						
1	1/2	4	9/2	.363559	17/2	1	0	1/2	2	15/2	.027804				
1	1/2	4	11/2	.265325			0	1/2	4	9/2	-.101097				
1	1/2	4	15/2	.514972			0	1/2	4	11/2	.302220				
1	1/2	6	3/2	.195283			0	1/2	4	15/2	-.406593				
1	1/2	6	5/2	.085229			0	1/2	5	9/2	.341412				
1	1/2	6	9/2	-.393425			0	1/2	5	11/2	.000000				
1	1/2	6	11/2	-.260512			0	1/2	5	15/2	-.265542				
1	1/2	6	15/2	.000000			0	1/2	8	3/2	-.130410				
1	3/2	4	7/2	.402228			0	1/2	8	5/2	-.364110				
1	3/2	6	7/2	.915540			0	1/2	8	9/2	.135426				
13/2	2	0	1/2	2			9/2	.109373	0	1/2	8	11/2	-.543021		
		0	1/2	2			11/2	.204911	0	1/2	8	15/2	-.287196		
		0	1/2	2			15/2	-.296280	1	1/2	2	15/2	-.479157		
		0	1/2	4			5/2	.278781	1	1/2	4	9/2	.212828		
		0	1/2	4			9/2	.174960	1	1/2	4	11/2	.413550		
		0	1/2	4			11/2	-.204447	1	1/2	4	15/2	-.046268		
		0	1/2	4	15/2	-.289844	1	1/2	6	5/2	-.392709				
		0	1/2	5	3/2	.000000	1	1/2	6	9/2	.052738				
		0	1/2	5	5/2	.167527	1	1/2	6	11/2	-.181818				
		0	1/2	5	9/2	.096979	1	1/2	6	15/2	.601571				
		0	1/2	5	11/2	-.347492	1	3/2	6	7/2	-1.00000				
		0	1/2	5	15/2	.346392	19/2	1	0	1/2	2	15/2	.197386		
		0	1/2	8	3/2	.041169			0	1/2	4	11/2	-.243599		
		0	1/2	8	5/2	.351985			0	1/2	4	15/2	-.134655		
		0	1/2	8	9/2	-.415553			0	1/2	5	9/2	.199900		
		0	1/2	8	11/2	-.197146			0	1/2	5	11/2	.316960		
0	1/2	8	15/2	.093711	0	1/2			5	15/2	.244082				
1	1/2	2	9/2	-.314151	0	1/2			8	3/2	-.207020				
1	1/2	2	11/2	.130791	0	1/2			8	5/2	.178376				
1	1/2	2	15/2	-.397580	0	1/2			8	9/2	.435385				

See page 321 for Explanation of Tables

TABLE II. The Transformation Coefficients $D_{(v) \alpha; J_N J_\mu}^{T_\lambda T_\mu J}$

J	∞	T_λ	T_μ	J_λ	J_μ	D	J	∞	T_λ	T_μ	J_λ	J_μ	D
$v = 3 \quad \dagger = 1/2$													
19/2	1	0	1/2	8	11/2	-.095009	19/2	1	1	1/2	6	9/2	-.312893
		0	1/2	8	15/2	.640550			1	1/2	6	11/2	-.512823
		1	1/2	2	15/2	.188982			1	1/2	6	15/2	.502740
		1	1/2	4	11/2	-.170941			1	3/2	6	7/2	1.000000
		1	1/2	4	15/2	.566947							
$v = 3 \quad \dagger = 3/2$													
3/2	1	0	3/2	2	7/2	.670059	9/2	1	1	1/2	6	9/2	.472132
		0	3/2	4	7/2	-.282120			1	1/2	6	11/2	.312841
		0	3/2	5	7/2	.686607			1	1/2	6	15/2	.081884
		1	1/2	2	3/2	-.346410			1	3/2	2	7/2	.321208
		1	1/2	2	5/2	-.268024			1	3/2	4	7/2	-.805823
		1	1/2	4	5/2	-.191663			1	3/2	6	7/2	.497468
		1	1/2	4	9/2	-.486172			2	1/2	0	9/2	-1.000000
		1	1/2	4	11/2	-.404520	11/2	1	0	3/2	2	7/2	.208063
		1	1/2	6	9/2	-.499350			0	3/2	4	7/2	.597614
		1	1/2	6	11/2	.155302			0	3/2	5	7/2	-.470200
		1	1/2	6	15/2	-.312984			0	3/2	8	7/2	.615206
		1	3/2	2	7/2	.462910			1	1/2	2	9/2	-.284268
		1	3/2	4	7/2	-.886405			1	1/2	2	11/2	.033890
		2	1/2	0	3/2	-1.000000			1	1/2	2	15/2	-.352693
5/2	1	0	3/2	2	7/2	-.154303			1	1/2	4	3/2	-.233550
		0	3/2	4	7/2	.861892			1	1/2	4	5/2	.223915
		0	3/2	5	7/2	.483046			1	1/2	4	9/2	-.052486
		1	1/2	2	3/2	.218841			1	1/2	4	11/2	.394213
		1	1/2	2	5/2	.401189			1	1/2	4	15/2	.198299
		1	1/2	2	9/2	-.271470			1	1/2	6	3/2	.089664
		1	1/2	4	3/2	.156492			1	1/2	6	5/2	-.404617
		1	1/2	4	5/2	-.353706			1	1/2	6	9/2	-.285583
		1	1/2	4	9/2	.145335			1	1/2	6	11/2	-.186519
		1	1/2	4	11/2	-.316663			1	1/2	6	15/2	.450982
		1	1/2	6	9/2	-.035855			1	3/2	2	7/2	-.527046
		1	1/2	6	11/2	.572215			1	3/2	4	7/2	.443813
		1	1/2	6	15/2	.343146			1	3/2	6	7/2	.724743
		1	3/2	2	7/2	.781736			2	1/2	0	11/2	-1.000000
		1	3/2	4	7/2	.246183	15/2	1	0	3/2	4	7/2	.256776
		1	3/2	6	7/2	-.572960			0	3/2	5	7/2	.416497
		2	1/2	0	5/2	-1.000000			0	3/2	8	7/2	-.872122
9/2	1	0	3/2	2	7/2	-.570616			1	1/2	2	11/2	-.305441
		0	3/2	4	7/2	.130209			1	1/2	2	15/2	.222627
		0	3/2	5	7/2	.621059			1	1/2	4	9/2	-.415834
		0	3/2	8	7/2	.521276			1	1/2	4	11/2	.171732
		1	1/2	2	5/2	-.210280			1	1/2	4	15/2	-.326621
		1	1/2	2	9/2	-.158910			1	1/2	6	3/2	-.156492
		1	1/2	2	11/2	.311400			1	1/2	6	5/2	-.210133
		1	1/2	4	3/2	.307482			1	1/2	6	9/2	-.064735
		1	1/2	4	5/2	.112576			1	1/2	6	11/2	.390562
		1	1/2	4	9/2	-.135545			1	1/2	6	15/2	.568047
		1	1/2	4	11/2	.057496			1	3/2	4	7/2	.476731
		1	1/2	4	15/2	.525993			1	3/2	6	7/2	-.879049
		1	1/2	6	3/2	.315817			2	1/2	0	15/2	-1.000000
		1	1/2	6	5/2	-.027773							
$v = 4 \quad \dagger = 0$													
0	1	0	0	2	2	.716476	0	1	1	1	6	6	-.432757
		0	0	4	4	-.614545	0	2	0	0	2	2	-.283904
		0	0	5	5	.283388			0	0	4	4	-.605764
		0	0	8	8	-.169374			0	0	5	5	-.162351
		1/2	1/2	3/2	3/2	.525416			0	0	8	8	.725321
		1/2	1/2	5/2	5/2	-.477750			1/2	1/2	3/2	3/2	-.301007
		1/2	1/2	9/2	9/2	.607090			1/2	1/2	5/2	5/2	-.630486
		1/2	1/2	11/2	11/2	-.303349			1/2	1/2	9/2	9/2	-.078421
		1/2	1/2	15/2	15/2	-.187386			1/2	1/2	11/2	11/2	-.118491
		1	1	2	2	-.391622			1/2	1/2	15/2	15/2	.701208
		1	1	4	4	.812006			1	1	2	2	-.813294

See page 321 for Explanation of Tables

TABLE II. The Transformation Coefficients $D_{(v)\alpha, J, \mu}^{T, T, J}$

J	∞	T_λ	T_μ	J_λ	J_μ	D	J	∞	T_λ	T_μ	J_λ	J_μ	D
$V = 4 \quad \xi = 0$													
0	2	1	1	4	4	-.085513	3	1	0	0	5	5	.000000
		1	1	6	6	.575535			0	0	5	8	-.621582
2	1	0	0	2	2	.052827			0	0	8	8	.000000
		0	0	2	4	-.242811			1/2	1/2	3/2	3/2	.000000
		0	0	4	4	-.284294			1/2	1/2	3/2	5/2	-.452856
		0	0	4	5	.100554			1/2	1/2	3/2	9/2	-.275993
		0	0	5	5	-.091417			1/2	1/2	5/2	5/2	.000000
		0	0	8	8	-.915948			1/2	1/2	5/2	9/2	.153304
		1/2	1/2	3/2	3/2	.025588			1/2	1/2	5/2	11/2	.071306
		1/2	1/2	3/2	5/2	-.164811			1/2	1/2	9/2	9/2	.000000
		1/2	1/2	5/2	5/2	.126144			1/2	1/2	9/2	11/2	.494106
		1/2	1/2	5/2	9/2	-.066307			1/2	1/2	9/2	15/2	.647827
		1/2	1/2	9/2	9/2	-.246002			1/2	1/2	11/2	11/2	.000000
		1/2	1/2	9/2	11/2	-.319127			1/2	1/2	11/2	15/2	.162305
		1/2	1/2	11/2	11/2	-.466306			1/2	1/2	15/2	15/2	.000000
		1/2	1/2	11/2	15/2	-.065991			1	1	2	2	.000000
		1/2	1/2	15/2	15/2	-.753471			1	1	2	4	.228218
		1	1	2	2	-.478714			1	1	4	4	.000000
		1	1	2	4	.117851			1	1	4	6	-.973610
		1	1	4	4	-.575259			1	1	6	6	.000000
		1	1	4	6	.218518	3	2	0	0	2	2	.000000
		1	1	6	6	-.615038			0	0	2	4	.378043
2	2	0	0	2	2	-.011971			0	0	2	5	.035584
		0	0	2	4	.395082			0	0	4	4	.000000
		0	0	4	4	.279607			0	0	4	5	-.693788
		0	0	4	5	-.789110			0	0	5	5	.000000
		0	0	5	5	-.283014			0	0	5	8	.611944
		0	0	8	8	-.250591			0	0	8	8	.000000
		1/2	1/2	3/2	3/2	-.023950			1/2	1/2	3/2	3/2	.000000
		1/2	1/2	3/2	5/2	.554487			1/2	1/2	3/2	5/2	-.459988
		1/2	1/2	5/2	5/2	-.477248			1/2	1/2	3/2	9/2	.271713
		1/2	1/2	5/2	9/2	.314122			1/2	1/2	5/2	5/2	.000000
		1/2	1/2	9/2	9/2	-.232608			1/2	1/2	5/2	9/2	.424033
		1/2	1/2	9/2	11/2	.061152			1/2	1/2	5/2	11/2	-.391118
		1/2	1/2	11/2	11/2	.299132			1/2	1/2	9/2	9/2	.000000
		1/2	1/2	11/2	15/2	-.324171			1/2	1/2	9/2	11/2	.254804
		1/2	1/2	15/2	15/2	-.336333			1/2	1/2	9/2	15/2	-.346225
		1	1	2	2	.755291			1/2	1/2	11/2	11/2	.000000
		1	1	2	4	.192243			1/2	1/2	11/2	15/2	-.443857
		1	1	4	4	-.068977			1/2	1/2	15/2	15/2	.000000
		1	1	4	6	.550639			1	1	2	2	.000000
		1	1	6	6	-.290889			1	1	2	4	.973610
2	3	0	0	2	2	-.355499			1	1	4	4	.000000
		0	0	2	4	.497532			1	1	4	6	.228218
		0	0	4	4	.016389			1	1	6	6	.000000
		0	0	4	5	.494498			1	1	6	6	.000000
		0	0	5	5	-.616073	4	1	0	0	2	2	-.455306
		0	0	8	8	-.041707			0	0	2	5	-.585256
		1/2	1/2	3/2	3/2	-.418057			0	0	4	4	-.041041
		1/2	1/2	3/2	5/2	.287933			0	0	4	5	.182149
		1/2	1/2	5/2	5/2	.097177			0	0	4	8	-.032361
		1/2	1/2	5/2	9/2	-.431152			0	0	5	5	-.382929
		1/2	1/2	9/2	9/2	-.095421			0	0	5	8	-.150840
		1/2	1/2	9/2	11/2	.669335			0	0	8	8	.486874
		1/2	1/2	11/2	11/2	-.282387			1/2	1/2	3/2	5/2	.105936
		1/2	1/2	11/2	15/2	.001109			1/2	1/2	3/2	9/2	.362198
		1/2	1/2	15/2	15/2	-.100640			1/2	1/2	3/2	11/2	.124113
		1	1	2	2	-.032386			1/2	1/2	5/2	5/2	.079674
		1	1	2	4	.693633			1/2	1/2	5/2	9/2	-.077994
		1	1	4	4	.472654			1/2	1/2	5/2	11/2	.144837
		1	1	4	6	-.355220			1/2	1/2	9/2	9/2	.614833
		1	1	6	6	-.410173			1/2	1/2	9/2	11/2	.522318
3	1	0	0	2	2	.000000			1/2	1/2	9/2	15/2	.193866
		0	0	2	4	.493710			1/2	1/2	11/2	11/2	.170566
		0	0	2	5	-.525487			1/2	1/2	11/2	15/2	.287262
		0	0	4	4	.000000			1/2	1/2	15/2	15/2	.093519
		0	0	4	5	-.306186			1	1	2	2	.169682

See page 321 for Explanation of Tables

TABLE II. The Transformation Coefficients $D_{(v) \alpha; J_N J_\mu}^{T_N T_\mu J}$

J	α	T_N	T_μ	J_N	J_μ	D	J	α	T_N	T_μ	J_N	J_μ	D
$v = 4 \quad t = 0$													
4	1	1	1	2	4	-.606500	4	4	0	0	8	8	.006532
		1	1	2	6	.185679			1/2	1/2	3/2	5/2	.033750
		1	1	4	4	-.438434			1/2	1/2	3/2	9/2	.119479
		1	1	4	6	-.517681			1/2	1/2	3/2	11/2	.417219
	2	1	1	6	6	-.329653		1/2	1/2	5/2	5/2	.025384	
		0	0	2	2	.251154		1/2	1/2	5/2	9/2	.441368	
		0	0	2	4	.458488		1/2	1/2	5/2	11/2	-.662675	
		0	0	2	5	.027027		1/2	1/2	9/2	9/2	.225629	
		0	0	4	4	-.631820		1/2	1/2	9/2	11/2	-.171870	
		0	0	4	5	-.418216		1/2	1/2	9/2	15/2	-.243791	
		0	0	4	8	-.171217		1/2	1/2	11/2	11/2	.000000	
		0	0	5	5	-.128628		1/2	1/2	11/2	15/2	.140461	
		0	0	5	8	-.309340		1/2	1/2	15/2	15/2	-.127713	
		0	0	8	8	.101619		1	1	2	2	-.861946	
		1/2	1/2	3/2	5/2	.354634		1	1	2	4	.112549	
		1/2	1/2	3/2	9/2	-.105413		1	1	2	6	-.003710	
		1/2	1/2	3/2	11/2	-.375720		1	1	4	4	-.322493	
		1/2	1/2	5/2	5/2	.266721		1	1	4	6	.089136	
		1/2	1/2	5/2	9/2	-.358482		1	1	6	6	-.363896	
		1/2	1/2	5/2	11/2	-.522795		5	1	0	0	2	4
	1/2	1/2	9/2	9/2	-.123644	0		0		2	5	-.362889	
	1/2	1/2	9/2	11/2	.017607	0		0		4	4	.000000	
	1/2	1/2	9/2	15/2	.160529	0		0		4	5	-.085592	
	1/2	1/2	11/2	11/2	.418089	0		0		4	8	.690567	
	1/2	1/2	11/2	15/2	.160286	0		0		5	5	.000000	
	1/2	1/2	15/2	15/2	-.084473	0		0		5	8	-.562338	
	1	1	2	2	-.073441	0		0		8	8	.000000	
	1	1	2	4	-.617375	1/2		1/2		3/2	9/2	-.218466	
	1	1	2	6	-.643936	1/2		1/2		3/2	11/2	-.382518	
	1	1	4	4	.237255	1/2		1/2		5/2	5/2	.000000	
	1	1	4	6	.352823	1/2		1/2		5/2	9/2	-.078931	
	1	1	6	6	-.134263	1/2		1/2		5/2	11/2	-.211881	
	3	0	0	2	2	.168991		1/2		1/2	5/2	15/2	.605228
		0	0	2	4	-.133378		1/2		1/2	9/2	9/2	.000000
		0	0	2	5	.112409		1/2		1/2	9/2	11/2	.262071
		0	0	4	4	-.058647		1/2	1/2	9/2	15/2	-.283343	
		0	0	4	5	.485139		1/2	1/2	11/2	11/2	.000000	
		0	0	4	8	.319756		1/2	1/2	11/2	15/2	.489452	
		0	0	5	5	.474385		1/2	1/2	15/2	15/2	.000000	
		0	0	5	8	-.483702		1	1	2	4	.000000	
0		0	8	8	.375453	1	1	2	6	.886405			
1/2		1/2	3/2	5/2	-.233945	1	1	4	4	.000000			
1/2		1/2	3/2	9/2	-.443233	1	1	4	6	.462910			
1/2		1/2	3/2	11/2	-.066513	1	1	6	6	.000000			
1/2		1/2	5/2	5/2	-.175950	5	2	0	0	2	4	.492366	
1/2		1/2	5/2	9/2	.190486	0		0	2	5	.369274		
1/2		1/2	5/2	11/2	-.034792	0		0	4	4	.000000		
1/2		1/2	9/2	9/2	-.208766	0		0	4	5	.452911		
1/2	1/2	9/2	11/2	.270998	0	0		4	8	.609023			
1/2	1/2	9/2	15/2	-.026975	0	0		5	5	.000000			
1/2	1/2	11/2	11/2	-.034450	0	0		5	8	.212544			
1/2	1/2	11/2	15/2	.714765	0	0		8	8	.000000			
1/2	1/2	15/2	15/2	.214732	1/2	1/2		3/2	9/2	.082572			
1	1	2	2	-.016202	1/2	1/2		3/2	11/2	.389249			
1	1	2	4	-.006144	1/2	1/2		5/2	5/2	.000000			
1	1	2	6	.351065	1/2	1/2		5/2	9/2	.626497			
1	1	4	4	.704677	1/2	1/2		5/2	11/2	-.215610			
1	1	4	6	-.079824	1/2	1/2		5/2	15/2	.400320			
1	1	6	6	-.611156	1/2	1/2		9/2	9/2	.000000			
4	4	0	0	2	2	-.215387		1/2	1/2	9/2	11/2	-.416025	
		0	0	2	4	-.462725	1/2	1/2	9/2	15/2	.187414		
		0	0	2	5	-.257437	1/2	1/2	11/2	11/2	.000000		
		0	0	4	4	-.345904	1/2	1/2	11/2	15/2	.184996		
		0	0	4	5	-.273494	1/2	1/2	15/2	15/2	.000000		
		0	0	4	8	.518935	1	1	2	4	-.887625		
		0	0	5	5	.267917	1	1	2	6	.213201		
		0	0	5	8	-.371023	1	1	4	4	.000000		

See page 321 for Explanation of Tables

TABLE II. The Transformation Coefficients $D_{(vt)\alpha_i J_i J_\mu}^{T_i T_\mu J}$

J	α	T_i	T_μ	J_i	J_μ	D	J	α	T_i	T_μ	J_i	J_μ	D			
$v = 4 \quad t = 0$																
5	2	1	1	4	6	-.408248	6	3	1/2	1/2	5/2	11/2	-.002833			
		1	1	6	6	.000000			1/2	1/2	5/2	15/2	-.287886			
6	1	0	0	2	4	.107787	1/2	1/2	9/2	9/2	-.058880					
		0	0	2	5	-.305615	1/2	1/2	9/2	11/2	-.078979					
		0	0	2	8	-.268062	1/2	1/2	9/2	15/2	.119022					
		0	0	4	4	.073412	1/2	1/2	11/2	11/2	-.344305					
		0	0	4	5	.280975	1/2	1/2	11/2	15/2	-.670650					
		0	0	4	8	-.005598	1/2	1/2	15/2	15/2	.150033					
		0	0	5	5	-.022154	1	1	2	4	.141487					
		0	0	5	8	-.472458	1	1	2	6	.127976					
		0	0	8	8	-.717669	1	1	4	4	-.035241					
		1/2	1/2	3/2	9/2	-.172844	1	1	4	6	-.783090					
		1/2	1/2	3/2	11/2	-.022122	1	1	6	6	.590875					
		1/2	1/2	3/2	15/2	.064868	6	4	0	0	2	4	-.158039			
		1/2	1/2	5/2	9/2	.123102			0	0	2	5	.440570			
		1/2	1/2	5/2	11/2	-.077865			0	0	2	8	.510380			
		1/2	1/2	5/2	15/2	.177867			0	0	4	4	-.181219			
		1/2	1/2	9/2	9/2	-.199040			0	0	4	5	.252829			
1/2	1/2	9/2	11/2	-.240192	0	0			4	8	.059615					
1/2	1/2	9/2	15/2	-.540995	0	0			5	5	-.297647					
1/2	1/2	11/2	11/2	.363601	0	0			5	8	-.572224					
1/2	1/2	11/2	15/2	-.355626	0	0			8	8	.063894					
1/2	1/2	15/2	15/2	.513726	1/2	1/2			3/2	9/2	.367291					
1	1	2	4	.018729	1/2	1/2			3/2	11/2	-.545673					
1	1	2	6	-.579197	1/2	1/2			3/2	15/2	-.353882					
1	1	4	4	-.420160	1/2	1/2			5/2	9/2	-.153287					
1	1	4	6	-.465278	1/2	1/2			5/2	11/2	-.019008					
1	1	6	6	-.520733	1/2	1/2			5/2	15/2	.332926					
6	2	0	0	2	4	.502984			1/2	1/2	9/2	9/2	-.250079			
		0	0	2	5	-.059964	1/2	1/2	9/2	11/2	.325465					
		0	0	2	8	.251364	1/2	1/2	9/2	15/2	.174953					
		0	0	4	4	-.030650	1/2	1/2	11/2	11/2	.204659					
		0	0	4	5	.187338	1/2	1/2	11/2	15/2	.109110					
		0	0	4	8	.122881	1/2	1/2	15/2	15/2	.233543					
		0	0	5	5	-.624385	1	1	2	4	-.916569					
		0	0	5	8	.447003	1	1	2	6	.016698					
		0	0	8	8	-.198557	1	1	4	4	.307510					
		1/2	1/2	3/2	9/2	.356086	1	1	4	6	-.240605					
		1/2	1/2	3/2	11/2	-.232284	1	1	6	6	-.084676					
		1/2	1/2	3/2	15/2	.185869	7	1	0	0	2	5	-.383982			
		1/2	1/2	5/2	9/2	.381066			0	0	2	8	-.667042			
		1/2	1/2	5/2	11/2	.281011			0	0	4	4	.000000			
		1/2	1/2	5/2	15/2	.042447			0	0	4	5	-.512061			
		1/2	1/2	9/2	9/2	.159790			0	0	4	8	.184065			
1/2	1/2	9/2	11/2	-.561314	0	0			5	5	.000000					
1/2	1/2	9/2	15/2	.404509	0	0			5	8	-.333957					
1/2	1/2	11/2	11/2	.123904	0	0			8	8	.000000					
1/2	1/2	11/2	15/2	-.196261	1/2	1/2			3/2	11/2	-.427153					
1/2	1/2	15/2	15/2	.024809	1/2	1/2			3/2	15/2	-.489143					
1	1	2	4	.220507	1/2	1/2			5/2	9/2	.259729					
1	1	2	6	-.636750	1/2	1/2			5/2	11/2	.168412					
1	1	4	4	.727540	1/2	1/2			5/2	15/2	-.126907					
1	1	4	6	.000289	1/2	1/2			9/2	9/2	.000000					
1	1	6	6	.128887	1/2	1/2			9/2	11/2	-.373566					
6	3	0	0	2	4	-.206238			1/2	1/2	9/2	15/2	-.567052			
		0	0	2	5	.370573	1/2	1/2	11/2	11/2	.000000					
		0	0	2	8	.081839	1/2	1/2	11/2	15/2	.072467					
		0	0	4	4	.300654	1/2	1/2	15/2	15/2	.000000					
		0	0	4	5	-.292539	1	1	2	6	.088359					
		0	0	4	8	-.653930	1	1	4	4	.000000					
		0	0	5	5	-.158298	1	1	4	6	-.996089					
		0	0	5	8	.160484	1	1	6	6	.000000					
		0	0	8	8	-.398790	7	2	0	0	2	5	-.031314			
		1/2	1/2	3/2	9/2	.192605			0	0	2	8	.329844			
		1/2	1/2	3/2	11/2	.068038			0	0	4	4	.000000			
		1/2	1/2	3/2	15/2	-.265980			0	0	4	5	-.542647			
		1/2	1/2	5/2	9/2	-.435827			0	0	4	8	-.568203			

See page 321 for Explanation of Tables

TABLE II. The Transformation Coefficients $D_{(v) \alpha; J \lambda \mu}^{T_\lambda T_\mu J}$

J	α	T_λ	T_μ	J_λ	J_μ	D	J	α	T_λ	T_μ	J_λ	J_μ	D		
$v = 4 \quad \dagger = 0$															
7	2	0	0	5	5	.000000	8	3	0	0	8	8	.135498		
		0	0	5	8	.522400			1/2	1/2	3/2	15/2	.090745		
	0	0	8	8	.000000	1/2		1/2	5/2	11/2	-.448647				
	1/2	1/2	3/2	11/2	-.034855	1/2		1/2	5/2	15/2	.599628				
	1/2	1/2	3/2	15/2	-.361437	1/2		1/2	9/2	9/2	-.061169				
	1/2	1/2	5/2	9/2	.297143	1/2		1/2	9/2	11/2	-.169410				
	1/2	1/2	5/2	11/2	.475695	1/2		1/2	9/2	15/2	.027992				
	1/2	1/2	5/2	15/2	-.480301	1/2		1/2	11/2	11/2	-.597742				
	1/2	1/2	9/2	9/2	.000000	1/2		1/2	11/2	15/2	.165842				
	1/2	1/2	9/2	11/2	-.186023	1/2		1/2	15/2	15/2	.113598				
	1/2	1/2	9/2	15/2	.280400	1		1	2	6	.809961				
	1/2	1/2	11/2	11/2	.000000	1		1	4	4	-.246001				
	1/2	1/2	11/2	15/2	.457877	1		1	4	6	.164020				
	1/2	1/2	15/2	15/2	.000000	1		1	6	6	-.506502				
8	1	1	1	2	6	.996089	9	1	0	0	2	8	-.338062		
		1	1	4	4	.000000			0	0	4	5	.491689		
		1	1	4	6	.088359		0	0	4	8	.385450			
		1	1	6	6	.000000		0	0	5	5	.000000			
		0	0	2	8	.172077		0	0	5	8	-.703836			
		0	0	4	4	-.092102		0	0	8	8	.000000			
		0	0	4	5	-.196094		1/2	1/2	3/2	15/2	-.443203			
		0	0	4	8	.186256		1/2	1/2	5/2	15/2	-.288675			
		0	0	5	5	.093197		1/2	1/2	9/2	9/2	.000000			
		0	0	5	8	.524980		1/2	1/2	9/2	11/2	-.602194			
		0	0	8	8	.777478		1/2	1/2	9/2	15/2	.170941			
		1/2	1/2	3/2	15/2	.130931		1/2	1/2	11/2	11/2	.000000			
		1/2	1/2	5/2	11/2	.125054		1/2	1/2	11/2	15/2	-.573045			
		1/2	1/2	5/2	15/2	-.105375		1/2	1/2	15/2	15/2	.000000			
1/2	1/2	9/2	9/2	.173759	1	1	4	6	1.000000						
1/2	1/2	9/2	11/2	.208993	1	1	6	6	.000000						
1/2	1/2	9/2	15/2	.470903	10	1	0	0	2	8	.519099				
1/2	1/2	11/2	11/2	-.244579			0	0	4	8	-.489415				
1/2	1/2	11/2	15/2	.413315		0	0	5	5	-.515079					
1/2	1/2	15/2	15/2	-.655627		0	0	5	8	.145545					
1	1	2	6	.239046		0	0	8	8	-.452240					
1	1	4	4	.152120		1/2	1/2	5/2	15/2	-.316136					
1	1	4	6	.778246		1/2	1/2	9/2	11/2	-.295201					
1	1	6	6	.560401		1/2	1/2	9/2	15/2	-.677731					
8	2	0	0	2		8	-.687017	1/2	1/2	11/2	11/2	.302220			
		0	0	4		4	-.059098	1/2	1/2	11/2	15/2	.486835			
	0	0	4	5		.275466	1/2	1/2	15/2	15/2	.158901				
	0	0	4	8		-.001631	1	1	4	6	.442498				
	0	0	5	5		.374538	1	1	6	6	.896770				
	0	0	5	8		.523996	10	2	0	0	2	8	-.247532		
	0	0	8	8	-.183794	0			0	4	8	-.689984			
	1/2	1/2	3/2	15/2	.620755	0		0	5	5	.000000				
	1/2	1/2	5/2	11/2	.198243	0		0	5	8	-.628388				
	1/2	1/2	5/2	15/2	-.003690	0		0	8	8	.260343				
	1/2	1/2	9/2	9/2	.456590	1/2		1/2	5/2	15/2	-.549157				
	1/2	1/2	9/2	11/2	-.398903	1/2		1/2	9/2	11/2	-.265892				
	1/2	1/2	9/2	15/2	-.379314	1/2		1/2	9/2	15/2	.597172				
	1/2	1/2	11/2	11/2	-.086727	1/2		1/2	11/2	11/2	-.214369				
1/2	1/2	11/2	15/2	-.153798	1/2	1/2		11/2	15/2	.337812					
1/2	1/2	15/2	15/2	-.180821	1/2	1/2		15/2	15/2	.333231					
1	1	2	6	-.357896	1	1		4	6	-.896770					
1	1	4	4	-.878473	1	1		6	6	.442498					
1	1	4	6	.313440	12	1		0	0	4	8	.359487			
1	1	6	6	-.044159			0	0	5	8	-.545108				
8	3	0	0	2		8	-.100429	0	0	8	8	-.757381			
		0	0	4		4	-.542579	1/2	1/2	9/2	15/2	-.312893			
	0	0	4	5		.040268	1/2	1/2	11/2	15/2	.711684				
	0	0	4	8		-.742820	1/2	1/2	15/2	15/2	-.628971				
	0	0	5	5		-.343355	1	1	6	6	-1.000000				
	0	0	5	8		.076599	$v = 4 \quad \dagger = 1$								
	1	1	1/2	1/2		3/2	3/2	-.183095	1	1	1/2	1/2	3/2	5/2	.164317

See page 321 for Explanation of Tables

TABLE II. The Transformation Coefficients $D_{(v)\alpha, J, J_\lambda, J_\mu}^{T_\lambda, T_\mu, J}$

J	α	T_λ	T_μ	J_λ	J_μ	D	J	α	T_λ	T_μ	J_λ	J_μ	D				
$v = 4 \quad \dagger = 1$																	
1	1	1/2	1/2	5/2	5/2	.206302	2	2	1	0	4	2	.109646				
		1/2	1/2	9/2	9/2	-.480201			1	0	4	4	.216534				
		1/2	1/2	9/2	11/2	-.712492			1	0	4	5	-.151358				
		1/2	1/2	11/2	11/2	-.202309			1	0	6	4	-.638243				
		1/2	1/2	15/2	15/2	.343146			1	0	6	5	.195047				
		1	0	2	2	-.207020			1	0	6	8	-.651073				
		1	0	4	4	-.545108			1	1	2	2	.000000				
		1	0	4	5	-.552679			1	1	2	4	.808290				
		1	0	6	5	-.595437			1	1	4	4	.000000				
		1	1	2	2	-.528550			1	1	4	6	.588784				
		1	1	4	4	-.676763			1	1	6	6	.000000				
		1	1	6	6	.512471			3/2	1/2	7/2	3/2	-.194202				
		3/2	1/2	7/2	5/2	.821584			3/2	1/2	7/2	5/2	-.675525				
		3/2	1/2	7/2	9/2	.570088			3/2	1/2	7/2	9/2	.261489				
		3/2	1/2	7/2	11/2	.428786			3/2	1/2	7/2	11/2	-.661495				
		1	2	1/2	1/2	3/2			3/2	.684105	3	1	1/2	1/2	3/2	3/2	.291302
				1/2	1/2	5/2			5/2	.048617			1/2	1/2	3/2	5/2	-.080563
				1/2	1/2	9/2			9/2	.276817			1/2	1/2	3/2	9/2	.240906
1/2	1/2			9/2	11/2	.076060	1/2	1/2	5/2	5/2			-.144180				
1/2	1/2			11/2	11/2	-.498078	1/2	1/2	5/2	9/2			.264443				
1/2	1/2			15/2	15/2	.123631	1/2	1/2	5/2	11/2			.041494				
1	0			2	2	.574594	1/2	1/2	9/2	9/2			.319641				
1	0			4	4	-.523723	1/2	1/2	9/2	11/2			.237341				
1	0			4	5	.575247	1/2	1/2	9/2	15/2			-.073946				
1	0			6	5	-.254257	1/2	1/2	11/2	11/2			-.005109				
1	1			2	2	-.825198	1/2	1/2	11/2	15/2			.462119				
1	1			4	4	.551268	1/2	1/2	15/2	15/2			-.616950				
1	1			6	6	-.123092	1	0	2	2			.039501				
3/2	1/2			7/2	5/2	.570088	1	0	2	4			.076095				
3/2	1/2			7/2	9/2	-.821584	1	0	2	5			-.125988				
3/2	1/2			7/2	11/2	.000000	1	0	4	2			-.144436				
2	1			1/2	1/2	3/2	5/2	-.545108	3	2			1	0	4	4	.352453
				1/2	1/2	5/2	5/2	.000000					1	0	4	5	.526207
		1/2	1/2	5/2	9/2	-.457738	1	0			6	4	-.270148				
		1/2	1/2	9/2	9/2	.000000	1	0			6	5	.507479				
		1/2	1/2	9/2	11/2	.677855	1	0			6	8	.473586				
		1/2	1/2	11/2	11/2	.000000	1	1			2	2	.026696				
		1/2	1/2	11/2	15/2	.183973	1	1			2	4	-.104561				
		1/2	1/2	15/2	15/2	.000000	1	1			4	4	-.557582				
		1	0	2	2	-.624500	1	1			4	6	-.094621				
		1	0	2	4	.247207	1	1			6	6	-.817621				
		1	0	4	2	-.289897	3/2	1/2			7/2	3/2	-.449489				
		1	0	4	4	.528463	3/2	1/2			7/2	5/2	-.455420				
		1	0	4	5	.042876	3/2	1/2			7/2	9/2	-.208360				
		1	0	6	4	-.049363	3/2	1/2			7/2	11/2	.739688				
		1	0	6	5	-.414885	1/2	1/2			3/2	3/2	.400588				
		1	0	6	8	.095764	1/2	1/2			3/2	5/2	-.070680				
		1	1	2	2	.000000	1/2	1/2			3/2	9/2	.101934				
		1	1	2	4	.588784	1/2	1/2			5/2	5/2	.478714				
1	1	4	4	.000000	1/2	1/2	5/2	9/2	.431828								
1	1	4	6	-.808290	1/2	1/2	5/2	11/2	.332648								
1	1	6	6	.000000	1/2	1/2	9/2	9/2	.185967								
3/2	1/2	7/2	3/2	.742679	1/2	1/2	9/2	11/2	.075516								
3/2	1/2	7/2	5/2	-.325832	1/2	1/2	9/2	15/2	.260760								
3/2	1/2	7/2	9/2	.495729	1/2	1/2	11/2	11/2	-.085776								
3/2	1/2	7/2	11/2	.310669	1/2	1/2	11/2	15/2	-.408962								
2	2	1/2	1/2	3/2	3/2	.000000	1/2	1/2	15/2	15/2	.122298						
		1/2	1/2	3/2	5/2	-.080178	1	0	2	2	.124897						
		1/2	1/2	5/2	5/2	.000000	1	0	2	4	-.316228						
		1/2	1/2	5/2	9/2	-.424366	1	0	2	5	-.618765						
		1/2	1/2	9/2	9/2	.000000	1	0	4	2	-.301965						
		1/2	1/2	9/2	11/2	-.108012	1	0	4	4	.281876						
		1/2	1/2	11/2	11/2	.000000	1	0	4	5	.256752						
		1/2	1/2	11/2	15/2	-.895443	1	0	6	4	.341720						
		1/2	1/2	15/2	15/2	.000000	1	0	6	5	-.363405						
		1	0	2	2	-.128307	1	0	6	8	-.127031						
		1	0	2	4	-.180073	1	1	2	2	.532916						

See page 321 for Explanation of Tables

TABLE II. The Transformation Coefficients $D_{(v) \alpha, J \lambda}^{T, T, J}$

J	∞	T_r	T_{μ}	J_r	J_{μ}	D	J	∞	T_r	T_{μ}	J_r	J_{μ}	D		
$v = 4 \quad t = 1$															
3	2	1	1	2	4	.390282	3	4	3/2	1/2	7/2	11/2	-.187180		
		1	1	4	4	-.500053			4	1	1/2	1/2	3/2	5/2	.459616
		1	1	4	6	-.430395			1/2	1/2	3/2	9/2	-.560582		
		1	1	6	6	.358313			1/2	1/2	3/2	11/2	.116143		
		3/2	1/2	7/2	3/2	.061133			1/2	1/2	5/2	5/2	.000000		
		3/2	1/2	7/2	5/2	.354431			1/2	1/2	5/2	9/2	.180954		
	3	3	3/2	1/2	7/2	9/2		.799760	1/2	1/2	5/2	11/2	.034165		
			3/2	1/2	7/2	11/2		.480650	1/2	1/2	9/2	9/2	.000000		
			1/2	1/2	3/2	3/2		-.174260	1/2	1/2	9/2	11/2	.475928		
			1/2	1/2	3/2	5/2		.025647	1/2	1/2	9/2	15/2	-.260038		
			1/2	1/2	3/2	9/2		-.196636	1/2	1/2	11/2	11/2	.000000		
			1/2	1/2	5/2	5/2		.268413	1/2	1/2	11/2	15/2	-.564655		
1/2			1/2	5/2	9/2	.195627	1/2	1/2	15/2	15/2	.000000				
1/2			1/2	5/2	11/2	.419758	1	0	2	2	-.298410				
1/2			1/2	9/2	9/2	-.414309	1	0	2	4	-.035441				
1/2		1/2	9/2	11/2	.175532	1	0	2	5	-.232944					
1/2		1/2	9/2	15/2	-.410116	1	0	4	2	.092426					
1/2		1/2	11/2	11/2	.491562	1	0	4	4	.320887					
1/2		1/2	11/2	15/2	.068465	1	0	4	5	-.696247					
1/2		1/2	15/2	15/2	-.163815	1	0	4	8	-.164064					
1		0	2	2	.118001	1	0	6	2	-.443034					
1		0	2	4	-.362385	1	0	6	4	-.091463					
1		0	2	5	-.026659	1	0	6	5	.113811					
1		0	4	2	.510764	1	0	6	8	.121024					
1	0	4	4	.208689	1	1	2	2	.000000						
1	0	4	5	-.320509	1	1	2	4	.996259						
1	0	6	4	.437954	1	1	2	6	-.070727						
1	0	6	5	.156237	1	1	4	4	.000000						
1	0	6	8	.480282	1	1	4	6	.049659						
1	1	2	2	.807877	1	1	6	6	.000000						
1	1	2	4	-.077708	3/2	1/2	7/2	3/2	.632333						
1	1	4	4	.237353	3/2	1/2	7/2	5/2	.476267						
1	1	4	6	.501264	3/2	1/2	7/2	9/2	-.524374						
1	1	6	6	-.183559	3/2	1/2	7/2	11/2	.055956						
3/2	1/2	7/2	5/2	.345513	3/2	1/2	7/2	15/2	-.308586						
3/2	1/2	7/2	5/2	.616988	4	2	1/2	1/2	3/2	5/2	.349091				
3/2	1/2	7/2	9/2	-.559594	1/2	1/2	3/2	9/2	.028451						
3/2	1/2	7/2	11/2	.432204	1/2	1/2	3/2	11/2	-.438204						
3	4	1/2	1/2	3/2	3/2	.050703	1/2	1/2	5/2	5/2	.000000				
		1/2	1/2	3/2	5/2	-.253192	1/2	1/2	5/2	9/2	-.507593				
		1/2	1/2	3/2	9/2	.100636	1/2	1/2	5/2	11/2	-.542646				
		1/2	1/2	5/2	5/2	-.002689	1/2	1/2	9/2	9/2	.000000				
		1/2	1/2	5/2	9/2	-.414677	1/2	1/2	9/2	11/2	-.225375				
		1/2	1/2	5/2	11/2	.364007	1/2	1/2	9/2	15/2	-.099425				
		1/2	1/2	9/2	9/2	.429859	1/2	1/2	11/2	11/2	.000000				
		1/2	1/2	9/2	11/2	-.500938	1/2	1/2	11/2	15/2	-.269276				
		1/2	1/2	9/2	15/2	-.045986	1/2	1/2	15/2	15/2	.000000				
		1/2	1/2	11/2	11/2	.415152	1	0	2	2	.439040				
		1/2	1/2	11/2	15/2	-.060699	1	0	2	4	-.411196				
		1/2	1/2	15/2	15/2	-.069727	1	0	2	5	-.385355				
	1	0	2	2	-.407670	1	0	4	2	-.117580					
	1	0	2	4	-.376561	1	0	4	4	.541700					
	1	0	2	5	.092103	1	0	4	5	.165968					
	1	0	4	2	-.451627	1	0	4	8	.138988					
	1	0	4	4	-.322077	1	0	6	2	-.096205					
	1	0	4	5	-.032677	1	0	6	4	.285380					
	1	0	6	4	.357446	1	0	6	5	.081093					
	1	0	6	5	.492502	1	0	6	8	-.195615					
	1	0	6	8	-.066579	1	1	2	2	.000000					
	1	1	2	2	.016263	1	1	2	4	-.086311					
	1	1	2	4	-.747395	1	1	2	6	-.785560					
	1	1	4	4	-.480098	1	1	4	4	.000000					
1	1	4	6	.230573	1	1	4	6	.612736						
1	1	6	6	.396834	1	1	6	6	.000000						
3/2	1/2	7/2	3/2	-.821488	3/2	1/2	7/2	3/2	-.056273						
3/2	1/2	7/2	5/2	.535067	3/2	1/2	7/2	5/2	.544245						
3/2	1/2	7/2	9/2	-.061839	3/2	1/2	7/2	9/2	.524334						

See page 321 for Explanation of Tables

TABLE II. The Transformation Coefficients $D_{(v) \alpha; J \mu}^{T \lambda T \mu J}$

J	α	T_λ	T_μ	λ	μ	D	J	α	T_λ	T_μ	λ	μ	D
$V = 4 \quad \xi = 1$													
4	2	3/2	1/2	7/2	11/2	.650668	5	1	3/2	1/2	7/2	15/2	-.516621
		3/2	1/2	7/2	15/2	-.048336	5	2	1/2	1/2	3/2	9/2	.123846
4	3	1/2	1/2	3/2	5/2	.041354			1/2	1/2	3/2	11/2	-.089770
		1/2	1/2	3/2	9/2	.239742			1/2	1/2	5/2	5/2	.060954
		1/2	1/2	3/2	11/2	-.325848			1/2	1/2	5/2	9/2	-.103782
		1/2	1/2	5/2	5/2	.000000			1/2	1/2	5/2	11/2	-.064150
		1/2	1/2	5/2	9/2	.079862			1/2	1/2	5/2	15/2	-.265109
		1/2	1/2	5/2	11/2	.269063			1/2	1/2	9/2	9/2	.125659
		1/2	1/2	9/2	9/2	.000000			1/2	1/2	9/2	11/2	-.512961
		1/2	1/2	9/2	11/2	-.007598			1/2	1/2	9/2	15/2	-.059030
		1/2	1/2	9/2	15/2	-.837802			1/2	1/2	11/2	11/2	-.194342
		1/2	1/2	11/2	11/2	.000000			1/2	1/2	11/2	15/2	.522684
		1/2	1/2	11/2	15/2	.232151			1/2	1/2	15/2	15/2	.542538
		1/2	1/2	15/2	15/2	.000000			1	0	2	4	.168457
		1	0	2	2	.040518			1	0	2	5	.218032
		1	0	2	4	-.042078			1	0	4	2	.043991
		1	0	2	5	.142323			1	0	4	4	.176267
		1	0	4	2	-.350741			1	0	4	5	-.195292
		1	0	4	4	-.047227			1	0	4	8	.342739
		1	0	4	5	-.026112			1	0	6	2	-.204204
		1	0	4	8	.650176			1	0	6	4	.327611
		1	0	6	2	-.404489			1	0	6	5	.212159
		1	0	6	4	-.099800			1	0	6	8	-.755820
		1	0	6	5	-.400426			1	1	2	4	.562250
		1	0	6	8	.306202			1	1	2	6	.009467
		1	1	2	2	.000000			1	1	4	4	.484429
		1	1	2	4	.004327			1	1	4	6	-.263671
		1	1	2	6	.614730			1	1	6	6	-.616110
		1	1	4	4	.000000			3/2	1/2	7/2	3/2	-.287572
		1	1	4	6	.788726			3/2	1/2	7/2	5/2	.030415
		1	1	6	6	.000000			3/2	1/2	7/2	9/2	.246749
		3/2	1/2	7/2	3/2	.607953			3/2	1/2	7/2	11/2	.622518
		3/2	1/2	7/2	5/2	-.144591			3/2	1/2	7/2	15/2	-.684079
		3/2	1/2	7/2	9/2	.166668	5	3	1/2	1/2	3/2	9/2	-.310487
		3/2	1/2	7/2	11/2	.095426			1/2	1/2	3/2	11/2	-.548289
		3/2	1/2	7/2	15/2	.756704			1/2	1/2	5/2	5/2	-.036900
5	1	1/2	1/2	3/2	9/2	-.089153			1/2	1/2	5/2	9/2	-.039353
		1/2	1/2	3/2	11/2	.004289			1/2	1/2	5/2	11/2	.179594
		1/2	1/2	5/2	5/2	-.300976			1/2	1/2	5/2	15/2	.031973
		1/2	1/2	5/2	9/2	-.248593			1/2	1/2	9/2	9/2	-.381614
		1/2	1/2	5/2	11/2	-.450445			1/2	1/2	9/2	11/2	-.341819
		1/2	1/2	5/2	15/2	.367272			1/2	1/2	9/2	15/2	.359984
		1/2	1/2	9/2	9/2	.208063			1/2	1/2	11/2	11/2	-.210378
		1/2	1/2	9/2	11/2	.185655			1/2	1/2	11/2	15/2	.094688
		1/2	1/2	9/2	15/2	.296696			1/2	1/2	15/2	15/2	-.348581
		1/2	1/2	11/2	11/2	-.618684			1	0	2	4	.315806
		1/2	1/2	11/2	15/2	-.203816			1	0	2	5	.207460
		1/2	1/2	15/2	15/2	.303363			1	0	4	2	-.238871
		1	0	2	4	.374136			1	0	4	4	.296017
		1	0	2	5	-.466664			1	0	4	5	.559248
		1	0	4	2	-.164515			1	0	4	8	-.218467
		1	0	4	4	.084761			1	0	6	2	-.513588
		1	0	4	5	-.134710			1	0	6	4	-.159293
		1	0	4	8	-.265589			1	0	6	5	.237604
		1	0	6	2	.049103			1	0	6	8	.080331
		1	0	6	4	-.454836			1	1	2	4	.127050
		1	0	6	5	-.336830			1	1	2	6	.071465
		1	0	6	8	-.443364			1	1	4	4	.713593
		1	1	2	4	-.011056			1	1	4	6	.506733
		1	1	2	6	.629063			1	1	6	6	.461257
		1	1	4	4	.147405			3/2	1/2	7/2	3/2	-.756417
		1	1	4	6	-.653028			3/2	1/2	7/2	5/2	.516095
		1	1	6	6	.394948			3/2	1/2	7/2	9/2	.243528
		3/2	1/2	7/2	3/2	.419570			3/2	1/2	7/2	11/2	-.243104
		3/2	1/2	7/2	5/2	.424470			3/2	1/2	7/2	15/2	.207542
		3/2	1/2	7/2	9/2	.322424	5	4	1/2	1/2	3/2	9/2	-.300627
		3/2	1/2	7/2	11/2	-.522428			1/2	1/2	3/2	11/2	.078979

See page 321 for Explanation of Tables

TABLE II. The Transformation Coefficients $D_{(v) \alpha; J \lambda J_{\mu}}^{T_{\lambda} T_{\mu} J}$

J	α	T_{λ}	T_{μ}	J_{λ}	J_{μ}	D	J	α	T_{λ}	T_{μ}	J_{λ}	J_{μ}	D
$v = 4 \quad t = 1$													
5	4	1/2	1/2	5/2	5/2	.336304	6	2	1/2	1/2	5/2	15/2	.537241
		1/2	1/2	5/2	9/2	.331777			1/2	1/2	9/2	9/2	.000000
		1/2	1/2	5/2	11/2	-.244940			1/2	1/2	9/2	11/2	-.489846
		1/2	1/2	5/2	15/2	-.176184			1/2	1/2	9/2	15/2	-.027200
		1/2	1/2	9/2	9/2	-.116957			1/2	1/2	11/2	11/2	.000000
		1/2	1/2	9/2	11/2	.131667			1/2	1/2	11/2	15/2	-.258163
		1/2	1/2	9/2	15/2	.594927			1/2	1/2	15/2	15/2	.000000
		1/2	1/2	11/2	11/2	.211068			1	0	2	4	.282546
		1/2	1/2	11/2	15/2	-.105121			1	0	2	5	-.309736
		1/2	1/2	15/2	15/2	.385511			1	0	2	8	.401222
		1	0	2	4	-.245952			1	0	4	2	-.215874
		1	0	2	5	.247969			1	0	4	4	.070314
		1	0	4	2	-.148440			1	0	4	5	-.085863
		1	0	4	4	-.345747			1	0	4	8	.232623
	6	1	1	0	4	5	.227136	1	0	6	2	.307967	
			1	0	4	8	-.323780	1	0	6	4	.610171	
			1	0	6	2	-.215649	1	0	6	5	.098433	
			1	0	6	4	.325334	1	0	6	8	.270886	
			1	0	6	5	-.602376	1	1	2	4	-.841192	
			1	0	6	8	-.254610	1	1	2	6	-.421678	
			1	1	2	4	-.621470	1	1	4	4	.000000	
			1	1	2	6	-.495528	1	1	4	6	-.338502	
			1	1	4	4	.464214	1	1	6	6	.000000	
			1	1	4	6	-.388374	3/2	1/2	7/2	5/2	-.553560	
			1	1	6	6	-.043549	3/2	1/2	7/2	9/2	-.607086	
			3/2	1/2	7/2	3/2	-.138191	3/2	1/2	7/2	11/2	.486717	
			3/2	1/2	7/2	5/2	-.664216	3/2	1/2	7/2	15/2	.296859	
			3/2	1/2	7/2	9/2	.684860	6	3	1/2	1/2	3/2	9/2
3/2	1/2	7/2	11/2	-.263442	1/2	1/2	3/2	11/2		.198267			
3/2	1/2	7/2	15/2	.035857	1/2	1/2	3/2	15/2		.312628			
1/2	1/2	3/2	9/2	.358100	1/2	1/2	5/2	9/2		-.442366			
1/2	1/2	3/2	11/2	-.198267	1/2	1/2	5/2	11/2		.173970			
1/2	1/2	3/2	15/2	-.312628	1/2	1/2	5/2	15/2		.582529			
1/2	1/2	5/2	9/2	.442366	1/2	1/2	9/2	9/2		.000000			
1/2	1/2	5/2	11/2	-.173970	1/2	1/2	9/2	11/2		.477028			
1/2	1/2	5/2	15/2	-.382529	1/2	1/2	9/2	15/2		.338228			
1/2	1/2	9/2	9/2	.000000	1/2	1/2	11/2	11/2		.000000			
1/2	1/2	9/2	11/2	-.477028	1/2	1/2	11/2	15/2		.143120			
1/2	1/2	9/2	15/2	-.338228	1/2	1/2	15/2	15/2		.000000			
1/2	1/2	11/2	11/2	.000000	1	0	2	4		.113669			
1/2	1/2	11/2	15/2	-.143120	1	0	2	5		-.287543			
1/2	1/2	15/2	15/2	.000000	1	0	2	8	.466308				
1	0	2	4	-.113669	1	0	4	2	.390524				
1	0	2	5	-.287543	1	0	4	4	-.525908				
1	0	2	8	-.466308	1	0	4	5	-.001548				
1	0	4	2	-.390524	1	0	4	8	-.248950				
1	0	4	4	.525908	1	0	6	2	-.151459				
1	0	4	5	.001548	1	0	6	4	.106149				
1	0	4	8	.248950	1	0	6	5	.400822				
1	0	6	2	.151459	1	0	6	8	-.031986				
1	0	6	4	-.106149	1	1	2	4	-.338414				
1	0	6	5	-.400822	1	1	2	6	-.077713				
1	0	6	8	.031986	1	1	4	4	.000000				
1	1	2	4	.338414	1	1	4	6	.937783				
1	1	2	6	.077713	1	1	6	6	.000000				
1	1	4	4	.000000	3/2	1/2	7/2	5/2	.351633				
1	1	4	6	-.937783	3/2	1/2	7/2	9/2	.445794				
1	1	6	6	.000000	3/2	1/2	7/2	11/2	.640845				
3/2	1/2	7/2	5/2	-.351633	3/2	1/2	7/2	15/2	.516662				
3/2	1/2	7/2	9/2	-.445794	7	1	1/2	1/2	3/2	11/2	-.452631		
3/2	1/2	7/2	11/2	-.640845	1/2		1/2	3/2	15/2	-.108891			
3/2	1/2	7/2	15/2	-.516662	1/2		1/2	5/2	9/2	-.251486			
1/2	1/2	3/2	9/2	.006641	1/2		1/2	5/2	11/2	.226651			
1/2	1/2	3/2	11/2	-.268682	1/2		1/2	5/2	15/2	-.455196			
1/2	1/2	3/2	15/2	-.249056	1/2		1/2	9/2	9/2	-.386492			
1/2	1/2	5/2	9/2	-.024917	1/2		1/2	9/2	11/2	.269016			
1/2	1/2	5/2	11/2	.518798	1/2		1/2	9/2	15/2	-.108889			

See page 321 for Explanation of Tables

TABLE II. The Transformation Coefficients $D_{(v) \alpha, J, J_\mu}^{T, T_\mu, J}$

J	α	T_λ	T_μ	J_λ	J_μ	D	J	α	T_λ	T_μ	J_λ	J_μ	D		
						$V = 4$									
						$\frac{1}{2} = 1$									
7	1	1/2	1/2	11/2	11/2	-.396900	7	3	1	1	4	4	.818344		
		1/2	1/2	11/2	15/2	-.254171			1	1	4	6	-.484215		
		1/2	1/2	15/2	15/2	-.075595			1	1	6	6	.300789		
		1	0	2	5	-.502923			3/2	1/2	7/2	9/2	-.758082		
		1	0	2	8	.359427			3/2	1/2	7/2	11/2	.643418		
		1	0	4	4	-.383414			3/2	1/2	7/2	15/2	-.106414		
		1	0	4	5	.034757			8	1	1/2	1/2	3/2	15/2	-.072002
		1	0	4	8	-.484009					1/2	1/2	5/2	11/2	-.024272
		1	0	6	2	-.098945					1/2	1/2	5/2	15/2	-.424956
		1	0	6	4	.204896					1/2	1/2	9/2	9/2	.000000
		1	0	6	5	.414065					1/2	1/2	9/2	11/2	.618071
		1	0	6	8	.110355					1/2	1/2	9/2	15/2	-.648364
		1	1	2	6	.552231					1/2	1/2	11/2	11/2	.000000
		1	1	4	4	-.495101					1/2	1/2	11/2	15/2	-.106070
		1	1	4	6	-.437060					1/2	1/2	15/2	15/2	.000000
		1	1	6	6	.508817					1	0	2	8	.155954
		3/2	1/2	7/2	9/2	.338520			1	0	4	4	.389346		
		3/2	1/2	7/2	11/2	.527697			1	0	4	5	.477609		
		3/2	1/2	7/2	15/2	.779064			1	0	4	8	-.395912		
		7	2	1/2	1/2	3/2			11/2	.070873	8	2	1/2	1/2	3/2
1/2	1/2			3/2	15/2	-.147746	1/2	1/2	5/2	11/2			.463588		
1/2	1/2			5/2	9/2	-.034170	1/2	1/2	5/2	15/2			.391588		
1/2	1/2			5/2	11/2	.142225	1/2	1/2	9/2	9/2			.000000		
1/2	1/2			5/2	15/2	.262101	1/2	1/2	9/2	11/2			-.131794		
1/2	1/2			9/2	9/2	-.125374	1/2	1/2	9/2	15/2			-.438690		
1/2	1/2			9/2	11/2	.116281	1/2	1/2	11/2	11/2			.000000		
1/2	1/2			9/2	15/2	.143985	1/2	1/2	11/2	15/2			.510920		
1/2	1/2			11/2	11/2	.339806	1/2	1/2	15/2	15/2			.000000		
1/2	1/2			11/2	15/2	-.598586	3/2	1/2	7/2	9/2			.407188		
1/2	1/2			15/2	15/2	-.599426	3/2	1/2	7/2	11/2			.852312		
1	0			2	5	.078748	3/2	1/2	7/2	15/2			-.328273		
1	0			2	8	.120078	1/2	1/2	3/2	15/2			-.401107		
1	0			4	4	.003702	1/2	1/2	5/2	11/2			.463588		
1	0			4	5	.386637	1/2	1/2	5/2	15/2			.391588		
1	0			4	8	-.105341	1/2	1/2	9/2	9/2			.000000		
1	0			6	2	.218471	1/2	1/2	9/2	11/2			-.131794		
1	0			6	4	-.318211	1/2	1/2	9/2	15/2			-.438690		
1	0			6	5	-.164734	1/2	1/2	11/2	11/2			.000000		
1	0			6	8	.801659	1/2	1/2	11/2	15/2			.510920		
1	1	2	6	-.683699	1/2	1/2	15/2	15/2	.000000						
1	1	4	4	-.133023	1	0	2	8	-.548703						
1	1	4	6	.111941	1	0	4	4	-.232388						
1	1	6	6	.708753	1	0	4	5	.161251						
3/2	1/2	7/2	9/2	-.557418	1	0	4	8	-.181376						
3/2	1/2	7/2	11/2	-.554571	1	0	6	2	.252345						
3/2	1/2	7/2	15/2	.617848	1	0	6	4	-.209759						
7	3	1/2	1/2	3/2	11/2	.036425	9	1	1/2	1/2	3/2	15/2	-.483318		
		1/2	1/2	3/2	15/2	-.564606			1/2	1/2	5/2	11/2	.251843		
		1/2	1/2	5/2	9/2	-.422322			1/2	1/2	5/2	15/2	-.469886		
		1/2	1/2	5/2	11/2	.152716			1/2	1/2	9/2	9/2	-.266660		
		1/2	1/2	5/2	15/2	-.323700			1/2	1/2	9/2	11/2	-.266396		
		1/2	1/2	9/2	9/2	.234460			1/2	1/2	9/2	15/2	-.266396		
		1/2	1/2	9/2	11/2	-.102067			1/2	1/2	11/2	11/2	-.382316		
		1/2	1/2	9/2	15/2	.493954			1/2	1/2	11/2	15/2	-.196401		
		1/2	1/2	11/2	11/2	.093181			1/2	1/2	15/2	15/2	-.394173		
		1/2	1/2	11/2	15/2	-.062162			1	0	2	8	.394920		
		1/2	1/2	15/2	15/2	.226950			1	0	4	5	.349742		
		1	0	2	5	.040472			1	0	4	8	-.644424		
		1	0	2	8	.436875			1	0	6	4	-.089722		
		1	0	4	4	-.308120			1	0	6	5	-.516125		
		1	0	4	5	.270624									
		1	0	4	8	.403987									
		1	0	6	2	.544073									
		1	0	6	4	.346309									
		1	0	6	5	-.156987									
		1	0	6	8	-.188495									
1	1	2	6	.073312											

See page 321 for Explanation of Tables

TABLE II. The Transformation Coefficients $D_{(v)l\alpha; J_\lambda J_\mu}^{T_\lambda T_\mu J}$

J	α	T_λ	T_μ	J_λ	J_μ	D	J	α	T_λ	T_μ	J_λ	J_μ	D						
$v = 4 \quad t = 1$																			
9	1	1	0	6	8	.178890	10	1	1/2	1/2	5/2	15/2	.250000						
		1	1	4	6	.890400			1/2	1/2	9/2	11/2	-.363136						
	1	1	6	6	-.455179	1/2		1/2	9/2	15/2	.492641								
	3/2	1/2	7/2	11/2	.264135	1/2		1/2	11/2	11/2	.000000								
	3/2	1/2	7/2	15/2	-.964486	1/2		1/2	11/2	15/2	.750291								
	9	2	1/2	1/2	3/2	15/2		.247076	1/2	1/2	15/2	15/2	.000000						
			1/2	1/2	5/2	15/2		.563256	1	0	2	8	-.417855						
		1/2	1/2	9/2	9/2	.000000		1	0	4	8	-.446245							
		1/2	1/2	9/2	11/2	.223807		1	0	6	4	.335888							
		1/2	1/2	9/2	15/2	.174709		1	0	6	5	-.258199							
		1/2	1/2	11/2	11/2	-.253125		1	0	6	8	.668413							
		1/2	1/2	11/2	15/2	-.604459		1	1	4	6	-1.00000							
		1/2	1/2	15/2	15/2	.334127		1	1	6	6	.000000							
		1	0	2	8	.465891		3/2	1/2	7/2	15/2	-1.00000							
1		0	4	5	.248321	11	1	1/2	1/2	9/2	15/2	-.494727							
1		0	4	8	.329435			1/2	1/2	11/2	11/2	-.428571							
1		0	6	4	.611556		1/2	1/2	11/2	15/2	.204313								
1	0	6	5	.341027	1/2		1/2	15/2	15/2	.727892									
1	0	6	8	.349936	1		0	4	8	.564076									
1	1	4	6	-.455179	1		0	6	5	.345033									
1	1	6	6	-.890400	1		0	6	8	.750180									
3/2	1/2	7/2	11/2	-.964486	1		1	6	6	1.00000									
3/2	1/2	7/2	15/2	-.264135	3/2		1/2	7/2	15/2	-1.00000									
$v = 4 \quad t = 2$																			
2	1	1	1	2	2	.335030	4	1	2	0	0	4	-1.00000						
		1	1	2	4	.329914			5	1	1	1	2	4	.460566				
	1	1	4	4	-.662338	1		1			2	6	.410891						
	1	1	4	6	-.535258	1		1		4	4	.000000							
	1	1	6	6	.231774	1		1		4	6	-.786796							
	3/2	1/2	7/2	3/2	.560612	1		1		6	6	.000000							
	3/2	1/2	7/2	5/2	-.158114	3/2		1/2		7/2	3/2	.387298							
	3/2	1/2	7/2	9/2	-.754854	3/2		1/2		7/2	5/2	.333712							
	3/2	1/2	7/2	11/2	-.301511	3/2		1/2		7/2	9/2	.553912							
	2	0	0	2	1.00000	3/2		1/2		7/2	11/2	.459390							
4	1	1	1	2	2	-.350467	3/2	1/2		7/2	15/2	.469871							
		1	1	2	4	-.485621	2	0	0	5	1.00000								
	1	1	2	6	.544331	8	1	1	1	2	6	-.398409							
	1	1	4	4	.196601			1	1	4	4	.380300							
	1	1	4	6	.142134		1	1	4	6	.518831								
	1	1	6	6	.534972		1	1	6	6	-.653802								
	3/2	1/2	7/2	3/2	.175933		3/2	1/2	7/2	9/2	-.373979								
	3/2	1/2	7/2	5/2	-.658281		3/2	1/2	7/2	11/2	.483494								
	3/2	1/2	7/2	9/2	-.128388		3/2	1/2	7/2	15/2	.791438								
	3/2	1/2	7/2	11/2	.645497		2	0	0	8	-1.00000								
3/2	1/2	7/2	15/2	-.320256	$v = 5 \quad t = 1/2$														
1/2	1	0	1/2	2	3/2		-.097702	1/2	2	0	1/2	2	5/2	.652602					
		0	1/2	2	5/2	.127911	0			1/2	4	9/2	-.583830						
	0	1/2	4	9/2	.275345	0	1/2		5	9/2	-.409735								
	0	1/2	5	9/2	-.392346	0	1/2		5	11/2	-.022106								
	0	1/2	5	11/2	.762652	0	1/2		8	15/2	.109446								
	0	1/2	8	15/2	-.403366	1	1/2		2	3/2	-.680907								
	1	1/2	2	3/2	-.580556	1	1/2		2	5/2	-.405744								
	1	1/2	2	5/2	.072203	1	1/2		4	9/2	.090827								
	1	1/2	4	9/2	.449806	1	1/2		6	11/2	-.602900								
	1	1/2	6	11/2	.674845	3/2	1		0	1/2	2	3/2	.125472						
	1/2	2	0	1/2	2				5/2	.095241									

See page 321 for Explanation of Tables

TABLE II. The Transformation Coefficients $D_{(v) \alpha_i J_i \mu_i}^{T_\lambda T_\mu J}$

J	α	T_λ	T_μ	J_i	J_μ	D	J	α	T_λ	T_μ	J_i	J_μ	D				
$v = 5 \quad t = 1/2$																	
3/2	1	0	1/2	4	5/2	-.068494	5/2	1	0	1/2	4	9/2	-.057254				
		0	1/2	4	9/2	.115701			0	1/2	4	11/2	-.394478				
		0	1/2	4	11/2	.203213			0	1/2	5	5/2	-.393117				
		0	1/2	5	9/2	.158686			0	1/2	5	9/2	.129577				
		0	1/2	5	11/2	.350437			0	1/2	5	11/2	.596991				
		0	1/2	8	15/2	.876256			0	1/2	5	15/2	.012978				
		1	1/2	2	3/2	.028198			0	1/2	8	11/2	.062873				
		1	1/2	2	5/2	-.279408			0	1/2	8	15/2	-.048586				
		1	1/2	4	5/2	-.023166			1	1/2	2	3/2	-.546237				
		1	1/2	4	9/2	.692413			1	1/2	2	5/2	.012433				
		1	1/2	4	11/2	.100779			1	1/2	2	9/2	-.332201				
		1	1/2	6	9/2	-.173478			1	1/2	4	3/2	-.191225				
		1	1/2	6	11/2	.288369			1	1/2	4	5/2	.035556				
		1	1/2	6	15/2	-.563698			1	1/2	4	9/2	-.383985				
		3/2	2	0	1/2	2			3/2	-.303826	5/2	2	0	1/2	4	11/2	.399548
				0	1/2	2			5/2	.104809			1	1/2	6	9/2	.291165
0	1/2			4	5/2	-.055930	1	1/2	6	11/2			.385144				
0	1/2			4	9/2	.379102	1	1/2	6	15/2			.114391				
0	1/2			4	11/2	-.039307	0	1/2	2	3/2			-.090978				
0	1/2			5	9/2	-.739005	0	1/2	2	5/2			-.386454				
0	1/2			5	11/2	-.362749	0	1/2	2	9/2			-.204915				
0	1/2			8	15/2	.265703	0	1/2	4	3/2			.237028				
1	1/2			2	3/2	-.001471	0	1/2	4	5/2			-.145391				
1	1/2			2	5/2	.014576	0	1/2	4	9/2			.560745				
1	1/2			4	5/2	-.451602	0	1/2	4	11/2			.038853				
1	1/2			4	9/2	-.376916	0	1/2	5	5/2			.204594				
1	1/2			4	11/2	.618869	0	1/2	5	9/2			-.035381				
1	1/2			6	9/2	.300742	0	1/2	5	11/2			.442302				
1	1/2			6	11/2	.333316	0	1/2	5	15/2			.265684				
1	1/2			6	15/2	-.263117	0	1/2	8	11/2			-.257209				
3/2	3	0	1/2	2	3/2	-.077724	5/2	3	0	1/2	8	15/2	-.177865				
		0	1/2	2	5/2	.023045			1	1/2	2	3/2	.088733				
		0	1/2	4	5/2	-.760851			1	1/2	2	5/2	.247741				
		0	1/2	4	9/2	-.095066			1	1/2	2	9/2	.156842				
		0	1/2	4	11/2	.604874			1	1/2	4	3/2	.060866				
		0	1/2	5	9/2	.039497			1	1/2	4	5/2	.463000				
		0	1/2	5	11/2	-.148753			1	1/2	4	9/2	-.127390				
		0	1/2	8	15/2	-.126236			1	1/2	4	11/2	-.403217				
		1	1/2	2	3/2	-.029856			1	1/2	6	9/2	.582850				
		1	1/2	2	5/2	-.773908			1	1/2	6	11/2	.198431				
		1	1/2	4	5/2	.414485			1	1/2	6	15/2	-.360800				
		1	1/2	4	9/2	-.132588			0	1/2	2	3/2	-.077399				
		1	1/2	4	11/2	.146595			0	1/2	2	5/2	.259773				
		1	1/2	6	9/2	.175583			0	1/2	2	9/2	-.149973				
		1	1/2	6	11/2	.255643			0	1/2	4	3/2	-.098737				
		1	1/2	6	15/2	.305163			0	1/2	4	5/2	-.004717				
3/2	4	0	1/2	2	3/2	-.210411	5/2	4	0	1/2	4	9/2	-.303170				
		0	1/2	2	5/2	-.641741			0	1/2	4	11/2	.347413				
		0	1/2	4	5/2	.058494			0	1/2	5	5/2	-.132995				
		0	1/2	4	9/2	-.567902			0	1/2	5	9/2	-.000926				
		0	1/2	4	11/2	.090864			0	1/2	5	11/2	-.069380				
		0	1/2	5	9/2	-.371537			0	1/2	5	15/2	.513972				
		0	1/2	5	11/2	.232523			0	1/2	8	11/2	-.628423				
		0	1/2	8	15/2	.132658			0	1/2	8	15/2	-.008498				
		1	1/2	2	3/2	.720505			1	1/2	2	3/2	.019354				
		1	1/2	2	5/2	.161962			1	1/2	2	5/2	.118459				
		1	1/2	4	5/2	.412573			1	1/2	2	9/2	-.597263				
		1	1/2	4	9/2	-.298910			1	1/2	4	3/2	.235676				
		1	1/2	4	11/2	.081601			1	1/2	4	5/2	-.393229				
		1	1/2	6	9/2	-.325436			1	1/2	4	9/2	-.056561				
		1	1/2	6	11/2	.187249			1	1/2	4	11/2	-.039198				
		1	1/2	6	15/2	-.217824			1	1/2	6	9/2	.265658				
5/2	1	0	1/2	2	3/2	-.254820	5/2	4	0	1/2	6	11/2	-.439748				
		0	1/2	2	5/2	.287219			1	1/2	6	15/2	-.387311				
		0	1/2	2	9/2	-.079446			0	1/2	2	3/2	-.408664				
		0	1/2	4	3/2	-.347098			0	1/2	2	5/2	-.301578				
		0	1/2	4	5/2	-.180777			0	1/2	2	9/2	-.479611				

See page 321 for Explanation of Tables

TABLE II. The Transformation Coefficients $D_{(v) \alpha; J \lambda \mu}^{T \lambda T \mu J}$

J	α	T_λ	T_μ	J	J	D	J	α	T_λ	T_μ	J_λ	J_μ	D		
$v = 5 \quad t = 1/2$															
5/2	4	0	1/2	4	3/2	.320100	7/2	1	1	1/2	4	11/2	-.031527		
		0	1/2	4	5/2	.106245			1	1/2	4	15/2	-.394842		
		0	1/2	4	9/2	-.201390			1	1/2	6	5/2	-.123618		
		0	1/2	4	11/2	-.326055			1	1/2	6	9/2	.156183		
		0	1/2	5	5/2	-.163826			1	1/2	6	11/2	.291556		
		0	1/2	5	9/2	.346101			1	1/2	6	15/2	-.091386		
		0	1/2	5	11/2	-.282372			7/2	2	0	1/2	2	3/2	-.134647
		0	1/2	5	15/2	.048262					0	1/2	2	5/2	.247904
		0	1/2	8	11/2	.008713					0	1/2	2	9/2	-.302642
		0	1/2	8	15/2	.150440					0	1/2	2	11/2	.100836
		1	1/2	2	3/2	.434417					0	1/2	4	3/2	-.230726
		1	1/2	2	5/2	-.575251					0	1/2	4	5/2	.213978
		1	1/2	2	9/2	-.021470					0	1/2	4	9/2	-.189143
		1	1/2	4	3/2	-.452461					0	1/2	4	11/2	-.112392
		1	1/2	4	5/2	-.306391					0	1/2	4	15/2	-.053251
		1	1/2	4	9/2	-.151351					0	1/2	5	3/2	.111932
		1	1/2	4	11/2	-.126788					0	1/2	5	5/2	.133081
		1	1/2	6	9/2	.354058					0	1/2	5	9/2	-.047097
		1	1/2	6	11/2	.114110					0	1/2	5	11/2	-.058471
		1	1/2	6	15/2	.062854					0	1/2	5	15/2	.286624
5/2	5	0	1/2	2	3/2	-.382967	0	1/2			8	9/2	.427463		
		0	1/2	2	5/2	.193028	0	1/2			8	11/2	.071933		
		0	1/2	2	9/2	-.362674	0	1/2			8	15/2	-.602053		
		0	1/2	4	3/2	-.378723	1	1/2			2	3/2	.009625		
		0	1/2	4	5/2	.069793	1	1/2			2	5/2	-.063127		
		0	1/2	4	9/2	.133538	1	1/2			2	9/2	.245666		
		0	1/2	4	11/2	.383483	1	1/2	2	11/2	-.367030				
		0	1/2	5	5/2	.432029	1	1/2	4	3/2	-.469081				
		0	1/2	5	9/2	.234055	1	1/2	4	5/2	.255292				
		0	1/2	5	11/2	.000628	1	1/2	4	9/2	.043983				
		0	1/2	5	15/2	-.358754	1	1/2	4	11/2	-.252998				
		0	1/2	8	11/2	.034767	1	1/2	4	15/2	.453615				
		0	1/2	8	15/2	.003133	1	1/2	6	5/2	.116727				
		1	1/2	2	3/2	.338991	1	1/2	6	9/2	-.037491				
		1	1/2	2	5/2	.606866	1	1/2	6	11/2	-.210154				
		1	1/2	2	9/2	.036053	1	1/2	6	15/2	.429817				
		1	1/2	4	3/2	-.580329	7/2	3	0	1/2	2	3/2	-.389714		
		1	1/2	4	5/2	-.024099			0	1/2	2	5/2	.327818		
		1	1/2	4	9/2	-.262258			0	1/2	2	9/2	-.280115		
		1	1/2	4	11/2	.230224			0	1/2	2	11/2	-.290128		
1	1/2	6	9/2	-.153938	0	1/2			4	3/2	-.229634				
1	1/2	6	11/2	-.145868	0	1/2			4	5/2	-.111806				
1	1/2	6	15/2	-.106677	0	1/2			4	9/2	-.073785				
7/2	1	0	1/2	2	3/2	.195000			0	1/2	4	11/2	-.154475		
		0	1/2	2	5/2	.338480			0	1/2	4	15/2	.135026		
		0	1/2	2	9/2	.234657			0	1/2	5	3/2	.066704		
		0	1/2	2	11/2	.102491			0	1/2	5	5/2	.085842		
		0	1/2	4	3/2	-.261545			0	1/2	5	9/2	-.508559		
		0	1/2	4	5/2	.702308			0	1/2	5	11/2	-.069322		
		0	1/2	4	9/2	.037758			0	1/2	5	15/2	-.283276		
		0	1/2	4	11/2	.084129			0	1/2	8	9/2	-.283538		
		0	1/2	4	15/2	.138484			0	1/2	8	11/2	-.110121		
		0	1/2	5	3/2	-.331825			0	1/2	8	15/2	.131252		
		0	1/2	5	5/2	-.149775			1	1/2	2	3/2	-.159111		
		0	1/2	5	9/2	-.049594			1	1/2	2	5/2	.125498		
		0	1/2	5	11/2	-.072520			1	1/2	2	9/2	.238100		
		0	1/2	5	15/2	-.059768	1	1/2	2	11/2	.012058				
		0	1/2	8	9/2	-.122239	1	1/2	4	3/2	-.290952				
		0	1/2	8	11/2	-.162042	1	1/2	4	5/2	-.003000				
		0	1/2	8	15/2	.086509	1	1/2	4	9/2	.635770				
		1	1/2	2	3/2	.282064	1	1/2	4	11/2	.030240				
		1	1/2	2	5/2	-.275724	1	1/2	4	15/2	-.286989				
		1	1/2	2	9/2	.375737	1	1/2	6	5/2	-.255005				
1	1/2	2	11/2	-.493306	1	1/2	6	9/2	.512433						
1	1/2	4	3/2	.104224	1	1/2	6	11/2	.003599						
1	1/2	4	5/2	.240394	1	1/2	6	15/2	-.048215						
1	1/2	4	9/2	-.318293	7/2	4	0	1/2	2	3/2	-.119603				

See page 321 for Explanation of Tables

TABLE II. The Transformation Coefficients $D_{(v)\alpha; J_N}^{T_\lambda T_\mu J}$

J	α	T_λ	T_μ	J_λ	J_μ	D	J	α	T_λ	T_μ	J_λ	J_μ	D				
$v = 5 \quad t = 1/2$																	
7/2	4	0	1/2	2	5/2	-.155014	7/2	6	0	1/2	4	15/2	-.327950				
		0	1/2	2	9/2	.084451			0	1/2	5	3/2	-.279133				
		0	1/2	2	11/2	-.513687			0	1/2	5	5/2	.176524				
		0	1/2	4	3/2	-.150269			0	1/2	5	9/2	.100971				
		0	1/2	4	5/2	.276869			0	1/2	5	11/2	-.104074				
		0	1/2	4	9/2	-.204379			0	1/2	5	15/2	.251336				
		0	1/2	4	11/2	.310272			0	1/2	8	9/2	.070077				
		0	1/2	4	15/2	-.057771			0	1/2	8	11/2	.356469				
		0	1/2	5	3/2	.240521			0	1/2	8	15/2	.338861				
		0	1/2	5	5/2	.062579			1	1/2	2	3/2	-.285395				
		0	1/2	5	9/2	.286455			1	1/2	2	5/2	.452682				
		0	1/2	5	11/2	.127461			1	1/2	2	9/2	.266642				
		0	1/2	5	15/2	-.017674			1	1/2	2	11/2	.050555				
		0	1/2	8	9/2	-.377654			1	1/2	4	3/2	-.024791				
		0	1/2	8	11/2	.318960			1	1/2	4	5/2	.157462				
		0	1/2	8	15/2	-.212851			1	1/2	4	9/2	-.152193				
		1	1/2	2	3/2	-.495245			1	1/2	4	11/2	-.447765				
		1	1/2	2	5/2	-.478935			1	1/2	4	15/2	.050327				
		1	1/2	2	9/2	-.447801			1	1/2	6	5/2	.367336				
		1	1/2	2	11/2	-.184533			1	1/2	6	9/2	.042731				
		1	1/2	4	3/2	.166609			1	1/2	6	11/2	.162882				
		1	1/2	4	5/2	.169487			1	1/2	6	15/2	-.474431				
		1	1/2	4	9/2	.117976			7/2	7	0	1/2	2	3/2	.263830		
		1	1/2	4	11/2	-.373909					0	1/2	2	5/2	.064497		
		1	1/2	4	15/2	-.188744					0	1/2	2	9/2	-.090394		
		1	1/2	6	5/2	.157765					0	1/2	2	11/2	.161067		
		1	1/2	6	9/2	.122586					0	1/2	4	3/2	.339638		
		1	1/2	6	11/2	-.067286					0	1/2	4	5/2	.017224		
		1	1/2	6	15/2	.022261					0	1/2	4	9/2	-.506321		
		7/2	5	0	1/2	2					3/2	-.050324	0	1/2	4	11/2	.118401
				0	1/2	2					5/2	.043142	0	1/2	4	15/2	.023809
				0	1/2	2					9/2	.017034	0	1/2	5	3/2	-.265523
0	1/2			2	11/2	.051393	0	1/2			5	5/2	.275940				
0	1/2			4	3/2	.051243	0	1/2			5	9/2	-.236557				
0	1/2			4	5/2	-.086968	0	1/2			5	11/2	.412451				
0	1/2			4	9/2	.153316	0	1/2			5	15/2	-.297099				
0	1/2			4	11/2	.067453	0	1/2			8	9/2	-.044473				
0	1/2			4	15/2	-.547170	0	1/2			8	11/2	.173647				
0	1/2			5	3/2	-.204074	0	1/2			8	15/2	-.111370				
0	1/2			5	5/2	-.541025	1	1/2			2	3/2	.105395				
0	1/2			5	9/2	-.199826	1	1/2			2	5/2	-.399094				
0	1/2			5	11/2	-.125221	1	1/2			2	9/2	.168535				
0	1/2			5	15/2	-.282500	1	1/2			2	11/2	.243105				
0	1/2			8	9/2	-.089608	1	1/2			4	3/2	-.219309				
0	1/2			8	11/2	.260702	1	1/2			4	5/2	-.542444				
0	1/2			8	15/2	-.330560	1	1/2			4	9/2	-.167834				
1	1/2			2	3/2	.418114	1	1/2			4	11/2	-.490654				
1	1/2			2	5/2	.197582	1	1/2			4	15/2	.095971				
1	1/2			2	9/2	-.275398	1	1/2			6	5/2	-.273032				
1	1/2			2	11/2	-.296570	1	1/2			6	9/2	.055822				
1	1/2			4	3/2	.000380	1	1/2			6	11/2	-.073185				
1	1/2			4	5/2	-.378417	1	1/2			6	15/2	-.196549				
1	1/2			4	9/2	-.025543	9/2	1			0	1/2	2	5/2	.276991		
1	1/2			4	11/2	-.076277					0	1/2	2	9/2	-.120046		
1	1/2			4	15/2	-.104393			0	1/2	2	11/2	-.214288				
1	1/2			6	5/2	.462344			0	1/2	4	3/2	-.341375				
1	1/2			6	9/2	.424079			0	1/2	4	5/2	-.123044				
1	1/2			6	11/2	-.261093			0	1/2	4	9/2	.239329				
1	1/2			6	15/2	.000653			0	1/2	4	11/2	-.023241				
7/2	6			0	1/2	2			3/2	.225328	0	1/2	4	15/2	.118433		
				0	1/2	2			5/2	.301833	0	1/2	5	3/2	-.165789		
		0	1/2	2	9/2	.110128			0	1/2	5	5/2	-.154803				
		0	1/2	2	11/2	-.176265			0	1/2	5	9/2	-.021663				
		0	1/2	4	3/2	-.361200			0	1/2	5	11/2	.423436				
		0	1/2	4	5/2	-.289385			0	1/2	5	15/2	.442793				
		0	1/2	4	9/2	-.206575			0	1/2	8	9/2	-.456321				
		0	1/2	4	11/2	-.102045			0	1/2	8	11/2	.045746				

See page 321 for Explanation of Tables

TABLE II. The Transformation Coefficients $D_{(v)\alpha; J_N J_\mu}^{T_\lambda T_\mu J}$

J	α	T_λ	T_μ	J_λ	J_μ	D	J	α	T_λ	T_μ	J_λ	J_μ	D				
$v = 5 \quad t = 1/2$																	
9/2	1	0	1/2	8	15/2	-.147718	9/2	3	1	1/2	6	3/2	-.473707				
		1	1/2	2	5/2	.170165			1	1/2	6	5/2	-.102059				
		1	1/2	2	9/2	.578104			1	1/2	6	9/2	.063552				
		1	1/2	2	11/2	-.045800			1	1/2	6	11/2	.124892				
		1	1/2	4	3/2	.307907			1	1/2	6	15/2	.120153				
		1	1/2	4	5/2	-.469185			9/2	4	0	1/2	2	5/2	-.030172		
		1	1/2	4	9/2	-.163439					0	1/2	2	9/2	-.093971		
		1	1/2	4	11/2	.376916					0	1/2	2	11/2	.282936		
		1	1/2	4	15/2	.176172					0	1/2	4	3/2	.027635		
		1	1/2	6	3/2	.084908					0	1/2	4	5/2	.275928		
		1	1/2	6	5/2	-.189677					0	1/2	4	9/2	-.194546		
		1	1/2	6	9/2	.026778					0	1/2	4	11/2	-.555754		
		1	1/2	6	11/2	-.213826					0	1/2	4	15/2	-.166383		
		1	1/2	6	15/2	-.174246					0	1/2	5	3/2	-.159309		
		9/2	2	0	1/2	2					5/2	-.398382	0	1/2	5	5/2	-.048239
				0	1/2	2					9/2	-.145117	0	1/2	5	9/2	.466746
0	1/2			2	11/2	.268779	0	1/2			5	11/2	.394290				
0	1/2			4	3/2	.291030	0	1/2			5	15/2	-.107241				
0	1/2			4	5/2	-.078366	0	1/2			8	9/2	-.090016				
0	1/2			4	9/2	-.424474	0	1/2			8	11/2	-.027492				
0	1/2			4	11/2	.086079	0	1/2			8	15/2	.193726				
0	1/2			4	15/2	-.135521	1	1/2	2	5/2	-.337740						
0	1/2			5	3/2	-.015195	1	1/2	2	9/2	.208140						
0	1/2			5	5/2	.059371	1	1/2	2	11/2	-.201098						
0	1/2			5	9/2	-.211498	1	1/2	4	3/2	-.191632						
0	1/2			5	11/2	-.046502	1	1/2	4	5/2	-.010136						
0	1/2			5	15/2	.465598	1	1/2	4	9/2	.284668						
0	1/2			8	9/2	-.375145	1	1/2	4	11/2	.290580						
0	1/2			8	11/2	-.188138	1	1/2	4	15/2	.089154						
0	1/2			8	15/2	-.087384	1	1/2	6	3/2	-.024435						
1	1/2	2	5/2	.153945	1	1/2	6	5/2	.639630								
1	1/2	2	9/2	-.225478	1	1/2	6	9/2	.305278								
1	1/2	2	11/2	-.139279	1	1/2	6	11/2	-.236092								
1	1/2	4	3/2	.025779	1	1/2	6	15/2	.182387								
1	1/2	4	5/2	.435214	9/2	5	0	1/2	2	5/2	.172869						
1	1/2	4	9/2	-.321763			0	1/2	2	9/2	-.462385						
1	1/2	4	11/2	.426633			0	1/2	2	11/2	.100101						
1	1/2	4	15/2	-.050827			0	1/2	4	3/2	.321233						
1	1/2	6	3/2	-.408091			0	1/2	4	5/2	.203066						
1	1/2	6	5/2	-.085512			0	1/2	4	9/2	.339899						
1	1/2	6	9/2	.338106			0	1/2	4	11/2	-.223365						
1	1/2	6	11/2	-.212054			0	1/2	4	15/2	.119742						
1	1/2	6	15/2	-.307769			0	1/2	5	3/2	.131751						
9/2	3	0	1/2	2			5/2	-.040308	0	1/2	5	5/2	.288672				
		0	1/2	2			9/2	.634089	0	1/2	5	9/2	.019937				
		0	1/2	2			11/2	.187946	0	1/2	5	11/2	-.336020				
		0	1/2	4			3/2	.134330	0	1/2	5	15/2	.071381				
		0	1/2	4			5/2	.100204	0	1/2	8	9/2	-.223212				
		0	1/2	4			9/2	.066594	0	1/2	8	11/2	.385331				
		0	1/2	4			11/2	-.184627	0	1/2	8	15/2	-.068648				
		0	1/2	4	15/2	.182526	1	1/2	2	5/2	-.559493						
		0	1/2	5	3/2	-.433262	1	1/2	2	9/2	.071978						
		0	1/2	5	5/2	.155323	1	1/2	2	11/2	.459805						
		0	1/2	5	9/2	-.171501	1	1/2	4	3/2	-.417517						
		0	1/2	5	11/2	-.000558	1	1/2	4	5/2	-.123349						
		0	1/2	5	15/2	.234163	1	1/2	4	9/2	-.349409						
		0	1/2	8	9/2	.099257	1	1/2	4	11/2	.176784						
		0	1/2	8	11/2	.376637	1	1/2	4	15/2	-.268631						
		0	1/2	8	15/2	-.115172	1	1/2	6	3/2	.069781						
1	1/2	2	5/2	-.136469	1	1/2	6	5/2	-.132288								
1	1/2	2	9/2	-.035400	1	1/2	6	9/2	-.045108								
1	1/2	2	11/2	.406314	1	1/2	6	11/2	.044224								
1	1/2	4	3/2	.424989	1	1/2	6	15/2	-.170204								
1	1/2	4	5/2	-.114061	9/2	6	0	1/2	2	5/2	.304071						
1	1/2	4	9/2	.471706			0	1/2	2	9/2	-.071750						
1	1/2	4	11/2	.198569			0	1/2	2	11/2	.423651						
1	1/2	4	15/2	-.300969			0	1/2	4	3/2	.220555						

See page 321 for Explanation of Tables

TABLE II. The Transformation Coefficients $D_{(v)\alpha; J_\lambda J_\mu}^{T_\lambda T_\mu J}$

J	∞	T_λ	T_μ	J_λ	J_μ	D	J	∞	T_λ	T_μ	J_λ	J_μ	D
$v = 5 \quad t = 1/2$													
9/2	6	0	1/2	4	5/2	-.181396	11/2	1	0	1/2	8	5/2	-.093444
		0	1/2	4	9/2	.062060			0	1/2	8	9/2	-.135089
		0	1/2	4	11/2	.540068			0	1/2	8	11/2	.394544
		0	1/2	4	15/2	.041754			0	1/2	8	15/2	.735759
		0	1/2	5	3/2	-.346201			1	1/2	2	9/2	-.308290
		0	1/2	5	5/2	-.143600			1	1/2	2	11/2	-.362368
		0	1/2	5	9/2	.447253			1	1/2	2	15/2	.119276
		0	1/2	5	11/2	-.051898			1	1/2	4	3/2	.133220
		0	1/2	5	15/2	.014238			1	1/2	4	5/2	-.110060
		0	1/2	8	9/2	.024410			1	1/2	4	9/2	.417846
		0	1/2	8	11/2	-.007512			1	1/2	4	11/2	.378192
		0	1/2	8	15/2	-.006008			1	1/2	4	15/2	.353388
	1	1/2	2	5/2	.251255	1	1/2	6	3/2	.056955			
	1	1/2	2	9/2	.335617	1	1/2	6	5/2	.054437			
	1	1/2	2	11/2	.184818	1	1/2	6	9/2	-.245335			
	1	1/2	4	3/2	-.470909	1	1/2	6	11/2	.131642			
	1	1/2	4	5/2	.246479	1	1/2	6	15/2	-.450917			
	1	1/2	4	9/2	.451951	11/2	2	0	1/2	2	9/2	.101176	
	1	1/2	4	11/2	-.037279			0	1/2	2	11/2	.261250	
	1	1/2	4	15/2	.080778			0	1/2	2	15/2	-.163926	
	1	1/2	6	3/2	.081551			0	1/2	4	3/2	.442544	
	1	1/2	6	5/2	-.412969			0	1/2	4	5/2	.074740	
	1	1/2	6	9/2	.341169			0	1/2	4	9/2	-.133450	
	1	1/2	6	11/2	-.029482			0	1/2	4	11/2	-.081731	
1	1/2	6	15/2	-.030539	0			1/2	4	15/2	.083502		
9/2	7	0	1/2	2	5/2			.249649	0	1/2	5	3/2	-.276192
		0	1/2	2	9/2			.106088	0	1/2	5	5/2	-.485668
		0	1/2	2	11/2			-.128327	0	1/2	5	9/2	-.365962
		0	1/2	4	3/2			.133144	0	1/2	5	11/2	.064964
		0	1/2	4	5/2	.294218	0	1/2	5	15/2	-.227329		
		0	1/2	4	9/2	.255522	0	1/2	8	5/2	-.104865		
		0	1/2	4	11/2	.118676	0	1/2	8	9/2	-.244506		
		0	1/2	4	15/2	-.563663	0	1/2	8	11/2	.226534		
		0	1/2	5	3/2	-.191275	0	1/2	8	15/2	.194081		
		0	1/2	5	5/2	.430908	1	1/2	2	9/2	.211269		
		0	1/2	5	9/2	-.113468	1	1/2	2	11/2	.243822		
		0	1/2	5	11/2	.067384	1	1/2	2	15/2	-.157939		
	0	1/2	5	15/2	.056570	1	1/2	4	3/2	-.164911			
	0	1/2	8	9/2	-.010497	1	1/2	4	5/2	.123742			
	0	1/2	8	11/2	-.406840	1	1/2	4	9/2	.008980			
	0	1/2	8	15/2	.007606	1	1/2	4	11/2	-.409656			
	1	1/2	2	5/2	-.226503	1	1/2	4	15/2	.593446			
	1	1/2	2	9/2	-.055837	1	1/2	6	3/2	-.326065			
	1	1/2	2	11/2	.151601	1	1/2	6	5/2	-.051290			
	1	1/2	4	3/2	.320776	1	1/2	6	9/2	-.267724			
	1	1/2	4	5/2	.319064	1	1/2	6	11/2	-.204983			
	1	1/2	4	9/2	.250652	1	1/2	6	15/2	-.292820			
	1	1/2	4	11/2	-.155352	11/2	3	0	1/2	2	9/2	.260176	
	1	1/2	4	15/2	.071934			0	1/2	2	11/2	.203671	
1	1/2	6	3/2	.282912	0			1/2	2	15/2	-.350370		
1	1/2	6	5/2	-.038147	0			1/2	4	3/2	-.144404		
1	1/2	6	9/2	-.210670	0			1/2	4	5/2	.009489		
1	1/2	6	11/2	-.635170	0			1/2	4	9/2	.058405		
1	1/2	6	15/2	-.310555	0			1/2	4	11/2	.024192		
11/2	1	0	1/2	2	9/2			.019396	0	1/2	4	15/2	.077926
		0	1/2	2	11/2			-.162998	0	1/2	5	3/2	-.113852
		0	1/2	2	15/2			-.118526	0	1/2	5	5/2	.237327
		0	1/2	4	3/2			-.226420	0	1/2	5	9/2	.153058
		0	1/2	4	5/2			-.028474	0	1/2	5	11/2	-.421125
		0	1/2	4	9/2	-.095817	0	1/2	5	15/2	-.098745		
		0	1/2	4	11/2	.299310	0	1/2	8	5/2	-.146940		
		0	1/2	4	15/2	-.008583	0	1/2	8	9/2	-.590912		
		0	1/2	5	3/2	.065392	0	1/2	8	11/2	-.259341		
		0	1/2	5	5/2	.255615	0	1/2	8	15/2	-.138635		
		0	1/2	5	9/2	-.066627	1	1/2	2	9/2	.111311		
		0	1/2	5	11/2	-.067222	1	1/2	2	11/2	-.097055		
0	1/2	5	15/2	.074350	1	1/2	2	15/2	.506344				

See page 321 for Explanation of Tables

TABLE II. The Transformation Coefficients $D_{(v)\alpha_i J_N J_B}^{T_\lambda T_\mu J}$

J	α	T_λ	T_μ	J_λ	J_μ	D	J	α	T_λ	T_μ	J_λ	J_μ	D		
$v = 5 \quad \frac{1}{2} = 1/2$															
11/2	3	1	1/2	4	3/2	.283960	11/2	5	1	1/2	6	9/2	-.195011		
			1/2		4	5/2				-.145184					
		1	1/2	4	9/2	.036066			1	1/2	6	11/2	-.048077		
			1/2		4	11/2				-.008911					
		1	1/2	4	15/2	.248573			11/2	6	0	1/2	2	9/2	-.080530
			1/2		6	3/2						-.311139			
		1	1/2	6	5/2	.138556			0	1/2	2	15/2	-.220608		
			1/2		6	9/2						-.278085			
		1	1/2	6	11/2	-.005785			0	1/2	4	3/2	.273644		
			1/2		6	15/2						.602955			
11/2	4	0	1/2	2	9/2	-.014630	0	1/2	4	3/2	4	9/2	.203870		
			1/2		2	11/2				-.223128					
0	1/2	2	15/2	.091097	0	1/2	4	15/2	-.026413						
			1/2	4				3/2	-.126726						
0	1/2	4	5/2	-.002330	0	1/2	5	3/2	.367488						
			1/2	4				9/2	-.223741						
0	1/2	4	11/2	.189814	0	1/2	5	5/2	-.146898						
			1/2	4				15/2	.434459						
0	1/2	5	3/2	-.118798	0	1/2	5	9/2	.182867						
			1/2	5				5/2	-.026286						
0	1/2	5	9/2	.150349	0	1/2	5	11/2	.100637						
			1/2	5				11/2	.168060						
0	1/2	5	15/2	-.426330	0	1/2	8	5/2	-.319736						
			1/2	8				5/2	-.551305						
0	1/2	8	9/2	.114884	0	1/2	8	9/2	.044234						
			1/2	8				11/2	.114237						
0	1/2	8	15/2	-.270549	0	1/2	8	11/2	-.290254						
			1/2	2				9/2	-.442256						
1	1/2	2	11/2	.301784	1	1/2	2	15/2	.058158						
			1/2	2				15/2	.314884						
1	1/2	4	3/2	.022706	1	1/2	4	3/2	.326700						
			1/2	4				5/2	-.043650						
1	1/2	4	9/2	-.158091	1	1/2	4	5/2	.630997						
			1/2	4				11/2	.169426						
1	1/2	4	15/2	.054247	11/2	7	0	1/2	2	9/2	-.061623				
			1/2	6				3/2	-.087346						
1	1/2	6	5/2	.176870	0	1/2	2	15/2	-.488470						
			1/2	6				9/2	.275318						
1	1/2	6	11/2	-.650617	0	1/2	4	3/2	.036844						
			1/2	6				15/2	.130797						
11/2	5	0	1/2	2	9/2	.105836	0	1/2	4	9/2	-.543502				
			1/2		2	11/2				-.001744					
0	1/2	2	15/2	.438483	0	1/2	4	11/2	-.121849						
			1/2	4				3/2	-.218864						
0	1/2	4	5/2	.101028	0	1/2	5	5/2	-.332497						
			1/2	4				9/2	-.075587						
0	1/2	4	11/2	-.068454	0	1/2	5	9/2	.223964						
			1/2	4				15/2	.219613						
0	1/2	5	3/2	-.459068	0	1/2	5	11/2	-.355960						
			1/2	5				5/2	-.199986						
0	1/2	5	9/2	-.084587	0	1/2	5	15/2	.065283						
			1/2	5				11/2	-.434780						
0	1/2	5	15/2	.240865	0	1/2	8	5/2	.014860						
			1/2	8				5/2	-.096466						
0	1/2	8	9/2	.202461	0	1/2	8	9/2	-.085928						
			1/2	8				11/2	-.266734						
0	1/2	8	15/2	.231095	0	1/2	8	11/2	.127636						
			1/2	2				9/2	.450305						
1	1/2	2	11/2	.289309	1	1/2	2	9/2	-.129900						
			1/2	2				15/2	-.122562						
1	1/2	4	3/2	-.330434	1	1/2	2	11/2	.229101						
			1/2	4				5/2	-.219440						
1	1/2	4	9/2	-.051261	1	1/2	2	15/2	-.175847						
			1/2	4				11/2	.346763						
1	1/2	4	15/2	.139211	1	1/2	4	3/2	.564661						
			1/2	4				9/2	-.051261						
1	1/2	6	3/2	.488282	13/2	1	0	1/2	2	9/2	-.359722				
			1/2	6				5/2	.346605						
0	1/2	4	11/2	-.156647	0	1/2	6	15/2	.059102						
			1/2	4				15/2	.038685						
1	1/2	6	3/2	.380124	1	1/2	6	5/2	-.323088						
			1/2	6				9/2	.020961						
1	1/2	6	11/2	-.291842	1	1/2	6	11/2	-.291842						
			1/2	6				15/2	.452892						
0	1/2	4	9/2	-.056297	0	1/2	4	5/2	-.056297						

See page 321 for Explanation of Tables

TABLE II. The Transformation Coefficients $D_{(v)l\alpha; J, J_\mu}^{T, T_\mu, J}$

J	α	T_λ	T_μ	J_λ	J_μ	D	J	α	T_λ	T_μ	J_λ	J_μ	D		
$v = 5 \quad \tau = 1/2$															
13/2	1	0	1/2	4	9/2	.001008	13/2	3	0	1/2	8	5/2	-.491794		
		0	1/2	4	11/2	-.197569			0	1/2	8	9/2	.391184		
		0	1/2	4	15/2	-.108939			0	1/2	8	11/2	.038701		
		0	1/2	5	3/2	-.107250			0	1/2	8	15/2	.035210		
		0	1/2	5	5/2	.098518			1	1/2	2	9/2	.059545		
		0	1/2	5	9/2	-.281543			1	1/2	2	11/2	-.198154		
		0	1/2	5	11/2	.103331			1	1/2	2	15/2	.522365		
		0	1/2	5	15/2	.175033			1	1/2	4	5/2	-.070289		
		0	1/2	8	3/2	.407545			1	1/2	4	9/2	.098053		
		0	1/2	8	5/2	-.221901			1	1/2	4	11/2	-.205573		
		0	1/2	8	9/2	-.456502			1	1/2	4	15/2	.089835		
		0	1/2	8	11/2	.121767			1	1/2	6	3/2	-.513827		
		0	1/2	8	15/2	-.162473			1	1/2	6	5/2	.348211		
		1	1/2	2	9/2	.029470			1	1/2	6	9/2	-.166745		
		1	1/2	2	11/2	.055212			1	1/2	6	11/2	-.396655		
		1	1/2	2	15/2	.227970			1	1/2	6	15/2	.221428		
		1	1/2	4	5/2	.012677			13/2	4	0	1/2	2	9/2	-.123586
		1	1/2	4	9/2	.118280					0	1/2	2	11/2	-.052132
		1	1/2	4	11/2	.258006					0	1/2	2	15/2	-.142233
		1	1/2	4	15/2	-.632627					0	1/2	4	5/2	-.016469
1	1/2	6	3/2	.182505	0	1/2	4	9/2			-.430721				
1	1/2	6	5/2	-.078398	0	1/2	4	11/2			-.184931				
1	1/2	6	9/2	-.577709	0	1/2	4	15/2			.046401				
1	1/2	6	11/2	-.172367	0	1/2	5	3/2			-.019562				
1	1/2	6	15/2	-.245490	0	1/2	5	5/2			.199360				
13/2	2	0	1/2	2	9/2	.217008	0	1/2			5	9/2	-.278872		
		0	1/2	2	11/2	.160689	0	1/2			5	11/2	.291526		
		0	1/2	2	15/2	.308420	0	1/2			5	15/2	-.221234		
		0	1/2	4	5/2	-.172517	0	1/2			8	3/2	-.010697		
		0	1/2	4	9/2	-.252461	0	1/2			8	5/2	.052585		
		0	1/2	4	11/2	-.118072	0	1/2			8	9/2	-.099702		
		0	1/2	4	15/2	.126705	0	1/2			8	11/2	-.590855		
		0	1/2	5	3/2	-.414612	0	1/2			8	15/2	.354790		
		0	1/2	5	5/2	.367504	1	1/2			2	9/2	.102631		
		0	1/2	5	9/2	.581815	1	1/2			2	11/2	-.488248		
		0	1/2	5	11/2	.099779	1	1/2			2	15/2	-.362780		
		0	1/2	5	15/2	.047455	1	1/2	4	5/2	-.371539				
		0	1/2	8	3/2	.084597	1	1/2	4	9/2	.297581				
		0	1/2	8	5/2	.156629	1	1/2	4	11/2	-.185485				
		0	1/2	8	9/2	.037293	1	1/2	4	15/2	-.360254				
		0	1/2	8	11/2	.070440	1	1/2	6	3/2	.050228				
		0	1/2	8	15/2	.112916	1	1/2	6	5/2	-.189195				
		1	1/2	2	9/2	-.337308	1	1/2	6	9/2	.255900				
		1	1/2	2	11/2	-.174731	1	1/2	6	11/2	-.322247				
		1	1/2	2	15/2	-.063304	1	1/2	6	15/2	.145061				
1	1/2	4	5/2	.011786	13/2	5	0	1/2	2	9/2	.115177				
1	1/2	4	9/2	-.505880			0	1/2	2	11/2	-.221110				
1	1/2	4	11/2	-.621908			0	1/2	2	15/2	.103951				
1	1/2	4	15/2	.034811			0	1/2	4	5/2	-.050689				
1	1/2	6	3/2	.267467			0	1/2	4	9/2	.360502				
1	1/2	6	5/2	-.075517			0	1/2	4	11/2	-.339332				
1	1/2	6	9/2	-.338648			0	1/2	4	15/2	-.386975				
1	1/2	6	11/2	-.124111			0	1/2	5	3/2	-.037834				
1	1/2	6	15/2	-.017989			0	1/2	5	5/2	-.255343				
13/2	3	0	1/2	2			9/2	-.041106	0	1/2	5	9/2	.305538		
		0	1/2	2			11/2	.303853	0	1/2	5	11/2	.020765		
		0	1/2	2			15/2	-.288201	0	1/2	5	15/2	-.363042		
		0	1/2	4			5/2	.058478	0	1/2	8	3/2	.072044		
		0	1/2	4			9/2	-.202842	0	1/2	8	5/2	-.312035		
		0	1/2	4			11/2	-.017360	0	1/2	8	9/2	-.078327		
		0	1/2	4			15/2	-.445864	0	1/2	8	11/2	-.108662		
		0	1/2	5			3/2	-.110468	0	1/2	8	15/2	.341902		
		0	1/2	5			5/2	.060980	1	1/2	2	9/2	.203352		
		0	1/2	5			9/2	.018911	1	1/2	2	11/2	-.060196		
		0	1/2	5			11/2	.167067	1	1/2	2	15/2	.221850		
		0	1/2	5	15/2	.366428	1	1/2	4	5/2	.661430				
		0	1/2	8	3/2	.056383	1	1/2	4	9/2	-.056709				

See page 321 for Explanation of Tables

TABLE II. The Transformation Coefficients $D_{(v)\alpha; J, \mu}^{T_\lambda T_\mu J}$

J	α	T_λ	T_μ	J_λ	J_μ	D	J	α	T_λ	T_μ	J_λ	J_μ	D					
						$v = 5$												
						$\frac{1}{2} = 1/2$												
13/2	5	1	1/2	4	11/2	-.049950	15/2	1	0	1/2	4	9/2	.203837					
		1	1/2	4	15/2	-.143722			0	1/2	4	11/2	-.365886					
		1	1/2	6	3/2	.401204			0	1/2	4	15/2	-.342662					
		1	1/2	6	5/2	.069403			0	1/2	5	5/2	.076665					
		1	1/2	6	9/2	.385951			0	1/2	5	9/2	.180141					
		1	1/2	6	11/2	-.328114			0	1/2	5	11/2	.255175					
13/2	6	1	1/2	6	15/2	.139826	0	1/2	5	15/2	.131340	15/2	2	0	1/2	8	3/2	-.000312
		0	1/2	2	9/2	-.273226	0	1/2	8	5/2	.363994							
		0	1/2	2	11/2	.519028	0	1/2	8	9/2	.086203							
		0	1/2	2	15/2	.009103	0	1/2	8	11/2	-.503675							
		0	1/2	4	5/2	-.045955	0	1/2	8	15/2	-.429978							
		0	1/2	4	9/2	.013449	1	1/2	2	11/2	.555305							
		0	1/2	4	11/2	.043640	1	1/2	2	15/2	.375443							
		0	1/2	4	15/2	.024909	1	1/2	4	9/2	-.017407							
		0	1/2	5	3/2	.103931	1	1/2	4	11/2	-.379346							
		0	1/2	5	5/2	-.106101	1	1/2	4	15/2	-.210270							
		0	1/2	5	9/2	.020435	1	1/2	6	3/2	-.030741							
		0	1/2	5	11/2	-.332383	1	1/2	6	5/2	.129428							
		0	1/2	5	15/2	-.369454	1	1/2	6	9/2	.292077							
		0	1/2	8	3/2	.491404	1	1/2	6	11/2	.491550							
		0	1/2	8	5/2	.178166	1	1/2	6	15/2	-.132785							
		0	1/2	8	9/2	.298699	0	1/2	2	11/2	-.280531							
		0	1/2	8	11/2	-.052020	0	1/2	2	15/2	-.348263							
		0	1/2	8	15/2	.128286	0	1/2	4	9/2	.102237							
1	1/2	2	9/2	-.708006	0	1/2	4	11/2	-.346728									
1	1/2	2	11/2	.250901	0	1/2	4	15/2	.036907									
1	1/2	2	15/2	.111615	0	1/2	5	5/2	.090698									
1	1/2	4	5/2	.155843	0	1/2	5	9/2	-.148376									
1	1/2	4	9/2	.528794	0	1/2	5	11/2	.199155									
1	1/2	4	11/2	-.222052	0	1/2	5	15/2	-.306766									
1	1/2	4	15/2	-.147191	0	1/2	8	3/2	-.487827									
1	1/2	6	3/2	-.021180	0	1/2	8	5/2	.193353									
1	1/2	6	5/2	-.081732	0	1/2	8	9/2	.278316									
1	1/2	6	9/2	.128672	0	1/2	8	11/2	.387308									
1	1/2	6	11/2	.078059	0	1/2	8	15/2	-.033797									
1	1/2	6	15/2	.136594	1	1/2	2	11/2	.346529									
13/2	7	0	1/2	2	9/2	.040257	1	1/2	2	15/2	-.506148	15/2	3	0	1/2	2	11/2	-.013677
		0	1/2	2	11/2	.029062	1	1/2	2	15/2	-.075328							
		0	1/2	2	15/2	.221127	1	1/2	4	9/2	-.042530							
		0	1/2	4	5/2	.514105	1	1/2	4	11/2	-.069903							
		0	1/2	4	9/2	-.119219	1	1/2	4	15/2	-.518388							
		0	1/2	4	11/2	.590427	1	1/2	6	3/2	-.287835							
		0	1/2	4	15/2	-.275440	1	1/2	6	5/2	.312020							
		0	1/2	5	3/2	-.058126	1	1/2	6	9/2	-.354999							
		0	1/2	5	5/2	-.215400	1	1/2	6	11/2	-.127998							
		0	1/2	5	9/2	.128317	1	1/2	6	15/2	.160305							
		0	1/2	5	11/2	.319378	0	1/2	2	11/2	-.013677							
		0	1/2	5	15/2	-.089174	0	1/2	2	15/2	-.075328							
		0	1/2	8	3/2	.117289	0	1/2	4	9/2	.130426							
		0	1/2	8	5/2	.154308	0	1/2	4	11/2	-.333474							
		0	1/2	8	9/2	-.149119	0	1/2	4	15/2	-.092963							
		0	1/2	8	11/2	-.051354	0	1/2	5	5/2	.162955							
		0	1/2	8	15/2	.083742	0	1/2	5	9/2	-.209595							
		1	1/2	2	9/2	.083363	0	1/2	5	11/2	-.301264							
		1	1/2	2	11/2	.405093	0	1/2	5	15/2	.491937							
		1	1/2	2	15/2	-.297883	0	1/2	8	3/2	.041711							
		1	1/2	4	5/2	-.215234	0	1/2	8	5/2	.388982							
		1	1/2	4	9/2	.052834	0	1/2	8	9/2	-.369171							
		1	1/2	4	11/2	-.097790	0	1/2	8	11/2	.179728							
		1	1/2	4	15/2	-.121783	0	1/2	8	15/2	.363865							
1	1/2	6	3/2	.285455	1	1/2	2	11/2	.244266									
1	1/2	6	5/2	.709785	1	1/2	2	15/2	-.159042									
1	1/2	6	9/2	-.075077	1	1/2	4	9/2	.383133									
1	1/2	6	11/2	-.075113	1	1/2	4	11/2	-.130909									
1	1/2	6	15/2	.264854	1	1/2	4	15/2	.330687									
15/2	1	0	1/2	2	11/2	.061853	1	1/2	6	3/2	.376637	15/2	3	1	1/2	6	5/2	-.004176
		0	1/2	2	15/2	.064420	1	1/2	6	9/2	-.004176							

See page 321 for Explanation of Tables

TABLE II. The Transformation Coefficients $D_{(v) \alpha_i J_i \mu_i}^{T_\lambda T_\mu J}$

J	α	T_λ	T_μ	J_i	J_μ	D	J	α	T_λ	T_μ	J_i	J_μ	D
$v = 5 \quad t = 1/2$													
15/2	3	1	1/2	6	9/2	-.100350	15/2	6	1	1/2	4	9/2	.044619
		1	1/2	6	11/2	.167380			1	1/2	4	11/2	-.218266
		1	1/2	6	15/2	.679558			1	1/2	4	15/2	-.000492
15/2	4	0	1/2	2	11/2	-.094173			1	1/2	6	3/2	.225510
		0	1/2	2	15/2	-.484010			1	1/2	6	5/2	.422259
		0	1/2	4	9/2	.363651			1	1/2	6	9/2	-.152699
		0	1/2	4	11/2	.293829			1	1/2	6	11/2	.552546
		0	1/2	4	15/2	.054733			1	1/2	6	15/2	-.235979
		0	1/2	5	5/2	-.389620	15/2	7	0	1/2	2	11/2	-.211564
		0	1/2	5	9/2	.373833			0	1/2	2	15/2	.189951
		0	1/2	5	11/2	-.097766			0	1/2	4	9/2	.163424
		0	1/2	5	15/2	.128611			0	1/2	4	11/2	.548090
		0	1/2	8	3/2	-.334020			0	1/2	4	15/2	.431970
		0	1/2	8	5/2	.010271			0	1/2	5	5/2	-.347692
		0	1/2	8	9/2	-.262054			0	1/2	5	9/2	-.202289
		0	1/2	8	11/2	-.189123			0	1/2	5	11/2	-.097884
		0	1/2	8	15/2	.039035			0	1/2	5	15/2	.091305
		1	1/2	2	11/2	-.203614			0	1/2	8	3/2	.263970
		1	1/2	2	15/2	.247350			0	1/2	8	5/2	-.170994
		1	1/2	4	9/2	.544453			0	1/2	8	9/2	.071343
		1	1/2	4	11/2	-.379875			0	1/2	8	11/2	.142522
		1	1/2	4	15/2	-.199653			0	1/2	8	15/2	.318435
		1	1/2	6	3/2	-.254089			1	1/2	2	11/2	-.210958
		1	1/2	6	5/2	-.398494			1	1/2	2	15/2	.122104
		1	1/2	6	9/2	-.432572			1	1/2	4	9/2	-.159289
		1	1/2	6	11/2	.006533			1	1/2	4	11/2	.191868
		1	1/2	6	15/2	-.079016			1	1/2	4	15/2	.227176
15/2	5	0	1/2	2	11/2	.507392			1	1/2	6	3/2	.108084
		0	1/2	2	15/2	-.191303			1	1/2	6	5/2	-.567186
		0	1/2	4	9/2	-.321770			1	1/2	6	9/2	-.168156
		0	1/2	4	11/2	-.323731			1	1/2	6	11/2	-.679140
		0	1/2	4	15/2	.182043			1	1/2	6	15/2	.062467
		0	1/2	5	5/2	-.045072	17/2	1	0	1/2	2	15/2	.355568
		0	1/2	5	9/2	.445533			0	1/2	4	9/2	.252462
		0	1/2	5	11/2	.325210			0	1/2	4	11/2	.248563
		0	1/2	5	15/2	-.027472			0	1/2	4	15/2	-.482703
		0	1/2	8	3/2	.058962			0	1/2	5	9/2	.235854
		0	1/2	8	5/2	-.014615			0	1/2	5	11/2	.273853
		0	1/2	8	9/2	-.293985			0	1/2	5	15/2	.196408
		0	1/2	8	11/2	.259244			0	1/2	8	3/2	.024170
		0	1/2	8	15/2	.010389			0	1/2	8	5/2	.086766
		1	1/2	2	11/2	-.083875			0	1/2	8	9/2	.323259
		1	1/2	2	15/2	-.004131			0	1/2	8	11/2	.456541
		1	1/2	4	9/2	.529704			0	1/2	8	15/2	.157516
		1	1/2	4	11/2	.446785			1	1/2	2	15/2	.114651
		1	1/2	4	15/2	.042390			1	1/2	4	9/2	.206378
		1	1/2	6	3/2	-.525302			1	1/2	4	11/2	.209322
		1	1/2	6	5/2	.267262			1	1/2	4	15/2	.121778
		1	1/2	6	9/2	.340763			1	1/2	6	5/2	-.628086
		1	1/2	6	11/2	.198274			1	1/2	6	9/2	-.297446
		1	1/2	6	15/2	.090246			1	1/2	6	11/2	.537148
15/2	6	0	1/2	2	11/2	.109526			1	1/2	6	15/2	-.337821
		0	1/2	2	15/2	-.196816	17/2	2	0	1/2	2	15/2	-.020677
		0	1/2	4	9/2	-.315286			0	1/2	4	9/2	.095289
		0	1/2	4	11/2	-.021415			0	1/2	4	11/2	.196391
		0	1/2	4	15/2	-.482179			0	1/2	4	15/2	-.106065
		0	1/2	5	5/2	.393598			0	1/2	5	9/2	-.109089
		0	1/2	5	9/2	.062547			0	1/2	5	11/2	-.057341
		0	1/2	5	11/2	-.421768			0	1/2	5	15/2	-.156268
		0	1/2	5	15/2	-.181503			0	1/2	8	3/2	.070251
		0	1/2	8	3/2	-.324405			0	1/2	8	5/2	.090636
		0	1/2	8	5/2	-.282678			0	1/2	8	9/2	-.374686
		0	1/2	8	9/2	-.190553			0	1/2	8	11/2	.409416
		0	1/2	8	11/2	-.122362			0	1/2	8	15/2	-.761515
		0	1/2	8	15/2	-.104004			1	1/2	2	15/2	.406676
		1	1/2	2	11/2	-.501698			1	1/2	4	9/2	-.112603
		1	1/2	2	15/2	-.291891			1	1/2	4	11/2	-.175557

See page 321 for Explanation of Tables

TABLE II. The Transformation Coefficients $D_{(v) \alpha; J \lambda J \mu}^{T \lambda T \mu J}$

J	α	T_λ	T_μ	J_λ	J_μ	D	J	α	T_λ	T_μ	J_λ	J_μ	D
						$v = 5$							
						$k = 1/2$							
17/2	2	1	1/2	4	15/2	.653033	19/2	1	0	1/2	4	15/2	.070853
		1	1/2	6	5/2	-.200323			0	1/2	5	9/2	.014617
		1	1/2	6	9/2	-.325386			0	1/2	5	11/2	-.430905
		1	1/2	6	11/2	-.327981			0	1/2	5	15/2	-.207108
		1	1/2	6	15/2	.333296			0	1/2	8	3/2	-.368957
17/2	3	0	1/2	2	15/2	-.421140			0	1/2	8	5/2	-.064985
		0	1/2	4	9/2	-.467730			0	1/2	8	9/2	.476769
		0	1/2	4	11/2	.181284			0	1/2	8	11/2	.284462
		0	1/2	4	15/2	-.327467			0	1/2	8	15/2	.022750
		0	1/2	5	9/2	-.016243			1	1/2	2	15/2	-.220331
		0	1/2	5	11/2	-.042088			1	1/2	4	11/2	-.049069
		0	1/2	5	15/2	.211416			1	1/2	4	15/2	.553104
		0	1/2	8	3/2	-.392260			1	1/2	6	9/2	.786592
		0	1/2	8	5/2	.508687			1	1/2	6	11/2	.138149
		0	1/2	8	9/2	-.033862			1	1/2	6	15/2	.072872
		0	1/2	8	11/2	.013300	19/2	2	0	1/2	2	15/2	-.042179
		0	1/2	8	15/2	.055551			0	1/2	4	11/2	.186438
		1	1/2	2	15/2	.340878			0	1/2	4	15/2	-.309171
		1	1/2	4	9/2	-.515918			0	1/2	5	9/2	.157094
		1	1/2	4	11/2	.655512			0	1/2	5	11/2	.085271
		1	1/2	4	15/2	-.139855			0	1/2	5	15/2	-.281148
		1	1/2	6	5/2	-.134646			0	1/2	8	3/2	-.124515
		1	1/2	6	9/2	.149835			0	1/2	8	5/2	-.063888
		1	1/2	6	11/2	-.297453			0	1/2	8	9/2	.348363
		1	1/2	6	15/2	-.198286			0	1/2	8	11/2	-.712052
17/2	4	0	1/2	2	15/2	.110148			0	1/2	8	15/2	-.330031
		0	1/2	4	9/2	-.127897			1	1/2	2	15/2	.485570
		0	1/2	4	11/2	-.001976			1	1/2	4	11/2	-.371729
		0	1/2	4	15/2	.352611			1	1/2	4	15/2	.380347
		0	1/2	5	9/2	.193602			1	1/2	6	9/2	-.116784
		0	1/2	5	11/2	-.206432			1	1/2	6	11/2	.137896
		0	1/2	5	15/2	.629405			1	1/2	6	15/2	-.669867
		0	1/2	8	3/2	-.259994	19/2	3	0	1/2	2	15/2	.324820
		0	1/2	8	5/2	-.209641			0	1/2	4	11/2	-.239569
		0	1/2	8	9/2	.327453			0	1/2	4	15/2	-.165736
		0	1/2	8	11/2	.066245			0	1/2	5	9/2	.507178
		0	1/2	8	15/2	-.384402			0	1/2	5	11/2	-.296098
		1	1/2	2	15/2	-.198677			0	1/2	5	15/2	-.171226
		1	1/2	4	9/2	.012637			0	1/2	8	3/2	-.327969
		1	1/2	4	11/2	.468030			0	1/2	8	5/2	-.427796
		1	1/2	4	15/2	.194944			0	1/2	8	9/2	-.369127
		1	1/2	6	5/2	.565930			0	1/2	8	11/2	.006346
		1	1/2	6	9/2	-.604178			0	1/2	8	15/2	.092416
		1	1/2	6	11/2	.134020			1	1/2	2	15/2	-.571381
		1	1/2	6	15/2	-.006558			1	1/2	4	11/2	.382569
17/2	5	0	1/2	2	15/2	-.289761			1	1/2	4	15/2	.286186
		0	1/2	4	9/2	.302480			1	1/2	6	9/2	-.224610
		0	1/2	4	11/2	.128845			1	1/2	6	11/2	-.377256
		0	1/2	4	15/2	.040827			1	1/2	6	15/2	-.502485
		0	1/2	5	9/2	.290807	19/2	4	0	1/2	2	15/2	.135401
		0	1/2	5	11/2	.573828			0	1/2	4	11/2	.388080
		0	1/2	5	15/2	.194341			0	1/2	4	15/2	.504541
		0	1/2	8	3/2	-.424050			0	1/2	5	9/2	.143442
		0	1/2	8	5/2	-.366846			0	1/2	5	11/2	.002439
		0	1/2	8	9/2	-.196434			0	1/2	5	15/2	-.358152
		0	1/2	8	11/2	-.025869			0	1/2	8	3/2	-.397424
		0	1/2	8	15/2	.031791			0	1/2	8	5/2	.470546
		1	1/2	2	15/2	-.530515			0	1/2	8	9/2	-.156429
		1	1/2	4	9/2	-.679812			0	1/2	8	11/2	-.066029
		1	1/2	4	11/2	-.134999			0	1/2	8	15/2	.139481
		1	1/2	4	15/2	.373329			1	1/2	2	15/2	.218931
		1	1/2	6	5/2	-.104320			1	1/2	4	11/2	.658658
		1	1/2	6	9/2	.135847			1	1/2	4	15/2	.351218
		1	1/2	6	11/2	.255888			1	1/2	6	9/2	-.255805
		1	1/2	6	15/2	-.063205			1	1/2	6	11/2	.553706
19/2	1	0	1/2	2	15/2	-.538483			1	1/2	6	15/2	.151189
		0	1/2	4	11/2	-.164716	21/2	1	0	1/2	4	15/2	.384911

See page 321 for Explanation of Tables

TABLE II. The Transformation Coefficients $D_{(v)\alpha; J\lambda J\mu}^{T_s T_\mu J}$

J	α	T_s	T_μ	J_λ	J_μ	D	J	α	T_s	T_μ	J_λ	J_μ	D
$v = 5 \quad t = 1/2$													
21/2	1	0	1/2	5	11/2	.563221	21/2	3	1	1/2	4	15/2	.448223
		0	1/2	5	15/2	-.290725			1	1/2	6	9/2	.688424
		0	1/2	8	5/2	.231162			1	1/2	6	11/2	-.400903
		0	1/2	8	9/2	.497551			1	1/2	6	15/2	-.405518
		0	1/2	8	11/2	.328762	23/2	1	0	1/2	4	15/2	.517790
		0	1/2	8	15/2	.202551			0	1/2	5	15/2	-.019417
		1	1/2	4	15/2	-.456196			0	1/2	8	9/2	.376851
		1	1/2	6	9/2	-.370294			0	1/2	8	11/2	-.767619
		1	1/2	6	11/2	-.512556			0	1/2	8	15/2	.016156
		1	1/2	6	15/2	-.626142			1	1/2	4	15/2	-.719985
21/2	2	0	1/2	4	15/2	-.237235			1	1/2	6	11/2	-.460504
		0	1/2	5	11/2	-.033899			1	1/2	6	15/2	.519189
		0	1/2	5	15/2	.334518	23/2	2	0	1/2	4	15/2	.198961
		0	1/2	8	5/2	-.002135			0	1/2	5	15/2	-.572883
		0	1/2	8	9/2	.217825			0	1/2	8	9/2	-.619562
		0	1/2	8	11/2	-.224006			0	1/2	8	11/2	-.145435
		0	1/2	8	15/2	.856176			0	1/2	8	15/2	.476667
		1	1/2	4	15/2	-.369371			1	1/2	4	15/2	.612830
		1	1/2	6	9/2	.347692			1	1/2	6	11/2	-.772955
		1	1/2	6	11/2	.696889			1	1/2	6	15/2	.164255
		1	1/2	6	15/2	-.506972	25/2	1	0	1/2	5	15/2	.507093
21/2	3	0	1/2	4	15/2	.494767			0	1/2	8	9/2	.419790
		0	1/2	5	11/2	.000000			0	1/2	8	11/2	.558291
		0	1/2	5	15/2	.589971			0	1/2	8	15/2	.504921
		0	1/2	8	5/2	.588693			1	1/2	6	15/2	1.00000
		0	1/2	8	9/2	-.194583	27/2	1	0	1/2	8	11/2	-.414039
		0	1/2	8	11/2	-.129907			0	1/2	8	15/2	.910259
		0	1/2	8	15/2	-.076431			1	1/2	6	15/2	-.100000
$v = 5 \quad t = 3/2$													
1/2	1	0	3/2	4	7/2	-1.00000	5/2	2	1	1/2	4	11/2	-.396843
		1	1/2	2	3/2	.175933			1	1/2	6	9/2	-.115543
		1	1/2	2	5/2	-.891316			1	1/2	6	11/2	.012805
		1	1/2	4	9/2	-.188982			1	1/2	6	15/2	-.225254
		1	1/2	6	11/2	.372678	7/2	1	0	3/2	2	7/2	1.00000
3/2	1	0	3/2	2	7/2	.715678			0	3/2	4	7/2	.000000
		0	3/2	4	7/2	.000000			0	3/2	5	7/2	.000000
		0	3/2	5	7/2	-.698430			1	1/2	2	3/2	.163478
		1	1/2	2	3/2	.202195			1	1/2	2	5/2	-.107583
		1	1/2	2	5/2	-.167997			1	1/2	2	9/2	.425565
		1	1/2	4	5/2	.056359			1	1/2	2	11/2	-.041031
		1	1/2	4	9/2	-.145111			1	1/2	4	3/2	.563465
		1	1/2	4	11/2	-.425718			1	1/2	4	5/2	-.074536
		1	1/2	6	9/2	.643373			1	1/2	4	9/2	.478591
		1	1/2	6	11/2	-.259582			1	1/2	4	11/2	-.172754
		1	1/2	6	15/2	-.494079			1	1/2	4	15/2	.000000
3/2	2	0	3/2	2	7/2	-.122806			1	1/2	6	5/2	.173472
		0	3/2	4	7/2	-.597935			1	1/2	6	9/2	-.295454
		0	3/2	5	7/2	-.125839			1	1/2	6	11/2	-.282106
		1	1/2	2	3/2	-.316109			1	1/2	6	15/2	.000000
		1	1/2	2	5/2	-.022234	7/2	2	0	3/2	2	7/2	.000000
		1	1/2	4	5/2	.373645			0	3/2	4	7/2	-1.00000
		1	1/2	4	9/2	-.107033			0	3/2	5	7/2	.000000
		1	1/2	4	11/2	.436251			1	1/2	2	3/2	.176828
		1	1/2	6	9/2	-.136223			1	1/2	2	5/2	-.310316
		1	1/2	6	11/2	-.549031			1	1/2	2	9/2	.081400
		1	1/2	6	15/2	-.312570			1	1/2	2	11/2	.369844
5/2	2	0	3/2	2	7/2	-.262265			1	1/2	4	3/2	-.194952
		0	3/2	4	7/2	-.507093			1	1/2	4	5/2	.439759
		0	3/2	5	7/2	.821020			1	1/2	4	9/2	-.099383
		1	1/2	2	3/2	-.466880			1	1/2	4	11/2	.215610
		1	1/2	2	5/2	.071824			1	1/2	4	15/2	-.083201
		1	1/2	2	9/2	.437409			1	1/2	6	5/2	.227441
		1	1/2	4	3/2	-.121405			1	1/2	6	9/2	.126068
		1	1/2	4	5/2	-.532663			1	1/2	6	11/2	-.508574
		1	1/2	4	9/2	-.255599			1	1/2	6	15/2	-.328746

See page 321 for Explanation of Tables

TABLE II. The Transformation Coefficients $D_{(v) \alpha; J \lambda J \mu}^{T \lambda T \mu J}$

J	α	T_λ	T_μ	J_λ	J_μ	D	J	α	T_λ	T_μ	J_λ	J_μ	D
$v = 5 \quad t = 3/2$													
7/2	3	0	3/2	2	7/2	.000000	11/2	1	0	3/2	2	7/2	.947291
		0	3/2	4	7/2	.000000			0	3/2	4	7/2	.000000
		0	3/2	5	7/2	1.000000			0	3/2	5	7/2	.000000
		1	1/2	2	3/2	.412599			0	3/2	8	7/2	-.320374
		1	1/2	2	5/2	-.077579			1	1/2	2	9/2	-.175275
		1	1/2	2	9/2	-.142451			1	1/2	2	11/2	-.260037
		1	1/2	2	11/2	.369844			1	1/2	2	15/2	.223170
		1	1/2	4	3/2	.215473			1	1/2	4	3/2	.046223
		1	1/2	4	5/2	.317604			1	1/2	4	5/2	-.044316
		1	1/2	4	9/2	.157243			1	1/2	4	9/2	-.491426
		1	1/2	4	11/2	-.263523			1	1/2	4	11/2	-.332302
		1	1/2	4	15/2	.303089			1	1/2	4	15/2	-.142697
		1	1/2	6	5/2	.030617			1	1/2	6	3/2	.372662
		1	1/2	6	9/2	.346688			1	1/2	6	5/2	-.140140
		1	1/2	6	11/2	.430332			1	1/2	6	9/2	-.519625
		9/2	1	1	1/2	6			15/2	.164373	1	1/2	6
0	3/2			2	7/2	.674466	1	1/2	6	15/2	-.162559		
0	3/2			4	7/2	.000000	11/2	2	0	3/2	2	7/2	.216937
0	3/2			5	7/2	.000000			0	3/2	4	7/2	-.735856
0	3/2			8	7/2	.738306			0	3/2	5	7/2	.000000
1	1/2			2	5/2	-.024310			0	3/2	8	7/2	.641447
1	1/2			2	9/2	-.061413			1	1/2	2	9/2	-.382491
1	1/2			2	11/2	-.284145			1	1/2	2	11/2	.130916
1	1/2			4	3/2	.182815			1	1/2	2	15/2	-.500194
1	1/2			4	5/2	-.083447			1	1/2	4	3/2	.132469
1	1/2			4	9/2	.077034			1	1/2	4	5/2	-.441615
1	1/2			4	11/2	-.024689			1	1/2	4	9/2	-.213678
1	1/2			4	15/2	-.638974			1	1/2	4	11/2	-.116960
1	1/2			6	3/2	.474643			1	1/2	4	15/2	.105675
1	1/2			6	5/2	-.041741			1	1/2	6	3/2	-.040639
1	1/2			6	9/2	.421212			1	1/2	6	5/2	.479563
1	1/2	6	11/2	.130507	1	1/2			6	9/2	-.110147		
9/2	2	1	1/2	6	15/2	-.195454			1	1/2	6	11/2	.206143
		0	3/2	2	7/2	-.122657	1	1/2	6	15/2	.130504		
		0	3/2	4	7/2	-.986103	11/2	3	0	3/2	2	7/2	.110849
		0	3/2	5	7/2	.000000			0	3/2	4	7/2	.318390
		0	3/2	8	7/2	.112051			0	3/2	5	7/2	.882560
		1	1/2	2	5/2	-.494005			0	3/2	8	7/2	.327763
		1	1/2	2	9/2	.108025			1	1/2	2	9/2	.127619
		1	1/2	2	11/2	-.515089			1	1/2	2	11/2	-.112840
		1	1/2	4	3/2	.070871			1	1/2	2	15/2	-.021771
		1	1/2	4	5/2	.227076			1	1/2	4	3/2	.386195
		1	1/2	4	9/2	.062937			1	1/2	4	5/2	.245445
		1	1/2	4	11/2	.179710			1	1/2	4	9/2	-.508374
		1	1/2	4	15/2	.070857			1	1/2	4	11/2	.156427
		1	1/2	6	3/2	-.016139			1	1/2	4	15/2	.502985
		1	1/2	6	5/2	-.502597			1	1/2	6	3/2	.213343
		1	1/2	6	9/2	-.178391			1	1/2	6	5/2	-.035573
1	1/2	6	11/2	.125866	1	1/2			6	9/2	.380621		
1	1/2	6	15/2	.283865	1	1/2			6	11/2	.181427		
9/2	3	0	3/2	2	7/2	.452160	1	1/2	6	15/2	-.025308		
		0	3/2	4	7/2	-.103179	13/2	1	0	3/2	4	7/2	-1.000000
		0	3/2	5	7/2	.783764			0	3/2	5	7/2	.000000
		0	3/2	8	7/2	-.413062			0	3/2	8	7/2	.000000
		1	1/2	2	5/2	.185911			1	1/2	2	9/2	-.050927
		1	1/2	2	9/2	-.574751			1	1/2	2	11/2	.435831
		1	1/2	2	11/2	.025028			1	1/2	2	15/2	.175090
		1	1/2	4	3/2	-.185351			1	1/2	4	5/2	-.366466
		1	1/2	4	5/2	-.282089			1	1/2	4	9/2	-.094448
		1	1/2	4	9/2	.196097			1	1/2	4	11/2	.175722
		1	1/2	4	11/2	.501397			1	1/2	4	15/2	.268715
		1	1/2	4	15/2	.063414			1	1/2	6	3/2	.208167
		1	1/2	6	3/2	.298255			1	1/2	6	5/2	-.404701
		1	1/2	6	5/2	-.162953			1	1/2	6	9/2	.067002
		1	1/2	6	9/2	-.123530			1	1/2	6	11/2	-.534036
		1	1/2	6	11/2	-.210583			1	1/2	6	15/2	.183567
1	1/2	6	15/2	.227056	13/2	2			0	3/2	4	7/2	.000000

See page 321 for Explanation of Tables

TABLE II. The Transformation Coefficients $D_{(v) \alpha; J \lambda J \mu}^{T \lambda T \mu J}$

J	α	T_λ	T_μ	J_λ	J_μ	D	J	α	T_λ	T_μ	J_λ	J_μ	D									
$v = 5 \quad \zeta = 3/2$																						
13/2	2	0	3/2	5	7/2	1.00000	15/2	2	1	1/2	2	15/2	.365844									
		0	3/2	8	7/2	.000000			1	1/2	4	9/2	.254719									
		1	1/2	2	9/2	.346237			1	1/2	4	11/2	.447816									
		1	1/2	2	11/2	.308893			1	1/2	4	15/2	-.457995									
		1	1/2	2	15/2	-.326824			1	1/2	6	3/2	.543203									
		1	1/2	4	5/2	.335393			1	1/2	6	5/2	.222799									
		1	1/2	4	9/2	.070321			1	1/2	6	9/2	-.181068									
		1	1/2	4	11/2	-.234669			1	1/2	6	11/2	-.091276									
		1	1/2	4	15/2	-.073402			1	1/2	6	15/2	-.064281									
		1	1/2	6	3/2	-.326599			17/2	1	0	3/2	5	7/2	1.00000							
		1	1/2	6	5/2	-.357158					0	3/2	8	7/2	.000000							
		1	1/2	6	9/2	-.313172					1	1/2	2	15/2	.274585							
		1	1/2	6	11/2	.000000					1	1/2	4	9/2	.173315							
		1	1/2	6	15/2	.409505					1	1/2	4	11/2	.273448							
13/2	3	0	3/2	4	7/2	.000000	1	1/2			4	15/2	.397712									
		0	3/2	5	7/2	.000000	1	1/2			6	5/2	.248734									
		0	3/2	8	7/2	-1.00000	1	1/2			6	9/2	.582853									
		1	1/2	2	9/2	-.287642	1	1/2			6	11/2	.446538									
		1	1/2	2	11/2	-.256617	1	1/2			6	15/2	.246239									
		1	1/2	2	15/2	.023373	17/2	2			0	3/2	5	7/2	.000000							
		1	1/2	4	5/2	.000000					0	3/2	8	7/2	-1.00000							
		1	1/2	4	9/2	-.318656					1	1/2	2	15/2	.281718							
		1	1/2	4	11/2	.450377					1	1/2	4	9/2	-.375393							
		1	1/2	4	15/2	-.170292			1	1/2	4	11/2	-.112221									
		1	1/2	6	3/2	.000000			1	1/2	4	15/2	-.448849									
		1	1/2	6	5/2	.000000			1	1/2	6	5/2	.000000									
		1	1/2	6	9/2	-.055652			1	1/2	6	9/2	-.239198									
		1	1/2	6	11/2	.176496			1	1/2	6	11/2	.446685									
1	1/2	6	15/2	.695151	1	1/2			6	15/2	.555800											
15/2	1	0	3/2	4	7/2	-.959285			19/2	1	0	3/2	8	7/2	-1.00000							
		0	3/2	5	7/2	.000000					1	1/2	2	15/2	.552771							
		0	3/2	8	7/2	-.282440					1	1/2	4	11/2	.500000							
		1	1/2	2	11/2	.260417					1	1/2	4	15/2	-.150756							
		1	1/2	2	15/2	-.393019	1	1/2			6	9/2	.392232									
		1	1/2	4	9/2	.050052	1	1/2			6	11/2	-.500000									
		1	1/2	4	11/2	.396189	1	1/2			6	15/2	-.133683									
		1	1/2	4	15/2	-.041383	21/2	1			0	3/2	8	7/2	-1.00000							
		1	1/2	6	3/2	.106739					1	1/2	4	15/2	.674200							
		1	1/2	6	5/2	-.573306					1	1/2	6	9/2	-.517750							
		1	1/2	6	9/2	-.086941					1	1/2	6	11/2	.301511							
		1	1/2	6	11/2	.424743					1	1/2	6	15/2	-.431834							
		1	1/2	6	15/2	-.297485					23/2	1	0	3/2	8	7/2	-1.00000					
		1	1/2	4	7/2	-.117635							1	1/2	4	15/2	.325669					
0	3/2	5	7/2	.909137	1	1/2			6	11/2			.436436									
0	3/2	8	7/2	.399539	1	1/2			6	15/2			.838727									
1	1/2	2	11/2	.031934	$v = 6 \quad \zeta = 0$																	
1	1	0	0	2	2	-.171129			1	2			1/2	1/2	3/2	5/2	.238684					
		0	0	4	4	-.876648							1/2	1/2	5/2	5/2	-.428199					
		0	0	4	5	.020742							1/2	1/2	9/2	9/2	.284446					
		0	0	5	5	.426280							1/2	1/2	9/2	11/2	.071843					
		0	0	8	8	.141630	1/2	1/2					11/2	11/2	-.177887							
		1/2	1/2	3/2	3/2	.303920	1/2	1/2					15/2	15/2	.167413							
		1/2	1/2	3/2	5/2	-.558653	1	3					0	0	2	2	-.526508					
		1/2	1/2	5/2	5/2	-.503290							0	0	4	4	-.055053					
		1/2	1/2	9/2	9/2	.205515							0	0	4	5	.614876					
		1/2	1/2	9/2	11/2	-.253483					0	0	5	5	-.469979							
		1/2	1/2	11/2	11/2	-.417938					0	0	8	8	.347571							
		1/2	1/2	15/2	15/2	.247136					1/2	1/2	3/2	3/2	-.100022							
		1	2	0	0	2					2	.706257	1/2	1/2	3/2	5/2	-.214517					
				0	0	4					4	-.349953	1/2	1/2	5/2	5/2	.219639					
0	0			4	5	-.007114			1/2	1/2	9/2	9/2	-.413855									
0	0			5	5	-.536157			1/2	1/2	9/2	11/2	.630799									
0	0			8	8	.302025			1/2	1/2	11/2	11/2	-.389107									
1/2	1/2			3/2	3/2	-.783539			1/2	1/2	15/2	15/2	.418508									

See page 321 for Explanation of Tables

TABLE II. The Transformation Coefficients $D_{(v) \alpha; J \lambda J_{\mu}}^{T_{\lambda} T_{\mu} J}$

J	α	T_{λ}	T_{μ}	J_{λ}	J_{μ}	D	J	α	T_{λ}	T_{μ}	J_{λ}	J_{μ}	D				
$v = 6 \quad t = 0$																	
1	4	0	0	2	2	-.421544	3	2	0	0	5	5	-.390857				
		0	0	4	4	-.062848			0	0	5	8	-.502543				
		0	0	4	5	-.788319			0	0	8	8	-.512580				
		0	0	5	5	-.350522			1/2	1/2	3/2	3/2	-.168382				
		0	0	8	8	.272101			1/2	1/2	3/2	5/2	.295394				
		1/2	1/2	3/2	5/2	.240438			1/2	1/2	3/2	9/2	-.098953				
		1/2	1/2	3/2	5/2	.299864			1/2	1/2	5/2	5/2	-.121158				
		1/2	1/2	5/2	5/2	-.663640			1/2	1/2	5/2	9/2	-.043754				
		1/2	1/2	9/2	9/2	-.507987			1/2	1/2	5/2	11/2	.044974				
		1/2	1/2	9/2	11/2	.138735			1/2	1/2	9/2	9/2	-.177676				
		1/2	1/2	11/2	11/2	.331771			1/2	1/2	9/2	11/2	-.060066				
		1/2	1/2	15/2	15/2	.156471			1/2	1/2	9/2	15/2	.636042				
		2	1	0	0	2			2	.000000	3	3	0	0	2	2	-.062662
				0	0	2			4	.328362			0	0	2	4	-.637680
0	0			4	4	.000000	0	0	2	5			.194671				
0	0			4	5	.944552	0	0	4	4			.176611				
0	0			5	5	.000000	0	0	4	5			.158715				
0	0			8	8	.000000	0	0	5	5			.469640				
1/2	1/2			3/2	3/2	.000000	0	0	5	8			-.481427				
1/2	1/2			3/2	5/2	.637201	0	0	8	8			-.206945				
1/2	1/2			5/2	5/2	.000000	1/2	1/2	3/2	3/2			.099245				
1/2	1/2			5/2	9/2	-.713728	1/2	1/2	3/2	5/2			.242826				
1/2	1/2			9/2	9/2	.000000	1/2	1/2	3/2	9/2			-.516504				
1/2	1/2			9/2	11/2	-.047416	1/2	1/2	5/2	5/2			-.089647				
1/2	1/2			11/2	11/2	.000000	1/2	1/2	5/2	9/2			.218209				
1/2	1/2			11/2	15/2	.286912	1/2	1/2	5/2	11/2			.395453				
1/2	1/2	15/2	15/2	.000000	1/2	1/2	9/2	9/2	-.126604								
2	2	0	0	2	2	.000000	3	4	0	0	2	2	.000000				
		0	0	2	4	.944552			0	0	2	4	.427036				
		0	0	4	4	.000000			0	0	2	5	.086528				
		0	0	4	5	-.328362			0	0	4	4	.095494				
		0	0	5	5	.000000			0	0	4	5	.311270				
		0	0	8	8	.000000			0	0	5	5	.247439				
		1/2	1/2	3/2	3/2	.000000			0	0	5	8	-.225748				
		1/2	1/2	3/2	5/2	.538891			0	0	8	8	-.214287				
		1/2	1/2	5/2	5/2	.000000			1/2	1/2	3/2	3/2	.114421				
		1/2	1/2	5/2	9/2	.317776			1/2	1/2	3/2	5/2	-.496510				
		1/2	1/2	9/2	9/2	.000000			1/2	1/2	3/2	9/2	.459286				
		1/2	1/2	9/2	11/2	.725671			1/2	1/2	5/2	5/2	.099947				
		1/2	1/2	11/2	11/2	.000000			1/2	1/2	5/2	9/2	-.152623				
		1/2	1/2	11/2	15/2	-.286386			1/2	1/2	5/2	11/2	.062360				
1/2	1/2	15/2	15/2	.000000	1/2	1/2	9/2	9/2	.600105								
3	1	0	0	2	2	-.303968	3	5	0	0	2	2	-.086969				
		0	0	2	4	.066541			0	0	2	4	.331439				
		0	0	2	5	-.008522			0	0	2	5	.430783				
		0	0	4	4	.080544			0	0	4	4	.820400				
		0	0	4	5	.499195			0	0	4	5	-.052728				
		0	0	5	5	-.134033			0	0	5	5	-.074527				
		0	0	5	8	.522872			0	0	5	8	-.082847				
		0	0	8	8	-.724713			0	0	8	8	.093576				
		1/2	1/2	3/2	3/2	-.121761			1/2	1/2	3/2	3/2	.368181				
		1/2	1/2	3/2	5/2	-.275019			1/2	1/2	3/2	5/2	-.000249				
		1/2	1/2	3/2	9/2	-.209523			1/2	1/2	3/2	9/2	-.000260				
		1/2	1/2	5/2	5/2	.085603			1/2	1/2	5/2	5/2	-.717767				
		1/2	1/2	5/2	9/2	-.245895											
		1/2	1/2	5/2	11/2	.187812											
1/2	1/2	9/2	9/2	-.032333													
1/2	1/2	9/2	11/2	.022521													
1/2	1/2	9/2	15/2	-.301359													
1/2	1/2	11/2	11/2	-.606714													
1/2	1/2	11/2	15/2	-.336126													
1/2	1/2	15/2	15/2	-.434879													
3	2	0	0	2	2	.042936											
		0	0	2	4	.064082											
		0	0	2	5	-.237757											
		0	0	4	4	.042465											
		0	0	4	5	-.517360											

See page 321 for Explanation of Tables

TABLE II. The Transformation Coefficients $D_{(v) \alpha; J N}^{T_\lambda T_\mu J}$

J	α	T_λ	T_μ	J_λ	J_μ	D	J	α	T_λ	T_μ	J_λ	J_μ	D		
$v = 6 \quad \zeta = 0$															
3	5	1/2	1/2	5/2	9/2	-.064150	4	1	1/2	1/2	11/2	15/2	-.674473		
		1/2	1/2	5/2	11/2	.380894			1/2	1/2	15/2	15/2	.000000		
		1/2	1/2	9/2	9/2	-.162370			4	2	0	0	2	2	.000000
		1/2	1/2	9/2	11/2	.270581					0	0	2	4	.420728
		1/2	1/2	9/2	15/2	-.060916					0	0	2	5	-.666617
		1/2	1/2	11/2	11/2	.032506					0	0	4	4	.000000
		1/2	1/2	11/2	15/2	-.254319					0	0	4	5	-.322692
		1/2	1/2	15/2	15/2	.176165					0	0	4	8	-.476928
3	6	0	0	2	2	-.466654	0	0			5	5	.000000		
		0	0	2	4	.430524	0	0			5	8	.216838		
		0	0	2	5	.431581	0	0	8	8	.000000				
		0	0	4	4	-.435219	1/2	1/2	3/2	5/2	.159331				
		0	0	4	5	-.222166	1/2	1/2	3/2	9/2	.719038				
		0	0	5	5	.363222	1/2	1/2	3/2	11/2	-.088916				
		0	0	5	8	-.165396	1/2	1/2	5/2	5/2	.000000				
		0	0	8	8	-.112080	1/2	1/2	5/2	9/2	.028210				
		1/2	1/2	3/2	3/2	.630903	1/2	1/2	5/2	11/2	.131757				
		1/2	1/2	3/2	5/2	-.171002	1/2	1/2	9/2	9/2	.000000				
		1/2	1/2	3/2	9/2	-.558535	1/2	1/2	9/2	11/2	.503278				
		1/2	1/2	5/2	5/2	.113362	1/2	1/2	9/2	15/2	.183249				
		1/2	1/2	5/2	9/2	-.146351	1/2	1/2	11/2	11/2	.000000				
		1/2	1/2	5/2	11/2	-.383021	1/2	1/2	11/2	15/2	-.380352				
		1/2	1/2	9/2	9/2	-.155385	1/2	1/2	15/2	15/2	.000000				
		3	7	1/2	1/2	9/2	11/2	-.083197	4	3	0	0	2	2	.000000
1/2	1/2			9/2	15/2	-.005022	0	0			2	4	.550850		
1/2	1/2			11/2	11/2	.186274	0	0			2	5	-.040074		
1/2	1/2			11/2	15/2	.011436	0	0			4	4	.000000		
1/2	1/2			15/2	15/2	-.117745	0	0			4	5	.684987		
0	0			2	2	-.056980	0	0			4	8	-.129373		
0	0			2	4	.177385	0	0			5	5	.000000		
0	0			2	5	-.564258	0	0			5	8	-.457180		
0	0			4	4	.296737	0	0			8	8	.000000		
0	0			4	5	-.283468	1/2	1/2			3/2	5/2	.598090		
0	0			5	5	.637341	1/2	1/2			3/2	9/2	-.061013		
0	0			5	8	.236452	1/2	1/2			3/2	11/2	-.410897		
0	0			8	8	-.127987	1/2	1/2			5/2	5/2	.000000		
1/2	1/2			3/2	3/2	-.280578	1/2	1/2			5/2	9/2	.188973		
1/2	1/2			3/2	5/2	-.571076	1/2	1/2			5/2	11/2	.345073		
1/2	1/2			3/2	9/2	-.188296	1/2	1/2			9/2	9/2	.000000		
1/2	1/2	5/2	5/2	-.324864	1/2	1/2	9/2	11/2	-.148705						
1/2	1/2	5/2	9/2	.578149	1/2	1/2	9/2	15/2	.402332						
1/2	1/2	5/2	11/2	-.166149	1/2	1/2	11/2	11/2	.000000						
1/2	1/2	9/2	9/2	.042464	1/2	1/2	11/2	15/2	.361882						
1/2	1/2	9/2	11/2	-.230672	1/2	1/2	15/2	15/2	.000000						
1/2	1/2	9/2	15/2	.034579	4	4	0	0	2	2	.000000				
1/2	1/2	11/2	11/2	.110598			0	0	2	4	.153834				
1/2	1/2	11/2	15/2	-.154318			0	0	2	5	.412956				
1/2	1/2	15/2	15/2	-.006265			0	0	4	4	.000000				
4	1	0	0	2			2	.000000	0	0	4	5	-.568992		
		0	0	2			4	.257305	0	0	4	8	-.333402		
		0	0	2			5	.606163	0	0	5	5	.000000		
		0	0	4			4	.000000	0	0	5	8	-.609011		
		0	0	4			5	.138517	0	0	8	8	.000000		
		0	0	4			8	-.445514	1/2	1/2	3/2	5/2	-.513192		
		0	0	5			5	.000000	1/2	1/2	3/2	9/2	-.318786		
		0	0	5			8	.590500	1/2	1/2	3/2	11/2	-.654587		
		0	0	8			8	.000000	1/2	1/2	5/2	5/2	.000000		
		1/2	1/2	3/2			5/2	-.100062	1/2	1/2	5/2	9/2	-.143345		
		1/2	1/2	3/2			9/2	-.024050	1/2	1/2	5/2	11/2	.173721		
		1/2	1/2	3/2			11/2	-.130967	1/2	1/2	9/2	9/2	.000000		
		1/2	1/2	5/2	5/2	.000000	1/2	1/2	9/2	11/2	.355139				
		1/2	1/2	5/2	9/2	.312459	1/2	1/2	9/2	15/2	.157789				
		1/2	1/2	5/2	11/2	.318694	1/2	1/2	11/2	11/2	.000000				
		1/2	1/2	9/2	9/2	.000000	1/2	1/2	11/2	15/2	-.069121				
1/2	1/2	9/2	11/2	-.563946	1/2	1/2	15/2	15/2	.000000						
1/2	1/2	9/2	15/2	-.010529	4	5	0	0	2	2	.000000				
1/2	1/2	11/2	11/2	.000000			0	0	2	4	-.655501				

See page 321 for Explanation of Tables

TABLE II. The Transformation Coefficients $D_{(v)\alpha; J_\lambda J_\mu}^{T_\lambda T_\mu J}$

J	α	T_λ	T_μ	J_λ	J_μ	D	J	α	T_λ	T_μ	J_λ	J_μ	D
$v = 6 \quad t = 0$													
4	5	0	0	2	5	-.126687	5	3	1/2	1/2	3/2	9/2	-.158766
		0	0	4	4	.000000			1/2	1/2	3/2	11/2	.344981
		0	0	4	5	.289352			1/2	1/2	5/2	5/2	.561860
		0	0	4	8	-.667954			1/2	1/2	5/2	9/2	.138460
		0	0	5	5	.000000			1/2	1/2	5/2	11/2	.269863
		0	0	5	8	-.156149			1/2	1/2	5/2	15/2	.588253
	0	0	8	8	.000000	1/2		1/2	9/2	9/2	-.004744		
	1/2	1/2	3/2	5/2	.093288	1/2		1/2	9/2	11/2	-.211159		
	1/2	1/2	3/2	9/2	-.067238	1/2		1/2	9/2	15/2	-.089952		
	1/2	1/2	3/2	11/2	.256775	1/2		1/2	11/2	11/2	-.180369		
	1/2	1/2	5/2	5/2	.000000	1/2		1/2	11/2	15/2	.128094		
	1/2	1/2	5/2	9/2	-.740636	1/2		1/2	15/2	15/2	-.020311		
	1/2	1/2	5/2	11/2	.603153	5		4	0	0	2	4	-.333713
	1/2	1/2	9/2	9/2	.000000				0	0	2	5	.233627
	1/2	1/2	9/2	11/2	-.055506				0	0	4	4	.350773
	1/2	1/2	9/2	15/2	-.011077				0	0	4	5	.575747
	1/2	1/2	11/2	11/2	.000000				0	0	4	8	-.292795
	1/2	1/2	11/2	15/2	-.072834				0	0	5	5	.540031
1/2	1/2	15/2	15/2	.000000	0	0	5	8	-.045282				
0	0	8	8	-.010721	1/2	1/2	3/2	9/2	-.101084				
5	1	0	0	2	4	-.369347	1/2	1/2	3/2	11/2	.135145		
		0	0	2	5	-.119851	1/2	1/2	5/2	5/2	-.161839		
		0	0	4	4	.234561	1/2	1/2	5/2	9/2	.394647		
		0	0	4	5	.395986	1/2	1/2	5/2	11/2	.362882		
		0	0	4	8	.041137	1/2	1/2	5/2	15/2	-.279198		
		0	0	5	5	-.751556	1/2	1/2	9/2	9/2	-.445367		
	0	0	5	8	-.259395	1/2	1/2	9/2	11/2	.306748			
	0	0	8	8	-.059844	1/2	1/2	9/2	15/2	-.257593			
	1/2	1/2	3/2	9/2	.408493	1/2	1/2	11/2	11/2	-.420293			
	1/2	1/2	3/2	11/2	-.555815	1/2	1/2	11/2	15/2	.060225			
	1/2	1/2	5/2	5/2	.099808	1/2	1/2	15/2	15/2	.202167			
	1/2	1/2	5/2	9/2	.242606	5	5	0	0	2	4	.421231	
	1/2	1/2	5/2	11/2	.449468			0	0	2	5	-.679820	
	1/2	1/2	5/2	15/2	.231317			0	0	4	4	.215733	
	1/2	1/2	9/2	9/2	.183658			0	0	4	5	.239769	
	1/2	1/2	9/2	11/2	.153043			0	0	4	8	-.308212	
	1/2	1/2	9/2	15/2	.064334			0	0	5	5	.008635	
	1/2	1/2	11/2	11/2	.154552	0	0	5	8	.112586			
1/2	1/2	11/2	15/2	-.134877	0	0	8	8	.385531				
1/2	1/2	15/2	15/2	.310622	1/2	1/2	3/2	9/2	-.521995				
5	2	0	0	2	4	.249021	1/2	1/2	3/2	11/2	.062396		
		0	0	2	5	-.323692	1/2	1/2	5/2	5/2	-.092880		
		0	0	4	4	-.022283	1/2	1/2	5/2	9/2	-.110197		
		0	0	4	5	.079456	1/2	1/2	5/2	11/2	.508290		
		0	0	4	8	-.053177	1/2	1/2	5/2	15/2	-.236164		
		0	0	5	5	.148852	1/2	1/2	9/2	9/2	.573748		
	0	0	5	8	-.353870	1/2	1/2	9/2	11/2	.126350			
	0	0	8	8	-.822310	1/2	1/2	9/2	15/2	.089472			
	1/2	1/2	3/2	9/2	-.460027	1/2	1/2	11/2	11/2	.100706			
	1/2	1/2	3/2	11/2	-.127463	1/2	1/2	11/2	15/2	.151428			
	1/2	1/2	5/2	5/2	-.150932	1/2	1/2	15/2	15/2	-.049968			
	1/2	1/2	5/2	9/2	-.126460	5	6	0	0	2	4	.631675	
	1/2	1/2	5/2	11/2	.006877			0	0	2	5	.514710	
	1/2	1/2	5/2	15/2	.149168			0	0	4	4	-.074004	
	1/2	1/2	9/2	9/2	-.168713			0	0	4	5	.274908	
	1/2	1/2	9/2	11/2	-.280776			0	0	4	8	-.041624	
	1/2	1/2	9/2	15/2	-.418347			0	0	5	5	-.133679	
	1/2	1/2	11/2	11/2	.275691	0	0	5	8	-.447203			
1/2	1/2	11/2	15/2	-.438928	0	0	8	8	.188192				
1/2	1/2	15/2	15/2	.400102	1/2	1/2	3/2	9/2	.139896				
5	3	0	0	2	4	.208662	1/2	1/2	3/2	11/2	.270920		
		0	0	2	5	.030174	1/2	1/2	5/2	5/2	-.206654		
	0	0	4	4	.717418	1/2	1/2	5/2	9/2	-.472860			
	0	0	4	5	-.079171	1/2	1/2	5/2	11/2	.323804			
	0	0	4	8	.649305	1/2	1/2	5/2	15/2	.182343			
	0	0	5	5	.091031	1/2	1/2	9/2	9/2	-.422544			
	0	0	5	8	.062558								
	0	0	8	8	-.028210								

See page 321 for Explanation of Tables

TABLE II. The Transformation Coefficients $D_{(v) \alpha; J_N J}^{T_\lambda T_\mu J}$

J	α	T_λ	T_μ	J_λ	J_μ	D	J	α	T_λ	T_μ	J_λ	J_μ	D
$v = 6 \quad \dagger = 0$													
5	6	1/2	1/2	9/2	11/2	.128284	6	3	0	0	2	4	.112511
		1/2	1/2	9/2	15/2	.284457			0	0	2	5	-.599362
		1/2	1/2	11/2	11/2	.347241			0	0	2	8	-.766696
		1/2	1/2	11/2	15/2	.257872			0	0	4	4	.000000
		1/2	1/2	15/2	15/2	.199102			0	0	4	5	.068728
5	7	0	0	2	4	-.201329	0	0	4	8	.009062		
		0	0	2	5	-.085888	0	0	5	5	.000000		
		0	0	4	4	.281773	0	0	5	8	.188356		
		0	0	4	5	-.537720	0	0	8	8	.000000		
		0	0	4	8	-.249434	1/2	1/2	3/2	9/2	.028428		
		0	0	5	5	.116231	1/2	1/2	3/2	11/2	.561528		
		0	0	5	8	-.671245	1/2	1/2	3/2	15/2	.586935		
		0	0	8	8	.239279	1/2	1/2	5/2	9/2	-.086659		
		1/2	1/2	3/2	9/2	-.131068	1/2	1/2	5/2	11/2	-.021265		
		1/2	1/2	3/2	11/2	-.316017	1/2	1/2	5/2	15/2	-.166730		
		1/2	1/2	5/2	5/2	.541607	1/2	1/2	9/2	9/2	.000000		
		1/2	1/2	5/2	9/2	-.498526	1/2	1/2	9/2	11/2	-.163472		
		1/2	1/2	5/2	11/2	-.109734	1/2	1/2	9/2	15/2	-.526205		
		1/2	1/2	5/2	15/2	-.122718	1/2	1/2	11/2	11/2	.000000		
		1/2	1/2	9/2	9/2	-.113517	1/2	1/2	11/2	15/2	.003190		
1/2	1/2	9/2	11/2	.467524	1/2	1/2	15/2	15/2	.000000				
6	1	1/2	1/2	9/2	15/2	-.239791	6	4	0	0	2	4	.378397
		1/2	1/2	11/2	11/2	-.110260			0	0	2	5	-.354237
		1/2	1/2	11/2	15/2	.098397			0	0	2	8	.308948
		1/2	1/2	15/2	15/2	.056424			0	0	4	4	.000000
		0	0	2	4	-.467584			0	0	4	5	.402651
		0	0	2	5	-.001002			0	0	4	8	-.655135
		0	0	2	8	.135236			0	0	5	5	.000000
		0	0	4	4	.000000			0	0	5	8	-.211075
		0	0	4	5	-.171603			0	0	8	8	.000000
		0	0	4	8	-.351881			1/2	1/2	3/2	9/2	.536427
		0	0	5	5	.000000			1/2	1/2	3/2	11/2	.006204
		0	0	5	8	.780901			1/2	1/2	3/2	15/2	-.031131
		0	0	8	8	.000000			1/2	1/2	5/2	9/2	-.559415
		1/2	1/2	3/2	9/2	.267335			1/2	1/2	5/2	11/2	-.389041
		1/2	1/2	3/2	11/2	.466044			1/2	1/2	5/2	15/2	.137294
1/2	1/2	3/2	15/2	-.019873	1/2	1/2	9/2	9/2	.000000				
1/2	1/2	5/2	9/2	.246478	1/2	1/2	9/2	11/2	.040163				
1/2	1/2	5/2	11/2	.293488	1/2	1/2	9/2	15/2	.049877				
1/2	1/2	5/2	15/2	-.431810	1/2	1/2	11/2	11/2	.000000				
1/2	1/2	9/2	9/2	.000000	1/2	1/2	11/2	15/2	-.473276				
1/2	1/2	9/2	11/2	.211443	1/2	1/2	15/2	15/2	.000000				
1/2	1/2	9/2	15/2	.506612	6	5	0	0	2	4	-.151861		
1/2	1/2	11/2	11/2	.000000			0	0	2	5	-.487376		
1/2	1/2	11/2	15/2	-.276098			0	0	2	8	.275303		
1/2	1/2	15/2	15/2	.000000			0	0	4	4	.000000		
0	0	2	4	.739443			0	0	4	5	-.795604		
0	0	2	5	.308177			0	0	4	8	-.170114		
0	0	2	8	-.049148			0	0	5	5	.000000		
0	0	4	4	.000000			0	0	5	8	-.041054		
0	0	4	5	-.344288			0	0	8	8	.000000		
0	0	4	8	-.125934			1/2	1/2	3/2	9/2	.275945		
0	0	5	5	.000000			1/2	1/2	3/2	11/2	-.345532		
0	0	5	8	.470577			1/2	1/2	3/2	15/2	-.005671		
0	0	8	8	.000000			1/2	1/2	5/2	9/2	-.406472		
1/2	1/2	3/2	9/2	-.335532			1/2	1/2	5/2	11/2	.659832		
1/2	1/2	3/2	11/2	-.170385			1/2	1/2	5/2	15/2	-.314955		
1/2	1/2	3/2	15/2	.227652	1/2	1/2	9/2	9/2	.000000				
1/2	1/2	5/2	9/2	-.340830	1/2	1/2	9/2	11/2	.132326				
1/2	1/2	5/2	11/2	-.028314	1/2	1/2	9/2	15/2	-.260340				
1/2	1/2	5/2	15/2	-.369648	1/2	1/2	11/2	11/2	.000000				
1/2	1/2	9/2	9/2	.000000	1/2	1/2	11/2	15/2	.139095				
1/2	1/2	9/2	11/2	-.609467	1/2	1/2	15/2	15/2	.000000				
1/2	1/2	9/2	15/2	.417189	6	6	0	0	2	4	.235976		
1/2	1/2	11/2	11/2	.000000			0	0	2	5	-.427518		
1/2	1/2	11/2	15/2	-.086360			0	0	2	8	.469288		
1/2	1/2	15/2	15/2	.000000			0	0	4	4	.000000		

See page 321 for Explanation of Tables

TABLE II. The Transformation Coefficients $D_{(v) \alpha J \mu}^{T_\lambda T_\mu J}$

J	α	T_λ	T_μ	J_λ	J_μ	D	J	α	T_λ	T_μ	J_λ	J_μ	D
$v = 6 \quad t = 0$													
6	6	0	0	4	5	.228431	7	3	1/2	1/2	5/2	15/2	-.396359
		0	0	4	8	.634112			1/2	1/2	9/2	9/2	.151729
		0	0	5	5	.000000			1/2	1/2	9/2	11/2	-.326005
		0	0	5	8	.295016			1/2	1/2	9/2	15/2	.227342
		0	0	8	8	.000000			1/2	1/2	11/2	11/2	.148480
	1/2	1/2	3/2	9/2	.561608	1/2		1/2	11/2	15/2	-.476588		
	1/2	1/2	3/2	11/2	-.132448	1/2		1/2	15/2	15/2	.230425		
	1/2	1/2	3/2	15/2	.429246	7		4	0	0	2	5	-.391780
	1/2	1/2	5/2	9/2	.186214				0	0	2	8	-.114507
	1/2	1/2	5/2	11/2	.021600				0	0	4	4	.024886
	1/2	1/2	5/2	15/2	.276130				0	0	4	5	.149310
	1/2	1/2	9/2	9/2	.000000				0	0	4	8	.196626
	1/2	1/2	9/2	11/2	-.229165	0		0	5	5	.753480		
	1/2	1/2	9/2	15/2	.322757	0		0	5	8	.393885		
	1/2	1/2	11/2	11/2	.000000	0		0	8	8	-.221235		
1/2	1/2	11/2	15/2	.463382	1/2	1/2	3/2	11/2	.331731				
1/2	1/2	15/2	15/2	.000000	1/2	1/2	3/2	15/2	.201115				
7	7	0	0	2	5	-.408057	1/2	1/2	5/2	9/2	-.418468		
		0	0	2	8	.269640	1/2	1/2	5/2	11/2	.085042		
		0	0	4	4	-.610789	1/2	1/2	5/2	15/2	-.389554		
		0	0	4	5	-.389347	1/2	1/2	9/2	9/2	.193706		
		0	0	4	8	.274615	1/2	1/2	9/2	11/2	-.335584		
	0	0	5	5	-.081541	1/2	1/2	9/2	15/2	-.496601			
	0	0	5	8	-.278052	1/2	1/2	11/2	11/2	.191460			
	0	0	8	8	-.277065	1/2	1/2	11/2	15/2	.031633			
	1/2	1/2	3/2	11/2	.424805	1/2	1/2	15/2	15/2	-.284603			
	1/2	1/2	3/2	15/2	-.052704	7	5	0	0	2	5	.169198	
	1/2	1/2	5/2	9/2	.147911			0	0	2	8	-.392946	
	1/2	1/2	5/2	11/2	.614533			0	0	4	4	-.234104	
	1/2	1/2	5/2	15/2	.001959			0	0	4	5	.420364	
	1/2	1/2	9/2	9/2	-.553079			0	0	4	8	.731968	
	1/2	1/2	9/2	11/2	-.038671	0	0	5	5	-.199413			
1/2	1/2	9/2	15/2	-.035677	0	0	5	8	-.019602				
1/2	1/2	11/2	11/2	.150898	0	0	8	8	.097608				
1/2	1/2	11/2	15/2	.119220	1/2	1/2	3/2	11/2	-.637443				
1/2	1/2	15/2	15/2	.267549	1/2	1/2	3/2	15/2	-.052886				
7	7	0	0	2	5	.312878	1/2	1/2	5/2	9/2	.146049		
		0	0	2	8	.682574	1/2	1/2	5/2	11/2	.453345		
		0	0	4	4	-.066337	1/2	1/2	5/2	15/2	.028773		
		0	0	4	5	.530588	1/2	1/2	9/2	9/2	.208782		
		0	0	4	8	.047557	1/2	1/2	9/2	11/2	-.092770		
	0	0	5	5	.237353	1/2	1/2	9/2	15/2	-.124781			
	0	0	5	8	-.255946	1/2	1/2	11/2	11/2	.436227			
	0	0	8	8	-.161769	1/2	1/2	11/2	15/2	.307724			
	1/2	1/2	3/2	11/2	-.027024	1/2	1/2	15/2	15/2	-.102153			
	1/2	1/2	3/2	15/2	.558533	7	6	0	0	2	5	.630401	
	1/2	1/2	5/2	9/2	-.471140			0	0	2	8	-.352625	
	1/2	1/2	5/2	11/2	-.002105			0	0	4	4	-.395292	
	1/2	1/2	5/2	15/2	.183205			0	0	4	5	-.201726	
	1/2	1/2	9/2	9/2	.023070			0	0	4	8	-.217720	
	1/2	1/2	9/2	11/2	.356274	0	0	5	5	.277562			
1/2	1/2	9/2	15/2	.189319	0	0	5	8	-.018522				
1/2	1/2	11/2	11/2	.395976	0	0	8	8	-.395620				
1/2	1/2	11/2	15/2	-.032823	1/2	1/2	3/2	11/2	.122701				
1/2	1/2	15/2	15/2	.332604	1/2	1/2	3/2	15/2	-.079923				
7	7	0	0	2	5	.155714	1/2	1/2	5/2	9/2	.045166		
		0	0	2	8	.207282	1/2	1/2	5/2	11/2	.408613		
		0	0	4	4	.351633	1/2	1/2	5/2	15/2	.221441		
		0	0	4	5	-.164129	1/2	1/2	9/2	9/2	.544597		
		0	0	4	8	.281498	1/2	1/2	9/2	11/2	.281818		
	0	0	5	5	-.350758	1/2	1/2	9/2	15/2	-.349512			
	0	0	5	8	.434205	1/2	1/2	11/2	11/2	-.287148			
	0	0	8	8	-.625617	1/2	1/2	11/2	15/2	-.337682			
	1/2	1/2	3/2	11/2	-.033935	1/2	1/2	15/2	15/2	.256646			
	1/2	1/2	3/2	15/2	.375300	7	7	0	0	2	5	.181319	
	1/2	1/2	5/2	9/2	.465562			0	0	2	8	-.019962	
	1/2	1/2	5/2	11/2	.029773			0	0	4	4	.483935	

See page 321 for Explanation of Tables

TABLE II. The Transformation Coefficients $D_{(v)\alpha_i J_i J_\mu}^{T_\lambda T_\mu J}$

J	α	T_λ	T_μ	J_λ	J_μ	D	J	α	T_λ	T_μ	J_λ	J_μ	D
$v = 6 \quad \xi = 0$													
7	7	0	0	4	5	-.430073	8	4	0	0	4	8	.729328
		0	0	4	8	.417656			0	0	5	5	.000000
		0	0	5	5	.336534			0	0	5	8	.062658
		0	0	5	8	-.504620			0	0	8	8	.000000
		0	0	8	8	.072361			1/2	1/2	3/2	15/2	-.149981
		1/2	1/2	3/2	11/2	.141058			1/2	1/2	5/2	11/2	-.015557
		1/2	1/2	3/2	15/2	-.223155			1/2	1/2	5/2	15/2	-.777822
		1/2	1/2	5/2	9/2	.285411			1/2	1/2	9/2	9/2	.000000
		1/2	1/2	5/2	11/2	-.236288			1/2	1/2	9/2	11/2	-.382898
		1/2	1/2	5/2	15/2	-.447058			1/2	1/2	9/2	15/2	.085596
		1/2	1/2	9/2	9/2	.038720			1/2	1/2	11/2	11/2	.000000
		1/2	1/2	9/2	11/2	.634201			1/2	1/2	11/2	15/2	.467246
		1/2	1/2	9/2	15/2	-.203456			1/2	1/2	15/2	15/2	.000000
		1/2	1/2	11/2	11/2	.379135			9	1	0	0	2
1/2	1/2	11/2	15/2	.061152	0	0	4	5			.298439		
1/2	1/2	15/2	15/2	.023787	0	0	4	8			.245633		
8	1	0	0	2	8	.183058	0	0			5	5	-.258903
		0	0	4	4	.000000	0	0			5	8	.337702
		0	0	4	5	-.092843	0	0			8	8	.818131
		0	0	4	8	-.212537	1/2	1/2			3/2	15/2	.015864
		0	0	5	5	.000000	1/2	1/2			5/2	15/2	-.049662
		0	0	5	8	.955352	1/2	1/2			9/2	9/2	.235853
		0	0	8	8	.000000	1/2	1/2			9/2	11/2	.545581
		1/2	1/2	3/2	15/2	.498585	1/2	1/2			9/2	15/2	.335980
		1/2	1/2	5/2	11/2	.004899	1/2	1/2			11/2	11/2	-.438505
		1/2	1/2	5/2	15/2	.086332	1/2	1/2			11/2	15/2	.129221
		1/2	1/2	9/2	9/2	.000000	1/2	1/2			15/2	15/2	-.567564
		1/2	1/2	9/2	11/2	.493047	9	2	0	0	2	8	-.377790
		1/2	1/2	9/2	15/2	.249532			0	0	4	5	-.237700
		1/2	1/2	11/2	11/2	.000000			0	0	4	8	.435058
1/2	1/2	11/2	15/2	.662249	0	0			5	5	.333175		
1/2	1/2	15/2	15/2	.000000	0	0			5	8	-.627438		
8	2	0	0	2	8	.486657			0	0	8	8	.326824
		0	0	4	4	.000000			1/2	1/2	3/2	15/2	-.377176
		0	0	4	5	.708482			1/2	1/2	5/2	15/2	-.277151
		0	0	4	8	.503529			1/2	1/2	9/2	9/2	-.006434
		0	0	5	5	.000000			1/2	1/2	9/2	11/2	-.218937
		0	0	5	8	.087622			1/2	1/2	9/2	15/2	.707952
		0	0	8	8	.000000			1/2	1/2	11/2	11/2	.233367
		1/2	1/2	3/2	15/2	-.279584			1/2	1/2	11/2	15/2	-.417368
		1/2	1/2	5/2	11/2	.702116			1/2	1/2	15/2	15/2	-.055664
		1/2	1/2	5/2	15/2	-.194387	9	3	0	0	2	8	.007929
		1/2	1/2	9/2	9/2	.000000			0	0	4	5	.259277
		1/2	1/2	9/2	11/2	.336608			0	0	4	8	-.464573
		1/2	1/2	9/2	15/2	.486295			0	0	5	5	-.538138
		1/2	1/2	11/2	11/2	.000000			0	0	5	8	-.638901
1/2	1/2	11/2	15/2	-.203204	0	0			8	8	.138193		
1/2	1/2	15/2	15/2	.000000	1/2	1/2			3/2	15/2	-.435403		
8	3	0	0	2	8	.833345			1/2	1/2	5/2	15/2	-.140176
		0	0	4	4	.000000			1/2	1/2	9/2	9/2	-.101974
		0	0	4	5	-.245908			1/2	1/2	9/2	11/2	.152011
		0	0	4	8	-.411543			1/2	1/2	9/2	15/2	.161401
		0	0	5	5	.000000			1/2	1/2	11/2	11/2	-.462923
		0	0	5	8	-.275133			1/2	1/2	11/2	15/2	.338746
		0	0	8	8	.000000			1/2	1/2	15/2	15/2	.634171
		1/2	1/2	3/2	15/2	-.696189	9	4	0	0	2	8	-.721909
		1/2	1/2	5/2	11/2	-.539689			0	0	4	5	.631094
		1/2	1/2	5/2	15/2	.125798			0	0	4	8	-.048870
		1/2	1/2	9/2	9/2	.000000			0	0	5	5	.135028
		1/2	1/2	9/2	11/2	.312421			0	0	5	8	.123185
		1/2	1/2	9/2	15/2	.284779			0	0	8	8	-.211597
		1/2	1/2	11/2	11/2	.000000			1/2	1/2	3/2	15/2	.091549
1/2	1/2	11/2	15/2	.171829	1/2	1/2			5/2	15/2	-.493347		
1/2	1/2	15/2	15/2	.000000	1/2	1/2			9/2	9/2	.462576		
8	4	0	0	2	8	.187594			1/2	1/2	9/2	11/2	-.277456
		0	0	4	4	.000000			1/2	1/2	9/2	15/2	-.304848
		0	0	4	5	-.654952			1/2	1/2	11/2	11/2	-.453915

See page 321 for Explanation of Tables

TABLE II. The Transformation Coefficients $D_{(v) \alpha; J N \mu}^{T_\lambda T_\mu J}$

J	α	T_λ	T_μ	J_λ	J_μ	D	J	α	T_λ	T_μ	J_λ	J_μ	D
$v = 6 \quad k = 0$													
9	4	1/2	1/2	11/2	15/2	.394499	10	3	0	0	4	8	-.927518
		1/2	1/2	15/2	15/2	.051662			0	0	5	5	.000000
9	5	0	0	2	8	.579034			0	0	5	8	-.281108
		0	0	4	5	.622627			0	0	8	8	.000000
		0	0	4	8	.252260			1/2	1/2	5/2	15/2	-.904543
		0	0	5	5	.373477			1/2	1/2	9/2	11/2	.226585
		0	0	5	8	-.257216			1/2	1/2	9/2	15/2	.281641
		0	0	8	8	-.088172			1/2	1/2	11/2	11/2	.000000
		1/2	1/2	3/2	15/2	.259849			1/2	1/2	11/2	15/2	.226138
		1/2	1/2	5/2	15/2	-.526307			1/2	1/2	15/2	15/2	.000000
		1/2	1/2	9/2	9/2	-.649870	11	1	0	0	4	8	-.733726
		1/2	1/2	9/2	11/2	.395875			0	0	5	8	.103669
		1/2	1/2	9/2	15/2	-.102649			0	0	8	8	-.671490
		1/2	1/2	11/2	11/2	.013798			1/2	1/2	9/2	15/2	-.258570
		1/2	1/2	11/2	15/2	-.253989			1/2	1/2	11/2	11/2	.688779
		1/2	1/2	15/2	15/2	.034549			1/2	1/2	11/2	15/2	.676109
9	6	0	0	2	8	-.024338			1/2	1/2	15/2	15/2	.040021
		0	0	4	5	.035555	11	2	0	0	4	8	-.056222
		0	0	4	8	.684498			0	0	5	8	-.994166
		0	0	5	5	-.612089			0	0	8	8	-.092053
		0	0	5	8	-.052432			1/2	1/2	9/2	15/2	.517874
		0	0	8	8	-.390132			1/2	1/2	11/2	11/2	-.481246
		1/2	1/2	3/2	15/2	-.545312			1/2	1/2	11/2	15/2	.695818
		1/2	1/2	5/2	15/2	.000551			1/2	1/2	15/2	15/2	-.126676
		1/2	1/2	9/2	9/2	.277186	11	3	0	0	4	8	.677115
		1/2	1/2	9/2	11/2	.525742			0	0	5	8	.029789
		1/2	1/2	9/2	15/2	-.393589			0	0	8	8	-.735273
		1/2	1/2	11/2	11/2	.349984			1/2	1/2	9/2	15/2	-.648223
		1/2	1/2	11/2	15/2	-.265091			1/2	1/2	11/2	11/2	-.332133
		1/2	1/2	15/2	15/2	.041525			1/2	1/2	11/2	15/2	.130272
10	1	0	0	2	8	.860432			1/2	1/2	15/2	15/2	-.672699
		0	0	4	8	-.342800	12	1	0	0	4	8	-.371040
		0	0	5	5	.000000			0	0	5	8	-.928617
		0	0	5	8	.377022			0	0	8	8	.000000
		0	0	8	8	.000000			1/2	1/2	9/2	15/2	-.999053
		1/2	1/2	5/2	15/2	-.149278			1/2	1/2	11/2	15/2	-.043505
		1/2	1/2	9/2	11/2	-.109207			1/2	1/2	15/2	15/2	.000000
		1/2	1/2	9/2	15/2	-.822918	12	2	0	0	4	8	-.928617
		1/2	1/2	11/2	11/2	.000000			0	0	5	8	.371040
		1/2	1/2	11/2	15/2	.537212			0	0	8	8	.000000
		1/2	1/2	15/2	15/2	.000000			1/2	1/2	9/2	15/2	.043505
10	2	0	0	2	8	.446058			1/2	1/2	11/2	15/2	-.999053
		0	0	4	8	.148994			1/2	1/2	15/2	15/2	.000000
		0	0	5	5	.000000	13	1	0	0	5	8	-.996803
		0	0	5	8	-.882515			0	0	8	8	-.079902
		0	0	8	8	.000000			1/2	1/2	11/2	15/2	-.575364
		1/2	1/2	5/2	15/2	-.311476			1/2	1/2	15/2	15/2	-.817897
		1/2	1/2	9/2	11/2	-.897143	13	2	0	0	5	8	-.079902
		1/2	1/2	9/2	15/2	-.028102			0	0	8	8	-.996803
		1/2	1/2	11/2	11/2	.000000			1/2	1/2	11/2	15/2	-.817897
		1/2	1/2	11/2	15/2	-.311975			1/2	1/2	15/2	15/2	-.575364
		1/2	1/2	15/2	15/2	.000000	15	1	0	0	8	8	-1.000000
10	3	0	0	2	8	-.246352			1/2	1/2	15/2	15/2	1.000000
$v = 6 \quad k = 1$													
0	1	1/2	1/2	3/2	3/2	-.635674	0	2	1/2	1/2	15/2	15/2	.373979
		1/2	1/2	5/2	5/2	.302765			1	0	2	2	.000000
		1/2	1/2	9/2	9/2	.593916			1	0	4	4	1.000000
		1/2	1/2	11/2	11/2	-.389249	1	1	1/2	1/2	3/2	3/2	.000000
		1/2	1/2	15/2	15/2	.000000			1/2	1/2	3/2	5/2	-.540575
		1	0	2	2	-1.000000			1/2	1/2	5/2	5/2	.000000
		1	0	4	4	.000000			1/2	1/2	9/2	9/2	.000000
0	2	1/2	1/2	3/2	3/2	.381993			1/2	1/2	9/2	11/2	-.841296
		1/2	1/2	5/2	5/2	.396958			1/2	1/2	11/2	11/2	.000000
		1/2	1/2	9/2	9/2	-.253420			1/2	1/2	15/2	15/2	.000000
		1/2	1/2	11/2	11/2	-.701730			1	0	2	2	-.718669

See page 321 for Explanation of Tables

TABLE II. The Transformation Coefficients $D_{(v) \alpha; J_\lambda J_\mu}^{T_\lambda T_\mu J}$

J	α	T_λ	T_μ	J_λ	J_μ	D	J	α	T_λ	T_μ	J_λ	J_μ	D
$v = 6 \quad \ell = 1$													
1	1	1	0	4	4	.040518	2	4	1/2	1/2	5/2	5/2	-.765015
		1	0	4	5	.601867			1/2	1/2	5/2	9/2	-.313008
		1	0	6	5	-.345876			1/2	1/2	9/2	9/2	-.066430
1	2	1/2	1/2	3/2	3/2	.000000	1/2	1/2	1/2	9/2	11/2	-.183326	
		1/2	1/2	3/2	5/2	.841296	1/2	1/2	11/2	11/2	-.429458		
		1/2	1/2	5/2	5/2	.000000	1/2	1/2	11/2	15/2	-.028608		
		1/2	1/2	9/2	9/2	.000000	1/2	1/2	15/2	15/2	.289113		
		1/2	1/2	9/2	11/2	-.540575	1	0	2	2	-.017338		
		1/2	1/2	11/2	11/2	.000000	1	0	2	4	-.822982		
		1/2	1/2	15/2	15/2	.000000	1	0	4	2	.061873		
		1	0	2	2	.332415	1	0	4	4	.441948		
		1	0	4	4	.653399	1	0	4	5	.036248		
		1	0	4	5	-.037323	1	0	6	4	.106773		
2	1	1	0	6	5	-.679101	1	0	6	5	.118201		
		1/2	1/2	3/2	3/2	.505908	1	0	6	8	.310754		
		1/2	1/2	3/2	5/2	.365288	1/2	1/2	3/2	3/2	.482656		
		1/2	1/2	5/2	5/2	.137580	1/2	1/2	3/2	5/2	.355913		
		1/2	1/2	5/2	9/2	.168072	1/2	1/2	5/2	5/2	.116359		
		1/2	1/2	9/2	9/2	.473377	1/2	1/2	5/2	9/2	.170485		
		1/2	1/2	9/2	11/2	.119645	1/2	1/2	9/2	9/2	.494198		
		1/2	1/2	11/2	11/2	-.487172	1/2	1/2	9/2	11/2	.112361		
		1/2	1/2	11/2	15/2	-.288463	1/2	1/2	11/2	11/2	-.498082		
		1/2	1/2	15/2	15/2	.067058	1/2	1/2	11/2	15/2	-.296904		
2	2	1	0	2	2	-.047641	1/2	1/2	15/2	15/2	.068332		
		1	0	2	4	.186002	1	0	2	2	-.113987		
		1	0	4	2	-.051147	1	0	2	4	.320273		
		1	0	4	4	.123056	1	0	4	2	-.033071		
		1	0	4	5	-.858891	1	0	4	4	.242090		
		1	0	6	4	.006467	1	0	4	5	-.268975		
		1	0	6	5	.352220	1	0	6	4	.015282		
		1	0	6	8	.289104	1	0	6	5	.655111		
		1/2	1/2	3/2	3/2	.488549	1	0	6	8	.568313		
		1/2	1/2	3/2	5/2	-.038140	1/2	1/2	3/2	3/2	.000000		
2	3	1/2	1/2	5/2	5/2	.150798	1/2	1/2	3/2	5/2	-.277786		
		1/2	1/2	5/2	9/2	.079903	1/2	1/2	3/2	9/2	-.062161		
		1/2	1/2	9/2	9/2	-.772623	1/2	1/2	5/2	5/2	.000000		
		1/2	1/2	9/2	11/2	.236875	1/2	1/2	5/2	9/2	-.030858		
		1/2	1/2	11/2	11/2	-.102122	1/2	1/2	5/2	11/2	.822523		
		1/2	1/2	11/2	15/2	-.009940	1/2	1/2	9/2	9/2	.000000		
		1/2	1/2	15/2	15/2	.259149	1/2	1/2	9/2	11/2	-.093685		
		1	0	2	2	-.062937	1/2	1/2	9/2	15/2	-.115077		
		1	0	2	4	-.063480	1/2	1/2	11/2	11/2	.000000		
		1	0	4	2	-.829017	1/2	1/2	11/2	15/2	-.468460		
2	4	1	0	4	4	-.123397	1/2	1/2	15/2	15/2	.000000		
		1	0	4	5	.210642	1	0	2	2	.067633		
		1	0	6	4	-.013380	1	0	2	4	.676834		
		1	0	6	5	.493422	1	0	2	5	.168158		
		1	0	6	8	-.038727	1	0	4	2	-.091766		
		1/2	1/2	3/2	3/2	.423382	1	0	4	4	.087874		
		1/2	1/2	3/2	5/2	.409048	1	0	4	5	.149151		
		1/2	1/2	5/2	5/2	.016480	1	0	6	4	.684743		
		1/2	1/2	5/2	9/2	-.583415	1	0	6	5	.032000		
		1/2	1/2	9/2	9/2	.038184	1	0	6	8	.027541		
3	2	1/2	1/2	9/2	11/2	-.194965	1/2	1/2	3/2	3/2	.000000		
		1/2	1/2	11/2	11/2	.268164	1/2	1/2	3/2	5/2	.603806		
		1/2	1/2	11/2	15/2	.421611	1/2	1/2	3/2	9/2	-.185017		
		1/2	1/2	15/2	15/2	-.153771	1/2	1/2	5/2	5/2	.000000		
		1	0	2	2	.715070	1/2	1/2	5/2	9/2	.272592		
		1	0	2	4	.046663	1/2	1/2	5/2	11/2	-.087737		
		1	0	4	2	-.361056	1/2	1/2	9/2	9/2	.000000		
		1	0	4	4	.401851	1/2	1/2	9/2	11/2	.111991		
		1	0	4	5	-.162706	1/2	1/2	9/2	15/2	.357237		
		1	0	6	4	.052540	1/2	1/2	11/2	11/2	.000000		
2	4	1	0	6	5	-.353780	1/2	1/2	11/2	15/2	-.615648		
		1	0	6	8	-.200646	1/2	1/2	15/2	15/2	.000000		
2	4	1/2	1/2	3/2	3/2	.019826	1	0	2	2	-.040946		
		1/2	1/2	3/2	5/2	-.097597	1	0	2	4	-.296745		

See page 321 for Explanation of Tables

TABLE II. The Transformation Coefficients $D_{(v) \alpha; J_N J_\mu}^{T_\lambda T_\mu J}$

J	α	T_λ	T_μ	J_N	J_μ	D	J	α	T_λ	T_μ	J_N	J_μ	D		
$v = 6 \quad t = 1$															
3	2	1	0	2	5	.581666	3	5	1	0	4	2	.420242		
		1	0	4	2	-.093420			1	0	4	4	-.465217		
		1	0	4	4	-.098281			1	0	4	5	.506114		
		1	0	4	5	.429611			1	0	6	4	.118679		
		1	0	6	4	.070344			1	0	6	5	.234138		
	1	0	6	5	-.495509	1		0	6	8	-.300162				
	1	0	6	8	.344239	4		1	1/2	1/2	3/2	5/2	-.359527		
	3	3	1/2	1/2	3/2				5/2	.000000	1/2	1/2	3/2	9/2	.043219
			1/2	1/2	3/2				5/2	.023395	1/2	1/2	3/2	11/2	-.457644
			1/2	1/2	3/2				9/2	.716358	1/2	1/2	5/2	5/2	.486388
1/2			1/2	5/2	5/2		.000000		1/2	1/2	5/2	9/2	.392231		
1/2			1/2	5/2	9/2		-.536182		1/2	1/2	5/2	11/2	-.088550		
1/2			1/2	5/2	11/2		-.001949		1/2	1/2	9/2	9/2	.007706		
1/2			1/2	9/2	9/2		.000000		1/2	1/2	9/2	11/2	.369039		
1/2			1/2	9/2	11/2		.242128		1/2	1/2	9/2	15/2	-.043691		
1/2			1/2	9/2	15/2		.314761		1/2	1/2	11/2	11/2	-.152372		
1/2			1/2	11/2	11/2	.000000	1/2	1/2	11/2	15/2	-.194427				
1/2	1/2	11/2	15/2	-.202772	1/2	1/2	15/2	15/2	-.248992						
1/2	1/2	15/2	15/2	.000000	1	0	2	2	.370018						
1	0	2	2	.707199	1	0	2	4	-.213437						
1	0	2	4	.012574	1	0	2	5	.614297						
1	0	2	5	-.009215	1	0	4	2	-.300935						
1	0	4	2	-.463043	1	0	4	4	-.092970						
1	0	4	4	-.317317	1	0	4	5	-.382603						
1	0	4	5	-.295680	1	0	4	8	-.081255						
1	0	6	4	-.050354	1	0	6	2	-.062038						
1	0	6	5	.022985	1	0	6	4	-.055259						
1	0	6	8	.306656	1	0	6	5	.271949						
3	4	1/2	1/2	3/2	3/2	.000000	4	2	1/2	1/2	3/2	5/2	-.327290		
		1/2	1/2	3/2	5/2	.284679			1/2	1/2	3/2	9/2	.109073		
		1/2	1/2	3/2	9/2	.486791			1/2	1/2	3/2	11/2	-.026070		
		1/2	1/2	5/2	5/2	.000000			1/2	1/2	5/2	5/2	-.003705		
		1/2	1/2	5/2	9/2	.599578			1/2	1/2	5/2	9/2	-.267192		
		1/2	1/2	5/2	11/2	.384329			1/2	1/2	5/2	11/2	-.052842		
		1/2	1/2	9/2	9/2	.000000			1/2	1/2	5/2	15/2	-.241702		
		1/2	1/2	9/2	11/2	.198327			1/2	1/2	9/2	9/2	-.118265		
		1/2	1/2	9/2	15/2	-.021124			1/2	1/2	9/2	11/2	.520436		
		1/2	1/2	11/2	11/2	.000000			1/2	1/2	9/2	15/2	-.426899		
1/2	1/2	11/2	15/2	.367437	1/2	1/2	11/2	11/2	.080626						
1/2	1/2	15/2	15/2	.000000	1/2	1/2	11/2	15/2	-.423371						
1	0	2	2	.357366	1/2	1/2	15/2	15/2	.449422						
1	0	2	4	-.235908	1	0	2	2	-.201441						
1	0	2	5	.470420	1	0	2	4	.359610						
1	0	4	2	-.122260	1	0	2	5	.153453						
1	0	4	4	.560842	1	0	4	2	-.273750						
1	0	4	5	-.054790	1	0	4	4	.136789						
1	0	6	4	.015325	1	0	4	5	.439704						
1	0	6	5	.203794	1	0	4	8	-.102094						
1	0	6	8	-.470193	1	0	6	2	-.486735						
3	5	1/2	1/2	3/2	3/2	.000000	4	3	1/2	1/2	3/2	5/2	.217274		
		1/2	1/2	3/2	5/2	.244943			1/2	1/2	3/2	9/2	-.652635		
		1/2	1/2	3/2	9/2	-.248594			1/2	1/2	3/2	11/2	-.110418		
		1/2	1/2	5/2	5/2	.000000			1/2	1/2	5/2	5/2	.122172		
		1/2	1/2	5/2	9/2	-.272856			1/2	1/2	5/2	9/2	-.025581		
		1/2	1/2	5/2	11/2	.099934			1/2	1/2	5/2	11/2	.159176		
		1/2	1/2	9/2	9/2	.000000			1/2	1/2	5/2	15/2	-.570065		
		1/2	1/2	9/2	11/2	.756079			1/2	1/2	9/2	9/2	-.104030		
		1/2	1/2	9/2	15/2	-.469113			1/2	1/2	9/2	11/2	-.352671		
		1/2	1/2	11/2	11/2	.000000			1/2	1/2	9/2	15/2	-.023473		
1/2	1/2	11/2	15/2	.045213	1/2	1/2	11/2	11/2	-.084764						
1/2	1/2	15/2	15/2	.000000	1/2	1/2	11/2	15/2							
1	0	2	2	.410646											
1	0	2	4	-.138258											
1	0	2	5	-.063802											

See page 321 for Explanation of Tables

TABLE II. The Transformation Coefficients $D_{(w)\alpha; J_N \mu}^{T, T, J}$

J	α	T_x	T_y	J_x	J_y	D	J	α	T_x	T_y	J_x	J_y	D				
$V = 6 \quad \xi = 1$																	
4	3	1/2	1/2	15/2	15/2	-.076423	4	6	1/2	1/2	11/2	11/2	.196540				
		1	0	2	2	.303336			1/2	1/2	11/2	15/2	-.176001				
		1	0	2	4	-.070141			1/2	1/2	15/2	15/2	-.170461				
		1	0	2	5	.203165			1	0	2	2	.213868				
		1	0	4	2	.686567			1	0	2	4	.324126				
		1	0	4	4	-.082605			1	0	2	5	-.405214				
		1	0	4	5	.197053			1	0	4	2	.145378				
		1	0	4	8	-.118557			1	0	4	4	-.392759				
		1	0	6	2	-.534779			1	0	4	5	-.177711				
		1	0	6	4	-.088617			1	0	4	8	.467697				
		1	0	6	5	-.178505			1	0	6	2	-.073649				
		1	0	6	8	-.070728			1	0	6	4	-.076113				
		4	4	1/2	1/2	3/2			5/2	.362704	1	0	6	5	.390102		
				1/2	1/2	3/2			9/2	.009109	1	0	6	8	-.309662		
				1/2	1/2	3/2			11/2	.395268	4	7	1/2	1/2	3/2	5/2	-.374787
				1/2	1/2	5/2			5/2	.635892			1/2	1/2	3/2	9/2	-.098610
1/2	1/2			5/2	9/2	-.020507	1/2	1/2	3/2	11/2			.169832				
1/2	1/2			5/2	11/2	.229942	1/2	1/2	5/2	5/2			.253672				
1/2	1/2			9/2	9/2	-.358593	1/2	1/2	5/2	9/2			.179616				
1/2	1/2			9/2	11/2	.131720	1/2	1/2	5/2	11/2			.152343				
1/2	1/2			9/2	15/2	-.252351	1/2	1/2	9/2	9/2			.002043				
1/2	1/2			11/2	11/2	-.136800	1/2	1/2	9/2	11/2			-.183607				
1/2	1/2			11/2	15/2	.138473	1/2	1/2	9/2	15/2			.014698				
1/2	1/2			15/2	15/2	.083452	1/2	1/2	11/2	11/2			.744284				
1	0			2	2	-.547757	1/2	1/2	11/2	15/2			-.132343				
1	0			2	4	-.646044	1/2	1/2	15/2	15/2			.309425				
1	0			2	5	-.192179	1	0	2	2			.108080				
1	0			4	2	-.124700	1	0	2	4			.222003				
1	0	4	4	-.337697	1	0	2	5	.048888								
1	0	4	5	.241682	1	0	4	2	.000350								
1	0	4	8	-.046056	1	0	4	4	.469717								
1	0	6	2	-.164456	1	0	4	5	.135844								
1	0	6	4	-.393809	1	0	4	8	.073178								
1	0	6	5	.168105	1	0	6	2	.141185								
1	0	6	8	-.155719	1	0	6	4	-.813572								
4	5	1/2	1/2	3/2	5/2	.263423	1	0	6	5	.052821						
		1/2	1/2	3/2	9/2	.233097	1	0	6	8	-.087056						
		1/2	1/2	3/2	11/2	-.418234	5	1	1/2	1/2	3/2	9/2	-.252726				
		1/2	1/2	5/2	5/2	.108870			1/2	1/2	3/2	11/2	-.406005				
		1/2	1/2	5/2	9/2	.307449			1/2	1/2	5/2	5/2	.000000				
		1/2	1/2	5/2	11/2	.019374			1/2	1/2	5/2	9/2	.385441				
		1/2	1/2	9/2	9/2	.116296			1/2	1/2	5/2	11/2	-.180483				
		1/2	1/2	9/2	11/2	-.346292			1/2	1/2	5/2	15/2	-.483741				
		1/2	1/2	9/2	15/2	.025219			1/2	1/2	9/2	9/2	.000000				
		1/2	1/2	11/2	11/2	-.191821			1/2	1/2	9/2	11/2	.141797				
		1/2	1/2	11/2	15/2	.101452			1/2	1/2	9/2	15/2	.465410				
		1/2	1/2	15/2	15/2	.642989			1/2	1/2	11/2	11/2	.000000				
		1	0	2	2	.499256			1/2	1/2	11/2	15/2	.345588				
		1	0	2	4	-.024058			1/2	1/2	15/2	15/2	.000000				
		1	0	2	5	-.218962			1	0	2	4	.082867				
		1	0	4	2	-.156133			1	0	2	5	-.660280				
1	0	4	4	-.231094	1	0			4	2	-.198519						
1	0	4	5	-.003672	1	0			4	4	-.114526						
1	0	4	8	-.313241	1	0	4	5	-.042446								
1	0	6	2	-.023273	1	0	4	8	.246861								
1	0	6	4	-.177733	1	0	6	2	-.456619								
1	0	6	5	.211357	1	0	6	4	.429676								
1	0	6	8	.670450	1	0	6	5	-.036229								
4	6	1/2	1/2	3/2	5/2	.508920	1	0	6	8	.217852						
		1/2	1/2	3/2	9/2	-.190175	5	2	1/2	1/2	3/2	9/2	-.220625				
		1/2	1/2	3/2	11/2	.038388			1/2	1/2	3/2	11/2	.160448				
		1/2	1/2	5/2	5/2	-.201351			1/2	1/2	5/2	5/2	.000000				
		1/2	1/2	5/2	9/2	.577907			1/2	1/2	5/2	9/2	.426460				
		1/2	1/2	5/2	11/2	.148650			1/2	1/2	5/2	11/2	-.129697				
		1/2	1/2	9/2	9/2	-.139930			1/2	1/2	5/2	15/2	-.354295				
		1/2	1/2	9/2	11/2	-.175832			1/2	1/2	9/2	9/2	.000000				
		1/2	1/2	9/2	15/2	.396972			1/2	1/2	9/2	11/2	.117063				

See page 321 for Explanation of Tables

TABLE II. The Transformation Coefficients $D_{(v) \alpha, J, J_\mu}^{T_\lambda T_\mu J}$

J	α	T_λ	T_μ	J_λ	J_μ	D	J	α	T_λ	T_μ	J_λ	J_μ	D		
$v = 6 \quad t = 1$															
5	2	1/2	1/2	9/2	15/2	-.766062	5	5	1/2	1/2	11/2	11/2	.000000		
		1/2	1/2	11/2	11/2	.000000			1/2	1/2	11/2	15/2	-.230604		
		1/2	1/2	11/2	15/2	-.028506			1/2	1/2	15/2	15/2	.000000		
		1/2	1/2	15/2	15/2	.000000			1	0	2	4	-.025276		
		1	0	2	4	.254669			1	0	2	5	-.108254		
		1	0	2	5	-.268559			1	0	4	2	.396842		
		1	0	4	2	.325995			1	0	4	4	.202325		
		1	0	4	4	-.280598			1	0	4	5	.535018		
		1	0	4	5	.433986			1	0	4	8	.551994		
		1	0	4	8	-.315053			1	0	6	2	.061564		
		1	0	6	2	.360373			1	0	6	4	-.134078		
		1	0	6	4	.341684			1	0	6	5	-.417422		
		1	0	6	5	.332083			1	0	6	8	-.047690		
		1	0	6	8	-.183067			5	6	1/2	1/2	3/2	9/2	-.095009
		1/2	1/2	3/2	11/2	-.050918					1/2	1/2	3/2	11/2	-.559638
		1/2	1/2	5/2	5/2	.000000					1/2	1/2	5/2	5/2	.000000
1/2	1/2	5/2	9/2	.298725	1/2	1/2	5/2	9/2			.391437				
1/2	1/2	5/2	11/2	-.270688	1/2	1/2	5/2	11/2			.520537				
1/2	1/2	5/2	15/2	.165729	1/2	1/2	5/2	15/2			.217617				
1/2	1/2	9/2	9/2	.000000	1/2	1/2	9/2	9/2			.000000				
1/2	1/2	9/2	11/2	.660690	1/2	1/2	9/2	11/2			-.222026				
1/2	1/2	9/2	15/2	.114000	1/2	1/2	9/2	15/2			-.080207				
1/2	1/2	11/2	11/2	.000000	1/2	1/2	11/2	11/2			.000000				
1/2	1/2	11/2	15/2	-.404911	1/2	1/2	11/2	15/2			-.387957				
1/2	1/2	15/2	15/2	.000000	1/2	1/2	15/2	15/2			.000000				
1	0	2	4	.145639	1	0	2	4			-.526098				
1	0	2	5	.086718	1	0	2	5			-.185242				
1	0	4	2	-.739981	1	0	4	2			-.079658				
1	0	4	4	-.137349	1	0	4	4			-.424017				
1	0	4	5	.231177	1	0	4	5	.186976						
1	0	4	8	.349241	1	0	4	8	.138561						
1	0	6	2	.474417	1	0	6	2	-.205434						
1	0	6	4	.062870	1	0	6	4	-.431274						
1	0	6	5	.008586	1	0	6	5	.363677						
1	0	6	8	-.017980	1	0	6	8	-.296901						
5	4	1/2	1/2	3/2	9/2	.295633	6	1	1/2	1/2	3/2	9/2	.379256		
		1/2	1/2	3/2	11/2	.225619			1/2	1/2	3/2	11/2	-.004162		
		1/2	1/2	5/2	5/2	.000000			1/2	1/2	3/2	15/2	-.346715		
		1/2	1/2	5/2	9/2	.166043			1/2	1/2	5/2	9/2	.284726		
		1/2	1/2	5/2	11/2	.692463			1/2	1/2	5/2	11/2	.195285		
		1/2	1/2	5/2	15/2	-.034375			1/2	1/2	5/2	15/2	-.168497		
		1/2	1/2	9/2	9/2	.000000			1/2	1/2	9/2	9/2	-.358132		
		1/2	1/2	9/2	11/2	.339028			1/2	1/2	9/2	11/2	-.155464		
		1/2	1/2	9/2	15/2	-.013149			1/2	1/2	9/2	15/2	-.511697		
		1/2	1/2	11/2	11/2	.000000			1/2	1/2	11/2	11/2	-.177397		
		1/2	1/2	11/2	15/2	.488188			1/2	1/2	11/2	15/2	.101091		
		1/2	1/2	15/2	15/2	.000000			1/2	1/2	15/2	15/2	-.363853		
		1	0	2	4	.014617			1	0	2	4	.014617		
		1	0	2	5	-.548705			1	0	2	5	.245434		
		1	0	2	8	-.261746			1	0	2	8	.334535		
		1	0	4	2	-.186609			1	0	4	2	.088339		
1	0	4	4	.650490	1	0	4	4	.015267						
1	0	4	5	.120718	1	0	4	5	.188753						
1	0	4	8	-.231013	1	0	4	8	-.185238						
1	0	6	2	.190204	1	0	6	2	.540960						
1	0	6	4	.212796	1	0	6	4	.002390						
1	0	6	5	.063677	1	0	6	5	-.574429						
1	0	6	8	-.137833	1	0	6	8	-.356435						
5	5	1/2	1/2	3/2	9/2	-.736553	6	2	1/2	1/2	3/2	9/2	.556945		
		1/2	1/2	3/2	11/2	.380643			1/2	1/2	3/2	11/2	-.031603		
		1/2	1/2	5/2	5/2	.000000			1/2	1/2	3/2	15/2	.047050		
		1/2	1/2	5/2	9/2	.028429			1/2	1/2	5/2	9/2	-.119312		
		1/2	1/2	5/2	11/2	.188383			1/2	1/2	5/2	11/2	-.270482		
		1/2	1/2	5/2	15/2	.194700			1/2	1/2	5/2	15/2	-.115100		
		1/2	1/2	9/2	9/2	.000000			1/2	1/2	9/2	9/2	.479038		
		1/2	1/2	9/2	11/2	.351689			1/2	1/2	9/2	11/2	.170052		
		1/2	1/2	9/2	15/2	.248059			1/2	1/2	9/2	15/2	-.242680		

See page 321 for Explanation of Tables

TABLE II. The Transformation Coefficients $D_{(v) \alpha; J \lambda \mu}^{T_x T_\mu J}$

J	α	T_x	T_μ	J_λ	J_μ	D	J	α	T_x	T_μ	J_λ	J_μ	D
$v = 6 \quad t = 1$													
6	2	1/2	1/2	11/2	11/2	.504971	6	5	1/2	1/2	9/2	11/2	.292195
		1/2	1/2	11/2	15/2	-.239150			1/2	1/2	9/2	15/2	.075340
		1/2	1/2	15/2	15/2	-.373173			1/2	1/2	11/2	11/2	-.312835
		1	0	2	4	.053226			1/2	1/2	11/2	15/2	-.282233
		1	0	2	5	-.335593			1/2	1/2	15/2	15/2	.043505
		1	0	2	8	.274203			1	0	2	4	-.542155
		1	0	4	2	-.396069			1	0	2	5	.346805
		1	0	4	4	.055592			1	0	2	8	-.016174
		1	0	4	5	.379714			1	0	4	2	.034872
		1	0	4	8	-.107807			1	0	4	4	.390944
		1	0	6	2	-.392802			1	0	4	5	.328914
		1	0	6	4	.008703			1	0	4	8	.084460
		1	0	6	5	.103524			1	0	6	2	.174212
		1	0	6	8	-.573153			1	0	6	4	.296693
6	3	1/2	1/2	3/2	9/2	.396849	1	0	6	5	.437251		
		1/2	1/2	3/2	11/2	-.120048	1	0	6	8	-.081217		
		1/2	1/2	3/2	15/2	.754092	6	6	1/2	1/2	.168027		
		1/2	1/2	5/2	9/2	-.015748	1/2	1/2	3/2	11/2	.328047		
		1/2	1/2	5/2	11/2	-.078780	1/2	1/2	3/2	15/2	-.080354		
		1/2	1/2	5/2	15/2	-.109487	1/2	1/2	5/2	9/2	.094949		
		1/2	1/2	9/2	9/2	-.213688	1/2	1/2	5/2	11/2	.670430		
		1/2	1/2	9/2	11/2	.265520	1/2	1/2	5/2	15/2	-.142825		
		1/2	1/2	9/2	15/2	-.153225	1/2	1/2	9/2	9/2	.268330		
		1/2	1/2	11/2	11/2	-.284366	1/2	1/2	9/2	11/2	.389884		
		1/2	1/2	11/2	15/2	-.001398	1/2	1/2	9/2	15/2	-.068179		
		1/2	1/2	15/2	15/2	.143165	1/2	1/2	11/2	11/2	.128552		
		1	0	2	4	.052999	1/2	1/2	11/2	15/2	.043796		
		1	0	2	5	-.077030	1/2	1/2	15/2	15/2	.362907		
1	0	2	8	.130298	1	0	2	4	.718060				
1	0	4	2	.493323	1	0	2	5	.324200				
1	0	4	4	.055355	1	0	2	8	-.193032				
1	0	4	5	.477229	1	0	4	2	-.033954				
1	0	4	8	.553564	1	0	4	4	.346676				
1	0	6	2	-.305699	1	0	4	5	.346100				
1	0	6	4	.008666	1	0	4	8	-.234288				
1	0	6	5	-.279715	1	0	6	2	.006239				
1	0	6	8	.147984	1	0	6	4	-.044947				
6	4	1/2	1/2	3/2	9/2	-.316882	1	0	6	5	.157435		
		1/2	1/2	3/2	11/2	-.666469	1	0	6	8	.138433		
		1/2	1/2	3/2	15/2	-.064332	6	7	1/2	1/2	-.639882		
		1/2	1/2	5/2	9/2	.201799	1/2	1/2	3/2	11/2	-.144138		
		1/2	1/2	5/2	11/2	.095799	1/2	1/2	3/2	15/2	-.044313		
		1/2	1/2	5/2	15/2	-.221603	1/2	1/2	5/2	9/2	.031307		
		1/2	1/2	9/2	9/2	.410765	1/2	1/2	5/2	11/2	.179872		
		1/2	1/2	9/2	11/2	.132524	1/2	1/2	5/2	15/2	.126672		
		1/2	1/2	9/2	15/2	-.235688	1/2	1/2	9/2	9/2	-.015895		
		1/2	1/2	11/2	11/2	-.316026	1/2	1/2	9/2	11/2	-.051957		
		1/2	1/2	11/2	15/2	-.089522	1/2	1/2	9/2	15/2	.398045		
		1/2	1/2	15/2	15/2	.050312	1/2	1/2	11/2	11/2	-.350926		
		1	0	2	4	-.050583	1/2	1/2	11/2	15/2	.107506		
		1	0	2	5	.606414	1/2	1/2	15/2	15/2	.471523		
1	0	2	8	.258353	1	0	2	4	-.059351				
1	0	4	2	-.529161	1	0	2	5	.364794				
1	0	4	4	-.052832	1	0	2	8	-.331632				
1	0	4	5	-.115194	1	0	4	2	.000000				
1	0	4	8	.250279	1	0	4	4	-.061991				
1	0	6	2	-.338423	1	0	4	5	-.507885				
1	0	6	4	-.008271	1	0	4	8	.135746				
1	0	6	5	-.230433	1	0	6	2	.000000				
1	0	6	8	.191173	1	0	6	4	-.009705				
6	5	1/2	1/2	3/2	9/2	.120067	1	0	6	5	.197120		
		1/2	1/2	3/2	11/2	.259123	1	0	6	8	.658982		
		1/2	1/2	3/2	15/2	-.158101	7	1	1/2	1/2	-.412030		
		1/2	1/2	5/2	9/2	.566986	1/2	1/2	3/2	15/2	.188774		
		1/2	1/2	5/2	11/2	-.336550	1/2	1/2	5/2	9/2	-.132056		
		1/2	1/2	5/2	15/2	.407321	1/2	1/2	5/2	11/2	.386745		
1/2	1/2	9/2	9/2	.149419	1/2	1/2	5/2	15/2	.754349				

See page 321 for Explanation of Tables

TABLE II. The Transformation Coefficients $D_{(v) \alpha; J \lambda J \mu}^{T_\lambda T_\mu J}$

J	α	T_λ	T_μ	J_λ	J_μ	D	J	α	T_λ	T_μ	J_λ	J_μ	D		
$v = 6 \quad \frac{1}{2} = 1$															
7	1	1/2	1/2	9/2	9/2	.000000	7	4	1	0	2	8	.222891		
		1/2	1/2	9/2	11/2	-.049031			1	0	4	4	-.502696		
		1/2	1/2	9/2	15/2	.093228			1	0	4	5	-.164162		
		1/2	1/2	11/2	11/2	.000000			1	0	4	8	-.064110		
		1/2	1/2	11/2	15/2	.217823			1	0	6	2	.016534		
		1/2	1/2	15/2	15/2	.000000			1	0	6	4	-.734240		
		1	0	2	5	-.556677			1	0	6	5	-.010333		
		1	0	2	8	.168589			1	0	6	8	-.280057		
		1	0	4	4	.254344			7	5	1/2	1/2	3/2	11/2	.277100
		1	0	4	5	.453888					1/2	1/2	3/2	15/2	.037596
		1	0	4	8	.073976					1/2	1/2	5/2	9/2	-.508125
		1	0	6	2	-.263647					1/2	1/2	5/2	11/2	.502481
		1	0	6	4	-.284186					1/2	1/2	5/2	15/2	-.350182
		1	0	6	5	-.380967					1/2	1/2	9/2	9/2	.000000
		1	0	6	8	-.300172					1/2	1/2	9/2	11/2	.288060
		7	2	1/2	1/2	3/2					11/2	.259149	1/2	1/2	9/2
1/2	1/2			3/2	15/2	-.679380	1/2	1/2			11/2	11/2	.000000		
1/2	1/2			5/2	9/2	-.255243	1/2	1/2			11/2	15/2	-.446973		
1/2	1/2			5/2	11/2	.251959	1/2	1/2			15/2	15/2	.000000		
1/2	1/2			5/2	15/2	.035312	1	0			2	5	-.281422		
1/2	1/2			9/2	9/2	.000000	1	0			2	8	-.633955		
1/2	1/2			9/2	11/2	-.256806	1	0			4	4	-.558160		
1/2	1/2			9/2	15/2	.519534	1	0			4	5	.204166		
1/2	1/2			11/2	11/2	.000000	1	0			4	8	.373600		
1/2	1/2			11/2	15/2	.074430	1	0	6	2	-.096392				
1/2	1/2			15/2	15/2	.000000	1	0	6	4	-.017794				
1	0			2	5	-.045389	1	0	6	5	.067943				
1	0			2	8	-.399587	1	0	6	8	.108973				
1	0			4	4	-.092739	7	6	1/2	1/2	3/2	11/2	.249533		
1	0			4	5	.072613			1/2	1/2	3/2	15/2	-.292778		
1	0			4	8	-.628077			1/2	1/2	5/2	9/2	.329686		
1	0	6	2	.461281	1/2	1/2			5/2	11/2	.318518				
1	0	6	4	.071586	1/2	1/2			5/2	15/2	.108299				
1	0	6	5	-.397813	1/2	1/2			9/2	9/2	.000000				
1	0	6	8	-.231855	1/2	1/2			9/2	11/2	.740965				
7	3	1/2	1/2	3/2	11/2	-.396505			1/2	1/2	9/2	15/2	-.173305		
		1/2	1/2	3/2	15/2	-.106517			1/2	1/2	11/2	11/2	.000000		
		1/2	1/2	5/2	9/2	.573001			1/2	1/2	11/2	15/2	.225999		
		1/2	1/2	5/2	11/2	-.048080			1/2	1/2	15/2	15/2	.000000		
		1/2	1/2	5/2	15/2	.024829			1	0	2	5	-.500991		
		1/2	1/2	9/2	9/2	.000000			1	0	2	8	.061707		
		1/2	1/2	9/2	11/2	.119272			1	0	4	4	.026544		
		1/2	1/2	9/2	15/2	.491422			1	0	4	5	-.696443		
		1/2	1/2	11/2	11/2	.000000			1	0	4	8	.196279		
		1/2	1/2	11/2	15/2	-.494427	1	0	6	2	.253449				
		1/2	1/2	15/2	15/2	.000000	1	0	6	4	-.090419				
		1	0	2	5	-.220117	1	0	6	5	-.306540				
		1	0	2	8	-.148508	1	0	6	8	.233578				
		1	0	4	4	.346121	8	1	1/2	1/2	3/2	15/2	-.561008		
		1	0	4	5	.105424			1/2	1/2	5/2	11/2	.188961		
		1	0	4	8	.096265			1/2	1/2	5/2	15/2	.178045		
1	0	6	2	.538863	1/2	1/2			9/2	9/2	.257569				
1	0	6	4	-.321471	1/2	1/2			9/2	11/2	-.168769				
1	0	6	5	.612117	1/2	1/2			9/2	15/2	-.487516				
1	0	6	8	-.144601	1/2	1/2			11/2	11/2	.064869				
7	4	1/2	1/2	3/2	11/2	.532102			1/2	1/2	11/2	15/2	.510730		
		1/2	1/2	3/2	15/2	.185555			1/2	1/2	15/2	15/2	-.142531		
		1/2	1/2	5/2	9/2	.257769			1	0	2	8	.690436		
		1/2	1/2	5/2	11/2	.419576			1	0	4	4	.070513		
		1/2	1/2	5/2	15/2	.218960			1	0	4	5	-.115985		
		1/2	1/2	9/2	9/2	.000000			1	0	4	8	.206657		
		1/2	1/2	9/2	11/2	-.333552			1	0	6	2	.361666		
		1/2	1/2	9/2	15/2	-.209659			1	0	6	4	.041768		
		1/2	1/2	11/2	11/2	.000000			1	0	6	5	.500003		
		1/2	1/2	11/2	15/2	-.4886613	1	0	6	8	.282164				
		1/2	1/2	15/2	15/2	.000000	8	2	1/2	1/2	3/2	15/2	-.127756		
		1	0	2	5	.220539			1/2	1/2	5/2	11/2	.166173		

See page 321 for Explanation of Tables

TABLE II. The Transformation Coefficients $D_{(v) \alpha; J \lambda}^{T, T, J}$

J	∞	T_λ	T_μ	J_λ	J_μ	D	J	∞	T_λ	T_μ	J_λ	J_μ	D
$v = 6 \quad \dagger = 1$													
8	2	1/2	1/2	5/2	15/2	.292899	8	6	1/2	1/2	5/2	11/2	-.048236
		1/2	1/2	9/2	9/2	-.352413			1/2	1/2	5/2	15/2	-.533364
	1/2	1/2	9/2	11/2	-.657365	1/2		1/2	9/2	9/2	-.595434		
	1/2	1/2	9/2	15/2	.309933	1/2		1/2	9/2	11/2	-.215197		
	1/2	1/2	11/2	11/2	.274301	1/2		1/2	9/2	15/2	-.347745		
	1/2	1/2	11/2	15/2	-.175714	1/2		1/2	11/2	11/2	-.379372		
	1/2	1/2	15/2	15/2	-.334329	1/2		1/2	11/2	15/2	-.141860		
	1	0	2	8	.154285	1/2		1/2	15/2	15/2	-.161819		
	1	0	4	4	.117415	1		0	2	8	-.260309		
	1	0	4	5	.060219	1		0	4	4	.394616		
	1	0	4	8	.055802	1		0	4	5	.485671		
	1	0	6	2	-.731586	1		0	4	8	.704821		
	1	0	6	4	.069550	1		0	6	2	.022338		
	1	0	6	5	.508385	1		0	6	4	.118463		
	1	0	6	8	-.396433	1		0	6	5	.002452		
	8	3	1/2	1/2	3/2	15/2		.335719	9	1	1/2	1/2	3/2
1/2			1/2	5/2	11/2	-.414979	1/2	1/2			5/2	15/2	.201427
1/2		1/2	5/2	15/2	.230659	1/2	1/2	5/2		9/2	.787185		
1/2		1/2	9/2	9/2	-.264758	1/2	1/2	9/2		9/2	.000000		
1/2		1/2	9/2	11/2	.259343	1/2	1/2	9/2		11/2	.009437		
1/2		1/2	9/2	15/2	-.310273	1/2	1/2	9/2		15/2	-.058937		
1/2		1/2	11/2	11/2	.528266	1/2	1/2	11/2		11/2	.000000		
1/2		1/2	11/2	15/2	.206808	1/2	1/2	11/2		15/2	-.579834		
1/2		1/2	15/2	15/2	-.326225	1/2	1/2	15/2		15/2	.000000		
1		0	2	8	.023838	1	0	2		8	-.680684		
1		0	4	4	-.620098	1	0	4		5	.000000		
1		0	4	5	.199688	1	0	4		8	-.312543		
1		0	4	8	.128082	1	0	6		4	.661012		
1		0	6	2	.083820	1	0	6		5	.000000		
1		0	6	4	.728683	1	0	6		8	.045267		
1		0	6	5	.007356	1	0	6		8	-.201427		
1	0	6	8	-.143430	1	0	6	8	-.787183				
8	4	1/2	1/2	3/2	15/2	-.186074	9	2	1/2	1/2	3/2	15/2	.000000
		1/2	1/2	5/2	11/2	-.701488			1/2	1/2	5/2	15/2	-.009437
	1/2	1/2	5/2	15/2	-.403575	1/2		1/2	5/2	9/2	.058937		
	1/2	1/2	9/2	9/2	.371096	1/2		1/2	5/2	11/2	.000000		
	1/2	1/2	9/2	11/2	-.351533	1/2		1/2	5/2	15/2	.579834		
	1/2	1/2	9/2	15/2	.149579	1/2		1/2	5/2	15/2	.000000		
	1/2	1/2	11/2	11/2	.148086	1		0	2	8	.680684		
	1/2	1/2	11/2	15/2	-.002879	1		0	4	5	.000000		
	1/2	1/2	15/2	15/2	-.069427	1		0	4	8	.312543		
	1	0	2	8	-.261755	1		0	6	4	-.661012		
	1	0	4	4	.481520	1		0	6	5	.000000		
	1	0	4	5	-.378091	1		0	6	8	-.045267		
	1	0	4	8	-.275709	1		0	6	8	-.099764		
	1	0	6	2	-.023710	1		0	6	8	-.389882		
	1	0	6	4	.624660	1		0	6	8	.000000		
	1	0	6	5	.133168	1		0	6	8	.618870		
1	0	6	8	.268623	1	0	6	8	-.442813				
8	5	1/2	1/2	3/2	15/2	.331238	9	3	1/2	1/2	3/2	15/2	.000000
		1/2	1/2	5/2	11/2	.117633			1/2	1/2	5/2	15/2	-.508878
	1/2	1/2	5/2	15/2	-.106234	1/2		1/2	5/2	15/2	.000000		
	1/2	1/2	9/2	9/2	-.068592	1		0	2	8	-.274754		
	1/2	1/2	9/2	11/2	-.265975	1		0	4	5	.000000		
	1/2	1/2	9/2	15/2	.245535	1		0	4	8	.036798		
	1/2	1/2	11/2	11/2	.225828	1		0	6	4	-.327391		
	1/2	1/2	11/2	15/2	.650685	1		0	6	5	.000000		
	1/2	1/2	15/2	15/2	.505008	1		0	6	8	.903311		
	1	0	2	8	.193008	1		0	6	8	-.760442		
	1	0	4	4	-.059518	1		0	6	8	.235595		
	1	0	4	5	.556871	1		0	6	8	-.119378		
	1	0	4	8	-.418738	1		0	6	8	.140602		
	1	0	6	2	-.324211	1		0	6	8	-.532184		
	1	0	6	4	.020754	1		0	6	8	-.221323		
	1	0	6	5	-.063649	1		0	2	8	-.195349		
1	0	6	8	.603460	1	0	4	8	-.208621				
1	0	6	8	.034428	1	0	6	4	-.699913				

See page 321 for Explanation of Tables

TABLE II. The Transformation Coefficients $D_{(v) \alpha; J_N J_\mu}^{T_\lambda T_\mu J}$

J	α	T_λ	T_μ	J_λ	J_μ	D	J	α	T_λ	T_μ	J_λ	J_μ	D
$v = 6 \quad t = 1$													
10	1	1	0	6	5	.575144	10	4	1	0	6	4	.000000
		1	0	6	8	.312486			1	0	6	5	.000000
10	2	1/2	1/2	5/2	15/2	-.142172			1	0	6	8	.212459
		1/2	1/2	9/2	11/2	.423318	11	1	1/2	1/2	9/2	15/2	.743522
		1/2	1/2	9/2	15/2	-.161117			1/2	1/2	11/2	11/2	.000000
		1/2	1/2	11/2	11/2	-.596040			1/2	1/2	11/2	15/2	.668711
		1/2	1/2	11/2	15/2	.459142			1/2	1/2	15/2	15/2	.000000
		1/2	1/2	15/2	15/2	-.456678			1	0	4	8	.799265
		1	0	2	8	.605751			1	0	6	5	.000000
		1	0	4	8	.006142			1	0	6	8	-.600982
		1	0	6	4	.630319	11	2	1/2	1/2	9/2	15/2	.668711
		1	0	6	5	.776237			1/2	1/2	11/2	11/2	.000000
		1	0	6	8	-.009199			1/2	1/2	11/2	15/2	-.743522
10	3	1/2	1/2	5/2	15/2	.000000			1/2	1/2	15/2	15/2	.000000
		1/2	1/2	9/2	11/2	.627371			1	0	4	8	.207359
		1/2	1/2	9/2	15/2	.277961			1	0	6	5	-.938591
		1/2	1/2	11/2	11/2	.627154			1	0	6	8	.275772
		1/2	1/2	11/2	15/2	.366979	12	1	1/2	1/2	9/2	15/2	-.735516
		1/2	1/2	15/2	15/2	.033896			1/2	1/2	11/2	15/2	-.600546
		1	0	2	8	.882599			1/2	1/2	15/2	15/2	-.313625
		1	0	4	8	-.339786			1	0	4	8	.984227
		1	0	6	4	.000000			1	0	6	8	-.176908
		1	0	6	5	.000000	12	2	1/2	1/2	9/2	15/2	.600928
		1	0	6	8	.324906			1/2	1/2	11/2	15/2	-.364487
10	4	1/2	1/2	5/2	15/2	.000000			1/2	1/2	15/2	15/2	-.711361
		1/2	1/2	9/2	11/2	-.765763			1	0	4	8	.176908
		1/2	1/2	9/2	15/2	.000000			1	0	6	8	.984227
		1/2	1/2	11/2	11/2	-.201593	13	1	1/2	1/2	11/2	15/2	1.000000
		1/2	1/2	11/2	15/2	-.145602			1/2	1/2	15/2	15/2	.000000
		1/2	1/2	15/2	15/2	-.593100			1	0	6	8	1.000000
		1	0	2	8	-.534058	14	1	1/2	1/2	15/2	15/2	-1.000000
		1	0	4	8	.818317			1	0	6	8	-1.000000
$v = 7 \quad t = 1/2$													
1/2	1	0	1/2	2	3/2	.415027	3/2	2	0	1/2	5	11/2	.043033
		0	1/2	2	5/2	-.604843			0	1/2	8	15/2	-.080382
		0	1/2	4	9/2	-.545959	3/2	3	0	1/2	2	3/2	.038079
		0	1/2	5	9/2	-.060945			0	1/2	2	5/2	-.591772
		0	1/2	5	11/2	.118160			0	1/2	4	5/2	.320974
		0	1/2	8	15/2	-.382322			0	1/2	4	9/2	.476997
1/2	2	0	1/2	2	3/2	.503914			0	1/2	4	11/2	.418096
		0	1/2	2	5/2	.186832			0	1/2	5	9/2	.240688
		0	1/2	4	9/2	.445203			0	1/2	5	11/2	-.291654
		0	1/2	5	9/2	-.163329			0	1/2	8	15/2	-.002934
		0	1/2	5	11/2	-.479388	5/2	1	0	1/2	2	3/2	-.143308
		0	1/2	8	15/2	-.506429			0	1/2	2	5/2	-.356195
1/2	3	0	1/2	2	3/2	-.313224			0	1/2	2	9/2	-.147876
		0	1/2	2	5/2	.343580			0	1/2	4	3/2	-.359734
		0	1/2	4	9/2	-.267852			0	1/2	4	5/2	-.535696
		0	1/2	5	9/2	.593580			0	1/2	4	9/2	-.234698
		0	1/2	5	11/2	-.012842			0	1/2	4	11/2	-.130063
		0	1/2	8	15/2	-.599664			0	1/2	5	5/2	.142867
3/2	1	0	1/2	2	3/2	-.110817			0	1/2	5	9/2	-.537600
		0	1/2	2	5/2	.309344			0	1/2	5	11/2	-.171827
		0	1/2	4	5/2	.361512			0	1/2	5	15/2	-.020554
		0	1/2	4	9/2	.140248			0	1/2	8	11/2	-.020404
		0	1/2	4	11/2	.538157			0	1/2	8	15/2	.050546
		0	1/2	5	9/2	-.267127	5/2	2	0	1/2	2	3/2	.017230
		0	1/2	5	11/2	.539131			0	1/2	2	5/2	.478525
		0	1/2	8	15/2	-.300056			0	1/2	2	9/2	-.052577
3/2	2	0	1/2	2	3/2	.896333			0	1/2	4	3/2	.420956
		0	1/2	2	5/2	-.120241			0	1/2	4	5/2	-.496973
		0	1/2	4	5/2	-.101651			0	1/2	4	9/2	-.137043
		0	1/2	4	9/2	.057003			0	1/2	4	11/2	-.119862
		0	1/2	4	11/2	.020763			0	1/2	5	5/2	.452820
		0	1/2	5	9/2	-.399754			0	1/2	5	9/2	.099057

See page 321 for Explanation of Tables

TABLE II. The Transformation Coefficients $D_{(v)l\alpha; J\lambda\mu}^{T_\lambda T_\mu J}$

J	∞	T_λ	T_μ	J_λ	J_μ	D	J	∞	T_λ	T_μ	J_λ	J_μ	D
$V = 7 \quad \xi = 1/2$													
5/2	2	0	1/2	5	11/2	.029688	7/2	1	0	1/2	5	9/2	-.156346
		0	1/2	5	15/2	.203322			0	1/2	5	11/2	.570132
		0	1/2	8	11/2	.211441			0	1/2	5	15/2	.000933
5/2	3	0	1/2	8	15/2	.093975	7/2	2	0	1/2	8	9/2	.145914
		0	1/2	2	3/2	.191992			0	1/2	8	11/2	-.279313
		0	1/2	2	5/2	-.115249			0	1/2	8	15/2	-.081743
		0	1/2	2	9/2	.066149			0	1/2	2	3/2	.209292
		0	1/2	4	3/2	.146535			0	1/2	2	5/2	.417407
		0	1/2	4	5/2	.041108			0	1/2	2	9/2	.086916
		0	1/2	4	9/2	-.327452			0	1/2	2	11/2	-.035416
		0	1/2	4	11/2	-.148643			0	1/2	4	3/2	.385732
		0	1/2	5	5/2	.238977			0	1/2	4	5/2	.006374
		0	1/2	5	9/2	.068587			0	1/2	4	9/2	.324906
		0	1/2	5	11/2	.349204			0	1/2	4	11/2	-.261231
		0	1/2	5	15/2	-.475297			0	1/2	4	15/2	.135488
5/2	4	0	1/2	8	11/2	-.517175	7/2	3	0	1/2	5	3/2	.216644
		0	1/2	8	15/2	.340389			0	1/2	5	5/2	-.007052
		0	1/2	2	3/2	.014318			0	1/2	5	9/2	-.125000
		0	1/2	2	5/2	-.099612			0	1/2	5	11/2	.124393
		0	1/2	2	9/2	-.203477			0	1/2	5	15/2	.366973
		0	1/2	4	3/2	.356012			0	1/2	8	9/2	-.345118
		0	1/2	4	5/2	-.194084			0	1/2	8	11/2	.286461
		0	1/2	4	9/2	-.331302			0	1/2	8	15/2	-.135083
		0	1/2	4	11/2	.521004			0	1/2	2	3/2	-.594343
		0	1/2	5	5/2	-.326346			0	1/2	2	5/2	.044165
		0	1/2	5	9/2	-.102140			0	1/2	2	9/2	.418567
		0	1/2	5	11/2	.253644			0	1/2	2	11/2	-.165604
5/2	5	0	1/2	5	15/2	-.284555	7/2	4	0	1/2	4	3/2	.225553
		0	1/2	8	11/2	.211667			0	1/2	4	5/2	.085438
		0	1/2	8	15/2	-.309526			0	1/2	4	9/2	-.014835
		0	1/2	2	3/2	.620626			0	1/2	4	11/2	-.251867
		0	1/2	2	5/2	.158589			0	1/2	4	15/2	-.167197
		0	1/2	2	9/2	-.577933			0	1/2	5	3/2	-.322231
		0	1/2	4	3/2	-.099953			0	1/2	5	5/2	.063026
		0	1/2	4	5/2	-.192143			0	1/2	5	9/2	.048012
		0	1/2	4	9/2	.282090			0	1/2	5	11/2	.353918
		0	1/2	4	11/2	-.065642			0	1/2	5	15/2	.146185
		0	1/2	5	5/2	-.231923			0	1/2	8	9/2	.139572
		0	1/2	5	9/2	.050018			0	1/2	8	11/2	-.126989
0	1/2	5	11/2	-.162965	0	1/2	8	15/2	-.007196				
0	1/2	5	15/2	-.143616	0	1/2	2	3/2	-.237595				
0	1/2	8	11/2	-.080302	0	1/2	2	5/2	-.027406				
0	1/2	8	15/2	.122278	0	1/2	2	9/2	.331130				
5/2	6	0	1/2	2	3/2	-.047937	7/2	5	0	1/2	2	11/2	.190626
		0	1/2	2	5/2	-.222306			0	1/2	4	3/2	-.125671
		0	1/2	2	9/2	.369616			0	1/2	4	5/2	-.283005
		0	1/2	4	3/2	-.094089			0	1/2	4	9/2	.048747
		0	1/2	4	5/2	-.527355			0	1/2	4	11/2	.496696
		0	1/2	4	9/2	.152052			0	1/2	4	15/2	.434840
		0	1/2	4	11/2	.266518			0	1/2	5	3/2	-.205556
		0	1/2	5	5/2	-.223654			0	1/2	5	5/2	.038584
		0	1/2	5	9/2	.525530			0	1/2	5	9/2	-.256003
		0	1/2	5	11/2	-.119180			0	1/2	5	11/2	-.143510
		0	1/2	5	15/2	-.033112			0	1/2	5	15/2	.208805
		0	1/2	8	11/2	-.052811			0	1/2	8	9/2	-.014971
7/2	1	0	1/2	8	15/2	.293711	7/2	5	0	1/2	8	11/2	.245843
		0	1/2	2	3/2	.232967			0	1/2	8	15/2	-.169180
		0	1/2	2	5/2	.138573			0	1/2	2	3/2	.111652
		0	1/2	2	9/2	.283936			0	1/2	2	5/2	.155524
		0	1/2	2	11/2	-.065700			0	1/2	2	9/2	-.386265
		0	1/2	4	3/2	-.349537			0	1/2	2	11/2	-.514799
		0	1/2	4	5/2	-.239466			0	1/2	4	3/2	.176333
		0	1/2	4	9/2	-.034947			0	1/2	4	5/2	-.116437
		0	1/2	4	11/2	.109706			0	1/2	4	9/2	.139951
		0	1/2	4	15/2	-.020260			0	1/2	4	11/2	.216477
		0	1/2	5	3/2	.332359			0	1/2	4	15/2	.291865
		0	1/2	5	5/2	-.287149			0	1/2	5	3/2	-.393740

See page 321 for Explanation of Tables

TABLE II. The Transformation Coefficients $D_{(v)0\alpha; J_N J_\mu}^{T_N T_\mu J}$

J	α	T_N	T_μ	J_N	J_μ	D	J	α	T_N	T_μ	J_N	J_μ	D
						$v = 7$							
						$t = 1/2$							
7/2	5	0	1/2	5	5/2	-.286251	9/2	2	0	1/2	5	9/2	.156064
		0	1/2	5	9/2	.178908			0	1/2	5	11/2	-.231619
		0	1/2	5	11/2	.112270			0	1/2	5	15/2	-.088300
		0	1/2	5	15/2	.067171			0	1/2	8	9/2	-.389059
		0	1/2	8	9/2	.241378			0	1/2	8	11/2	.066913
7/2	6	0	1/2	8	11/2	-.082947	9/2	3	0	1/2	8	15/2	.349112
		0	1/2	8	15/2	-.040059			0	1/2	2	5/2	-.145404
		0	1/2	2	3/2	.057549			0	1/2	2	9/2	-.283780
		0	1/2	2	5/2	-.171485			0	1/2	2	11/2	.226712
		0	1/2	2	9/2	-.128054			0	1/2	4	3/2	-.562882
		0	1/2	2	11/2	.022195			0	1/2	4	5/2	.274488
		0	1/2	4	3/2	-.314863			0	1/2	4	9/2	-.142573
		0	1/2	4	5/2	.046093			0	1/2	4	11/2	.201365
		0	1/2	4	9/2	.646978			0	1/2	4	15/2	-.223983
		0	1/2	4	11/2	-.049572			0	1/2	5	3/2	-.103109
		0	1/2	4	15/2	-.034813			0	1/2	5	5/2	.174661
		0	1/2	5	3/2	-.189419			0	1/2	5	9/2	-.014951
		0	1/2	5	5/2	.415748			0	1/2	5	11/2	.004068
		0	1/2	5	9/2	-.022664			0	1/2	5	15/2	.055422
		7/2	7	0	1/2	5			11/2	.344330	9/2	4	0
0	1/2			5	15/2	-.221969	0	1/2	8	11/2			.291077
0	1/2			8	9/2	.044452	0	1/2	8	15/2			-.375563
0	1/2			8	11/2	.197083	0	1/2	2	5/2			.540108
0	1/2			8	15/2	-.094806	0	1/2	2	9/2			.007474
0	1/2			2	3/2	-.277969	0	1/2	2	11/2			.150513
0	1/2			2	5/2	.544994	0	1/2	4	3/2			-.090681
0	1/2			2	9/2	-.077565	0	1/2	4	5/2			-.264705
0	1/2			2	11/2	.341589	0	1/2	4	9/2			-.229766
0	1/2			4	3/2	.036311	0	1/2	4	11/2			-.349365
0	1/2			4	5/2	-.131495	0	1/2	4	15/2			-.263192
0	1/2			4	9/2	.071167	0	1/2	5	3/2			.150842
0	1/2			4	11/2	.243196	0	1/2	5	5/2			-.158812
0	1/2			4	15/2	-.004819	0	1/2	5	9/2			-.088697
0	1/2			5	3/2	.146013	0	1/2	5	11/2			-.281954
9/2	1	0	1/2	5	5/2	.030592	9/2	5	0	1/2	5	15/2	.361688
		0	1/2	5	9/2	.537050			0	1/2	8	9/2	.309285
		0	1/2	5	11/2	.103773			0	1/2	8	11/2	-.035372
		0	1/2	5	15/2	-.296820			0	1/2	8	15/2	.009821
		0	1/2	8	9/2	-.019018			0	1/2	2	5/2	-.018338
		0	1/2	8	11/2	.050466			0	1/2	2	9/2	-.055858
		0	1/2	8	15/2	.087839			0	1/2	2	11/2	-.377133
		0	1/2	2	5/2	-.265353			0	1/2	4	3/2	.245791
		0	1/2	2	9/2	-.069204			0	1/2	4	5/2	-.099753
		0	1/2	2	11/2	-.482447			0	1/2	4	9/2	-.201425
		0	1/2	4	3/2	-.066587			0	1/2	4	11/2	.069182
		0	1/2	4	5/2	.057223			0	1/2	4	15/2	.182938
		0	1/2	4	9/2	.006473			0	1/2	5	3/2	.171470
		0	1/2	4	11/2	-.061763			0	1/2	5	5/2	.399159
		0	1/2	4	15/2	-.198939			0	1/2	5	9/2	.387703
0	1/2	5	3/2	-.424987	0	1/2	5	11/2	.284820				
9/2	2	0	1/2	5	5/2	-.229598	9/2	6	0	1/2	5	15/2	.344685
		0	1/2	5	9/2	.312838			0	1/2	8	9/2	.387167
		0	1/2	5	11/2	-.484680			0	1/2	8	11/2	.058678
		0	1/2	5	15/2	.205904			0	1/2	8	15/2	-.113183
		0	1/2	8	9/2	-.005311			0	1/2	2	5/2	-.191525
		0	1/2	8	11/2	.073502			0	1/2	2	9/2	-.311542
		0	1/2	8	15/2	.164202			0	1/2	2	11/2	.107061
		0	1/2	2	5/2	.213472			0	1/2	4	3/2	-.108634
		0	1/2	2	9/2	.189769			0	1/2	4	5/2	-.587833
		0	1/2	2	11/2	-.015064			0	1/2	4	9/2	.189984
		0	1/2	4	3/2	-.359589			0	1/2	4	11/2	-.216609
		0	1/2	4	5/2	-.057151			0	1/2	4	15/2	.058784
		0	1/2	4	9/2	-.372513			0	1/2	5	3/2	-.396187
		0	1/2	4	11/2	.103318			0	1/2	5	5/2	.347819
		0	1/2	4	15/2	.140510			0	1/2	5	9/2	-.170465
0	1/2	5	3/2	.031510	0	1/2	5	11/2	.062865				
0	1/2	5	5/2	.501916	0	1/2	5	15/2	-.111415				

See page 321 for Explanation of Tables

TABLE II. The Transformation Coefficients $D_{(v) \alpha; J_N J_\mu}^{T, T', J}$

J	α	T_λ	T_μ	J_λ	J_μ	D	J	α	T_λ	T_μ	J_λ	J_μ	D
$v = 7 \quad t = 1/2$													
9/2	6	0	1/2	8	9/2	.191914	11/2	3	0	1/2	8	9/2	.227182
		0	1/2	8	11/2	-.122792			0	1/2	8	11/2	-.259253
		0	1/2	8	15/2	.188957			0	1/2	8	15/2	.037206
9/2	7	0	1/2	2	5/2	-.225725	11/2	4	0	1/2	2	9/2	-.028936
		0	1/2	2	9/2	.258008			0	1/2	2	11/2	.293140
		0	1/2	2	11/2	.068377			0	1/2	2	15/2	.242972
		0	1/2	4	3/2	-.011408			0	1/2	4	3/2	-.062412
		0	1/2	4	5/2	-.421960			0	1/2	4	5/2	.460383
		0	1/2	4	9/2	.258500			0	1/2	4	9/2	-.343230
		0	1/2	4	11/2	.022262			0	1/2	4	11/2	.481365
		0	1/2	4	15/2	-.538004			0	1/2	4	15/2	.202707
		0	1/2	5	3/2	.327871			0	1/2	5	3/2	.195908
		0	1/2	5	5/2	.058153			0	1/2	5	5/2	.015028
		0	1/2	5	9/2	.248430			0	1/2	5	9/2	-.091961
		0	1/2	5	11/2	.069485			0	1/2	5	11/2	.137341
0	1/2	5	15/2	-.022344	0	1/2	5	15/2	.086184				
0	1/2	8	9/2	-.176859	0	1/2	8	5/2	.334029				
0	1/2	8	11/2	.362834	0	1/2	8	9/2	-.207262				
0	1/2	8	15/2	-.044769	0	1/2	8	11/2	-.087138				
11/2	1	0	1/2	2	9/2	-.012852	11/2	5	0	1/2	8	15/2	-.110725
		0	1/2	2	11/2	.248461			0	1/2	2	9/2	-.174191
		0	1/2	2	15/2	.206678			0	1/2	2	11/2	.370908
		0	1/2	4	3/2	.336149			0	1/2	2	15/2	-.329216
		0	1/2	4	5/2	-.294597			0	1/2	4	3/2	.028902
		0	1/2	4	9/2	-.390671			0	1/2	4	5/2	.097999
		0	1/2	4	11/2	-.054884			0	1/2	4	9/2	-.070200
		0	1/2	4	15/2	-.170949			0	1/2	4	11/2	.179657
		0	1/2	5	3/2	.381901			0	1/2	4	15/2	-.109179
		0	1/2	5	5/2	.270049			0	1/2	5	3/2	-.125394
		0	1/2	5	9/2	-.183731			0	1/2	5	5/2	.122623
		0	1/2	5	11/2	-.252347			0	1/2	5	9/2	-.107413
		0	1/2	5	15/2	-.161301			0	1/2	5	11/2	-.242309
		0	1/2	8	5/2	-.196997			0	1/2	5	15/2	.421408
		0	1/2	8	9/2	.141589			0	1/2	8	5/2	-.252054
0	1/2	8	11/2	-.291837	0	1/2	8	9/2	.358897				
0	1/2	8	15/2	.156494	0	1/2	8	11/2	.332544				
11/2	2	0	1/2	2	9/2	.027633	11/2	6	0	1/2	8	15/2	-.287434
		0	1/2	2	11/2	-.172027			0	1/2	2	9/2	-.754886
		0	1/2	2	15/2	-.155095			0	1/2	2	11/2	.047545
		0	1/2	4	3/2	-.216114			0	1/2	2	15/2	-.013660
		0	1/2	4	5/2	-.398925			0	1/2	4	3/2	-.102750
		0	1/2	4	9/2	-.048207			0	1/2	4	5/2	.111373
		0	1/2	4	11/2	.436698			0	1/2	4	9/2	.278613
		0	1/2	4	15/2	-.231269			0	1/2	4	11/2	.172231
		0	1/2	5	3/2	.014596			0	1/2	4	15/2	-.072185
		0	1/2	5	5/2	-.351983			0	1/2	5	3/2	.044704
		0	1/2	5	9/2	-.328400			0	1/2	5	5/2	-.181479
		0	1/2	5	11/2	.183744			0	1/2	5	9/2	-.032358
		0	1/2	5	15/2	.226877			0	1/2	5	11/2	-.301647
		0	1/2	8	5/2	-.168980			0	1/2	5	15/2	-.380547
		0	1/2	8	9/2	-.102872			0	1/2	8	5/2	-.015287
0	1/2	8	11/2	-.357330	0	1/2	8	9/2	-.035012				
0	1/2	8	15/2	-.096018	0	1/2	8	11/2	-.109494				
11/2	3	0	1/2	2	9/2	-.039791	11/2	7	0	1/2	8	15/2	.083686
		0	1/2	2	11/2	-.195419			0	1/2	2	9/2	.087984
		0	1/2	2	15/2	-.455398			0	1/2	2	11/2	.253883
		0	1/2	4	3/2	-.151400			0	1/2	2	15/2	.138477
		0	1/2	4	5/2	.196298			0	1/2	4	3/2	-.540151
		0	1/2	4	9/2	-.120494			0	1/2	4	5/2	.078822
		0	1/2	4	11/2	-.258163			0	1/2	4	9/2	.073273
		0	1/2	4	15/2	.189887			0	1/2	4	11/2	-.404308
		0	1/2	5	3/2	-.028528			0	1/2	4	15/2	-.006032
		0	1/2	5	5/2	.233387			0	1/2	5	3/2	.462120
		0	1/2	5	9/2	-.549587			0	1/2	5	5/2	-.222536
		0	1/2	5	11/2	.007007			0	1/2	5	9/2	-.255368
		0	1/2	5	15/2	-.095367			0	1/2	5	11/2	.012004
		0	1/2	8	5/2	.295773			0	1/2	5	15/2	.011746

See page 321 for Explanation of Tables

TABLE II. The Transformation Coefficients $D_{(v) \alpha; J_\lambda J_\mu}^{T_\lambda T_\mu J}$

J	α	T_λ	T_μ	J_λ	J_μ	D	J	α	T_λ	T_μ	J_λ	J_μ	D
						$v = 7$							
						$t = 1/2$							
11/2	7	0	1/2	8	5/2	-.235011	13/2	3	0	1/2	8	3/2	.548236
		0	1/2	8	9/2	-.106180			0	1/2	8	5/2	.041608
		0	1/2	8	11/2	.207453			0	1/2	8	9/2	.132437
		0	1/2	8	15/2	-.060556			0	1/2	8	11/2	-.283104
11/2	8	0	1/2	2	9/2	.418767	13/2	4	0	1/2	8	15/2	.062705
		0	1/2	2	11/2	-.270051			0	1/2	2	9/2	-.138426
		0	1/2	2	15/2	.115864			0	1/2	2	11/2	-.455148
		0	1/2	4	3/2	.211213			0	1/2	2	15/2	-.018750
		0	1/2	4	5/2	.404683			0	1/2	4	5/2	.027788
		0	1/2	4	9/2	.413049			0	1/2	4	9/2	-.387572
		0	1/2	4	11/2	.265770			0	1/2	4	11/2	-.317222
		0	1/2	4	15/2	-.252228			0	1/2	4	15/2	-.189374
		0	1/2	5	3/2	.191857			0	1/2	5	3/2	-.039610
		0	1/2	5	5/2	.013059			0	1/2	5	5/2	-.387969
		0	1/2	5	9/2	-.260140			0	1/2	5	9/2	.084992
		0	1/2	5	11/2	-.244043			0	1/2	5	11/2	-.055752
0	1/2	5	15/2	-.139672	0	1/2	5	15/2	.183823				
0	1/2	8	5/2	-.122620	0	1/2	8	3/2	.242691				
0	1/2	8	9/2	.132935	0	1/2	8	5/2	.380421				
0	1/2	8	11/2	.028258	0	1/2	8	9/2	.237642				
0	1/2	8	15/2	-.088455	0	1/2	8	11/2	.068434				
13/2	1	0	1/2	2	9/2	-.021954	13/2	5	0	1/2	8	15/2	-.157682
		0	1/2	2	11/2	-.092782			0	1/2	2	9/2	-.471613
		0	1/2	2	15/2	-.032554			0	1/2	2	11/2	-.386215
		0	1/2	4	5/2	.671908			0	1/2	2	15/2	-.376234
		0	1/2	4	9/2	.015252			0	1/2	4	5/2	.031847
		0	1/2	4	11/2	-.317474			0	1/2	4	9/2	.211679
		0	1/2	4	15/2	.409561			0	1/2	4	11/2	.250622
		0	1/2	5	3/2	.255137			0	1/2	4	15/2	-.033376
		0	1/2	5	5/2	.184753			0	1/2	5	3/2	-.351364
		0	1/2	5	9/2	.110522			0	1/2	5	5/2	.379702
		0	1/2	5	11/2	.095467			0	1/2	5	9/2	.183133
		0	1/2	5	15/2	.001238			0	1/2	5	11/2	-.040304
		0	1/2	8	3/2	.181494			0	1/2	5	15/2	-.170170
		0	1/2	8	5/2	-.178179			0	1/2	8	3/2	.158458
		0	1/2	8	9/2	.116572			0	1/2	8	5/2	-.027759
		0	1/2	8	11/2	.220899			0	1/2	8	9/2	.016105
0	1/2	8	15/2	.148303	0	1/2	8	11/2	-.007048				
13/2	2	0	1/2	2	9/2	.110895	13/2	6	0	1/2	8	15/2	-.138497
		0	1/2	2	11/2	.026846			0	1/2	2	9/2	.175788
		0	1/2	2	15/2	.146390			0	1/2	2	11/2	.261894
		0	1/2	4	5/2	.236789			0	1/2	2	15/2	-.443010
		0	1/2	4	9/2	.014034			0	1/2	4	5/2	-.062615
		0	1/2	4	11/2	-.031886			0	1/2	4	9/2	.017796
		0	1/2	4	15/2	.232531			0	1/2	4	11/2	-.201787
		0	1/2	5	3/2	-.274139			0	1/2	4	15/2	.081688
		0	1/2	5	5/2	-.196778			0	1/2	5	3/2	-.041992
		0	1/2	5	9/2	.092395			0	1/2	5	5/2	-.192465
		0	1/2	5	11/2	-.250565			0	1/2	5	9/2	.103650
		0	1/2	5	15/2	.041418			0	1/2	5	11/2	.475584
0	1/2	8	3/2	.027425	0	1/2	5	15/2	-.270288				
0	1/2	8	5/2	-.290818	0	1/2	8	3/2	.171275				
0	1/2	8	9/2	.082612	0	1/2	8	5/2	.071958				
0	1/2	8	11/2	-.604645	0	1/2	8	9/2	-.250729				
0	1/2	8	15/2	-.457757	0	1/2	8	11/2	.109278				
13/2	3	0	1/2	2	9/2	.287081	13/2	7	0	1/2	8	15/2	-.441043
		0	1/2	2	11/2	-.196235			0	1/2	2	9/2	.247573
		0	1/2	2	15/2	-.025171			0	1/2	2	11/2	-.151175
		0	1/2	4	5/2	-.259678			0	1/2	2	15/2	.015098
		0	1/2	4	9/2	.289341			0	1/2	4	5/2	-.036678
		0	1/2	4	11/2	.198252			0	1/2	4	9/2	-.396697
		0	1/2	4	15/2	.116546			0	1/2	4	11/2	.099811
		0	1/2	5	3/2	.291850			0	1/2	4	15/2	-.274020
		0	1/2	5	5/2	.095411			0	1/2	5	3/2	.459008
		0	1/2	5	9/2	.025022			0	1/2	5	5/2	.340466
		0	1/2	5	11/2	.240728			0	1/2	5	9/2	.124924
		0	1/2	5	15/2	.342982			0	1/2	5	11/2	-.282188

See page 321 for Explanation of Tables

TABLE II. The Transformation Coefficients $D_{(vt)\alpha_i J_i J_\mu}^{T_i T_\mu J}$

J	α	T_i	T_μ	J_i	J_μ	D	J	α	T_i	T_μ	J_i	J_μ	D
$v = 7 \quad t = 1/2$													
13/2	7	0	1/2	5	15/2	-.283071	15/2	4	0	1/2	4	9/2	-.127959
		0	1/2	8	3/2	.118714			0	1/2	4	11/2	.196993
		0	1/2	8	5/2	-.201011			0	1/2	4	15/2	.160951
		0	1/2	8	9/2	-.141614			0	1/2	5	5/2	.133783
		0	1/2	8	11/2	.021756			0	1/2	5	9/2	-.031633
		0	1/2	8	15/2	-.308003			0	1/2	5	11/2	.199701
13/2	8	0	1/2	2	9/2	.407609	15/2	5	0	1/2	2	11/2	-.224716
		0	1/2	2	11/2	-.056259			0	1/2	8	3/2	-.491052
		0	1/2	2	15/2	.130007			0	1/2	8	5/2	.343456
		0	1/2	4	5/2	.182228			0	1/2	8	9/2	-.185577
		0	1/2	4	9/2	.194905			0	1/2	8	11/2	-.307974
		0	1/2	4	11/2	-.132935			0	1/2	8	15/2	.395677
		0	1/2	4	15/2	-.239374			0	1/2	2	11/2	.120823
		0	1/2	5	3/2	-.310624			0	1/2	2	15/2	-.083978
		0	1/2	5	5/2	.290913			0	1/2	4	9/2	-.056903
		0	1/2	5	9/2	-.505727			0	1/2	4	11/2	-.297764
		0	1/2	5	11/2	.027122			0	1/2	4	15/2	.684330
		0	1/2	5	15/2	-.228856			0	1/2	5	5/2	.121427
15/2	1	0	1/2	8	3/2	.094451	15/2	6	0	1/2	5	9/2	-.004082
		0	1/2	8	5/2	.203116			0	1/2	5	11/2	-.423211
		0	1/2	8	9/2	.316740			0	1/2	5	15/2	.100377
		0	1/2	8	11/2	.090568			0	1/2	8	3/2	-.122706
		0	1/2	8	15/2	-.137587			0	1/2	8	5/2	-.071698
		0	1/2	2	11/2	-.254245			0	1/2	8	9/2	.246060
		0	1/2	2	15/2	.074569			0	1/2	8	11/2	-.343950
		0	1/2	4	9/2	-.645432			0	1/2	8	15/2	-.123090
		0	1/2	4	11/2	-.067136			0	1/2	2	11/2	.088179
		0	1/2	4	15/2	-.095254			0	1/2	2	15/2	.375034
		0	1/2	5	5/2	-.474572			0	1/2	4	9/2	.080818
		0	1/2	5	9/2	-.084195			0	1/2	4	11/2	-.153417
		0	1/2	5	11/2	.042793			0	1/2	4	15/2	-.047582
		0	1/2	5	15/2	.417075			0	1/2	5	5/2	-.452417
		0	1/2	8	3/2	-.270330			0	1/2	5	9/2	.106504
		0	1/2	8	5/2	.019009			0	1/2	5	11/2	-.488942
		0	1/2	8	9/2	.096449			0	1/2	5	15/2	-.397237
		0	1/2	8	11/2	-.037331			0	1/2	8	3/2	-.031107
0	1/2	8	15/2	-.086080	0	1/2	8	5/2	.270277				
15/2	2	0	1/2	2	11/2	-.404140	15/2	7	0	1/2	8	9/2	-.136473
		0	1/2	2	15/2	-.126974			0	1/2	8	11/2	.233188
		0	1/2	4	9/2	-.297187			0	1/2	8	15/2	-.243592
		0	1/2	4	11/2	.318694			0	1/2	2	11/2	-.454559
		0	1/2	4	15/2	.236161			0	1/2	2	15/2	.300643
		0	1/2	5	5/2	.328871			0	1/2	4	9/2	.032394
		0	1/2	5	9/2	.187375			0	1/2	4	11/2	-.228864
		0	1/2	5	11/2	-.047411			0	1/2	4	15/2	-.045584
		0	1/2	5	15/2	-.057353			0	1/2	5	5/2	.142558
		0	1/2	8	3/2	.212465			0	1/2	5	9/2	.666443
		0	1/2	8	5/2	.444821			0	1/2	5	11/2	-.076510
		0	1/2	8	9/2	-.225253			0	1/2	5	15/2	.033001
15/2	3	0	1/2	8	11/2	.084603	17/2	1	0	1/2	8	3/2	.018876
		0	1/2	8	15/2	-.353814			0	1/2	8	5/2	-.163958
		0	1/2	2	11/2	.329678			0	1/2	8	9/2	.165102
		0	1/2	2	15/2	-.228690			0	1/2	8	11/2	.036651
		0	1/2	4	9/2	-.149654			0	1/2	8	15/2	.346746
		0	1/2	4	11/2	.254635			0	1/2	2	15/2	.582772
		0	1/2	4	15/2	-.196417			0	1/2	4	9/2	.051104
		0	1/2	5	5/2	-.020737			0	1/2	4	11/2	.172014
		0	1/2	5	9/2	.198953			0	1/2	4	15/2	-.131247
		0	1/2	5	11/2	-.208016			0	1/2	5	9/2	-.370252
		0	1/2	5	15/2	.020063			0	1/2	5	11/2	-.089825
		0	1/2	8	3/2	.119446			0	1/2	5	15/2	.361360
15/2	4	0	1/2	8	5/2	.416897	17/2	2	0	1/2	8	3/2	-.005880
		0	1/2	8	9/2	.609240			0	1/2	8	5/2	.196328
		0	1/2	8	11/2	.050492			0	1/2	8	9/2	-.349643
		0	1/2	8	15/2	.260230			0	1/2	8	11/2	-.417492
		0	1/2	2	11/2	-.138763			0	1/2	8	15/2	.009263
		0	1/2	2	15/2	.381369			0	1/2	2	15/2	-.026613

See page 321 for Explanation of Tables

TABLE II. The Transformation Coefficients $D_{(v) \alpha_i J_i J_\mu}^{T_\lambda T_\mu J}$

J	α	T_λ	T_μ	J_λ	J_μ	D	J	α	T_λ	T_μ	J_λ	J_μ	D		
						$v = 7$									
						$t = 1/2$									
17/2	2	0	1/2	4	9/2	-.041052	19/2	1	0	1/2	8	9/2	-.311315		
		0	1/2	4	11/2	-.457696			0	1/2	8	11/2	-.227625		
	0	1/2	4	15/2	-.148016	0		1/2	8	15/2	-.275983				
	0	1/2	5	9/2	.577057	19/2		2	0	1/2	2	15/2	.392284		
	0	1/2	5	11/2	.240657				0	1/2	4	11/2	-.278268		
	0	1/2	5	15/2	.292824	0		1/2	4	15/2	-.133614				
	0	1/2	8	3/2	.138178	0		1/2	5	9/2	-.091791				
	0	1/2	8	5/2	.002024	0		1/2	5	11/2	.372883				
	0	1/2	8	9/2	-.515095	0		1/2	5	15/2	-.400475				
	0	1/2	8	11/2	-.064605	0		1/2	8	3/2	-.122798				
	0	1/2	8	15/2	-.031017	0		1/2	8	5/2	.130926				
	17/2	3	0	1/2	2	15/2		.259064	19/2	3	0	1/2	8	9/2	.208745
			0	1/2	4	9/2		-.695952			0	1/2	8	11/2	.446283
		0	1/2	4	11/2	.316427		0		1/2	8	15/2	-.409897		
0		1/2	4	15/2	.229375	0	1/2	2		15/2	-.478930				
0		1/2	5	9/2	.014329	0	1/2	4		11/2	.106907				
0		1/2	5	11/2	.319651	0	1/2	4		15/2	-.511932				
0		1/2	5	15/2	-.084422	0	1/2	5		9/2	.118814				
0		1/2	8	3/2	.135518	0	1/2	5		11/2	.302815				
0		1/2	8	5/2	-.257324	0	1/2	5		15/2	-.368344				
0		1/2	8	9/2	-.187859	0	1/2	8		3/2	.069680				
0		1/2	8	11/2	.217622	0	1/2	8		5/2	.164261				
0		1/2	8	15/2	.138047	0	1/2	8		9/2	-.350860				
17/2		4	0	1/2	2	15/2	-.345913	19/2		4	0	1/2	8	11/2	.161329
			0	1/2	4	9/2	-.134793				0	1/2	8	15/2	.273248
	0	1/2	4	11/2	-.001065	0	1/2		2	15/2	-.165473				
	0	1/2	4	15/2	-.321563	0	1/2		4	11/2	.367503				
	0	1/2	5	9/2	-.323044	0	1/2		4	15/2	-.029804				
	0	1/2	5	11/2	-.018050	0	1/2		5	9/2	.469811				
	0	1/2	5	15/2	.374604	0	1/2		5	11/2	.282704				
	0	1/2	8	3/2	.643203	0	1/2		5	15/2	.506060				
	0	1/2	8	5/2	-.271114	0	1/2		8	3/2	-.269297				
	0	1/2	8	9/2	.145128	0	1/2		8	5/2	-.055597				
	0	1/2	8	11/2	-.043516	0	1/2		8	9/2	.034875				
	0	1/2	8	15/2	-.059931	0	1/2		8	11/2	.286892				
	17/2	5	0	1/2	2	15/2	-.138891		19/2	5	0	1/2	8	15/2	-.347559
			0	1/2	4	9/2	.154197				0	1/2	2	15/2	-.025290
0		1/2	4	11/2	.330751	0	1/2	4		11/2	.127445				
0		1/2	4	15/2	-.063513	0	1/2	4		15/2	-.053923				
0		1/2	5	9/2	.168100	0	1/2	5		9/2	-.609040				
0		1/2	5	11/2	-.591244	0	1/2	5		11/2	.257047				
0		1/2	5	15/2	.101541	0	1/2	5		15/2	.078087				
0		1/2	8	3/2	-.076611	0	1/2	8		3/2	-.588482				
0		1/2	8	5/2	-.348225	0	1/2	8		5/2	-.386618				
0		1/2	8	9/2	-.381835	0	1/2	8		9/2	-.165547				
0		1/2	8	11/2	.212583	0	1/2	8		11/2	-.065129				
0		1/2	8	15/2	.370466	0	1/2	8		15/2	.098377				
17/2		6	0	1/2	2	15/2	.229186	19/2		6	0	1/2	2	15/2	-.333971
			0	1/2	4	9/2	-.244432				0	1/2	4	11/2	-.423818
	0	1/2	4	11/2	-.556995	0	1/2		4	15/2	.545308				
	0	1/2	4	15/2	-.397504	0	1/2		5	9/2	.194346				
	0	1/2	5	9/2	-.301155	0	1/2		5	11/2	.479129				
	0	1/2	5	11/2	-.173191	0	1/2		5	15/2	-.128981				
	0	1/2	5	15/2	-.117403	0	1/2		8	3/2	.080638				
	0	1/2	8	3/2	-.345136	0	1/2		8	5/2	-.272311				
	0	1/2	8	5/2	-.338919	0	1/2		8	9/2	-.093988				
	0	1/2	8	9/2	.009553	0	1/2		8	11/2	-.187296				
	0	1/2	8	11/2	.225665	0	1/2		8	15/2	-.054222				
	19/2	1	0	1/2	8	15/2	-.000369		21/2	1	0	1/2	4	15/2	.247736
			0	1/2	2	15/2	-.150451				0	1/2	5	11/2	.019641
		0	1/2	4	11/2	-.500983	0			1/2	5	15/2	.346421		
0		1/2	4	15/2	-.134710	0	1/2	8		5/2	-.484179				
0		1/2	5	9/2	-.073350	0	1/2	8		9/2	-.307965				
0		1/2	5	11/2	-.112284	0	1/2	8		11/2	.673661				
0		1/2	5	15/2	.293270	0	1/2	8		15/2	.187468				
0		1/2	8	3/2	-.307785	21/2	2	0		1/2	4	15/2	-.684579		
0		1/2	8	5/2	.533492			0		1/2	5	11/2	.352775		

See page 321 for Explanation of Tables

TABLE II. The Transformation Coefficients $D_{(v)\alpha_i J_\lambda J_\mu}^{T_\lambda T_\mu J}$

J	α	T_λ	T_μ	J_λ	J_μ	D	J	α	T_λ	T_μ	J_λ	J_μ	D
$v = 7 \quad t = 1/2$													
21/2	2	0	1/2	5	15/2	.366704	23/2	2	0	1/2	5	15/2	-.342196
		0	1/2	8	5/2	.280606			0	1/2	8	9/2	.666781
		0	1/2	8	9/2	.077172			0	1/2	8	11/2	.240406
		0	1/2	8	11/2	.357838			0	1/2	8	15/2	.595661
		0	1/2	8	15/2	-.244307	23/2	3	0	1/2	4	15/2	.721706
21/2	3	0	1/2	4	15/2	.136853			0	1/2	5	15/2	-.270982
		0	1/2	5	11/2	.309234			0	1/2	8	9/2	.115729
		0	1/2	5	15/2	.426893			0	1/2	8	11/2	.543955
		0	1/2	8	5/2	-.529152			0	1/2	8	15/2	-.310532
		0	1/2	8	9/2	.420208	25/2	1	0	1/2	5	15/2	.494594
		0	1/2	8	11/2	-.377060			0	1/2	8	9/2	-.792532
		0	1/2	8	15/2	-.323507			0	1/2	8	11/2	-.147211
21/2	4	0	1/2	4	15/2	.044935			0	1/2	8	15/2	.324959
		0	1/2	5	11/2	-.679095	25/2	2	0	1/2	5	15/2	-.354897
		0	1/2	5	15/2	.137088			0	1/2	8	9/2	.185618
		0	1/2	8	5/2	.082635			0	1/2	8	11/2	-.507314
		0	1/2	8	9/2	.624309			0	1/2	8	15/2	.763037
		0	1/2	8	11/2	.317522	25/2	3	0	1/2	5	15/2	-.610149
		0	1/2	8	15/2	-.143552			0	1/2	8	9/2	-.401516
23/2	1	0	1/2	4	15/2	-.381774			0	1/2	8	11/2	.639744
		0	1/2	5	15/2	-.693469			0	1/2	8	15/2	.239228
		0	1/2	8	9/2	.127027	27/2	1	0	1/2	8	11/2	.910259
		0	1/2	8	11/2	-.189549			0	1/2	8	15/2	.414039
		0	1/2	8	15/2	-.566820	29/2	1	0	1/2	8	15/2	-.100000
23/2	2	0	1/2	4	15/2	-.160305	31/2	1	0	1/2	8	15/2	1.00000
$v = 8 \quad t = 0$													
0	1	0	0	2	2	.535736	3	2	0	0	4	5	.024980
		0	0	4	4	.202729			0	0	5	5	.000000
		0	0	5	5	-.794625			0	0	5	8	-.317696
		0	0	8	8	.201146			0	0	8	8	.000000
1	1	0	0	2	2	.000000	4	1	0	0	2	2	-.141607
		0	0	4	4	.000000			0	0	2	4	-.006822
		0	0	4	5	-.100000			0	0	2	5	-.078909
		0	0	5	5	.000000			0	0	4	4	.002238
		0	0	8	8	.000000			0	0	4	5	.278773
2	1	0	0	2	2	.041542			0	0	4	8	.467328
		0	0	2	4	-.594380			0	0	5	5	-.341397
		0	0	4	4	-.209116			0	0	5	8	-.333184
		0	0	4	5	-.208986			0	0	8	8	-.670818
		0	0	5	5	-.695664	4	2	0	0	2	2	-.221939
		0	0	8	8	.271356			0	0	2	4	.159157
2	2	0	0	2	2	-.396278			0	0	2	5	.105071
		0	0	2	4	-.424863			0	0	4	4	-.616816
		0	0	4	4	.792439			0	0	4	5	.539996
		0	0	4	5	.116405			0	0	4	8	-.311261
		0	0	5	5	.009844			0	0	5	5	.136500
		0	0	8	8	-.144390			0	0	5	8	.305556
2	3	0	0	2	2	.843756			0	0	8	8	-.182852
		0	0	2	4	.060156	4	3	0	0	2	2	-.258096
		0	0	4	4	.411143			0	0	2	4	.080317
		0	0	4	5	.255815			0	0	2	5	.674528
		0	0	5	5	-.218987			0	0	4	4	.044838
		0	0	8	8	-.044955			0	0	4	5	.074705
3	1	0	0	2	2	.000000			0	0	4	8	.378605
		0	0	2	4	-.616200			0	0	5	5	-.379047
		0	0	2	5	.240380			0	0	5	8	.253484
		0	0	4	4	.000000			0	0	8	8	.336278
		0	0	4	5	-.651371	4	4	0	0	2	2	.667221
		0	0	5	5	.000000			0	0	2	4	.141671
		0	0	5	8	-.371793			0	0	2	5	-.296252
		0	0	8	8	.000000			0	0	4	4	.048428
3	2	0	0	2	2	.000000			0	0	4	5	.325369
		0	0	2	4	.483353			0	0	4	8	.253563
		0	0	2	5	.815362			0	0	5	5	-.235974
		0	0	4	4	.000000			0	0	5	8	.457489

See page 321 for Explanation of Tables

TABLE II. The Transformation Coefficients $D_{(w)0\alpha; J_\lambda J_\mu}^{T_\lambda T_\mu J}$

J	α	T_λ	T_μ	J_λ	J_μ	D	J	α	T_λ	T_μ	J_λ	J_μ	D
$v = 8 \quad t = 0$													
4	4	0	0	8	8	.097447	6	4	0	0	5	5	-.109076
4	5	0	0	2	2	.271225			0	0	5	8	-.072543
		0	0	2	4	-.705802			0	0	8	8	-.031271
		0	0	2	5	.133473	6	5	0	0	2	4	-.266690
		0	0	4	4	-.302008			0	0	2	5	-.161416
		0	0	4	5	.031670			0	0	2	8	.484315
		0	0	4	8	-.274200			0	0	4	4	-.502578
		0	0	5	5	-.453272			0	0	4	5	.025935
		0	0	5	8	-.178896			0	0	4	8	.042095
5	1	0	0	8	8	.074890			0	0	5	5	.387711
		0	0	2	4	.159481			0	0	5	8	.308995
		0	0	2	5	-.025212			0	0	8	8	-.409187
		0	0	4	4	.000000	7	1	0	0	2	5	-.030638
		0	0	4	5	-.807820			0	0	2	8	-.597385
		0	0	4	8	.325011			0	0	4	4	.000000
		0	0	5	5	.000000			0	0	4	5	.440820
		0	0	5	8	.464461			0	0	4	8	.171302
5	2	0	0	8	8	.000000			0	0	5	5	.000000
		0	0	2	4	-.813249			0	0	5	8	.646936
		0	0	2	5	.281519			0	0	8	8	.000000
		0	0	4	4	.000000	7	2	0	0	2	5	-.222667
		0	0	4	5	.164905			0	0	2	8	.152561
		0	0	4	8	.213366			0	0	4	4	.000000
		0	0	5	5	.000000			0	0	4	5	.488456
		0	0	5	8	.432035			0	0	4	8	.729400
5	3	0	0	8	8	.000000			0	0	5	5	.000000
		0	0	2	4	.053743			0	0	5	8	-.395639
		0	0	2	5	-.807502			0	0	8	8	.000000
		0	0	4	4	.000000	7	3	0	0	2	5	-.895018
		0	0	4	5	.328296			0	0	2	8	.257129
		0	0	4	8	.032408			0	0	4	4	.000000
		0	0	5	5	.000000			0	0	4	5	.102061
		0	0	5	8	.486028			0	0	4	8	.286176
6	1	0	0	8	8	.000000			0	0	5	5	.000000
		0	0	2	4	.177941			0	0	5	8	.201281
		0	0	2	5	.388483			0	0	8	8	.000000
		0	0	2	8	.129671	8	1	0	0	2	8	-.329710
		0	0	4	4	.496940			0	0	4	4	.704658
		0	0	4	5	.505311			0	0	4	5	-.429876
		0	0	4	8	.162114			0	0	4	8	-.338008
		0	0	5	5	.478998			0	0	5	5	-.276692
6	2	0	0	5	8	.190325			0	0	5	8	.102499
		0	0	8	8	-.079821			0	0	8	8	.092959
		0	0	2	4	-.643902	8	2	0	0	2	8	.364862
		0	0	2	5	.205301			0	0	4	4	-.097920
		0	0	2	8	-.394798			0	0	4	5	-.325084
		0	0	4	4	-.023845			0	0	4	8	.070452
		0	0	4	5	.240777			0	0	5	5	-.233187
		0	0	4	8	.371447			0	0	5	8	.604648
6	3	0	0	5	5	-.308618			0	0	8	8	-.571550
		0	0	5	8	.283030	8	3	0	0	2	8	-.492320
		0	0	8	8	-.124538			0	0	4	4	-.350446
		0	0	2	4	-.260378			0	0	4	5	-.323234
		0	0	2	5	-.439995			0	0	4	8	.518318
		0	0	2	8	.099523			0	0	5	5	-.486213
		0	0	4	4	.092042			0	0	5	8	-.156842
		0	0	4	5	.587310			0	0	8	8	.025941
6	4	0	0	4	8	-.517085	8	4	0	0	2	8	-.064029
		0	0	5	5	-.095386			0	0	4	4	-.254343
		0	0	5	8	.081895			0	0	4	5	-.699350
		0	0	8	8	.303508			0	0	4	8	-.160183
		0	0	2	4	-.287551			0	0	5	5	.604819
		0	0	2	5	-.398571			0	0	5	8	-.207970
		0	0	2	8	.425003			0	0	8	8	.086045
		0	0	4	4	.601551	9	1	0	0	2	8	-.278461
0	0	4	5	-.278457			0	0	4	5	-.355696		
0	0	4	8	.346826			0	0	4	8	-.729167		

See page 321 for Explanation of Tables

TABLE II. The Transformation Coefficients $D_{(v) \alpha; J_N J_\mu}^{T_\lambda T_\mu J}$

J	α	T_λ	T_μ	J_λ	J_μ	D	J	α	T_λ	T_μ	J_λ	J_μ	D		
						$v = 8 \quad t = 0$									
9	1	0	0	2	8	-.278461	10	2	0	0	5	5	-.392999		
		0	0	4	5	-.355696			0	0	5	8	-.713033		
		0	0	4	8	-.729167			0	0	8	8	-.124413		
		0	0	5	5	.000000			10	3	0	0	2	8	.743018
		0	0	5	8	-.514058					0	0	4	8	-.045021
9	2	0	0	8	8	.000000	0	0	5	5	.627348				
		0	0	2	8	.233728	0	0	5	8	-.191249				
		0	0	4	5	.783505	11	1	0	0	8	8	.125521		
		0	0	4	8	-.561432			0	0	4	8	.968109		
		0	0	5	5	.000000			0	0	5	8	.250528		
9	3	0	0	5	8	.127619	0	0	8	8	.000000				
		0	0	8	8	.000000	11	2	0	0	4	8	.250528		
		0	0	2	8	-.868070			0	0	5	8	-.968109		
		0	0	4	5	.133576	0	0	8	8	.000000				
		0	0	4	8	-.067372	12	1	0	0	4	8	-.792293		
0	0	5	5	.000000	0	0			5	8	-.607095				
0	0	5	8	.473364	0	0			8	8	.060885				
10	1	0	0	8	8	.000000	12	2	0	0	4	8	.492992		
		0	0	2	8	.276793			0	0	5	8	-.578180		
		0	0	4	8	.035841	13	1	0	0	8	8	.650128		
		0	0	5	5	-.432066			0	0	5	8	-.100000		
		0	0	5	8	.197367			0	0	8	8	.000000		
10	2	0	0	8	8	.834546	14	1	0	0	8	8	1.00000		
		0	0	2	8	.201429	16	1	0	0	8	8	1.00000		
		0	0	4	8	.530174									

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TABLE III. The Primed Reduced Matrix Elements $\langle J'_\lambda T'_\lambda \| \Delta \| J_\lambda T_\lambda \rangle'$

$$\langle a' b' \| \Delta \| a b \rangle' = \langle a b \| \Delta \| a' b' \rangle' = \langle a' b' \| M \| a b \rangle' = \langle a b \| M \| a' b' \rangle'$$

$(J'T')$	(02)
(JT)	
$(\frac{7}{2} \frac{3}{2})$	$-2\sqrt{10}$

$(J'T')$	$(\frac{7}{2} \frac{3}{2})$
(JT)	
(21)	$-2\sqrt{2 \cdot 5}$
(41)	$-2\sqrt{2 \cdot 9}$
(61)	$-2\sqrt{2 \cdot 13}$

$(J'T')$	(21)	(41)	(61)
(JT)			
$(\frac{3}{2} \frac{1}{2})$	$+3\sqrt{\frac{6}{7}}$	$-3\sqrt{\frac{22}{7}}$	0
$(\frac{5}{2} \frac{1}{2})$	$-\sqrt{33}$	$-6\sqrt{\frac{1}{11}}$	$+\sqrt{\frac{15 \cdot 13}{11}}$
$(\frac{9}{2} \frac{1}{2})$	$-\sqrt{\frac{65}{7}}$	$+30\sqrt{\frac{5}{77}}$	$-7\sqrt{\frac{5}{11}}$
$(\frac{11}{2} \frac{1}{2})$	$-\sqrt{30}$	$+3\sqrt{\frac{26}{11}}$	$+4\sqrt{\frac{39}{11}}$
$(\frac{15}{2} \frac{1}{2})$	0	$6\sqrt{\frac{10}{11}}$	$-6\sqrt{\frac{34}{11}}$

$(J'T')$	$(\frac{3}{2} \frac{1}{2})$	$(\frac{5}{2} \frac{1}{2})$	$(\frac{9}{2} \frac{1}{2})$	$(\frac{11}{2} \frac{1}{2})$	$(\frac{15}{2} \frac{1}{2})$
(JT)					
(20)	$-2\sqrt{\frac{22}{7}}$	-1	$-3\sqrt{\frac{15 \cdot 13}{77}}$	$+2\sqrt{\frac{10}{11}}$	0
(40)	$+\sqrt{\frac{78}{35}}$	$+2\sqrt{\frac{39}{5}}$	$+6\sqrt{\frac{3}{91}}$	$+\sqrt{30}$	$-4\sqrt{\frac{6}{13}}$
(50)	$-\sqrt{\frac{66}{5}}$	$+7\sqrt{\frac{1}{5}}$	$+3\sqrt{3}$	$-\sqrt{\frac{130}{7}}$	$-2\sqrt{\frac{34}{7}}$
(80)	0	0	$+4\sqrt{\frac{10 \cdot 17}{11 \cdot 13}}$	$+12\sqrt{\frac{17}{77}}$	$+2\sqrt{\frac{617 \cdot 19}{7 \cdot 13}}$

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TABLE IV. The Reduced Matrix Elements $\langle J'_\mu T'_\mu || [M \times M]^{J_0 T_0} || J_\mu T_\mu \rangle$
 $J'_\mu T'_\mu(\text{text}) \equiv \text{JL TL (table)}; J_\mu T_\mu(\text{text}) \equiv \text{JR TR (table)}$

JL	TL	JR	TR	J0T0	J0T0	JL	TL	JR	TR	J0T0	J0T0	J0T0	J0T0
2	0	2	0	1 0	1.195229	0 1	0.0	3/2	1/2	3/2	1/2	1 0	1.195229
				3 0	4.993502	2 1	0.0					3 0	4.119639
				3 0	-2.725541	2 1	0.0	3/2	1/2	5/2	1/2	1 0	0.000000
				5 0	-2.138090	4 1	0.0					3 0	4.427189
				3 0	4.512609	2 1	0.0					5 0	0.0
				5 0	-3.741657	4 1	0.0	3/2	1/2	9/2	1/2	3 0	5.781745
				7 0	-4.558423	6 1	0.0					5 0	-4.535574
				7 0	-5.147184	6 1	0.0					7 0	0.0
				1 0	0.0	0 1	0.000000	3/2	1/2	11/2	1/2	5 0	-3.741657
				3 0	0.0	2 1	-4.494895					7 0	-4.810702
				5 0	0.0	4 1	-3.129843	3/2	1/2	15/2	1/2	7 0	-6.233550
				3 0	0.0	2 1	-3.129843	3/2	1/2	7/2	3/2	3 0	0.0
				5 0	0.0	4 1	8.886192					5 0	0.0
				7 0	0.0	6 1	5.077905	5/2	1/2	5/2	1/2	1 0	2.236068
				5 0	0.0	4 1	5.077905					3 0	-1.310794
				7 0	0.0	6 1	-3.109569					5 0	-6.657190
				1 0	2.927700	0 1	0.0	5/2	1/2	9/2	1/2	3 0	2.810106
				3 0	-0.414039	2 1	0.0					5 0	5.018497
				5 0	-7.348814	4 1	0.0					7 0	-2.647433
				7 0	4.718840	6 1	0.0	5/2	1/2	11/2	1/2	3 0	-3.485507
				1 0	-0.000000	0 1	0.0					5 0	-5.526794
				3 0	-4.732864	2 1	0.0					7 0	-6.181818
				5 0	3.441824	4 1	0.0	5/2	1/2	15/2	1/2	5 0	6.996503
				7 0	4.920466	6 1	0.0					7 0	3.378252
				5 0	7.120269	4 1	0.0	5/2	1/2	7/2	3/2	3 0	0.0
				7 0	-3.135163	6 1	0.0					5 0	0.0
				3 0	0.0	2 1	-6.308401					7 0	0.0
				5 0	0.0	4 1	-6.180945	9/2	1/2	9/2	1/2	1 0	4.855042
				7 0	0.0	6 1	6.928203					3 0	-4.234118
				1 0	0.0	0 1	-0.000000					5 0	0.512841
				3 0	0.0	2 1	-6.180945					7 0	-7.738292
				5 0	0.0	4 1	3.538812	9/2	1/2	11/2	1/2	1 0	-0.000000
				7 0	0.0	6 1	1.809068					3 0	-6.586989
				3 0	0.0	2 1	6.928203					5 0	4.847319
				5 0	0.0	4 1	1.809068					7 0	-5.271659
				7 0	0.0	6 1	9.629500	9/2	1/2	15/2	1/2	3 0	-5.846087
				1 0	3.964125	0 1	0.0					5 0	-2.771561
				3 0	0.861892	2 1	0.0					7 0	-9.366543
				5 0	5.014265	4 1	0.0	9/2	1/2	7/2	3/2	3 0	0.0
				7 0	-2.607681	6 1	0.0					5 0	0.0
				3 0	5.147184	2 1	0.0					7 0	0.0
				5 0	-4.614835	4 1	0.0	11/2	1/2	11/2	1/2	1 0	6.391959
				7 0	-7.362730	6 1	0.0					3 0	0.303463
				5 0	0.0	4 1	-6.480741					5 0	4.883048
				7 0	0.0	6 1	-5.781745					7 0	7.306739
				3 0	0.0	2 1	6.480741	11/2	1/2	15/2	1/2	3 0	-4.533491
				5 0	0.0	4 1	11.071198					5 0	10.161533
				7 0	0.0	6 1	5.781745					7 0	-7.020087
				5 0	0.0	4 1	-11.071198	11/2	1/2	7/2	3/2	3 0	0.0
				7 0	0.0	6 1	0.000000					5 0	0.0
				1 0	7.634508	0 1	0.0					7 0	0.0
				3 0	-4.096245	2 1	0.0	15/2	1/2	15/2	1/2	1 0	9.856108
				5 0	4.901739	4 1	0.0					3 0	-3.592644
				7 0	-10.949294	6 1	0.0					5 0	6.445613
				1 0	0.0	0 1	-6.969321					7 0	12.643156
				3 0	0.0	2 1	9.408103	15/2	1/2	7/2	3/2	5 0	0.0
				5 0	0.0	4 1	9.075832					7 0	0.0
				3 0	0.0	2 1	-6.969321	7/2	3/2	7/2	3/2	1 0	4.898979
				5 0	0.0	4 1	9.075832					3 0	7.493315
				7 0	0.0	6 1	-16.174155					5 0	9.380832
				1 0	2.070197	0 1	5.477226					7 0	10.954451
				3 0	-3.964125	2 1	5.111013						
				5 0	0.0	4 1	-7.340133						
				3 0	5.855400	2 1	-7.340133						
				5 0	-7.464200	4 1	0.817254						
				7 0	0.0	6 1	-5.954372						
				5 0	8.366600	4 1	-5.954372						
				7 0	-7.745967	6 1	-9.723449						
				3 0	0.0	2 1	7.071068						
				1 0	5.070926	0 1	7.348469						
				3 0	-6.193457	2 1	0.817254						
				5 0	2.735054	4 1	7.785972						
				7 0	-6.037076	6 1	-12.438277						
				3 0	7.948179	2 1	-5.954372						
				5 0	4.369114	4 1	-12.438277						
				7 0	-12.318058	6 1	6.620779						
				5 0	0.0	4 1	9.486833						
				1 0	8.831761	0 1	8.831761						
				3 0	1.734435	2 1	-9.723449						
				5 0	-9.945305	4 1	6.620779						
				7 0	-8.948891	6 1	16.661928						
				1 0	0.0	0 1	11.401754						
				1 0	0.0	0 1	5.477226						

See page 321 for Explanation of Tables

TABLE V. The Reduced Matrix Element Sums

$$\sum_{J''_μ T''_μ} \frac{\langle J''_μ T''_μ || [M \times M]^{J_o T_o} || J_μ T_μ \rangle^2}{(2J_μ + 1)(2T_μ + 1)}$$

J	T	J _o	T _o	Σ	J _o	T _o	Σ
0	2	0	1	6			
		2	1	10			
		4	1	18			-
		6	1	26			
2	1	0	1	2	1	0	2/7
		2	1	38/3	3	0	10/3
		4	1	12	5	0	176/21
		6	1	52/3	7	0	4
4	1	0	1	2	1	0	20/21
		2	1	20/3	3	0	166/33
		4	1	18	5	0	64/21
		6	1	52/3	7	0	230/33
6	1	0	1	2	1	0	2
		2	1	20/3	3	0	56/33
		4	1	12	5	0	188/39
		6	1	70/3	7	0	1070/143
2	0	0	1	--	1	0	2/7
		2	1	6	3	0	116/11
		4	1	252/11	5	0	26/7
		6	1	78/11	7	0	104/11
4	0	0	1	--	1	0	20/21
		2	1	14	3	0	10/3
		4	1	6	5	0	3674/273
		6	1	16	7	0	244/39
5	0	0	1	--	1	0	10/7
		2	1	48/7	3	0	70/11
		4	1	1152/77	5	0	46/7
		6	1	156/11	7	0	106/11
8	0	0	1	--	1	0	24/7
		2	1	20/7	3	0	28/11
		4	1	774/77	5	0	514/91
		6	1	254/11	7	0	1770/143
7/2	3/2	0	1	15/4	1	0	3/4
		2	1	35/4	3	0	7/4
		4	1	63/4	5	0	11/4
		6	1	91/4	7	0	15/4
3/2	1/2	0	1	3/4	1	0	5/28
		2	1	213/28	3	0	35/4
		4	1	585/28	5	0	121/28
		6	1	39/4	7	0	31/4
5/2	1/2	0	1	3/4	1	0	5/12
		2	1	59/4	3	0	455/132
		4	1	345/44	5	0	149/12
		6	1	689/44	7	0	623/132
9/2	1/2	0	1	3/4	1	0	33/28
		2	1	157/28	3	0	301/44
		4	1	5679/308	5	0	1405/364
		6	1	625/44	7	0	5217/572
11/2	1/2	0	1	3/4	1	0	143/84
		2	1	35/4	3	0	419/132
		4	1	453/44	5	0	683/84
		6	1	845/44	7	0	1055/132
15/2	1/2	0	1	3/4	1	0	85/28
		2	1	15/4	3	0	93/44
		4	1	477/44	5	0	1821/364
		6	1	1041/44	7	0	6205/572

See page 321 for Explanation of Tables