

# PURIFICATION FACTOR CHARACTERIZATION OF ZONE REFINING

BY

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## ABSTRACT

A quantity  $\pi_T$ , termed the purification factor, defines the potential state of purity realizable in a specimen that has undergone zone-refinement treatment. An exact analysis appears intractable, but neglect of the terminal zone perturbation (which becomes vanishingly small for the infinite ingot) allows a lower bound to be established on the remanent solute impurity. Such numerical values of  $\pi_T$  are evaluated for some sensible distribution coefficients and zone dimensions involving a maximum of ten passes. An original expression for the solute impurity distribution is deduced and numerically appraised for a range of operational conditions not presently tabulated; the relation has been applied to the indicated  $\pi_T$  determinations.

## INTRODUCTION

The purpose here is to describe in some detail a useful parameter for characterizing the progress made at any stage of the zone-refining process. In doing so, it may also be of value to present still another manner for expressing the impurity distribution which evidently lends itself more readily to numerical calculation. Thus a quantity identified as a purification factor is explicitly evaluated for a range of conditions considered to be representative of zone-refining practice.

Actually, the present treatment is restricted to an upper bound identification of the degree of purification attained during the refinement procedure; analytic treatment of the terminal zone effect does not appear to be tractable, although the correction could be numerically evaluated. The technique of terminal zone cropping tends to moderate the departure from the ideal purification factor since it operates to offset the approach to an equilibrium impurity distribution. A brief description of this approach was offered earlier (1).<sup>3</sup>

## IMPURITY BALANCE AND THE PURIFICATION FACTOR

A simple impurity balance may be posed ignoring the terminal zone perturbation. Conservation of solute in an ingot of length  $L$  having an initial distribution  $C_0(x)$  may be represented as follows:

$$\sum S = C_0 L = S_T = S_{I,n} + S_{II,n} + S_{III,n-1} + \sum_{n=1} S_{f,n-1} \quad (1)$$

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<sup>3</sup> The boldface numbers in parentheses refer to the references appended to this paper.

where the total impurity solute  $S_T$  is expressed in terms of the components  $S_{I,n}$ , the solute in the purified zone after the  $n^{\text{th}}$  pass,  $S_{II,n}$ , the solute in the liquid zone,  $S_{III,n-1}$ , the solute in the remaining ingot from the previous pass, exclusive of the terminal zone, which must be summed over  $S_{f,n-1}$  for the maximum accumulation of impurity after  $n - 1$  passes.

The compartmental distribution of impurity then is prescribed by the relations

$$S_{I,n} = \int_0^x C_n(x) dx \quad (2a)$$

$$S_{II,n} = \frac{l}{k} C_n(x) \quad (2b)$$

$$S_{III,n-1} = \int_{x+l}^{L-l} C_{n-1}(x) dx \quad (2c)$$

$$S_{f,n-1} = lC_{n-1}(x) \Big|_{x=L-l} \quad (2d)$$

where  $l$  is the zone length and  $k$  is the solute distribution coefficient.

Thus for the fraction of solute impurity removed after the  $n^{\text{th}}$  pass  $P_n$  there derives

$$P_n = \frac{1}{C_0 L} \int_0^{L-l} [C_{n-1}(x) - C_n(x)] dx \quad (3)$$

whereas for the cumulative removal of impurity it follows that

$$P_T = \sum_n P_n = \left( C_0 L - \int_0^{L-l} C_n(x) dx \right) (C_0 L)^{-1}. \quad (4)$$

The fraction of impurity yet to be transferred to the terminal zone may be defined as the purification factor  $\pi_T$  and is clearly the result

$$\pi_T = 1 - P_T. \quad (5)$$

Explicit calculation of the purification factor demands identification of  $C_n(x)$  and the subsequent evaluation of Eq. 4; the next section deals with this aspect.

#### ELABORATION OF THE $P_T$ RELATION<sup>4</sup>: A NEW FORM FOR $C_n(X)$

The detailed calculations of the purification factors are based upon a form of  $C_n(x)$  not previously described in the literature (2). Starting with the underlying equation (3) which specifies the spatial distribution

<sup>4</sup> The usual idealizations are embodied as, for example, perfect mixing of components in the liquidus, limited diffusion in the solidus, etc.

of solute

$$\frac{dS_n(x)}{dx} = C_{(n-1)}(x) - \frac{k}{l} S_n(x) \quad (6)$$

the solution may readily be shown to be of the form

$$S_n(x) = e^{-(k/l)x} \left\{ \int_0^x C_{(n-1)} e^{(k/l)x} dx + K_{(n-1)} \right\} \quad (7)$$

wherein the  $K_{(n-1)}$  are integration constants prescribed by the initial condition

$$C_n(x)|_{x=0} = k\bar{c}, \quad \bar{c} = \frac{1}{l} \int_0^l C_{(n-1)}(x) dx \quad (8)$$

when utilized in conjunction with

$$C_n(x) = \frac{k}{l} S_n(x). \quad (9)$$

In the appendix are provided details for the inductive prescription of  $Q_n(x)$  in the generalized form of  $C_n(x)$  which resembles that of the single pass result:

$$C_n(x)/C_0 = 1 - Q_n(1 - k)e^{-(k/l)x} \quad (10a)$$

with

$$Q_n = \sum_{p=n}^1 A_p \frac{\left(\frac{k}{l}x\right)^{n-p}}{(n-p)!} \quad (10b)$$

and the diverse  $A_p$  in turn given by

$$A_j = 1 - \frac{A_{j-1}S_1}{0!} - \frac{A_{j-2}S_2}{1!} - \frac{A_{j-3}S_3}{2!} - \dots - \frac{A_{2j}S_{j-2}}{(j-3)!} + \frac{1}{(j-2)!} \left(\frac{k}{l}\right)^{j-1} \int_0^l x^{j-2} e^{-(k/l)x} dx. \quad (10c)$$

In (10c) the  $S_m$  takes on values determined from

$$S_m = - \int_0^k x^{m-1} e^{-x} dx = - \left[ \int k^{m-1} e^{-k} dk + (m-1)! \right]. \quad (10d)$$

Typically, for  $j = 1$ ,  $A_1 = 1$  and  $Q_1 = 1$ .

In Table I are collected the solute distributions  $C_n(x)/C_0$  as a function of  $x/l$  for  $n = 1$  to 10 with  $k$  values selected as 0.001, 0.007, 0.05, 0.07 and 0.12. The over-all behavior of the solute distribution is exhibited in Figs. 1-6; two different ranges are displayed in Figs. 1 and 2, with the latter appropriate for small  $x/l$  and  $k = 0.001$ . Other values

TABLE I.— $-C_n(x)/C_0$  vs  $x/1$  Data for  $k = 0.001, 0.007, 0.05, 0.07, 0.12$ .

TABLE I.—*Continued.*

$\frac{C_1(x)}{C_0}$	$\frac{C_2(x)}{C_0}$	$\frac{C_3(x)}{C_0}$	$\frac{C_4(x)}{C_0}$	$\frac{C_5(x)}{C_0}$	$\frac{C_6(x)}{C_0}$	$\frac{C_7(x)}{C_0}$	$\frac{C_8(x)}{C_0}$	$\frac{C_9(x)}{C_0}$
0	.05	.003668	.000260	.0000134	.00000013	.00000001	0	
1	.0963	.007076	.000501	.0000354*	.0000025	.0000002	0	
4	.2222	.02853	.002780	.000229	.0000172	.0000013	.0000001	
10	.4238	.1076	.01945	.002751	.000323	.0000330	.0000002	
15	.5512	.1928	.04357	.009541	.001539	.000212	.0000258	
20	.6505	.2840	.09094	.02283	.004706	.000824*	.0001169	
30	.7880	.4597	.2050	.07293	.02146	.005372	.000225	
40	.8714	.6080	.3379	.1530	.05790	.01875	.001324	
50	.9220	.7233	.4698	.2541	.1164	.04591	.005295	
60	.9527	.8085	.5886	.3648	.1940	.08964	.01586	
80	.9826	.9122	.7695	.5768	.3817	.2234	.03645	
100	.9936	.9613	.8797	.7423	.5688	.3935	.2458	
120	.9976	.9834	.9403	.8534	.7220	.5629	.4024	
140	.9991	.9930	.9715	.9209	.8318	.7060	.5582	
160	.9997	.9971	.9868	.9591	.9033	.8136	.6931	
180	.9999	.9988	.9940	.9795	.9468	.8875	.79800	
200	1.0	.9995	.9993	.9900	.9717	.9349	.8732	
220	1.0	.9998	.9988	.9953	.9854	.9636	.9235	
240	1.0	.9999	.9995	.9978	.9927	.9803	.9555	

TABLE I—Continued.

$\frac{x}{t}$	$\frac{C_1(x)}{C_0}$	$\frac{C_3(x)}{C_0}$	$\frac{C_4(x)}{C_0}$	$\frac{C_5(x)}{C_0}$	$\frac{C_6(x)}{C_0}$	$\frac{C_7(x)}{C_0}$	$\frac{C_8(x)}{C_0}$	$\frac{C_9(x)}{C_0}$	$\frac{C_{10}(x)}{C_0}$	$\frac{C_{11}(x)}{C_0}$
0	.07	.007126	.0007007	.00006879	.00000668	.0000007	0	0	0	0
1	1.329	.01355	.001333	.0001308	.00001285	.0000013	0	0	0	0
3	.2462	.03689	.004352	.0004585	.00004608	.00000446	.0000004	0	0	0
5	.3446	.07096	.01078	.001355	.0001514	.00001582	.0000016	0	0	0
8	.4688	.1354	.02840	.004701	.0006603	.0000202	.0000093	0	0	0
10	.5382	.1837	.0458	.008885	.001448	.00002051	.00002604	.0000030	.0000044	0
15	.6746	.3108	.106991	.02859	.006370	.001214	.0002029	.00003041	.0000042	0
20	.7707	.4341	.1861	.06360	.01801	.004354	.0009189	.0001724	.00002921	.00000452
30	.8861	.6393	.3712	.1767	.07063	.02423	.007265	.001934	.0004628	.0000065
40	.9434	.7813	.5485	.3255	.1650	.07250	.02801	.009634	.002983	.0002007
50	.9719	.8717	.6929	.4799	.2894	.1532	.07178	.03009	.01139	.008397
60	.9860	.9265	.7995	.6185	.4252	.2598	.1418	.06969	.03103	.003928
70										.0012419
80	.9966	.9771	.9218	.8174	.6693	.5012	.3422	.2348	.1313	.01262
100	.9992	.9932	.9720	.9220	.8338	.7089	.5617	.4129	.2132	.01341
110										.004713
120	.9998	.9980	.9905	.9694	.9245	.8486	.7413	.6114	.4758	.2343
130	.9999	.9989	.9946	.9812	.9507	.8946	.8088	.6964	.5674	.3154
140										.4017
150										.03085
160										.1043
180	1.0	1.0	.9997	.9986	.9953	.9868	.9687	.9320	.8737	.5728
200			.9999	.9996	.9983	.9947	.9864			.7198
220					.9999	.9980	.9944			.8293
250										.9029

TABLE I.—Continued.

$\frac{x}{t}$	$\frac{C_1(x)}{C_0}$	$\frac{C_4(x)}{C_0}$	$\frac{C_5(x)}{C_0}$	$\frac{C_6(x)}{C_0}$	$\frac{C_7(x)}{C_0}$	$\frac{C_8(x)}{C_0}$	$\frac{C_{10}(x)}{C_0}$
0	.12	.02049	.003386	.0005588	.00009223	.00001522	.0000025
1	.3132	.03759	.006214	.001025	.0001692	.00002794	.0000008
2	.3908	.06335	.01118	.001875	.0003104	.00005125	.0000014
3	.4597	.09560	.01888	.003343	.0005649	.00009387	.0000026
4	.5208	.1325	.02965	.005692	.001005	.0001703	.0000047
5	.5750	.1727	.04358	.009175	.001724	.0003031	.0000086
6	.6230	.2148	.06059	.01402	.002832	.0005234	.00001554
7	.6657	.2580	.08051	.02041	.004450	.0007711	.00002771
8	.7035	.3015	.1031	.02848	.006704	.001400	.0002683
9	.7370	.3446	.1280	.03834	.009718	.002166	.0004379
10	.7668	.3869	.1550	.05001	.01361	.003236	.0006918
20	.9202	.7195	.4664	.2525	.1162	.046334	.01629
30	.9788	.8867	.7206	.5143	.3215	.1771	.08679
40	.9936	.9572	.8697	.7261	.5490	.3743	.2303
50	.9981	.9845	.9437	.8605	.7330	.5767	.4168
75	.9999	.9989	.9944	.9807	.9494	.8923	.8055
100	1.0	.9999	.9995	.9979	.9931	.9813	.9575
125	1.0			.9998	.9992	.9975	.9930
150				1.0	.9999	.9997	.9990
175					1.0		.9996

of  $k$ , ranging from 0.007, 0.05, 0.07 to 0.12 are displayed successively in Figs. 3, 4, 5, and 6.

These results of  $C_n(x)/C_0$  are restricted to the infinite bar (that is, terminal zone freezing neglected) and supplement data now incorporated as standard matter (2). The validity of Eqs. 10 is thus established.

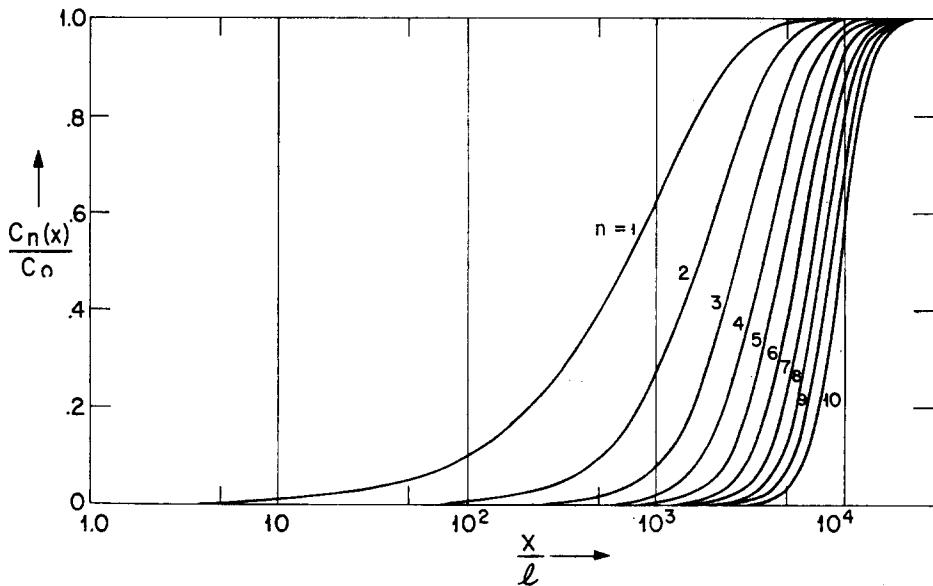


FIG. 1. Transformation of the solute distribution  $C_n(x)/C_0$  by cascade zone refining. The parameter  $n$  indicates stage of purification. The case  $k = 0.001$  showing approach to a limiting distribution as  $n \rightarrow \infty$ .

Incorporating the new findings in Eq. 4 produces

$$P_T = \frac{l}{L} + \frac{(1-k)}{L} \int_0^{L-l} e^{-(k/l)x} \cdot \sum_{p=n}^1 A_p \frac{\left(\frac{k}{l}x\right)^{n-p}}{(n-p)!} dx \quad (11)$$

whence the purification factor may be written in the form

$$\pi_T = 1 - \frac{l}{L} + \frac{(1-k)}{L} \cdot \frac{l}{k} \left[ \frac{A_n B_1}{0!} + \frac{A_{n-1} B_2}{1!} + \frac{A_{n-2} B_3}{2!} + \dots + \frac{A_1 B_n}{(n-1)!} \right] \quad (12a)$$

wherein the  $A_n$  are as stated in Eq. 10c and now

$$B_n = \left(\frac{k}{l}\right)^n \int_0^{L-l} x^{n-1} e^{-(k/l)x} dx. \quad (12b)$$

## CONCLUSION

The paramount objective of characterizing the zone-refinement operation by introduction of a purification factor has now been fulfilled. The investigation may be appreciated more fully by numerical

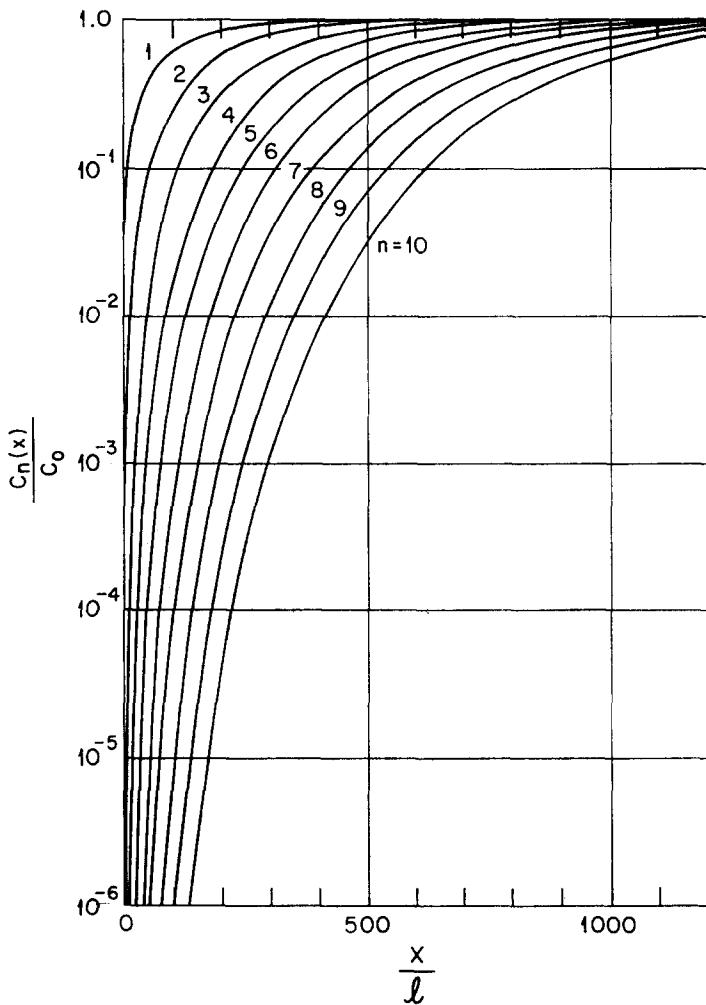
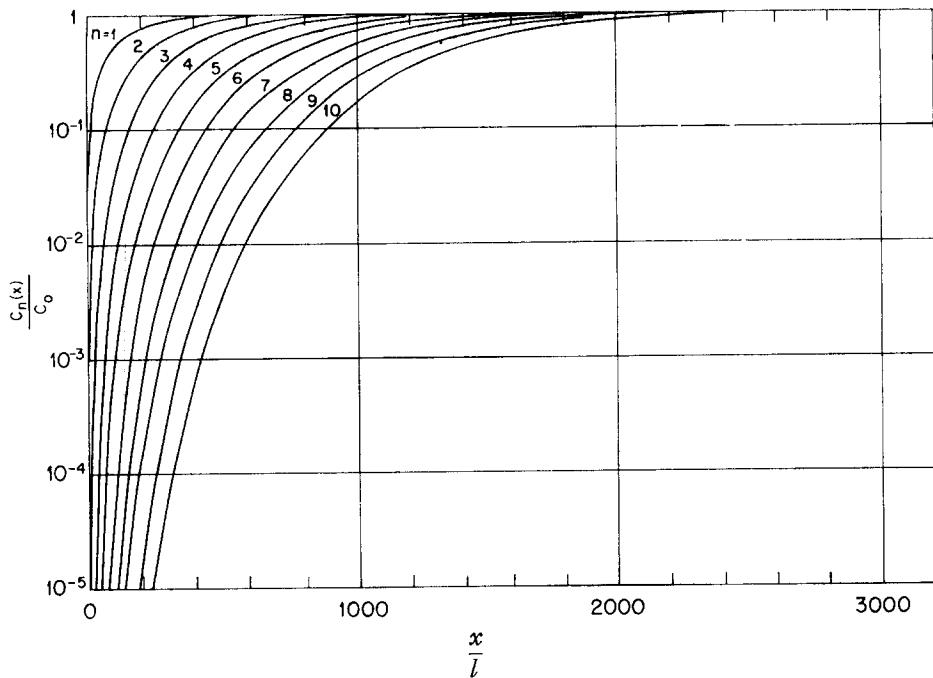
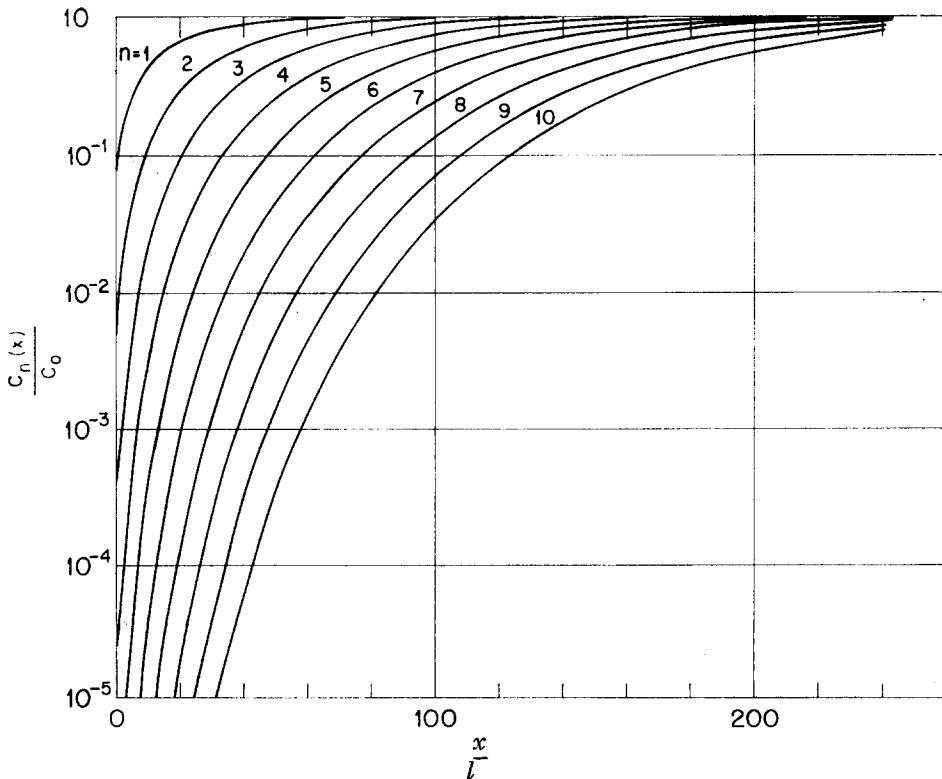


FIG. 2. The case  $k = 0.001$  in the region of  $\frac{x}{l} \rightarrow 0$ . (Cf. Fig. 1.)

description of  $\pi_T$  for the values of  $k$  already embodied in the delineation of the solute distribution. Table II contains the  $\pi_T$  behavior for three selected values of  $l/L$ , viz.  $1/2$ ,  $1/4$  and  $1/10$ . Finally, Figs. 7, 8 and 9 depict the expected fall-off of the purification factor with increasing passes for the gamut of  $k$  and  $l/L$  indicated.

FIG. 3. The case  $k = 0.007$ . (Cf. Fig. 1.)FIG. 4. The case  $k = 0.05$ . (Cf. Fig. 1.)

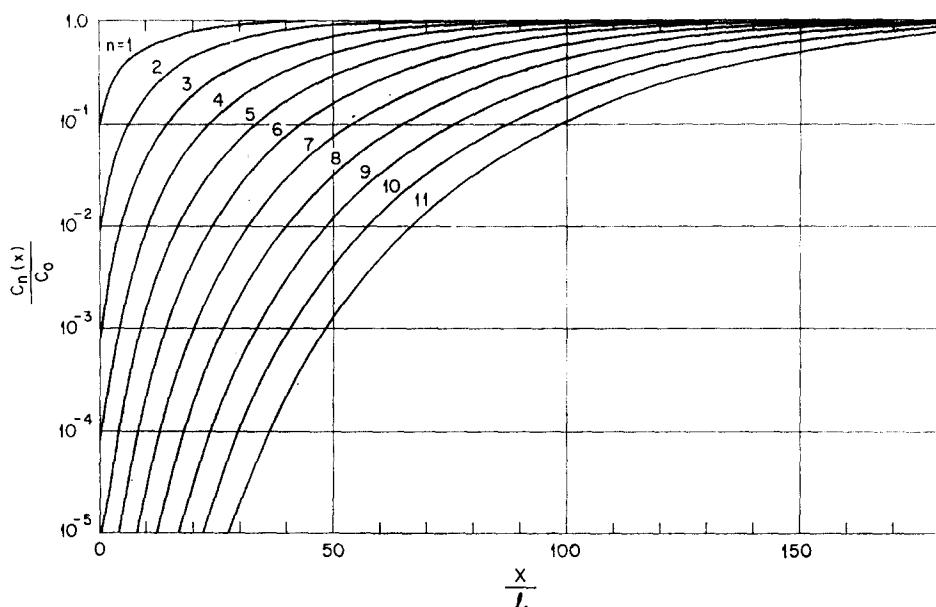
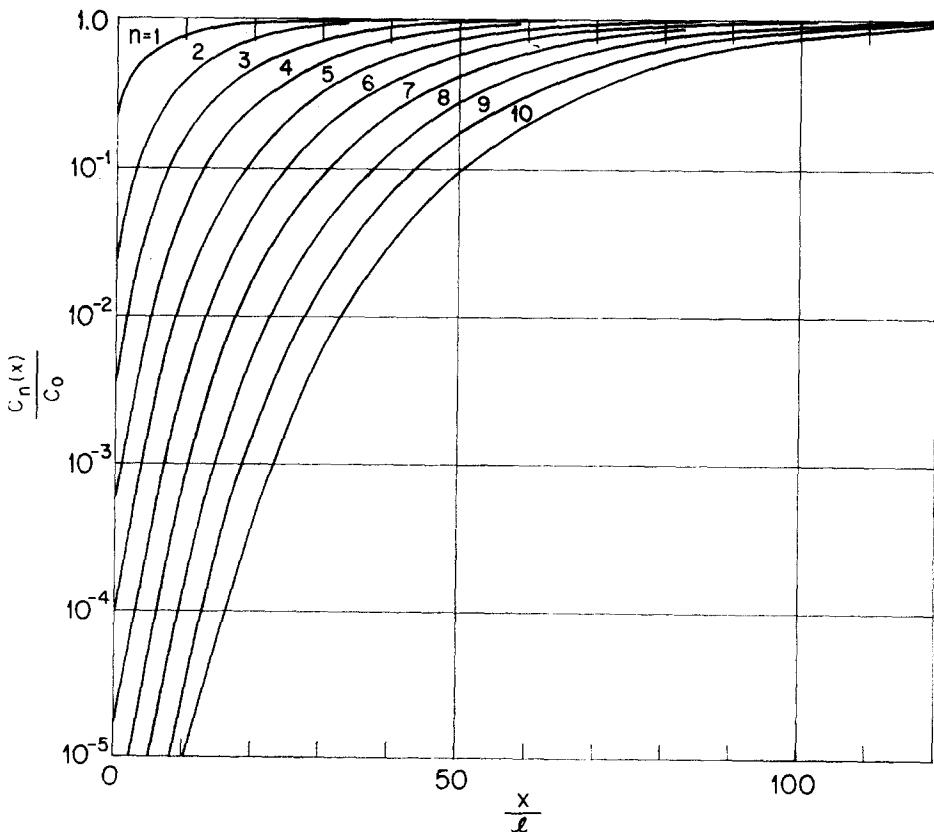
FIG. 5. The case  $k = 0.07$ . (Cf. Fig. 1.)FIG. 6. The case  $k = 0.12$ . (Cf. Fig. 1.)

TABLE II.— $\pi_T$  vs n Data for  $1/L = 0.5, 0.25, 0.10$ .

n	$L/L = 0.5$	$L/L = 0.25$	$L/L = 0.10$
$k = .001$			
1	.0007496	.0018728	.0058298
2	.0000010	.0000034	.0000174
3	0	0	0
$k = .007$			
1	.0052337	.0130154	.0338696
2	.0000528	.0001633	.00083117
3	.0000005	.0000018	.0000156
4	0	0	.0000002
5			0
$k = .05$			
1	.0366795	.0883629	.2114935
2	.0025966	.0077118	.0345802
3	.0001836	.0005898	.0044488
4	.0000130	.0000428	.0004804
5	.0000009	.0000030	.0000455
6	0	.0000002	.0000039
7		0	.0000003
8			0
$k = .07$			
1	.0509018	.1208691	.2790148
2	.0050049	.0145876	.0618266
3	.0004914	.0015478	.0109057
4	.0000483	.0001559	.0016245
5	.0000047	.0000154	.0002129
6	.0000005	.0000015	.0000254
7	0	.0000001	.0000028
8		0	.0000003
9			0
$k = .12$			
1	.0853749	.1957399	.4157034
2	.0141092	.0392708	.1456024
3	.0023283	.0069822	.0417406
4	.0003843	.0011810	.0102595
5	.0000634	.0001963	.0022383
6	.0000105	.0000324	.0004459
7	.0000017	.0000054	.0000830
8	.0000003	.0000009	.0000148
9	0	0	.0000025
10			.0000004

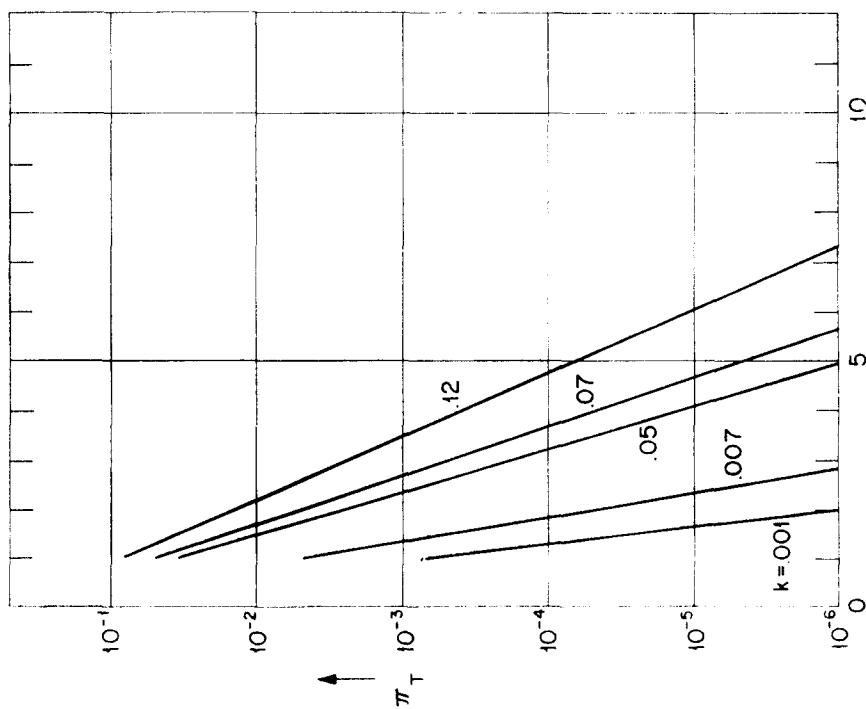


Fig. 7. The purification factor  $\pi_T$  after the  $n^{\text{th}}$  pass with indicated  $k$  values as a parameter. The case for  $l/L = 0.5$ .

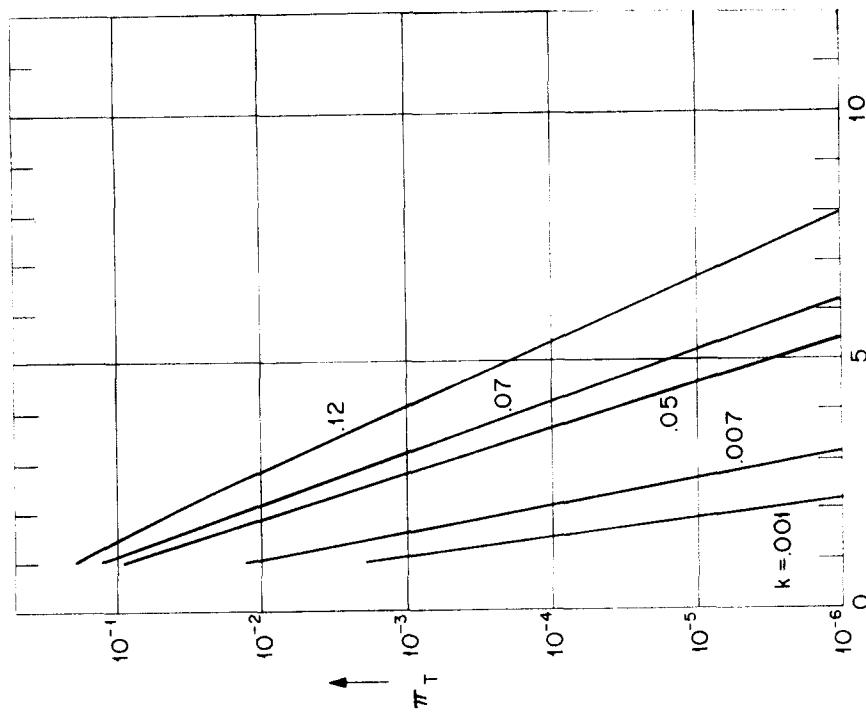
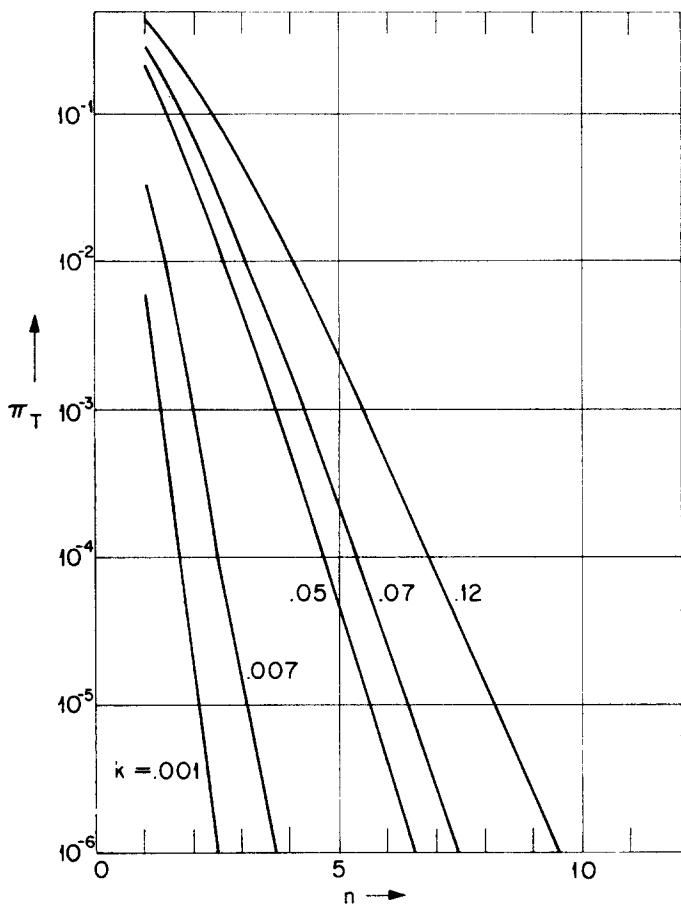


Fig. 8. The case for  $l/L = 0.25$ . (Cf. Fig. 7.)

FIG. 9. The case for  $l/L = 0.10$ . (Cf. Fig. 7.)

## APPENDIX

The  $Q_n(x)$  coefficients of Eq. 10a assume successively the values:

$$Q_1 = 1$$

$$Q_2 = 2 - e^{-k} + \left( \frac{k}{l} x \right)$$

$$Q_3 = (2 - e^{-k})^2 - ke^{-k} + (2 - e^{-k}) \left( \frac{k}{l} x \right) + \left( \frac{k}{l} x \right)^2 / 2!$$

$$Q_4 = (2 - e^{-k})^3 - 2ke^{-k}(2 - e^{-k}) \frac{k^2}{2} e^{-k} + [(2 - e^{-k})^2 - ke^{-k}] \frac{k}{l} x \\ + (2 - e^{-k}) \left( \frac{k}{l} x \right)^2 + \left( \frac{k}{l} x \right)^3 / 3!$$

$$\begin{aligned}
Q_5 &= \left[ (2 - e^{-k})^4 - 3ke^{-k}(2 - e^{-k})^2 - 2k^2e^{-k}(1 - e^{-k}) - \frac{k^3}{6}e^{-k} \right] \\
&\quad + \left[ (2 - e^{-k})^3 - 2ke^{-k}(2 - e^{-k}) - \frac{k^2}{2}e^{-k} \right] \frac{k}{l} x \\
&\quad + [(2 - e^{-k})^2 - ke^{-k}] \left[ \left( \frac{k}{l} x \right)^2 / 2! \right] + (2 - e^{-k}) \left( \frac{k}{l} x \right)^3 / 3! + \left( \frac{k}{l} x \right)^4 / 4! \\
Q_6 &= \left[ (2 - e^{-k})^5 - 4ke^{-k}(2 - e^{-k})^3 - 6k^2e^{-k}(1 - e^{-k})^2 \right. \\
&\quad \left. + \frac{3}{2}k^2e^{-3k} - \frac{2}{3}k^3e^{-k}(1 - 2e^{-k}) - \frac{k^4}{24}e^{-k} \right] \\
&\quad + \left[ (2 - e^{-k})^4 - 3ke^{-k}(2 - e^{-k})^2 - 2k^2e^{-k}(1 - e^{-k}) - \frac{k^3}{6}e^{-k} \right] \left( \frac{k}{l} x \right) \\
&\quad + \left[ (2 - e^{-k})^3 - 2ke^{-k}(2 - e^{-k}) - \frac{k^2}{2}e^{-k} \right] \left( \frac{k}{l} x \right)^2 / 2! \\
&\quad + [(2 - e^{-k})^2 - ke^{-k}] \left( \frac{k}{l} x \right)^3 / 3! + (2 - e^{-k}) \left( \frac{k}{l} x \right)^4 / 4! + \left( \frac{k}{l} x \right)^5 / 5! \quad (\text{A-1})
\end{aligned}$$

whence the recursion formula (10b) is deduced.

Applying the boundary condition at  $x = 0$ , there obtains from Eqs. 7 and 9

$$\frac{C_n(0)}{C_0} = \frac{k}{l} \int_0^l \frac{C_{n-1}(x) dx}{C_0} = 1 - (1 - k)A_n$$

or

$$A_n = (1 - k)^{-1} \left( 1 - \frac{C_n(0)}{C_0} \right). \quad (\text{A-2})$$

In this manner Eqs. 10c and 10d follow with the first few coefficients identified as

$$A_1 = 1, \quad A_2 = 2 - e^{-k}, \quad A_3 = (2 - e^{-k})^2 - ke^{-k}$$

and

$$S_1 = e^{-k} - 1, \quad S_2 = e^{-k}(k + 1) - 1, \quad S_3 = e^{-k}(k^2 + 2k + 2) - 2.$$

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