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**ADVANCED
OPTICAL
MATERIALS**

Supporting Information

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**Processing-Dependent Microstructure of AgCl–CsAgCl₂
Eutectic Photonic Crystals**

*Jaewon Choi, Ashish A. Kulkarni, Erik Hanson, Daniel
Bacon-Brown, Katsuyo Thornton, and Paul V. Braun**

Supporting Information

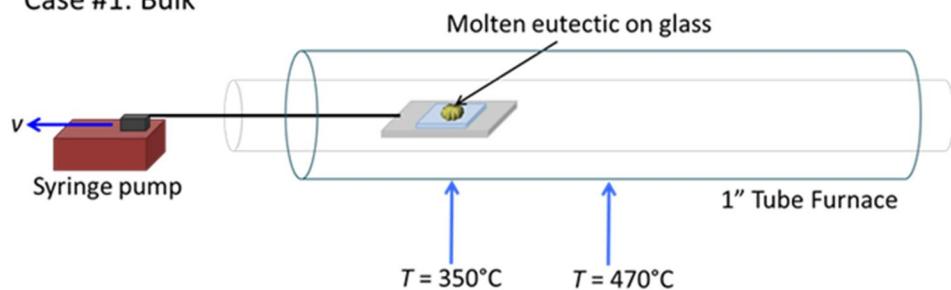
Processing-Dependent Microstructure of AgCl-CsAgCl₂ Eutectic Photonic Crystals

Jaewon Choi[#], Ashish A. Kulkarni[#], Erik Hanson, Daniel Bacon-Brown, Katsuyo Thornton and Paul V.

Braun*

[#] contributed equally to this work

(a) Case #1: Bulk



(b) Case #2: Eutectic-infilled capillary

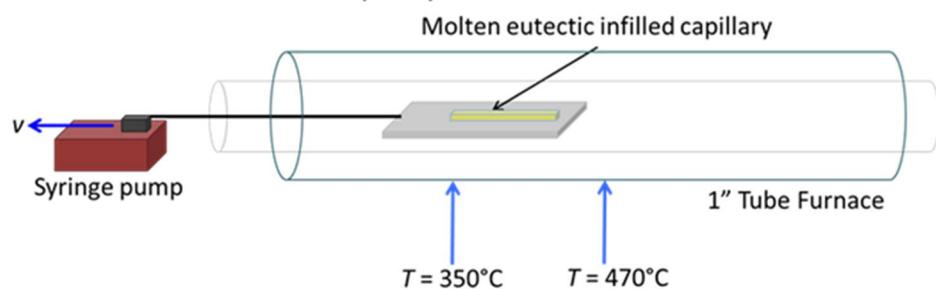


Figure S1: Schematic of the experimental setup for directional solidification of (a) bulk and (b) capillary samples. See the Experimental Section for details.

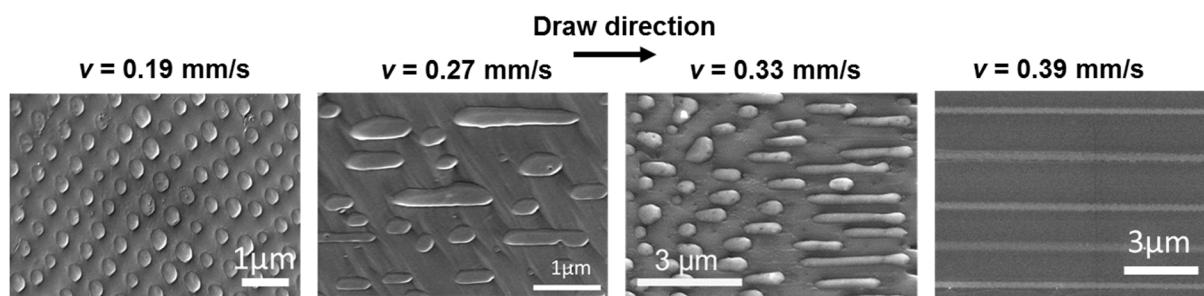


Figure S2: Plan view SEM images of bulk samples directionally solidified at different draw rates. Arrow indicates the draw direction.

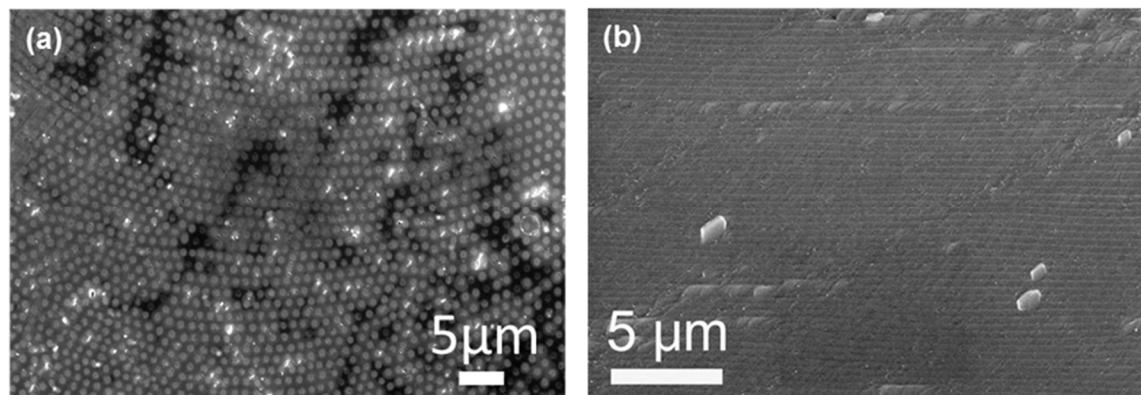


Figure S3: Low magnification plan view SEM images of bulk samples showing the (a) rod and (b) lamellar structure of the eutectic.

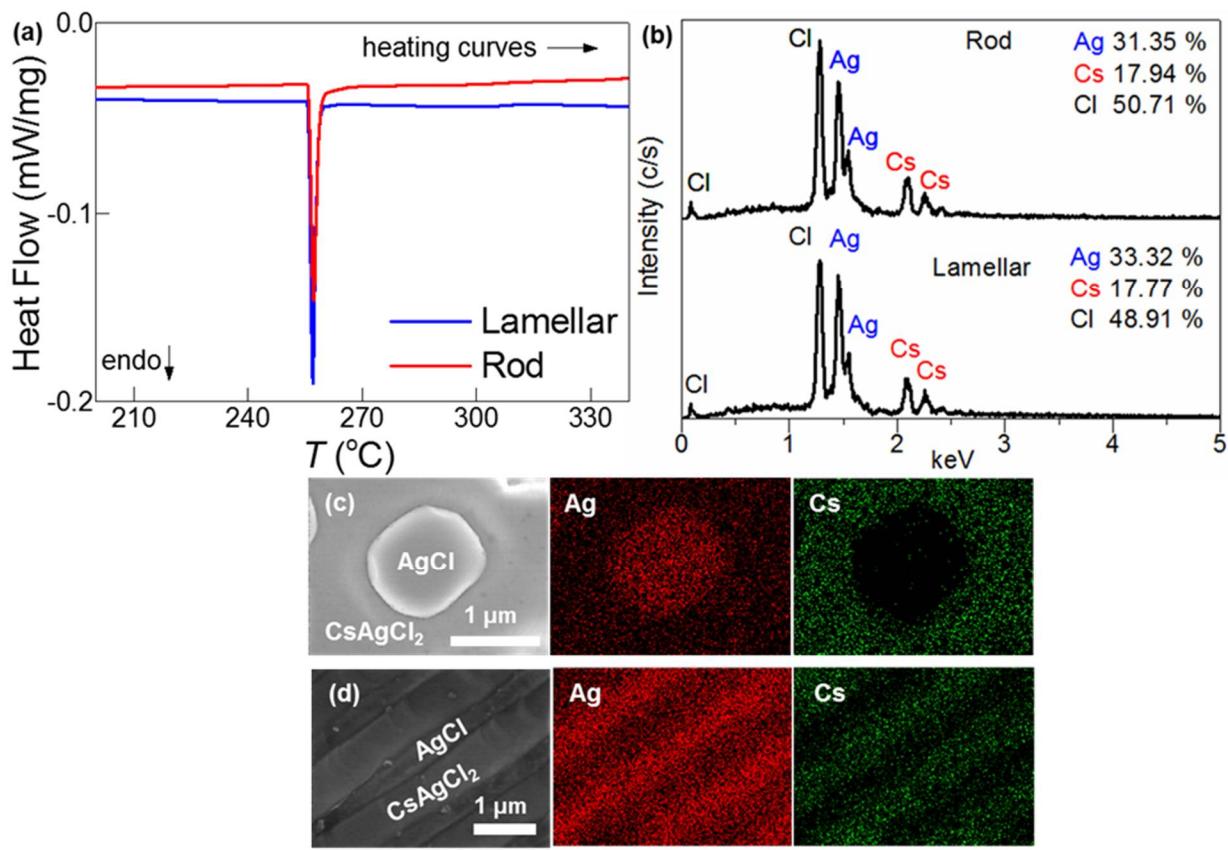


Figure S4: (a) Heat flow curves (taken with DSC) for samples with lamellar and rod structures, depicting the same melting points of 258 °C. (b) EDS analysis showing the at.% Ag, Cs and Cl as expected for the AgCl-CsAgCl₂ eutectic (Cs:Ag:Cl=1:2:3). Elemental mapping of Ag and Cs in the (c) rod and (d) lamellar microstructures of the eutectic.

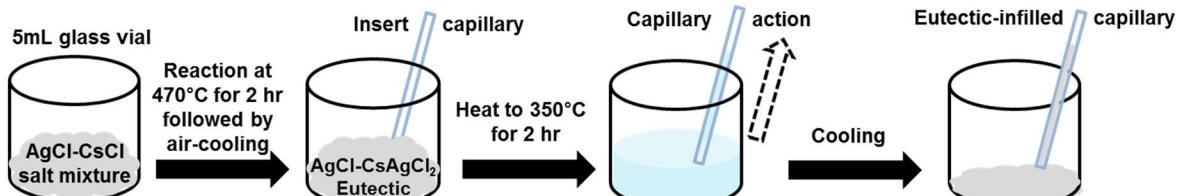


Figure S5: Schematic of the fabrication of a eutectic-infilled capillary.

Table S1: Parameters used in the phase field modeling, where $\alpha = \text{CsAgCl}_2$ and $\beta = \text{AgCl}$ phase.

Parameter	Symbol	Units	Value	Reference
Eutectic Temperature	T_E	K	531	(i)
Eutectic Composition	C_E	mol %	72	(i)
α Phase Composition at T_E	C_α	mol %	50	(i)
β Phase Composition at T_E	C_β	mol %	100	(i)
β Volume Fraction	V_f	%	36	Calculated from (i)
α Liquidus Slope (at T_E)	m_α	K/mol%	-3.33	Calculated from (i)
β Liquidus Slope (at T_E)	m_β	K/mol%	14.25	Calculated from (i)
α Partition Coefficient (at T_E)	k_α	-	0.694	Calculated from (i)
β Partition Coefficient (at T_E)	k_β	-	1.389	Calculated from (i)
α -Liquid Surface Tension (at T_E)	$\sigma_{\alpha L}$	mJ/m ²	135	Assumed $\sigma_{\alpha L} = \sigma_{\alpha\beta}$
β -Liquid Surface Tension (at T_E)	$\sigma_{\beta L}$	mJ/m ²	135	Assumed $\sigma_{\beta L} = \sigma_{\alpha\beta}$
α - β Surface Tension (at T_E)	$\sigma_{\alpha\beta}$	mJ/m ²	135	Extrapolated from (ii)
Eutectic Latent Heat of Fusion	L_E	J/kg	4.69×10^4	Experiment (DSC)
α Latent Heat of Fusion	L_α	J/m ³	3.43×10^8	Experiment (DSC)
β Latent Heat of Fusion	L_β	J/m ³	5.13×10^8	(iii)
Diffusion Coefficient (at T_E)	D	m ² /s	2.53×10^{-10}	(iv)
α Contact Angle	θ_α	°	30	(v)
β Contact Angle	θ_β	°	30	(v)

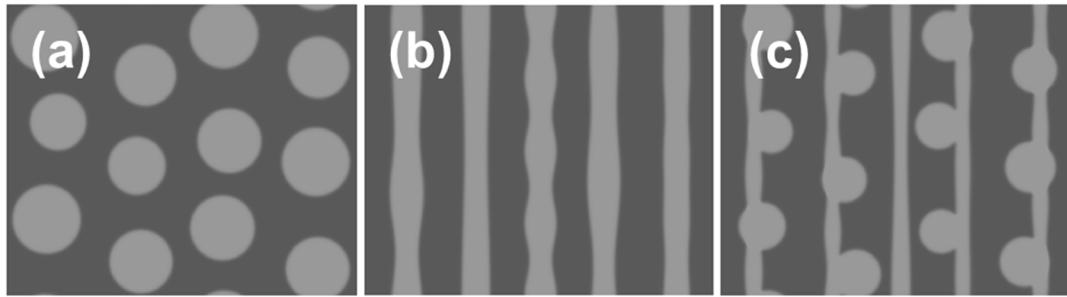


Figure S6: Cross-sections in the y - z plane (perpendicular to the solidification direction) of the initial conditions (i.e. solid seed) for the eutectic structure as assumed during the phase-field simulations. Light gray and dark gray represent AgCl and CsAgCl₂, respectively. (a) Rod initial condition. (b) Lamellar initial condition. (c) Mixed rod and lamellar initial condition.

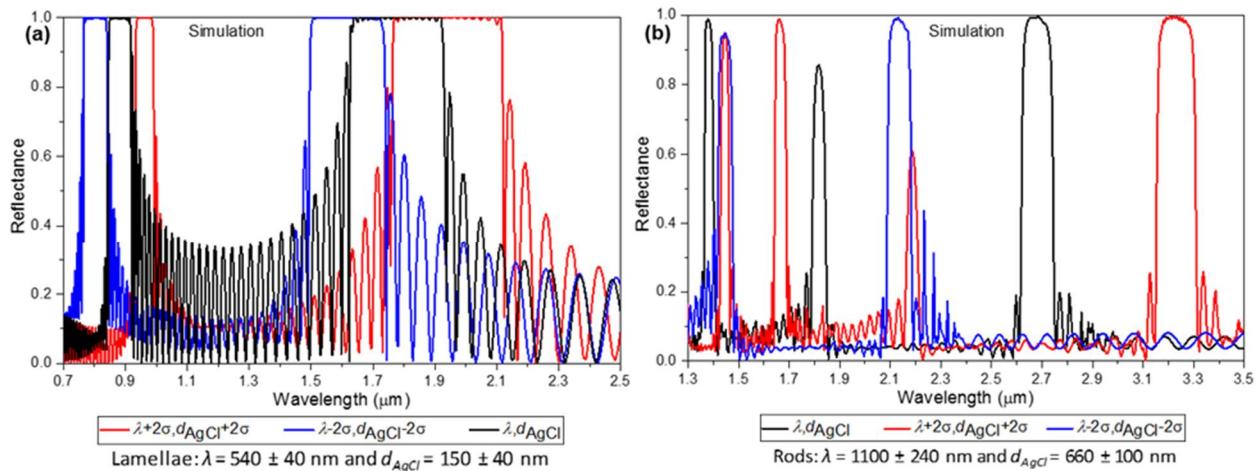


Figure S7: FDTD simulations showing the range of reflectance peaks for the experimentally observed size distribution in (a) lamellae and (b) rods.

References

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