Copyright WILEY-VCH Verlag GmbH & Co. KGaA, 69469 Weinheim, Germany, 2019.

# **ADVANCED MATERIALS**

## Supporting Information

for Adv. Mater., DOI: 10.1002/adma.201903480

Are Cu<sub>2</sub>Te-Based Compounds Excellent Thermoelectric Materials?

Kunpeng Zhao, Ke Liu, Zhongmou Yue, Yancheng Wang, Qingfeng Song, Jian Li, Mengjia Guan, Qing Xu, Pengfei Qiu,\* Hong Zhu, Lidong Chen,\* and Xun Shi\* Copyright WILEY-VCH Verlag GmbH & Co. KGaA, 69469 Weinheim, Germany, 2019.

## **Supporting Information**

#### Are Cu<sub>2</sub>Te-based Compounds Excellent Thermoelectric Materials

Kunpeng Zhao<sup>1</sup>, Ke Liu<sup>2</sup>, Zhongmou Yue<sup>3,4</sup>, Yancheng Wang<sup>3,4</sup>, Qingfeng Song<sup>3,4</sup>, Jian Li<sup>3,4</sup>, Mengjia Guan<sup>3,4</sup>, Qing Xu<sup>3,4</sup>, Pengfei Qiu<sup>3\*</sup>, Hong Zhu<sup>2</sup>, Lidong Chen<sup>3,4\*</sup>, and Xun Shi<sup>1,3,4\*</sup>

1 State Key Laboratory of Metal Matrix Composites, School of Materials Science and Engineering, Shanghai Jiao Tong University, Shanghai 200240, China.

2 University of Michigan-Shanghai Jiao Tong University Joint Institute, Shanghai Jiao Tong University, Shanghai 200240, China

3 State Key Laboratory of High Performance Ceramics and Superfine Microstructure, Shanghai Institute of Ceramics, Chinese Academy of Sciences, Shanghai 200050, China.

4 Center of Materials Science and Optoelectronics Engineering, University of Chinese Academy of Sciences, Beijing 100049, China.

\* Corresponding authors. E-mail: qiupf@mail.sic.ac.cn, cld@mail.sic.ac.cn and xshi@sjtu.edu.cn



Figure S1. Powder X-ray diffraction pattern of Cu<sub>2</sub>Te at room temperature

## WILEY-VCH



**Figure S2.** (a) Backscattered electron microscopy (BSE) image and (b, c, d) corresponding elemental energy-dispersive X-ray spectroscopy (EDS) mapping for  $Cu_2Te+35\%Ag_2Te$  at room temperature. (e, f) Quantitative EDS results for the areas denoted in figure (a). The solubility of Ag in  $Cu_2Te$  is quite low at room temperature, which is in accordance with previous reports. Besides the cationic elements, it is very surprising that the anion element Te is also not homogenously distributed. The concentration of Te in CuAgTe phases is obviously higher than that in  $Cu_2Te$  phases. The quantitatively EDS analysis reveals that  $Cu_2Te$  phases are Cu deficient while CuAgTe phases are Te deficient, which implies that  $Cu_2Te$  is p-type conduction while CuAgTe is n-type conduction.

## WILEY-VCH



**Figure S3**. Crystal structures of  $Cu_2Te$  and CuAgTe used for defect formation energy calculations. In the CuAgTe crystal structure, both Cu and Ag atoms occupy half of 8c sites. This model is on behalf of the case where Cu and Ag have uniform distributions.



**Figure S4**. Vacancy formation energies as a function of the reciprocal of supercell size based on defect calculations for  $1 \times 1 \times 1$ ,  $2 \times 2 \times 2$  and  $3 \times 3 \times 3$  supercells. *L* is the side length of the supercells. For charged defect, the electron potential is set to the valence band maximum. The electrostatic potential of defected system is aligned to that of bulk.



**Figure S5.** Lattice thermal conductivity  $\kappa_L$  as a function of Ag<sub>2</sub>Te content at 900 K. The purple dashed line represents the minimum lattice thermal conductivity ( $\kappa_{min}$ ) estimated by the Cahill's model.<sup>[1]</sup> The minimum lattice thermal conductivity  $\kappa_{min}$  for a normal solid can be expressed as

$$\kappa_{min} = \left(\frac{\pi}{6}\right)^{1/3} k_B n^{2/3} \sum_i v_i \left(\frac{T}{\Theta_i}\right)^2 \int_0^{\Theta_i/T} \frac{x^3 e^x}{(e^x - 1)^2} dx$$
(S1),

where  $v_i$  is the speed of sound,  $\Theta_i (= v_i (\hbar/k_B)(6\pi^2 n)^{1/3})$  is the cutoff frequency, and *n* is the number density of atoms. This model assumes that a material has a completely disordered structure with three phonon modes (one longitudinal and two transverse) taken into account. The calculated  $\kappa_{min}$  values for Cu<sub>2</sub>Te + x% Ag<sub>2</sub>Te (x = 0, 15, 35, 40, 50, and 55) are around 0.4 W m<sup>-1</sup> K<sup>-1</sup>.



**Figure S6.** Repeatability test on the electrical transport properties for  $Cu_2Te + 50\%$  Ag<sub>2</sub>Te. The measurements were repeated six cycles at different cycling temperatures.



**Figure S7**. Temperature dependent heat capacity at constant pressure  $(C_p)$  for Cu<sub>2</sub>Te + 55% Ag<sub>2</sub>Te sample. The dashed line represents the theoretical heat capacity at constant volume  $(C_v)$  derived from Dulong-Petit law. The  $C_p$  is significantly changed during phase transitions.<sup>[2, 3]</sup> But the measured  $C_p$  values at high temperature are very close to the value estimated by the Dulong-Petit law.



**Figure S8**. (a) Special Quasirandom Structure (SQS) of CuAgTe generated by "mcsqs" code of the Alloy Theoretic Automated Toolkit (ATAT). (b) Comparison of the defect formation energy for uniform distribution (Fig. S3b) and quasirandom distribution (Fig. S8a) of Cu and Ag in CuAgTe.

#### **Single Parabolic Band Model**

Based on the Fermi statistics, the Seebeck coefficient S can be expressed as

$$S = \frac{k_B}{e} \left[ \frac{(2+\lambda)F_{\lambda+1}(\eta)}{(1+\lambda)F_{\lambda}(\eta)} - \eta \right]$$
, (S2)

where  $k_B$  is the Boltzmann constant, *e* is the electron charge,  $\lambda$  is the scattering factor (0 for acoustic phonon scattering), and  $\eta (=E_F/k_BT)$  is the reduced Fermi energy. The Fermi integrals

#### WILEY-VCH

are given by  $F_m(\eta) = \int_0^\infty \frac{x^m dx}{1 + \exp(x - \eta)}$ , where *x* is the reduced carrier energy. The Hall carrier concentration *p* can also be expressed as a function of Fermi integrals

$$p = 4\pi \left(\frac{2m^* k_B T}{h^2}\right)^{3/2} \frac{F_{1/2}(\eta)}{r_H} , (S3)$$
$$r_H = \frac{3}{4} \frac{F_{1/2}(\eta) F_{-1/2}(\eta)}{F_0^2(\eta)} , (S4)$$

where  $m^*$  is the electronic effective mass, *h* is the Planck constant and  $r_H$  is the Hall factor. The Hall mobility  $\mu$  for acoustic phonon scattering in the non-degenerate limit can be expressed as

$$\mu = \frac{1}{2} \frac{F_{-1/2}(\eta)}{F_0(\eta)} \cdot \mu_0$$
 (S5)

where  $\mu_0$  represents the drift mobility. Thus the electrical conductivity  $\sigma$  can be obtained by

$$\sigma = pe\mu = \frac{16\sqrt{2}\pi ek_B^{3/2}T^{3/2}F_0(\eta)}{3h^3} \ \mu_0 m^{*3/2} \qquad . (S6)$$

Through Equation S2 and Equation S6, we can calculate the *S*- $\sigma$  (Seebeck coefficient *vs* electrical conductivity) relation if  $\mu_0 m^{*3/2}$  (also called weighted mobility) is given.

#### References

[1] D. Cahill, S. Watson, R. Pohl, *Phys. Rev. B* **1992**, *46*, 6131.

[2] M. T. Agne, P. W. Voorhees, G. J. Snyder, *Adv. Mater.* **2019**, 1902980.

[3] H. Chen, Z. Yue, D. Ren, H. Zeng, T. Wei, K. Zhao, R. Yang, P. Qiu, L. Chen, X. Shi, *Adv. Mater.* 2018, *31*, 1806518.