

SCATTERING BY RESISTIVE STRIPS AND PLATES

by

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## CHAPTER I. INTRODUCTION

This is the final report of the work carried out for the Northrop Corporation under purchase order 36-4385 during the period ending 31 May 1985. The purpose of the study was to examine the effect of non-zero resistivity on the backscattering cross sections of strips and plates with particular reference to angles of incidence which are close to grazing.

In the case of a strip with the incident electric vector parallel to the surface attention is confined to edge-on incidence, and the analysis is presented in Chapter II. The backscattering cross section is determined for a variety of uniform and quadratically-tapered resistivities, and one of the significant conclusions is that tapering is not always better. When the incident magnetic vector is parallel to the surface, the scattering for edge-on incidence is zero regardless of the resistivity, and the incidence which is most important is that corresponding to the traveling wave lobe. The nature of this lobe is examined in Chapter III, and it is shown that even a small resistivity is sufficient to eliminate the traveling wave as such. Unfortunately, this merely bares a far side lobe of the specular flash.

A strip is the two-dimensional analogue of a finite plate and in spite of the useful information that can be derived from a study of the simpler two-dimensional structure, there are many circumstances under which the model is irrelevant to the realistic problems of a finite plate. Substantial effort has been devoted to the development

of an efficient and effective code to compute the scattering from a finite resistive plate of arbitrary shape and resistivity. The work that has been accomplished is described in Chapter IV, and though there is still much to be done, the program in its present form does compute the current induced in the plate. The development of the program was carried out by Mr. J. W. Burns and Professor D. A. Ksienski (a present and former student, respectively, of the author), and it is a pleasure to acknowledge their assistance.

## CHAPTER II. E POLARIZATION

One of the more difficult problems in cross section reduction is to reduce the scattering from the edge of an electrically thin structure such as an aircraft wing or tail fin. This is particularly true at angles close to grazing incidence with the electric vector parallel to the surface, and the significant scattering that can occur in this case is dominated by the edges. We shall consider here the problem of a resistive strip or ribbon illuminated by an E-polarized plane wave at edge-on incidence ( $\phi_0 = \pi$ ) and examine the magnitude of the backscattered field compared with that of the corresponding perfectly conducting strip.

### 2.1 Uniform Resistivity

For a uniform resistive strip with resistivity  $R$  ohms per square the backscattered far field amplitude  $P(\pi, \pi)$  can be expressed as a sum of front and rear edge contributions as (Senior, 1979a):

$$P(\pi, \pi) = p^f + p^r \quad . \quad (2.1)$$

In terms of  $P$  the backscattering cross section per unit length is

$$\sigma = \frac{2\lambda}{\pi} |P(\pi, \pi)|^2 \quad . \quad (2.2)$$

If the strip width  $w$  is more than about  $\lambda/2$  where  $\lambda = 2\pi/k$  is the wavelength, the front edge return  $p^f$  is identical to that for a half plane of the same resistivity and

$$p^f = -\frac{i\eta}{16} \{ZJ(0,\eta)\}^2 = -\frac{i}{4} \{K(0,\eta)\}^2 \quad (2.3)$$

where  $\eta = 2R/Z$ ,  $J(x,\eta)$  is the current on a resistive half plane at a distance  $x$  from the edge for the same incident plane wave, and  $K(0,\eta)$  is a "split" function which appears in the Wiener-Hopf solution for a half plane.  $Z$  is the intrinsic impedance of free space and a time variation  $e^{-i\omega t}$  has been assumed.

$K(0,\eta)$  is real for real  $\eta$  and its values have been tabulated (Senior, 1979a). For complex  $\eta$

$$K(0,\eta) \cong \begin{cases} 2^{1/2} \exp \{-\eta/\pi [1 - \ln(\eta/2)]\} & |\eta| \ll 1 \\ \eta^{-1/2} \exp \{-1/(\pi\eta)\} & |\eta| \gg 1 \end{cases} \quad (2.4)$$

and  $K(0,\eta)$  can also be expressed in terms of the function  $\psi_\pi(z)$  introduced by Maliuzhinets (1958) as

$$K(0,\eta) = \frac{4\sqrt{\eta}}{(\sqrt{\eta} + \sqrt{1+\eta})^2} \left\{ \frac{\psi_\pi(\chi)}{\psi_\pi(\pi/2)} \right\}^4 \quad (2.5)$$

where  $\cos \chi = 1/\eta$ . In a recent article (Volakis and Senior, 1985), two simple expressions for  $\psi_\pi(z)$  are derived which, when used in conjunction with known identities, approximate the function to a high degree of accuracy throughout the entire complex  $z$  plane.

For the rear edge scattering and with the same restriction on  $w$ ,

$$p^r = i\gamma \{ZJ(w,\eta)\}^2 \quad (2.6)$$

where (Senior, 1979b)

$$\gamma = \{4K(0,\eta)\}^{-2}, \quad (2.7)$$

so that

$$p^r = \frac{1}{4\eta} \left\{ \frac{ZJ(w,\eta)}{ZJ(0,\eta)} \right\}^2. \quad (2.8)$$

The above formulas are valid for complex  $\eta$  as well as real, and a procedure for computing the exact analytical expression for  $J(x,\eta)$  is described in Senior (1981). In the special case of perfect conductivity,

$$ZJ(x,0) = 2 \sqrt{\frac{2}{\pi kx}} e^{i(kx+\pi/4)}. \quad (2.9)$$

If  $\eta$  is real and non-zero,  $J(x,\eta)$  is asymptotic to  $J(x,0)$  as  $kx \rightarrow \infty$ , but if  $\eta \gg 1$ ,  $kx$  has to be very large indeed before (2.9) constitutes a good approximation to  $J(x,\eta)$ . The current on a resistive half plane never exceeds its value at the corresponding point of a perfectly conducting half plane, and since its magnitude is a monotonically decreasing function of  $x$  and  $\eta$ , it follows from (2.8) that

$$|p^r| \leq \frac{1}{4\eta} \quad (2.10)$$

for all  $w$  and  $\eta$ .

For a perfectly conducting strip the front and rear edge contributions have particularly simple expressions. Since  $K(0,0) = \sqrt{2}$ , Eq. (2.3) gives

$$p^f = -\frac{i}{2} , \quad (2.11)$$

and from (2.6), (2.7) and (2.9),

$$p^r = -\frac{e^{2ikw}}{4\pi kw} . \quad (2.12)$$

This is the smallest rear edge contribution that can be achieved with any uniform resistive strip whose width  $w$  is such that  $kw > \eta$ , and the behavior of  $|p^r|$  as a function of  $\eta$  is illustrated in Fig. 2.1.

To make the edge-on backscattering cross section of a strip as small as possible over a wide band of frequencies, it is necessary to minimize the front and rear edge contributions individually. The smallest value of  $|p^f|$  is achieved by choosing  $\eta$  as large as possible, and if, for example,  $\eta = 4$ , the resulting front edge contribution is almost 20 dB below that for a perfectly conducting strip. For the rear edge the preceding results suggest that the minimum return is obtained with a perfectly conducting strip. This is certainly true for all except the very narrowest strips, and Fig. 2.2 shows  $|p^r|$  as a function of  $w/\lambda$  for five different values of (real)  $\eta$ . Having  $\eta \neq 0$  inevitably increases  $|p^r|$  and though, for fixed  $w/\lambda$ , the return ultimately decreases as  $\eta$  increases, it remains above that for  $\eta = 0$  for all reasonable values of  $kw$  and  $\eta$ . The obvious solution is to taper the resistivity from a maximum at the front to zero at the rear, and provided this is done smoothly, it is natural to expect a rear edge contribution comparable to that for a perfectly conducting strip with no new source of scattering created.

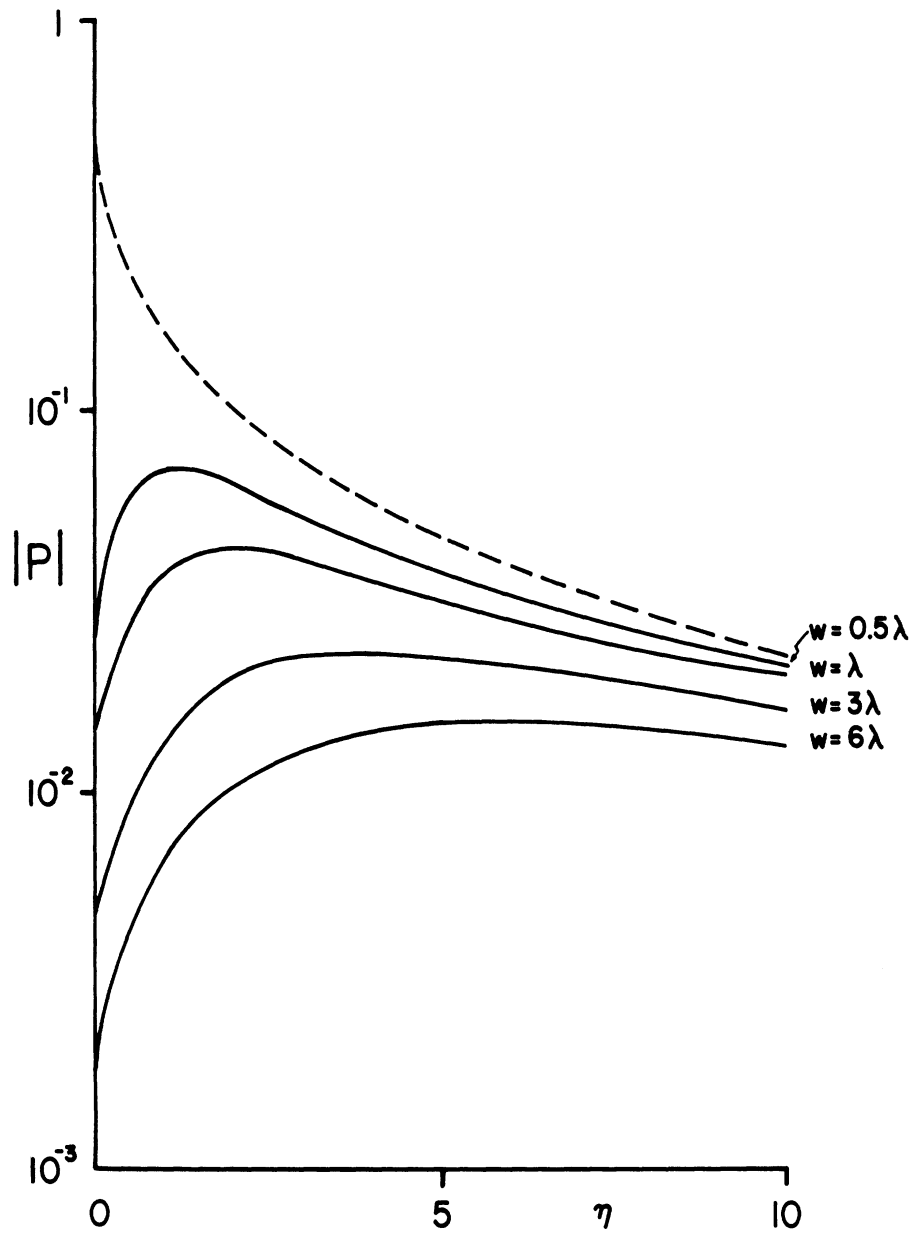


Fig. 2.1: The magnitudes of the front (---) and rear (—) edge contribution of uniform resistive strips as functions of  $\eta$ . (This is an expanded version of Fig. 2 of Senior and Liepa, 1984.)



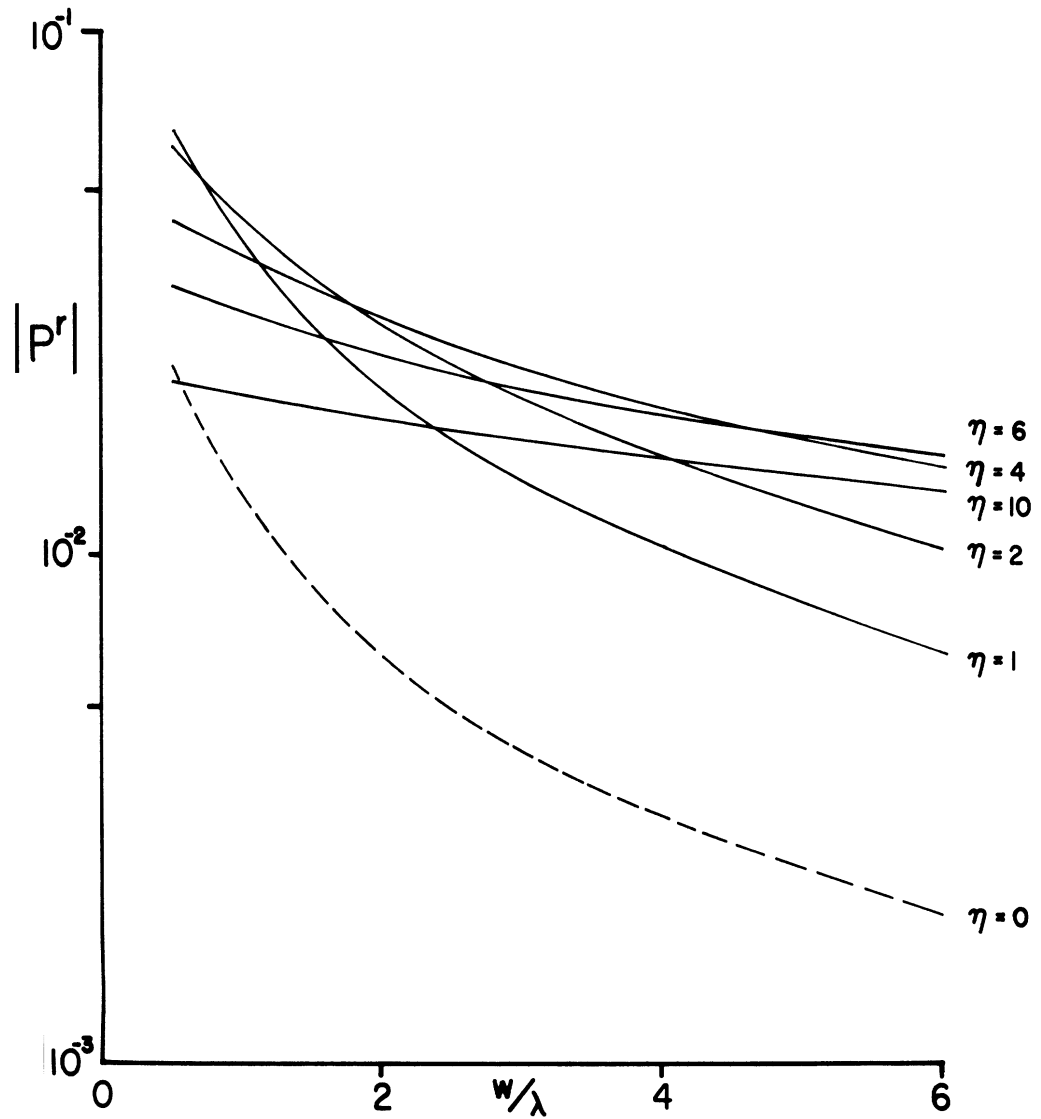


Fig. 2.2: The magnitudes of the rear edge contribution (—) for five uniform resistive strips, compared with the contribution for perfectly conducting strips (---) computed using (2.12).

## 2.2 Quadratically-Tapered Resistivity

Based on prior experience with resistive tapers, attention was confined to the quadratic form

$$R(x) = \frac{\eta}{2} Z \left(1 - \frac{x}{w}\right)^2 \quad (2.13)$$

where  $x$  is measured from the front edge. Thus,  $\eta$  specifies the largest value of the resistivity, occurring at the front of the strip.

Using program REST-E which solves the integral equation for an E-polarized plane wave incident on a resistive strip, the total induced current and the backscattered far field were computed as a function of  $w/\lambda$  for a sequence of real  $\eta$ . From the computed data for  $P(\pi, \pi)$ , the real and imaginary parts of  $P^f$  and  $P^r$  were extracted (Ksienski, 1985a), and the resulting values of  $P^f$  were almost identical to those for the front edge contribution of a uniform resistive strip having the same  $\eta$ . The magnitudes of the rear edge contributions are plotted in Fig. 2.3, and we observe that they exceed the contribution for a perfectly conducting strip but show a similar dependence on  $w/\lambda$ . An empirical expression for  $P^r$  is

$$p^r = - \frac{e^{2ikw}}{4\pi kw} \left\{ 1 + \frac{5.8\eta}{(kw)^{2/3}} \right\}, \quad (2.14)$$

and since the first term in parentheses in the rear edge contribution for a perfectly conducting strip, the second term is the additive effect of the resistive taper.

Under all circumstances, however, the rear edge return exceeds that for perfect conductivity, and for a narrow strip may even exceed

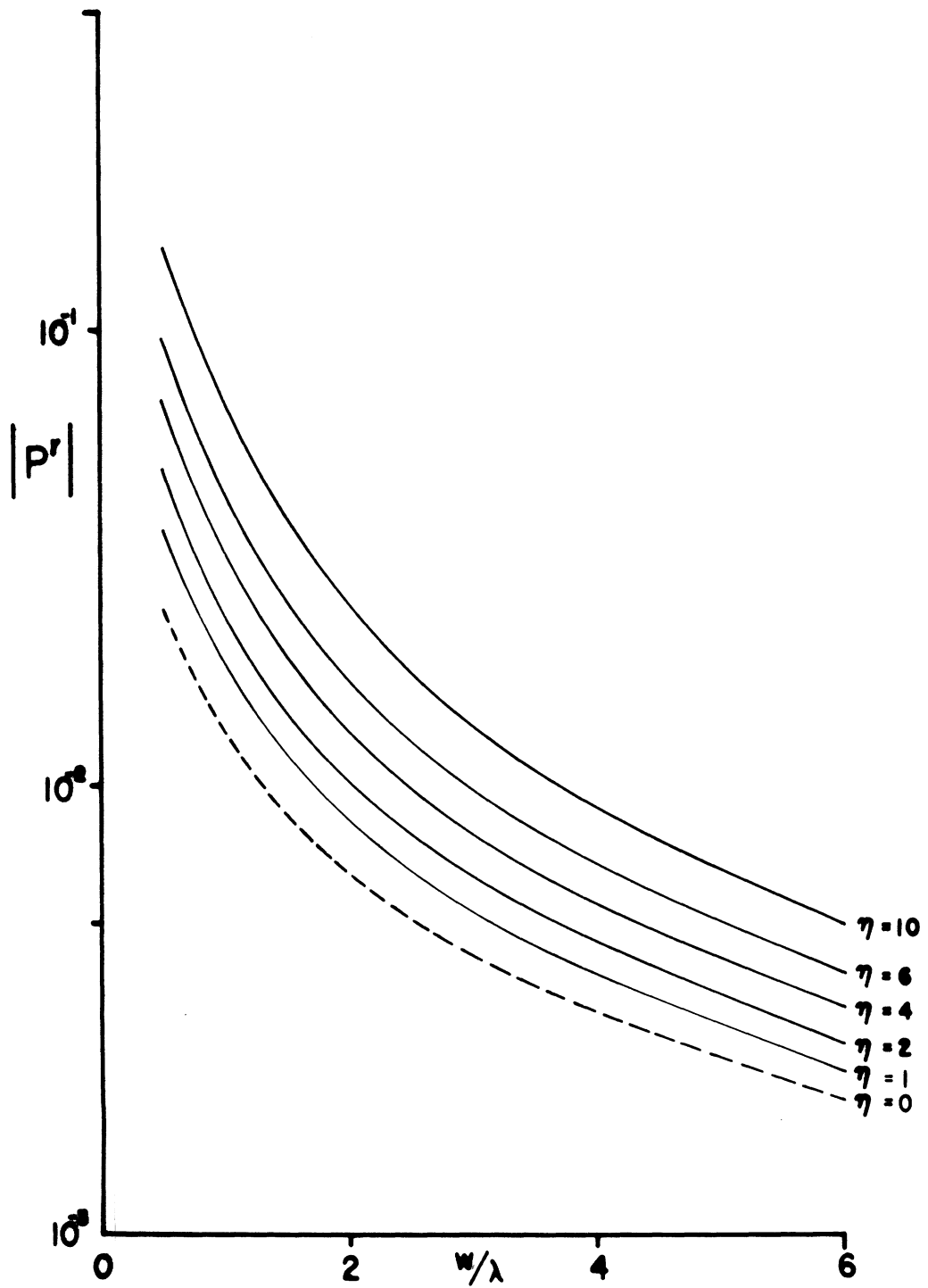


Fig. 2.3: The magnitudes of the rear edge contribution for tapered strips with five different values of  $\eta$  compared with the contribution (---) for perfectly conducting strips.

the return for the corresponding uniform resistive strip. Comparison of Figs. 2.1 and 2.3 shows that if  $\eta = 10$  the tapering is only effective if  $w > 2.4 \lambda$ , and the analogous conditions for  $\eta = 6$  and  $\eta = 4$  are  $w > 1.4 \lambda$  and  $w > 0.9 \lambda$  respectively. Thus, as the strip width and/or frequency is reduced, we ultimately reach a point at which tapering becomes counter productive.

Equations (2.14) and (2.3) are sufficient to provide the edge-on backscattered field of a resistive strip with a quadratic taper, and confirm that at high frequencies for which  $w \gg \lambda$  the most effective way to reduce the scattering is to increase the resistivity at the front edge to as large a value as possible and to taper the resistivity smoothly to zero at the rear. Although we have considered only the particular taper (2.13), it seems probable that the results for other smooth monotonic tapers will be similar.

## CHAPTER III: H POLARIZATION

Traveling waves are a major contributor to the backscattering cross section of a long thin body when the magnetic vector is perpendicular to the plane of incidence, and our work with H-polarization was concerned with studying the effect of traveling waves on the backscattering cross section of a strip or ribbon.

### 3.1 Traveling Wave Considerations\*

Traveling waves are one of the most important contributors to the scattering from long slender bodies, and in the case of structures such as the fuselage of an aircraft it is possible to produce a reasonably complete description of the backscattering by taking into account the traveling waves and, where appropriate, the specular contributions and the side lobes thereof. When the incident magnetic vector is perpendicular to the plane formed by the direction of incidence and the axis of the body, the fan-shaped pattern characteristic of a traveling wave is a key feature of the overall scattering pattern, and the first lobe is often the major contributor to the scattering at angles close to end-on incidence.

The scattering pattern of a thin plate or strips also displays a similar lobe structure at angles close to edge-on incidence when the magnetic vector is parallel to the surface, and it is customary to

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\* A shortened version of this section has been published by Senior and Yang (1984).

attribute at least the first lobe to a traveling wave. In effect, we are thinking of each narrow slice of the plate as a filament or wire supporting a traveling wave and the angle at which the lobe appears is consistent with this argument. Mathematically, however, there is no justification for this reasoning, and it is therefore of interest to compare the high frequency expressions for the backscattered fields of wires and strips.

For a wire of length  $\ell$  viewed at an angle  $\theta$  to end-on, an approximate form of the expression obtained by Peters (1958) for the backscattering cross section attributable to traveling waves is

$$\sigma = \frac{\lambda^2}{\pi} |S|^2$$

where

$$|S| = \frac{\Gamma}{C} \left\{ \frac{k\ell}{2} \sin \theta \operatorname{sinc} \left[ \frac{k\ell}{2} (1 - \cos \theta) \right] \right\}^2. \quad (3.1)$$

$$\operatorname{sinc} X = \frac{\sin X}{X},$$

and  $\Gamma$  is the effective voltage reflection coefficient for the traveling wave. In deriving (3.1) we have assumed that the phase velocity is that of light and that  $k\ell \gg 1$ , implying

$$C = \ln(2k\ell) - (1 - \gamma)$$

where  $\gamma = 0.5772\dots$  is Euler's constant.

The angles  $\theta = \theta_n$ ,  $n = 1, 2, 3, \dots$ , at which the maxima of the traveling wave lobes occur are given by the solutions of the transcendental equation

$$\tan \phi_n = (1 + \cos \theta_n) \phi_n \quad (3.2)$$

with

$$\phi_n = \frac{k\ell}{2} (1 - \cos \theta_n) .$$

For large  $\ell/\lambda$

$$\theta_1 \cong 49.4 \sqrt{\frac{\lambda}{\ell}} \quad (\text{degrees}) , \quad (3.3)$$

$$\theta_2 \cong 98.1 \sqrt{\frac{\lambda}{\ell}} \quad (\text{degrees}) , \quad (3.4)$$

and comparison with numerical solutions of (3.2) shows that  $\theta_1$  is accurate to within one percent for  $\ell/\lambda \geq 1.8$  and  $\theta_2$  is accurate to three percent for  $\ell/\lambda \geq 3.6$ . The results are also in good agreement with measured data. Chang and Liepa (1967) measured the backscattering patterns of a series of 81 wires having lengths varying from 0.3 to  $5.42 \lambda$  and radius  $6.27 \times 10^{-3} \lambda$ , and the values of  $\theta_1$  and  $\theta_2$  obtained from these patterns are shown in Fig. 3.1, along with the curves corresponding to (3.3) and (3.4). We have also used the measured amplitude of the first lobe to determine the effective reflection coefficient  $\Gamma$  in (3.1). The amplitudes oscillate in a quite regular manner with a maximum to minimum ratio of about 6 dB and maxima occurring at  $\ell/\lambda = 0.4 + 0.5n$ ,  $n = 0, 1, 2, \dots$  (approx.). It is clear that this is attributable to a resonance behavior of the wire, a feature which is not reproduced by (3.1), but if we incorporate this into the effective reflection coefficient, the resulting values of  $\Gamma$  appropriate to the

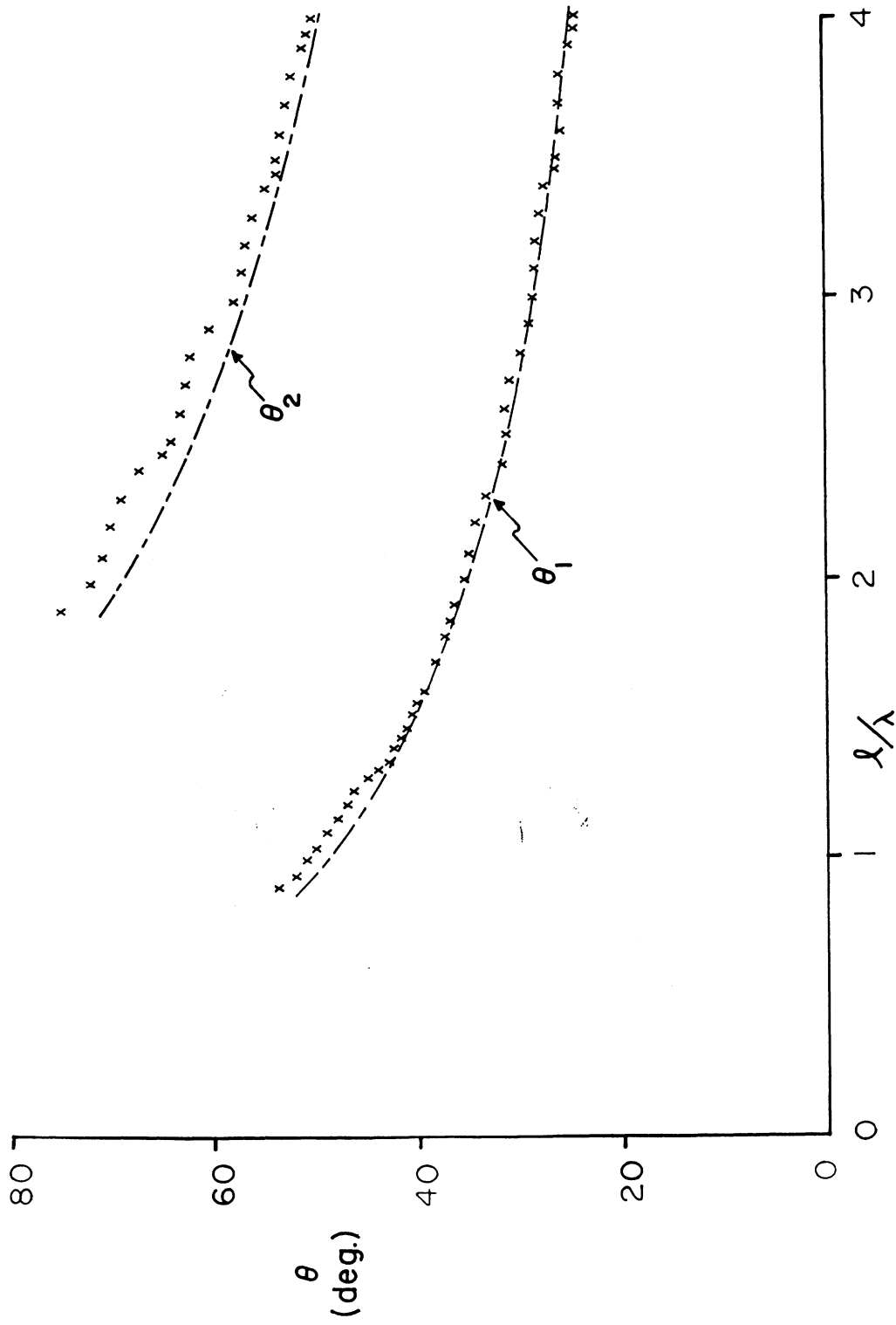


Fig. 3.1: Measured angles (xxx) of the first and second traveling wave lobes for a thin wire. The theoretical curves were computed using (3.3) and (3.4).



first lobe are shown in Fig. 3.2. The average is about 0.65 and varies little with  $\ell/\lambda$ , and this is consistent with the value generally assumed (Ruck et al., 1970) for a pointed body.

We now consider an infinitesimally thin, perfectly conducting strip of width  $w$  occupying the region  $0 \leq x \leq w$ ,  $-\infty < \tau < \infty$  of the plane  $y = 0$  of a Cartesian coordinate system  $x, y, z$  and illuminated by a plane wave having

$$\vec{H}^i = \hat{z} e^{-ik(x \cos \phi_0 + y \sin \phi_0)} .$$

At large distances the scattered magnetic field can be written as

$$\vec{H}^s = \hat{z} \sqrt{\frac{2}{\pi k \rho}} e^{i(i\rho - \pi/4)} P(\phi, \phi_0)$$

where  $\rho, \phi$  are cylindrical polar coordinates with  $x = \rho \cos \phi$ ,  $y = \rho \sin \phi$ . In terms of  $P$  the scattering cross section per unit length in the  $z$  direction is

$$\sigma = \frac{2\lambda}{\pi} |P(\phi, \phi_0)|^2$$

and in the particular case of backscattering,  $\phi_0 = \phi$ .

For  $kw \gg 1$  a uniform second order GTD expression for the backscattered far field amplitude is (Senior, 1979b)

$$P(\phi, \phi) = -\frac{i}{4} \frac{1 + \cos \phi}{\cos \phi} \left\{ 1 - \frac{2}{\sqrt{\pi}} e^{-i\pi/4} \cos \frac{\phi}{2} F \left( \sqrt{2kw} \sin \frac{\phi}{2} \right) \right\}^2$$

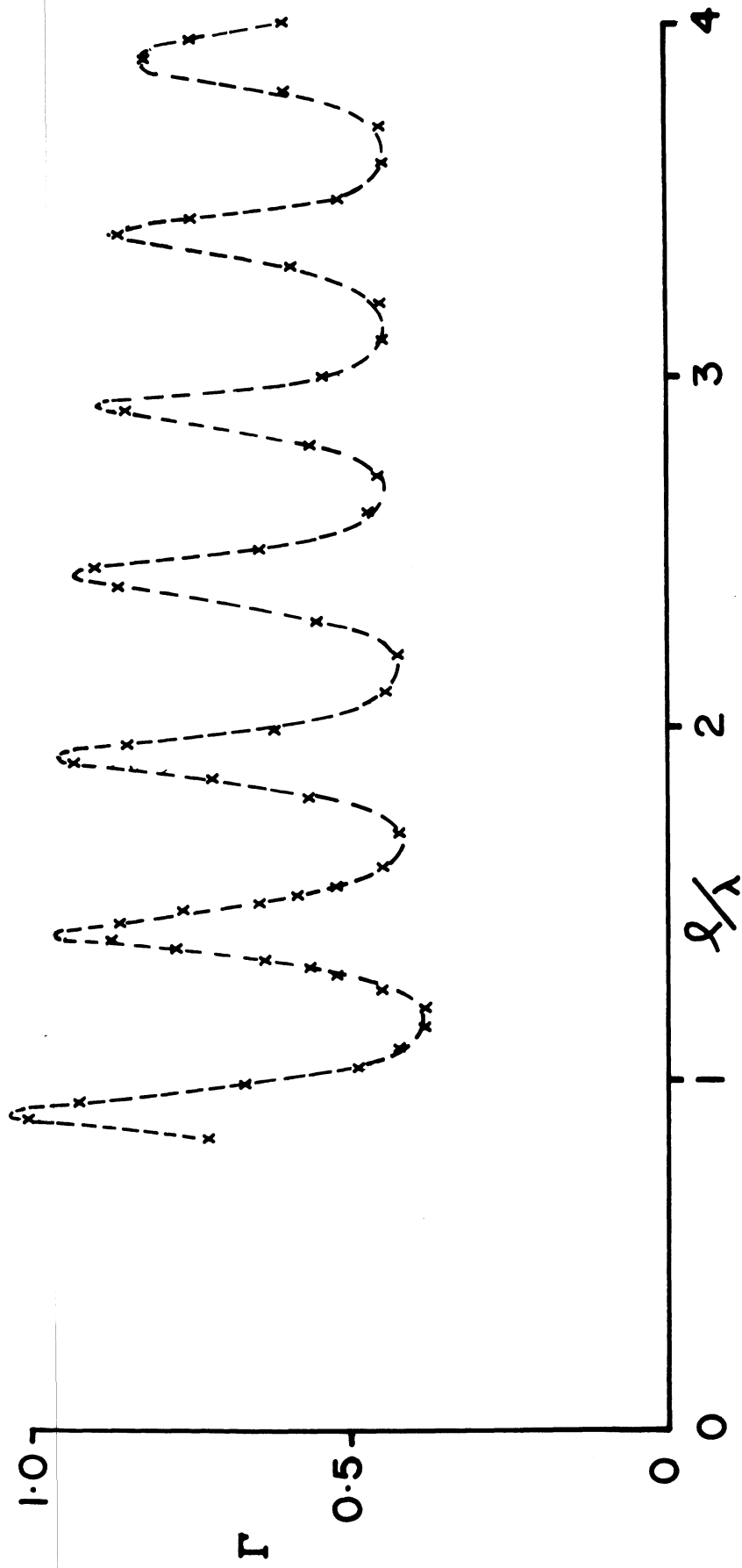


Fig. 3.2: Effective reflection coefficient  $\Gamma$  deduced from the thin wire data. The dashed curve is only to guide the eye.

$$\frac{i}{4} \frac{1 - \cos \phi}{\cos \phi} e^{-2ikw \cos \phi} \left\{ 1 - \frac{2}{\sqrt{\pi}} e^{-i\pi/4} \sin \frac{\phi}{2} F \left( \sqrt{2kw} \cos \frac{\phi}{2} \right) \right\}^2 \quad (3.5)$$

$$+ O([kw]^{-1}) \quad ,$$

valid for  $0 \leq \phi \leq \pi$ .  $F(\tau)$  is the Fresnel integral

$$F(\tau) = \int_{\tau}^{\infty} e^{iu^2} du \quad ,$$

and (3.5) is identical to the result obtained by asymptotic expansion of the expression obtained by Khaskind and Vainshteyn (1964). A simple program to compute  $P(\phi, \phi_0)$  has been developed for use on an IBM PC computer. It is designated P-RIB-H and is described in Appendix A.

When  $\phi = 0$  or  $\pi$ ,  $|P| = 0$  as expected, and the backscattering pattern of a strip is illustrated by the plot of  $|P|$  versus  $\phi$  for  $w/\lambda = 4$  in Fig. 3.3. Since the pattern is symmetrical about the broadside aspect, it is sufficient to consider only  $0 \leq \phi \leq \pi/2$ . The lobe centered on  $\phi = 24$  degrees is the one usually attributed to a traveling wave, and the locations of this and the adjacent peaks are shown in Fig. 3.4. From the variation as a function of  $w/\lambda$  it is evident that all peaks other than the first are most logically associated with the side lobes of the specular return. The first peak is primarily determined by the first term in (3.5), and its magnitude is

$$\frac{1}{4} \left( \frac{2kw - u}{kw - u} \right) \left| 1 - \left( 1 - \frac{u}{2kw} \right)^{1/2} \left\{ 1 - C(u) - S(u) + i[C(u) - S(u)] \right\} \right|^2$$

where

$$u = kw(1 - \cos \phi)$$

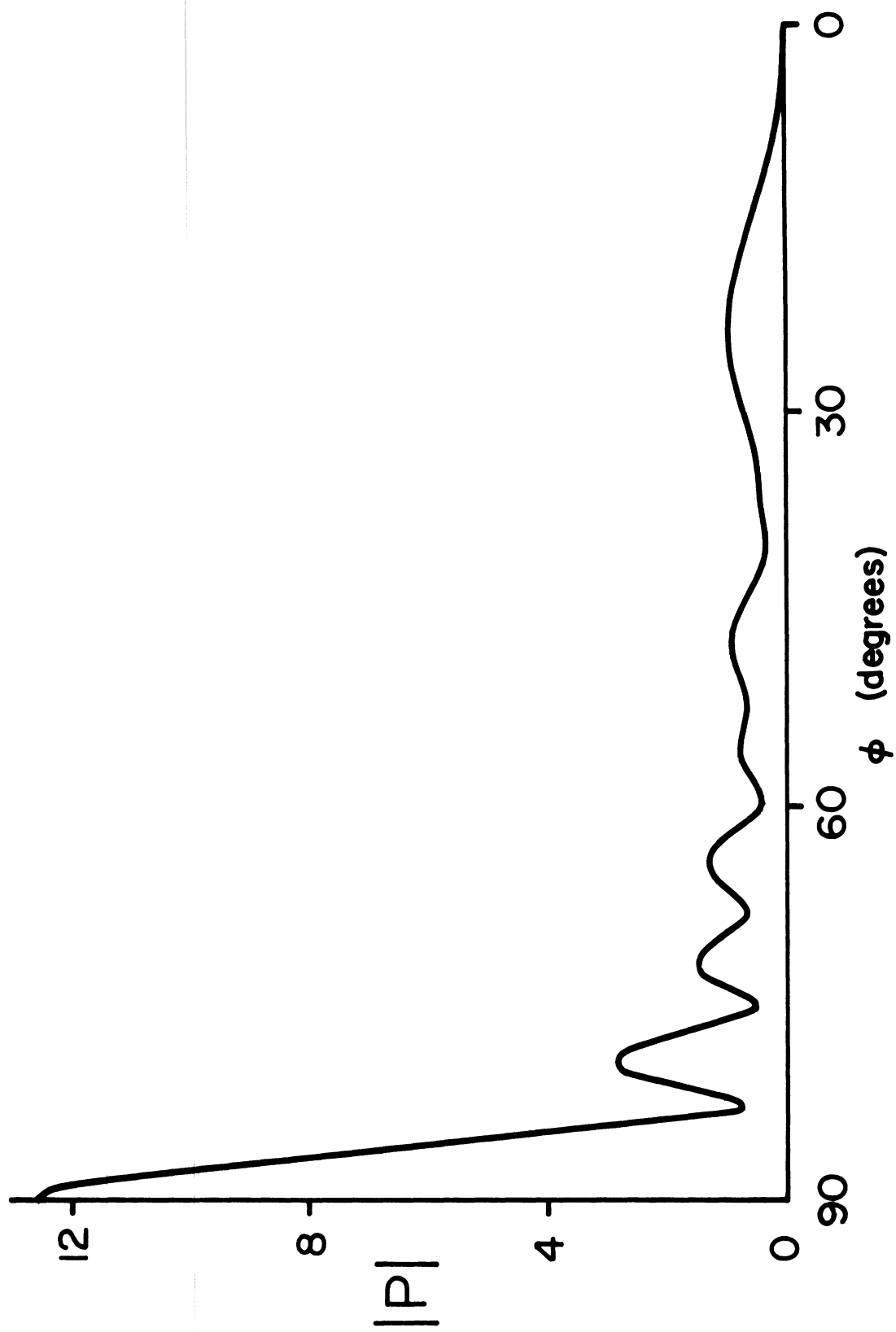


Fig. 3.3: Backscattering pattern of a strip of width  $w = 4\lambda$  computed using (3.5).

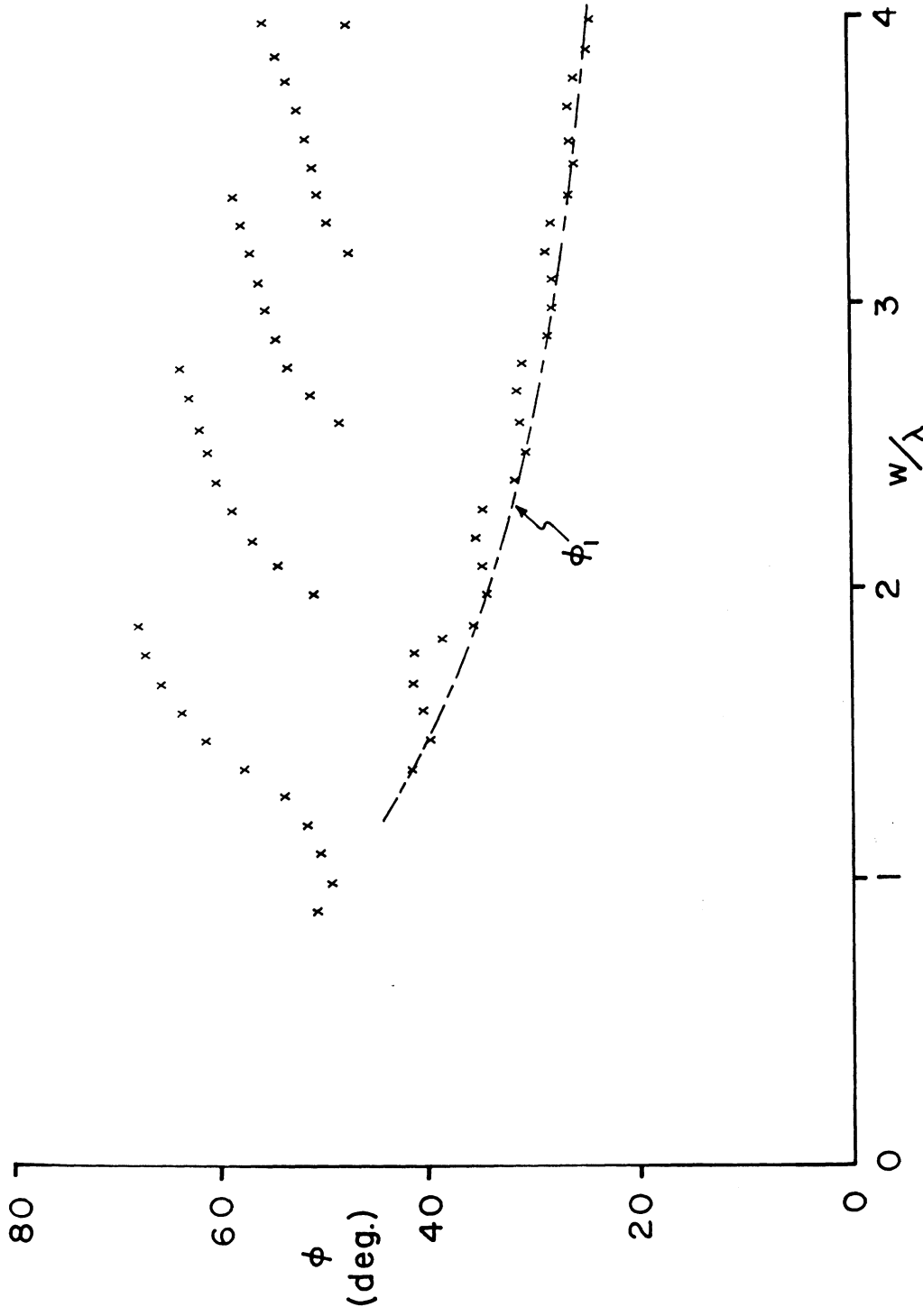


Fig. 3.4: Angles at which the maxima in the pattern occur. The theoretical curve was computed using (3.6).

and  $C(u)$  and  $S(u)$  are the real integrals defined and tabulated in Abramowitz and Stegun (1964). For  $kw \gg 1$  the magnitude is approximately  $\{C(u)\}^2 + \{S(u)\}^2$ , and its maximum is 0.901 occurring at  $u = u_1 = 2.29$ . The resulting value of  $\phi$  is

$$\phi_1 = 48.9 \sqrt{\frac{\lambda}{w}} \quad (\text{degrees}) \quad , \quad (3.6)$$

and the corresponding curve is included in Fig. 3.4. To the next order in  $1/(kw)$  the peak value is

$$\{C(u_1)\}^2 + \{S(u_1)\}^2 + \frac{u_1}{4kw} \{C(u_1) + S(u_1)\} = 0.901 \left(1 + 0.136 \frac{\lambda}{w}\right) \quad , \quad (3.7)$$

and this is plotted in Fig. 3.5 along with the peak values obtained from computations of  $|P|$ . The oscillations are attributable to the effect of the second term in (3.5) which was neglected in our analysis, and (3.7) is an excellent approximation to the mean.

In spite of the different mathematical formulas which describe the effects of traveling waves on wires and strips, the close agreement between the angles  $\theta_1$  and  $\phi_1$  at which the first (dominant) lobe occurs is remarkable. For all practical purposes, it is sufficient to use (3.3) to locate the lobe, thereby lending support to the idea of treating a planar structure as an assemblage of elementary wires, and to using the term "traveling wave" in the case of a strip.

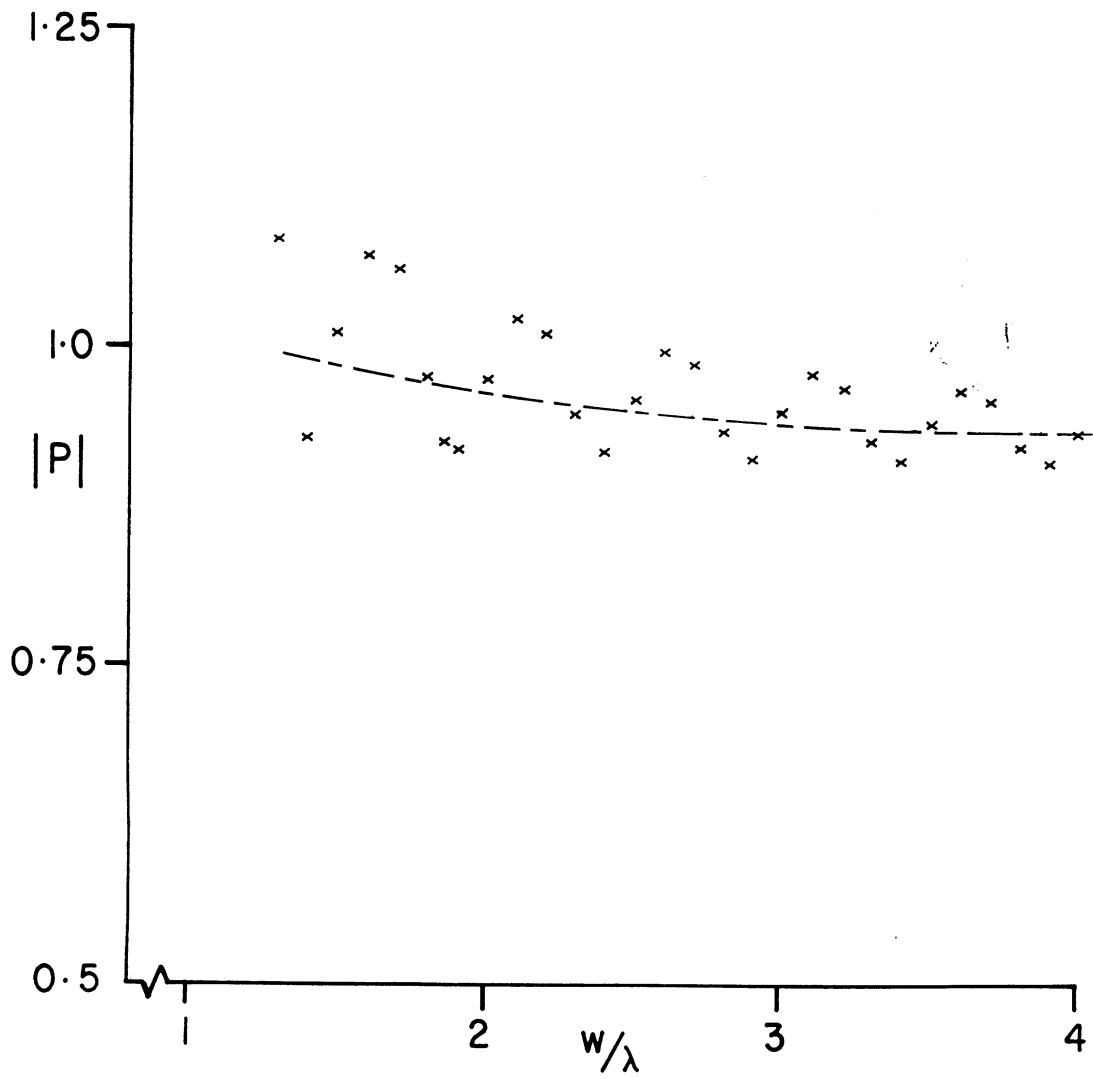


Fig. 3.5: Peak values (xxx) of the traveling wave lobe for a strip compared with the value (—) given by (3.7).

## 2.2 Effect of Non-Zero Resistivity

As we have seen, a traveling wave is a significant contributor to the backscattering cross section of a perfectly conducting strip at angles close to edge-on. It may be necessary to reduce the magnitude of the resulting peak, and the prevailing wisdom is that a relatively small amount of loss is adequate for this purpose. To determine the reduction as a function of the resistivity, we have used program REST-H or its specialized version STRIP-H (see Memorandum 2500-394-M) to compute the backscattered fields of uniform resistive strips of width  $w = 1.0(0.1)4.0 \lambda$  and have examined the magnitudes and locations of the peaks in the backscattered patterns.

For perfectly conducting strips the angle  $\phi$  (measured in degrees from edge-on) at which the maxima are found to occur are shown in Fig. 3.6(a), and the results are almost identical to those obtained using the second order GTD expression (3.5) for the field. We observe that there are two distinct types of maxima; the ones associated with the main lobe of a traveling wave whose location is given approximately by the formula (3.6), and those which are more logically attributable to the side lobes of the specular flash. The latter correspond to the maxima of the pattern factor  $(\sin X)/X$  with  $X = kw \cos \phi$ , and are given by

$$\phi = \arccos \left\{ (2n + 1) \frac{\lambda}{4w} \right\} \quad (3.8)$$

with  $n = 1, 2, 3, \dots$ . As seen from Fig. 3.6(a), they lie on a sequence of trajectories which are distinct from the oscillatory curve describing the traveling wave peak. For large  $w/\lambda$  the traveling wave dominates the far side lobes, which then show up only as an oscillation in the



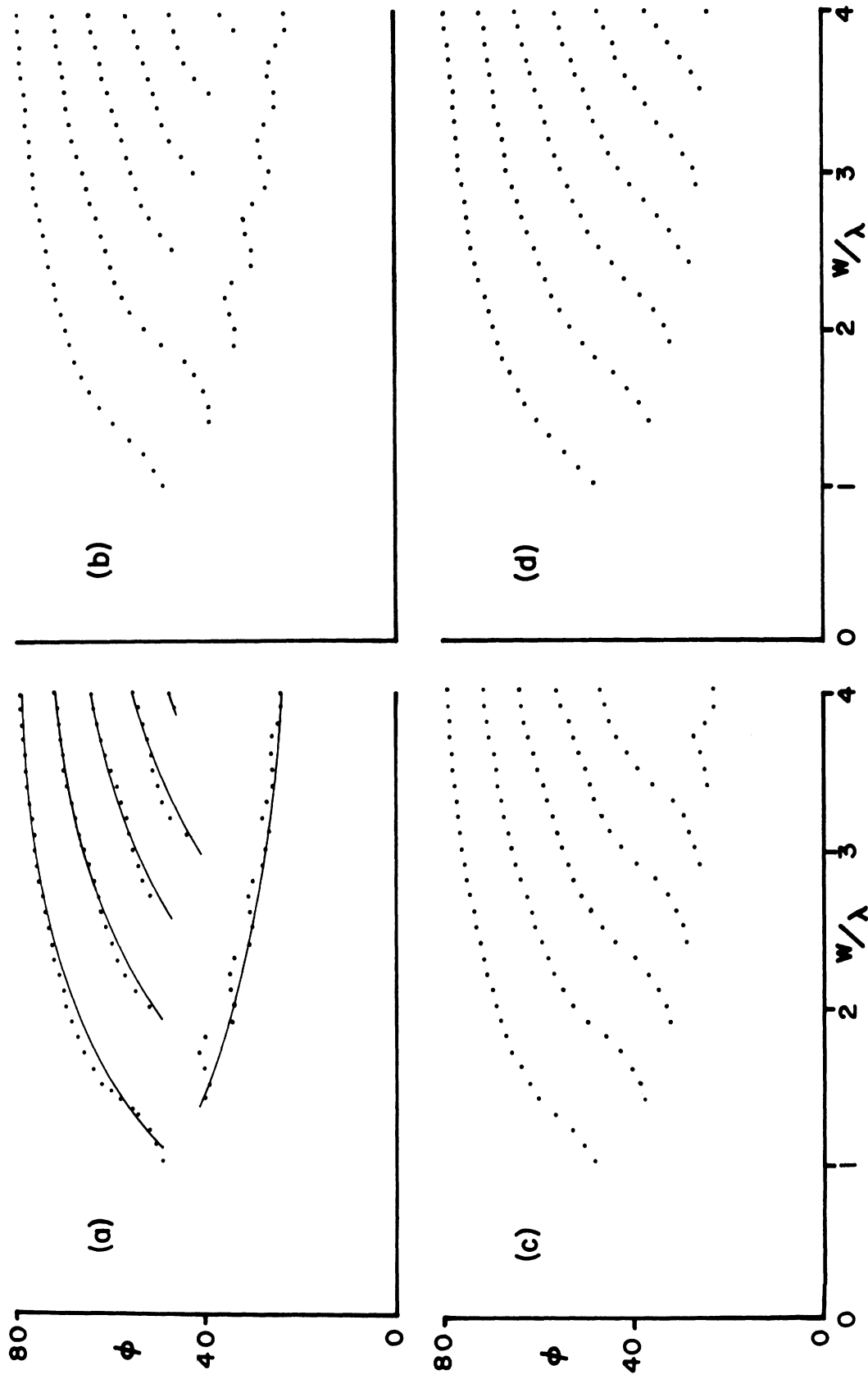


Fig. 3.6: Angles  $\phi$  (in degrees) at which peaks in the backscattering pattern occur for (a)  $R = 0$ , (b)  $R/Z = 0.05$ , (c)  $R/Z = 0.10$  and (d)  $R/Z = 0.20$ . The curves in (a) are plotted using (3.6) and (3.8).

location and the magnitude of the traveling wave lobe. The corresponding peak values of  $|P|$  (in dB) are shown in Fig. 3.7(a).

The analogous results for resistive strips having  $R/Z = 0.05, 0.1$  and  $0.2$  are shown in Figs. 3.6 and 3.7, (b) through (d). The point to be observed is that as  $R$  increases from zero the minimum strip width for which a traveling wave exists also increases. Thus, for  $R/Z = 0.05$  (corresponding to 19 ohms), a traveling wave is present only for  $w/\lambda \geq 1.9$ , and for smaller  $w/\lambda$  the peak which occurs at almost the expected position (see Fig. 3.6(b)) is actually a side lobe of the specular flash. This is evident from the manner in which the peak location changes with increasing  $w/\lambda$ , and the logical explanation is that for  $w/\lambda < 1.9$  the small amount of loss has reduced the traveling wave peak below the level of the side lobe. When  $R/Z = 0.1$  there is no traveling wave lobe unless  $w/\lambda \geq 3.4$ . The way in which the peaks for  $w/\lambda < 3.4$  are "taken over" by the side lobe of the specular flash is graphically illustrated in Fig. 3.7(c), and when  $R/Z = 0.2$  there is no evidence of a traveling wave for any  $w/\lambda < 4$ . It is apparent that even a small amount of loss is sufficient to eliminate a traveling wave for modest values of  $w/\lambda$ .

On the other hand, if the purpose of the non-zero resistivity is to reduce the near edge-on cross section, the presence of the peaks regardless of their origin could still be of concern. If we simply take the peak which occurs closest to edge-on, skipping from (side lobe) trajectory to trajectory as necessary, and plot its magnitude as a function of  $w/\lambda$ , the results shown in Fig. 3.8 are obtained. For  $R/Z \leq 0.15$  the points form a reasonably smooth oscillatory curve for all  $w/\lambda \geq 1.4$ , but when  $R/Z = 0.2$  the consequence of changing trajectories is

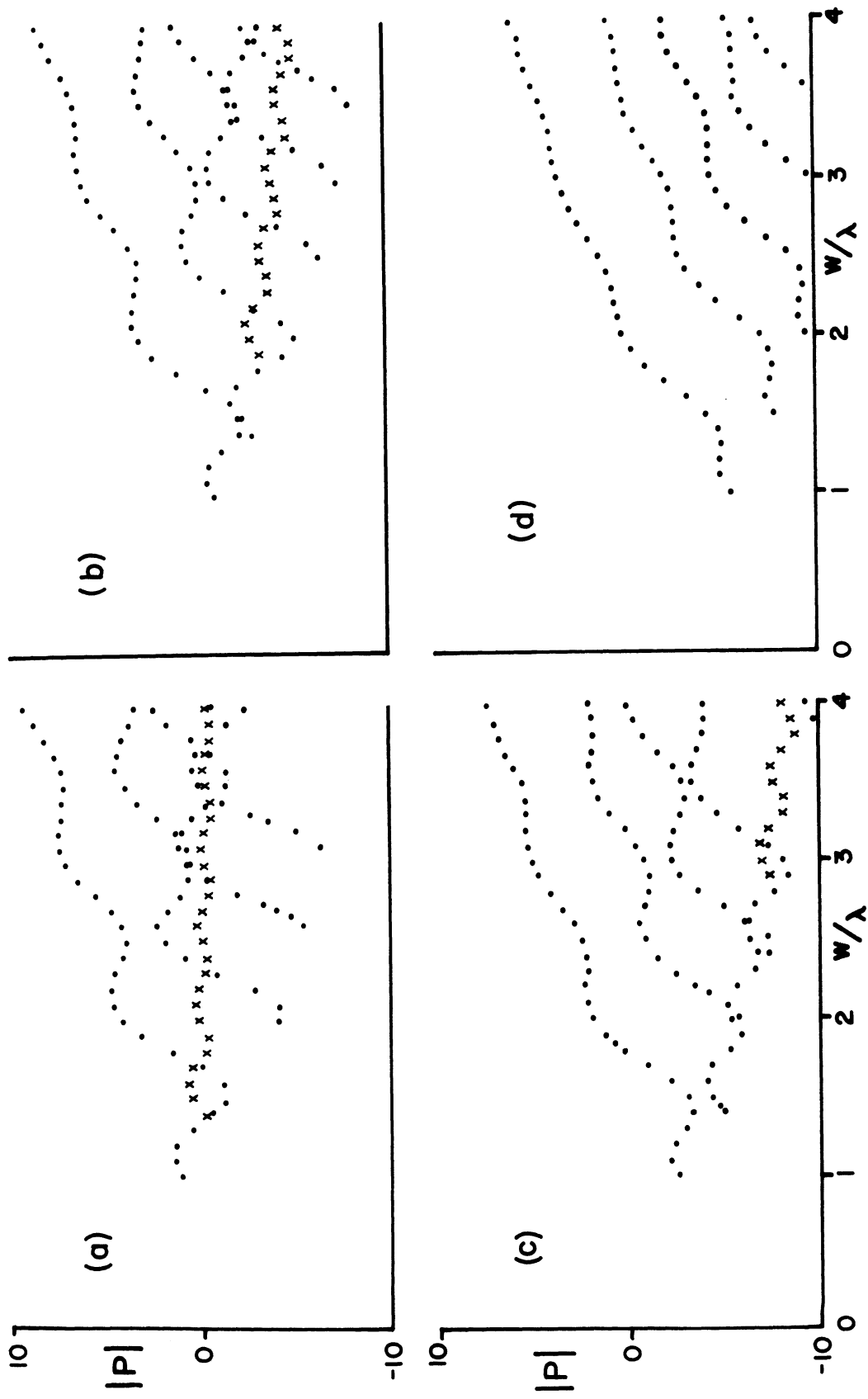


Fig. 3.7: Magnitudes  $|P|$  in dB of the peaks for (a)  $R = 0$ , (b)  $R/Z = 0.10$  and (c)  $R/Z = 0.05$  and (d)  $R/Z = 0.2$ .

The curves are merely to guide the eye and the crosses correspond to the traveling wave.

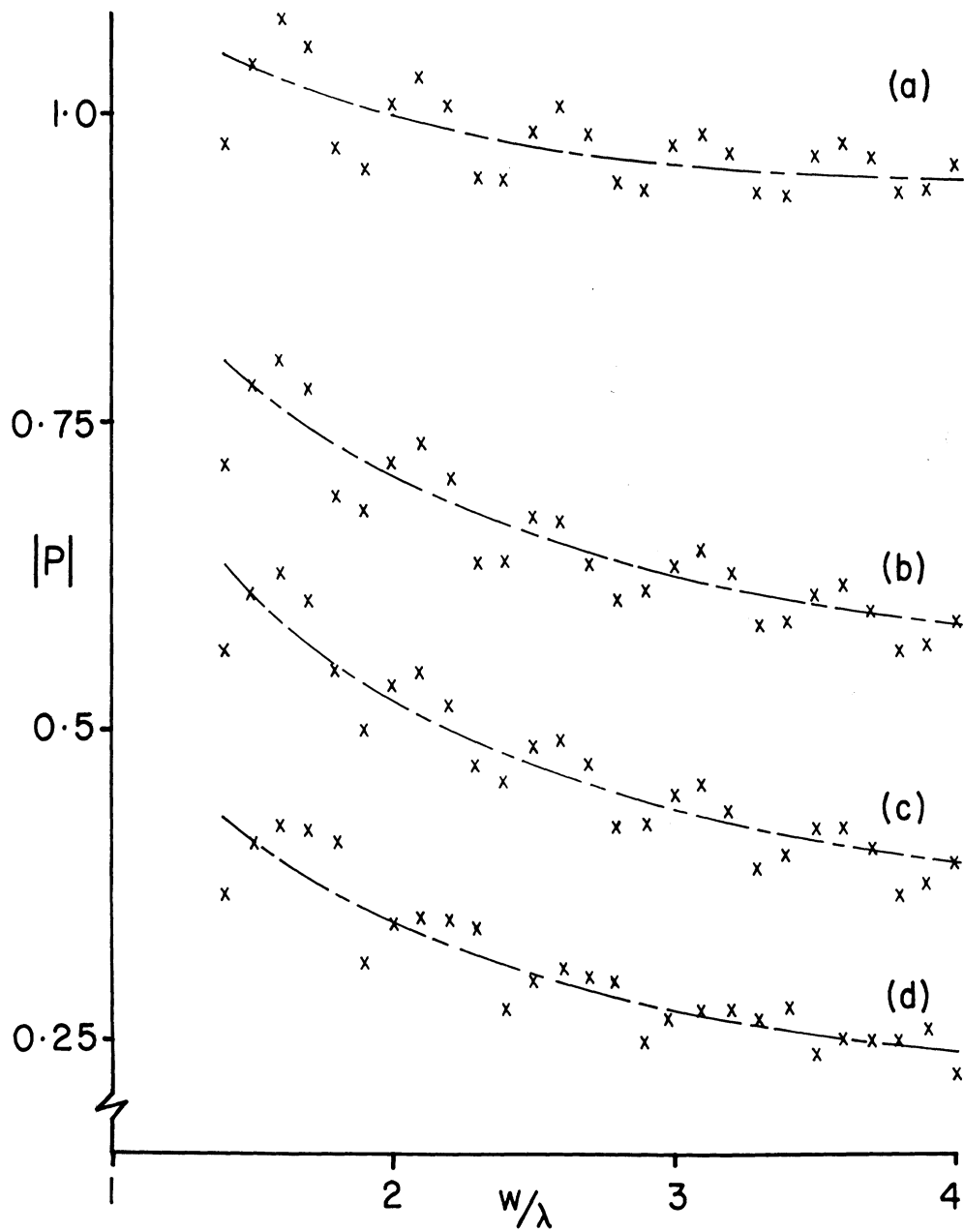


Fig. 3.8: Magnitudes of the actual or nearby traveling wave peak for (a)  $R = 0$ , (b)  $R/Z = 0.05$ , (c)  $R/Z = 0.10$  and (d)  $R/Z = 0.20$ . The curves were obtained using (3.9).

to produce noticeable discontinuities. As expected, a non-zero resistivity decreases the magnitude of the peak, and the reduction below the value for a perfectly conducting strip increases with increasing  $R/Z$  and  $w/\lambda$ . For  $R/Z = 0.2$  and  $w/\lambda = 4$  the reduction is approximately 12 dB.

We have not succeeded in developing a theoretical formula for the traveling wave peak showing the dependence on  $R/Z$  and  $w/\lambda$ . Though a uniform rigorous second order GTD expression for the bistatic scattered field of a uniform resistive strip is available (Senior 1979b), the result for H polarization is discontinuous in the limit  $R \rightarrow 0$  and cannot be used to show the effect of resistivities as small as those of interest here. Nevertheless, from an examination of the data in Fig. 3.8 it appears that an expression of the form

$$|P| = A + B \frac{\lambda}{w} \quad (3.9)$$

is adequate to predict the average return as a function of  $w/\lambda$  for a given  $R$ . By a least squares fit it is found that

$R/Z = 0$	,	$A = 0.88$	,	$B = 0.23$
$= 0.05$	,	$= 0.67$	,	$= 0.45$
$= 0.10$	,	$= 0.26$	,	$= 0.53$
$= 0.20$	,	$= 0.13$	,	$= 0.42$

and it is reasonable that these values be used in conjunction with (3.9) to estimate the effect of a small amount of resistivity.

## CHAPTER IV. RESISTIVE PLATES

The strip or ribbon is a two-dimensional analogue of a finite plate, and there is a considerable amount of useful information about the scattering from a lossy plate that can be obtained by considering the simpler two-dimensional problem. Nevertheless, the information is limited in its applicability, and in cases such as near-grazing incidence when the side edges of a plate play a role it is necessary to consider the plate directly.

### 4.1 Background

A major activity has been the development of an effective and efficient code to compute the scattering from a finite, planar resistive plate of infinitesimal thickness when illuminated by an incident plane wave. We remark that the restriction to a resistive plate is not, in fact, a restriction at all. As pointed out in a recent publication (Senior, 1985: included here as Appendix B), a thin layer whose permittivity and permeability both differ from the free space values of the surrounding medium can be simulated using superposed (electrically) resistive and (magnetically) "conductive" sheets, and these sheets are uncoupled when they are planar. A conductive sheet is the electromagnetic dual of a resistive one, and thus by running the program twice with the polarization and the sheet parameters appropriately defined, the solution for the most general imperfect plate can be obtained by addition. A special case of a combination sheet is the opaque plate having an impedance boundary condition imposed at its surfaces.

Several years ago a program was developed (Naor and Senior, 1981) to solve the integro-differential equations for the components of the total electric current induced in a resistive plate when illuminated by a plane wave. The program employs rectangular subdomains and uses simple differencing to carry out the differentiations numerically, and because of this the accuracy and generality are less than what we would like. Based on our recent experience with a program to treat dielectric plates at low frequencies (Ksienski, 1985) where a static analysis is appropriate, it was felt that the numerical differentiation could be avoided, and that a more efficient, accurate and general program would result. The efficiency is important because of our desire to treat plates up to a square wavelength or two in area with a matrix of only modest (e.g. 128 x 128) size, and this was one factor that led to our use of the C language. It is also important that the program accommodate plates of general shape (and this motivated the choice of arbitrary triangular subdomains), having an arbitrarily specified non-uniform resistivity when illuminated by a plane wave incident in any direction with any polarization. It is believed that these objectives are met by the program we have developed.

#### 4.2 Program Description

The plate is assumed to lie in the plane  $z = 0$  of a Cartesian coordinate system  $x,y,z$ , and is simulated by a resistive sheet whose resistivity  $R$  (ohms per square) is

$$R = \frac{iZ}{kt(\epsilon_r - 1)} \quad (4.1)$$

where  $t$  and  $\epsilon_r$  are the thickness and relative permittivity of the plate material,  $k$  and  $Z$  are the propagation constant and intrinsic impedance

of free space, and a time factor  $e^{-i\omega t}$  is assumed and suppressed. The boundary conditions at the plate are

$$\hat{z} \times \bar{E}|_{-}^{+} = 0$$

and

$$\hat{z} \times \bar{E} = R \hat{z} \times \bar{J} ,$$

where

$$R = \hat{z} \times \bar{H}|_{-}^{+}$$

is the total electric current, and an electric field integral equation (EFIE) for  $\bar{J}$  is then

$$R \hat{z} \times \bar{J} = \hat{z} \times \bar{E}^{inc} + i \frac{kZ}{4\pi} \hat{z} \times \left( 1 + \frac{1}{k^2} \nabla \nabla \cdot \right) \int_S \bar{J} G dS' \quad (4.2)$$

where  $G$  is the free space Green's function  $G = (e^{ikr})/r$ .

An equivalent version of (4.2) can be derived using vector and scalar potentials and is

$$R \hat{z} \times \bar{J} = \hat{z} \times \bar{E}^{inc} + i \frac{kZ}{4\pi} \hat{z} \times \int_S \bar{J} G dS' - \frac{1}{4\pi} \hat{z} \times \nabla \int_S \rho/\epsilon G dS' \quad (4.3)$$

with

$$\frac{Z}{ik} \nabla \cdot \bar{J} = \rho/\epsilon \quad (4.4)$$

and this is actually the form used by Naor and Senior (1981). In both instances the differentiation was carried out numerically. To avoid this, we first split (4.2) into Cartesian components as follows:



$$RJ_x = E_x^{inc} + i \frac{kZ}{4\pi} \int_S J_x \frac{e^{ikr}}{r} dS' + \frac{iZ}{4\pi k} \int_S \left( J_x \frac{\partial^2}{\partial x^2} + J_y \frac{\partial^2}{\partial x \partial y} \right) \frac{e^{ikr}}{r} dS' \quad (4.5)$$

$$RJ_y = E_y^{inc} + i \frac{kZ}{4\pi} \int_S J_y \frac{e^{ikr}}{r} dS' + \frac{iZ}{4\pi k} \int_S \left( J_x \frac{\partial^2}{\partial x \partial y} + J_y \frac{\partial^2}{\partial y^2} \right) \frac{e^{ikr}}{r} dS' .$$

When discretized and put in matrix form the equations become

$$[R](J_x) = (E_x^{inc}) + [A](J_x) + [B](J_y) \quad (4.6)$$

$$[R](J_y) = (E_y^{inc}) + [C](J_x) + [D](J_y)$$

where  $(E_{x(y)}^{inc})$  is an N-element column vector containing the  $x(y)$  component of incident field on each subdomain,  
 $(J_{x(y)})$  is an N-element column vector containing the  $x(y)$  component of the induced current at the sampling points,

$[R]$  is an  $N \times N$  matrix containing the resistivities at the sampling points, and

$[A],[B],[C],[D]$  are  $N \times N$  matrices containing the mutual impedances between the subdomains.

The equations (4.6) can be written as a single matrix equation as

$$\begin{pmatrix} -E_x^{inc} \\ \hline -E_y^{inc} \end{pmatrix} = \begin{bmatrix} [A]-[R] & [B] \\ [C] & [D]-[R] \end{bmatrix} \begin{pmatrix} J_x \\ \hline J_y \end{pmatrix}$$

$\uparrow$   $\uparrow$   $\uparrow$   
 2N-element 2N x 2N matrix 2N-element  
 column matrix column matrix

so that

$$\begin{pmatrix} J_x \\ -J_y \end{pmatrix} = \begin{bmatrix} [A]-[R] & [B] \\ [C] & [D]-[R] \end{bmatrix}^{-1} \begin{pmatrix} -E_x^{inc} \\ -E_y^{inc} \end{pmatrix}. \quad (4.8)$$

The matrix inversion is carried out using standard IBM FORTRAN library routines employing LU decomposition contained in the MTS NAAS package.

The discretization is based on triangular subdomains, with "tent" subsectional basis functions. The latter produce a current which is linearly varying over each subdomain and piecewise continuous over the plate. The concepts are illustrated in Figs. 4.1 and 4.2. If the currents at the vertices V1, V2 and V3 of a triangular subdomain are

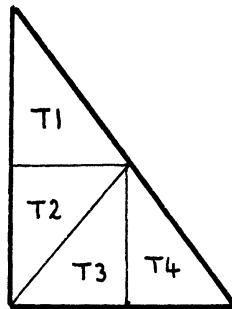


Fig. 4.1: Simple example of triangular subdomains for a triangular plate.

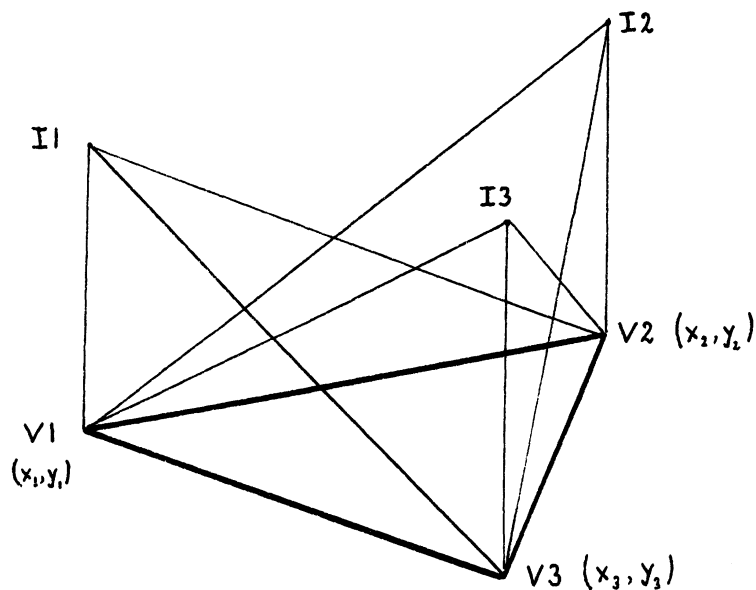


Fig. 4.2: "Tent" current basis functions.

I1, I2 and I3 respectively, then

$$I1 = \alpha_{11} x_1 + \beta_{11} y_1 + \gamma_1$$

$$I2 = \alpha_{22} x_2 + \beta_{22} y_2 + \gamma_2$$

$$I3 = \alpha_{33} x_3 + \beta_{33} y_3 + \gamma_3$$

and the current over the entire subdomain is

$$I(x,y) = (\alpha_1 + \alpha_2 + \alpha_3)x + (\beta_1 + \beta_2 + \beta_3)y + \gamma_1 + \gamma_2 + \gamma_3 .$$

The resistivity is specified at the vertices of the subdomains, and assumed to be linearly varying over the subdomain and piecewise continuous over the plate.

Special care is necessary when computing the matrix elements in (4.8) and the novel features of the program are concerned with this. In the progenitor (static) program (Ksienski, 1985b) the vertices of the subdomains were used as the sampling points, and because the singularity of the kernel of the integral equation is integrable, there is no difficulty in computing the field of the current over each subdomain at the vertices. For the dynamic problem, the higher order singularities make this approach impossible, and after examining a variety of generalized function theory methods (e.g., Fikioris, 1965; Lee et al, 1980; Asvestas, 1983; Miron, 1983), an alternative procedure was developed. For each subdomain including the self cell, the kernel was rationalized in the manner shown below and the sampling points were chosen at the centroids of the triangles. The program still computes the current at the vertices, but does so by linearly interpolating the values of the current at the centroids of the adjacent subdomains. Thus,

in Fig. 4.3, the current at VI is found by interpolating the known currents at C1, C2, C3 and C4 found from the integral equations.

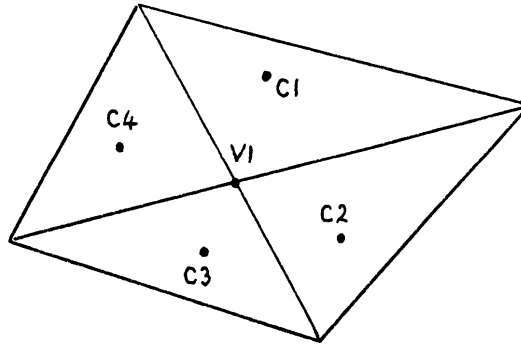


Fig. 4.3: Current computation based on the centroids.

As much as possible of the integration and differentiation was done analytically to maximize the speed and accuracy of the computation. To this end, the singular parts of the dynamic kernel which are most troublesome numerically were treated analytically, and the integrals over the subdomains were evaluated by conversion to line integrals using the method of Wilton et al (1984). Thus, the kernel was written as

$$\frac{e^{ikr}}{r} = \frac{1}{r} + ik - \frac{k^2 r}{2} + \left[ \frac{e^{ikr}}{r} - \frac{1}{r} - ik + \frac{k^2 r}{2} \right]$$

and the numerical integration and differentiation was limited to the bracketted terms. The resulting equation for the x component of the current at the jth centroid is as follows:

$$R_{xj}^J = E_{xj}^{inc} + \frac{ikZ}{4\pi} \sum_i \int_{S_i} J_{xi} \left( \frac{1}{r} + ik - \frac{k^2 r}{2} \right) dS' \quad (\text{evaluated analytically})$$

$$+ \frac{ikZ}{4\pi} \sum_i \int_{S_i} J_{xi} \left( \frac{e^{ikr}}{r} - \frac{1}{r} - ik + \frac{k^2 r}{2} \right) dS' \quad (\text{evaluated numerically})$$

(cont.)

$$\begin{aligned}
 & + \frac{iZ}{4\pi k} \sum_i \frac{\partial^2}{\partial x^2} \int_{S_i} J_{xi} \left( \frac{1}{r} + ik - \frac{k^2 r}{2} \right) dS' \text{ (evaluated analytically)} \\
 & + \frac{iZ}{4\pi k} \sum_i \int_{S_i} J_{xi} \frac{\partial^2}{\partial x^2} \left( \frac{e^{ikr}}{r} - \frac{1}{r} - ik + \frac{k^2 r}{2} \right) dS' \text{ (evaluated numerically)} \\
 & + \frac{iZ}{4\pi k} \sum_i \frac{\partial^2}{\partial x \partial y} \int_{S_i} J_{yi} \left( \frac{1}{r} + ik - \frac{k^2 r}{2} \right) dS' \text{ (evaluated analytically)} \\
 & + \frac{iZ}{4\pi k} \sum_i \int_{S_i} J_{yi} \frac{\partial^2}{\partial x \partial y} \left( \frac{e^{ikr}}{r} - \frac{1}{r} - ik + \frac{k^2 r}{2} \right) dS' \text{ (evaluated numerically)}
 \end{aligned}$$

The equation for  $J_{yj}$  is similar. Note that the derivatives are taken inside the integrals only when the integrands are non-singular. The numerical integration was carried out using the method of Hammer et al (1956), which is exact for a fifth order polynomial.

Because of time limitations the program is not yet complete. The final part necessary to compute the scattered field of the plate has not been finished, nor does the program make use of any symmetries that the plate may possess. In its present form the program is limited to the computation of the current induced in a plate of arbitrary size and resistivity. The source code consists of approximately 2200 lines of C language code, plus approximately 1000 lines of IBM FORTRAN NAAS library routines. The program compiles and, to judge from the few runs that have been made on a VAX, appears to produce accurate results. Nevertheless, there is further work that must be done and apart from the

additions necessary to compute the scattered field we are also aware of some changes that should be made to improve the accuracy.

A source listing is included as an attachment to this report.

APPENDIX A: IBM PC PROGRAM P-RIB-H

A program has been developed for use on an IBM PC computer to determine the high frequency bistatic scattered field of a perfectly conducting strip or ribbon for H polarization.

A perfectly conducting strip of width  $w$  occupies the region  $0 \leq x \leq w$ ,  $-\infty < z < \infty$  of the plane  $y = 0$  of a Cartesian coordinate system  $x, y, z$ , and is illuminated by an H-polarized plane wave having

$$\vec{H}^i = \hat{z} e^{-ik(x \cos \phi_0 + y \sin \phi_0)}$$

where a time factor  $e^{-i\omega t}$  is assumed and suppressed. At large distances the scattered magnetic field can be written as

$$\vec{H}^s \sim \hat{z} \sqrt{\frac{2}{\pi k \rho}} e^{i(k\rho - \pi/4)} P(\phi, \phi_0)$$

where  $\rho, \phi$  are cylindrical polar coordinates with  $x = \rho \cos \phi$ ,  $y = \rho \sin \phi$ . In terms of the two-dimensional far field amplitude  $P$  the scattering cross section per unit length in the  $z$  direction is

$$\sigma(\phi, \phi_0) = \frac{2\lambda}{\pi} |P(\phi, \phi_0)|^2, \quad (1)$$

and in the particular case of backscattering,  $\phi_0 = \phi$ . From symmetry it is sufficient to consider only  $\pi/2 \leq \phi \leq \pi$  where  $\phi = \pi$  corresponds to grazing incidence.

Using a GTD approach, Senior (1979b) developed an expression for the bistatic scattered field of a uniform resistive strip through second order terms, and when specialized to the case of a perfectly conducting strip with  $\phi_0 = \phi$ , the result is

$$P(\phi, \phi) = -\frac{i}{4} \frac{1 + \cos \phi}{\cos \phi} + \frac{i}{4} \frac{1 - \cos \phi}{\cos \phi} e^{-2ikw \cos \phi} - \left(\frac{2}{\pi kw}\right)^{1/2} e^{-i\pi/4} \frac{e^{ikw(1 - \cos \phi)}}{\sin \phi} + O([kw]^{-1}) \quad (2)$$

where the origin of phase is at the left hand edge of the strip. At broadside ( $\phi = \pi/2$ ) the infinities of the first two terms cancel and (2) reduces to

$$P\left(\frac{\pi}{2}, \frac{\pi}{2}\right) = \frac{1}{2} kw - \frac{i}{2} - \left(\frac{2}{\pi kw}\right)^{1/2} e^{i(kw - \pi/4)} + O([kw]^{-1}) \quad (3)$$

For  $\phi > \pi/2$  the first and second terms on the right hand side of (2) are the contributions of the front and rear edges respectively, with the former vanishing for grazing incidence. The third term is the second order contribution and this clearly fails when  $\phi = \pi$ , but by expressing (2) in terms of the half plane current and then using a uniform asymptotic representation of the current, a uniform expression for  $P(\phi, \phi)$  valid for  $\pi/2 < \phi \leq \pi$  is found to be

$$P(\phi, \phi) = -\frac{i}{4} \frac{1 + \cos \phi}{\cos \phi} \left[ 1 - \left(\frac{2}{\pi kw}\right)^{1/2} e^{i\pi/4 + ikw(1 - \cos \phi)} \cot \frac{\phi}{2} + \frac{i}{4} \frac{1 - \cos \phi}{\cos \phi} e^{-2ikw \cos \phi} \left[ 1 - \frac{2}{\sqrt{\pi}} e^{-i\pi/4} \sin \frac{\phi}{2} F\left(\sqrt{2kw} \cos \frac{\phi}{2}\right) \right]^2 + O([kw]^{-1}) \quad (4)$$



where  $F(\tau)$  is the Fresnel integral

$$F(\tau) = \int_{\tau}^{\infty} e^{iu^2} du \quad . \quad (5)$$

For large values of  $\tau$ ,

$$F(\tau) \sim \frac{i}{2\tau} e^{i\tau^2}$$

and when this is substituted into (4) we recover the asymptotic expression (2). On the other hand, for small  $\tau$

$$F(\tau) = \frac{1}{2} \sqrt{\pi} e^{i\pi/4} + O(\tau)$$

showing that  $P(\pi, \pi) = 0$ , as expected. In general

$$F(\tau) = \sqrt{\frac{\pi}{2}} \left\{ \frac{1}{2} - C(\tau^2) + i \left[ \frac{1}{2} - S(\tau^2) \right] \right\} \quad , \quad (6)$$

where  $C$  and  $S$  are cosine and sine integrals whose computation is described by Boersma (1960). Thus

$$\frac{2}{\sqrt{\pi}} e^{-i\pi/4} \sin \frac{\phi}{2} F(\sqrt{2kw} \cos \phi) = \sin \frac{\phi}{2} \{1 - C(u) - S(u) + i[C(u) - S(u)]\}$$

where

$$u = kw(1 + \cos \phi) \quad .$$

The introduction of the Fresnel integral to provide a uniform behavior in the vicinity of  $\phi = \pi$  produces a difficulty near broadside

since the infinities of the first two terms on the right hand side of (4) no longer cancel precisely when  $\phi = \pi/2$ . For this reason it is desirable to introduce a second Fresnel integral whose main effect is to produce a uniform behavior near  $\phi = 0$  in spite of the fact that we are only concerned with  $\phi \geq \pi/2$ . The result is

$$\begin{aligned}
 P(\phi, \phi) = & -\frac{i}{4} \frac{1 + \cos \phi}{\cos \phi} \left\{ 1 - \frac{2}{\sqrt{\pi}} e^{-i\pi/4} \cos \frac{\phi}{2} F \left( \sqrt{2kw} \sin \frac{\phi}{2} \right) \right\}^2 \\
 & + \frac{i}{4} \frac{1 - \cos \phi}{\cos \phi} e^{-2ikw \cos \phi} \left\{ 1 - \frac{2}{\sqrt{\pi}} e^{-i\pi/4} \sin \frac{\phi}{2} F \left( \sqrt{2kw} \cos \frac{\phi}{2} \right) \right\}^2 \\
 & + O([kw]^{-1}) \tag{7}
 \end{aligned}$$

valid for  $0 \leq \phi \leq \pi$ . The infinities at  $\phi = \pi/2$  now cancel precisely, and we remark that (7) is identical to the result obtained by asymptotic expansion of the uniform expression of Khaskind and Vainshteyn (1964).

A program designated P-RIB-H (perfectly conducting-ribbon-H polarization) has been written to compute the function  $P(\phi, \phi)$  using (7). It is coded in BASIC on our IBM personal computer and computes  $\sigma/\lambda$  (in dB),  $|P|$  and  $\arg P$  (in degrees) as functions of the angle  $\phi$  for  $91 \leq \phi \leq 179$  degrees. The broadside angle  $\phi = 90$  degrees is omitted to avoid numerical problems, but in practice, a knowledge of the far field at 91 degrees is sufficient to determine the broadside return. When  $\phi = 180$  degrees,  $|P| = 0$ , and this angle is also omitted to avoid problems in computing  $\arg P$ .

Some results obtained with P-RIB-H are compared with those of an integral equation solution by the moment method in Figs. 1 through 6.

The agreement is good for all  $w/\lambda \gtrsim 0.5$ , though we do observe a somewhat larger phase discrepancy than expected for  $\phi \geq 130$  degrees with  $w/\lambda = 2$ . The traveling wave lobe is faithfully reproduced and this enables us to use (7) or, indeed, (4) for studying traveling wave effects. From the GTD viewpoint the Fresnel integrals were introduced to match the second order expansion for  $0 < \phi < \pi$  into the zero values at grazing incidence, but one interesting consequence is that (7), as opposed to (2), is reasonably accurate even for small values of  $w/\lambda$ .

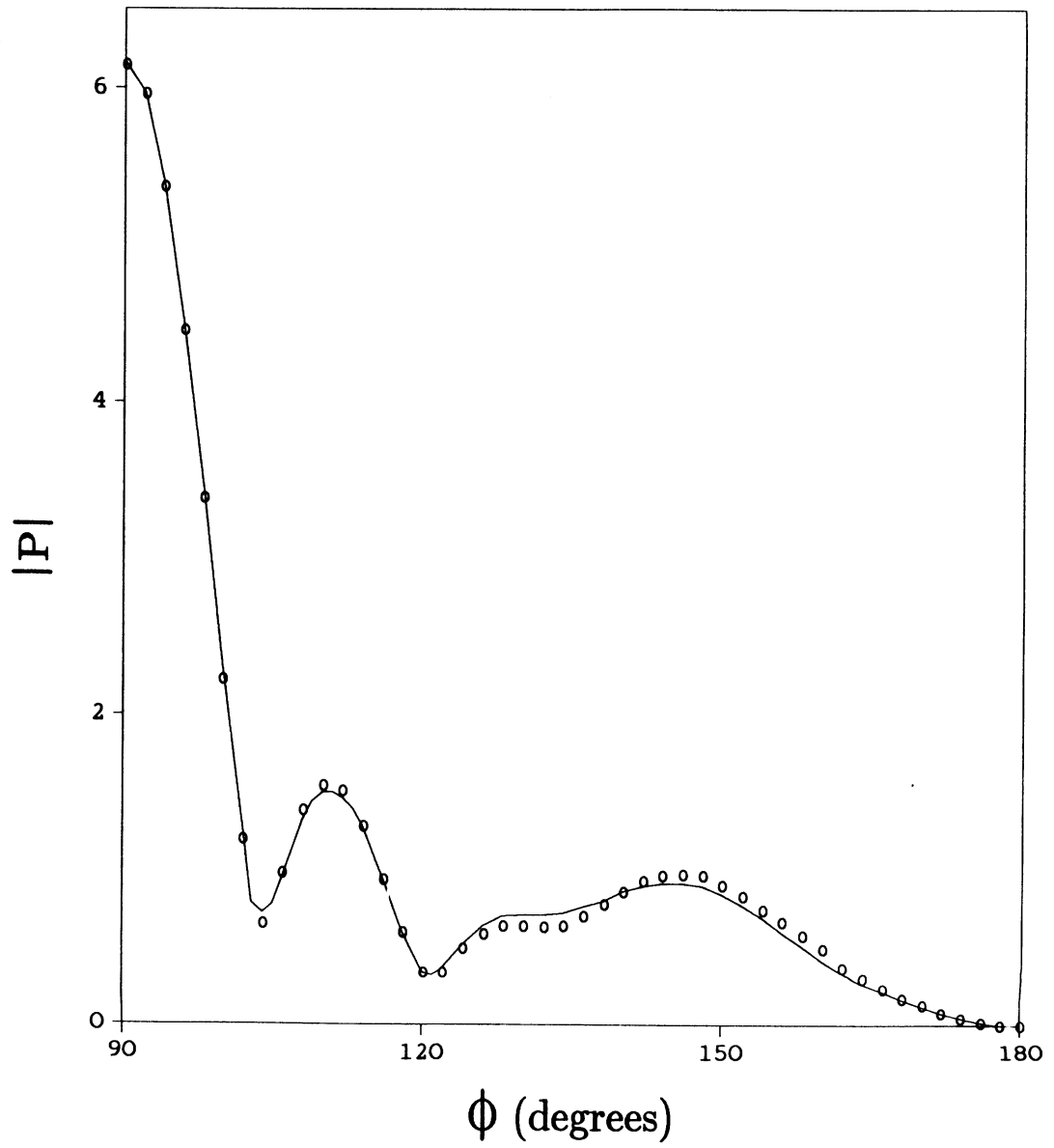


Fig. 1:  $|P|$  for  $w/\lambda = 2$  computed using P-RIB-H (ooo) compared with the results of an integral equation method (—).

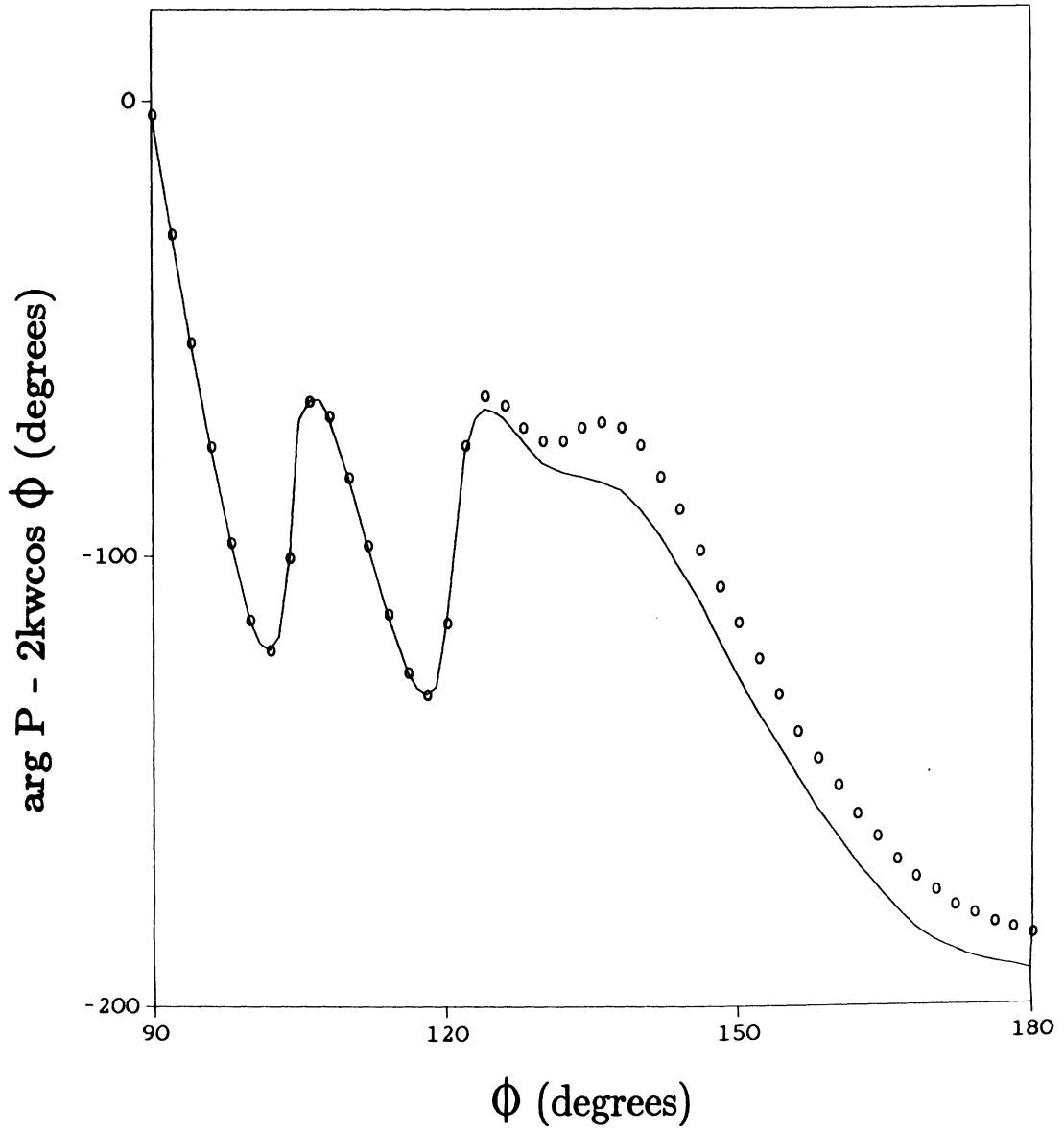


Fig. 2: Arg P for  $w/\lambda = 2$  computed using P-RIB-H (ooo) compared with the results of an integral equation method (—).

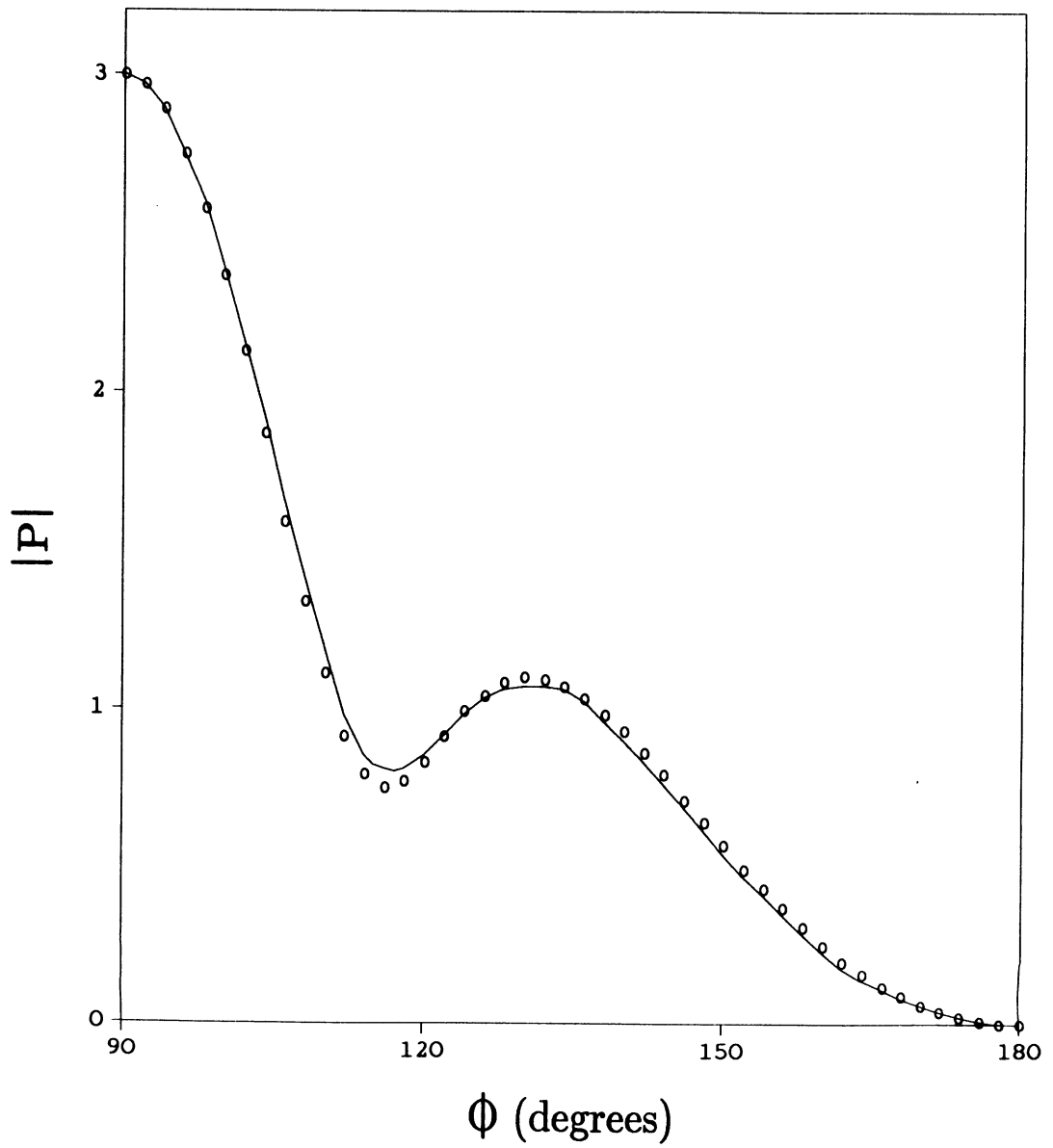


Fig. 3: Arg P for  $w/\lambda = 1$  computed using P-RIB-H (ooo) compared with the results of an integral equation method (—).

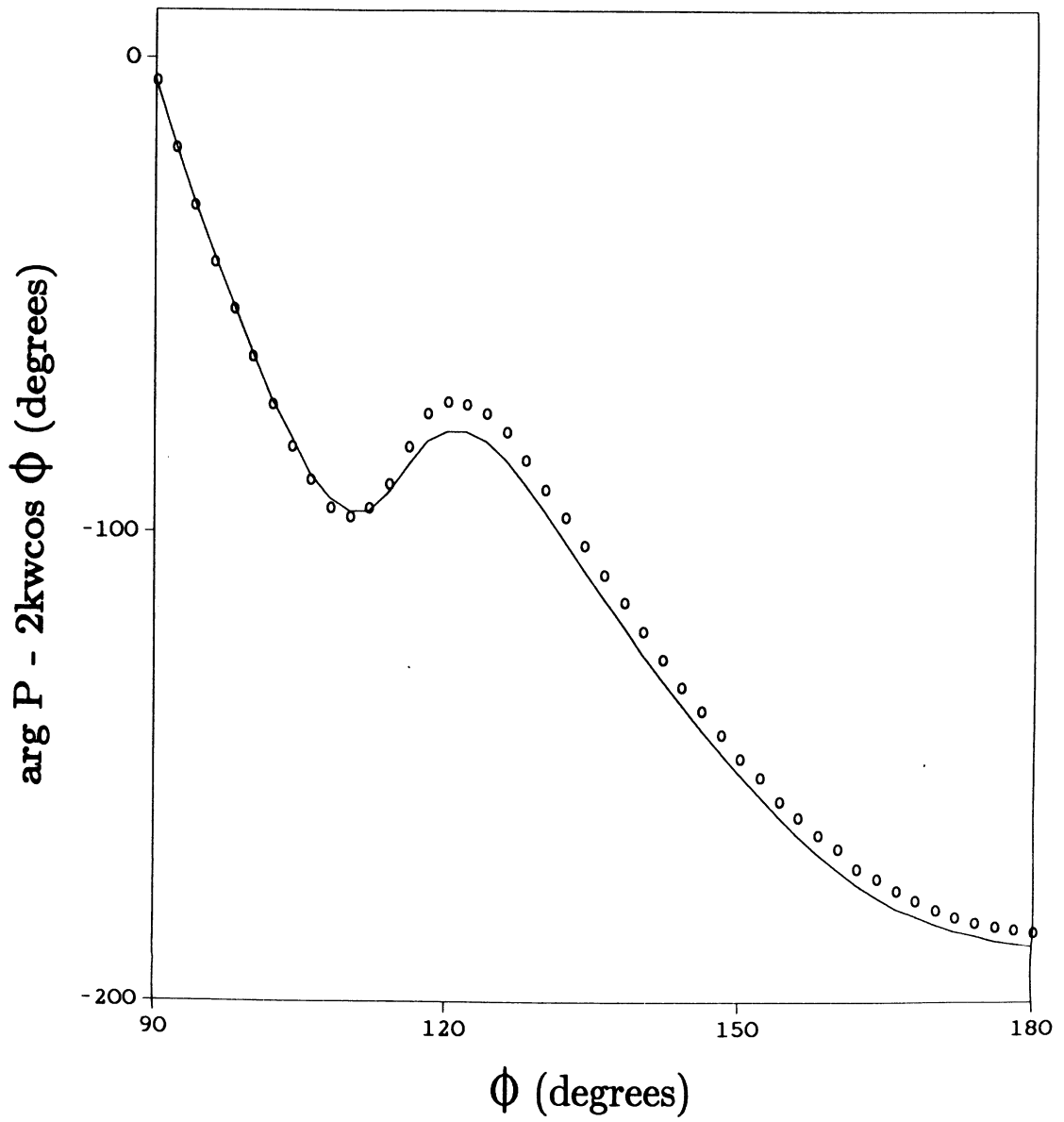


Fig. 4: Arg P for  $w/\lambda = 1$  computed using P-RIB-H (ooo) compared with the results of an integral equation method (—).

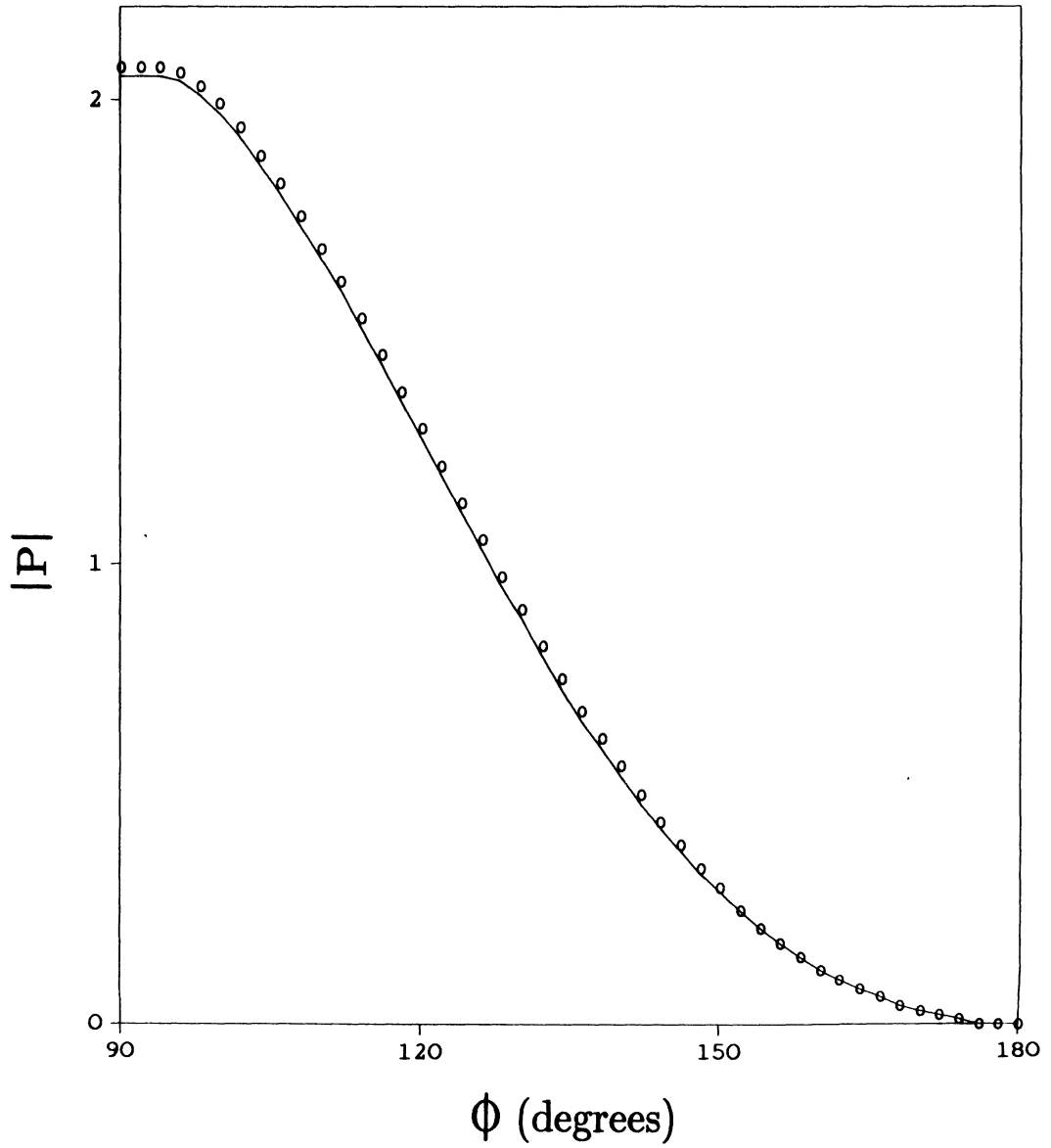


Fig. 5: Arg P for  $w/\lambda = 0.5$  computed using P-RIB-H (ooo) compared with the results of an integral equation method (—).



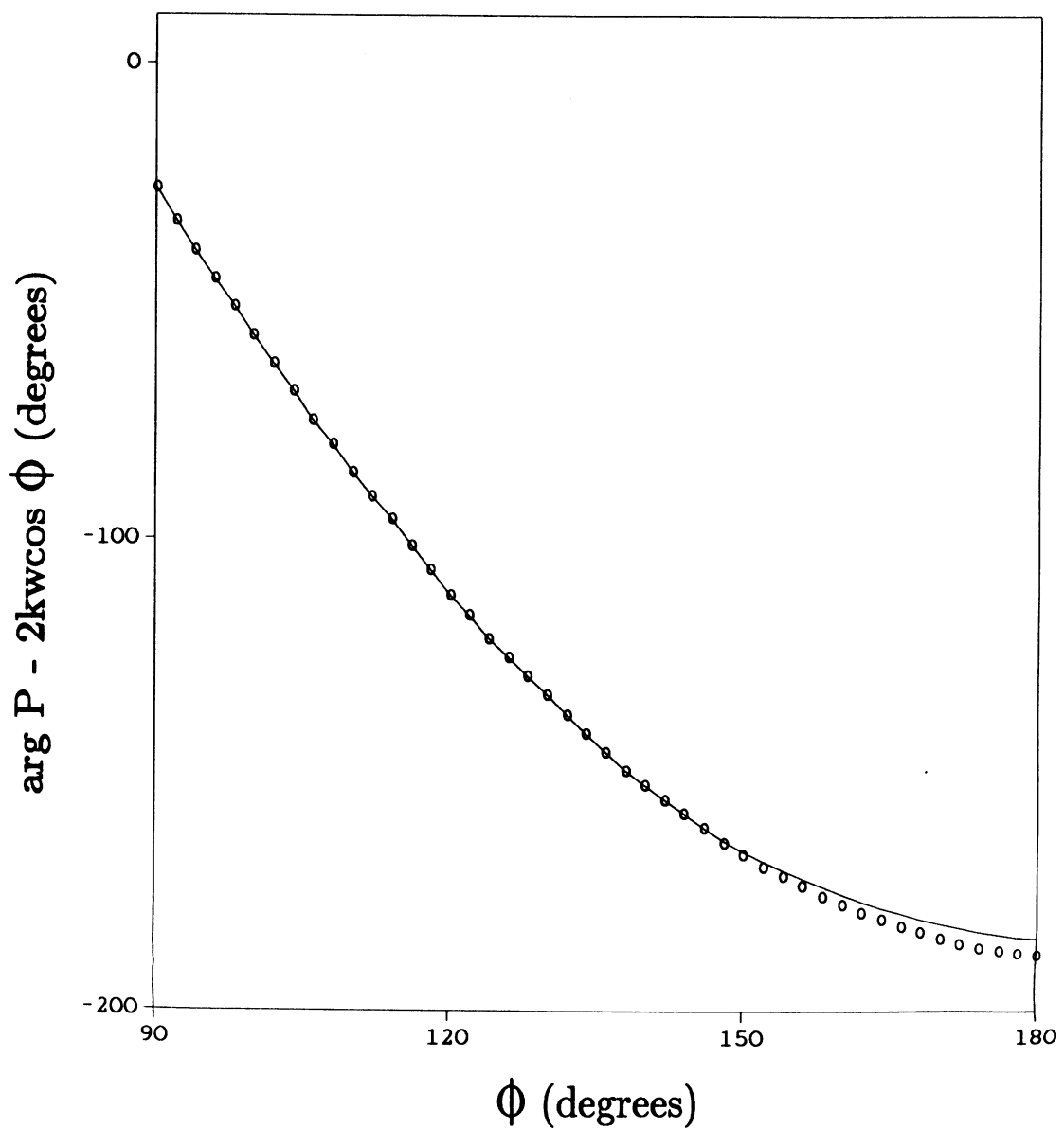


Fig. 6: Arg P for  $w/\lambda = 0.5$  computed using P-RIB-H (ooo) compared with the results of an integral equation method (—).

```
5 *          PROGRAM P-RIB-H
7 *
10 * THIS PROGRAM CALCULATES THE BACKSCATTERED FIELD OF A PERFECTLY CONDUCTING
20 * STRIP (OR RIBBON) FOR H POLARIZATION USING A SECOND ORDER UNIFORM GTD
30 * APPROXIMATION. THE QUANTITIES COMPUTED ARE BACKSCATTERING CROSS SECTION PER
    UNIT LENGTH SIGMA/LAMDA [DB],MAG P AND PHASE P [DEGREES],WHERE P IS THE FAR
40 * FIELD COEFFICIENT, AS FUNCTIONS OF THE INCIDENT ANGLE PHI, 91 <= PHI <= 179
45 * [DEGREES], FOR A SPECIFIED VALUE OF KW WHERE W IS THE STRIP WIDTH.
50 *
60 * THE USER ENTERS:
70 *   1) DX - THE ANGULAR STEP INCREMENT USED IN PLOTTING. .5 TO 2 DEGREES
80 *       IS GOOD
90 *   2) W/LAMDA - WHERE LAMDA =WAVELENGTH, W=STRIP WIDTH
100 *   3) MAXP - THE MAXIMUM HEIGHT FOR THE PLOT.
110 INPUT "ENTER ANGLE INCREMENT IN DEGREES   ",DX
120 INPUT "ENTER W/LAMDA   ",W
130 INPUT "ENTER MAXIMUM Y COORDINATE   ",MAXP
132 LPRINT "W/LAMDA = "; W
140 PI=3.141593
145 KW=2*PI*W
150 R2=SQR(2)
160 RPI=SQR(PI)
161 D=.1
162 D1=.025
170 *
180 *SET UP THE SCREEN
190 CLS
195 KEY OFF
200 SCREEN 2
210 WINDOW (1,-2)-(3.5,MAXP+1)
220 LINE (PI/2,0)-(PI,0)
230 LINE (PI/2,0)-(PI/2,MAXP)
232 FOR I=1 TO MAXP STEP 1
233 LINE (PI/2-D1,I)-(PI/2+D1,I)
234 NEXT
235 FOR J= 1 TO 9 STEP 1
236 LINE (PI/2+J*PI/18,D)-(PI/2+J*PI/18,-D)
237 NEXT
240 LOCATE 5,40: PRINT "W/LAMDA = ";W
241 LOCATE 3,15: PRINT USING "##.##";MAXP
242 LOCATE 21,15: PRINT "0.0"
243 LOCATE 22,18: PRINT "90"
244 LOCATE 22,70: PRINT "180"
245 LOCATE 22,35: PRINT "ANGLE [DEGREE]"
246 LOCATE 10,13: PRINT "MAG P"
250 *ALL THE FOLLOWING FUNCTIONS ARE DEFINED BECAUSE THERE IS NO
260 *COMPLEX ARITHMETIC. THE FINAL FUNCTION TO BE PLOTTED IS CALLED
270 *MAGP.
280 DEF FNA(X)=(1+COS(X))/(4*COS(X))
300 DEF FNC(X)=(1-COS(X))/(4*COS(X))
320 DEF FNANG3(X)=-2*KW*COS(X)
370 DEF FNREP(X)= FA*FR1I - FC*(FR2R*SIN(ANG3) + FR2I*COS(ANG3))
380 DEF FNIMPP(X)= -FA*FR1R +FC*(FR2R*COS(ANG3) -FR2I*SIN(ANG3))
390 DEF FNMAGP(X)=SQR(FNREP(X)^2+FNIMPP(X)^2)
400 *
```

```
410 'THE FIRST POINT TO BE PLOTTED IS FOR A VALUE OF 91 DEGREES.  THE FOLLOWING
420 'PRESETS THIS FIRST POINT SO WE CAN MOVE INTO THE LOOP.
430 'WE DO NOT USE 90 DEGREES TO AVOID DIVISION BY ZERO.
631 LPRINT "ANGLE  SIGMA/LAM [DB]          MAG P    PHASE P
640 '
650 'NOW WE ARE READY TO LOOP THROUGH AND PLOT THE FUNCTION FROM 91 DEGREES
660 'TO 179 DEGREES.
662 I=1
670 DX=DX*(PI/180)
680 FOR X=PI/2+PI/180 TO PI-PI/180 STEP DX
690 Z=KW*(1-COS(X))
700 GOSUB 900
710 CS1=CS
720 SN1=SN
730 Z= KW*(1+ COS(X))
740 GOSUB 900
750 CS2=CS
760 SN2=SN
810 ANG3=FNANG3(X)
820 FA=FNA(X)
830 FC=FNC(X)
840 FR1= 1-COS(X/2)*(1-CS1-SN1):  FR2=COS(X/2)*(SN1-CS1)
850 FS1= 1-SIN(X/2)*(1-CS2-SN2):  FS2=SIN(X/2)*(SN2-CS2)
855 FR1R= FR1^2 - FR2^2 :  FR1I= 2* FR1 * FR2
857 FR2R= FS1^2 - FS2^2 :  FR2I= 2* FS1 * FS2
860 YY=FNMAGP(X)
865 IF I=1, THEN PRESET (PI/2,YY)  ELSE  LINE  -(X,YY)
870 I=I+1
871 GOSUB 1200
880 NEXT
890 END
900 '
910 'THIS SUBROUTINE COMPUTES THE FRESNEL INTEGRAL.  IT USES TWO DIFFERENT
920 'APPROXIMATIONS FOR ARGUMENTS GREATER OR LESS THAN FOUR.
930 'REFERENCES:  "COMPUTATION OF FRESNEL INTEGRAL" BY BOERSMA, MATHEMATICAL
940 '              TABLES AND OTHER AIDS TO COMPUTATION, VOL. 14, 1960
950 '              NO. 72, PAGE 380
960 'C(X)=REAL PART OF INTEGRAL EXP(it)/SQRT(2*pai*t) FROM 0 TO X
970 'S(X)=IMAGINARY PART OF THE ABOVE INTEGRAL
990 IF Z>4 GOTO 1080
1000 ZY=Z/4
1010 AR=1.59576914# - 1.702E-06*Z  -6.808568854##ZY^2 -5.76361E-04*ZY^3  + 6.920
691902##ZY^4  -.016898657##ZY^5  -3.05048566##ZY^6  - .075752419##ZY^7  +.850663781
##ZY^8  - .025639041##ZY^9  -.15023096##ZY^10  + .034404779##ZY^11
1030 AI=-(-3.3E-08 + 4.255387524##ZY-9.281E-05*ZY^2 -7.7800204##ZY^3  - 9.520895E
-03*ZY^4  + 5.075161298##ZY^5  - .138341947##ZY^6  - 1.363729124##ZY^7  -.403349276
##ZY^8  + .702222016##ZY^9  -.216195929##ZY^10  + .019547031##ZY^11)
1040 CS=SQR(ZY)*(AR*COS(Z)-AI*SIN(Z))
1050 SN=SQR(ZY)*(AR*SIN(Z)+AI*COS(Z))
1070 RETURN
```

```
1080 ZZ=4/Z
1110 BR=-.024933975##ZZ + 3.936E-06*ZZ^2 + 5.770956E-03*ZZ^3 +6.89892E-04*ZZ^4
-9.497136E-03*ZZ^5 + .011948809##ZZ^6 -6.748873E-03*ZZ^7 +2.4642E-04*ZZ^8
+2.102967E-03*ZZ^9-1.21793E-03*ZZ^10 +2.33939E-04*ZZ^11
1120 BI=-(.19947114# +2.3E-08*ZZ -9.351341E-03*ZZ^2 +2.3006E-05*ZZ^3 +4.851466E-
03*ZZ^4 +1.903218E-03*ZZ^5 -.017122914##ZZ^6 +2.906467E-02*ZZ^7 -.027928955##ZZ^
8 +.016497308##ZZ^9 -5.598515E-03*ZZ^10 +8.38386E-04*ZZ^11)
1130 CS=.5 + SQR(ZZ)*(BR*COS(Z) - BI*SIN(Z))
1140 SN=.5 + SQR(ZZ)*(BR*SIN(Z) + BI*COS(Z))
1180 RETURN
1200 ANGLE= 57.29578*X
1210 IF FNMAGP(X)=0, THEN SCS=-999.99 ELSE SCS=20*LOG(FNMAGP(X))/LOG(10)-1.9612
1215 FFF=FNIMPP(X)/FNREP(X)
1220 IF FNREP(X)=0, THEN PHASY=-999.99 ELSE PHASY=57.29578*ATN(FFF)
1222 IF FNREP(X) >= 0, THEN PHASE= PHASY ELSE PHASE= PHASY +SGN(FNIMPP(X))*180
1230 LPRINT USING "#####.##"; ANGLE;SCS;
1240 LPRINT USING "#####.#####"; FNMAGP(X);
1250 LPRINT USING "#####.###"; PHASE
1260 RETURN
```

## Combined Resistive and Conductive Sheets

THOMAS B. A. SENIOR, FELLOW, IEEE

**Abstract**—To simulate a thin layer of material whose permittivity and permeability both differ from the values for the surrounding medium, a combination resistive and conductive sheet is defined and its properties described.

### I. INTRODUCTION

Thin layers of lossy material are of obvious interest for cross section reduction purposes. A mathematical model of such a layer is a resistive sheet, and during the last few years the scattering from this type of sheet has been extensively explored [1]–[3]. The electromagnetic dual of an electrically resistive sheet is a “magnetically conductive” one [4], and to simulate a thin layer whose permittivity and permeability both differ from the surrounding medium, it may be necessary to include this sheet as well.

The properties of a combined sheet consisting of coincident resistive and conductive ones are examined. Although the two sheets are, in general, coupled, with each affecting the scattering from the other, decoupling occurs when the sheets lie in a plane. This is true regardless of the (planar) configuration, and has implications for the development of analytical and numerical methods to predict the scattering from lossy plates.

### II. BOUNDARY CONDITIONS

An electrically resistive sheet is simply an electric current sheet whose strength is proportional to the tangential electric field at its surface, and in recent years the concept of such a sheet has found many useful applications. As noted by Levi-Civita (see [4, p. 19]), its electromagnetic properties are completely specified by its resistivity  $R$  in ohms per square, and the boundary conditions at its surface are

$$\hat{n} \times \vec{E}(+) - \hat{n} \times \vec{E}(-) = 0, \quad (1)$$

$$\hat{n} \times \vec{H}(+) - \hat{n} \times \vec{H}(-) = \vec{J} \quad (2)$$

with

$$\hat{n} \times \{\hat{n} \times \vec{E}(\pm)\} = -R\vec{J} \quad (3)$$

where  $\hat{n}$  is a unit vector normal drawn outward to the positive (plus) side of the sheet and  $\vec{J}$  is the total electric current sup-

ported. Equation (1) implies that there is no magnetic current and, hence, that the permeability of the corresponding layer is the same as that of the surrounding (free space) medium. Because of this, (3) can be written as

$$\hat{n} \times \{\hat{n} \times [\vec{E}(+) + \vec{E}(-)]\} = -2R\vec{J}, \quad (4)$$

and in the special case  $R = 0$  the sheet is perfectly conducting, whereas if  $R = \infty$  the sheet is no longer present. For a material of large conductivity  $\sigma$ ,

$$R = (\sigma\tau)^{-1}$$

where  $\tau$  is the thickness of the layer, and an alternative expression is [5]

$$R = \frac{iZ}{(\epsilon_r - 1)k\tau} \quad (5)$$

valid if  $|\epsilon_r - 1| \gg 1$ . In (5),  $k$  and  $Z (=1/Y)$  are the propagation constant and impedance, respectively, of free space,  $\epsilon_r$  is the relative permittivity of the layer material, and a time factor  $e^{-i\omega t}$  has been assumed.

The electromagnetic dual is a magnetically conductive sheet [6] supporting only a magnetic current  $\vec{J}^*$ , and by analogy with (1), (2), and (4) the boundary conditions at its surface are

$$\hat{n} \times \vec{H}(+) - \hat{n} \times \vec{H}(-) = 0, \quad (6)$$

$$\hat{n} \times \vec{E}(+) - \hat{n} \times \vec{E}(-) = -\vec{J}^* \quad (7)$$

with

$$\hat{n} \times \{\hat{n} \times [\vec{H}(+) + \vec{H}(-)]\} = -2R^*\vec{J}^* \quad (8)$$

where  $R^*$  is the conductivity. By virtue of (6), a layer modeled by such a sheet must have its relative permittivity unity, and from (5) an expression for  $R^*$  is

$$R^* = \frac{iY}{(\mu_r - 1)k\tau} \quad (9)$$

valid for  $|\mu_r - 1| \gg 1$  where  $\mu_r$  is the relative permeability of the layer material.

### III. COMBINATION SHEET

To model a layer whose permittivity and permeability both differ from their free space values a logical approach is to consider a combination sheet consisting of coincident resistive and conductive sheets at which the boundary conditions are (2)–(4) and (6)–(8). If  $\hat{s}$  and  $\hat{t}$  are unit vectors in the plane of the sheet such that at every point  $\hat{s} \cdot \hat{t} = 0$  and  $\hat{s} \times \hat{t} = \hat{n}$ , implying that  $\hat{s}$ ,  $\hat{t}$ , and  $\hat{n}$  form a right-handed system, (3), (4), (7), and (8) can be written as

$$E_s(+) + E_s(-) = -2R\{H_t(+) - H_t(-)\},$$

$$E_s(+) - E_s(-) = -(2R^*)^{-1}\{H_t(+) + H_t(-)\};$$

$$E_t(+) + E_t(-) = 2R\{H_s(+) - H_s(-)\},$$

$$E_t(+) - E_t(-) = (2R^*)^{-1}\{H_s(+) + H_s(-)\}.$$

Addition and subtraction of the equations in pairs gives

$$\begin{aligned} E_s(\pm) &= -R \left(1 \pm \frac{1}{4RR^*}\right) H_t(+) + R \left(1 \mp \frac{1}{4RR^*}\right) H_t(-) \\ E_t(\pm) &= R \left(1 \pm \frac{1}{4RR^*}\right) H_s(+) - R \left(1 \mp \frac{1}{4RR^*}\right) H_s(-) \end{aligned} \quad (10)$$

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showing that, in general, the sheet is partially transparent, but if

$$4RR^* = 1 \quad (11)$$

the conditions (10) reduce to Leontovich boundary conditions [7] on the two sides of the sheet. The combined sheet is then opaque and is simply an impedance (boundary condition) sheet with the same surface impedance  $\eta = 2R$  on each side. In view of (11) an equivalent formula for the surface impedance is  $\eta = (R/R^*)^{1/2}$ , and when the expressions for  $R$  and  $R^*$  are inserted, we find

$$\eta = Z \left( \frac{\mu_r - 1}{\epsilon_r - 1} \right)^{1/2} \cong Z \left( \frac{\mu_r}{\epsilon_r} \right)^{1/2} \quad (12)$$

as expected.

Under most circumstances the resistive and conductive sheets comprising a combination sheet are coupled inasmuch as the strength (as measured by the current supported) and the scattering of each sheet are effected by the presence of the other. To illustrate this fact, consider a closed cylindrical sheet illuminated by an  $E$ -polarized wave. In terms of the cylindrical polar coordinates  $\rho$ ,  $\phi$ ,  $z$ , the sheet is defined as the surface  $\rho = a$  and the incident plane wave is assumed to have

$$\vec{E}^i = \hat{z} e^{-ik\rho \cos \phi}$$

By expanding the scattered and interior fields in cylindrical wave functions, the solution for each type of sheet can be obtained by mode matching. In particular, the interior field is

$$\vec{E}^{int} = \hat{z} \sum_{n=0}^{\infty} \epsilon_n (-i)^n A_n J_n(k\rho) \cos n\phi \quad (13)$$

where  $\epsilon_0 = 1$  and  $\epsilon_n = 2$ ,  $n > 0$ , and for a resistive sheet

$$A_n = \left\{ 1 + \frac{\pi ka}{2} \frac{Z}{R} J_n(ka) H_n^{(1)}(ka) \right\}^{-1} \quad (14)$$

For a conductive sheet

$$A_n = \left\{ 1 + \frac{\pi ka}{2} \frac{Y}{R^*} J_n'(ka) H_n^{(1)'}(ka) \right\}^{-1} \quad (15)$$

where the prime denotes differentiation with respect to  $ka$ , but for a combination sheet

$$A_n = \left( 1 - \frac{1}{4RR^*} \right) \left\{ 1 + \frac{1}{4RR^*} + \frac{\pi ka}{2} \frac{Z}{R} J_n(ka) H_n^{(1)}(ka) + \frac{\pi ka}{2} \frac{Y}{R^*} J_n'(ka) H_n^{(1)'}(ka) \right\}^{-1} \quad (16)$$

If (11) is satisfied the field interior to the combination sheet vanishes, showing that the sheet is then opaque, and we also observe that (14) and (15) can be obtained from (16) by taking the limits  $R^* \rightarrow \infty$  and  $R \rightarrow \infty$ , respectively. More importantly, however, the coefficient  $A_n$  for the combination sheet is not the sum of the coefficients for the individual sheets, which demonstrates the coupling.

#### IV. PLANAR SHEET

Although the sheets comprising a combination sheet are generally coupled, an exception occurs in the special case of a planar sheet. To prove this, let

$$\vec{E} = \vec{E}^i + \vec{E}^{(1)} + \vec{E}^{(2)}$$

where  $\vec{E}^{(1)}$  and  $\vec{E}^{(2)}$  are the electric fields radiated by the induced electric and magnetic currents, respectively. If  $\vec{H}^{(1)}$  and  $\vec{H}^{(2)}$  are the associated magnetic fields, the symmetry about a planar magnetic sheet implies

$$\hat{n} \times \{ \vec{H}^{(2)}(+)-\vec{H}^{(2)}(-) \} = 0$$

and

$$\hat{n} \times \vec{E}^{(2)}(\pm) = \pm \frac{1}{2} \vec{J}^*$$

Hence

$$\hat{n} \times \{ \vec{E}^{(2)}(+)+\vec{E}^{(2)}(-) \} = 0,$$

and when these expressions are substituted into the boundary condition (4) for a combination sheet, we find

$$\begin{aligned} \hat{n} \times \{ \hat{n} \times [ \vec{E}^i(+)+\vec{E}^{(1)}(+)+\vec{E}^i(-)+\vec{E}^{(1)}(-) ] \} \\ = -R\hat{n} \times \{ \vec{H}^{(1)}(+)-\vec{H}^{(1)}(-) \} \end{aligned}$$

which is simply the condition for the corresponding resistive sheet in isolation. Similarly, (8) reduces to the condition for a conductive sheet by itself, showing that for a planar combination sheet the resistive and conductive parts scatter independently of one another.

This is true for a plate of any (planar) configuration and it is therefore sufficient to restrict the development of analytical and/or numerical procedures to the simple case of a resistive plate. By application of the duality principle the solution for the corresponding conductive plate can be deduced, and the solution for the combination plate then follows by addition of the component solutions. Thus, for a planar plate, we can achieve the added generality of a combination sheet without any increase in complexity. The resulting plate is partially transparent unless (11) is satisfied, which represents the special case when the impedance boundary condition is applied.

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```

1 /* function definitions */
2 #include <math.h>
3 double darea(), area(), sumang();
4 /* macro definitions */
5 #define Darray(Ara,I1,I2,L1,L2) Ara[(I1)+(I2)*(L1)] /* Macro to generate other\
6 macros to mimic fortran\
7 arrays */
8 #define Mnumpoi 100 /* maximum number of points */
9 #define Mnumtri 100 /* maximum number of triangular patches */
10 #define Mnumatri 10 /* maximum number of triangles which may share a \
11 common point, 6 is average for internal points, 8 accounts for\
12 most schemes, thus 10 is a reasonable upper bound */
13 #define True 1 /* value of logical true */
14 #define False 0 /* value of logical false */
15 #define Tri(J1,J2) Darray(tri,J1,J2,Mnumatri,Mnumpoi) /* set up tri as two\
16 dimensional array with limits (Mnumatri, Mnumpoi) */
17 #define Poi1(J1,J2) Darray(poi1,J1,J2,Mnumatri,Mnumpoi) /* set up poi1 as two\
18 dimensional array with limits (Mnumatri, Mnumpoi) */
19 #define Poi2(J1,J2) Darray(poi2,J1,J2,Mnumatri,Mnumpoi) /* set up poi2 as two\
20 dimensional array with limits (Mnumatri, Mnumpoi) */
21 #define Poi(J1,J2) Darray(poi,J1,J2,Mnumtri,3) /* set up poi as two dimensional\
22 array with limits (Mnumtri,3) */
23 #define Matrix(J1,J2) Darray(matrix,J1,J2,Mnumpoi,Mnumpoi) /* set up matrix as\
24 two dimensional array with limits (Mnumpoi,Mnumpoi) */
25 #define Cmatrix(J1,J2) Darray(cmatrix,J1,J2,Mnumpoi,Mnumpoi) /* complex\
26 version of Matrix, used with the complex\
27 structure */
28 #define Cvmat(J1,J2) Darray(cvmat,J1,J2,2*Mnumtri,2*Mnumpoi) /* define Cvmat,\
29 used to store centroid-vertex contributions */
30 #define Vvmat(J1,J2) Darray(vvmat,J1,J2,2*Mnumpoi,2*Mnumpoi) /* define Vvmat,\
31 used to store vertex-vertex contributions */
32 struct complex {
33     double real;
34     double imag;
35 };
36 /*
37 /*
38 /*
39 /*
40 /*
41 int flagsym; /* flagsym may assume values of 0,1,2, or 3. Flagsym is used
42 by low level routines to incorporate symmetry in a manner
43 invisible to the rest of the program.
44 0 - indicates no symmetry
45 1 - indicates object possesses mirror symmetry about x=0
46 2 - indicates object possesses mirror symmetry about y=0
47 3 - indicates object possesses mirror symmetry about x=0 and y=0
48 Flagsym is set at the beginning of the main program and after
49 that is never changed
50 int flagsyms; /* flagsyms is used in conjunction with flagsym to generate
51 mirror images of the source patches while calculating
52 contributions to the field point. The initial object
53 description is assumed to lie in the first quadrant, however
54 if flagsym is 0, this is not necessary. Flagsyms is always
55 less than or equal to flagsym, and may assume the values of
56 0,1,2, or 3. These values are given the following meanings:

```

```

57 0 - source patch is original patch (presumably first quadrant)
58 1 - source patch is in second quadrant
59 2 - source patch is in fourth quadrant
60 3 - source patch is in third quadrant */
61 int eof; /* end of file variable (=0 means end of file) */
62 int potflag; /* flag marks whether or not potentials have been computed
63 0 - potential has not been computed
64 1 - potential has been computed assuming x excitation
65 2 - potential has been computed assuming y excitation
66 3 - potential has been computed assuming z excitation */
67 struct {
68     double x[Mnumpoi];
69     double y[Mnumpoi];
70     struct complex res[Mnumpoi];
71     struct complex j [2*Mnumpoi];
72     struct complex jtotx[Mnumpoi];
73     struct complex jtoty[Mnumpoi];
74 }point; /* point is a structure which contains the locations of all
75 of the points used in defining the triangular patches. A point
76 number 0 is permitted as C defines arrays beginning with 0.
77 X and y are the coordinates of the points, j is the computed
78 current resulting from a single excitation with x components
79 listed first and y components displaced by Mnumpoi. jtotx and
80 jtoty contain the x and y components of the total current. */
81
82 struct {
83     int numatri[Mnumpoi];
84     int Tri(Mnumatri,Mnumpoi-1);
85     int Poi1(Mnumatri,Mnumpoi-1);
86     int Poi2(Mnumatri,Mnumpoi-1);
87 } apoint; /* apoint is a structure which contains lists of triangles
88 associated with each point. numatri contains the number of
89 triangles associated with each point; tri contains the list of
90 triangle numbers associated with each point; and poi1 and poi2
91 contain the other two vertices used in defining the triangle.
92 poi1 and poi2 are indices to point. tri is an index to
93 triang. */
94 struct {
95     struct {
96         double x[Mnumtri];
97         double y[Mnumtri];
98     } centroid;
99     int Poi(Mnumtri,3-1);
100     double poten[Mnumtri];
101     struct complex cpoten[Mnumtri]; /* complex version of poten */
102     struct complex ctriang; /* triang is used to solve the scattering problem with z
103 excitation. centroid .x and .y contain the coordinates
104 of the centroid of each triangle. poi contains the list of
105 points (vertices) associated with each triangle, and is an
106 index to point. poten is the potential of each triangle as
107 determined from solution of the matrix problem. */
108     double Matrix(Mnumpoi,Mnumpoi-1); /* This is "THE" matrix. Trivial points
109 (ie, those which have zero potential from
110 symmetry considerations) are skipped when
111 reading or filling the matrix, which is
112 always done sequentially. */

```

```

113 struct complex Cmatrix(Mnumpoi,Mnumpoi-1); /* complex version of Matrix */
114 struct complex Cvmat(2*Mnumtri,2*Mnumpoi-1);
115 struct complex Vmat(2*Mnumpoi,2*Mnumpoi-1);
116 struct complex evec[2*Mnumtri];
117 struct complex evec[2*Mnumpoi];
118 double fvect[Mnumpoi]; /* fvect is the forcing vector for the matrix problem
119 and after solution of the matrix problem contains
120 the solution vector. */
121 struct complex cfvect[Mnumpoi]; /* complex version of fvect */
122 int mnumpoi; /* This is the total number of points. Points are assumed to be
123 numbered sequentially from 0. mnumpoi <= Mnumpoi. */
124 int mnumtri; /* This is the total number of triangles. Triangles are assumed
125 to be numbered sequentially from 0. mnumtri <= Mnumtri. */
126 union {
127     char str[2];
128     char let;
129     } com;
130 /* This is the first character of each input line, and is
131 interpreted as a command. Valid commands are:
132 d - display linkup of points and triangles
133 and display potentials if defined
134 e - specify direction of exciting field,
135 and solve the resultant matrix problem.
136 g - graph potentials of points/triangles
137 h - enter heading, ie, a descriptive one line title.
138 m - enter material parameters of plate: t and tau.
139 p - enter coordinates of next point
140 r - regenerate matrix problem using finer mesh
141 s - define symmetry to be assumed in solving problem
142 t - enter definition of next triangle
143 char hedstr[82]; /* contains one line heading, description of data */
144 double dYk;
145 double dYZ = 376.7; /* impedance of free space */
146 double t; /* Thickness of the plate */
147 double tau; /* permittivity of the plate */
148 double tau; /* imaginary part of the permittivity. This variable is also
149 used as a flag: if tau is zero, computations are performed
150 assuming "tau" is purely real; if tau is non-zero, the routines
151 appropriate for a complex tau are invoked */
152 double dipmom; /* contains the real part of the computed dipole moment */
153 double dipmomi; /* contains the imaginary part of the computed dipole moment */
154 double Epsilon = 1e-9; /* A very small number, used for approximate equality */
155 double P1 = 3.1415926535; /* P1 */
156 double dYxr,dYxi,dYyr,dYyi; /* used in interface */
157 double theta, phi, alpha; /* specifies the direction of propagation (theta
158 and phi), and the polarization of the electric
159 vector with alpha. alpha is specified in the
160 same manner as phi. */
161 double rtheta, rphi, ralpha; /* contains angles in radians */
162 /*****
163 */
164 /* M A I N P R O G R A M
165 */
166 /* This is a program which calculates scattering by an arbitrarily shaped,
167 /* thin, flat, resistive plate. Excitation may be specified in the x, y,
168 /* or z directions. The plate is made up of an arbitrary number (nominally

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169 /* less than 50) of triangular patches, upon which a method of moments
170 /* solution is obtained. Contributions from each patch is calculated via
171 /* surface integrals which are evaluated analytically, thus contributions
172 /* from each patch is obtained exactly (at least to 10 plus digits). The
173 /* only approximations which are made are that the potential varies linearly
174 /* with z inside the plate, and the division of the plate into triangular
175 /* patches, inside of which the field varies linearly with x and y. The
176 /* shape and size of the triangular patches are completely arbitrary, and it
177 /* is noted that the patches need not be contiguous.
178 /*
179 /******
180 main() {
181     hedstr[0] = '\0';
182     for(eof=scanf("%1s",com.str);eof == 1;) {
183         switch (com.let) {
184             case 'p':
185             case 'p.':
186             case 't':
187             case 't.':
188                 rdata(); /* read in the data */
189                 continue;
190             case 'R':
191             case 'r':
192                 rres(); /* read in the resistivity of each point */
193                 continue;
194             case 'H':
195             case 'h':
196                 gethed();
197                 break;
198             case 'E':
199             case 'e':
200                 suplup(); /* read in direction of excitation
201                 and solve the resulting matrix problem */
202                 default:
203                     printf("%c is an invalid command\n",com.let);
204                     while(scanf("%c",com.str),com.let != '\n');
205                     break;
206                 }
207             eof=scanf("%1s",com.str);
208         }
209     }
210 }
211 /******
212 /* ROUTINE: darea(1)
213 /*
214 /* darea is called by suplup to calculate the area of a triangle. darea
215 /* accomplishes this with a call to area. The argument i specifies the
216 /* triangle number.
217 /*
218 /******
219 double darea(1)
220 int i; /* pointer to triangle */
221 {
222     return(area(point.x[triang.Poi(1,0)],point.y[triang.Poi(1,0)],
223     point.x[triang.Poi(1,1)],point.y[triang.Poi(1,1)],

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225     point.x[triang.Poi(1,2)].point.y[triang.Poi(1,2)]];
226 }
227 /*****
228 /*
229 /* ROUTINE:  suplup
230 /*
231 /* suplup is called by the main program to read in excitation, decompose the
232 /* problem into several symmetric problems if appropriate and possible, and
233 /* compute the current induced on the resistive plate.
234 /*
235 /*****
236 suplup() {
237     int i, j, 12; /* loop variables */
238     scanf ("%le %le %le", &dyk, &theta, &phi, &alpha);
239     rtheta=theta*Pi/180.;
240     rphi=phi*Pi/180.;
241     ralpha=alpha*Pi/180.;
242     for (i=0; i<mnnumtri; i++) {
243         evec[i].real = cos(dyk*(triang.centroid.x[i]*sin(rtheta) *
244             cos(rphi)+triang.centroid.y[i]*sin(rtheta)*sin(rphi))) *
245             sqrt(sin(rtheta)*sin(rtheta)*sin(rphi)*sin(rphi)+cos(rtheta) *
246                 cos(rtheta)) *
247                 cos(ralpha);
248         evec[i].imag = sin(dyk*(triang.centroid.x[i]*sin(rtheta) *
249             cos(rphi)+triang.centroid.y[i]*sin(rtheta)*sin(rphi))) *
250             sqrt(sin(rtheta)*sin(rtheta)*sin(rphi)*sin(rphi)+cos(rtheta) *
251                 cos(rtheta)) *
252                 cos(ralpha);
253         evec[i+mnumtri].real =cos(dyk*(triang.centroid.x[i]*sin(rtheta) *
254             cos(rphi)+triang.centroid.y[i]*sin(rtheta)*sin(rphi))) *
255             sqrt(sin(rtheta)*sin(rtheta)*cos(rphi)*cos(rphi)+cos(rtheta) *
256                 cos(rtheta)) *
257                 sin(ralpha);
258         evec[i+mnumtri].imag =sin(dyk*(triang.centroid.x[i]*sin(rtheta) *
259             cos(rphi)+triang.centroid.y[i]*sin(rtheta)*sin(rphi))) *
260             sqrt(sin(rtheta)*sin(rtheta)*cos(rphi)*cos(rphi)+cos(rtheta) *
261                 cos(rtheta)) *
262                 sin(ralpha);
263         for (l2=0; l2<mnumpoi; l2++) { /* fill /cmat */
264             cpcon(l, l2);
265         }
266     }
267     cv2vv();
268     solvem(2*mnumpoi); /* using Vvmat, evec, and point.j */
269     for (i=0; i<mnumpoi; i++) {
270         point.jtotx[i].real=point.j[i].real;
271         point.jtotx[i].imag=point.j[i].imag;
272         point.jtoty[i].real=point.j[i+mnumpoi].real;
273         point.jtoty[i].imag=point.j[i+mnumpoi].imag;
274     }
275     printy();
276 }
277 /*****
278 /*
279 /* ROUTINE:  cv2vv
280 /*

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```

281 /* cv2vv is called by supllup to convert from the centroid vertex matrix to */
282 /* the vertex matrix. */
283 /*
284 /*****
285 cv2vv() {
286     int i,j,j2; /*loop variables*/
287     double sarea,tarea; /* stores area of triangles*/
288     for (j=0;j<mnumpoi;j++) { /* convert to point-point */
289         evvec[j+mnumpoi].real=evvec[j].imag=
290         j2<apoint.numatri[j];j2++) {
291             tarea=darea(apoint.Tri(j2,j));
292             sarea += tarea;
293             evvec[j].real += tarea*evvec[apoint.Tri(j2,j)].real;
294             evvec[j].imag += tarea*evvec[apoint.Tri(j2,j)].imag;
295             evvec[j+mnumpoi].real += tarea*
296             evvec[apoint.Tri(j2,j)+mnumtri].real;
297             evvec[j+mnumpoi].imag += tarea*
298             evvec[apoint.Tri(j2,j)+mnumtri].imag;
299         }
300     }
301     evvec[j].real /= sarea;
302     evvec[j].imag /= sarea;
303     evvec[j+mnumpoi].real /= sarea;
304     evvec[j+mnumpoi].imag /= sarea;
305     for (i=0;i<mnumpoi;i++) {
306         for (j2=0,sarea=0,Vvmat(1,j).real=Vvmat(1,j).imag=
307             Vvmat(1,j+mnumpoi).real=Vvmat(1,j+mnumpoi).imag=
308             Vvmat(1+mnumpoi,j).real=Vvmat(1+mnumpoi,j).imag=
309             Vvmat(1+mnumpoi,j+mnumpoi).real=
310             Vvmat(1+mnumpoi,j+mnumpoi).imag=0;
311             j2<apoint.numatri[i];j2++) {
312             tarea=darea(apoint.Tri(j2,i));
313             sarea += tarea;
314             Vvmat(1,j).real += tarea*Cvmat(apoint.Tri(j2,i),j).real;
315             Vvmat(1,j).imag += tarea*Cvmat(apoint.Tri(j2,i),j).imag;
316             Vvmat(1,j+mnumpoi).real += tarea*
317             Cvmat(apoint.Tri(j2,i),j+mnumpoi).real;
318             Vvmat(j+mnumpoi,i).imag += tarea*
319             Cvmat(apoint.Tri(j2,i),j+mnumpoi).imag;
320             Vvmat(1+mnumpoi,j).real += tarea*
321             Cvmat(apoint.Tri(j2,i)+mnumtri,j).real;
322             Vvmat(1+mnumpoi,j).imag += tarea*
323             Cvmat(apoint.Tri(j2,i)+mnumtri,j).imag;
324             Vvmat(1+mnumpoi,j+mnumpoi).real += tarea*
325             Cvmat(apoint.Tri(j2,i)+mnumtri,j+mnumpoi).real;
326             Vvmat(1+mnumpoi,j+mnumpoi).imag += tarea*
327             Cvmat(apoint.Tri(j2,i)+mnumtri,j+mnumpoi).imag;
328         }
329     }
330     Vvmat(1,j).real /= sarea;
331     Vvmat(1,j).imag /= sarea;
332     Vvmat(1,j+mnumpoi).real /= sarea;
333     Vvmat(1,j+mnumpoi).imag /= sarea;
334     Vvmat(1+mnumpoi,j).real /= sarea;
335     Vvmat(1+mnumpoi,j).imag /= sarea;
336     Vvmat(1+mnumpoi,j+mnumpoi).real /= sarea;
337     Vvmat(1+mnumpoi,j+mnumpoi).imag /= sarea;
338 }
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337 }
338 }
339 }
340 /*****
341 /* ROUTINE:  cpcon(i,12)
342 /*
343 /*
344 /* cpcon calculates the elements of the matrix in terms of the contribution
345 /* of a source point to a centroid.  The source point contribution is broken
346 /* up into triangle contributions, which are analyzed by calling contrib.
347 /* cpcon is the only routine which calls contrib, and thus is the
348 /* interface between the control program, written by Dave Ksienski, and the
349 /* matrix element numerical evaluation routines, written by Joe Burns.  cpcon**
350 /* also calculates the contribution to the self cell from the RJ term.
351 /*
352 /*****
353 cpcon(1,12)
354 int i,12;
355 {
356     struct complex rsum; /* holds values of resistance at centroid */
357     int iloop; /* loop variable */
358     for (Cvmat(1,12).real=Cvmat(1,12).imag=Cvmat(1,12+mnumpoi).real=
359           Cvmat(1,12+mnumpoi).imag=Cvmat(1+mnumtri,12).real=
360           Cvmat(1+mnumtri,12).imag=Cvmat(1+mnumtri,12+mnumpoi).real=
361           iloop=0;iloop<apoint.numtri[12];iloop++) {
362         contrib(triang.centroid.x[1],triang.centroid.y[1],point.x[12],
363               point.y[12],point.x[apoint.Poi1(1loop,12)],
364               point.y[apoint.Poi1(1loop,12)],point.x[apoint.Poi2(1loop,12)],
365               point.y[apoint.Poi2(1loop,12)]);
366     }
367     /* >>
368     /* >> contrib returns values through the external variables dYabc, where
369     /* >> a=x or y and represents the direction of the field
370     /* >> b=x or y and represents the direction of the current
371     /* >> c=r or i and represents either the real or imaginary part
372     /* >>
373     Cvmat(1,12).real+=dYxxr;
374     Cvmat(1,12).imag+=dYxxi;
375     Cvmat(1,12+mnumpoi).real+=dYxyr;
376     Cvmat(1,12+mnumpoi).imag+=dYxyi;
377     Cvmat(1+mnumtri,12).real+=dYyxr;
378     Cvmat(1+mnumtri,12).imag+=dYyxi;
379     Cvmat(1+mnumtri,12+mnumpoi).real+=dYyyr;
380     Cvmat(1+mnumtri,12+mnumpoi).imag+=dYyyi;
381     if(apoint.Tri(1loop,12) == 1) { /* self cell contribution */
382         rsum.real=(point.res[12].real+
383                   point.res[apoint.Poi1(1loop,12)].real+
384                   point.res[apoint.Poi2(1loop,12)].real)/3;
385         rsum.imag=(point.res[12].imag+
386                   point.res[apoint.Poi1(1loop,12)].imag+
387                   point.res[apoint.Poi2(1loop,12)].imag)/3;
388         Cvmat(1,12).real+=rsum.real;
389         Cvmat(1,12).imag+=rsum.imag;
390         Cvmat(1+mnumtri,12+mnumpoi).real+=rsum.real;
391         Cvmat(1+mnumtri,12+mnumpoi).imag+=rsum.imag;
392     }

```



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393 }
394 }
395 /*****
396 /*
397 /* ROUTINE: rres
398 /*
399 /* rres is called by the main program to read in the resistivity associated
400 /* with each point. The resistivity is assumed to be complex and linearly
401 /* varying. Upon encountering a non-"r" command rres retruns to the main
402 /* program.
403 /*
404 /*****
405 rres() {
406 int i,j;
407 int inumb; /* next point */
408 do {
409 switch (com.let) {
410 case 'R':
411 case 'r':
412 scanf("%d",&inumb);
413 scanf("%le %le",&point.res[inumb].real,
414 &point.res[inumb].imag);
415 continue;
416
417 default:
418 return;
419 }
420 } while (scanf("%is",com.str) == 1);
421 }
422 /*****
423 /*
424 /* ROUTINE: ddata
425 /*
426 /* ddata is called by the main program to display data. ddata display
427 /* locations of points, connections of points, and potentials of points if
428 /* they have been computed. ddata also displays status of various flags
429 /* which indicate symmetries of plate and direction of excitation.
430 /*
431 /*****
432 printy() {
433 int i,j; /* loop variables */
434 printf("%s\n",hedstr);
435 printf("k=%lf, theta=%lf, phi=%lf, alpha=%lf\n",dYk,theta,phi,alpha);
436 for (i=0; i<mnumpoi; i++) {
437 printf("point # %d is located at x = %lf, y = %lf\n",i,point.x[i],
438 point.y[i]);
439 printf(" and has current jx=%lf +i%lf, jy=%lf +i%lf\n",
440 point.jtotx[i].real,point.jtotx[i].imag,point.jtoty[i].real,
441 point.jtoty[i].imag);
442 printf(" and has resistivity R=%lf +i%lf\n",
443 point.res[i].real,point.res[i].imag);
444 printf("point %d is associated with points and triangles (tri,P1,P2)\n"
445 '.i');
446 for (j=0; j<apoint.numatri[i];j++) {
447 printf(" (%d,%d)",apoint.Tri(j,i), apoint.Poi1(j,i),
448 apoint.Poi2(j,i));

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449         if (j%6 == 5 || j == apoint.numatri[i]-1) printf("\n");
450     }
451 }
452 }
453 /*****
454 /* ROUTINE: rdata
455 /*
456 /* rdata is called by the main program to read in point and triangle
457 /* definitions. Upon encountering a non- "p" or "t" command, rdata calls
458 /* ldata to link the data, and then returns to the main program.
459 /*
460 /*
461 /*****
462 rdata() {
463     int i; /* loop variable */
464     int inumb; /* number of next point or triangle */
465     do {
466         switch (com.let) {
467             case 'p':
468                 scanf("%d", &inumb);
469                 scanf("%le %le", point.x+inumb, point.y+inumb);
470                 mnumpoi=inumb+1;
471                 continue;
472             case 'T':
473                 scanf("%d", &inumb);
474                 for (i=0; i<3; i++) scanf("%d", &triang.Poi(inumb, i));
475                 mnumtri=inumb+1;
476                 continue;
477             default:
478                 ldata();
479                 return;
480         }
481     } while (scanf("%is", com.str) == 1);
482 }
483 /*****
484 /* ROUTINE: ldata
485 /*
486 /* ldata links all information concerning points and triangles. This
487 /* information is needed to precisely define each patch on the plate.
488 /*
489 /*
490 /*****
491 ldata() {
492     /* loop variables */
493     int i, j; /* scratch variable */
494     int isl;
495     for (i=0; i<mnumpoi; i++) apoint.numatri[i]=0;
496     for (i=0; i<mnumtri; i++) {
497         for (triang.centroid.x[i]=triang.centroid.y[i]=0; j<3; j++) {
498             isl=triang.Poi(i, j);
499             triang.centroid.x[i] += point.x[isl]/3;
500             triang.centroid.y[i] += point.y[isl]/3;
501             apoint.Tri(apoint.numatri[isl], isl) = i;
502             apoint.Poi((apoint.numatri[isl], isl) = triang.Poi(i, (j+1)%3);
503         }
504     }

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```

505 apoint.Poi2(apoint.numatri[isi]++,isi) = triang.Poi(1,(j+2)%3);
506 }
507 return;
508 }
509 /*****
510 /* ROUTINE: solvem(N)
511 /*
512 /* solvem is used to solve the matrix problem. The matrix and forcing vector**/
513 /* are created in xsolv or ysolv. N is the dimension of the vector. solvem **/
514 /* solves the matrix problem by calling the two fortran routines dgeco and **/
515 /* dgesl which perform a decomposition and back substitution. solvem is the **/
516 /* only c routine which calls a fortran routine.
517 /*
518 /*
519 /*
520 /*****
521 solvem(N)
522 int N; /* N is the order of the matrix stored in the array matrix. N is less
523 than or equal to isize */
524 {
525 int i,j;
526 int isize,job; /* arguments for fortran routines, isize is the size of the
527 array matrix, job (=0) indicates type of matrix problem */
528 int ipvt[2*Mnumpoi]; /* an array used by the fortran routines to store the
529 pivoting vector */
530 double rcond; /* the condition number of the matrix. */
531 double z[2*Mnumpoi*2]; /* scratch vector, lengthened for complex case */
532 isize=2*Mnumpoi;
533 job=0;
534 for(i=0;i<13;i++){
535 for(j=0;j<13;j++){
536 printf("%lf %lf\n",Vvmat(1,j));
537 }
538 }
539 for(i=0;i<N+1;i++) {
540 point.j[i].real=evec[i].real;
541 point.j[i].imag=evec[i].imag;
542 }
543 cgeco (vpmat,&isize,&N,ipvt,&rcond,z);
544 printf("condition number is %e\n",1/rcond);
545 cgesl_ (vpmat,&isize,&N,ipvt,point.j,&job);
546 }
547 /*****
548 /* ROUTINE: gethed
549 /*
550 /* gethed is called by the main program to get the heading of the data.
551 /* gethed fills hedstr with the remainder of the line (the entire line
552 /* except for the letter H which must be in column 1.
553 /*
554 /*
555 /*****
556 gethed() {
557 int i; /* loop variable */
558 for (i=0; (hedstr[i]=getchar()) != '\n'; i++);
559 hedstr[i] = '\0';
560 return;

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561 }
562 /*****
563 */
564 /* ROUTINE: area
565 */
566 /* area is called by graphp to calculate the area of a triangle. This is
567 /* needed in the computation of the area coordinates.
568 */
569 /*****
570 double area(x1,y1,x2,y2,x3,y3)
571 double x1,y1,x2,y2,x3,y3; /* These are the coordinates of the three
572 /* points which delimit the triangle */
573 {
574 return(fabs(x2*y3-y2*x3-x1*y3+y1*x3+x1*y2-y1*x2)/2);
575 }
576 #include <math.h>
577 double dYk,dVz;
578 double Rk_re,Rk_1m,Rkx_re,Rkx_1m,Rky_re,Rky_1m;
579 double Dx2rk_re,Dx2rk_1m,Dx2rkk_re,Dx2rkk_1m,Dx2rky_re,Dx2rky_1m;
580 double Dy2rk_re,Dy2rk_1m,Dy2rkk_re,Dy2rkk_1m,Dy2rky_re,Dy2rky_1m;
581 double Dxyrk_re,Dxyrk_1m,Dxyrkk_re,Dxyrkk_1m,Dxyrky_re,Dxyrky_1m;
582 double IT1,IT2,IT3,IT4,IT5,IT6,IT7,IT8,IT9;
583 double DX2IT1,DY2IT1,DXYIT1;
584 double DX2IT2,DY2IT2,DXYIT2;
585 double DX2IT3,DY2IT3,DXYIT3;
586 double DX2IT7,DY2IT7,DXYIT7;
587 double DX2IT8,DY2IT8,DXYIT8;
588 double DX2IT9,DY2IT9,DXYIT9;
589 extern double dVxxr,dVxyr,dVxxi,dVxyi,dVxxr,dVxyr,dVxxi,dVxyi;
590
591 contrib(xo,yo,xs1,ys1,xs2,ys2,xs3,ys3)
592
593
594
595
596
597
598
599 /*****
600 */
601 /* This routine calculates the finite element contribution to the x
602 /* component of the current or the y component for x or y excitation
603 /* given the vertices of the source triangle xs1,ys1 xs2,ys2 xs3,ys3 and
604 /* the observation point. The finite element approximating the current
605 /* varies linearly over the triangular subdomain and is assumed to be
606 /* one at xs1,ys1 and zero at xs2,ys2 and xs3,ys3.
607 */
608 /*****
609 */
610 /* xo x coordinate of the observation point
611 /* yo y coordinate of the observation point
612 /* xs1 x coordinate of vertice 1 of the source triangle
613 /* ys1 y coordinate of vertice 1 of the source triangle
614 /* xs2 x coordinate of vertice 2 of the source triangle
615 /* ys2 y coordinate of vertice 2 of the source triangle
616 /* xs3 x coordinate of vertice 3 of the source triangle

```

```

617 /* ys3 y coordinate of vertice 3 of the source triangle */
618 /* a x coefficient of the finite element */
619 /* b y coefficient of the finite element */
620 /* c constant coefficient of the finite element */
621 /*
622 /******
623 /*
624 /* EXTERNAL VARIABLES
625 /*
626 /******
627 /* dYxxr real part of the x component of the current for x excitation */
628 /* dYxxi imag part of the x component of the current for x excitation */
629 /* dYxyr real part of the y component of the current for x excitation */
630 /* dYxyi imag part of the y component of the current for x excitation */
631 /* dYxrr real part of the x component of the current for y excitation */
632 /* dYxri imag part of the x component of the current for y excitation */
633 /* dYyrr real part of the y component of the current for y excitation */
634 /* dYyri imag part of the y component of the current for y excitation */
635 /*
636 /* IT1 is the integral of 1/R over the triangle */
637 /* IT2 is the integral of x/R over the triangle */
638 /* IT3 is the integral of y/R over the triangle */
639 /* IT4 is the integral of i. over the triangle */
640 /* IT5 is the integral of x over the triangle */
641 /* IT6 is the integral of y over the triangle */
642 /* IT7 is the integral of R over the triangle */
643 /* IT8 is the integral of xR over thr triangle */
644 /* IT9 is the integral of yR over the triangle */
645 /* DX2IT1 is second derivative of IT1 with respect to x */
646 /* DX2IT1 is second derivative of IT1 with respect to y */
647 /* DXYIT1 is derivative of IT1 with respect to x and y */
648 /* DX2IT2 is second derivative of IT2 with respect to x */
649 /* DX2IT2 is second derivative of IT2 with respect to y */
650 /* DX2IT3 is second derivative of IT3 with respect to x */
651 /* DX2IT3 is second derivative of IT3 with respect to y */
652 /* DXYIT3 is derivative of IT3 with respect to x and y */
653 /* DX2IT7 is second derivative of IT7 with respect to x */
654 /* DX2IT7 is second derivative of IT7 with respect to y */
655 /* DXYIT7 is derivative of IT7 with respect to x and y */
656 /* DX2IT8 is second derivative of IT8 with respect to x */
657 /* DX2IT8 is second derivative of IT8 with respect to y */
658 /* DXYIT8 is derivative of IT8 with respect to x and y */
659 /* DX2IT9 is second derivative of IT9 with respect to x */
660 /* DX2IT9 is second derivative of IT9 with respect to y */
661 /* DXYIT9 is derivative of IT9 with respect to x and y */
662 /* Rk_re real part of the rational kernel */
663 /* Rk_im imag part of the rational kernel */
664 /* Rkx_re real part of x times the rational kernel */
665 /* Rkx_im imag part of x times the rational kernel */
666 /* Rky_re real part of y times the rational kernel */
667 /* Rky_im imag part of y times the rational kernel */
668 /* Dx2rk_re real part of second derivative with respect to x of
669 /* the rational kernel */
670 /* Dx2rk_im imag part of second derivative with respect to x of
671 /* the rational kernel */
672 /*

```

```

673 /* Dx2rkx_re real part of x times second derivative with respect to x */
674 /* of the rational kernel */
675 /* Dx2rkx_im imag part of x times second derivative with respect to x */
676 /* of the rational kernel */
677 /* Dx2rky_re real part of y times second derivative with respect to x */
678 /* of the rational kernel */
679 /* Dx2rky_im imag part of y times second derivative with respect to x */
680 /* of the rational kernel */
681 /* Dy2rk_re real part of second derivative with respect to y of */
682 /* the rational kernel */
683 /* Dy2rk_im imag part of second derivative with respect to y of */
684 /* the rational kernel */
685 /* Dy2rkx_re real part of x times second derivative with respect to y */
686 /* of the rational kernel */
687 /* Dy2rkx_im imag part of x times second derivative with respect to y */
688 /* of the rational kernel */
689 /* Dy2rky_re real part of y times second derivative with respect to y */
690 /* of the rational kernel */
691 /* Dy2rky_im imag part of y times second derivative with respect to y */
692 /* of the rational kernel */
693 /* Dxyrk_re real part of derivative with respect to x and y of */
694 /* the rational kernel */
695 /* Dxyrk_im imag part of derivative with respect to x and y of */
696 /* the rational kernel */
697 /* Dxyrkx_re real part of x times derivative with respect to x and y */
698 /* of the rational kernel */
699 /* Dxyrkx_im imag part of x times derivative with respect to x and y */
700 /* of the rational kernel */
701 /* Dxyrky_re real part of y times derivative with respect to x and y */
702 /* of the rational kernel */
703 /* Dxyrky_im imag part of y times derivative with respect to x and y */
704 /* of the rational kernel */
705 /* dYk wavenumber */
706 /* dYZ impedance */
707 /*
708 /******
709
710 double a,b,c,k,k2,PI;
711 double ikrnl_re,ikrnl_im,ixyk_re,ixyk_im,ix2k_re,ix2k_im,iy2k_re,iy2k_im;
712
713 k=dYk;
714 k2=k*k/2.;
715 PI=3.1415926535;
716
717 /******
718 /*
719 /* Call routines numer and analyt to calculate external variables */
720 /*
721 /******
722
723 analyt(xo,yo,xs1,ys1,xs2,ys2,xs3,ys3);
724
725 numer(xo,yo,xs1,ys1,xs2,ys2,xs3,ys3);
726
727 /******
728 /*

```

```

729 /* Calculate coefficients of finite element
730 /*
731 /******
732 a=(ys2-ys3)/((xs1-xs2)*(ys2-ys3)-(xs2-xs3)*(ys1-ys2));
733
734 b=(xs3-xs2)/((xs1-xs2)*(ys2-ys3)-(xs2-xs3)*(ys1-ys2));
735
736 c=((xs2-xs3)*ys2-(ys2-ys3)*xs2)/((xs1-xs2)*(ys2-ys3)-(xs2-xs3)*(ys1-ys2));
737
738 /******
739 /* Calculate integrals of current over the triangle
740 /*
741 /*
742 /*
743 /******
744
745
746
747
748
749
750
751
752
753
754
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757
758
759
760
761
762
763
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781
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783
784

```

```

785 dYyxi=dYxyi;
786 }
787
788
789
790
791
792 analyt(xo,yo,xs1,ys1,xs2,ys2,xs3,ys3)
793
794 double xo,yo,xs1,ys1,xs2,ys2,xs3,ys3;
795
796 {
797 /*****
798 /* Calculate the contribution of a particular triangle given its vertices
799 /* x[1],y[1] x[2],y[2] x[3],y[3] and the field point xo,yo
800 /*
801 /*
802 /* List of Variables:
803 /*
804 /* x[n] x coordinates of the vertices of the triangle
805 /* y[n] y coordinates of the vertices of the triangle
806 /* xo x coordinate of the field point
807 /* yo y coordinate of the field point
808 /* ai[n] slopes of lines through segments
809 /* alpi[n] 1./sqrt(1.+ai**2)
810 /* gln] ai[n]*qi[n]
811 /* bli[n] y-intercept of lines through segments
812 /* li[n] length of ith segment
813 /* cln] constant related to the parameterization
814 /* exi[n] indicates sense of x direction along integration path
815 /* eyi[n] indicates sense of y direction along integration path
816 /* Dxi[n] derivative of x' with respect to path length parameter t
817 /* DyI[n] derivative of y' with respect to path length parameter t
818 /* A[n] term of R
819 /* B[n] term of R
820 /* C[n] term of R
821 /* C2[n] sqrt(C[n])
822 /* Rip[n] distance from observation point to plus end of ith segment
823 /* Rim[n] distance from observation point to minus end of ith segment
824 /* tip[n] path length to plus end of ith segment
825 /* tim[m] path length to minus end of ith segment
826 /* I1i[n] integral of 1./R over a segment
827 /* I2i[n] integral of t/R over a segment
828 /* I3i[n] integral of t**2/R over a segment
829 /* I4i[n] integral of R over a segment
830 /* I5i[n] integral of tR over a segment
831 /* I6i[n] integral of (t**2)R over a segment
832 /* sign temporary variable
833 /* t temporary variable
834 /* R temporary variable
835 /* xt[n] temporary variable
836 /* yt[n] temporary variable
837 /* ntrmx temporary variable
838 /* ntrmy temporary variable
839 /* dtrm tempoaray variable
840 /* delta[n] (4AC-BB)/(8C)

```



```

841 /* DXI11 is first derivative of I11 with respect to x
842 /* DYI11 is first derivative of I11 with respect to y
843 /* DX2I11 is second derivative of I11 with respect to x
844 /* DY2I11 is second derivative of I11 with respect to y
845 /* DXYI11 is derivative of I11 with respect to x and y
846 /* DXI21 is first derivative of I21 with respect to x
847 /* DYI21 is first derivative of I21 with respect to y
848 /* DX2I21 is second derivative of I21 with respect to x
849 /* DY2I21 is second derivative of I21 with respect to y
850 /* DXYI21 is derivative of I21 with respect to x and y
851 /* DXI31 is first derivative of I31 with respect to x
852 /* DYI31 is first derivative of I31 with respect to y
853 /* DX2I31 is second derivative of I31 with respect to x
854 /* DY2I31 is second derivative of I31 with respect to y
855 /* DXYI31 is derivative of I31 with respect to x and y
856 /* DXI41 is first derivative of I41 with respect to x
857 /* DYI41 is first derivative of I41 with respect to y
858 /* DX2I41 is second derivative of I41 with respect to x
859 /* DY2I41 is second derivative of I41 with respect to y
860 /* DXYI41 is derivative of I41 with respect to x and y
861 /* DXI51 is first derivative of I51 with respect to x
862 /* DYI51 is first derivative of I51 with respect to y
863 /* DX2I51 is second derivative of I51 with respect to x
864 /* DY2I51 is second derivative of I51 with respect to y
865 /* DXYI51 is derivative of I51 with respect to x and y
866 /* DXI61 is first derivative of I61 with respect to x
867 /* DYI61 is first derivative of I61 with respect to y
868 /* DX2I61 is second derivative of I61 with respect to x
869 /* DY2I61 is second derivative of I61 with respect to y
870 /* DXYI61 is derivative of I61 with respect to x and y
871 /* DXIT1 is first derivative of IT1 with respect to x
872 /* DYIT1 is first derivative of IT1 with respect to y
873 /* DXIT7 is first derivative of IT7 with respect to x
874 /* DYIT7 is first derivative of IT7 with respect to y
875 /* temp temporary variable
876 /* *****
877 /* *****
878 /* *****
879 /* *****
880 /* *****
881 /* IT1 is the integral of 1/R over the triangle
882 /* IT2 is the integral of x/R over the triangle
883 /* IT3 is the integral of y/R over the triangle
884 /* IT4 is the integral of 1. over the triangle
885 /* IT5 is the integral of x over the triangle
886 /* IT6 is the integral of y over the triangle
887 /* IT7 is the integral of R over the triangle
888 /* IT8 is the integral of xR over thr triangle
889 /* IT9 is the integral of yR over the triangle
890 /* DX2IT1 is second derivative of IT1 with respect to x
891 /* DY2IT1 is second derivative of IT1 with respect to y
892 /* DXYIT1 is derivative of IT1 with respect to x and y
893 /* DX2IT2 is second derivative of IT2 with respect to x
894 /* DY2IT2 is second derivative of IT2 with respect to y
895 /* DXYIT2 is derivative of IT2 with respect to x and y
896 /* DX2IT3 is second derivative of IT3 with respect to x

```

EXTERNAL VARIABLES

```

897 /* DY2IT3 is second derivative of IT3 with respect to y
898 /* DXYIT3 is derivative of IT3 with respect to x and y
899 /* DX2IT7 is second derivative of IT7 with respect to x
900 /* DY2IT7 is second derivative of IT7 with respect to y
901 /* DXYIT7 is derivative of IT7 with respect to x and y
902 /* DX2IT8 is second derivative of IT8 with respect to x
903 /* DY2IT8 is second derivative of IT8 with respect to y
904 /* DXYIT8 is derivative of IT8 with respect to x and y
905 /* DX2IT9 is second derivative of IT9 with respect to x
906 /* DY2IT9 is second derivative of IT9 with respect to y
907 /* DXYIT9 is derivative of IT9 with respect to x and y
908 /******
909
910 double a1[4], alpi[4], g1[4], bi[4], li[4], ci[4], exi[4], eyi[4], Dxi[4], Dyi[4];
911 double Rim[4], tip[4], tim[4], x[5], y[5], Rip[4], A[4], B[4], C[4], C2[4];
912 double li1[4], i2i[4], i3i[4], i4i[4], i5i[4], i6i[4], di[4];
913 double DXI1i[4], DYI1i[4], DX2I1i[4], DY2I1i[4], DXYI1i[4];
914 double DXI2i[4], DYI2i[4], DX2I2i[4], DY2I2i[4], DXYI2i[4];
915 double DXI3i[4], DYI3i[4], DX2I3i[4], DY2I3i[4], DXYI3i[4];
916 double DXI4i[4], DYI4i[4], DX2I4i[4], DY2I4i[4], DXYI4i[4];
917 double DXI5i[4], DYI5i[4], DX2I5i[4], DY2I5i[4], DXYI5i[4];
918 double DXI6i[4], DYI6i[4], DX2I6i[4], DY2I6i[4], DXYI6i[4];
919 double DXITI, DYITI, DXIT7, DYIT7;
920 double sign,t[3],R[3],xt[3],yt[3],ntrmx,ntrmy,dtrm,delta[4],temp;
921 double sqrt().log().fabs();
922 int n,m;
923
924 /******
925 /*
926 /* Calculate ai[n]. If segment is parallel to the y-axis, ai[n] would go
927 /* infinity; consequently, set ai[n] in this case to zero. This will not
928 /* affect any calculations since this feature of ai[n] has been accounted
929 /* for.
930 /*
931 /******
932
933 x[1]=xs1;
934 y[1]=ys1;
935 x[2]=xs2;
936 y[2]=ys2;
937 x[3]=xs3;
938 y[3]=ys3;
939 x[4]=x[1];
940 y[4]=y[1];
941
942 for(n=1;n<=3;n++)
943 {
944 if(x[n+1]==x[n])
945 ai[n]=0.;
946 else
947 ai[n]=(y[n+1]-y[n])/(x[n+1]-x[n]);
948 }
949
950 /******
951 /* Calculate alpi[n]. Note when ai[n] goes to infinity, qi[n] goes to zero. */
952

```

```

953 /*
954 /*****
955
956 for(n=1;n<=3;n++)
957 {
958     if(x[n+1] == x[n])
959         alpi[n]=0.;
960     else
961         alpi[n]=1.0/sqrt(1.0+ai[n]*ai[n]);
962 }
963
964 /*****
965 /*
966 /* Calculate g1[n]. Note when ai[n] goes to infinity, g1[n] goes to one.
967 /*
968 /*****
969
970 for(n=1;n<=3;n++)
971 {
972     if(x[n+1] == x[n])
973         g1[n]=1.;
974     else
975         g1[n]=ai[n]*alpi[n];
976 }
977
978 /*****
979 /*
980 /* Calculate b1[n], l1[n], C[n], B[n], A[n], ci[n], di[n], tip[n], tim[n], Rip[n]
981 /*
982 /*
983 /*****
984
985 for(n=1;n<=3;n++)
986 {
987     b1[n]=y[n]-ai[n]*x[n];
988     l1[n]=sqrt((x[n+1]-x[n])*(x[n+1]-x[n])+(y[n+1]-y[n])*(y[n+1]-y[n]));
989     C[n]=alpi[n]*alpi[n]+g1[n]*g1[n];
990     C2[n]=sqrt(C[n]);
991 }
992
993 c1[1]=x[1];
994 c1[2]=x[2]-alpi[2]*l1[1];
995 c1[3]=x[3]-alpi[3]*(l1[1]+l1[2]);
996
997 d1[1]=y[1];
998 d1[2]=y[2]-g1[2]*l1[1];
999 d1[3]=y[3]-g1[3]*(l1[1]+l1[2]);
1000
1001 tim[1]=l1[1];
1002 tim[2]=l1[1]+l1[2];
1003 tim[3]=l1[1]+l1[2]+l1[3];
1004
1005
1006
1007
1008

```

```

1009 tim[1]=0.;
1010 tim[2]=tip[1];
1011 tim[3]=tip[2];
1012
1013 for(n=1;n<=3;n++)
1014 {
1015
1016 B[n]=(-2.0)*(alpi[n]*(xo-ci[n])+gi[n]*(yo-di[n]));
1017
1018 A[n]=(xo-ci[n])*(xo-ci[n])+(yo-di[n])*(yo-di[n]);
1019
1020 Rip[n]=sqrt(C[n]*tip[n]*tip[n]+B[n]*tim[n]+A[n]);
1021
1022 Rim[n]=sqrt(C[n]*tim[n]*tim[n]+B[n]*tim[n]+A[n]);
1023
1024 }
1025
1026 /*****
1027 /* Calculate Dxi[n],Dyi[n]
1028 /*
1029 /*
1030 /*****
1031
1032 for(n=1;n<=3;n++)
1033 {
1034
1035 if( x[n+1] >= x[n] )
1036     ex1[n]=1.0;
1037 if( x[n+1] < x[n] )
1038     ex1[n]=(-1.0);
1039 if( y[n+1] >= y[n] )
1040     ey1[n]=1.0;
1041 if( y[n+1] < y[n] )
1042     ey1[n]=(-1.0);
1043
1044 Dxi[n]=ex1[n]*alpi[n];
1045
1046 Dy1[n]=ey1[n]*fabs(g1[n]);
1047 }
1048
1049 /*****
1050 /* Calculate integral of 1./R over a segment
1051 /* Calculate integral of t/R over a segment
1052 /* Calculate integral of t**2/R over a segment
1053 /* Calculate integral of R over a segment
1054 /* Calculate integral of tR over a segment
1055 /* Calculate integral of (t**2)R over a segment
1056 /*
1057 /*
1058 /*****
1059
1060 for(n=1;n<=3;n++)
1061 {
1062
1063 I11[n]=(1og(2.*C2[n]*R1p[n]+2.*C[n]*tip[n]+B[n])-log(2.*C2[n]*R1m[n]+2.
1064         *C[n]*tim[n]+B[n]))/C2[n];

```

```

1065 I21[n]=(R1p[n]-R1m[n])/C2[n]-B[n]*I11[n]/(2.*C[n]);
1066
1067 I31[n]=(((t1p[n]-3.*B[n]/(2.*C[n]))*R1p[n]-(t1m[n]-3.*B[n]/(2.*C[n]))
1068 *R1m[n])+(3.*B[n]*B[n]/(4.*C[n])-A[n])*I11[n])/(2.*C[n]);
1069
1070 I41[n]=((2.*C[n]*t1p[n]+B[n])*R1p[n]-(2.*C[n]*t1m[n]+B[n])*R1m[n])/(4.
1071 *C[n])+(4.*A[n]*C[n]-B[n]*B[n])*I11[n]/(8.*C[n]);
1072
1073 I61[n]=(powr(R1p[n],3)-powr(R1m[n],3))/(3.*C[n])-B[n]*I41[n]/(2.*C[n]);
1074
1075 I61[n]=(((t1p[n]-5.*B[n]/(6.*C[n]))*powr(R1p[n],3)-(t1m[n]-5.*B[n]/(6.*C[n])
1076 ))*powr(R1m[n],3)+(5.*B[n]*B[n]/(4.*C[n])-A[n])*I41[n])/(4.*C[n]);
1077
1078 }
1079
1080 /***** Calculate integral of 1/R over the triangle *****/
1081 /*
1082 /*
1083 /*
1084 /*****
1085
1086 IT1=0.;
1087 for(n=1;n<=3;n++)
1088 IT1=IT1+(Dy1[n]*(alpi1[n]*I21[n]-(xo-c1[n])*I11[n])-Dx1[n]*(g1[n]*I21[n]
1089 -yo-d1[n])*I11[n]);
1090
1091 /***** Calculate integral of x/R over the triangle *****/
1092 /*
1093 /*
1094 /*
1095 /*****
1096
1097 IT2=0.;
1098 for(n=1;n<=3;n++)
1099 IT2=IT2+(Dy1[n]*(alpi1[n]*alpi1[n]*I31[n]+alpi1[n]*(2.*c1[n]-xo)*I21[n]+c1[n]
1100 *(c1[n]-xo)*I11[n])-Dx1[n]*(g1[n]*alpi1[n]*I31[n]+(g1[n]*c1[n]
1101 +alpi1[n]*(d1[n]-yo))*I21[n]+c1[n]*(d1[n]-yo)*I11[n]);
1102
1103 IT2=IT2/2.0+xo*IT1/2.0;
1104
1105 /***** Calculate integral of y/R over the triangle *****/
1106 /*
1107 /*
1108 /*****
1109
1110 IT3=0.;
1111 for(n=1;n<=3;n++)
1112 IT3=IT3+(Dy1[n]*(alpi1[n]*g1[n]*I31[n]+(g1[n]*(c1[n]-xo)+alpi1[n]*d1[n])
1113 *I21[n]+d1[n]*(c1[n]-xo)*I11[n])-Dx1[n]*(g1[n]*I31[n]+g1[n]
1114 *(2.*d1[n]-yo)*I21[n]+d1[n]*(d1[n]-yo)*I11[n]);
1115
1116 IT3=IT3/2.0+yo*IT1/2.0;
1117
1118 /***** Calculate integral of 1 over the triangle *****/
1119 /*
1120 /*

```

```

1121 /*****
1122
1123 IT4=0.;
1124 for (n=1;n<=3;n++)
1125     IT4=IT4+((alpi[n]*Dyi[n]*Dxi[n]-gi[n]*tip[n]*tip[n]-tim[n]*tim[n])/2.0
1126     +(Dyi[n]*ci[n]-Dxi[n]*di[n])*(tip[n]-tim[n]))/2.0;
1127
1128 /*****
1129 /*
1130 /*      Calculate integral of x over the triangle      IT5
1131 /*
1132 /*****
1133
1134 IT5=0.;
1135 for (n=1;n<=3;n++)
1136     IT5=IT5+(Dyi[n]*(alpi[n]*alpi[n]*(powr(tip[n],3)-powr(tim[n],3))/3.0
1137     +alpi[n]*ci[n]*(tip[n]*tim[n]-tim[n]*tim[n])+ci[n]*ci[n]*(tip[n]
1138     -tim[n]))/2.0;
1139
1140 /*****
1141 /*
1142 /*      Calculate integral of y over the triangle      IT6
1143 /*
1144 /*****
1145
1146 IT6=0.;
1147 for (n=1;n<=3;n++)
1148     IT6=IT6+(Dxi[n]*(gi[n]*gi[n]*(powr(tip[n],3)-powr(tim[n],3))/3.0+gi[n]
1149     *di[n]*(tip[n]*tip[n]-tim[n]*tim[n])+di[n]*di[n]*(tip[n]-tim[n]))/2.0;
1150
1151 /*****
1152 /*
1153 /*      Calculate integral of R over the triangle      IT7
1154 /*
1155 /*****
1156
1157 IT7=0.;
1158 for (n=1;n<=3;n++)
1159     IT7=IT7+(Dyi[n]*(alpi[n]*I61[n]-(xo-ci[n])*I41[n]-Dxi[n]*(gi[n]*I51[n]
1160     -(yo-di[n])*I41[n]))/3.0;
1161
1162 /*****
1163 /*
1164 /*      Calculate integral of xR over the triangle      IT8
1165 /*
1166 /*****
1167
1168 IT8=0.;
1169 for (n=1;n<=3;n++)
1170     IT8=IT8+(Dyi[n]*(alpi[n]*alpi[n]*I61[n]+alpi[n]*(2.*ci[n]-xo)*I51[n]+ci[n]
1171     *(ci[n]-xo)*I41[n]-Dxi[n]*(gi[n]*alpi[n]*I61[n]+(gi[n]*ci[n]
1172     +alpi[n]*(di[n]-yo))*I61[n]+ci[n]*(di[n]-yo)*I41[n]));
1173
1174 IT8=IT8/4.0+XO*IT7/4.0;
1175 /*****
1176 /*

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1177 /* Calculate integral of yR over the triangle IT9 */
1178 /* */
1179 /****** */
1180 /****** */
1181 IT9=0.;
1182 for(n=1;n<=3;n++)
1183 IT9=IT9+(DY1[n]*(alpi[n]*gi[n]*I61[n]+(gi[n]*(ci[n]-xo)+alpi[n]*d1[n])
1184 *I51[n]+d1[n]*(ci[n]-xo)*I41[n])-DX1[n]*(gi[n]*I61[n]+g1[n]
1185 *(2.*d1[n]-yo)*I51[n]+d1[n]*(d1[n]-yo)*I41[n]));
1186 IT9=IT9/4.0+yo*IT7/4.0;
1187
1188 /****** */
1189 /* Calculate derivatives of I11 */
1190 /* DX111 is first derivative of I11 with respect to x */
1191 /* DY111 is first derivative of I11 with respect to y */
1192 /* DX2111 is second derivative of I11 with respect to x */
1193 /* DY2111 is second derivative of I11 with respect to y */
1194 /* DXY111 is derivative of I11 with respect to x and y */
1195 /* */
1196 /****** */
1197
1198
1199 for(n=1;n<=3;n++)
1200 {
1201 DX111[n]=0.0;
1202 DY111[n]=0.0;
1203 DX2111[n]=0.0;
1204 DY2111[n]=0.0;
1205 DXY111[n]=0.0;
1206
1207 t[1]=t1p[n];
1208 t[2]=t1m[n];
1209
1210 R[1]=R1p[n];
1211 R[2]=R1m[n];
1212
1213 sign=1.0;
1214
1215 for(m=1;m<=2;m++)
1216 {
1217 xt[m]=xo-(alpi[n]*t[m]+ci[n]);
1218 yt[m]=yo-(gi[n]*t[m]+d1[n]);
1219 ntrmx=2.0*alpi[n]*C2[n]*R[m]-2.0*C[n]*xt[m];
1220 dtrm=2.0*C2[n]*R[m]+2.0*C[n]*t[m]+B[n];
1221 ntrmy=2.0*gi[n]*C2[n]*R[m]-2.0*C[n]*yt[m];
1222
1223 if(m==2)
1224 sign=(-1.0);
1225
1226 DXI111[n]=DXI111[n]-sign*ntrmx/(C[n]*R[m]*dtrm);
1227
1228 DYI111[n]=DYI111[n]-sign*ntrmy/(C[n]*R[m]*dtrm);
1229
1230 DX2I111[n]=DX2I111[n]+sign*(-(ntrmx*ntrmx)/(C[n]*sqrt(C[n])*R[m]
1231 *R[m]*dtrm*dtrm)+(2.0/dtrm)*(1.0/R[m]-(xt[m]*xt[m])/
1232 powr(R[m],3)));

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DY2I111[n]=DYI111[n]+sign*(-(ntrmy*ntrmy)/(C[n]*sqrt(C[n]))*R[m]
    *R[m]*dtrm*dtrm)+(2.0/dtrm)*(1.0/R[m])-(yt[m]*yt[m])/
    powr(R[m],3));
DXYI111[n]=DXYI111[n]+sign*(-(ntrmx*ntrmy)/(C[n]*sqrt(C[n]))*R[m]
    *R[m]*dtrm*dtrm)-(2.0*xt[m]*yt[m])/(dtrm*powr(R[m],3));
}

/*****
/*
/* Calculate derivatives of I21
/* DXI21 is first derivative of I21 with respect to x
/* DYI21 is first derivative of I21 with respect to y
/* DX2I21 is second derivative of I21 with respect to x
/* DY2I21 is second derivative of I21 with respect to y
/* DXYI21 is derivative of I21 with respect to x and y
/*
*****/
DXI21[n]=(xt[1]/R[1]-xt[2]/R[2])/sqrt(C[n])-B[n]*DXI111[n]/(2.*C[n])
+alpi[n]*I11[n]/C[n];
DYI21[n]=(yt[1]/R[1]-yt[2]/R[2])/sqrt(C[n])-B[n]*DYI111[n]/(2.*C[n])
+g1[n]*I11[n]/C[n];
DX2I21[n]=((1.0/R[1]-xt[1]*xt[1]/powr(R[1],3))-(1.0/R[2]-xt[2]*xt[2]/
    powr(R[2],3))/sqrt(C[n])-B[n]*DX2I111[n]/(2.*C[n])+2.
    *alpi[n]*DXI111[n]/C[n];
DY2I21[n]=((1.0/R[1]-yt[1]*yt[1]/powr(R[1],3))-(1.0/R[2]-yt[2]*yt[2]/
    powr(R[2],3))/sqrt(C[n])-B[n]*DY2I111[n]/(2.*C[n])+2.*g1[n]
    *DYI111[n]/C[n];
DXYI21[n]=(xt[2]*yt[2]/powr(R[2],3)-xt[1]*yt[1]/powr(R[1],3))/C2[n]
+g1[n]*DXI111[n]/C[n]+alpi[n]*DYI111[n]/C[n]-B[n]*DXYI111[n]/
    (2.*C[n]);
/*****
/*
/* Calculate derivatives of I31
/* DXI31 is first derivative of I31 with respect to x
/* DYI31 is first derivative of I31 with respect to y
/* DX2I31 is second derivative of I31 with respect to x
/* DY2I31 is second derivative of I31 with respect to y
/* DXYI31 is derivative of I31 with respect to x and y
/*
*****/
DXI31[n]=(((t[1]-3.*B[n]/(2.*C[n]))*xt[1]/R[1]+3.*alpi[n]*R[1]/C[n])
    -((t[2]-3.*B[n]/(2.*C[n]))*xt[2]/R[2]+3.*alpi[n]*R[2]/C[n]))
    /(2.*C[n]);
DXYI31[n]=DXI31[n]+(3.*B[n]*B[n]/(4.*C[n])-A[n])*DXI111[n]/(2.*C[n])
    -(3.*B[n]*alpi[n]/(2.*C[n])+(xo-c1[n])*I11[n]/C[n]);
DYI31[n]=(((t[1]-3.*B[n]/(2.*C[n]))*yt[1]/R[1]+3.*g1[n]*R[1]/C[n])
    -((t[2]-3.*B[n]/(2.*C[n]))*yt[2]/R[2]+3.*g1[n]*R[2]/C[n]))
    /(2.*C[n]);

```



```

1289      -((t[2]-3.*B[n]/(2.*C[n]))*yt[2]/R[2]+3.*g1[n]*R[2]/C[n]))
1290      /(2.*C[n]);
1291      DYI31[n]=DYI31[n]+(3.*B[n]*B[n]/(4.*C[n])-A[n])*DYI11[n]/(2.*C[n])
1292      -(3.*B[n]*g1[n]/(2.*C[n])+(yo-di[n]))*I11[n]/C[n];
1293
1294      DX2I31[n]=(3.*alpi[n]*xt[1]/(C[n]*C[n]*R[1])+(t[1]-3.*B[n]/(2.*C[n]))
1295      *(1./R[1]-xt[1]*xt[1]/powr(R[1],3))/(2.*C[n])-(3.*alpi[n]
1296      *xt[2]/(C[n]*C[n]*R[2])+(t[2]-3.*B[n]/(2.*C[n]))*(1./R[2]
1297      -xt[2]*xt[2]/powr(R[2],3))/(2.*C[n]);
1298      DX2I31[n]+(3.*B[n]*B[n]/(4.*C[n]));
1299      -A[n])*DX2I11[n]/(2.*C[n])-(3.*B[n]*alpi[n]/C[n]-2.*(xo
1300      -ci[n]))*DXI11[n]/C[n]+(3.*alpi[n]*alpi[n]/C[n]-1.)*I11[n]/
1301      C[n];
1302
1303      DY2I31[n]=(3.*g1[n]*yt[1]/(C[n]*C[n]*R[1])+(t[1]-3.*B[n]/(2.*C[n]))
1304      *(1./R[1]-yt[1]*yt[1]/powr(R[1],3))/(2.*C[n])-(3.*g1[n]
1305      *yt[2]/(C[n]*C[n]*R[2])+(t[2]-3.*B[n]/(2.*C[n]))*(1./R[2]
1306      -yt[2]*yt[2]/powr(R[2],3))/(2.*C[n]);
1307      DY2I31[n]=DY2I31[n]+(3.*B[n]*B[n]/(4.*C[n]));
1308      -A[n])*DY2I11[n]/(2.*C[n])-(3.*B[n]*g1[n]/C[n]-2.*(yo
1309      -di[n]))*DYI11[n]/C[n]+(3.*g1[n]*g1[n]/C[n]-1.)*I11[n]/C[n];
1310
1311      DXYI31[n]=3.*alpi[n]*yt[1]/(2.*C[n]*C[n]*R[1])-(t[1]-3.*B[n]/(2.
1312      *C[n]))*yt[1]*xt[1]/(2.*C[n]*powr(R[1],3))+3.*g1[n]*xt[1]/(2.
1313      *C[n]*C[n]*R[1]);
1314      DXYI31[n]=DXYI31[n]-(3.*alpi[n]*yt[2]/(2.*C[n]*C[n]*R[2])-(t[2]
1315      -3.*B[n]/(2.*C[n]))*yt[2]*xt[2]/(2.*C[n]*powr(R[2],3))+3.
1316      *g1[n]*xt[2]/(2.*C[n]*C[n]*R[2]));
1317      DXYI31[n]=DXYI31[n]-(3.*B[n]*alpi[n]/(2.*C[n])
1318      +xo-ci[n])*DYI11[n]/C[n]+(3.*B[n]*B[n]/(4.*C[n])-A[n])
1319      *DXI11[n]/(2.*C[n]);
1320      DXYI31[n]=DXYI31[n]-(3.*B[n]*g1[n]/(2.*C[n])+yo-di[n])
1321      *DXI11[n]/C[n]+3.*g1[n]*g1[n]/C[n]*C[n]);
1322
1323      /*****
1324      /*
1325      /* Calculate derivatives of I41
1326      /* DXI41 is first derivative of I41 with respect to x
1327      /* DYI41 is first derivative of I41 with respect to y
1328      /* DX2I41 is second derivative of I41 with respect to x
1329      /* DY2I41 is second derivative of I41 with respect to y
1330      /* DXYI41 is derivative of I41 with respect to x and y
1331      /*
1332      /*
1333      /*
1334      delta[n]=(4.*A[n]*C[n]-B[n]*B[n])/(8.*C[n]);
1335
1336      DXI41[n]=(((2.0*C[n]*t[1]+B[n])*xt[1]/R[1]-2.*alpi[n]*R[1])-(2.0*C[n]
1337      *t[2]+B[n])*xt[2]/R[2]-2.0*alpi[n]*R[2])/(4.0*C[n])+(xo
1338      -ci[n]+B[n]*alpi[n]/(2.0*C[n]))*I11[n]+delta[n]*DXI11[n];
1339
1340      DYI41[n]=(((2.0*C[n]*t[1]+B[n])*yt[1]/R[1]-2.*g1[n]*R[1])-(2.0*C[n]
1341      *t[2]+B[n])*yt[2]/R[2]-2.0*g1[n]*R[2])/(4.0*C[n])+(yo
1342      -di[n]+B[n]*g1[n]/(2.0*C[n]))*I11[n]+delta[n]*DYI11[n];
1343
1344      DX2I41[n]=(((2.0*C[n]*t[1]+B[n]-4.0*alpi[n]*xt[1])/R[1]-(2.0*C[n]*t[1]

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```

1345 +B[n])*xt[1]*xt[1]/powr(R[1],3))-((2.0*C[n]*t[2]
1346 +B[n]-4.0*alpi[n]*xt[2])/R[2]-(2.0*C[n]*t[2]+B[n])*xt[2]
1347 *xt[2]/powr(R[2],3))/(4.0*C[n]);
1348 DX2I41[n]=DX2I41[n]+(1.0-alpi[n]*alpi[n]/C[n])
1349 *I11[n]+(2.0*(xo-ci[n]+B[n]*alpi[n]/C[n])*DXI11[n]+delta[n]
1350 *DX2I11[n]);
1351
1352 DY2I41[n]=(((2.0*C[n]*t[1]+B[n]-4.0*gi[n]*yt[1])/R[1]-(2.0*C[n]*t[1]
1353 +B[n])*yt[1]*yt[1]/powr(R[1],3))-((2.0*C[n]*t[2]
1354 +B[n]-4.0*gi[n]*yt[2])/R[2]-(2.0*C[n]*t[2]+B[n])*yt[2]
1355 *yt[2]/powr(R[2],3))/(4.0*C[n]);
1356 DY2I41[n]=DY2I41[n]+(1.0-gi[n]*gi[n]/C[n])
1357 *I11[n]+(2.0*(yo-di[n]+B[n]*gi[n]/C[n])*DYI11[n]+delta[n]
1358 *DY2I11[n]);
1359
1360 DXVI41[n]=((2.0*(gi[n]*xt[2]+alpi[n]*yt[2])/R[2]+(2.0
1361 *C[n]*t[2]+B[n])*xt[2]*yt[2]/powr(R[2],3))-((2.0*(gi[n]*xt[1]
1362 +alpi[n]*yt[1])/R[1]+(2.0*C[n]*t[1]+B[n])*xt[1]*yt[1]
1363 /powr(R[1],3)))/(4.0*C[n]);
1364 DXVI41[n]=DXVI41[n]-gi[n]*alpi[n]*I11[n]/C[n]
1365 +(xo-ci[n]+B[n]*alpi[n]/(2.0*C[n]))*DYI11[n]+(yo-di[n]+gi[n]
1366 *B[n]/(2.0*C[n]))*DXI11[n]+delta[n]*DXVI11[n];
1367
1368 /*****
1369 /*
1370 /* Calculate derivatives of I61
1371 /* DXI61 is first derivative of I61 with respect to x
1372 /* DYI61 is first derivative of I61 with respect to y
1373 /* DX2I61 is second derivative of I61 with respect to x
1374 /* DY2I61 is second derivative of I61 with respect to y
1375 /* DXVI61 is derivative of I61 with respect to x and y
1376 /*
1377 /*****
1378
1379 DXI61[n]=(R[1]*xt[1]-R[2]*xt[2]-B[n]*DXI41[n]/2.0+alpi[n]*I41[n])
1380 /C[n];
1381
1382 DYI61[n]=(R[1]*yt[1]-R[2]*yt[2]-B[n]*DYI41[n]/2.0+gi[n]*I41[n])/C[n];
1383
1384 DX2I61[n]=(R[1]+xt[1]*xt[1]/R[1]-R[2]-xt[2]*xt[2]/R[2]-B[n]*DX2I41[n]
1385 /2.0+2.0*alpi[n]*DXI41[n])/C[n];
1386
1387 DY2I61[n]=(R[1]+yt[1]*yt[1]/R[1]-R[2]-yt[2]*yt[2]/R[2]-B[n]*DY2I41[n]
1388 /2.0+2.0*gi[n]*DYI41[n])/C[n];
1389
1390 DXVI61[n]=(xt[1]*yt[1]/R[1]-xt[2]*yt[2]/R[2]+gi[n]*DXI41[n]-B[n]
1391 *DXVI41[n])/2.0+alpi[n]*DYI41[n])/C[n];
1392
1393 /*****
1394 /*
1395 /* Calculate derivatives of I61
1396 /* DXI61 is first derivative of I61 with respect to x
1397 /* DYI61 is first derivative of I61 with respect to y
1398 /* DX2I61 is second derivative of I61 with respect to x
1399 /* DY2I61 is second derivative of I61 with respect to y
1400 /* DXVI61 is derivative of I61 with respect to x and y

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1401 /*
1402 /******
1403 /******
1404 DXI61[n]=(5.*alpi[n]*powr(R[1],3)/(12.*C[n]*C[n])+(t[1]/(4.*C[n]))-5.
1405 *B[n]/(24.*C[n]*C[n]))*3.*R[1]*xt[1])-(5.*alpi[n]*powr(R[2],3)/
1406 (12.*C[n]*C[n])+(t[2]/(4.*C[n]))-5.*B[n]/(24.*C[n]*C[n]))*3.*R[2]
1407 *xt[2]);
1408 DXI61[n]=DXI61[n]-(5.*B[n]*alpi[n]/(4.*C[n]*C[n])+(xo-ci[n])/(2.*C[n]))
1409 *I41[n]+(5.*B[n]*B[n]/(16.*C[n]*C[n])-A[n]/(4.*C[n]))
1410 *DXI41[n];
1411
1412 DYI61[n]=(5.*g1[n]*powr(R[1],3)/(12.*C[n]*C[n])+(t[1]/(4.*C[n]))-5.
1413 *B[n]/(24.*C[n]*C[n]))*3.*R[1]*yt[1])-(5.*g1[n]*powr(R[2],3)/
1414 (12.*C[n]*C[n])+(t[2]/(4.*C[n]))-5.*B[n]/(24.*C[n]*C[n]))*3.*R[2]
1415 *yt[2]);
1416 DYI61[n]=DYI61[n]-(5.*B[n]*g1[n]/(4.*C[n]*C[n])+(yo-d1[n])/(2.*C[n]))
1417 *I41[n]+(5.*B[n]*B[n]/(16.*C[n]*C[n])-A[n]/(4.*C[n]))
1418 *DYI41[n];
1419
1420 DX2I61[n]=(5.*alpi[n]*R[1]*xt[1]/(2.*C[n]*C[n])+3.*(t[1]/(4.*C[n]))-5.
1421 *B[n]/(24.*C[n]*C[n]))*(R[1]+xt[1]*xt[1]/R[1]);
1422 DX2I61[n]=DX2I61[n]-(5.*alpi[n]
1423 *R[2]*xt[2]/(2.*C[n]*C[n])+3.*(t[2]/(4.*C[n]))-5.*B[n]/(24.
1424 *C[n]*C[n]))*(R[2]+xt[2]*xt[2]/R[2]);
1425 DX2I61[n]=DX2I61[n]-2.*(5.*B[n]*alpi[n]/
1426 (4.*C[n]*C[n])+(xo-ci[n])/(2.*C[n]))*DXI41[n]-(1.-5.*alpi[n]
1427 *alpi[n]/C[n])*I41[n]/(2.*C[n]);
1428 DX2I61[n]=DX2I61[n]+(5.*B[n]*B[n]/(16.*C[n]*C[n])
1429 -A[n]/(4.*C[n]))*DX2I41[n];
1430
1431 DY2I61[n]=(5.*g1[n]*R[1]*yt[1]/(2.*C[n]*C[n])+3.*(t[1]/(4.*C[n]))-5.
1432 *B[n]/(24.*C[n]*C[n]))*(R[1]+yt[1]*yt[1]/R[1]);
1433 DY2I61[n]=DY2I61[n]-(5.*g1[n]
1434 *R[2]*yt[2]/(2.*C[n]*C[n])+3.*(t[2]/(4.*C[n]))-5.*B[n]/(24.
1435 *C[n]*C[n]))*(R[2]+yt[2]*yt[2]/R[2]);
1436 DY2I61[n]=DY2I61[n]-2.*(5.*B[n]*g1[n]/(4.
1437 *C[n]*C[n])+(yo-d1[n])/(2.*C[n]))*DYI41[n]-(1.-5.*g1[n]*g1[n]
1438 /C[n])*I41[n]/(2.*C[n]);
1439 DY2I61[n]=DY2I61[n]+(5.*B[n]*B[n]/(16.*C[n]*C[n])
1440 -A[n]/(4.*C[n]))*DY2I41[n];
1441
1442 DXYI61[n]=(5.*g1[n]*R[1]*xt[1]/(4.*C[n]*C[n])+5.*alpi[n]*R[1]*yt[1]/
1443 (4.*C[n]*C[n])+3.*(t[1]/(4.*C[n]))-5.*B[n]/(24.*C[n]*C[n]))
1444 *xt[1]*yt[1]/R[1]);
1445 DXYI61[n]=DXYI61[n]-(5.*g1[n]*R[2]*xt[2]/(4.*C[n]*C[n])+5.
1446 *alpi[n]*R[2]*yt[2]/(4.*C[n]*C[n])+3.*(t[2]/(4.*C[n]))-5.
1447 *B[n]/(24.*C[n]*C[n]))*xt[2]*yt[2]/R[2]);
1448 DXYI61[n]=DXYI61[n]-5.*alpi[n]*g1[n]
1449 *I41[n]/(2.*C[n]*C[n])-(5.*B[n]*g1[n]/(2.*C[n])+yo-d1[n])
1450 *DXI41[n]/(2.*C[n]);
1451 DXYI61[n]=DXYI61[n]-(5.*B[n]*alpi[n]/(2.*C[n])+(xo-ci[n])
1452 *DYI41[n]/(2.*C[n]))+(5.*B[n]*B[n]/(16.*C[n]*C[n])-A[n]/(4.
1453 *C[n]))*DXYI41[n];
1454
1455
1456

```

```

1457 /***** Calculate derivatives of IT1 with respect to x *****/
1458 /*
1459 /*
1460 /*
1461 /*
1462 /*
1463 /*
1464 /*
1465 /*
1466 /*
1467 /***** Calculate derivatives of IT1 with respect to x *****/
1468 /*
1469 /*
1470 /*
1471 /*
1472 /*
1473 /*
1474 /*
1475 /*
1476 /*
1477 /*
1478 /*
1479 /*
1480 /*
1481 /*
1482 /*
1483 /*
1484 /*
1485 /*
1486 /*
1487 /*
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1489 /*
1490 /*
1491 /*
1492 /*
1493 /***** Calculate derivatives of IT2 with respect to x *****/
1494 /*
1495 /*
1496 /*
1497 /*
1498 /*
1499 /*
1500 /*
1501 /*
1502 /*
1503 /*
1504 /*
1505 /*
1506 /*
1507 /*
1508 /*
1509 /*
1510 /*
1511 /*
1512 /*

```

Calculate derivatives of IT1 with respect to x  
 DXIT1 is first derivative of IT1 with respect to x  
 DYIT1 is first derivative of IT1 with respect to y  
 DX2IT1 is second derivative of IT1 with respect to x  
 DY2IT1 is second derivative of IT1 with respect to y  
 DXYIT1 is derivative of IT1 with respect to x and y

```

DXIT1=0.0;
DYIT1=0.0;
DX2IT1=0.0;
DY2IT1=0.0;
DXYIT1=0.0;
for (n=1;n<=3;n++)
{
  DXIT1=DXIT1+Dy1[n]*(alp1[n]*DXI21[n]+(c1[n]-xo)*DXI11[n]-I11[n])
    -Dx1[n]*(g1[n]*DXI21[n]+(d1[n]-yo)*DXI11[n]);
  DYIT1=DYIT1+Dy1[n]*(alp1[n]*DYI21[n]+(c1[n]-xo)*DYI11[n])
    -Dx1[n]*(g1[n]*DYI21[n]+(d1[n]-yo)*DYI11[n]-I11[n]);
  DX2IT1=DX2IT1+Dy1[n]*(alp1[n]*DX2I21[n]+(c1[n]-xo)*DX2I11[n]-2.
    *DXI11[n])-Dx1[n]*(g1[n]*DX2I21[n]+(d1[n]-yo)*DX2I11[n]);
  DY2IT1=DY2IT1+Dy1[n]*(alp1[n]*DY2I21[n]+(c1[n]-xo)*DY2I11[n])
    -Dx1[n]*(g1[n]*DY2I21[n]+(d1[n]-yo)*DY2I11[n]-2.*DYI11[n]);
  DXYIT1=DXYIT1+Dy1[n]*(alp1[n]*DXYI21[n]+(c1[n]-xo)*DXYI11[n]-DYI11[n])
    -Dx1[n]*(g1[n]*DXYI21[n]+(d1[n]-yo)*DXYI11[n]-DXI11[n]);
}

```

Calculate derivatives of IT2 with respect to x  
 DX2IT2 is second derivative of IT2 with respect to x  
 DY2IT2 is second derivative of IT2 with respect to y  
 DXYIT2 is derivative of IT2 with respect to x and y

```

DX2IT2=0.0;
DY2IT2=0.0;
DXYIT2=0.0;
for (n=1;n<=3;n++)
{
  DX2IT2=DX2IT2+Dy1[n]*(alp1[n]*alp1[n]*DX2I31[n]+alp1[n]*(2.*c1[n]-xo)
    *DX2I21[n]-2.*alp1[n]*DXI21[n]+c1[n]*(c1[n]-xo)*DX2I11[n]-2.
    *c1[n]*DXI11[n]);
  DX2IT2=DX2IT2-Dx1[n]*(alp1[n]*g1[n]*DX2I31[n]+(g1[n]*c1[n]
    +alp1[n]*(d1[n]-yo))*DX2I21[n]+c1[n]*(d1[n]-yo)*DX2I11[n]);
}

```

```

1513
1514 DY2IT2=DY2IT2+Dy1[n]*(alpi1[n]*alpi1[n]*DY2I31[n]+alpi1[n]*(2.*ci1[n]-xo)
1515 *DY2I21[n]+ci1[n]*ci1[n]*DY2I11[n]);
1516 DY2IT2=DY2IT2-Dx1[n]*(g1[n]*alpi1[n]
1517 *DY2I31[n]-2.*alpi1[n]*DYI21[n]+(g1[n]*ci1[n]+alpi1[n]*(di1[n]-yo))
1518 *DY2I21[n]-2.*ci1[n]*DYI11[n]+ci1[n]*(di1[n]-yo)*DY2I11[n]);
1519
1520 DXYIT2=DXYIT2+Dy1[n]*(alpi1[n]*alpi1[n]*DXYI31[n]+alpi1[n]*(2.*ci1[n]-xo)
1521 *DXYI21[n]-alpi1[n]*DYI21[n]+ci1[n]*(ci1[n]-xo)*DXYI11[n]-ci1[n]
1522 *DYI11[n]);
1523 DXYIT2=DXYIT2-Dx1[n]*(alpi1[n]*g1[n]*DXYI31[n]+(g1[n]*ci1[n]+alpi1[n]
1524 *(di1[n]-yo))*DXYI21[n]-alpi1[n]*DXI21[n]+ci1[n]*(di1[n]-yo)
1525 *DXYI11[n]-ci1[n]*DXI11[n]);
1526
1527
1528 DX2IT2=DX2IT2/2.0+xo*DX2IT1/2.0+DXIT1;
1529 DY2IT2=DY2IT2/2.0+yo*DY2IT1/2.0;
1530 DXYIT2=DXYIT2/2.0+DYIT1/2.0+xo*DXYIT1/2.0;
1531
1532 /*****
1533 /* Calculate derivatives of IT3
1534 /* DX2IT3 is second derivative of IT3 with respect to x
1535 /* DY2IT3 is second derivative of IT3 with respect to y
1536 /* DXYIT3 is derivative of IT3 with respect to x and y
1537 /*
1538 /*
1539 /*****
1540
1541 DX2IT3=0.0;
1542 DY2IT3=0.0;
1543 DXYIT3=0.0;
1544
1545 for(n=1;n<=3;n++)
1546 {
1547 DX2IT3=DX2IT3+Dy1[n]*(alpi1[n]*g1[n]*DX2I31[n]+(g1[n]*(ci1[n]-xo)+d1[n])
1548 *DX2I21[n]-2.*g1[n]*DXI21[n]+d1[n]*(ci1[n]-xo)*DX2I11[n]-2.*d1[n]
1549 *I11[n]);
1550 DX2IT3=DX2IT3-Dx1[n]*(g1[n]*g1[n]*DX2I31[n]+g1[n]*(2.*d1[n]-yo)
1551 *DX2I21[n]+d1[n]*(d1[n]-yo)*DX2I11[n]);
1552
1553 DY2IT3=DY2IT3+Dy1[n]*(g1[n]*alpi1[n]*DY2I31[n]+(g1[n]*(ci1[n]-xo)+d1[n])
1554 *DY2I21[n]+d1[n]*(ci1[n]-xo)*DY2I11[n]);
1555 DY2IT3=DY2IT3-Dx1[n]*(g1[n]*g1[n]
1556 *DY2I31[n]+g1[n]*(2.*d1[n]-yo)*DY2I21[n]-2.*g1[n]*DYI21[n]+d1[n]
1557 *(d1[n]-yo)*DY2I11[n]-2.*d1[n]*DYI11[n]);
1558
1559 DXYIT3=DXYIT3+Dy1[n]*(alpi1[n]*g1[n]*DXYI31[n]+(g1[n]*(ci1[n]-xo)+d1[n])
1560 *DXYI21[n]-g1[n]*DYI21[n]+d1[n]*(ci1[n]-xo)*DXYI11[n]-d1[n]
1561 *DYI11[n]);
1562 DXYIT3=DXYIT3-Dx1[n]*(g1[n]*g1[n]*DXYI31[n]+g1[n]*(2.*d1[n]-yo)
1563 *DXYI21[n]-g1[n]*DXI21[n]+d1[n]*(d1[n]-yo)*DXYI11[n]-d1[n]
1564 *DXI11[n]);
1565
1566
1567
1568 DX2IT3=DX2IT3/2.0+yo*DX2IT1/2.0;

```

```

1569 DY2IT3=DY2IT3/2.0+yo*DY2IT1/2.0+DYIT1;
1570 DXYIT3=DXYIT3/2.0+DXIT1/2.0+yo*DXYIT1/2.0;
1571
1572 /*****
1573 /*
1574 /* Calculate derivatives of IT7
1575 /* DXIT7 is first derivative of IT7 with respect to x
1576 /* DYIT7 is first derivative of IT7 with respect to y
1577 /* DX2IT7 is second derivative of IT7 with respect to x
1578 /* DY2IT7 is second derivative of IT7 with respect to y
1579 /* DXYIT7 is derivative of IT7 with respect to x and y
1580 /*
1581 /*****
1582
1583 DXIT7=0.0;
1584 DYIT7=0.0;
1585 DX2IT7=0.0;
1586 DY2IT7=0.0;
1587 DXYIT7=0.0;
1588
1589 for (n=1;n<=3;n++)
1590 {
1591     DXIT7=DXIT7+Dy1[n]*(alp1[n]*DXI51[n]+(c1[n]-xo)*DXI41[n]-I41[n])
1592     -Dx1[n]*(g1[n]*DXI51[n]+(d1[n]-yo)*DXI41[n]);
1593     DYIT7=DYIT7+Dy1[n]*(alp1[n]*DYI51[n]+(c1[n]-xo)*DYI41[n])
1594     -Dx1[n]*(g1[n]*DYI51[n]+(d1[n]-yo)*DYI41[n]-I41[n]);
1595     DX2IT7=DX2IT7+Dy1[n]*(alp1[n]*DX2I51[n]+(c1[n]-xo)*DX2I41[n]-2.
1596     *DXI41[n])-Dx1[n]*(g1[n]*DX2I51[n]+(d1[n]-yo)*DX2I41[n]);
1597     DY2IT7=DY2IT7+Dy1[n]*(alp1[n]*DY2I51[n]+(c1[n]-xo)*DY2I41[n])
1598     -Dx1[n]*(g1[n]*DY2I51[n]+(d1[n]-yo)*DY2I41[n]-2.*DYI41[n]);
1599     DXYIT7=DXYIT7+Dy1[n]*(alp1[n]*DXYI51[n]+(c1[n]-xo)*DXYI41[n])
1600     -Dx1[n]*(g1[n]*DXYI51[n]+(d1[n]-yo)*DXYI41[n]-DXI41[n]);
1601
1602 }
1603
1604 DXYIT7=DXYIT7+Dy1[n]*(alp1[n]*DXYI51[n]+(c1[n]-xo)*DXYI41[n]-DYI41[n])
1605 -Dx1[n]*(g1[n]*DXYI51[n]+(d1[n]-yo)*DXYI41[n]-DXI41[n]);
1606
1607
1608 DXIT7=DXIT7/3.0;
1609 DYIT7=DYIT7/3.0;
1610 DX2IT7=DX2IT7/3.0;
1611 DY2IT7=DY2IT7/3.0;
1612 DXYIT7=DXYIT7/3.0;
1613
1614 /*****
1615 /*
1616 /* Calculate derivatives of IT8
1617 /* DX2IT8 is second derivative of IT8 with respect to x
1618 /* DY2IT8 is second derivative of IT8 with respect to y
1619 /* DXYIT8 is derivative of IT8 with respect to x and y
1620 /*
1621 /*****
1622
1623 DX2IT8=0.0;
1624 DY2IT8=0.0;

```

**MISSING  
PAGE**

```

1626  *****-0.0;
1627  for(n=1;n<=3;n++)
1628  {
1629  DX2IT8=DX2IT8+DY1[n]*(alpi[n]*alpi[n]*DX2I61[n]+alpi[n]*(2.*ci[n]-xo)
1630  *DX2I51[n]-2.*alpi[n]*DXI51[n]+ci[n]*(ci[n]-xo)*DX2I41[n]-2.
1631  *ci[n]*DXI41[n]);
1632  DX2IT8=DX2IT8-DX1[n]*(alpi[n]*gi[n]*DX2I61[n]+(gi[n]*ci[n]
1633  +alpi[n]*(di[n]-yo))*DX2I51[n]+ci[n]*(di[n]-yo)*DX2I41[n]);
1634
1635  DY2IT8=DY2IT8+DY1[n]*(alpi[n]*alpi[n]*DY2I61[n]+alpi[n]*(2.*ci[n]-xo)
1636  *DY2I51[n]+ci[n]*(ci[n]-xo)*DY2I41[n]);
1637  DY2IT8=DY2IT8-DX1[n]*(gi[n]*alpi[n]
1638  *DY2I61[n]-2.*alpi[n]*DYI51[n]+(gi[n]*ci[n]+alpi[n]*(di[n]-yo)
1639  *DY2I51[n]-2.*ci[n]*DYI41[n]+ci[n]*(di[n]-yo)*DY2I41[n]);
1640
1641  DXYIT8=DXYIT8+DY1[n]*(alpi[n]*alpi[n]*DXVI61[n]+alpi[n]*(2.*ci[n]-xo)
1642  *DXYI51[n]-alpi[n]*DYI51[n]+ci[n]*(ci[n]-xo)*DXYI41[n]-ci[n]
1643  *DYI41[n]);
1644  DXYIT8=DXYIT8-DX1[n]*(alpi[n]*gi[n]*DXVI61[n]+(gi[n]*ci[n]+alpi[n]
1645  *(di[n]-yo))*DXYI51[n]-alpi[n]*DXI51[n]+ci[n]*(di[n]-yo)
1646  *DXYI41[n]-ci[n]*DXI41[n]);
1647  }
1648
1649  DX2IT8=DX2IT8/4.0+xo*DX2IT7/4.0+DXIT1/2.0;
1650  DY2IT8=DY2IT8/4.0+xo*DY2IT7/4.0;
1651  DXYIT8=DXYIT8/4.0+DYIT7/4.0+xo*DXYIT1/4.0;
1652
1653  *****
1654  /*
1655  /* Calculate derivatives of IT9
1656  /* DX2IT9 is second derivative of IT9 with respect to x
1657  /* DY2IT9 is second derivative of IT9 with respect to y
1658  /* DXYIT9 is derivative of IT9 with respect to x and y
1659  /*
1660  /*
1661  *****
1662  DX2IT9=0.0;
1663  DY2IT9=0.0;
1664  DXYIT9=0.0;
1665
1666  for(n=1;n<=3;n++)
1667  {
1668  DX2IT9=DX2IT9+DY1[n]*(alpi[n]*gi[n]*DX2I61[n]+(gi[n]*(ci[n]-xo)+d1[n])
1669  *DX2I51[n]-2.*gi[n]*DXI51[n]+d1[n]*(ci[n]-xo)*DX2I41[n]-2.*d1[n]
1670  *I41[n]);
1671  DX2IT9=DX2IT9-DX1[n]*(gi[n]*gi[n]*DX2I61[n]+gi[n]*(2.*d1[n]-yo)
1672  *DX2I51[n]+d1[n]*(d1[n]-yo)*DX2I41[n]);
1673
1674  DY2IT9=DY2IT9+DY1[n]*(gi[n]*alpi[n]*DY2I61[n]+(gi[n]*(ci[n]-xo)+d1[n])
1675  *DY2I51[n]+d1[n]*(ci[n]-xo)*DY2I41[n]);
1676  DY2IT9=DY2IT9-DX1[n]*(gi[n]*gi[n]
1677  *DY2I61[n]+gi[n]*(2.*d1[n]-yo)*DY2I51[n]-2.*gi[n]*DYI51[n]+d1[n]
1678  *(d1[n]-yo)*DY2I41[n]-2.*d1[n]*DYI41[n]);
1679
1680
1733  DY2IT9=(-1)*DY2I1I9;
1734  DXYIT9=(-1)*DXYIT9;
1735  }
1736

```



```

1737 }
1738 powr(x,n)
1739 double x;
1740 int n;
1741 {
1742     double p,pow();
1743     if(x == 0.)
1744     {
1745         p=0.;
1746         return(p);
1747     }
1748     else
1749     {
1750         p=pow(x,n);
1751         return(p);
1752     }
1753 }
1754
1755 numer(xo,yo,xs1,ys1,xs2,ys2,xs3,ys3)
1756 double xo,yo,xs1,ys1,xs2,ys2,xs3,ys3;
1757 {
1758     /* ***** This routine performs the numerical evaluations over the triangles ***** */
1759     /* xo x coordinate of the field point */
1760     /* yo y coordinate of the field point */
1761     /* xs1 x coordinate of vertice 1 of source triangle */
1762     /* ys1 y coordinate of vertice 1 of source triangle */
1763     /* xs2 x coordinate of vertice 2 of source triangle */
1764     /* ys2 y coordinate of vertice 2 of source triangle */
1765     /* xs3 x coordinate of vertice 3 of source triangle */
1766     /* ys3 y coordinate of vertice 3 of source triangle */
1767     /* a weight factor */
1768     /* b weight factor */
1769     /* c weight factor */
1770     /* r evaluation point constant */
1771     /* s evaluation point constant */
1772     /* ctrdx x coordinate of the centroid */
1773     /* ctrdy y coordinate of the centroid */
1774     /* xp[n] x coordinates of the evaluation points */
1775     /* yp[n] y coordinates of the evaluation points */
1776     /* area area of the triangle */
1777     /* k wavenumber */
1778     /* rkr[n] real part of the rational kernel */
1779 }

```

```

1793 /* rki[n] imag part of the rational kernel */
1794 /* rkrx[n] real part of x times the rational kernel */
1795 /* rkix[n] imag part of x times the rational kernel */
1796 /* rkry[n] real part of y times the rational kernel */
1797 /* rkly[n] imag part of y times the rational kernel */
1798 /* dx2rkr[n] real part of second derivative with respect to x of
1799 /* the rational kernel */
1800 /* dx2rki[n] imag part of second derivative with respect to x of
1801 /* the rational kernel */
1802 /* dx2rkrx[n] real part of x times second derivative with respect to x of */
1803 /* the rational kernel */
1804 /* dx2rkix[n] imag part of x times second derivative with respect to x of */
1805 /* the rational kernel */
1806 /* dx2rkry[n] real part of y times second derivative with respect to x of */
1807 /* the rational kernel */
1808 /* dx2rkly[n] imag part of y times second derivative with respect to x of */
1809 /* the rational kernel */
1810 /* dy2rkr[n] real part of second derivative with respect to y of */
1811 /* the rational kernel */
1812 /* dy2rki[n] imag part of second derivative with respect to y of */
1813 /* the rational kernel */
1814 /* dy2rkrx[n] real part of x times second derivative with respect to y of */
1815 /* the rational kernel */
1816 /* dy2rkix[n] imag part of x times second derivative with respect to y of */
1817 /* the rational kernel */
1818 /* dy2rkry[n] real part of y times second derivative with respect to y of */
1819 /* the rational kernel */
1820 /* dy2rkly[n] imag part of y times second derivative with respect to y of */
1821 /* the rational kernel */
1822 /* dxyrkr[n] real part of derivative with respect to x and y of */
1823 /* the rational kernel */
1824 /* dxyrki[n] imag part of derivative with respect to x and y of */
1825 /* the rational kernel */
1826 /* dxyrkrx[n] real part of x times derivative with respect to x and y of */
1827 /* the rational kernel */
1828 /* dxyrkix[n] imag part of x times derivative with respect to x and y of */
1829 /* the rational kernel */
1830 /* dxyrkry[n] real part of y times derivative with respect to x and y of */
1831 /* the rational kernel */
1832 /* dxyrkly[n] imag part of y times derivative with respect to x and y of */
1833 /* the rational kernel */
1834 /* ***** */
1835 /* EXTERNAL VARIABLES */
1836 /* */
1837 /* ***** */
1838 /* Rk_re real part of the rational kernel */
1839 /* Rk_im imag part of the rational kernel */
1840 /* Rk_re real part of x times the rational kernel */
1841 /* Rk_im imag part of x times the rational kernel */
1842 /* Rk_re real part of y times the rational kernel */
1843 /* Rk_im imag part of y times the rational kernel */
1844 /* Dx2rk_re real part of second derivative with respect to x of
1845 /* the rational kernel */
1846 /* Dx2rk_im imag part of second derivative with respect to x of
1847 /* the rational kernel */
1848 /* */

```

```

1849 /* Dx2rkx_re real part of x times second derivative with respect to x of */
1850 /* the rational kernel */
1851 /* Dx2rkx_im imag part of x times second derivative with respect to x of */
1852 /* the rational kernel */
1853 /* Dx2rky_re real part of y times second derivative with respect to x of */
1854 /* the rational kernel */
1855 /* Dx2rky_im imag part of y times second derivative with respect to x of */
1856 /* the rational kernel */
1857 /* Dy2rk_re real part of second derivative with respect to y of */
1858 /* the rational kernel */
1859 /* Dy2rk_im imag part of second derivative with respect to y of */
1860 /* the rational kernel */
1861 /* Dy2rkx_re real part of x times second derivative with respect to y of */
1862 /* the rational kernel */
1863 /* Dy2rkx_im imag part of x times second derivative with respect to y of */
1864 /* the rational kernel */
1865 /* Dy2rky_re real part of y times second derivative with respect to y of */
1866 /* the rational kernel */
1867 /* Dy2rky_im imag part of y times second derivative with respect to y of */
1868 /* the rational kernel */
1869 /* Dxyrk_re real part of derivative with respect to x and y of */
1870 /* the rational kernel */
1871 /* Dxyrk_im imag part of derivative with respect to x and y of */
1872 /* the rational kernel */
1873 /* Dxyrkx_re real part of x times derivative with respect to x and y of */
1874 /* the rational kernel */
1875 /* Dxyrkx_im imag part of x times derivative with respect to x and y of */
1876 /* the rational kernel */
1877 /* Dxyrky_re real part of y times derivative with respect to x and y of */
1878 /* the rational kernel */
1879 /* Dxyrky_im imag part of y times derivative with respect to x and y of */
1880 /* the rational kernel */
1881 /* dyk wavenumber */
1882 /* ***** */
1883
1884 double x[4],y[4],a,b,c,r,s,k,ctrdx,ctrdy,xp[8],yp[8],area,R[8];
1885 double rkr[8],rki[8],rkrx[8],rkix[8],rkry[8],rkiy[8];
1886 double dx2rkr[8],dx2rki[8],dx2rkrx[8],dx2rkix[8],dx2rkry[8],dx2rkiy[8];
1887 double dy2rkr[8],dy2rki[8],dy2rkrx[8],dy2rkix[8],dy2rkry[8],dy2rkiy[8];
1888 double dxyrkr[8],dxyrki[8],dxyrkrx[8],dxyrkix[8],dxyrkry[8],dxyrkiy[8];
1889 double sqrt(),pow();
1890 int n;
1891
1892 area=IT4;
1893 k=dYk;
1894
1895 x[1]=xs1;
1896 y[1]=ys1;
1897 x[2]=xs2;
1898 y[2]=ys2;
1899 x[3]=xs3;
1900 y[3]=ys3;
1901
1902 /* ***** */
1903 /* Calculate the centroid of the triangle */
1904 /* ***** */

```

```

1905 /*
1906 /******
1907
1908 ctrdx=(x[1]+x[2]+x[3])/3.0;
1909 ctrdy=(y[1]+y[2]+y[3])/3.0;
1910
1911 /******
1912 /*
1913 /* If the field point and the centroid are coincident use the numerical*/
1914 /* method described in Hammer for a quadratic function to avoid the */
1915 /* singularity problem */
1916 /*
1917 /******
1918
1919 if( xo == ctrdx && yo == ctrdy )
1920 {
1921     r=0.5;
1922     for(n=1;n<=3;n++)
1923     {
1924         xp[n]=r*x[n]+(1.0-r)*ctrdx;
1925         yp[n]=r*y[n]+(1.0-r)*ctrdy;
1926     }
1927     for(n=1;n<=3;n++)
1928         R[n]=sqrt((xo-xp[n])*(xo-xp[n])+(yo-yp[n])*(yo-yp[n]));
1929
1930     for(n=1;n<=3;n++)
1931     {
1932
1933         rkr[n]=cos(k*R[n])/R[n]-1.0/R[n]+k*k*R[n]/2.0;
1934         rki[n]=sin(k*R[n])/R[n]-k;
1935         rkrx[n]=xp[n]*(cos(k*R[n])/R[n]-1.0/R[n]+k*k*R[n]/2.0);
1936         rkix[n]=xp[n]*(sin(k*R[n])/R[n]-k);
1937         rkry[n]=yp[n]*(cos(k*R[n])/R[n]-1.0/R[n]+k*k*R[n]/2.0);
1938         rkly[n]=yp[n]*(sin(k*R[n])/R[n]-k);
1939
1940         dx2rkr[n]=(3.*(xo-xp[n])*(xo-xp[n])/R[n]*R[n])-1.0-k*k
1941             *(xo-xp[n])*(xo-xp[n])*cos(k*R[n])/pow(R[n],3)
1942             -(1.-3.*(xo-xp[n])*(xo-xp[n]))*(xo-xp[n])*(xo-xp[n])*k
1943             *sin(k*R[n])/R[n]*R[n]);
1944
1945         dx2rki[n]=(1.0-3.*(xo-xp[n])*(xo-xp[n])/R[n]*R[n])*k*cos(k*R[n])
1946             /R[n]*R[n]+(3.*(xo-xp[n])*(xo-xp[n])/R[n]*R[n])-1.0
1947             -k*k*(xo-xp[n])*(xo-xp[n])*sin(k*R[n])/pow(R[n],3);
1948
1949         dx2rkrx[n]=xp[n]*((3.*(xo-xp[n])*(xo-xp[n])/R[n]*R[n])-1.0-k*k
1950             *(xo-xp[n])*(xo-xp[n])*cos(k*R[n])/pow(R[n],3)
1951             -(1.-3.*(xo-xp[n])*(xo-xp[n]))*(xo-xp[n])*(xo-xp[n])*k
1952             *sin(k*R[n])/R[n]*R[n]);
1953
1954         dx2rkix[n]=xp[n]*((1.0-3.*(xo-xp[n])*(xo-xp[n])/R[n]*R[n])*k*cos(k
1955             *R[n])/R[n]*R[n]+(3.*(xo-xp[n])*(xo-xp[n])/R[n]*R[n])-1.0
1956             -k*k*(xo-xp[n])*(xo-xp[n])*sin(k*R[n])/pow(R[n],3));
1957
1958         dx2rkry[n]=yp[n]*((3.*(xo-xp[n])*(xo-xp[n])/R[n]*R[n])-1.0-k*k

```

```

1961 * (xo-yp[n]) * (xo-xp[n]) * cos(k*R[n]) / pow(R[n], 3)
1962 -(1.-3. * (xo-yp[n]) * (xo-xp[n]) / (R[n] * R[n])) * k
1963 * sin(k*R[n]) / (R[n] * R[n]);
1964
1965 dx2rkiy[n] = yp[n] * ((1.0-3. * (xo-yp[n]) * (xo-xp[n]) / (R[n] * R[n])) * k * cos(k
1966 * R[n]) / (R[n] * R[n]) + (3. * (xo-yp[n]) * (xo-xp[n]) / (R[n] * R[n]) - 1.0
1967 -k*k*(xo-yp[n]) * (xo-xp[n]) * sin(k*R[n]) / pow(R[n], 3));
1968
1969
1970
1971 dy2rkr[n] = (3. * (yo-yp[n]) * (yo-yp[n]) / (R[n] * R[n]) - 1.0 - k*k * (yo-yp[n])
1972 * (yo-yp[n]) * cos(k*R[n]) / pow(R[n], 3) - (1.-3. * (yo-yp[n]) *
1973 (yo-yp[n]) / (R[n] * R[n])) * k * sin(k*R[n]) / (R[n] * R[n]));
1974
1975 dy2rki[n] = (1.0-3. * (yo-yp[n]) * (yo-yp[n]) / (R[n] * R[n])) * k * cos(k*R[n])
1976 / (R[n] * R[n]) + (3. * (yo-yp[n]) * (yo-yp[n]) / (R[n] * R[n]) - 1.0
1977 -k*k * (yo-yp[n]) * (yo-yp[n]) * sin(k*R[n]) / pow(R[n], 3);
1978
1979 dy2rkrx[n] = xp[n] * ((3. * (yo-yp[n]) * (yo-yp[n]) / (R[n] * R[n]) - 1.0 - k*k * (yo-
1980 yp[n]) * (yo-yp[n]) * cos(k*R[n]) / pow(R[n], 3) - (1.-3. * (yo-yp[n]) *
1981 (yo-yp[n]) / (R[n] * R[n])) * k * sin(k*R[n]) / (R[n] * R[n]));
1982
1983 dy2rkix[n] = xp[n] * ((1.0-3. * (yo-yp[n]) * (yo-yp[n]) / (R[n] * R[n])) * k * cos(k
1984 * R[n]) / (R[n] * R[n]) + (3. * (yo-yp[n]) * (yo-yp[n]) / (R[n] * R[n]) - 1.0
1985 -k*k * (yo-yp[n]) * (yo-yp[n]) * sin(k*R[n]) / pow(R[n], 3));
1986
1987 dy2rkry[n] = yp[n] * ((3. * (yo-yp[n]) * (yo-yp[n]) / (R[n] * R[n]) - 1.0 - k*k * (yo-
1988 yp[n]) * (yo-yp[n]) * cos(k*R[n]) / pow(R[n], 3) - (1.-3. * (yo-yp[n]) *
1989 (yo-yp[n]) / (R[n] * R[n])) * k * sin(k*R[n]) / (R[n] * R[n]));
1990
1991 dy2rkix[n] = yp[n] * ((1.0-3. * (yo-yp[n]) * (yo-yp[n]) / (R[n] * R[n])) * k * cos(k
1992 * R[n]) / (R[n] * R[n]) + (3. * (yo-yp[n]) * (yo-yp[n]) / (R[n] * R[n]) - 1.0
1993 -k*k * (yo-yp[n]) * (yo-yp[n]) * sin(k*R[n]) / pow(R[n], 3));
1994
1995
1996
1997
1998 dxyrkr[n] = ((3. - k*k*R[n] * R[n]) * cos(k*R[n]) + 3. * k*R[n] * sin(k*R[n]))
1999 * (xo-yp[n]) * (yo-yp[n]) / pow(R[n], 5);
2000
2001 dxyrki[n] = ((3. - k*k*R[n] * R[n]) * sin(k*R[n]) - 3. * k*R[n] * cos(k*R[n]))
2002 * (xo-yp[n]) * (yo-yp[n]) / pow(R[n], 5);
2003
2004 dxyrkrx[n] = xp[n] * ((3. - k*k*R[n] * R[n]) * cos(k*R[n]) + 3. * k*R[n] * sin(k
2005 * R[n]) * (xo-yp[n]) * (yo-yp[n]) / pow(R[n], 5);
2006
2007 dxyrkix[n] = xp[n] * ((3. - k*k*R[n] * R[n]) * sin(k*R[n]) - 3. * k*R[n] * cos(k
2008 * R[n]) * (xo-yp[n]) * (yo-yp[n]) / pow(R[n], 5);
2009
2010 dxyrkry[n] = yp[n] * ((3. - k*k*R[n] * R[n]) * cos(k*R[n]) + 3. * k*R[n] * sin(k
2011 * R[n]) * (xo-yp[n]) * (yo-yp[n]) / pow(R[n], 5);
2012
2013 dxyrkiy[n] = yp[n] * ((3. - k*k*R[n] * R[n]) * sin(k*R[n]) - 3. * k*R[n] * cos(k
2014 * R[n]) * (xo-yp[n]) * (yo-yp[n]) / pow(R[n], 5);
2015
2016

```

}

```

2017 Rk_re=(rkr[1]+rkr[2]+rkr[3])*area/3.0;
2018
2019 Rk_1m=(rk1[1]+rk1[2]+rk1[3])*area/3.0;
2020
2021 Rkx_re=(rkrx[1]+rkrx[2]+rkrx[3])*area/3.0;
2022
2023 Rkx_1m=(rk1x[1]+rk1x[2]+rk1x[3])*area/3.0;
2024
2025 Rky_re=(rkry[1]+rkry[2]+rkry[3])*area/3.0;
2026
2027 Rky_1m=(rk1y[1]+rk1y[2]+rk1y[3])*area/3.0;
2028
2029
2030 Dx2rk_re=(dx2rkr[1]+dx2rkr[2]+dx2rkr[3])*area/3.0;
2031
2032 Dx2rk_1m=(dx2rk1[1]+dx2rk1[2]+dx2rk1[3])*area/3.0;
2033
2034 Dx2rkx_re=(dx2rkrx[1]+dx2rkrx[2]+dx2rkrx[3])*area/3.0;
2035
2036 Dx2rkx_1m=(dx2rk1x[1]+dx2rk1x[2]+dx2rk1x[3])*area/3.0;
2037
2038 Dx2rky_re=(dx2rkry[1]+dx2rkry[2]+dx2rkry[3])*area/3.0;
2039
2040 Dx2rky_1m=(dx2rk1y[1]+dx2rk1y[2]+dx2rk1y[3])*area/3.0;
2041
2042
2043 Dy2rk_re=(dy2rkr[1]+dy2rkr[2]+dy2rkr[3])*area/3.0;
2044
2045 Dy2rk_1m=(dy2rk1[1]+dy2rk1[2]+dy2rk1[3])*area/3.0;
2046
2047 Dy2rkx_re=(dy2rkrx[1]+dy2rkrx[2]+dy2rkrx[3])*area/3.0;
2048
2049 Dy2rkx_1m=(dy2rk1x[1]+dy2rk1x[2]+dy2rk1x[3])*area/3.0;
2050
2051 Dy2rky_re=(dy2rkry[1]+dy2rkry[2]+dy2rkry[3])*area/3.0;
2052
2053 Dy2rky_1m=(dy2rk1y[1]+dy2rk1y[2]+dy2rk1y[3])*area/3.0;
2054
2055
2056 Dxyrk_re=(dxyrkr[1]+dxyrkr[2]+dxyrkr[3])*area/3.0;
2057
2058 Dxyrk_1m=(dxyrk1[1]+dxyrk1[2]+dxyrk1[3])*area/3.0;
2059
2060 Dxyrkx_re=(dxyrkrx[1]+dxyrkrx[2]+dxyrkrx[3])*area/3.0;
2061
2062 Dxyrkx_1m=(dxyrk1x[1]+dxyrk1x[2]+dxyrk1x[3])*area/3.0;
2063
2064 Dxyrky_re=(dxyrkry[1]+dxyrkry[2]+dxyrkry[3])*area/3.0;
2065
2066 Dxyrky_1m=(dxyrk1y[1]+dxyrk1y[2]+dxyrk1y[3])*area/3.0;
2067
2068
2069

```

```

}
/*****
/*
/* If the field point and the centroid are not coincident use the
/*
*****/

```

```

2073 /* numerical method described in Hammer for a quintic function */
2074 /* */
2075 /****** */
2076 /****** */
2077 else
2078 {
2079   r=(1.0+sqrt(15.0))/7.0;
2080   s=(1.0-sqrt(15.0))/7.0;
2081
2082   a=(155.-sqrt(15.0))*area/1200.;
2083   b=(155.+sqrt(15.0))*area/1200.;
2084   c=9.0*area/40.0;
2085
2086   xp[1]=ctrdx;
2087   yp[1]=ctrdy;
2088
2089   for(n=1;n<=3;n++)
2090   {
2091     xp[n+1]=r*x[n]+(1.0-r)*ctrdx;
2092     yp[n+1]=r*y[n]+(1.0-r)*ctrdy;
2093     xp[n+4]=s*x[n]+(1.0-s)*ctrdx;
2094     yp[n+4]=s*y[n]+(1.0-s)*ctrdy;
2095   }
2096
2097   for(n=1;n<=7;n++)
2098     R[n]=sqrt((xo-xp[n])*(xo-xp[n])+(yo-yp[n])*(yo-yp[n]));
2099
2100   for(n=1;n<=7;n++)
2101   {
2102
2103     rkr[n]=cos(k*R[n])/R[n]-1.0/R[n]+k*k*R[n]/2.0;
2104     rki[n]=sin(k*R[n])/R[n]-k;
2105     rkrx[n]=xp[n]*(cos(k*R[n])/R[n]-1.0/R[n]+k*k*R[n]/2.0);
2106     rkix[n]=xp[n]*(sin(k*R[n])/R[n]-k);
2107     rkry[n]=yp[n]*(cos(k*R[n])/R[n]-1.0/R[n]+k*k*R[n]/2.0);
2108     rkly[n]=yp[n]*(sin(k*R[n])/R[n]-k);
2109
2110     dx2rkr[n]=(3.*(xo-xp[n])*(xo-xp[n])/R[n]*R[n]-1.0-k*k
2111               *(xo-xp[n])*(xo-xp[n]))*cos(k*R[n])/pow(R[n],3)
2112               -(1.-3.*(xo-xp[n])*(xo-xp[n])/R[n]*R[n]))*k
2113               *sin(k*R[n])/R[n]*R[n]);
2114
2115     dx2rki[n]=(1.0-3.*(xo-xp[n])*(xo-xp[n])/R[n]*R[n]))*k*cos(k*R[n])
2116               /R[n]*R[n]+(3.*(xo-xp[n])*(xo-xp[n])/R[n]*R[n])-1.0
2117               -k*k*(xo-xp[n])*(xo-xp[n])*sin(k*R[n])/pow(R[n],3);
2118
2119     dx2rkrx[n]=xp[n]*(3.*(xo-xp[n])*(xo-xp[n])/R[n]*R[n])-1.0-k*k
2120               *(xo-xp[n])*(xo-xp[n])*cos(k*R[n])/pow(R[n],3)
2121               -(1.-3.*(xo-xp[n])*(xo-xp[n])/R[n]*R[n]))*k
2122               *sin(k*R[n])/R[n]*R[n]);
2123
2124     dx2rkiy[n]=xp[n]*((1.0-3.*(xo-xp[n])*(xo-xp[n])/R[n]*R[n]))*k*cos(k
2125               *R[n])/R[n]*R[n]+(3.*(xo-xp[n])*(xo-xp[n])/R[n]*R[n])-1.0
2126               -k*k*(xo-xp[n])*(xo-xp[n])*sin(k*R[n])/pow(R[n],3));
2127
2128

```

2129  
 2130 dx2rkry[n]=yp[n]\*((3.\*(xo-xp[n])\*(xo-xp[n]))/(R[n]\*R[n])-1.0-k\*k  
 2131 \*(xo-xp[n])\*(xo-xp[n]))\*cos(k\*R[n])/pow(R[n],3)  
 2132 -(1.-3.\*(xo-xp[n])\*(xo-xp[n]))/(R[n]\*R[n])\*k  
 2133 \*sin(k\*R[n])/R[n]\*R[n]);  
 2134  
 2135 dx2rk1y[n]=yp[n]\*((1.0-3.\*(xo-xp[n])\*(xo-xp[n]))/(R[n]\*R[n]))\*k\*cos(k  
 2136 \*R[n])/R[n]\*R[n]+(3.\*(xo-xp[n])\*(xo-xp[n]))/(R[n]\*R[n])-1.0  
 2137 -k\*k\*(xo-xp[n])\*(xo-xp[n]))\*sin(k\*R[n])/pow(R[n],3);  
 2138  
 2139  
 2140  
 2141 dy2rkr[n]=(3.\*(yo-yp[n])\*(yo-yp[n]))/(R[n]\*R[n])-1.0-k\*k\*(yo-yp[n])  
 2142 \*(yo-yp[n])\*cos(k\*R[n])/pow(R[n],3)-(1.-3.\*(yo-yp[n])\*(  
 2143 yo-yp[n]))/(R[n]\*R[n])\*k\*sin(k\*R[n])/R[n]\*R[n];  
 2144  
 2145 dy2rk1[n]=(1.0-3.\*(yo-yp[n])\*(yo-yp[n]))/(R[n]\*R[n])\*k\*cos(k\*R[n])  
 2146 /R[n]\*R[n]+(3.\*(yo-yp[n])\*(yo-yp[n]))/(R[n]\*R[n])-1.0  
 2147 -k\*k\*(yo-yp[n])\*(yo-yp[n]))\*sin(k\*R[n])/pow(R[n],3);  
 2148  
 2149 dy2rkrx[n]=xp[n]\*((3.\*(yo-yp[n])\*(yo-yp[n]))/(R[n]\*R[n])-1.0-k\*k\*(yo-  
 2150 yp[n])\*(yo-yp[n]))\*cos(k\*R[n])/pow(R[n],3)-(1.-3.\*(yo-yp[n])\*(  
 2151 yo-yp[n]))/(R[n]\*R[n])\*k\*sin(k\*R[n])/R[n]\*R[n];  
 2152  
 2153 dy2rk1x[n]=xp[n]\*((1.0-3.\*(yo-yp[n])\*(yo-yp[n]))/(R[n]\*R[n]))\*k\*cos(k  
 2154 \*R[n])/R[n]\*R[n]+(3.\*(yo-yp[n])\*(yo-yp[n]))/(R[n]\*R[n])-1.0  
 2155 -k\*k\*(yo-yp[n])\*(yo-yp[n]))\*sin(k\*R[n])/pow(R[n],3);  
 2156  
 2157 dy2rkry[n]=yp[n]\*((3.\*(yo-yp[n])\*(yo-yp[n]))/(R[n]\*R[n])-1.0-k\*k\*(yo-  
 2158 yp[n])\*(yo-yp[n]))\*cos(k\*R[n])/pow(R[n],3)-(1.-3.\*(yo-yp[n])\*(  
 2159 yo-yp[n]))/(R[n]\*R[n])\*k\*sin(k\*R[n])/R[n]\*R[n];  
 2160  
 2161 dy2rk1y[n]=yp[n]\*((1.0-3.\*(yo-yp[n])\*(yo-yp[n]))/(R[n]\*R[n]))\*k\*cos(k  
 2162 \*R[n])/R[n]\*R[n]+(3.\*(yo-yp[n])\*(yo-yp[n]))/(R[n]\*R[n])-1.0  
 2163 -k\*k\*(yo-yp[n])\*(yo-yp[n]))\*sin(k\*R[n])/pow(R[n],3);  
 2164  
 2165  
 2166  
 2167 dxyrkr[n]=((3.-k\*k\*R[n]\*R[n])\*cos(k\*R[n])+3.\*k\*R[n]\*sin(k\*R[n]))  
 2168 \*(xo-xp[n])\*(yo-yp[n])/pow(R[n],5);  
 2169  
 2170 dxyrk1[n]=((3.-k\*k\*R[n]\*R[n])\*sin(k\*R[n])-3.\*k\*R[n]\*cos(k\*R[n]))  
 2171 \*(xo-xp[n])\*(yo-yp[n])/pow(R[n],5);  
 2172  
 2173 dxyrkrx[n]=xp[n]\*((3.-k\*k\*R[n]\*R[n])\*cos(k\*R[n])+3.\*k\*R[n]\*sin(k  
 2174 \*R[n]))\*(xo-xp[n])\*(yo-yp[n])/pow(R[n],5);  
 2175  
 2176 dxyrk1x[n]=xp[n]\*((3.-k\*k\*R[n]\*R[n])\*sin(k\*R[n])-3.\*k\*R[n]\*cos(k  
 2177 \*R[n]))\*(xo-xp[n])\*(yo-yp[n])/pow(R[n],5);  
 2178  
 2179 dxyrkry[n]=yp[n]\*((3.-k\*k\*R[n]\*R[n])\*cos(k\*R[n])+3.\*k\*R[n]\*sin(k  
 2180 \*R[n]))\*(xo-xp[n])\*(yo-yp[n])/pow(R[n],5);  
 2181  
 2182 dxyrk1y[n]=yp[n]\*((3.-k\*k\*R[n]\*R[n])\*sin(k\*R[n])-3.\*k\*R[n]\*cos(k  
 2183 \*R[n]))\*(xo-xp[n])\*(yo-yp[n])/pow(R[n],5);  
 2184



```

2185 }
2186
2187
2188 Rk_re=c*rkr[1]+a*(rkr[2]+rkr[3]+rkr[4])+b*(rkr[5]+rkr[6]+rkr[7]);
2189 Rk_im=c*rki[1]+a*(rki[2]+rki[3]+rki[4])+b*(rki[5]+rki[6]+rki[7]);
2190 Rkx_re=c*rkrx[1]+a*(rkrx[2]+rkrx[3]+rkrx[4])+b*(rkrx[5]+rkrx[6]+rkrx[7]);
2191 Rkx_im=c*rkix[1]+a*(rkix[2]+rkix[3]+rkix[4])+b*(rkix[5]+rkix[6]+rkix[7]);
2192 Rky_re=c*rkry[1]+a*(rkry[2]+rkry[3]+rkry[4])+b*(rkry[5]+rkry[6]+rkry[7]);
2193
2194
2195 Dx2rk_re=c*dx2rkr[1]+a*(dx2rkr[2]+dx2rkr[3]+dx2rkr[4])+b
2196 * (dx2rkr[5]+dx2rkr[6]+dx2rkr[7]);
2197
2198 Dx2rk_im=c*dx2rki[1]+a*(dx2rki[2]+dx2rki[3]+dx2rki[4])+b
2199 * (dx2rki[5]+dx2rki[6]+dx2rki[7]);
2200
2201 Dx2rkr_re=c*dx2rkrx[1]+a*(dx2rkrx[2]+dx2rkrx[3]+dx2rkrx[4])+b
2202 * (dx2rkrx[5]+dx2rkrx[6]+dx2rkrx[7]);
2203
2204 Dx2rkr_im=c*dx2rki[1]+a*(dx2rki[2]+dx2rki[3]+dx2rki[4])+b
2205 * (dx2rki[5]+dx2rki[6]+dx2rki[7]);
2206
2207 Dx2rky_re=c*dx2rkry[1]+a*(dx2rkry[2]+dx2rkry[3]+dx2rkry[4])+b
2208 * (dx2rkry[5]+dx2rkry[6]+dx2rkry[7]);
2209
2210 Dx2rky_im=c*dx2rkiy[1]+a*(dx2rkiy[2]+dx2rkiy[3]+dx2rkiy[4])+b
2211 * (dx2rkiy[5]+dx2rkiy[6]+dx2rkiy[7]);
2212
2213
2214
2215 Dy2rk_re=c*dy2rkr[1]+a*(dy2rkr[2]+dy2rkr[3]+dy2rkr[4])+b
2216 * (dy2rkr[5]+dy2rkr[6]+dy2rkr[7]);
2217
2218 Dy2rk_im=c*dy2rki[1]+a*(dy2rki[2]+dy2rki[3]+dy2rki[4])+b
2219 * (dy2rki[5]+dy2rki[6]+dy2rki[7]);
2220
2221 Dy2rkr_re=c*dy2rkrx[1]+a*(dy2rkrx[2]+dy2rkrx[3]+dy2rkrx[4])+b
2222 * (dy2rkrx[5]+dy2rkrx[6]+dy2rkrx[7]);
2223
2224 Dy2rkr_im=c*dy2rki[1]+a*(dy2rki[2]+dy2rki[3]+dy2rki[4])+b
2225 * (dy2rki[5]+dy2rki[6]+dy2rki[7]);
2226
2227 Dy2rky_re=c*dy2rkry[1]+a*(dy2rkry[2]+dy2rkry[3]+dy2rkry[4])+b
2228 * (dy2rkry[5]+dy2rkry[6]+dy2rkry[7]);
2229
2230 Dy2rky_im=c*dy2rkiy[1]+a*(dy2rkiy[2]+dy2rkiy[3]+dy2rkiy[4])+b
2231 * (dy2rkiy[5]+dy2rkiy[6]+dy2rkiy[7]);
2232
2233
2234
2235 Dxyrk_re=c*dxyrkr[1]+a*(dxyrkr[2]+dxyrkr[3]+dxyrkr[4])+b
2236 * (dxyrkr[5]+dxyrkr[6]+dxyrkr[7]);
2237
2238 Dxyrk_im=c*dxyrki[1]+a*(dxyrki[2]+dxyrki[3]+dxyrki[4])+b
2239 * (dxyrki[5]+dxyrki[6]+dxyrki[7]);
2240 Dxyrkr_re=c*dxyrkrx[1]+a*(dxyrkrx[2]+dxyrkrx[3]+dxyrkrx[4])+b

```

```

2241      *(dxykrx[5]+dxykrx[6]+dxykrx[7]);
2242
2243      Dxyrkx_im=c*dxyrkix[1]+a*(dxyrkix[2]+dxyrkix[3]+dxyrkix[4])+b
2244      *(dxyrkix[5]+dxyrkix[6]+dxyrkix[7]);
2245
2246      Dxyrky_re=c*dxyrkry[1]+a*(dxyrkry[2]+dxyrkry[3]+dxyrkry[4])+b
2247      *(dxyrkry[5]+dxyrkry[6]+dxyrkry[7]);
2248
2249      Dxyrky_im=c*dxyrkly[1]+a*(dxyrkly[2]+dxyrkly[3]+dxyrkly[4])+b
2250      *(dxyrkly[5]+dxyrkly[6]+dxyrkly[7]);
2251    }
2252  }
2253  C NAASA 2.1.042 CGECO FTN-A 05-02-78 THE UNIV OF MICH COMP CTR
2254  SUBROUTINE CGECO(A,LDA,N,IPVT,RCOND,Z)
2255  IMPLICIT REAL*8(A-H,O-Z)
2256  INTEGER LDA,N,IPVT(1)
2257  COMPLEX*16 A(LDA,1),Z(1)
2258  REAL*8 RCOND
2259  C
2260  CGECO FACTORS A COMPLEX MATRIX BY GAUSSIAN ELIMINATION
2261  AND ESTIMATES THE CONDITION OF THE MATRIX.
2262  C
2263  IF RCOND IS NOT NEEDED, CGEFA IS SLIGHTLY FASTER.
2264  TO SOLVE A*X = B, FOLLOW CGECO BY CGESL.
2265  TO COMPUTE INVERSE(A)*C, FOLLOW CGECO BY CGESL.
2266  TO COMPUTE DETERMINANT(A), FOLLOW CGECO BY CGEDI.
2267  TO COMPUTE INVERSE(A), FOLLOW CGECO BY CGEDI.
2268  C
2269  ON ENTRY
2270  C
2271  A COMPLEX(LDA, N)
2272  THE MATRIX TO BE FACTORED.
2273  C
2274  LDA INTEGER
2275  THE LEADING DIMENSION OF THE ARRAY A.
2276  C
2277  N INTEGER
2278  THE ORDER OF THE MATRIX A.
2279  C
2280  ON RETURN
2281  C
2282  A AN UPPER TRIANGULAR MATRIX AND THE MULTIPLIERS
2283  WHICH WERE USED TO OBTAIN IT.
2284  THE FACTORIZATION CAN BE WRITTEN A = L*U WHERE
2285  L IS A PRODUCT OF PERMUTATION AND UNIT LOWER
2286  TRIANGULAR MATRICES AND U IS UPPER TRIANGULAR.
2287  C
2288  IPVT INTEGER(N)
2289  AN INTEGER VECTOR OF PIVOT INDICES.
2290  C
2291  RCOND REAL
2292  AN ESTIMATE OF THE RECIPROCAL CONDITION OF A.
2293  FOR THE SYSTEM A*X = B, RELATIVE PERTURBATIONS
2294  IN A AND B OF SIZE EPSILON MAY CAUSE
2295  RELATIVE PERTURBATIONS IN X OF SIZE EPSILON/RCOND.
2296  IF RCOND IS SO SMALL THAT THE LOGICAL EXPRESSION

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2297 C          1.0 + RCOND .EQ. 1.0
2298 C      IS TRUE, THEN A MAY BE SINGULAR TO WORKING
2299 C      PRECISION. IN PARTICULAR, RCOND IS ZERO IF
2300 C      EXACT SINGULARITY IS DETECTED OR THE ESTIMATE
2301 C      UNDERFLOWS.
2302 C
2303 C      Z      COMPLEX(N)
2304 C      A WORK VECTOR WHOSE CONTENTS ARE USUALLY UNIMPORTANT.
2305 C      IF A IS CLOSE TO A SINGULAR MATRIX, THEN Z IS
2306 C      AN APPROXIMATE NULL VECTOR IN THE SENSE THAT
2307 C       $NORM(A*Z) = RCOND * NORM(A) * NORM(Z)$  .
2308 C
2309 C      LINPACK. THIS VERSION DATED 07/14/77
2310 C      CLEVE MOLER, UNIVERSITY OF NEW MEXICO, ARGONNE NATIONAL LABS.
2311 C
2312 C      SUBROUTINES AND FUNCTIONS
2313 C
2314 C      LINPACK CGEFA
2315 C      BLAS CAXPY, CDOTC, CSSCAL, SCASUM
2316 C      FORTRAN DABS, DIMAG, DMAX1, DCMPLX, DCONJG, REAL
2317 C
2318 C      INTERNAL VARIABLES
2319 C
2320 C      IMPLICIT REAL*8(A-H,O-Z)
2321 C      COMPLEX*16 CDOTC,EK,I,WK,WKM
2322 C      REAL*8 ANORM,S,SCASUM,SM,YNORM
2323 C      INTEGER INFO,J,K,KB,KP1,L
2324 C
2325 C      COMPLEX*16 ZDUM,ZDUM1,ZDUM2,CSIGN1
2326 C      REAL*8 CABS1
2327 C      CABS1(ZDUM) = DABS(DREAL(ZDUM)) + DABS(DIMAG(ZDUM))
2328 C      CSIGN1(ZDUM1,ZDUM2) = CABS1(ZDUM1)*(ZDUM2/CABS1(ZDUM2))
2329 C
2330 C      COMPUTE 1-NORM OF A
2331 C
2332 C      ANORM = 0.0D0
2333 C      DO 10 J = 1, N
2334 C          ANORM = DMAX1(ANORM,SCASUM(N,A(1,J),1))
2335 C      10 CONTINUE
2336 C
2337 C      FACTOR
2338 C
2339 C      CALL CGEFA(A,LDA,N,IPVT,INFO)
2340 C
2341 C      RCOND = 1/(NORM(A)*(ESTIMATE OF NORM(INVERSE(A))))
2342 C      ESTIMATE = NORM(Z)/NORM(Y) WHERE A*Z = Y AND CTRANS(A)*Y = E .
2343 C      CTRANS(A) IS THE CONJUGATE TRANSPOSE OF A .
2344 C      THE COMPONENTS OF E ARE CHOSEN TO CAUSE MAXIMUM LOCAL
2345 C      GROWTH IN THE ELEMENTS OF W WHERE CTRANS(U)*W = E .
2346 C      THE VECTORS ARE FREQUENTLY RESCALED TO AVOID OVERFLOW.
2347 C
2348 C      SOLVE CTRANS(U)*W = E
2349 C
2350 C      EK = DCMPLX(1.0D0,0.0D0)
2351 C      DO 20 J = 1, N
2352 C          Z(J) = DCMPLX(0.0D0,0.0D0)

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2353 20 CONTINUE
2354 DO 100 K = 1, N
2355 IF (CABS1(Z(K)) .NE. 0.0D0) EK = CSIGN1(EK, -Z(K))
2356 IF (CABS1(EK-Z(K)) .LE. CABS1(A(K,K))) GO TO 30
2357 S = CABS1(A(K,K))/CABS1(EK-Z(K))
2358 CALL CSSCAL(N,S,Z,1)
2359 EK = DCPLX(S,0.0D0)*EK
2360 CONTINUE
2361 WK = EK - Z(K)
2362 WKM = -EK - Z(K)
2363 S = CABS1(WK)
2364 SM = CABS1(WKM)
2365 IF (CABS1(A(K,K)) .EQ. 0.0D0) GO TO 40
2366 WK = WK/DCONJG(A(K,K))
2367 WKM = WKM/DCONJG(A(K,K))
2368 GO TO 50
2369 CONTINUE
2370 WK = DCPLX(1.0D0,0.0D0)
2371 WKM = DCPLX(1.0D0,0.0D0)
2372 CONTINUE
2373 KP1 = K + 1
2374 IF (KP1 .GT. N) GO TO 80
2375 DO 60 J = KP1, N
2376 SM = SM + CABS1(Z(J)+WKM*DCONJG(A(K,J)))
2377 Z(J) = Z(J) + WK*DCONJG(A(K,J))
2378 S = S + CABS1(Z(J))
2379 CONTINUE
2380 IF (S .GE. SM) GO TO 80
2381 T = WKM - WK
2382 WK = WKM
2383 DO 70 J = KP1, N
2384 Z(J) = Z(J) + T*DCONJG(A(K,J))
2385 CONTINUE
2386 CONTINUE
2387 Z(K) = WK
2388 CONTINUE
2389 S = 1.0D0/SCASUM(N,Z,1)
2390 CALL CSSCAL(N,S,Z,1)
2391 C
2392 C
2393 C
2394 C
2395 DO 120 KB = 1, N
2396 K = N + 1 - KB
2397 IF (K .LT. N) Z(K) = Z(K) + CDOTC(N-K,A(K+1,K),1,Z(K+1),1)
2398 IF (CABS1(Z(K)) .LE. 1.0D0) GO TO 110
2399 S = 1.0D0/CABS1(Z(K))
2400 CALL CSSCAL(N,S,Z,1)
2401 CONTINUE
2402 L = IPVT(K)
2403 T = Z(L)
2404 Z(L) = Z(K)
2405 Z(K) = T
2406 CONTINUE
2407 S = 1.0D0/SCASUM(N,Z,1)
2408 CALL CSSCAL(N,S,Z,1)

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2409 C
2410 YNORM = 1.0D0
2411 C
2412 SOLVE L*V = Y
2413 C
2414 DO 140 K = 1, N
2415 L = IPVT(K)
2416 T = Z(L)
2417 Z(L) = Z(K)
2418 Z(K) = T
2419 IF (K.LT.N) CALL CAXPY(N-K,T,A(K+1,K),1,Z(K+1),1)
2420 IF (CABS1(Z(K)) .LE. 1.0D0) GO TO 130
2421 S = 1.0D0/CABS1(Z(K))
2422 CALL CSSCAL(N,S,Z,1)
2423 YNORM = S*YNORM
2424
2425 130 CONTINUE
2426 140 CONTINUE
2427 S = 1.0D0/SCASUM(N,Z,1)
2428 CALL CSSCAL(N,S,Z,1)
2429 YNORM = S*YNORM
2430 C
2431 SOLVE U*Z = V
2432 C
2433 DO 160 KB = 1, N
2434 K = N + 1 - KB
2435 IF (CABS1(Z(K)) .LE. CABS1(A(K,K))) GO TO 150
2436 S = CABS1(A(K,K))/CABS1(Z(K))
2437 CALL CSSCAL(N,S,Z,1)
2438 YNORM = S*YNORM
2439 150 CONTINUE
2440 IF (CABS1(A(K,K)) .NE. 0.0D0) Z(K) = Z(K)/A(K,K)
2441 IF (CABS1(A(K,K)) .EQ. 0.0D0) Z(K) = DCMLPX(1.0D0,0.0D0)
2442 T = -Z(K)
2443 CALL CAXPY(K-1,T,A(1,K),1,Z(1),1)
2444 160 CONTINUE
2445 C
2446 MAKE ZNORM = 1.0
2447 S = 1.0D0/SCASUM(N,Z,1)
2448 CALL CSSCAL(N,S,Z,1)
2449 YNORM = S*YNORM
2450 C
2451 IF (ANORM .NE. 0.0D0) RCOND = YNORM/ANORM
2452 IF (ANORM .EQ. 0.0D0) RCOND = 0.0D0
2453 RETURN
2454 END
2455 C
2456 NAASA 2.1.044 CGESL FTN-A 05-02-78 THE UNIV OF MICH COMP CTR
2457 SUBROUTINE CGESL(A,LDA,N,IPVT,B,JOB)
2458 IMPLICIT REAL*8(A-H,O-Z)
2459 INTEGER LDA,N,IPVT(1),JOB
2460 COMPLEX*16 A(LDA,1),B(1)
2461 C
2462 CGESL SOLVES THE COMPLEX SYSTEM
2463 A * X = B OR CTRANS(A) * X = B
2464 USING THE FACTORS COMPUTED BY CGECO OR CGEFA.
2465 ON ENTRY
2466 C
2467 C
2468 C
2469 C
2470 C
2471 C
2472 C
2473 C
2474 C
2475 C
2476 C
2477 C
2478 C
2479 C
2480 C
2481 C
2482 C
2483 C
2484 C
2485 C
2486 C
2487 C
2488 C
2489 C
2490 C
2491 C
2492 C
2493 C
2494 C
2495 C
2496 C
2497 C
2498 C
2499 C
2500 C

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2465 C      A      COMPLEX(LDA, N)
2466 C      THE OUTPUT FROM CGECO OR CGEFA.
2467 C
2468 C      LDA      INTEGER
2469 C      THE LEADING DIMENSION OF THE ARRAY A .
2470 C
2471 C      N      INTEGER
2472 C      THE ORDER OF THE MATRIX A .
2473 C
2474 C      IPVT     INTEGER(N)
2475 C      THE PIVOT VECTOR FROM CGECO OR CGEFA.
2476 C
2477 C      B      COMPLEX(N)
2478 C      THE RIGHT HAND SIDE VECTOR.
2479 C
2480 C      JOB      INTEGER
2481 C      = 0      TO SOLVE A*X = B
2482 C      = NONZERO TO SOLVE CTRANS(A)*X = B WHERE
2483 C      CTRANS(A) IS THE CONJUGATE TRANSPOSE.
2484 C
2485 C      ON RETURN
2486 C
2487 C      B      THE SOLUTION VECTOR X .
2488 C
2489 C      ERROR CONDITION
2490 C
2491 C      A DIVISION BY ZERO WILL OCCUR IF THE INPUT FACTOR CONTAINS A
2492 C      ZERO ON THE DIAGONAL. TECHNICALLY THIS INDICATES SINGULARITY
2493 C      BUT IT IS OFTEN CAUSED BY IMPROPER ARGUMENTS OR IMPROPER
2494 C      SETTING OF LDA . IT WILL NOT OCCUR IF THE SUBROUTINES ARE
2495 C      CALLED CORRECTLY AND IF CGECO HAS SET RCOND .GT. 0.0
2496 C      OR CGEFA HAS SET INFO .EQ. 0 .
2497 C
2498 C      TO COMPUTE INVERSE(A) * C WHERE C IS A MATRIX
2499 C      WITH P COLUMNS
2500 C      CALL CGECO(A,LDA,N,IPVT,RCOND,Z)
2501 C      IF (RCOND IS TOO SMALL) GO TO ...
2502 C      DO 10 J = 1, P
2503 C      CALL CGESL(A,LDA,N,IPVT,C(1,J),0)
2504 C      10 CONTINUE
2505 C
2506 C      LINPACK. THIS VERSION DATED 07/14/77 .
2507 C      CLEVE MOLER, UNIVERSITY OF NEW MEXICO, ARGONNE NATIONAL LABS.
2508 C
2509 C      SUBROUTINES AND FUNCTIONS
2510 C
2511 C      BLAS CAXPY,CDOTC
2512 C      FORTRAN DCONJG
2513 C
2514 C      INTERNAL VARIABLES
2515 C
2516 C      COMPLEX*16 CDOTC,T
2517 C      INTEGER K,KB,L,NM1
2518 C
2519 C      NM1 = N - 1
2520 C      IF (JOB .NE. 0) GO TO 60

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2521 C
2522 C      JOB = 0 , SOLVE  A * X = B
2523 C      FIRST SOLVE  L*Y = B
2524 C
2525 C      IF (NM1 .LT. 1) GO TO 30
2526 C      DO 20 K = 1, NM1
2527 C      L = IPVT(K)
2528 C      T = B(L)
2529 C      IF (L .EQ. K) GO TO 10
2530 C      B(L) = B(K)
2531 C      B(K) = T
2532 C      CONTINUE
2533 C      CALL CAXPY(N-K,T,A(K+1,K),1,B(K+1),1)
2534 C      CONTINUE
2535 C      CONTINUE
2536 C
2537 C      NOW SOLVE  U*X = Y
2538 C
2539 C      DO 40 KB = 1, N
2540 C      K = N + 1 - KB
2541 C      B(K) = B(K)/A(K,K)
2542 C      T = -B(K)
2543 C      CALL CAXPY(K-1,T,A(1,K),1,B(1),1)
2544 C      CONTINUE
2545 C      GO TO 100
2546 C      CONTINUE
2547 C
2548 C      JOB = NONZERO. SOLVE  CTRANS(A) * X = B
2549 C      FIRST SOLVE  CTRANS(U)*Y = B
2550 C
2551 C      DO 60 K = 1, N
2552 C      T = CDOTC(K-1,A(1,K),1,B(1),1)
2553 C      B(K) = (B(K) - T)/DCONJG(A(K,K))
2554 C      CONTINUE
2555 C
2556 C      NOW SOLVE  CTRANS(L)*X = Y
2557 C
2558 C      IF (NM1 .LT. 1) GO TO 90
2559 C      DO 80 KB = 1, NM1
2560 C      K = N - KB
2561 C      B(K) = B(K) + CDOTC(N-K,A(K+1,K),1,B(K+1),1)
2562 C      L = IPVT(K)
2563 C      IF (L .EQ. K) GO TO 70
2564 C      T = B(L)
2565 C      B(L) = B(K)
2566 C      B(K) = T
2567 C      CONTINUE
2568 C      CONTINUE
2569 C      CONTINUE
2570 C      CONTINUE
2571 C      RETURN
2572 C      END
2573 C      NAASA 2.1.043 CGEFA  FTN-A 05-02-78
2574 C      SUBROUTINE CGEFA(A,LDA,N,IPVT,INFO)
2575 C      IMPLICIT REAL*8(A-H,O-Z)
2576 C      INTEGER LDA,N,IPVT(1),INFO

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2577 C COMPLEX\*16 A(LDA,1)  
 2578 C CGEFA FACTORS A COMPLEX MATRIX BY GAUSSIAN ELIMINATION.  
 2579 C  
 2580 C CGEFA IS USUALLY CALLED BY CGECO, BUT IT CAN BE CALLED  
 2581 C DIRECTLY WITH A SAVING IN TIME IF RCOND IS NOT NEEDED.  
 2582 C (TIME FOR CGECO) = (1 + 9/N)\*(TIME FOR CGEFA)  
 2583 C  
 2584 C ON ENTRY  
 2585 C  
 2586 C A COMPLEX(LDA, N)  
 2587 C THE MATRIX TO BE FACTORED.  
 2588 C  
 2589 C LDA INTEGER  
 2590 C THE LEADING DIMENSION OF THE ARRAY A .  
 2591 C  
 2592 C N INTEGER  
 2593 C THE ORDER OF THE MATRIX A .  
 2594 C  
 2595 C ON RETURN  
 2596 C  
 2597 C A AN UPPER TRIANGULAR MATRIX AND THE MULTIPLIERS  
 2598 C WHICH WERE USED TO OBTAIN IT.  
 2599 C THE FACTORIZATION CAN BE WRITTEN A = L\*U WHERE  
 2600 C L IS A PRODUCT OF PERMUTATION AND UNIT LOWER  
 2601 C TRIANGULAR MATRICES AND U IS UPPER TRIANGULAR.  
 2602 C  
 2603 C IPVT INTEGER(N)  
 2604 C AN INTEGER VECTOR OF PIVOT INDICES.  
 2605 C  
 2606 C INFO INTEGER  
 2607 C = 0 NORMAL VALUE.  
 2608 C = K IF U(K,K).EQ. 0.0 . THIS IS NOT AN ERROR  
 2609 C CONDITION FOR THIS SUBROUTINE, BUT IT DOES  
 2610 C INDICATE THAT CGESL OR CGEDI WILL DIVIDE BY ZERO  
 2611 C IF CALLED. USE RCOND IN CGECO FOR A RELIABLE  
 2612 C INDICATION OF SINGULARITY.  
 2613 C  
 2614 C LINPACK. THIS VERSION DATED 07/14/77  
 2615 C CLEVE MOLER, UNIVERSITY OF NEW MEXICO, ARGONNE NATIONAL LABS.  
 2616 C  
 2617 C SUBROUTINES AND FUNCTIONS  
 2618 C  
 2619 C BLAS CAXPY,CSCAL,ICAMAX  
 2620 C FORTRAN DABS,DIMAG,DCMPLX,DREAL  
 2621 C  
 2622 C INTERNAL VARIABLES  
 2623 C  
 2624 C COMPLEX\*16 T  
 2625 C INTEGER ICAMAX,J,K,KP1,L,NM1  
 2626 C  
 2627 C COMPLEX\*16 ZDUM  
 2628 C REAL\*8 CABS1  
 2629 C CABS1(ZDUM) = DABS(DREAL(ZDUM)) + DABS(DIMAG(ZDUM))  
 2630 C  
 2631 C GAUSSIAN ELIMINATION WITH PARTIAL PIVOTING  
 2632 C



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2633 C
2634 INFO = 0
2635 NM1 = N - 1
2636 IF (NM1 .LT. 1) GO TO 70
2637 DO 60 K = 1, NM1
2638 KP1 = K + 1
2639 C
2640 FIND L = PIVOT INDEX
2641 C
2642 L = ICAMAX(N-K+1,A(K,K),1) + K - 1
2643 IPVT(K) = L
2644 C
2645 ZERO PIVOT IMPLIES THIS COLUMN ALREADY TRIANGULARIZED
2646 C
2647 IF (CABS1(A(L,K)) .EQ. 0.0D0) GO TO 40
2648 C
2649 INTERCHANGE IF NECESSARY
2650 C
2651 IF (L .EQ. K) GO TO 10
2652 T = A(L,K)
2653 A(L,K) = A(K,K)
2654 A(K,K) = T
2655 CONTINUE
2656 C
2657 COMPUTE MULTIPLIERS
2658 C
2659 T = -DCMPLX(1.0D0,0.0D0)/A(K,K)
2660 CALL CSCAL(N-K,T,A(K+1,K),1)
2661 C
2662 ROW ELIMINATION WITH COLUMN INDEXING
2663 C
2664 DO 30 J = KP1, N
2665 T = A(L,J)
2666 IF (L .EQ. K) GO TO 20
2667 A(L,J) = A(K,J)
2668 A(K,J) = T
2669 CONTINUE
2670 CALL CAXPY(N-K,T,A(K+1,K),1,A(K+1,J),1)
2671 C
2672 GO TO 50
2673 CONTINUE
2674 INFO = K
2675 C
2676 CONTINUE
2677 C
2678 IPVT(N) = N
2679 IF (CABS1(A(N,N)) .EQ. 0.0D0) INFO = N
2680 RETURN
2681 END
2682 C NAASA 1.1.014 CAXPY FTN-A 05-02-78 THE UNIV OF MICH COMP CTR
2683 SUBROUTINE CAXPY(N,CA,CX,INCY,INCX,CY,INCY)
2684 C
2685 CONSTANT TIMES A VECTOR PLUS A VECTOR.
2686 JACK DONGARRA, LINPACK, 6/17/77.
2687 C
2688 IMPLICIT REAL*8(A-H,O-Z)

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2689 COMPLEX*16 CX(1),CY(1),CA
2690 INTEGER I,INCX,INCY,IX,IY,N
2691 C
2692 IF(N.LE.0)RETURN
2693 IF(DABS(DREAL(CA)) + DABS(DIMAG(CA)) .EQ. 0.0D0 ) RETURN
2694 IF(INCX.EQ.1.AND.INCY.EQ.1)GOTO 20
2695 C
2696 CODE FOR UNEQUAL INCREMENTS OR EQUAL INCREMENTS
2697 C NOT EQUAL TO 1
2698 C
2699 IX = 1
2700 IY = 1
2701 IF(INCX.LT.0)IX = (-N+1)*INCX + 1
2702 IF(INCY.LT.0)IY = (-N+1)*INCY + 1
2703 DO 10 I = 1,N
2704 CY(IY) = CY(IY) + CA*CX(IX)
2705 IX = IX + INCX
2706 IY = IY + INCY
2707 10 CONTINUE
2708 RETURN
2709 C
2710 CODE FOR BOTH INCREMENTS EQUAL TO 1
2711 C
2712 DO 30 I = 1,N
2713 CY(I) = CY(I) + CA*CX(I)
2714 30 CONTINUE
2715 RETURN
2716 END
2717 C NAASA 1.1.012 CDOTC FTN-A 05-02-78 THE UNIV OF MICH COMP CTR
2718 COMPLEX*16 FUNCTION CDOTC(N,CX,INCX,CY,INCY)
2719 C
2720 FORMS THE DOT PRODUCT OF TWO VECTORS, CONJUGATING THE FIRST
2721 VECTOR.
2722 C JACK DONGARRA, LINPACK, 6/17/77.
2723 C
2724 IMPLICIT REAL*8(A-H,O-Z)
2725 COMPLEX*16 CX(1),CY(1),CTEMP
2726 INTEGER I,INCX,INCY,IX,IY,N
2727 C
2728 CTEMP = DCMLPX(0.0D0,0.0D0)
2729 CDOTC = DCMLPX(0.0D0,0.0D0)
2730 IF(N.LE.0)RETURN
2731 IF(INCX.EQ.1.AND.INCY.EQ.1)GOTO 20
2732 C
2733 CODE FOR UNEQUAL INCREMENTS OR EQUAL INCREMENTS
2734 C NOT EQUAL TO 1
2735 C
2736 IX = 1
2737 IY = 1
2738 IF(INCX.LT.0)IX = (-N+1)*INCX + 1
2739 IF(INCY.LT.0)IY = (-N+1)*INCY + 1
2740 DO 10 I = 1,N
2741 CTEMP = CTEMP + DCONJG(CX(IX))*CY(IY)
2742 IX = IX + INCX
2743 IY = IY + INCY
2744 10 CONTINUE

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2745      CDOIC = CTEMP
2746      RETURN
2747      C
2748      C      CODE FOR BOTH INCREMENTS EQUAL TO 1
2749      C
2750      20 DO 30 I = 1,N
2751          CTEMP = CTEMP + DCONJG(CX(I))*CY(I)
2752      30 CONTINUE
2753      CDOIC = CTEMP
2754      RETURN
2755      END
2756      C NAASA 1.1.018 CSSCAL FTN-A 05-02-78 THE UNIV OF MICH COMP CTR
2757      SUBROUTINE CSSCAL(N,SA,CX,INCX)
2758      C
2759      C      SCALES A COMPLEX VECTOR BY A REAL CONSTANT.
2760      C      JACK DONGARRA, LINPACK, 6/17/77.
2761      C
2762      IMPLICIT REAL*8(A-H,O-Z)
2763      COMPLEX*16 CX(1)
2764      REAL*8 SA
2765      INTEGER I, INCX, N, NINCX
2766      C
2767      IF(N.LE.0)RETURN
2768      IF(INCX.EQ.1)GOTO 20
2769      C
2770      C      CODE FOR INCREMENT NOT EQUAL TO 1
2771      C
2772      NINCX = N*INCX
2773      DO 10 I = 1,NINCX,INCX
2774          CX(I) = DCMLX(SA*DREAL(CX(I)),SA*DIMAG(CX(I)))
2775      10 CONTINUE
2776      RETURN
2777      C
2778      C      CODE FOR INCREMENT EQUAL TO 1
2779      C
2780      20 DO 30 I = 1,N
2781          CX(I) = DCMLX(SA*DREAL(CX(I)),SA*DIMAG(CX(I)))
2782      30 CONTINUE
2783      RETURN
2784      END
2785      C NAASA 1.1.010 SCASUM FTN-A 05-02-78 THE UNIV OF MICH COMP CTR
2786      REAL*8 FUNCTION SCASUM(N,CX,INCX)
2787      C
2788      C      TAKES THE SUM OF THE ABSOLUTE VALUES OF A COMPLEX VECTOR AND
2789      C      RETURNS A SINGLE PRECISION RESULT.
2790      C      JACK DONGARRA, LINPACK, 6/17/77.
2791      C
2792      IMPLICIT REAL*8(A-H,O-Z)
2793      COMPLEX*16 CX(1)
2794      REAL*8 STEMP
2795      INTEGER I, INCX, N, NINCX
2796      C
2797      SCASUM = 0.0D0
2798      STEMP = 0.0D0
2799      IF(N.LE.0)RETURN
2800      IF(INCX.EQ.1)GOTO 20

```

```

2801 C
2802 C CODE FOR INCREMENT NOT EQUAL TO 1
2803 C
2804 NINCX = N*INCX
2805 DO 10 I = 1,NINCX,INCX
2806 STEMP = STEMP + DABS(DREAL(CX(I))) + DABS(DIMAG(CX(I)))
2807 10 CONTINUE
2808 SCASUM = STEMP
2809 RETURN
2810 C
2811 C CODE FOR INCREMENT EQUAL TO 1
2812 C
2813 20 DO 30 I = 1,N
2814 STEMP = STEMP + DABS(DREAL(CX(I))) + DABS(DIMAG(CX(I)))
2815 30 CONTINUE
2816 SCASUM = STEMP
2817 RETURN
2818 END
2819 C NAASA 1.1.019 CSCAL FTN-A 05-02-78 THE UNIV OF MICH COMP CTR
2820 SUBROUTINE CSCAL(N,CA,CX,INCX)
2821 C
2822 C SCALES A VECTOR BY A CONSTANT.
2823 C JACK DONGARRA, LINPACK, 6/17/77.
2824 C
2825 C IMPLICIT REAL*8 (A-H,O-Z)
2826 C COMPLEX*16 CA,CX(1)
2827 C INTEGER I,INCX,N,NINCX
2828 C
2829 C IF(N.LE.0)RETURN
2830 C IF(INCX.EQ.1)GOTO 20
2831 C
2832 C CODE FOR INCREMENT NOT EQUAL TO 1
2833 C
2834 NINCX = N*INCX
2835 DO 10 I = 1,NINCX,INCX
2836 CX(I) = CA*CX(I)
2837 10 CONTINUE
2838 RETURN
2839 C
2840 C CODE FOR INCREMENT EQUAL TO 1
2841 C
2842 20 DO 30 I = 1,N
2843 CX(I) = CA*CX(I)
2844 30 CONTINUE
2845 RETURN
2846 END
2847 C NAASA 1.1.021 ICAMAX FTN-A 05-02-78 THE UNIV OF MICH COMP CTR
2848 INTEGER FUNCTION ICAMAX(N,CX,INCX)
2849 C
2850 C FINDS THE INDEX OF ELEMENT HAVING MAX. ABSOLUTE VALUE.
2851 C JACK DONGARRA, LINPACK, 6/17/77.
2852 C
2853 C IMPLICIT REAL*8 (A-H,O-Z)
2854 C COMPLEX*16 CX(1)
2855 C REAL*8 SMAX
2856 C INTEGER I,INCX,IX,N

```

```

2857 COMPLEX*16 ZDUM
2858 REAL*8 CABS1
2859 CABS1(ZDUM) = DABS(DREAL(ZDUM)) + DABS(DIMAG(ZDUM))
2860 C
2861 ICAMAX = 1
2862 IF(N.LE.1)RETURN
2863 IF(INCX.EQ.1)GOTO 20
2864 C
2865 C CODE FOR INCREMENT NOT EQUAL TO 1
2866 C
2867 IX = 1
2868 SMAX = CABS1(CX(1))
2869 IX = IX + INCX
2870 DO 10 I = 2,N
2871 IF(CABS1(CX(IX)) .LE. SMAX) GO TO 5
2872 ICAMAX = I
2873 SMAX = CABS1(CX(IX))
2874 5 IX = IX + INCX
2875 10 CONTINUE
2876 RETURN
2877 C
2878 C CODE FOR INCREMENT EQUAL TO 1
2879 C
2880 20 SMAX = CABS1(CX(1))
2881 DO 30 I = 2,N
2882 IF(CABS1(CX(I)) .LE. SMAX) GO TO 30
2883 ICAMAX = I
2884 30 SMAX = CABS1(CX(I))
2885 CONTINUE
2886 RETURN
2887 END
2888 CCCCCCCCCCCCCCCCCCCCCC
2889 C DREAL DOESN'T SEEM TO WORK, SO THIS FUNCTION IS A SUBSTITUTE
2890 REAL*8 FUNCTION DREAL(X)
2891 COMPLEX*16 X,X2
2892 REAL*8 XA(2)
2893 EQUIVALENCE (X2,XA(1))
2894 X2=X
2895 DREAL=XA(1)
2896 RETURN
2897 END

```