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MEMO TO: File
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 SUBJECT: Surface field on a constant impedance half plane

To assist in understanding the behavior of impedance and resistive sheets, it is of interest to examine the field on the surface of a half plane of constant surface impedance when illuminated by a plane wave. Since an impedance sheet is equivalent to a resistive one only for edge-on incidence, we restrict our attention to this case.

For a half plane of constant surface impedance η illuminated by an E-polarised plane wave, the exact solution has been obtained by Senior (1952). For edge-on incidence ($\alpha = \pi$)

$$E_z = E_z^i - \frac{1}{2\pi i} \int_{C'} \frac{K_+(k)}{(\cos \beta - 1) K_-(k \cos \beta)} e^{ik\rho \cos(\beta - \theta)} d\beta$$

and when the observation point is on the upper surface ($\theta = 0$) of the sheet and at large distances from the edge, the integral can be evaluated by steepest descents to give (see eqs. 38 and 40 of Senior, 1952 with $\alpha = \pi$):

$$E_z \sim \frac{e^{ikx + i\pi/4}}{\sqrt{2\pi kx}} \lim_{\theta \rightarrow 0} \left\{ \frac{1}{\cos \theta - 1} \left(\frac{K_+(k)}{K_-(k \cos \theta)} - 2 \sin \frac{\theta}{2} \right) \right\} .$$

The limit can be found using l'Hôpital's rule and is 2η , but a somewhat simpler approach which avoids the limiting operation is to consider the total

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current*

$$I_2(x) = H_x(x, +0) - H_x(x, -0).$$

From Senior (1952, eq. 25, with $\alpha = \pi$),

$$I_2(x) = -\frac{iY_0}{\pi} \int_{C'} \frac{K_+(k)}{K_-(k \cos \beta)} \cos \frac{\beta}{2} e^{ikx \cos \beta} d\beta$$

$$\underset{kx \gg 1}{\sim} -iY_0 \sqrt{\frac{2}{\pi kx}} e^{ikx - i\pi/4} \lim_{\beta \rightarrow 0} \left\{ \frac{K_+(k)}{K_-(k \cos \beta)} \cot \frac{\beta}{2} \right\}.$$

But

$$\frac{1}{K_-(k \cos \beta)} = \frac{\sin \beta}{1 + \eta \sin \beta} \cdot \frac{1}{K_+(k \cos \beta)}$$

so that

$$\frac{K_+(k)}{K_-(k \cos \beta)} \cos \frac{\beta}{2} \xrightarrow{\beta \rightarrow 0} 2,$$

giving

$$I_2(x) \sim -2Y_0 \sqrt{\frac{2}{\pi kx}} e^{ikx + i\pi/4}.$$

Hence, from symmetry,

$$H_x(x, \pm 0) \sim \mp Y_0 \frac{2}{\pi kx} e^{ikx + i\pi/4}$$

which is precisely the same result as for a perfectly conducting half plane,

but since

$$E_z(x, \pm 0) = \mp \eta Z_0 H_x(x, \pm 0)$$

on the upper and lower surfaces respectively, we have

$$E_z(x, \pm 0) \sim \eta \frac{2}{\pi kx} e^{ikx + i\pi/4}.$$

* Note that $I_2(x)$ is the negative of the total current $J(x)$ used in the electrically resistive sheet program.

This is valid for $kx \gg 1$, but we can also determine the behavior for $kx \ll 1$ from the properties of the Fourier transform $\bar{I}_2(\xi)$ of $I_2(x)$ for large $|\xi|$. Since

$$\bar{I}_2(\xi) = iY_0 \sqrt{\frac{2}{\pi}} \frac{K_+(k)}{(\xi - k) K_-(\xi)}$$

and $K_-(\xi) = O(\text{const.})$ for large ξ , $\eta \neq 0$, it follows that

$$\bar{I}_2(\xi) = O(|\xi|^{-1})$$

and hence

$$I_2(x) = O(\text{const.}), \quad kx \ll 1.$$

It is somewhat difficult to determine the constant value of $I_2(0)$. Nevertheless from an examination of the 'split' functions, it appears that

$$\frac{K_+(k)}{K_+(\xi)} \rightarrow 1$$

as $|\xi| \rightarrow \infty$, and if this is true

$$\begin{aligned} \bar{I}_2(\xi) &= iY_0 \sqrt{\frac{2}{\pi}} \frac{1}{\xi - k} \frac{\sqrt{k^2 - \xi^2}}{k + \eta \sqrt{k^2 - \xi^2}} \frac{K_+(k)}{K_+(\xi)} \\ &\sim \frac{iY_0}{\eta \xi} \sqrt{\frac{2}{\pi}} \quad \text{as } |\xi| \rightarrow \infty, \end{aligned}$$

implying

$$I_2(0) = -2 \frac{Y_0}{\eta}.$$

Hence, from symmetry,

$$H_x(0, \pm 0) = \mp \frac{Y_0}{\eta}$$

and

$$E_z(0, \pm 0) = 1.$$

This is in excellent agreement with computed data for electrically resistive sheets with a parabolic variation of resistance. For $R_{\max} = 4$ (at the front), it is found that $J(0) = 0.240e^{i9.9^\circ}$ for sheets of length l , $0.7 \leq l/\lambda \leq 1.5$, and since $E_z = RJ$, it follows that

$$E_z(0, \pm 0) = 0.960e^{i9.9^\circ}.$$

The 4 percent difference in amplitude is no more than expected due to the variable resistivity, and though there is no obvious explanation for the non-zero phase, we note that it is equivalent to a displacement of the 'effective' end of the sheet by $\frac{\lambda}{36}$.

Reference

Senior, T. B. A. (1952) "Diffraction by a semi infinite metallic sheet", Proc. Roy. Soc. (London) 213A, 436-458.