

Final Report  
UM-HSRI-81-29

Project No. 1151

BASELINE DATA FOR DESCRIBING  
OCCUPANT SIDE IMPACTS AND  
PEDESTRIAN FRONT IMPACTS  
IN TWO DIMENSIONS

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## EXECUTIVE SUMMARY

Two areas of current interest and activity in automotive safety are the protection of occupants in side impacts and the protection of pedestrians. During the past ten years a variety of projects have been conducted to study the interaction of pedestrians with motor vehicles. Somewhat more recently the emphasis has been on studying the interaction of a vehicle occupant with side door structures. Experimental studies have utilized both dummy and cadaver test subjects and a variety of vehicle types, both experimental and production. Analytical studies have been conducted using both two- and three-dimensional crash simulation models.

An FY 80 project at HSRI supported by MVMA had the objective of reviewing past simulation efforts on these two topics and developing practical baseline data sets for use with three-dimensional crash simulation software. This report details the extension of these three-dimensional data sets to two dimensions. The resulting baseline two-dimensional data sets have been developed for use with the existing Version 4 of the MVMA two-dimensional dynamic occupant/pedestrian simulation (DOPS).

The data sets have been described in the language of anticipated automotive users. The procedures and assumptions used in developing the data have also been explained. Sample outputs and graphical results from computer exercises using the data sets are included. It was found that the two-dimensional approach yields kinematic results which are quite similar to those obtained using a three-dimensional simulation. In order to make the predictions more realistic than those obtained during the three-dimensional modeling project, friction between the pedestrian and the vehicle as well as energy absorption by the various contact panels were added. The improvements were dramatic.

There are two versions of the MVMA two-dimensional dynamic occupant/pedestrian simulation (DOPS) which are in use at present - Version 3 and Version 4. Version 3 is most commonly used in the automobile industry while Version 4 is most common outside. The data sets used in this project should be applicable to both versions although it is anticipated that some storage problems could arise in the pedestrian simulation using Version 3 due to the large number of potential contacts.



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## 1.0 INTRODUCTION

The objective of this project has been to modify baseline data sets developed for use with the Calspan three-dimensional crash victim simulation (HSRI Version, 1981) to a form compatible with Version 4 of the MVMA two-dimensional dynamic occupant/pedestrian simulation (1). This project is a continuation of Project 1150 from Fiscal Year 1980 (2).

This report describes the baseline vehicle geometry in Part 2. The occupant and pedestrian along with their contact interactions with the vehicle are described in Parts 3 and 4. The baseline data sets and a sampling of the resulting computer program output are given in Part 5.

## 2.0 THE VEHICLES

In order to define the geometry of vehicle components with which an occupant might possibly interact during a side impact event or the front exterior components of a vehicle in the case of a pedestrian, it was necessary to obtain measurements from existing vehicles. Three vehicles were selected which are representative of the most modern domestic small car production.

For the front exterior of each vehicle, at least three points were measured with respect to a common inertial coordinate system to define the following surfaces approximately as planes:

- bumper
- grille
- hood
- windshield
- roof

For the vehicle interior the following surfaces were anticipated to be involved during lateral or 300° oblique impact:

- seat cushion
- seat back
- front door sill region (foot/lower leg contact)
- door panel lower region (hip and upper leg contact)
- door panel upper region (head contact)
- window panel (head contact)
- door header (head contact)
- floor (foot contact)
- B-pillar (head contact)

Other data were obtained which would make it possible to expand the simulation to cases of frontal impact.

### 2.1. BASELINE INTERIOR FOR SIDE IMPACT

Figure 1 illustrates the individual and average baseline panel locations which form the basis for construction of a side impact data set. These data are used in constructing the actual data sets described in Part 5 of this report.

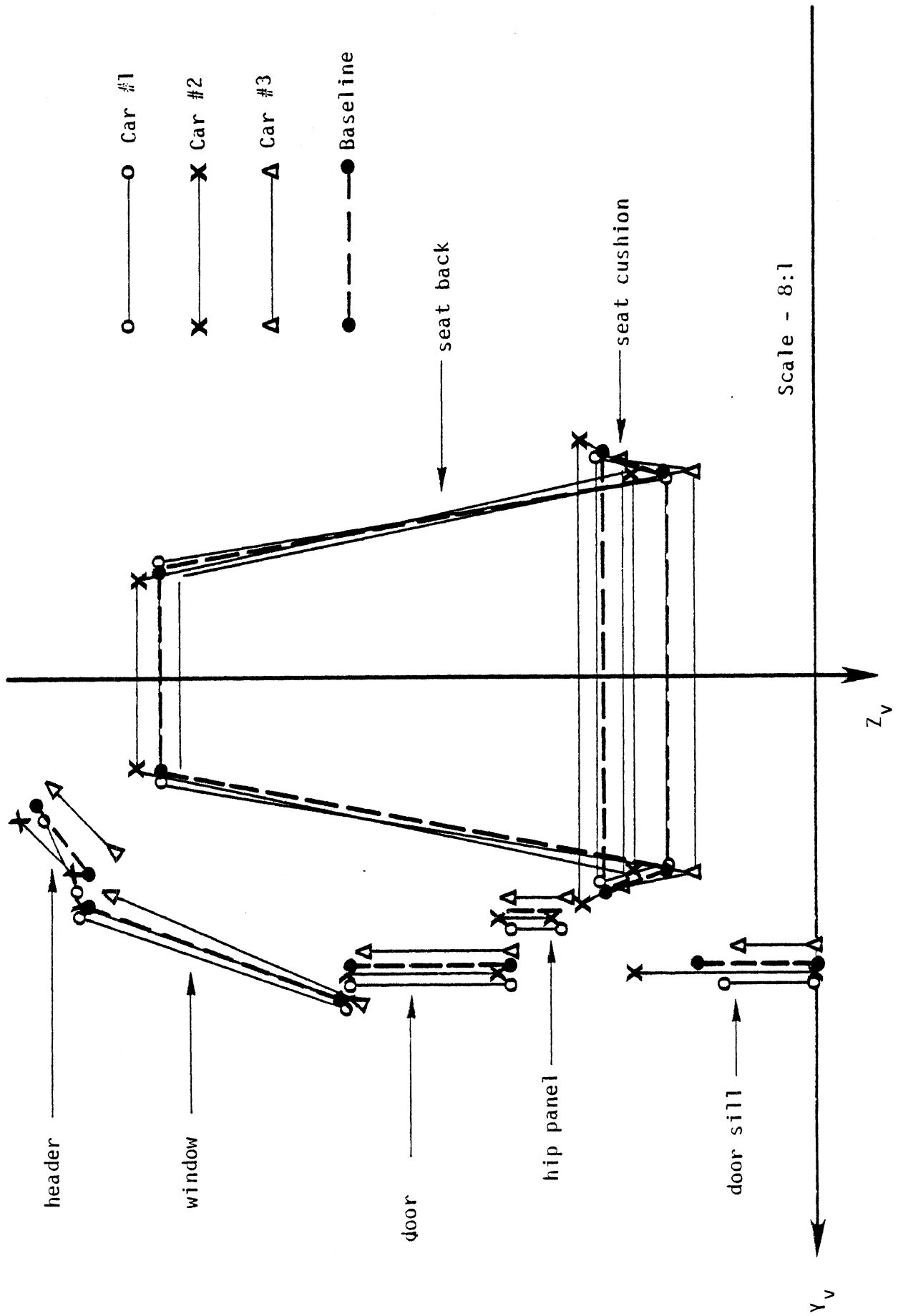


Figure 1. Vehicle interior for side impact (Front view)

## 2.2. BASELINE EXTERIOR FOR PEDESTRIAN IMPACT

Figure 2 illustrates the individual and average baseline panel locations which form the basis for a vehicle exterior intended for use in simulation of a pedestrian accident event. The baseline location has been used in constructing the actual data set described in Part 5 of this report. One surface which is not shown is the interface between the grille and hood. There was no clear definition for such a surface based on simple vehicle exterior measurements. Selection of a surface to represent this region was made to describe the intersection between the grille and the hood - a region which is estimated to have force-deformation properties different from those used to model the hood or grille regions.

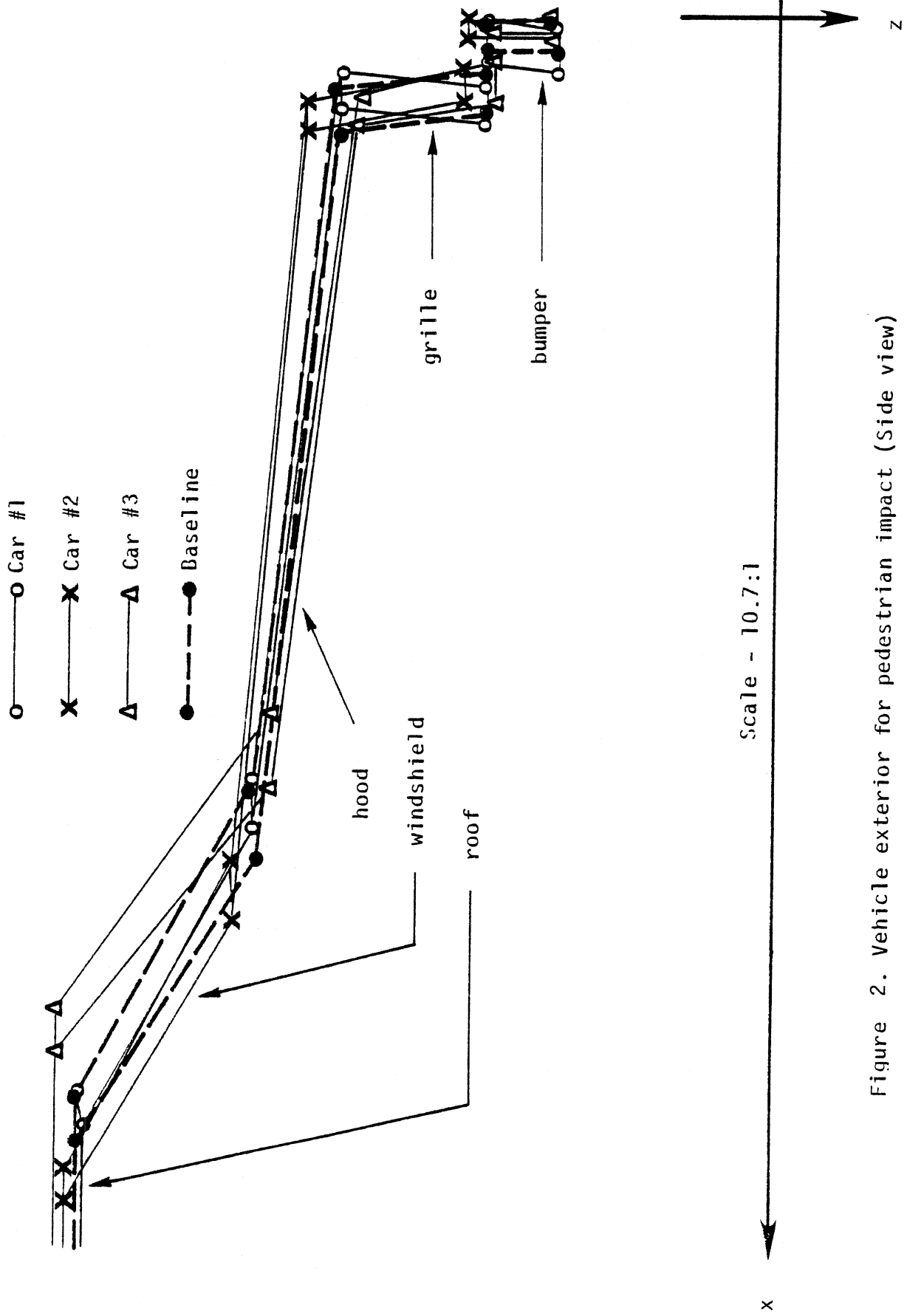


Figure 2. Vehicle exterior for pedestrian impact (Side view)

### 3.0 THE OCCUPANT AND PEDESTRIAN MODELS

During the previous project a survey was conducted to identify sources for the most complete and recent data sets describing, in three dimensions, an occupant in a side impact simulation and a pedestrian. Surprisingly little information was publicly available at the time. More recently, the Version 20 release tape containing the Calspan CVS included the most recent Part 572 experimental data. Although the data are not yet documented in a written report, they are so much more complete than any available up to this time that they were selected for use in constructing the baseline data sets for the current project.

#### 3.1 OCCUPANT FOR SIDE IMPACT SIMULATION

There were two steps in selecting the occupant. The first step was to project the original three-dimensional geometry to two dimensions. The second was to adjust the data to reflect the new Part 572 parameters. Figures 3 and 4 show side and rear views of the occupant model as they were modeled in three dimensions. Figure 5 illustrates the two-dimensional projection as it was used for the MVMA 2-D simulations. It should be noted that occupant outlines, as defined by contact ellipses, are very similar in Figures 4 and 5. The primary differences are the lack of a right arm and the lumping together of the left and right leg masses.

The numerical values for quantities such as segment mass, moment of inertia, position in space, ellipse axes, link angles, and joint properties are included in Part 5 which contains the complete listing of the output of the input data set. The mass of the upper arm was added to the torso while the mass and inertial properties of the upper and lower legs were combined. The new Part 572 data supplied with Calspan CVS Version 20 were used as a basis.

#### 3.2 PEDESTRIAN FOR IMPACT SIMULATION

The original three-dimensional pedestrian data set represented a person walking perpendicular to the path of the vehicle. Figure 6 shows the left side of the pedestrian with the left front of the vehicle behind him. In Figure 7 the view is that of the back of the pedestrian with a front-to-rear section of the vehicle projected through the y-



coordinate of the lower torso center of gravity. This section is on the left, or driver's side of the vehicle. This view was used as the basis for projecting the three-dimensional geometry to two dimensions as is shown in Figure 8. The outlines of the pedestrian, as defined by the contact ellipses, are similar in Figures 7 and 8. The differences are on the left side of the body in the arm and leg. The left arm is deleted and the mass lumped with the torso.

It was necessary to simplify the linkage for the two-dimensional case. To simulate the presence of two legs, a feature believed to be important because of the large mass and inertial properties of these segments as well as the fact that the initial energy transfer to the linkage is through the legs, two joints (4 and 5 as shown in Figure 8) were superimposed at the hip pivot point. This mechanism allowed the mass of the left leg to be represented by M4 while the right upper leg is represented by M5 and the right lower leg by M6. Contact between the left and right legs or between any of these segments and the vehicle is through the contact surfaces which are not affected (in inertial space) by this rearrangement of the linkage. The left and right legs pivot independently at the "hip."

The numerical values for quantities such as segment mass, moment of inertia, position in space, ellipse axes, link angles, and joint properties are included in Part 5 which contains the complete listing of the output of the input data set. The pelvic mass is ordinarily associated with the link between joints 4 and 5. As this link is now being used to simulate the leg leg (M4), the pelvic mass is moved to the link between joints 3 and 4 and lumped with the abdominal mass. The locations for centers of gravity, the mass values, and the moments of inertia are all derived from the new Part 572 data.

In the original three-dimensional simulation, all joints were free of constraints. It is believed that this is due to the fact that a purpose of simulation was to model the kinematics of a cadaver with no muscle tension to keep the body erect. The correct values for joint flexural properties were included to simulate Part 572.

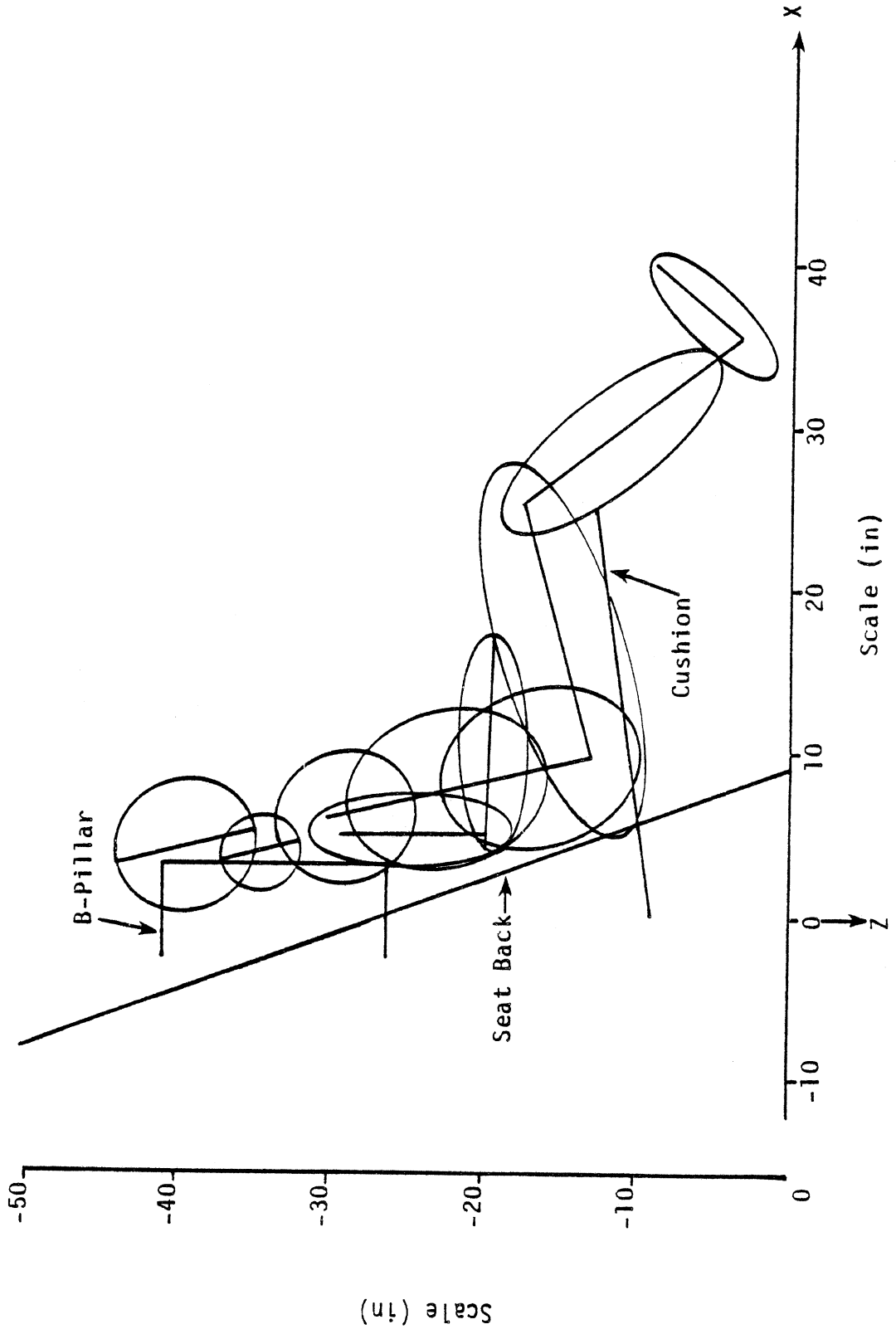


Fig. 3. Occupant for Side Impact Simulation (Side View)

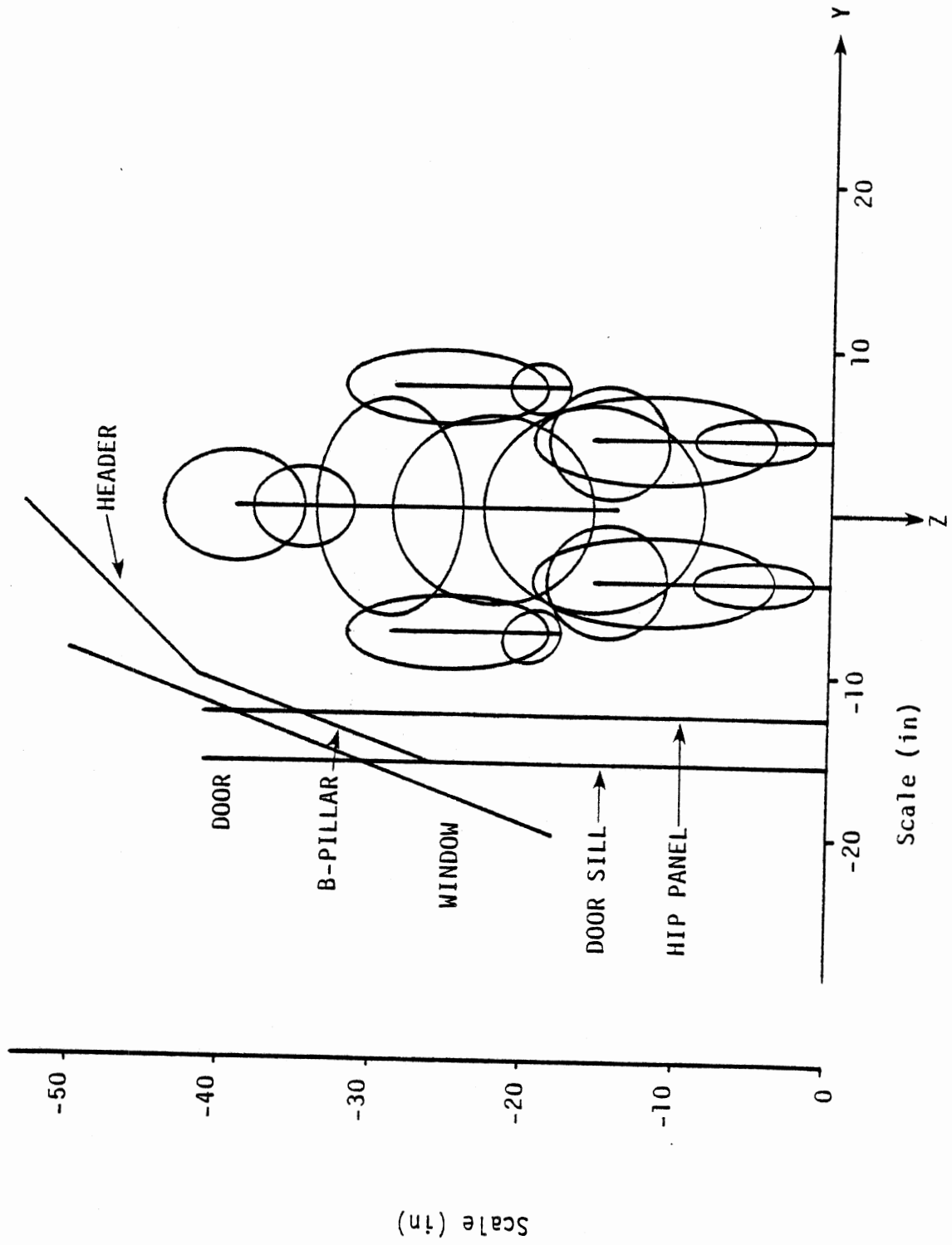


Fig. 4. Occupant for Side Impact Simulation (Rear View)

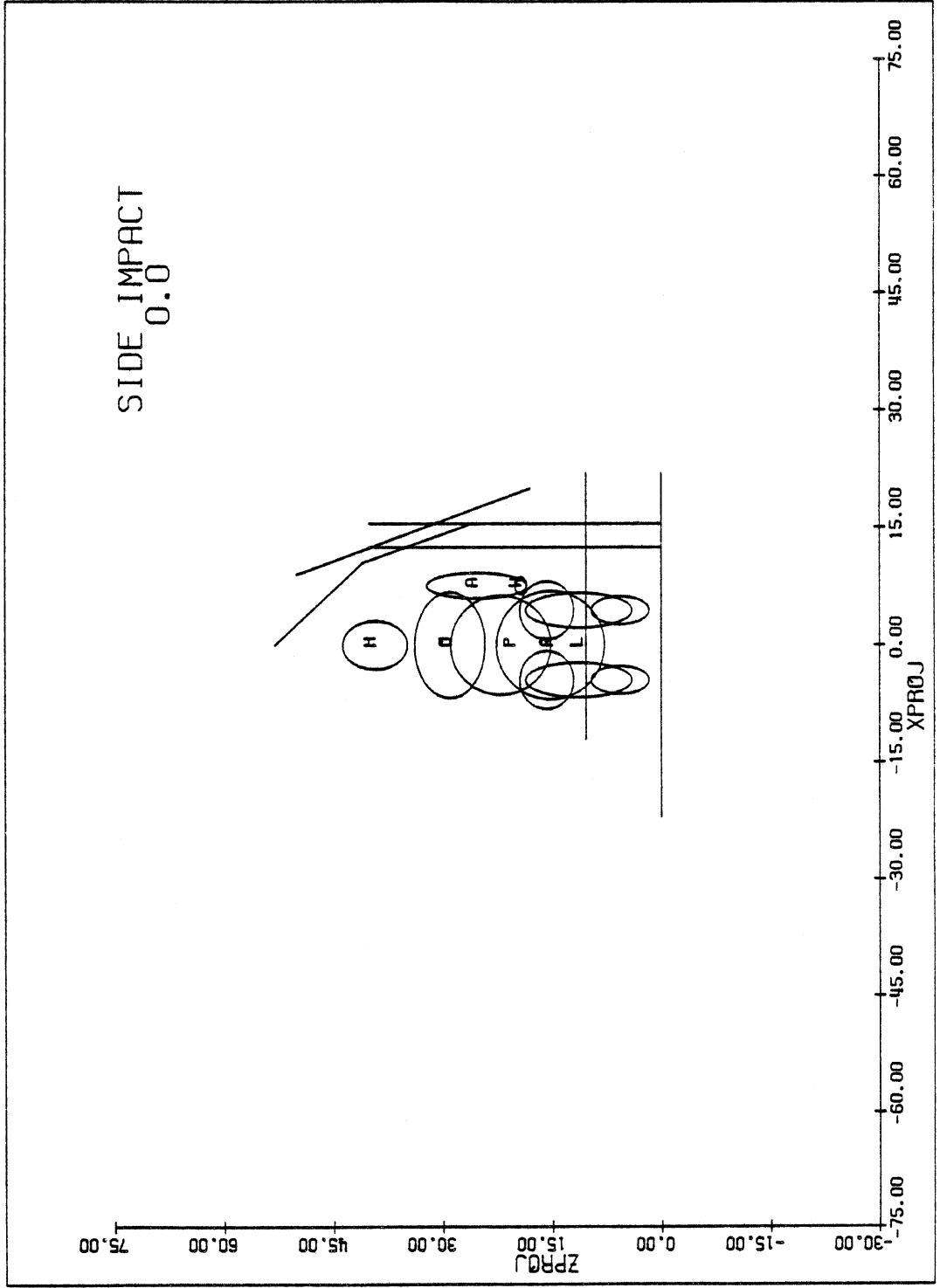


Fig. 5. Two-Dimensional Projection for Side Impact Simulation

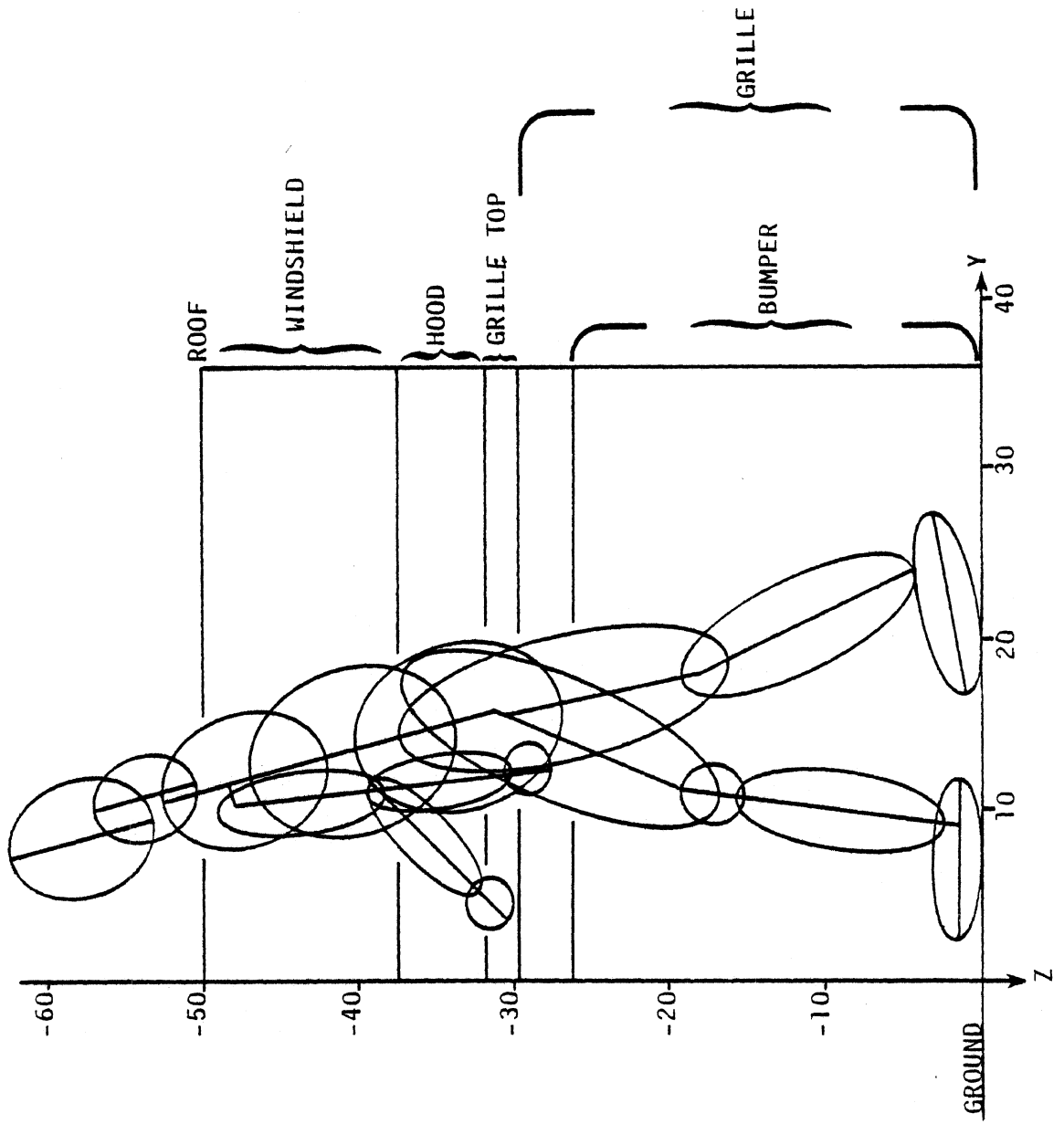


Fig. 6. Side View of Pedestrian (Initial Position).

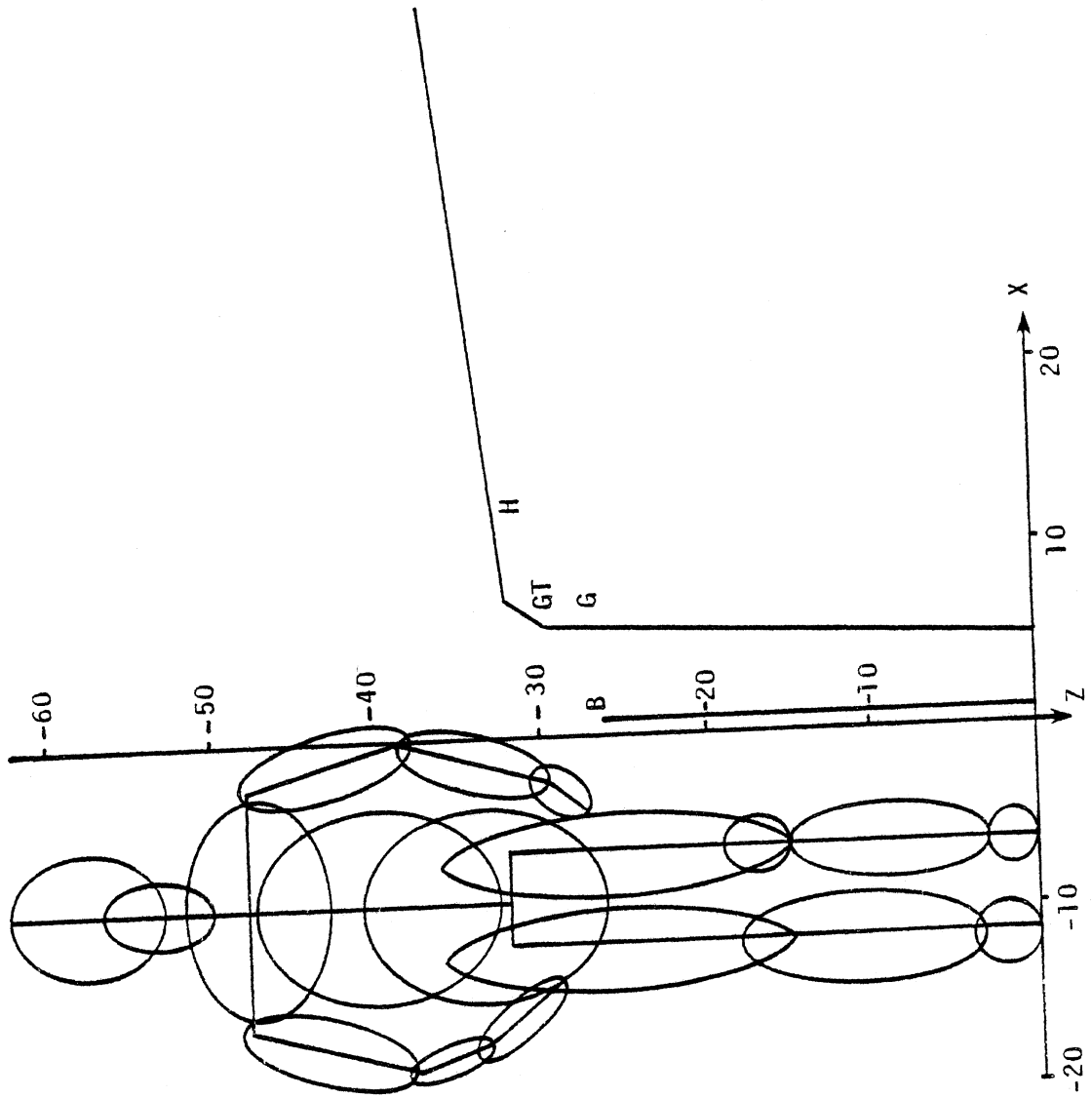


Fig. 7. Back View of Pedestrian (Initial Position)

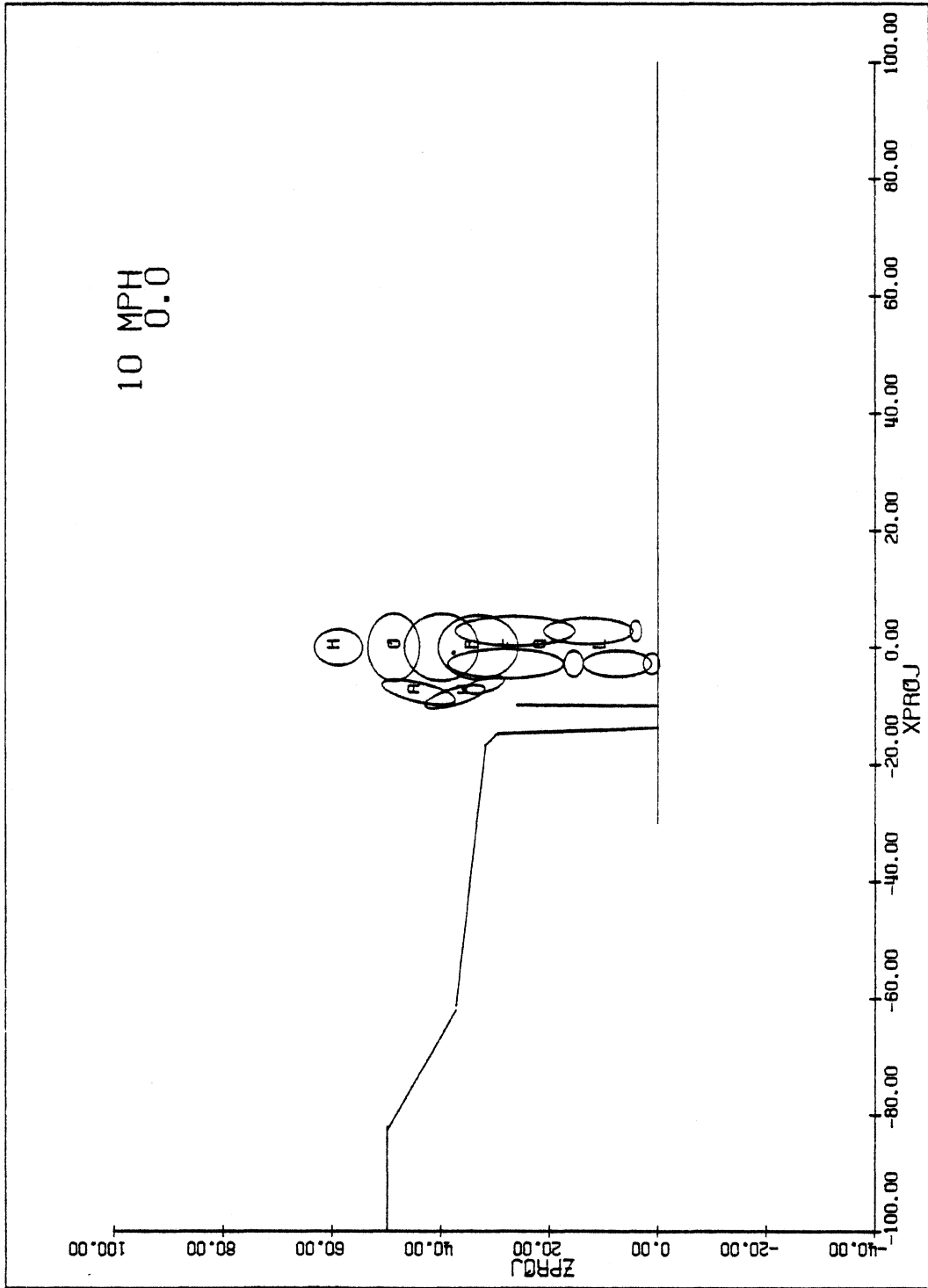


Fig. 8. Two-Dimensional Projection for Pedestrian Simulation.

A feature of the three-dimensional simulation was a special joint to model breaking of the lower leg. Because of limitations in the number of available masses for the MVMA 2-D model, breaking of the knee was substituted. This was handled by locking the joint using the Coulomb friction joint resistance option. The friction value was set at an estimated lateral knee joint fracture level.



#### 4.0 CONTACT INTERACTIONS WITH THE VEHICLE

A variety of contacts are allowed for both the occupant with the vehicle interior and the pedestrian with the vehicle exterior. Occupant or pedestrian ellipses may contact either flat panels attached to the vehicle or other of the ellipses on the subject. Table 1 shows the potential contacts which are allowed for the side impact occupant while Table 2 refers to the pedestrian.

The force-deflection characteristic curves governing interactions between the occupant or pedestrian and the vehicle have been derived from a variety of sources. Some are based on idealized vehicle component tests. Others are hypothetical estimates chosen to fill voids in our compilation of published, realistic vehicle descriptive data. All are intended to be treated as baseline data which should be replaced when measured data are available for use in actual engineering studies.

##### 4.1 VEHICLE INTERIOR FORCE - DEFORMATION CHARACTERISTICS

Five different force-deflection characteristic curves are used to define the properties of the contact surfaces used to define the vehicle interior for side impact. Figure 9 illustrates the curve for a structure entitled, "panel." Tabular implementation of these data define the deformation of the header, front door sill, and hip panel region. The door panel shoulder region contact surface is modeled as a fifth order polynomial fit to the table. The symbol "x" on Figure 9 shows the closeness of fit of this polynomial. The polynomial form is used for this contact surface to allow mutual deformation of the vehicle and occupant thorax. These data are derived from dynamic deformation tests of door interiors and represent a somewhat stiffer structure than that used in recent side impact simulations by Padgaonkar and Prasad (3). Because of a lack of experimental information on the header and front door sill, the data shown in Figure 9 have also been selected as hypothetical estimates for these surfaces.

Figure 10 shows the representative force-deflection curve for side window tempered glass which has been selected for inclusion in the data.

TABLE 1. OCCUPANT/VEHICLE INTERIOR CONTACTS

<u>Ellipse Name</u>	<u>Contact Panel or Ellipse Name</u>
Head	Window
Head	Header
Head	B-Pillar
Upper Torso	Door
Lower Torso	Seat Cushion
Lower Torso	Hip Panel
Right Upper Leg	Seat Cushion
Right Foot	Floor
Left Upper Leg	Seat Cushion
Left Upper Leg	Hip Panel
Left Lower Leg	Door Sill
Left Foot	Floor
Left Foot	Door Sill
Left Upper Arm	B-Pillar
Left Upper Arm	Door
Left Lower Arm	Door

TABLE 2. PEDESTRIAN/VEHICLE EXTERIOR CONTACT

<u>Ellipse Name</u>	<u>Contact Panel or Ellipse Name</u>
Head	Windshield
Head	Hood
Head	Car Front (Grille Top)
Head	Roof
Upper Torso	Roof
Upper Torso	Windshield
Upper Torso	Hood
Upper Torso	Car Front (Grille Top)
Lower Torso	Windshield
Lower Torso	Hood
Lower Torso	Car Front (Grille Top)
Lower Torso	Grill* (Grille)
Right Upper Leg	Hood
Right Upper Leg	Grill* (Grille)
Right Upper Leg	Car Front (Grille Top)
Right Upper Leg	Left Upper Leg
Right Knee	Bumper
Right Shin	Bumper
Right Foot	Ground
Right Foot	Grill* (Grille)
Left Upper Leg	Hood
Left Upper Leg	Grill* (Grille)
Left Upper Leg	Car Front (Grille Top)
Left Lower Leg	Bumper
Left Foot	Ground
Left Foot	Bumper
Left Foot	Grill* (Grille)
Right Upper Arm	Hood
Right Upper Arm	Windshield
Right Lower Arm	Hood
Right Lower Arm	Grill* (Grille)
Right Lower Arm	Car Front (Grille Top)

\*Note: The term "Grill" is the name used in the data set for the word "Grille".

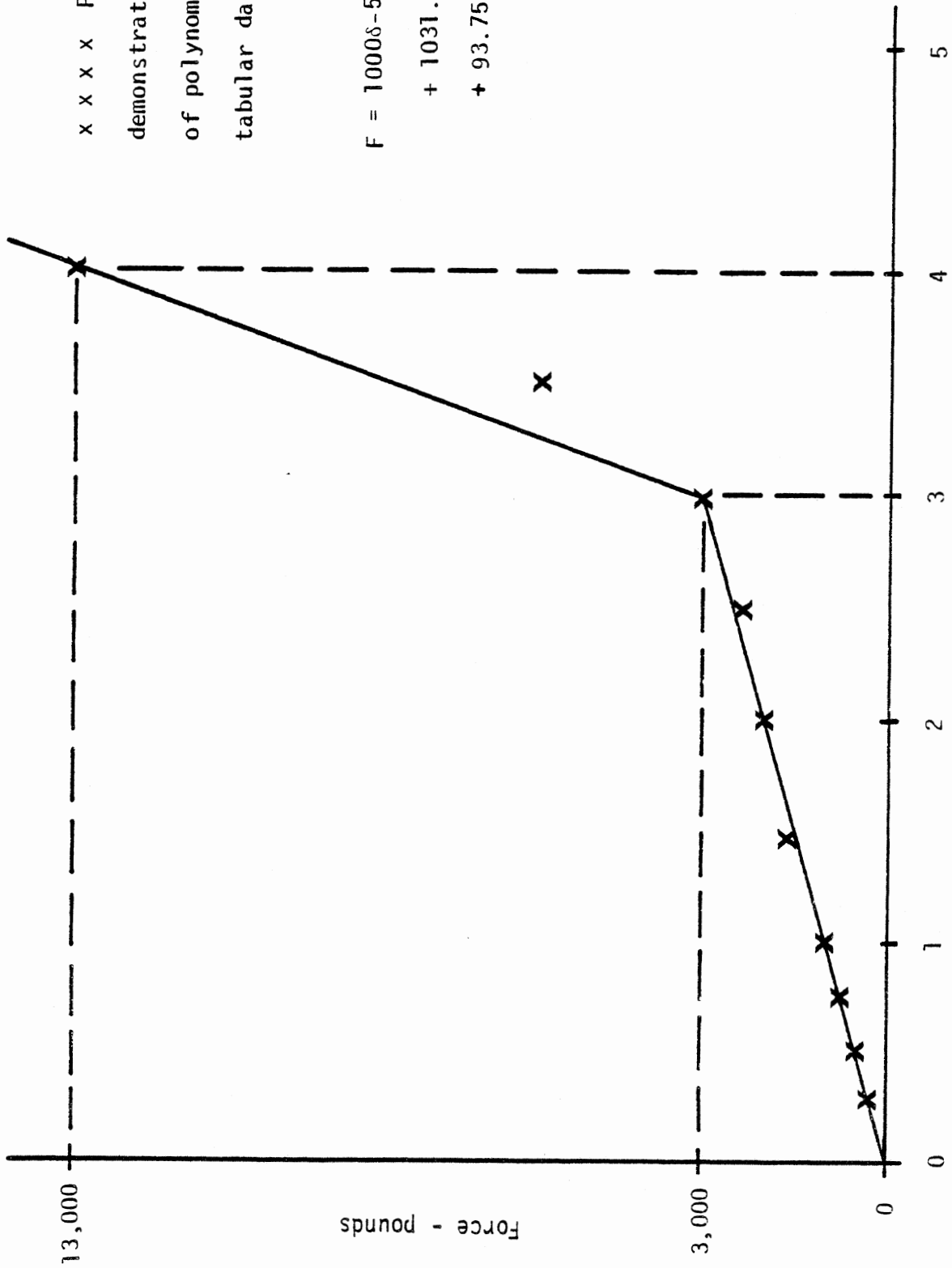
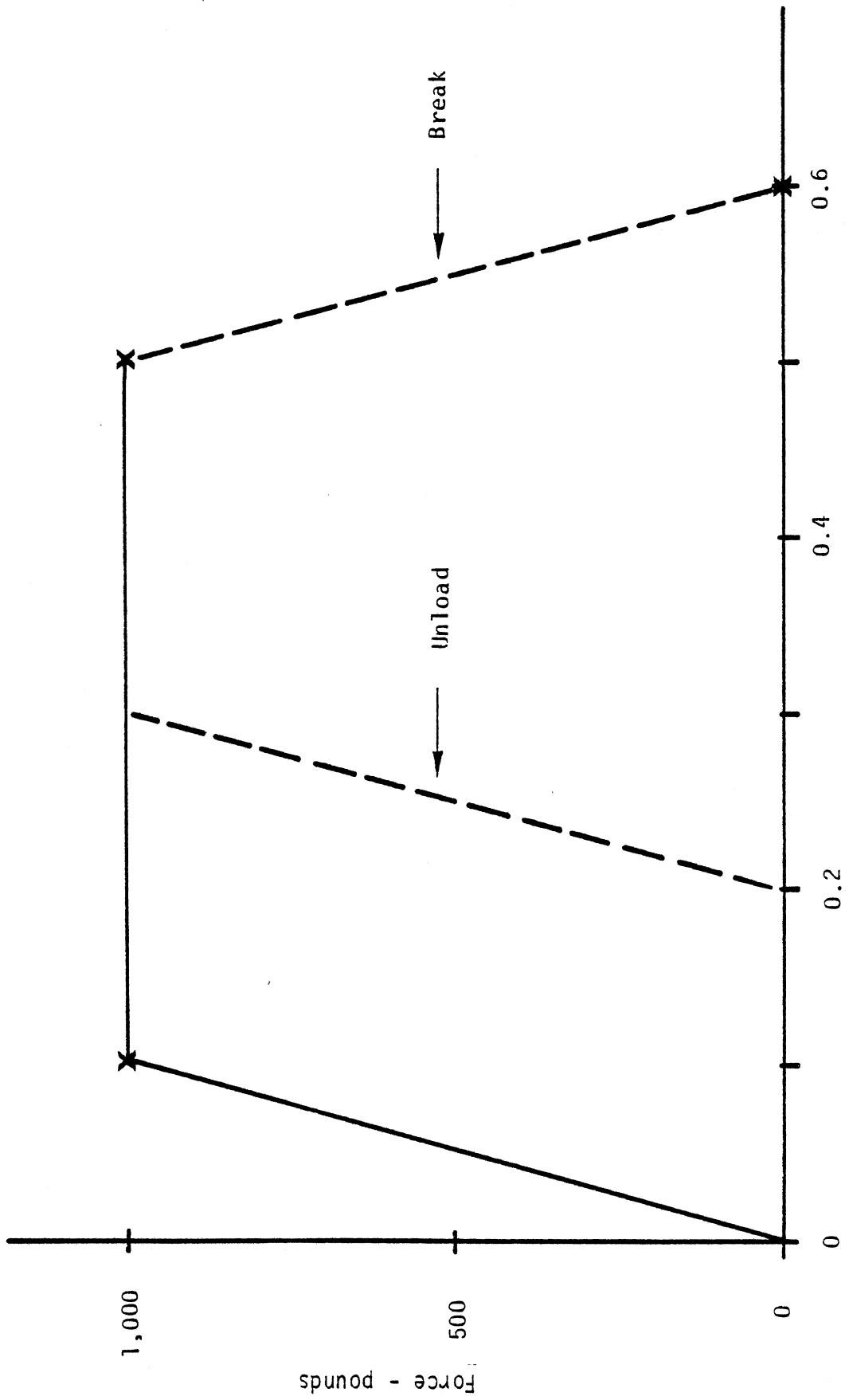


Figure 9. Panel force-deflection curve.



Deflection - inches  
 Figure 10. Side window force-deflection curve

This is an idealization of data presented at the 11th Stapp Car Crash Conference by Siemonsen and Bruckner (4). It should be noted that tempered glass holds substantial force for a larger deformation than annealed or laminated glass due to its larger bending stiffness. It is presumed that the glass panel breaks upon reaching a deflection of 0.5 inch and behaves elastically until that deformation is reached.

The floor, seat back, seat cushion, and B-pillar are modeled as linear polynomials in force and deformation. The following coefficients were supplied with the original frontal impact data set by Calspan Corporation while the B-pillar coefficient is a hypothetical estimate:

1. Seat back and seat cushion - 40 lb/in.
2. Floor - 860 lb/in.
3. B-pillar - 4000 lb/in.

#### 4.1.1 INTRUSION OF VEHICLE COMPONENTS DURING SIDE IMPACT

Figure 11 shows the intrusion of the hip and door contact surfaces during the baseline side impact accident event. The overall motions of the vehicle take place in the coordinate system indicated in the figure. However, in the case of intrusion, the various components of the vehicle move and deform with respect to the vehicle. To represent this physically observed phenomena and to provide a realistic, but hypothetical, example for the baseline exercise, the hip panel and door are seen to begin intrusion at 5 ms and continue moving inward until 30 ms when they stop with respect to the remainder of the vehicle. Total intrusion is 5 inches. The software is capable of linear motion, as is the case used in this example, and also of panel rotation.

#### 4.2 VEHICLE EXTERIOR FORCE-DEFORMATION CHARACTERISTICS

Three different force-deflection loading characteristic curves are used to define the properties of the seven contact surfaces which define the vehicle exterior and ground for pedestrian impact. All these curves are linear polynomials in deformation. The roof, windshield, hood, grille (GRLL), and bumper have a coefficient of 1000 lb/in. The ground coefficient is 470 lb/in. The grille top (car front) surface was to be twice the average of the hood and grille, which is 2000 lb/in. The body ellipses are all assumed to be rigid.

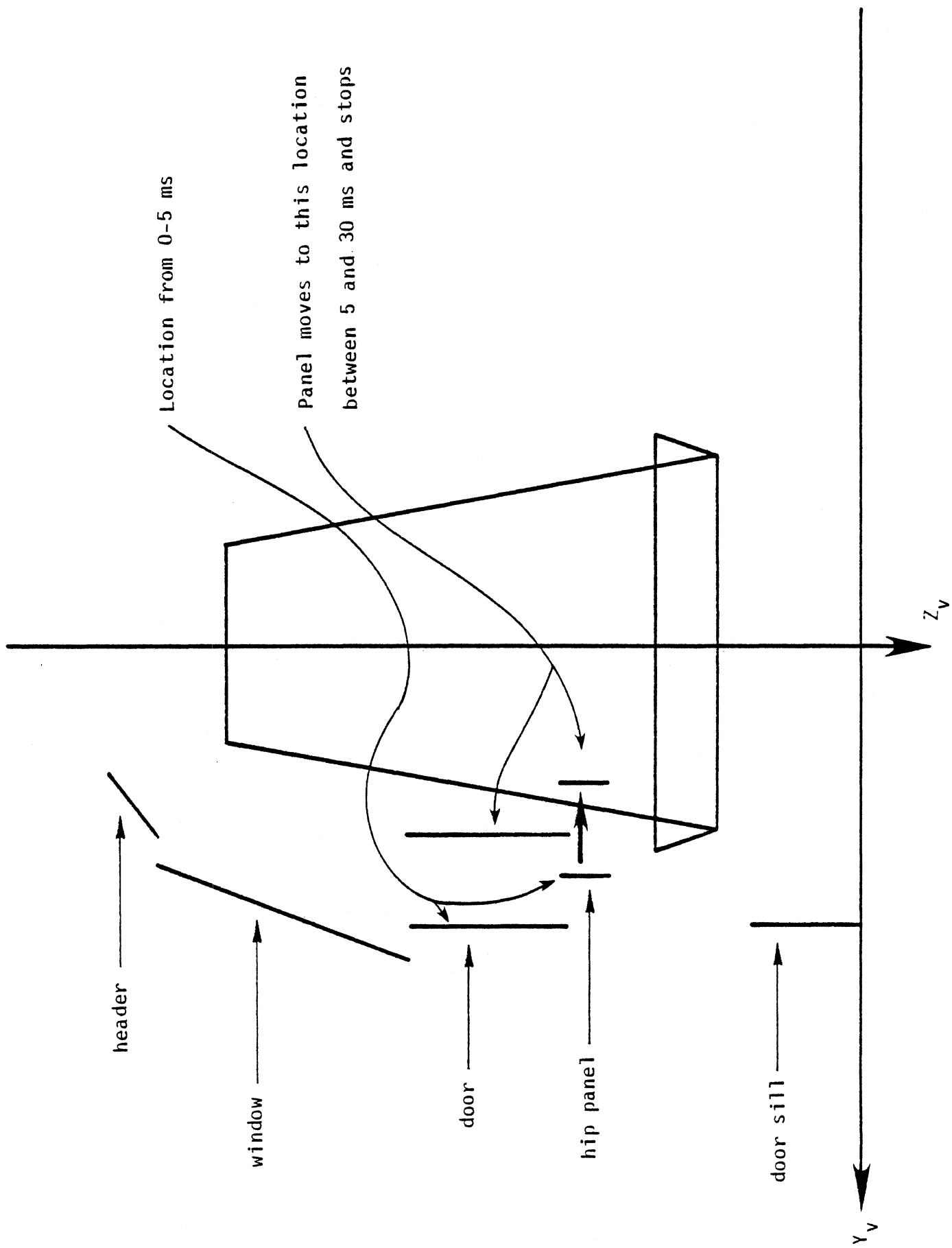


Figure 11. Intrusion of baseline hip panel and door contact surfaces during simulation.

Although the force-deflection loading curves used with the MVMA 2-D model are the same ones used in the three-dimensional simulations, the unloading curves are not. Pedestrian kinematics observed in the three-dimensional simulations and in the initial two-dimensional simulations resembled those of a rubber ball bouncing off the hood of the vehicle. These unloading curves demonstrated pure elastic behavior. To compensate for this problem the input data for unloading define an energy absorption of 99%. This had a marked effect on eliminating the marked vertical motion of the pedestrian.

Even with the changes just mentioned the results with the MVMA 2-D model still were not good. The pedestrian was not conforming to the vehicle, but rather, was sliding off. Contact friction was added for all interactions of the pedestrian with the vehicle. This change served to simulate the pedestrian in a manner similar to that observed in high speed movies of experimental impacts. It should be noted that contact with the ground was already modeled by a friction coefficient of 1.0 in both the MVMA 2-D and three dimensional simulations.

These data are incomplete and represent only hypothetical estimates for the properties of a vehicle exterior. It is recommended that the force-deformation and friction data contained in this baseline be regarded as preliminary and that further work should be done to improve their quality.



## 5.0 THE COMPUTER EXERCISES

The purpose of this part of the report is to present the numerical details of the two baseline data sets and give summary details of the resulting computer exercises. For a complete copy of the simulation output it is necessary to exercise the data set or obtain a copy of the tape containing the exercise from MVMA or HSRI.

### 5.1 VEHICLE DECELERATIONS AND MOTIONS

The dynamics of the side impact simulation are initiated by forcing an acceleration of the occupant compartment. This causes the vehicle (and its contact surfaces) to begin to move with respect to inertial coordinates. Superimposed upon this movement is the prescribed intrusion of the side door hip contact panel with respect to the vehicle coordinate system. The occupant, initially at rest with respect to both inertial and vehicle coordinate systems, is carried along by the vehicle motions through impacts with the vehicle interior contact surfaces. The lateral acceleration profile applied to the vehicle is shown graphically in Figure 12.

The pedestrian impact is initiated by prescribing motions for the vehicle which is given an initial velocity of 10 mph and maintains this non-stop velocity throughout the simulation. The contact surfaces of the vehicle are rigidly attached to the moving vehicle coordinate system. The occupant is motionless in inertial space at the beginning of the simulation and begins dynamic excursions when impacted by the bumper. The contact surface representing the ground does not move.

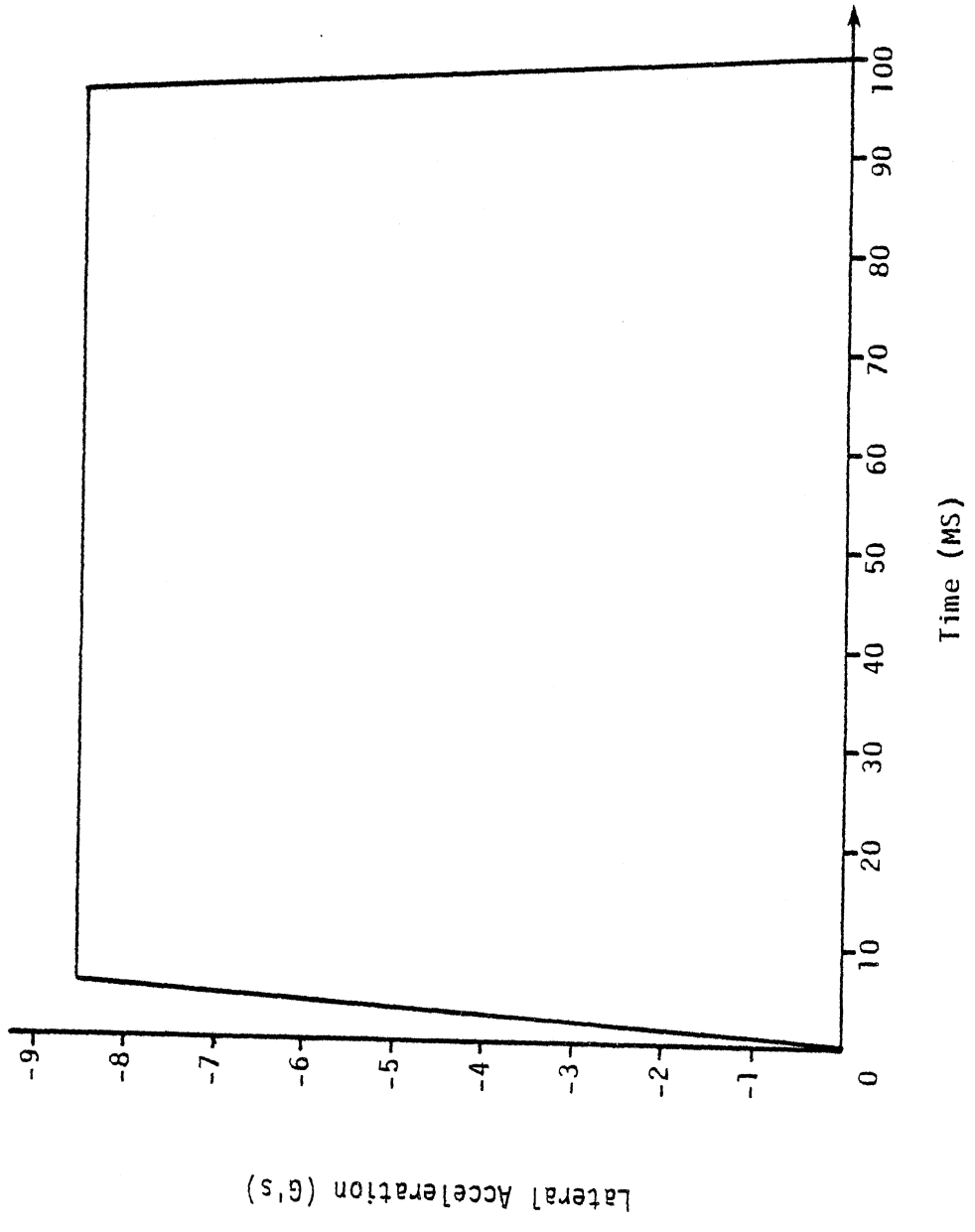


Fig. 12. Side Impact Vehicle Acceleration Curve.

## 5.2 SIDE IMPACT INPUT DATA

This part of the report contains the numerical details of the baseline MVMA 2-D side impact data set. Table 3 contains the output of the input data set after the input file has been processed by the IN section of the program. Not all pages are included. Those which are contain details of the linkage, joints, masses, inertial properties, contact ellipses, and program controls. Table 4 is a copy of the baseline data file which was constructed for the exercise.

SIMULATION CONTROL DATA

NO RESTRAINT BELTS PRESENT  
 FIXED RUNGE-KUTTA INTEGRATION METHOD IS USED  
 ACCELERATION DUE TO GRAVITY 32.1740 (FT/SEC\*\*2)  
 MINIMUM ACCELERATION MAGNITUDE 0.0 (IN/SEC\*\*2) OR (RAD/SEC\*\*2)  
 BEGINNING TIME 0.0 (MSEC)  
 FINAL TIME 100.00000 (MSEC)  
 NUMERICAL INTEGRATION STEP SIZE 1.00000 (MSEC)  
 OUTPUT PRINT INCREMENT 1.00000 (MSEC)  
 OUTPUT PLOT INCREMENT 205.00000 (MSEC) IF ZERO, NO PLOT RECORDING  
 ENGLISH UNITS ARE USED  
 STEERING COLUMN INTERACTION IS NOT DESIRED  
 AIRBAG INTERACTION IS NOT DESIRED  
 ELLIPSE-ELLIPSE CONTACTS SPECIFIED ON 106 CARDS ARE ALLOWED  
 ELLIPSE-REGION CONTACTS SPECIFIED ON 106 CARDS ARE ALLOWED  
 ELLIPSE-ELLIPSE CONTACTS CAN OCCUR  
 LENGTH OF SCALING RAMP TO INSURE CONTINUITY IN CONTACT FRICTION 10.000 (IN/SEC)  
 RELATIVE ERROR TOLERANCE FOR SINGULARITY IN MATRIX INVERSION STEP 0.000001  
 CPU TIME LIMIT FOR EXECUTION 2 (MIN)

TABLE 3. Output of Baseline Input Data Set. Side Impact (Page 1 of 8).

INTEGRATION CONTROLS

MAXIMUM STEP TO SEARCH FOR BALANCE IN SHARED DEFLECTION	0.200 (IN)
MINIMUM STEP TO SEARCH FOR BALANCE IN SHARED DEFLECTION	0.020000 (IN)
MAXIMUM FORCE FOR RIGID-RIGID CONTACT	600.00 (LB)
LINEAR ELASTIC COEFFICIENT FOR RIGID-RIGID CONTACT	500.00 (LB/IN)
MAXIMUM NUMBER OF ITERATIONS TO FIND FORCE BALANCE	30
FRACTION OF CURRENT RAMP LENGTH FOR VELOCITY CHANGE IN MOVING CONTACT LINES	0.050
NUMBER OF INTEGRATION STEPS FOR MAXIMUM RAMP LENGTH FOR VELOCITY CHANGE IN MOVING CONTACT LINES	10.
MINIMUM RATIO OF SHORTER TO LONGER SEMI-MAJOR AXIS FOR ELLIPSE TO BE TREATED AS CIRCLE	1.000
FRACTIONAL POSITION OF CIRCLE CENTER ALONG SEMI-MAJOR AXIS RELATIVE TO POSITION FOR CIRCLE-ELLIPSE TANGENCY AT END OF AXIS	1.000

DEBUGGING CONTROLS

TIME TO SET DEBUG SWITCHES (MSEC)	0.0	2000.0000	0.0	0.0
DEBUG SWITCH SETTING IN HEXADECIMAL FORMAT	00000000	00000000	00000000	00000000
TIME TO SET DEBUG SWITCHES (MSEC)	0.0	0.0	0.0	0.0
DEBUG SWITCH SETTING IN HEXADECIMAL FORMAT	00000000	00000000	00000000	00000000

DEBUG CONTROLS ARE TO OPERATE FOR ALL INTEGRATION EVALUATIONS AT EACH TIME

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TABLE 3. Output of Baseline Input Data Set. Side Impact (Page 2 of 8).

BODY PARAMETERS

BODY SEGMENT LENGTHS (IN)		END OF LINK TO CENTER-OF-MASS LENGTHS (IN)		MASS OF BODY SEGMENTS (LBS SEC**2 IN)	
HEAD LENGTH=	0.0	HEAD/NECK JOINT-HEAD CM LENGTH=	3.23	HEAD MASS=	0.0250
UPPER TORSO LENGTH=	8.80	NPCK-CHEST CM LENGTHS=	2.15	CHEST MASS=	0.0950
MIDDLE TORSO LENGTH=	4.70	UPPER TORSO JOINT-MIDDLE TORSO CM LENGTH=	2.25	MIDDLE TORSO MASS=	0.0310
LOWER TORSO LENGTH=	4.89	LOWER TORSO JOINT LOWER TORSO CM LENGTH=	2.45	LOWER TORSO MASS=	0.0980
HIP-KNEE LENGTH=	4.24	HIP-UPPER LEG CM LENGTH=	2.20	UPPER LEG (BOTH LEGS)=	0.0900
UPPER TORSO-SHOULDER=	0.0	KNEE-LOWER LEG CM LENGTH=	6.05	LOWER LEG (BOTH LEGS)=	0.0500
SHOULDER-ELBOW LENGTH=	10.70	SHOULDER-UPPER ARM CM LENGTH=	5.25	UPPER ARM (BOTH ARMS)=	0.0120
X REST POINT OF SHOULDER=	1.57	ELBOW-LOWER ARM CM LENGTH=	0.57	LOWER ARM (BOTH ARMS)=	0.0120
Z REST POINT OF SHOULDER=	-7.60			HEAD-NECK MASS=	0.0036
				UPPER TORSO-NECK MASS=	0.0011

	MOMENTS OF INERTIA (ABOUT CM) (LBS SEC**2 IN)	"NATURAL" LINK ANGLES (FOR ZERO TORQUE) (DEG)	INITIAL BODY LINK ANGLES (RELATIVE TO VEHICLE) (DEG)	INITIAL ANGULAR VELOCITIES (RELATIVE TO VEHICLE) (DEG/SEC)
HEAD	0.2970	0.0	90.00	0.0
UPPER TORSO	2.1700	0.0	90.00	0.0
MIDDLE TORSO	0.3100	0.0	90.00	0.0
LOWER TORSO	1.7800	0.0	90.00	0.0
UPPER LEG	0.7700	-180.00	90.00	0.0
LOWER LEG	1.0000	180.00	-90.00	0.0
UPPER ARM	0.1370	0.0	-90.00	0.0
LOWER ARM	0.2700	0.0	-90.00	0.0
NPCK	0.0		90.00	0.0

OCCUPANT JOINT PARAMETERS

	LINEAR ANGULAR DEFLECTION COEF. (IN-LBS/DEG)	QUADRATIC ANGULAR DEFLECTION COEF. (IN-LBS/DEG**2)	CUBIC ANGULAR DEFLECTION COEF. (IN-LBS/DEG**3)	CONSERVED-ABSORBED ENERGY RATIO
HEAD-NECK FORWARD	31.20000	0.0	0.0	1.00
NECK-UPPER TORSO FORWARD	31.20000	0.0	0.0	1.00
UPPER SPINE	50.00000	0.0	0.0	1.00
LOWER SPINE	50.00000	0.0	0.0	1.00
HIP	16.00000	0.0	0.0	1.00
KNEE	0.0	0.0	0.0	1.00
UPPER ARM-UPPER TORSO	0.0	0.0	0.0	0.0
ELBOW	0.0	0.0	0.0	0.0
HEAD-NECK REAR	31.20000	0.0	0.0	1.00
NPCK-UPPER TORSO REAR	31.20000	0.0	0.0	1.00
NECK (EXTENSIBLE) **	751.00000	0.0	757.00000	NA
SHOULDER (EXTENSIBLE) **	1000.00000	0.0	800.00000	1.00
NPCK (COMPRESSIBLE) **	751.00000	0.0	757.00000	NA

\*\* UNITS FOR THE NECK (EXTENSIBLE), (COMPRESSIBLE) AND SHOULDER (EXTENSIBLE) PARAMETERS ARE GIVEN IN THE ROW BELOW  
(LB/IN) (LB/IN\*\*2) (LB/IN\*\*3)

TABLE 3. Output of Baseline Input Data Set. Side Impact (Page 3 of 8).

	VISCIOUS FRICTION (IN LBS SEC/DEG)	CONSTANT FRICTION COEFFICIENT (IN-LBS)	VELOCITY THRESHOLD FOR CONST. FRICTION (DEG/SEC)	POS. JOINT STOP (DEG)	NEG. JOINT STOP (DEG)
HEAD-NECK FORWARD	0.0	0.0	0.0	0.0	0.0
NECK-UPPER TORSO FORWARD	0.0	0.0	0.0	0.0	0.0
UPPER SPINE	0.0	0.0	0.0	0.0	0.0
LOWER SPINE	0.0	0.0	0.0	0.0	0.0
HIP	0.0	0.0	0.0	0.0	0.0
KNEE	0.0	0.0	0.0	0.0	0.0
UPPER ARM-UPPER TORSO	0.0	0.0	0.0	0.0	0.0
ELBOW	0.0	0.0	0.0	0.0	0.0
HEAD-NECK REAR	0.0	0.0	0.0	0.0	0.0
NECK-UPPER TORSO REAR	0.0	0.0	0.0	0.0	0.0
NECK (EXTENSIBLE) **	1.9800	NA	NA	NA	NA
SHOULDER (EXTENSIBLE)**	2.5000	NA	NA	0.0	NA
NECK (COMPRESSIBLE) **	1.9800	NA	NA	NA	NA

\*\*UNITS FOR THE NECK (EXTENSIBLE), (COMPRESSIBLE) AND SHOULDER (EXTENSIBLE) PARAMETERS ARE GIVEN IN THE ROW BELOW (LB SEC/IN)

MUSCLE TENSION COEFFICIENTS

	STIFFNESS COEF. A1 (K=A1+A2IM1) (IN-LBS/DEG)	STIFFNESS COEF. A2 (K=A1+A2IM1) (1/DEG)	DAMPING COEF. A3 (C=A3IM1) (SEC/DEG)	INIT. MUSCLE FORCE OR MOMENT RESULTANT (IN-LBS)	NAME ASSIGNED TO MUSCLE TENSION TABLE (M) VS TIME
HEAD-NECK	0.0	0.0	0.0	0.0	
NECK-UPPER TORSO	0.0	0.0	0.0	0.0	
UPPER SPINE	0.0	0.0	0.0	0.0	
LOWER SPINE	0.0	0.0	0.0	0.0	
HIP	0.0	0.0	0.0	0.0	
KNEE	0.0	0.0	0.0	0.0	
UPPER ARM-UPPER TORSO	0.0	0.0	0.0	0.0	
ELBOW	0.0	0.0	0.0	0.0	
SHOULDER-UPPER TORSO	0.0	0.0	0.0	0.0	
NECK (EXTENSIBLE) **	0.0	0.0	0.0	0.0	
SHOULDER (EXTENSIBLE)**	0.0	0.0	0.0	0.0	

\*\*UNITS FOR NECK (EXTENSIBLE) AND SHOULDER (EXTENSIBLE) PARAMETERS ARE GIVEN IN THE ROW BELOW (LB/IN)

TABLE 3. Output of Baseline Input Data Set. Side Impact. (Page 4 of 8).

INITIAL CONDITIONS FOR UPPER TORSO AND NECK

INITIAL (X,Z) COORDINATE OF CENTERLINE POINT NUM.1 RELATIVE TO VEHICLE ORIGIN IN (IN) ( 0.0 , -29.00)  
 INITIAL (X,Z) VELOCITY OF CENTERLINE POINT NUM. 1 RELATIVE TO VEHICLE ORIGIN IN (FT/SEC) ( 0.0 , 0.0 )  
 INITIAL NECK LENGTH 4.89(IN)  
 INITIAL RATE OF EXTENSION OF NECK 0.0 (IN/SEC)

INITIAL SHOULDER LOCATION AND VELOCITY RELATIVE TO UPPER TORSO ATTACHMENT

INITIAL (X,Z) COORDINATES OF SHOULDER JOINT RELATIVE TO UPPER TORSO ATTACHMENT POINT IN (IN) ( 0.0 , 0.0 )  
 INITIAL (X,Z) VELOCITY IN UPPER TORSO SYSTEM IN (IN/SEC) ( 0.0 , 0.0 )

OCCUPANT ACCELEROMETER AND BELT ATTACHMENT PARAMETERS

DISTANCE ALONG HEAD-NECK CENTERLINE TO HEAD ACCELEROMETER 3.19(IN)  
 DISTANCE ALONG UPPER TORSO CENTERLINE TO CHEST ACCELEROMETER 2.13(IN)

VEHICLE INITIAL CONDITIONS AND ACCELEROMETER LOCATION

(X,Z) COORDINATES OF VEHICLE ORIGIN IN (IN) ( 0.0 , 0.0 )  
 INITIAL (X,Z) VEHICLE VELOCITY IN (FT/SEC) ( 0.0 , 0.0 )  
 INITIAL VEHICLE PITCH ANGLE 0.0 (DEG)  
 INITIAL VEHICLE PITCH ANGULAR VELOCITY 0.0 (DEG/SEC)  
 (X,Z) COORDINATES OF VEHICLE ACCELEROMETER IN (IN) ( 0.0 , 0.0 )  
 MASS OF VEHICLE 0.0 (LBS SEC\*\*2/IN)

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TABLE 3. Output of Baseline Input Data Set. Side Impact (Page 5 of 8).



ELLIPSES ATTACHED TO THE HEAD

NAME OF ELLIPSE IS HEAD	ELLIPSE IS ASSUMED RIGID	FRICITION CLASS IS	1
X-COORDINATE OF ELLIPSE CENTER IN BODY SEGMENT COORDINATES=	0.0 (IN)	SEMI-AXIS LENGTH ALONG X-COORDINATE=	4.490 (IN)
Z-COORDINATE OF ELLIPSE CENTER IN BODY SEGMENT COORDINATES=	0.0 (IN)	SEMI-AXIS LENGTH ALONG Z-COORDINATE=	3.100 (IN)

REGIONS WHICH ARE ALLOWED TO CONTACT THE ELLIPSE HEAD

WINDOW

HEADER

B-PILLAR

ELLIPSES ATTACHED TO THE UPPER TORSO

NAME OF ELLIPSE IS UPPER TORSO	ELLIPSE MATERIAL IS THORAX MATERIAL	FRICITION CLASS IS	1
X-COORDINATE OF ELLIPSE CENTER IN BODY SEGMENT COORDINATES=	0.0 (IN)	SEMI-AXIS LENGTH ALONG X-COORDINATE=	4.832 (IN)
Z-COORDINATE OF ELLIPSE CENTER IN BODY SEGMENT COORDINATES=	0.0 (IN)	SEMI-AXIS LENGTH ALONG Z-COORDINATE=	6.780 (IN)

REGIONS WHICH ARE ALLOWED TO CONTACT THE ELLIPSE UPPER TORSO

DOOR

ELLIPSES ATTACHED TO THE MIDDLE TORSO

NAME OF ELLIPSE IS CENTER TORSO	ELLIPSE IS ASSUMED RIGID	FRICITION CLASS IS	1
X-COORDINATE OF ELLIPSE CENTER IN BODY SEGMENT COORDINATES=	-1.956 (IN)	SEMI-AXIS LENGTH ALONG X-COORDINATE=	6.876 (IN)
Z-COORDINATE OF ELLIPSE CENTER IN BODY SEGMENT COORDINATES=	0.0 (IN)	SEMI-AXIS LENGTH ALONG Z-COORDINATE=	6.350 (IN)

ELLIPSES ATTACHED TO THE LOWER TORSO

NAME OF ELLIPSE IS LOWER TORSO	ELLIPSE IS ASSUMED RIGID	FRICITION CLASS IS	1
X-COORDINATE OF ELLIPSE CENTER IN BODY SEGMENT COORDINATES=	0.0 (IN)	SEMI-AXIS LENGTH ALONG X-COORDINATE=	7.434 (IN)
Z-COORDINATE OF ELLIPSE CENTER IN BODY SEGMENT COORDINATES=	0.0 (IN)	SEMI-AXIS LENGTH ALONG Z-COORDINATE=	6.940 (IN)

REGIONS WHICH ARE ALLOWED TO CONTACT THE ELLIPSE LOWER TORSO

SEAT CUSHION

HIP PANEL

TABLE 3. Output of Baseline Input Data Set. Side Impact (Page 6 of 8).

ELLIPSES ATTACHED TO THE UPPER LEG

NAME OF ELLIPSE IS LEFT UPPER LEG	ELLIPSE IS ASSUMED RIGID	FRICITION CLASS IS	1
X-COORDINATE OF ELLIPSE CENTER IN BODY SEGMENT COORDINATES=	0.782(IN)	SEMI-AXIS LENGTH ALONG X-COORDINATE=	3.729(IN)
Z-COORDINATE OF ELLIPSE CENTER IN BODY SEGMENT COORDINATES=	-4.450(IN)	SEMI-AXIS LENGTH ALONG Z-COORDINATE=	3.740(IN)

REGIONS WHICH ARE ALLOWED TO CONTACT THE ELLIPSE LEFT UPPER LEG

SEAT CUSHION  
HIP PANEL

NAME OF ELLIPSE IS RIGHT UPPER LEG	ELLIPSE IS ASSUMED RIGID	FRICITION CLASS IS	1
X-COORDINATE OF ELLIPSE CENTER IN BODY SEGMENT COORDINATES=	0.782(IN)	SEMI-AXIS LENGTH ALONG X-COORDINATE=	3.729(IN)
Z-COORDINATE OF ELLIPSE CENTER IN BODY SEGMENT COORDINATES=	4.450(IN)	SEMI-AXIS LENGTH ALONG Z-COORDINATE=	3.740(IN)

REGIONS WHICH ARE ALLOWED TO CONTACT THE ELLIPSE RIGHT UPPER LEG

SEAT CUSHION

ELLIPSES ATTACHED TO THE LOWER LEG

NAME OF ELLIPSE IS LEFT LOWER LEG	ELLIPSE IS ASSUMED RIGID	FRICITION CLASS IS	1
X-COORDINATE OF ELLIPSE CENTER IN BODY SEGMENT COORDINATES=	-0.364(IN)	SEMI-AXIS LENGTH ALONG X-COORDINATE=	7.338(IN)
Z-COORDINATE OF ELLIPSE CENTER IN BODY SEGMENT COORDINATES=	4.450(IN)	SEMI-AXIS LENGTH ALONG Z-COORDINATE=	2.230(IN)

REGIONS WHICH ARE ALLOWED TO CONTACT THE ELLIPSE LEFT LOWER LEG

DOOR SILL

NAME OF ELLIPSE IS LEFT FOOT	ELLIPSE IS ASSUMED RIGID	FRICITION CLASS IS	1
X-COORDINATE OF ELLIPSE CENTER IN BODY SEGMENT COORDINATES=	5.322(IN)	SEMI-AXIS LENGTH ALONG X-COORDINATE=	3.999(IN)
Z-COORDINATE OF ELLIPSE CENTER IN BODY SEGMENT COORDINATES=	4.450(IN)	SEMI-AXIS LENGTH ALONG Z-COORDINATE=	1.800(IN)

REGIONS WHICH ARE ALLOWED TO CONTACT THE ELLIPSE LEFT FOOT

FLOOR  
DOOR SILL

NAME OF ELLIPSE IS RIGHT FOOT	ELLIPSE IS ASSUMED RIGID	FRICITION CLASS IS	1
X-COORDINATE OF ELLIPSE CENTER IN BODY SEGMENT COORDINATES=	5.322(IN)	SEMI-AXIS LENGTH ALONG X-COORDINATE=	3.999(IN)
Z-COORDINATE OF ELLIPSE CENTER IN BODY SEGMENT COORDINATES=	-4.450(IN)	SEMI-AXIS LENGTH ALONG Z-COORDINATE=	1.800(IN)

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TABLE 3. Output of Baseline Input Data Set. Side Impact (Page 7 of 8).

REGIONS WHICH ARE ALLOWED TO CONTACT THE ELLIPSE RIGHT FOOT

FLOOR

NAME OF ELLIPSE IS RIGHT LOWER LEG ELLIPSE IS ASSUMED RIGID FRICTION CLASS IS 1  
 X-COORDINATE OF ELLIPSE CENTER IN BODY SEGMENT COORDINATES= -0.364 (IN) SEMI-AXIS LENGTH ALONG X-COORDINATE= 7.338 (IN)  
 Z-COORDINATE OF ELLIPSE CENTER IN BODY SEGMENT COORDINATES= -0.450 (IN) SEMI-AXIS LENGTH ALONG Z-COORDINATE= 2.230 (IN)

ELLIPSES ATTACHED TO THE UPPER ARM

NAME OF ELLIPSE IS LEFT UPPER ARM ELLIPSE IS ASSUMED RIGID FRICTION CLASS IS 1  
 X-COORDINATE OF ELLIPSE CENTER IN BODY SEGMENT COORDINATES= 0.0 (IN) SEMI-AXIS LENGTH ALONG X-COORDINATE= 6.880 (IN)  
 Z-COORDINATE OF ELLIPSE CENTER IN BODY SEGMENT COORDINATES= 0.0 (IN) SEMI-AXIS LENGTH ALONG Z-COORDINATE= 1.640 (IN)

REGIONS WHICH ARE ALLOWED TO CONTACT THE ELLIPSE LEFT UPPER ARM

B-PILLAR

DOOR

ELLIPSES ATTACHED TO THE LOWER ARM

NAME OF ELLIPSE IS LEFT LOWER ARM ELLIPSE IS ASSUMED RIGID FRICTION CLASS IS 1  
 X-COORDINATE OF ELLIPSE CENTER IN BODY SEGMENT COORDINATES= 0.0 (IN) SEMI-AXIS LENGTH ALONG X-COORDINATE= 0.818 (IN)  
 Z-COORDINATE OF ELLIPSE CENTER IN BODY SEGMENT COORDINATES= 0.0 (IN) SEMI-AXIS LENGTH ALONG Z-COORDINATE= 1.110 (IN)

REGIONS WHICH ARE ALLOWED TO CONTACT THE ELLIPSE LEFT LOWER ARM

DOOR

TABLE 3. Output of Baseline Input Data Set. Side Impact (Page 8 of 8).

SIDE IMPACT #1 -- 12 DEGREES										
1										100
2	3D-2D: LEFT ARM-AR									200
3	M LINKS/RIGHT ARM-L									300
4	UNPFD WITH TOPSO/RI									400
5	GHT AND LEFT LEGS-L									500
6	UNPFD TOGETHER									600
7	OCCUPANT IS STRUCK									700
8	FROM LEFT SIDE									800
9	1.	1.	32.174	0.	0.	100.	1.	1.	205.	101
10	0.	0.	0.	0.	0.	0.	10.	.000001	2.	102
11	.2	.02	600.	500.	30.	.05	10.	1.	1.	103
12	HEAD		WINDOW							106
13	HEAD		HEADFR							106
14	HEAD		B-PILLAR							106
15	UPPER TORSO		DOOR							106
16	LOWER TORSO		SEAT CUSHION							106
17	LOWER TORSO		HIP PANEL							106
19	RIGHT UPPER LEG		SEAT CUSHION							106
20	RIGHT FOOT		FLOOR							106
21	LEFT UPPER LEG		SEAT CUSHION							106
22	LEFT UPPER LEG		HIP PANEL							106
23	LEFT LOWER LEG		DOOR SILL							106
24	LEFT FOOT		FLOOR							106
25	LEFT FOOT		DOOR SILL							106
26	LEFT UPPER ARM		B-PILLAR							106
26.1	LEFT UPPER ARM		DOOR							106
26.2	LEFT LOWER ARM		DOOR							106
27	0.	0.	0.	0.	0.	0.	1.	0.	1.	107
28	0.	0.	0.	0.	0.	0.	1.	0.	1.	108
29	1.	1.	0.	0.	0.	0.	0.	0.	1.	109
30	1.	1.	0.	0.	0.	1.	1.	1.	1.	110
31	0.	0.	1.	0.	0.	0.	0.	0.	0.	111
32	HEAD					1.	1.			219
33	HEAD		0.	0.	4.4897	3.1				220
34	UPPER TORSO		THORAX MATERIAL		2.	1.				219
35	UPPER TORSO		0.	0.	4.83205	6.78				220
36	CENTER TOPSO				3.	1.				219
37	CENTER TORSO	-1.9563	0.		6.87638	6.35				220
38	LOWER TORSO				4.	1.				219
39	LOWER TORSO	0.	0.		7.4339	6.94				220
40	LEFT UPPER LEG				5.	1.				219
41	LEFT UPPER LEG	.781836	-4.45		3.72875	3.74				220
42	LEFT LOWER LEG				6.	1.				219
43	LEFT LOWER LEG	-.36406	4.45		7.33778	2.23				220
44	LEFT FOOT				6.	1.				219
45	LEFT FOOT	5.32208	4.45		3.99875	1.8				220
46	RIGHT UPPER LEG				5.	1.				219
47	RIGHT UPPER LEG	.781836	4.45		3.72875	3.74				220
48	RIGHT FOOT				6.	1.				219
49	RIGHT FOOT	5.32208	-4.45		3.99875	1.8				220
50	LEFT UPPER ARM				7.	1.				219
51	LEFT UPPER ARM	0.	0.		6.88	1.64				220
52	LEFT LOWER ARM				8.	1.				219
53	LEFT LOWER ARM	0.	0.		.817523	1.11				220
54	RIGHT LOWER LEG				6.	1.				219
55	RIGHT LOWER LEG	-.36406	-4.45		7.33778	2.23				220
56	0.	8.80333	4.69511	4.89074	4.24		10.7	1.56504	-7.6	201
57	3.22789	2.15193	2.24974	2.44537	2.1982	6.05145	5.25	.573496	.76	202
58	.025	.095	.031	.098	.090	.050	.012	.012	.0047	203
59	.297	2.17	.31	1.78	.77	1.0	.137	.27		204

TABLE 4. Listing of Baseline Side Impact Input Data File. (Page 1 of 3).



120	DOOR SILL LINE	DOOR SILL	7.	0.	1.	1.			409
121	B-PILLAR LINE	B-PILLAR	7.	.284	1.	1.			409
122	HIP PANEL LINE	HIP PANEL	7.5	0.	1.	1.			409
123	WINDOW LINE	WINDOW	4.5	0.	1.	1.			409
124	DOORLINE	DOOR	6.8	0.	1.	1.			409
125	FLOORLINE	FLOOR	4.	0.	1.	1.			409
126	SEAT CUSHION LN.	SRAT CUSHION	7.5	0.	-1.	1.			409
127	HEADERLINE	1.							410
128	DOOR SILL LINE	1.							410
129	B-PILLAR LINE	1.							410
130	HIP PANEL LINE	4.							410
131	WINDOW LINE	1.							410
132	DOORLINE	4.							410
133	FLOORLINE	1.							410
134	SEAT CUSHION LN.	1.							410
135	HEADERLINE	1.	-10.5	-41.	0.	-53.			411
136	DOOR SILL LINE	-1.	-15.5	0.	-15.5	-26.			411
137	B-PILLAR LINE	-1.	-15.5	-26.	-10.5	-41.			411
138	HIP PANEL LINE	0.	-12.5	0.	-12.5	-40.			411
139	HIP PANEL LINE	5.	-12.5	0.	-12.5	-40.			411
140	HIP PANEL LINE	30.	-7.5	0.	-7.5	-40.			411
141	HIP PANEL LINE	100.	-7.5	0.	-7.5	-40.			411
142	WINDOW LINE	-1.	-20.	-18.	-9.	-50.			411
143	DOORLINE	0.	-15.5	0.	-15.5	-40.			411
144	DOORLINE	5.	-15.5	0.	-15.5	-40.			411
145	DOORLINE	30.	-10.5	0.	-10.5	-40.			411
146	DOORLINE	100.	-10.5	0.	-10.5	-40.			411
147	FLOORLINE	-1.	-22.	.00001	22.	.00001			411
148	SEAT CUSHION LN.	-1.	-22.	-10.35	12.	-10.35			411
149	1.	1.	0.						412
150	0.	0.	0.	0.	0.	0.	0.	0.	601
151	4.	1.	1.						602
152	0.	0.	5.	8.5	95.	8.5	100.	0.	
153	2.	0.	1.						603
154	0.	0.	200.	0.					
155	2.	0.							604
156	0.	0.	200.	0.					
1000									1000
1001	-1								1001
1002	1.	0.	-40.	40.	3.	-55.	5.	1.	1500
1003	21.	0.	0.	1.	1.	0.	1.	0.	1501
1004									1600
END OF FILE									

### 5.3 PEDESTRIAN IMPACT INPUT DATA

This part of the report contains the numerical details of the baseline MVMA 2-D pedestrian impact data set. Table 5 contains the output of the input data set after the input file has been processed by the IN section of the program. Not all pages are included. Those which are contain details of the linkage, joints, masses, inertial properties, contact ellipses, and program controls. Table 6 is a copy of the baseline data file which was constructed for the exercise.

SIMULATION CONTROL DATA

NO RESTRAINT BELTS PRESENT  
FIXED RUNGE-KUTTA INTEGRATION METHOD IS USED  
ACCELERATION DUE TO GRAVITY 32.1740 (FT/SEC\*\*2)  
MINIMUM ACCELERATION MAGNITUDE 0.0 (IN/SEC\*\*2) OR (RAD/SEC\*\*2)  
BEGINNING TIME 0.0 (MSEC)  
FINAL TIME 1000.00000 (MSEC)  
NUMERICAL INTEGRATION STEP SIZE 5.00000 (MSEC)  
OUTPUT PRINT INCREMENT 5.00000 (MSEC)  
OUTPUT PLOT INCREMENT 540.00000 (MSEC) IF ZERO, NO PLOT RECORDING  
ENGLISH UNITS ARE USED  
STEERING COLUMN INTERACTION IS NOT DESIRED  
AIRBAG INTERACTION IS NOT DESIRED  
ELLIPSE-ELLIPSE CONTACTS SPECIFIED ON 106 CARDS ARE ALLOWED  
ELLIPSE-REGION CONTACTS SPECIFIED ON 106 CARDS ARE ALLOWED  
ELLIPSE-ELLIPSE CONTACTS CAN OCCUR  
LENGTH OF SCALING RAMP TO INSURE CONTINUITY IN CONTACT FRICTION 10.000 (IN/SEC)  
RELATIVE ERROR TOLERANCE FOR SINGULARITY IN MATRIX INVERSION STEP 0.000001  
CPU TIME LIMIT FOR EXECUTION 2 (MIN)

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TABLE 5. Output of Baseline Input Data Set. Pedestrian Impact (Page 1 of 9).



INTEGRATION CONTROLS

MAXIMUM STEP TO SEARCH FOR BALANCE IN SHARED DEFLECTION	0.200 (IN)
MINIMUM STEP TO SEARCH FOR BALANCE IN SHARED DEFLECTION	0.020000 (IN)
MAXIMUM FORCE FOR RIGID-RIGID CONTACT	600.00 (LB)
LINEAR ELASTIC COEFFICIENT FOR RIGID-RIGID CONTACT	500.00 (LB/IN)
MAXIMUM NUMBER OF ITERATIONS TO FIND FORCE BALANCE	30
FRACTION OF CURRENT RAMP LENGTH FOR VELOCITY CHANGE IN MOVING CONTACT LINES	0.050
NUMBER OF INTEGRATION STEPS FOR MAXIMUM RAMP LENGTH FOR VELOCITY CHANGE IN MOVING CONTACT LINES	10.
MINIMUM RATIO OF SHORTER TO LONGER SEMI-MAJOR AXIS FOR ELLIPSE TO BE TREATED AS CIRCLE	1.000
FRACTIONAL POSITION OF CIRCLE CENTER ALONG SEMI-MAJOR AXIS RELATIVE TO POSITION FOR CIRCLE-ELLIPSE TANGENCY AT END OF AXIS	1.000

DEBUGGING CONTROLS

TIME TO SET DEBUG SWITCHES (MSEC)	0.0	2000.0000	0.0	0.0
DEBUG SWITCH SETTING IN HEXADECIMAL FORMAT	00000000	00000000	00000000	00000000
TIME TO SET DEBUG SWITCHES (MSEC)	0.0	0.0	0.0	0.0
DEBUG SWITCH SETTING IN HEXADPCIMAL FORMAT	00000000	00000000	00000000	00000000

DEBUG CONTROLS ARE TO OPERATE FOR ALL INTEGRATION EVALUATIONS AT EACH TIME

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TABLE 5. Output of Baseline Input Data Set. Pedestrian Impact (Page 2 of 9).

BODY PARAMETERS

HEAD LENGTH=	0.0	END OF LINK TO CENTER-OF-MASS LENGTHS (IN)	3.19	MASS OF BODY SEGMENTS (LBS SEC**2 IN)	0.0250
UPPER TORSO LENGTH=	8.69	HEAD/NECK JOINT-HEAD CM LENGTH=	3.11	HEAD MASS=	0.1260
MIDDLE TORSO LENGTH=	8.49	NECK-CHEST CM LENGTHS=	8.49	CHEST MASS=	0.0790
LOWER TORSO LENGTH=	0.0	UPPER TORSO JOINT-MIDDLE TORSO CM LENGTH=	12.66	MIDDLE TORSO MASS=	0.0800
HIP-KNEE LENGTH=	13.41	LOWER TORSO JOINT LOWER TORSO CM LENGTH=	6.95	LOWER TORSO MASS=	0.0540
UPPER TORSO-SHOULDER=	0.0	HIP-UPPER LEG CM LENGTH=	10.32	UPPER LEG (BOTH LEGS)=	0.0250
SHOULDER-ELBOW LENGTH=	10.64	KNEE-LOWER LEG CM LENGTH=	5.22	LOWER LEG (BOTH LEGS)=	0.0120
X REST POINT OF SHOULDER=	1.55	SHOULDER-UPPER ARM CM LENGTH=	3.98	UPPER ARM (BOTH ARMS)=	0.0120
Z REST POINT OF SHOULDER=	6.60	ELBOW-LOWER ARM CM LENGTH=		LOWER ARM (BOTH ARMS)=	0.0036
				HEAD-NECK MASS=	0.0011
				UPPER TORSO-NECK MASS=	0.0011

MOMENTS OF INERTIA (ABOUT CM) INITIAL BODY LINK ANGLES INITIAL ANGULAR VELOCITIES (LBS SEC\*\*2 IN) (DEG) (DEG/SEC)

HEAD	0.2970	0.0	90.00	0.0
UPPER TORSO	2.8900	0.0	90.00	0.0
MIDDLE TORSO	2.1900	0.0	90.00	0.0
LOWER TORSO	1.0000	0.0	90.00	0.0
UPPER LEG	0.7700	0.0	-90.00	0.0
LOWER LEG	1.0000	0.0	-90.00	0.0
UPPER ARM	0.1370	-12.00	-78.00	0.0
LOWER ARM	0.2700	27.00	-105.00	0.0
NECK	0.0		90.00	0.0

OCCUPANT JOINT PARAMETERS

	LINEAR ANGULAR DEFLECTION COEFF. (IN-LBS/DEG)	QUADRATIC ANGULAR DEFLECTION COEFF. (IN-LBS/DEG**2)	CUBIC ANGULAR DEFLECTION COEF. (IN-LBS/DEG**3)	CONSERVED-ABSORBED ENERGY RATIO
HEAD-NECK FORWARD	31.20000	0.0	0.0	1.00
NECK-UPPER TORSO FORWARD	31.20000	0.0	0.0	1.00
UPPER SPINE	50.00000	0.0	0.0	1.00
LOWER SPINE	16.00000	0.0	0.0	1.00
HIP	16.00000	0.0	0.0	0.0
KNEE	0.0	0.0	0.0	0.0
UPPER ARM-UPPER TORSO	-10.00000	10.00000	0.0	0.25
ELBOW	-10.00000	10.00000	0.0	1.00
HEAD-NECK REAR	31.20000	0.0	0.0	1.00
NECK-UPPER TORSO REAR	31.20000	0.0	0.0	NA
NECK (EXTENSIBLE) **	751.00000	0.0	757.00000	0.50
SHOULDER (EXTENSIBLE)**	10.00000	0.0	100.00000	NA
NECK (COMPRESSIBLE) **	751.00000	0.0	757.00000	NA

\*\* UNITS FOR THE NECK (EXTENSIBLE), (COMPRESSIBLE) AND SHOULDER (EXTENSIBLE) PARAMETERS ARE GIVEN IN THE ROW BELOW (LB/IN\*\*2) (LB/IN\*\*3)

TABLE 5. Output of Baseline Input Data Set. Pedestrian Impact (Page 3 of 9).

	VISCOUS FRICTION (IN LBS SPC/DEG)	CONSTANT FRICTION COEFFICIENT (IN-LBS)	VELOCITY THRESHOLD FOR CONST. FRICTION (DEG/SEC)	POS. JOINT STOP (DEG)	NEG. JOINT STOP (DEG)
HEAD-NECK FORWARD	0.0	0.0	0.0	0.0	0.0
NECK-UPPER TORSO FORWARD	0.0	0.0	0.0	0.0	0.0
UPPER SPINF	0.0	0.0	0.0	0.0	0.0
LOWER SPINF	0.0	0.0	0.0	0.0	0.0
HIP	0.0	0.0	0.0	0.0	0.0
KNEE	0.0	505.50	1.00	0.0	0.0
UPPER ARM-UPPER TORSO	0.0	0.0	0.0	18.00	-42.00
ELBOV	0.0	0.0	0.0	57.00	-3.00
HEAD-NECK REAR	0.0	0.0	0.0	0.0	0.0
NECK-UPPER TORSO REAR	0.0	0.0	0.0	0.0	0.0
NECK (EXTENSIBLE) **	1.9800	NA	NA	NA	NA
SHOULDER (EXTENSIBLE) **	0.0	NA	NA	3.00	NA
NECK (COMPRESSIBLE) **	1.9800	NA	NA	NA	NA

\*\*UNITS FOR THE NECK (EXTENSIBLE), (COMPRESSIBLE) AND SHOULDER (EXTENSIBLE) PARAMETERS ARE GIVEN IN THE ROW BELOW (LB SEC/IN) (IN)

MUSCLE TENSION COEFFICIENTS

	STIFFNESS COEF. A1 (K=A1+A2(M)) (IN-LBS/DEG)	STIFFNESS COEF. A2 (K=A1+A2(M)) (1/DEG)	DAMPING COEF. A3 (C=A3(M)) (SEC/DEG)	INIT. MUSCLE FORCE OR MOMENT RESULTANT (IN-LBS)	MUSCLE ASSIGNED TO MUSCLE TENSION TABLE (M) VS TIME
HEAD-NECK	0.0	0.0	0.0	0.0	
NECK-UPPER TORSO	0.0	0.0	0.0	0.0	
UPPER SPINE	0.0	0.0	0.0	0.0	
LOWER SPINF	0.0	0.0	0.0	0.0	
HIP	0.0	0.0	0.0	0.0	
KNEE	0.0	0.0	0.0	0.0	
UPPER ARM-UPPER TORSO	0.0	0.0	0.0	0.0	
ELBOV	0.0	0.0	0.0	0.0	
SHOULDER-UPPER TORSO	0.0	0.0	0.0	0.0	
NECK (EXTENSIBLE) **	0.0	0.0	0.0	0.0	
SHOULDER (EXTENSIBLE) **	0.0	0.0	0.0	0.0	

\*\*UNITS FOR NECK (EXTENSIBLE) AND SHOULDER (EXTENSIBLE) PARAMETERS ARE GIVEN IN THE ROW BELOW (LB/IN) (SEC/IN) (LB)

TABLE 5. Output of Baseline Input Data Set. Pedestrian Impact (Page 4 of 9).

INITIAL CONDITIONS FOR UPPER TORSO AND NECK

INITIAL (X,Z) COORDINATE OF CENTERLINE POINT NUM. 1 RELATIVE TO VEHICLE ORIGIN IN (IN) ( 0.0 , -47.63 )  
INITIAL (X,Z) VELOCITY OF CENTERLINE POINT NUM. 1 RELATIVE TO VEHICLE ORIGIN IN (FT/SEC) ( 14.6667, 0.0 )  
INITIAL NECK LENGTH 4.83 (IN)  
INITIAL RATE OF EXTENSION OF NECK 0.0 (IN/SEC)

INITIAL SHOULDER LOCATION AND VELOCITY RELATIVE TO UPPER TORSO ATTACHMENT

INITIAL (X,Z) COORDINATES OF SHOULDER JOINT RELATIVE TO UPPER TORSO ATTACHMENT POINT IN (IN) ( 0.0 , 0.0 )  
INITIAL (X,Z) VELOCITY IN UPPER TORSO SYSTEM IN (IN/SEC) ( 0.0 , 0.0 )

OCCUPANT ACCELEROMETER AND BELT ATTACHMENT PARAMETERS

DISTANCE ALONG HEAD-NECK CENTERLINE TO HEAD ACCELEROMETER 3.19 (IN)  
DISTANCE ALONG UPPER TORSO CENTERLINE TO CHEST ACCELEROMETER 2.13 (IN)

VEHICLE INITIAL CONDITIONS AND ACCELEROMETER LOCATION

(X,Z) COORDINATES OF VEHICLE ORIGIN IN (IN) ( 0.0 , 0.0 )  
INITIAL (X,Z) VEHICLE VELOCITY IN (FT/SEC) ( -14.67, 0.0 )  
INITIAL VEHICLE PITCH ANGLE 0.0 (DEG)  
INITIAL VEHICLE PITCH ANGULAR VELOCITY 0.0 (DEG/SEC)  
(X,Z) COORDINATES OF VEHICLE ACCELEROMETER IN (IN) ( 0.0 , 0.0 )  
MASS OF VEHICLE 0.0 (LBS SEC\*\*2/IN)

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TABLE 5. Output of Baseline Input Data Set. Pedestrian Impact (Page 5 of 9).

ELLIPSES ATTACHED TO THE HEAD

NAME OF ELLIPSE IS HEAD	ELLIPSE IS ASSUMED RIGID	FRICITION CLASS IS	1
X-COORDINATE OF ELLIPSE CENTER IN BODY SEGMENT COORDINATES=	0.0 (IN)	SEMI-AXIS LENGTH ALONG X-COORDINATE=	4.434 (IN)
Z-COORDINATE OF ELLIPSE CENTER IN BODY SEGMENT COORDINATES=	0.0 (IN)	SEMI-AXIS LENGTH ALONG Z-COORDINATE=	3.100 (IN)

REGIONS WHICH ARE ALLOWED TO CONTACT THE ELLIPSE HEAD

WINDSHIELD  
 HOOD  
 CAR FRONT  
 ROOF

ELLIPSES ATTACHED TO THE UPPER TORSO

NAME OF ELLIPSE IS UPPER TORSO	ELLIPSE IS ASSUMED RIGID	FRICITION CLASS IS	1
X-COORDINATE OF ELLIPSE CENTER IN BODY SEGMENT COORDINATES=	-0.983 (IN)	SEMI-AXIS LENGTH ALONG X-COORDINATE=	4.772 (IN)
Z-COORDINATE OF ELLIPSE CENTER IN BODY SEGMENT COORDINATES=	0.0 (IN)	SEMI-AXIS LENGTH ALONG Z-COORDINATE=	5.800 (IN)

REGIONS WHICH ARE ALLOWED TO CONTACT THE ELLIPSE UPPER TORSO

ROOF  
 WINDSHIELD  
 HOOD  
 CAR FRONT

ELLIPSE IS ASSUMED RIGID

NAME OF ELLIPSE IS CENTER TORSO	ELLIPSE IS ASSUMED RIGID	FRICITION CLASS IS	1
X-COORDINATE OF ELLIPSE CENTER IN BODY SEGMENT COORDINATES=	7.759 (IN)	SEMI-AXIS LENGTH ALONG X-COORDINATE=	6.790 (IN)
Z-COORDINATE OF ELLIPSE CENTER IN BODY SEGMENT COORDINATES=	0.0 (IN)	SEMI-AXIS LENGTH ALONG Z-COORDINATE=	5.750 (IN)

ELLIPSES ATTACHED TO THE MIDDLE TORSO

ELLIPSE IS ASSUMED RIGID

NAME OF ELLIPSE IS LOWER TORSO	ELLIPSE IS ASSUMED RIGID	FRICITION CLASS IS	1
X-COORDINATE OF ELLIPSE CENTER IN BODY SEGMENT COORDINATES=	0.426 (IN)	SEMI-AXIS LENGTH ALONG X-COORDINATE=	7.341 (IN)
Z-COORDINATE OF ELLIPSE CENTER IN BODY SEGMENT COORDINATES=	0.0 (IN)	SEMI-AXIS LENGTH ALONG Z-COORDINATE=	5.500 (IN)

REGIONS WHICH ARE ALLOWED TO CONTACT THE ELLIPSE LOWER TORSO

WINDSHIELD

TABLE 5. Output of Baseline Input Data Set. Pedestrian Impact (Page 6 of 9).

REGIONS WHICH ARE ALLOWED TO CONTACT THE ELLIPSE LOWER TORSO

HOOD

CAR FRONT

GRLL

ELLIPSES ATTACHED TO THE LOWER TORSO

NAME OF ELLIPSP IS LEFT UPPER LEG

ELLIPSE IS ASSUMED RIGID

FRICTION CLASS IS 1

X-COORDINATE OF ELLIPSE CENTER IN BODY SEGMENT COORDINATES= -5.460 (IN)  
 Z-COORDINATE OF ELLIPSE CENTER IN BODY SEGMENT COORDINATES= 2.800 (IN)

SEMI-AXIS LENGTH ALONG X-COORDINATE= 11.030 (IN)  
 SEMI-AXIS LENGTH ALONG Z-COORDINATE= 2.500 (IN)

REGIONS WHICH ARE ALLOWED TO CONTACT THE ELLIPSE LEFT UPPER LEG

HOOD

GRLL

CAR FRONT

ELLIPSES WHICH ARE ALLOWED TO CONTACT THE ELLIPSE LEFT UPPER LEG

RIGHT UPPER LEG

NAME OF ELLIPSE IS LEFT LOWER LEG

ELLIPSE IS ASSUMED RIGID

FRICTION CLASS IS 1

X-COORDINATE OF ELLIPSE CENTER IN BODY SEGMENT COORDINATES= 8.005 (IN)  
 Z-COORDINATE OF ELLIPSE CENTER IN BODY SEGMENT COORDINATES= 2.800 (IN)

SEMI-AXIS LENGTH ALONG X-COORDINATE= 8.220 (IN)  
 SEMI-AXIS LENGTH ALONG Z-COORDINATE= 2.230 (IN)

REGIONS WHICH ARE ALLOWED TO CONTACT THE ELLIPSE LEFT LOWER LEG

BUMPER

NAME OF ELLIPSE IS LEFT FOOT

ELLIPSE IS ASSUMED RIGID

FRICTION CLASS IS 2

X-COORDINATE OF ELLIPSE CENTER IN BODY SEGMENT COORDINATES= 16.752 (IN)  
 Z-COORDINATE OF ELLIPSE CENTER IN BODY SEGMENT COORDINATES= 2.800 (IN)

SEMI-AXIS LENGTH ALONG X-COORDINATE= 1.085 (IN)  
 SEMI-AXIS LENGTH ALONG Z-COORDINATE= 1.800 (IN)

REGIONS WHICH ARE ALLOWED TO CONTACT THE ELLIPSE LEFT FOOT

GROUND

BUMPER

GRLL

TABLE 5. Output of Baseline Input Data Set. Pedestrian Impact (Page 7 of 9).

ELLIPSES ATTACHED TO THE UPPER LEG  
 ELLIPSE IS ASSUMED RIGID FRICTION CLASS IS 1  
 NAME OF ELLIPSE IS RIGHT UPPER LEG  
 X-COORDINATE OF ELLIPSE CENTER IN BODY SEGMENT COORDINATES= -1.427 (IN) SEMI-AXIS LENGTH ALONG X-COORDINATE= 10.652 (IN)  
 Z-COORDINATE OF ELLIPSE CENTER IN BODY SEGMENT COORDINATES= -2.800 (IN) SEMI-AXIS LENGTH ALONG Z-COORDINATE= 2.500 (IN)

REGIONS WHICH ARE ALLOWED TO CONTACT THE ELLIPSE RIGHT UPPER LEG  
 HOOD  
 GRILL  
 CAR FRONT  
 ELLIPSES WHICH ARE ALLOWED TO CONTACT THE ELLIPSE RIGHT UPPER LEG

ELLIPSES ATTACHED TO THE LOWER LEG  
 ELLIPSE IS ASSUMED RIGID FRICTION CLASS IS 1  
 NAME OF ELLIPSE IS RIGHT KNEE  
 X-COORDINATE OF ELLIPSE CENTER IN BODY SEGMENT COORDINATES= -5.699 (IN) SEMI-AXIS LENGTH ALONG X-COORDINATE= 1.740 (IN)  
 Z-COORDINATE OF ELLIPSE CENTER IN BODY SEGMENT COORDINATES= -2.800 (IN) SEMI-AXIS LENGTH ALONG Z-COORDINATE= 2.230 (IN)

REGIONS WHICH ARE ALLOWED TO CONTACT THE ELLIPSE RIGHT KNEE  
 BUMPER  
 ELLIPSE IS ASSUMED RIGID FRICTION CLASS IS 1  
 NAME OF ELLIPSE IS RIGHT SHIN  
 X-COORDINATE OF ELLIPSE CENTER IN BODY SEGMENT COORDINATES= 2.342 (IN) SEMI-AXIS LENGTH ALONG X-COORDINATE= 6.305 (IN)  
 Z-COORDINATE OF ELLIPSE CENTER IN BODY SEGMENT COORDINATES= -2.800 (IN) SEMI-AXIS LENGTH ALONG Z-COORDINATE= 2.230 (IN)

REGIONS WHICH ARE ALLOWED TO CONTACT THE ELLIPSE RIGHT SHIN  
 BUMPER  
 ELLIPSE IS ASSUMED RIGID FRICTION CLASS IS 2  
 NAME OF ELLIPSE IS RIGHT FOOT  
 X-COORDINATE OF ELLIPSE CENTER IN BODY SEGMENT COORDINATES= 8.642 (IN) SEMI-AXIS LENGTH ALONG X-COORDINATE= 1.520 (IN)  
 Z-COORDINATE OF ELLIPSE CENTER IN BODY SEGMENT COORDINATES= -2.800 (IN) SEMI-AXIS LENGTH ALONG Z-COORDINATE= 1.800 (IN)

REGIONS WHICH ARE ALLOWED TO CONTACT THE ELLIPSE RIGHT FOOT  
 GROUND  
 GRILL

TABLE 5. Output of Baseline Input Data Set. Pedestrian Impact (Page 8 of 9).

ELLIPSES ATTACHED TO THE UPPER ARM

NAME OF ELLIPSE IS RIGHT UPPER ARM	ELLIPSE IS ASSUMED RIGID	FRICITION CLASS IS	1
X-COORDINATE OF ELLIPSE CENTER IN BODY SEGMENT COORDINATES=	0.0 (IN)	SEMI-AXIS LENGTH ALONG Y-COORDINATE=	6.842(IN)
Z-COORDINATE OF ELLIPSE CENTER IN BODY SEGMENT COORDINATES=	0.0 (IN)	SEMI-AXIS LENGTH ALONG Z-COORDINATE=	1.640(IN)

REGIONS WHICH ARE ALLOWED TO CONTACT THE ELLIPSE RIGHT UPPER ARM

HOOD  
WINDSHIELD

ELLIPSES ATTACHED TO THE LOWER ARM

NAME OF ELLIPSE IS RIGHT LOWER ARM	ELLIPSE IS ASSUMED RIGID	FRICITION CLASS IS	1
X-COORDINATE OF ELLIPSE CENTER IN BODY SEGMENT COORDINATES=	-2.566 (IN)	SEMI-AXIS LENGTH ALONG Y-COORDINATE=	5.718(IN)
Z-COORDINATE OF ELLIPSE CENTER IN BODY SEGMENT COORDINATES=	0.0 (IN)	SEMI-AXIS LENGTH ALONG Z-COORDINATE=	1.400(IN)

REGIONS WHICH ARE ALLOWED TO CONTACT THE ELLIPSE RIGHT LOWER ARM

HOOD  
GRILL  
CAR FRONT

ELLIPSE IS ASSUMED RIGID

NAME OF ELLIPSE IS RIGHT HAND	ELLIPSE IS ASSUMED RIGID	FRICITION CLASS IS	1
X-COORDINATE OF ELLIPSE CENTER IN BODY SEGMENT COORDINATES=	3.333 (IN)	SEMI-AXIS LENGTH ALONG Y-COORDINATE=	3.680 (IN)
Z-COORDINATE OF ELLIPSE CENTER IN BODY SEGMENT COORDINATES=	0.515 (IN)	SEMI-AXIS LENGTH ALONG Z-COORDINATE=	1.200 (IN)

TABLE 5. Output of Baseline Input Data Set. Pedestrian Impact (Page 9 of 9).



\$SIG SNZQ T=1M P=500 C=0 PRIO=D \*J.M.BECKFR\*  
 BATCH,DEFERRED,UNIV  
 \*\*LAST SIGNON WAS: 10:27:49 WED MAY 20/81  
 USFR "SNZQ" SIGNED ON AT 00:26:34 ON THU MAY 21/81  
 INCOMING MESSAGES: 1 (1 NOT ACCESSED)

\$GET 15WALKIA  
 READY.  
 \$.01. \$.04T  
 \$SOURCE RUNM2D10  
 \$.00. \$.04T  
 \$EMPTY P10C1 OK  
 DONE.  
 \$.00. \$.04T  
 \$EMPTY CF8 OK  
 DONE.  
 \$.00. \$.04T  
 \$EMPTY CF7 OK  
 DONE.  
 \$.00. \$.04T  
 \$EMPTY CF9 OK  
 DONE.  
 \$.00. \$.04T  
 \$EMPTY CF10 OK  
 DONE.  
 \$.00. \$.05T  
 \$EMPTY TSRCA OK  
 DONE.  
 \$.00. \$.05T  
 \$EMPTY TSRCB OK  
 DONE.  
 \$.00. \$.05T  
 \$EMPTY TOBJA OK  
 DONE.  
 \$.00. \$.05T  
 \$LIST \*AFD\*

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		PEDESTRIAN #1 -- 15 DEGREES							
1									100
2	3D-2D:RT ARM-ARM LI								200
3	NKS/LT ARM-LUMPED W								300
4	.TORSO/RT LEG-LEG L								400
5	INKS/LT LEG-LOWER T								500
6	ORSO LINK/TORSO-UP								600
7	AND MID TORSO LINKS								700
8	IMPACT FROM RT								800
9	1. 1.	32.174	0.	0.	1000.	5.	5.	540.	101
10	0. 0.	0.	0.	0.	0.	10.	.000001	2.	102
11	.2 .02	600.	500.	30.	.05	10.	1.	1.	103
12	HEAD								106
13	HEAD								106
14	HEAD								106
15	HEAD								106
16	UPPER TORSO								106
17	UPPER TORSO								106
18	UPPER TORSO								106
19	UPPER TORSO								106
20	LOWER TORSO								106
21	LOWER TORSO								106
22	LOWER TORSO								106

TABLE 6. Listing of Baseline Pedestrian Impact Input Data File. (Page 1 of 4).







#### 5.4 REPRESENTATIVE SIDE IMPACT OUTPUT

Figures 13 through 15 are a graphical presentation of some of the important kinematic and dynamic variables produced by the computer exercise using the baseline side impact data. Figure 13 shows a sequence of three contacts as the occupant interacts with the side structures. It should be noted that significant forces are built up in the lower torso (hip) region by 30 ms. This point would have occurred much later without the intrusion of the door and hip panels. The upper torso forces reach their maximum at about 60 ms which reflects the fact that the door panel is outboard in the vehicle from the hip panel. The left arm (simulating Part 572 rather than dummies with collapsible shoulder structures) contacts the door at a much earlier period in time. The head rotates toward the window and hits side structures very hard by 75 ms after which rebound begins.

Figure 14 shows a trace of the motions of several body segments during the simulation. Lower torso linear motion to the side is relatively small due to the early interaction of the hip with the intruding hip panel. However, this does not prevent rotation of the lower legs toward the forward portion of the door structures which are not programmed for intrusion. The head pitches to the side but interacts only with the side header and B-pillar. In cases where B-pillar interaction is not expected, this contact should be suppressed for MVMA 2-D simulations as the B-pillar line will always be inboard from the window line thus preventing initial window contact. Also, the fact that lower torso side motion is limited due to the intrusion prohibits the head from moving too far to the side. Figure 15 is an assembly of Calcomp plots produced by the movie generation post-processor routines graphically documenting the kinematics just discussed.

Table 7 is a summary of all occupant/vehicle contact interactions. The time, deflection, and force are given for initiation of contact, peak force, and the final time of a contact event. In one case it is seen that the peak force occurs at the end of the simulation. For a further study of the output, including any cases of multiple peaks, it is necessary to review the complete simulation output.

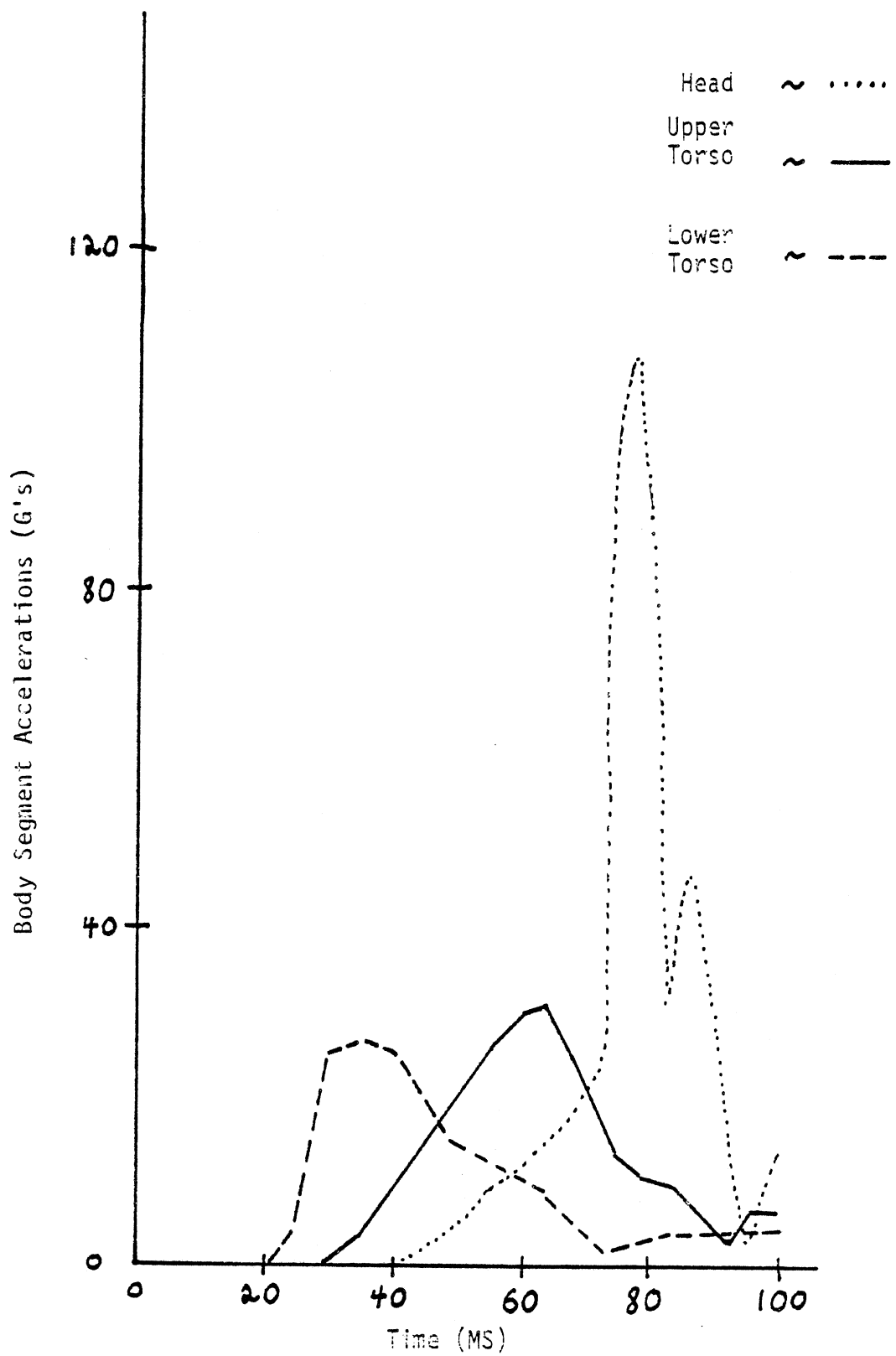


Fig. 13. Body Segment Accelerations. Side Impact.

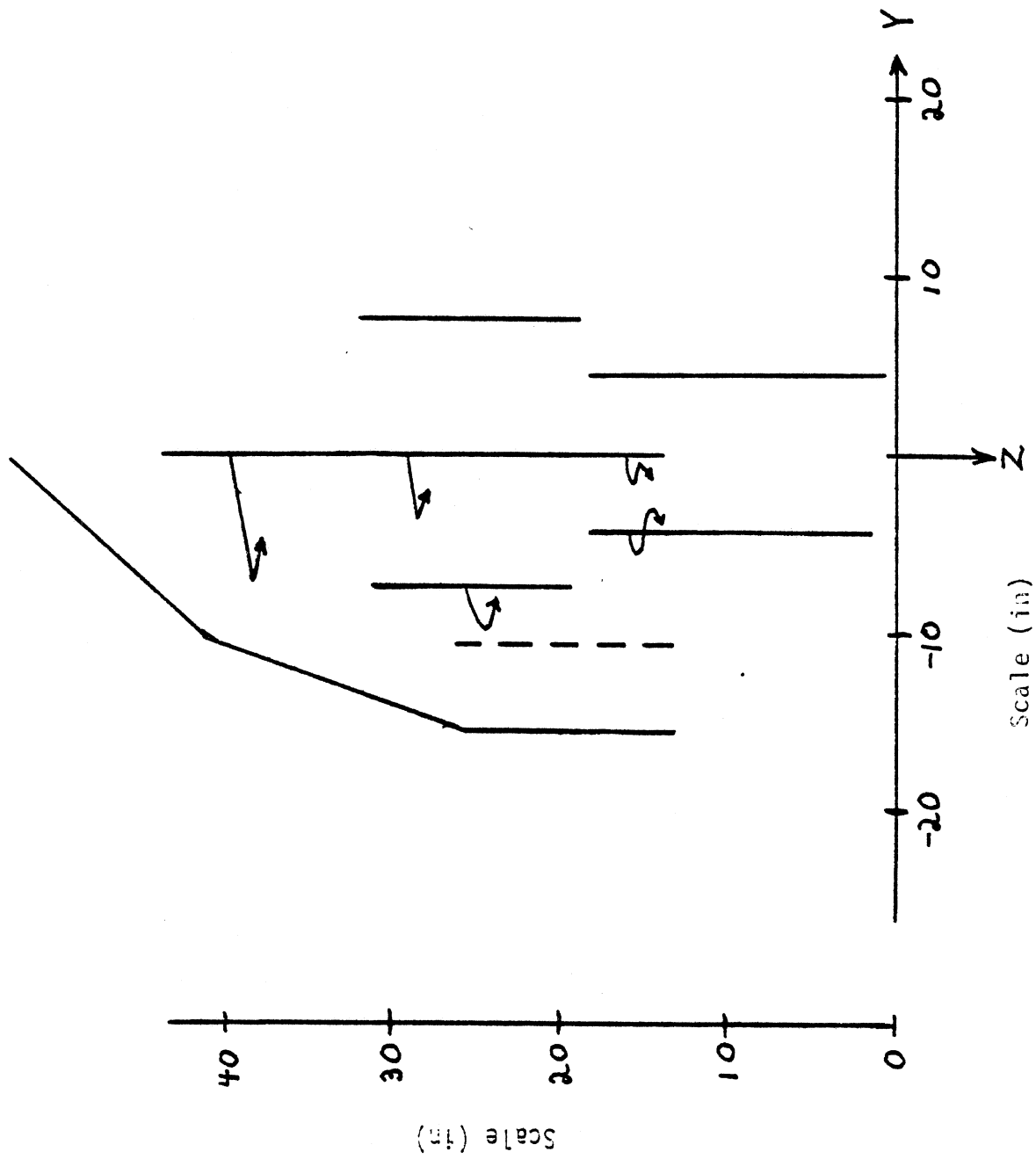


Fig. 14. Occupant Segment Motions in Side Impact Simulation.

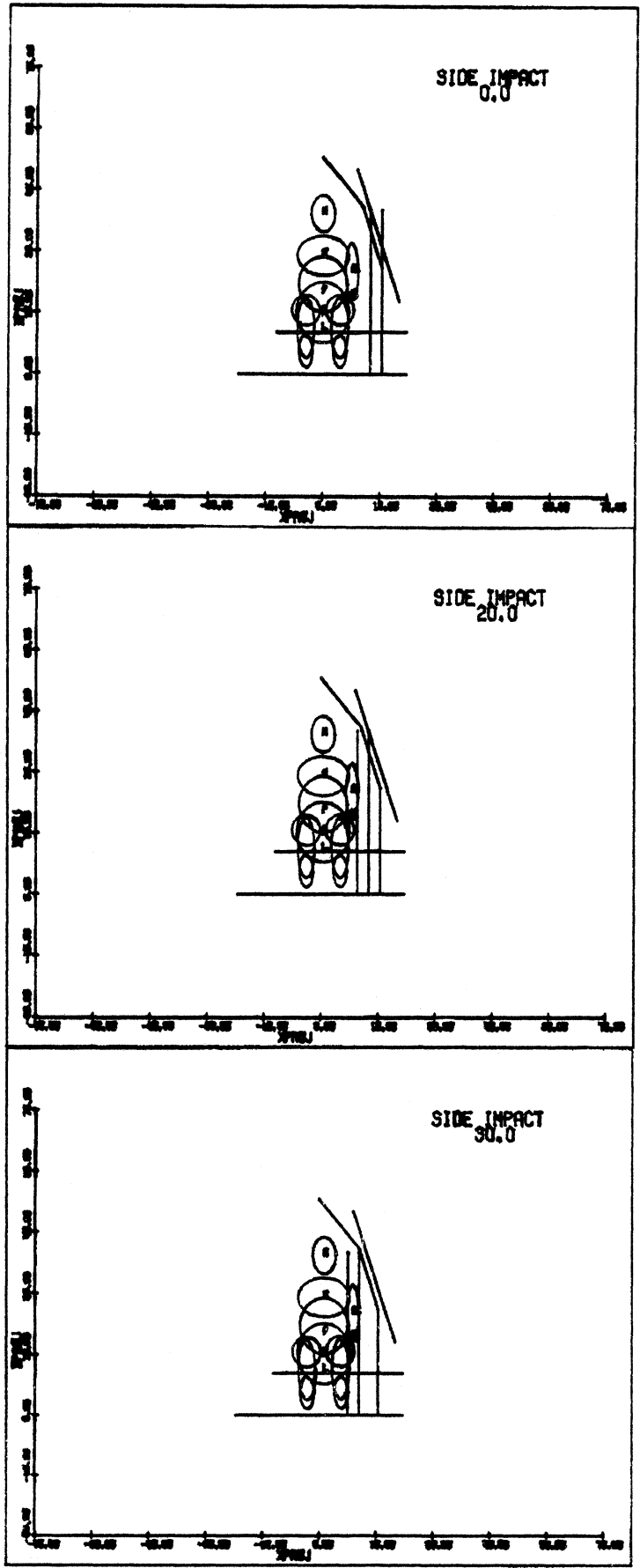


Fig. 15. Side Impact Occupant Kinematics. (1 of 2; 0, 20, 30 ms)



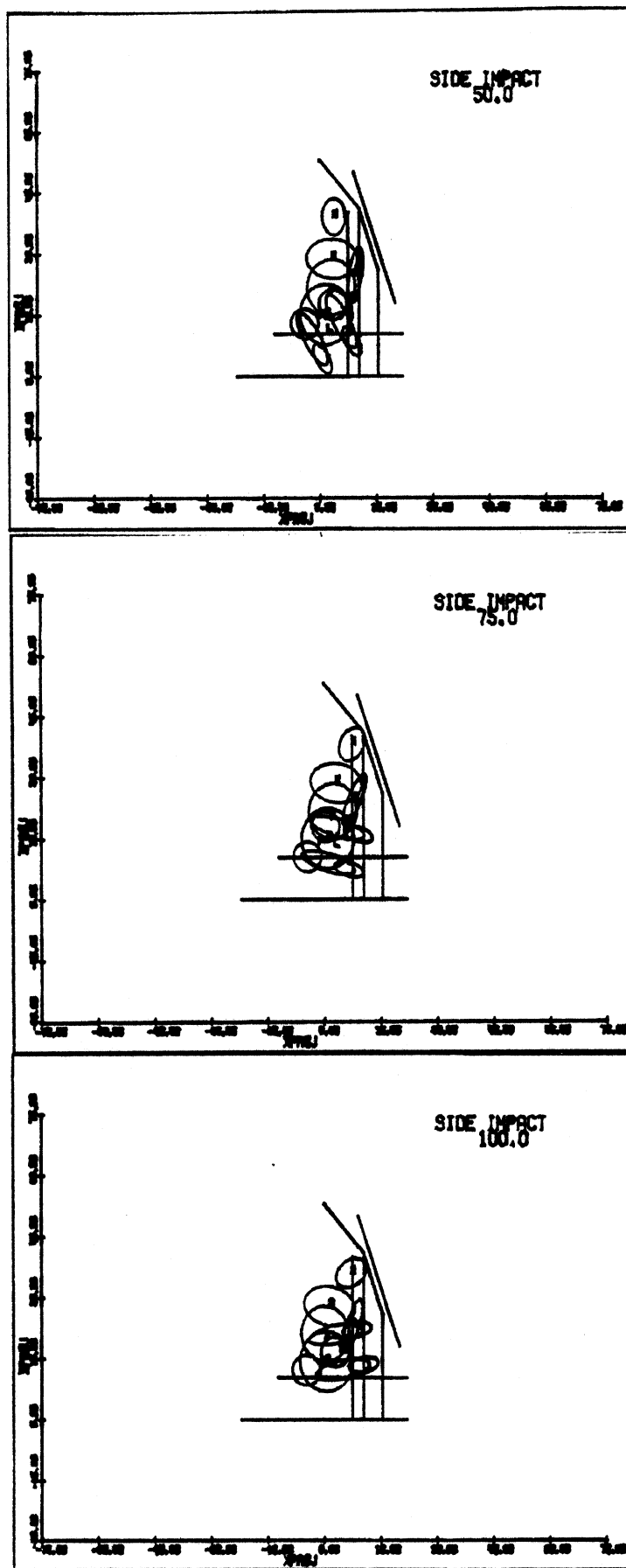


Fig. 15. Side Impact Occupant Kinematics. (2 of 2; 50, 75, 100 ms)

TABLE 7. SIDE IMPACT OCCUPANT/VEHICLE CONTACT HISTORY

Ellipse Name	Contact Name	Initial Contact			Peak Contact			Final Contact		
		Time (ms)	Deflection (in)	Force (lb)	Time (ms)	Deflection (in)	Force (lb)	Time (ms)	Deflection (in)	Force (lb)
Lower Torso	Seat Cushion	0	2.6	103	100	3.5	141	100	3.5	141
	Hip Panel	28	0.1	94	43	1.1	1092	95	0.0	16
Upper Torso	Door	60	0.0	1	62	0.0	13	63	0.0	9
	Header	73	0.0	3	76	0.2	98	79	0.1	38
Head	B-Pillar	74	0.0	22	79	0.4	978	83	0.1	155
	Seat Cushion	44	0.1	3	77	3.6	145	100	2.0	78
Left Upper Leg	Hip Panel	24	0.3	250	33	1.9	1880	48	0.1	110
	Door	31	0.1	77	62	1.2	1198	92	0.0	4
Left Lower Arm	Door	37	0.1	46	40	0.1	129	43	0.0	23

## 5.5 REPRESENTATIVE PEDESTRIAN IMPACT OUTPUT

Figure 16 includes a series of frames showing pedestrian kinematics at various time points during the exercise. The initial bumper contact with the right knee segment starts at 35 ms, peaks at 45 ms, and is over by 100 ms. The grille, grille top, and hood also contact the pedestrian lower torso and right lower arm early in the simulation. The right upper leg also is observed to contact the left lower leg.

The next sequence of major contacts is observed to take place as the upper torso rotates over onto the hood. Both segments of the right arm, the upper torso, and the head are active in this stage of the impact. Following this the pedestrian is pitched upward and in front of the moving vehicle.

By 815 ms the final stage of the impact event is begun as the feet hit the ground and the body begins to collapse. Contacts with the moving vehicle are again sensed near the end of the simulation. A three dimensional simulation would be required to sense whether the pedestrian rolled off to the side of the vehicle or ends up in a position where the vehicle can pass over him.

Table 8 is a summary of all pedestrian/vehicle exterior contacts. As in Table 7, the time, deflection, and force are given for initiation of contact, peak force and the final time of each contact event.

Figures 17 through 19 give the resultant accelerations predicted in the upper torso, head, and hip segment while Figures 20 through 23 report the time history of four important contact interactions. The hip acceleration and resulting contact force between the lower torso and the grille appear to provide the major initial force in controlling overall body kinematics. The upper torso and head accelerations peak at a later time. The leading force transmitter in this second interaction is the right upper arm which interacted with the hood.

It was necessary to "soften" the flexible shoulder element in order to obtain a successful exercise. A total of 5 inches of shoulder joint motion in the inferior direction was predicted as the subject rotated onto the hood (See Figure 16 at 160 ms.)

It should be noted that the force-deflection curves used to govern the interactions between the vehicle and pedestrian are hypothetical. In order to improve the qualitative agreement between the simulation and observed movies of experimental pedestrian impacts, both energy absorption and friction were included with dramatic effect. Before inclusion of these factors, the results very nearly matched the predictions obtained in the earlier project using the HSRI version of the CAL3D model.

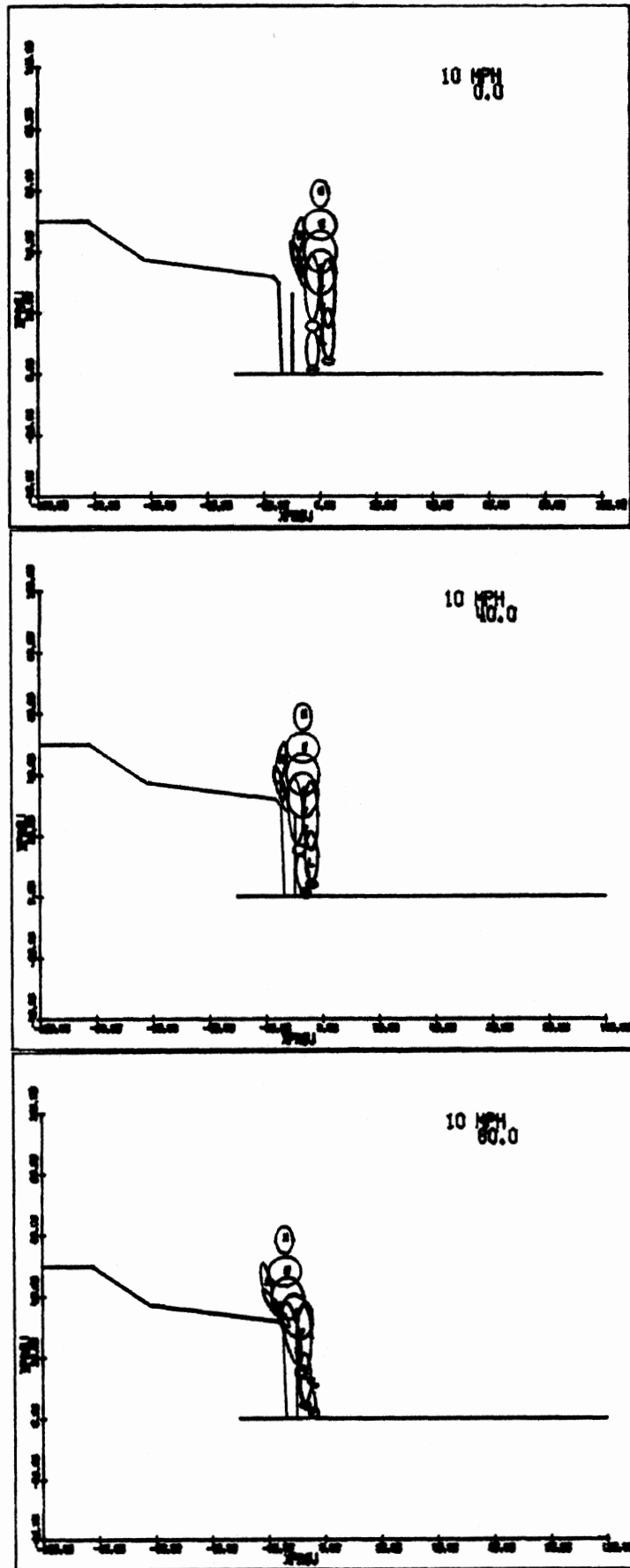


Fig. 16. Pedestrian Kinematics. (1 of 3; 0, 40, 80 ms)

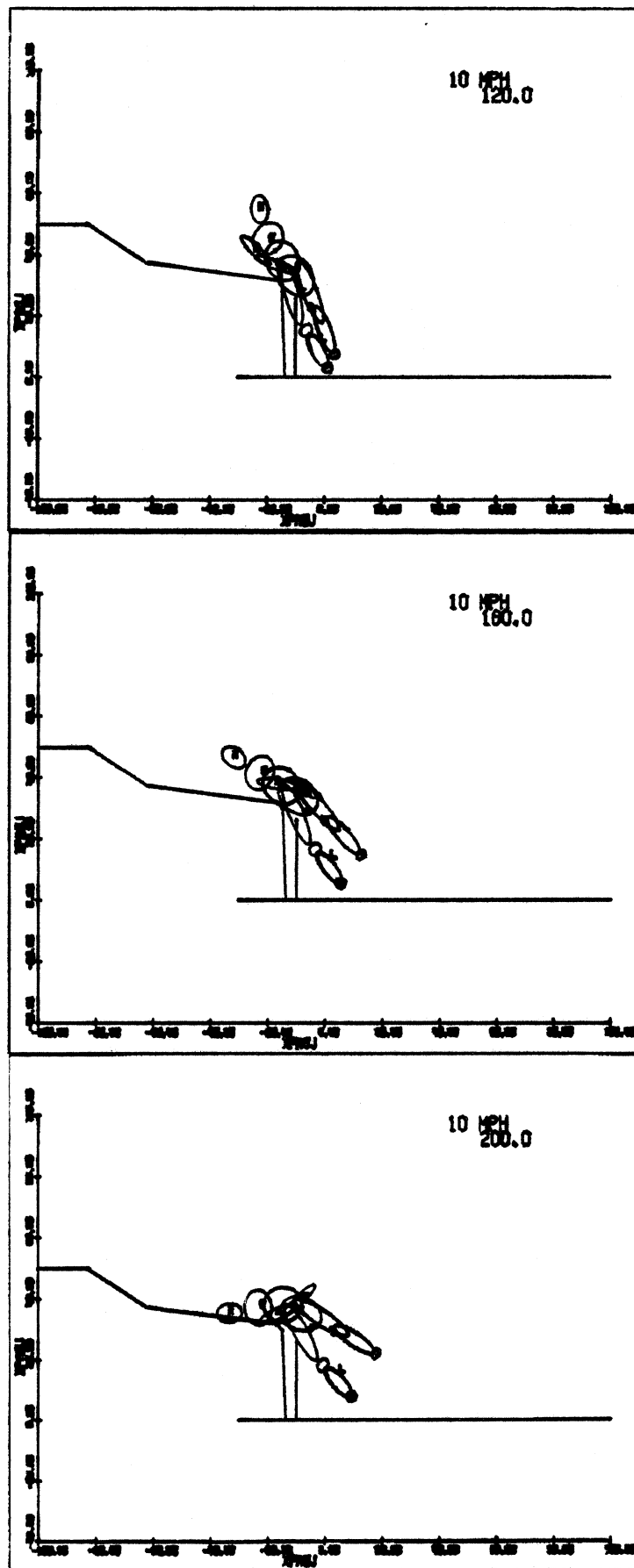


Fig. 16. Pedestrian Kinematics. (2 of 3; 120, 160, 200 ms)

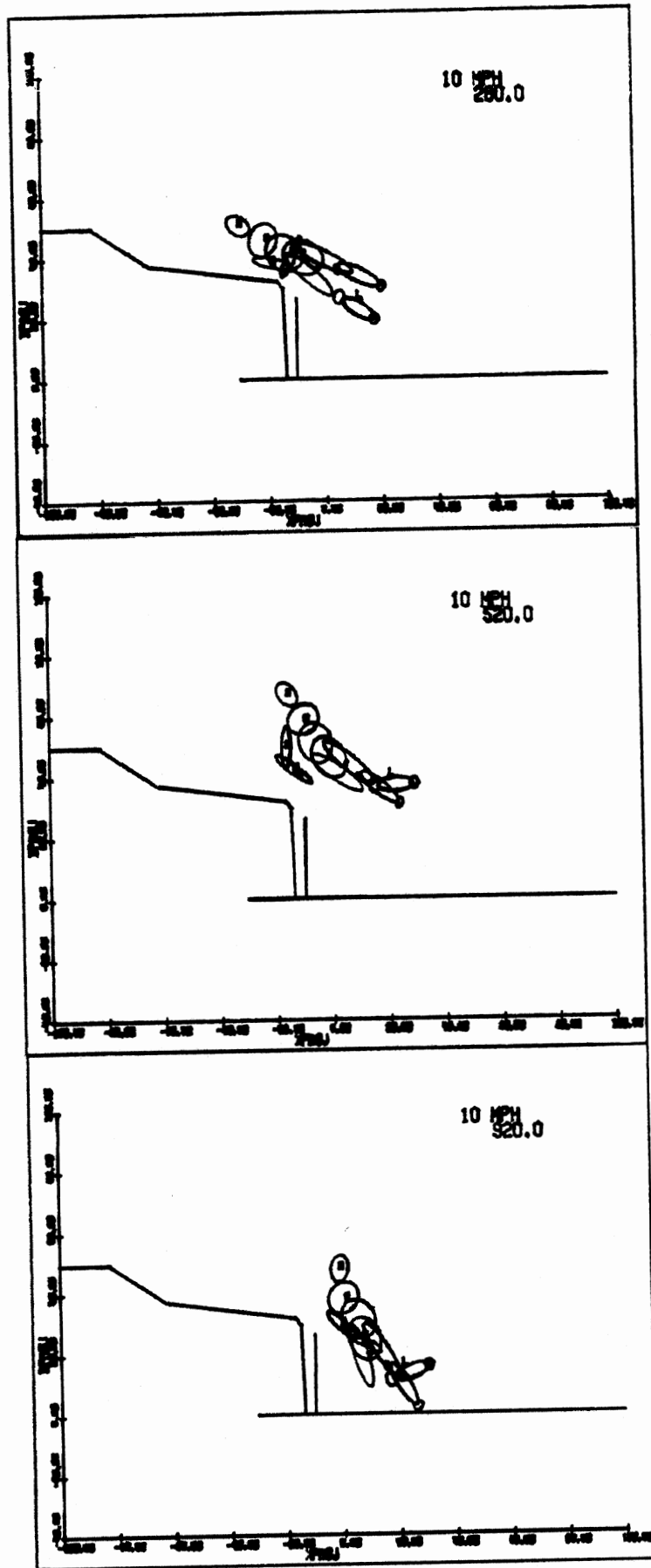


Fig. 16. Pedestrian Kinematics. (3 of 3; 280, 520, 920 ms)

TABLE 8. PEDESTRIAN/VEHICLE CONTACT HISTORY (PAGE 1 of 2)

Ellipse Name	Contact Name	Initial Contact				Peak Contact				Final Contact			
		Time (ms)	Deflection (in)	Force (lb)	Time (ms)	Deflection (in)	Force (lb)	Time (ms)	Deflection (in)	Force (lb)	Time (ms)	Deflection (in)	Force (lb)
Right Foot	Road Surface	0	0.34	160	25	0.52	243	70	0.03	16			
		815	0.28	131	830	1.46	686	835	0.95	446			
Right Knee	Bumperline	35	0.36	360	45	0.86	860	100	0.07	69			
Lower Torso	Hoodline	35	4.63	17	60	5.02	736	220	0.12	11			
Lower Torso	Grille	55	0.02	8	130	1.47	359	230	0.00	1			
Right Lower Arm	Hoodline	45	0.03	13	55	0.24	115	60	0.10	51			
		180	1.11	397	185	1.46	513	190	0.51	181			
	Grille Top	55	0.18	138	55	0.18	138	60	0.18	104			
		115	9.27	117	145	5.49	220	170	0.32	77			
	Grille	200	0.03	7	215	0.92	118	220	0.59	86			
		265	0.21	59	275	1.35	399	280	0.68	205			
		315	0.27	22	315	0.27	22	320	0.41	9			
		560	0.64	6	560	0.64	6	565	0.84	0			
Right Upper Arm	Hoodline	175	0.16	106	180	0.61	392	185	0.13	76			
		200	0.37	276	200	0.37	276	205	0.04	28			
		215	0.09	67	215	0.09	67	220	0.02	13			
		980	6.20	18	990	5.76	356	1000	4.12	294			
Head	Hoodline	190	0.66	662	195	1.80	1801	205	0.55	548			



TABLE 8. PEDESTRIAN/VEHICLE CONTACT HISTORY (PAGE 2 of 2)

Ellipse Name	Contact Name	Initial Contact				Peak Contact				Final Contact	
		Time (ms)	Deflection (in)	Force (lb)	Time (ms)	Deflection (in)	Force (lb)	Time (ms)	Deflection (in)	Force (lb)	
Upper Torso	Hoodline	190	0.22	184	210	1.62	1295	225	0.59	477	
		825	0.42	199	865	3.09	1451	905	0.08	36	
Left Foot	Road Surface	45	0.47	233	65	2.35	600	90	0.66	328	
		165	0.03	15	210	0.35	175	260	0.01	3	
Left Upper Leg	Right Upper Leg	345	0.16	82	355	0.62	310	365	0.03	14	
		495	0.08	39	505	0.15	73	515	0.07	34	
		605	0.02	8	615	0.08	41	625	0.03	16	
		845	0.07	35	875	0.45	226	910	0.03	13	
		970	0.11	57	980	0.80	401	990	0.37	185	

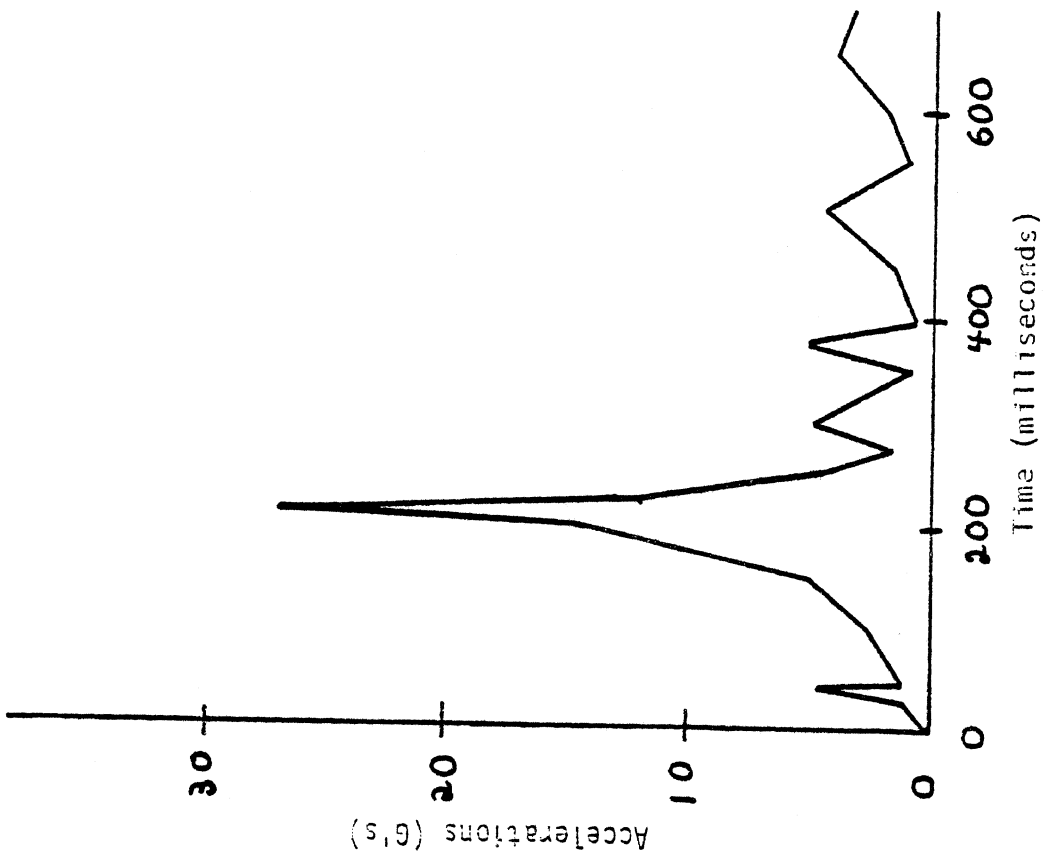


Fig. 17. Upper Torso Accelerations

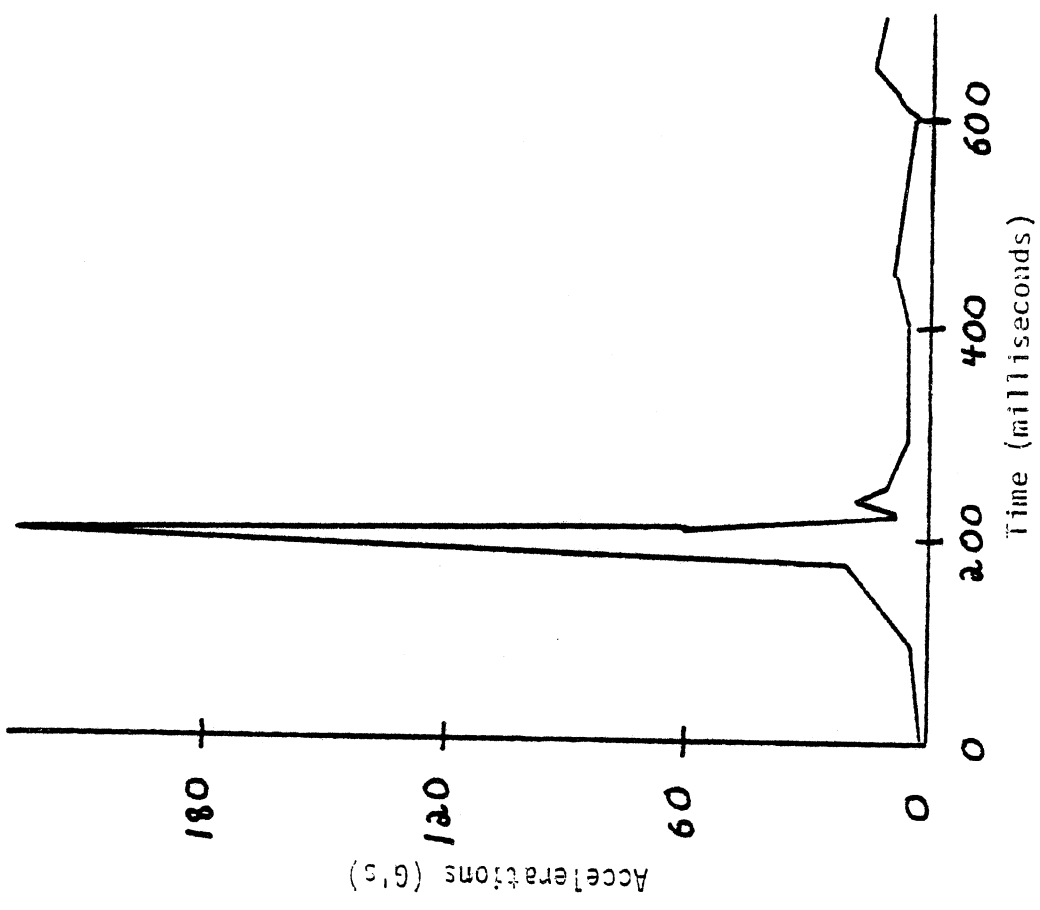


Fig. 18. Head Acceleration

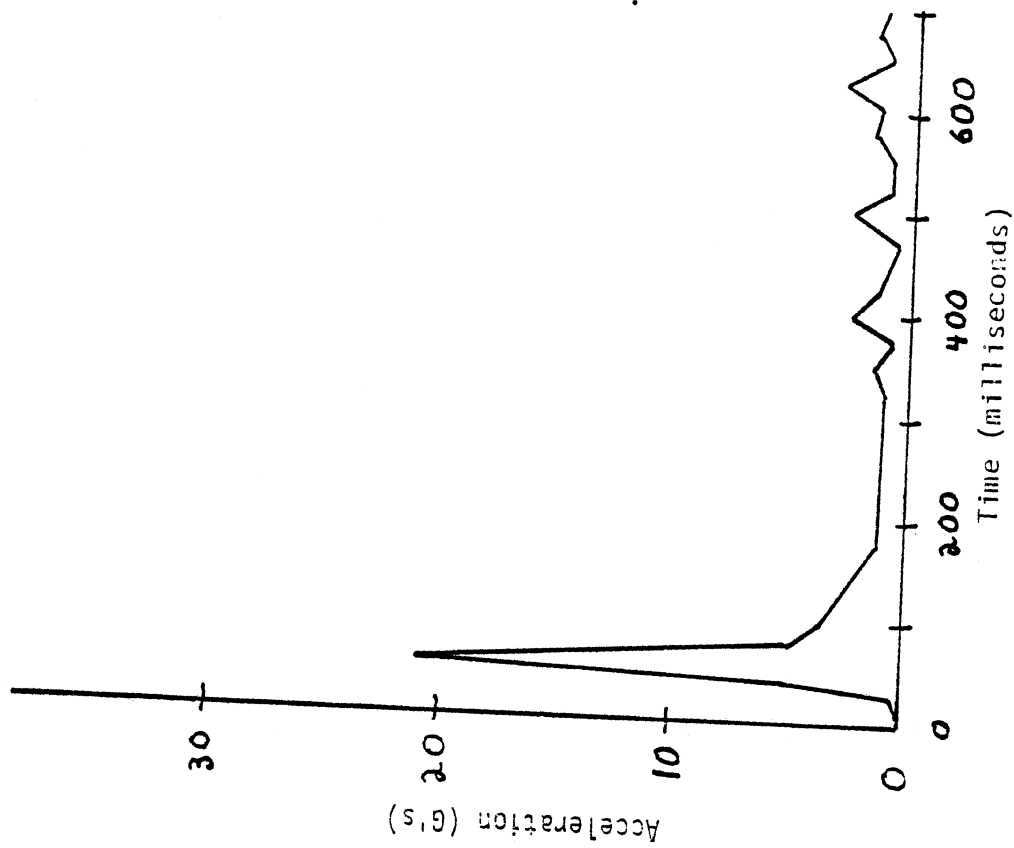


Fig. 19. Hip Accelerations

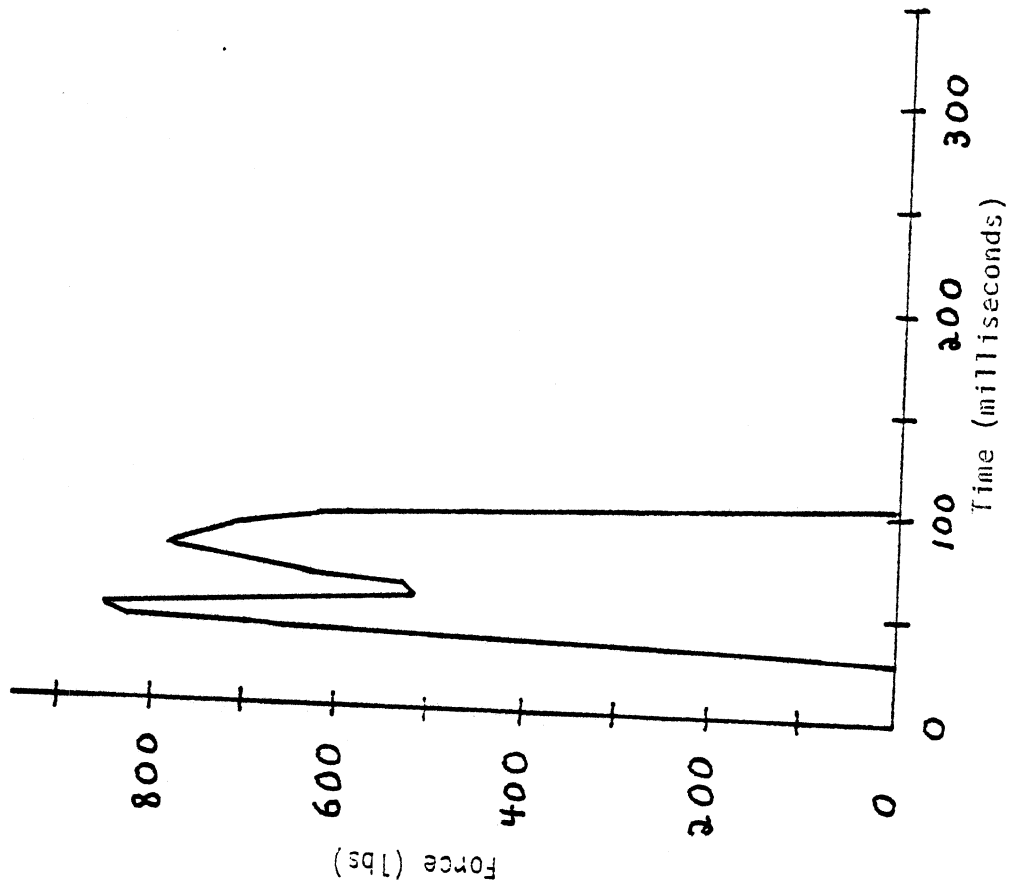


Fig. 20. Contact Force. Knee-bumper.

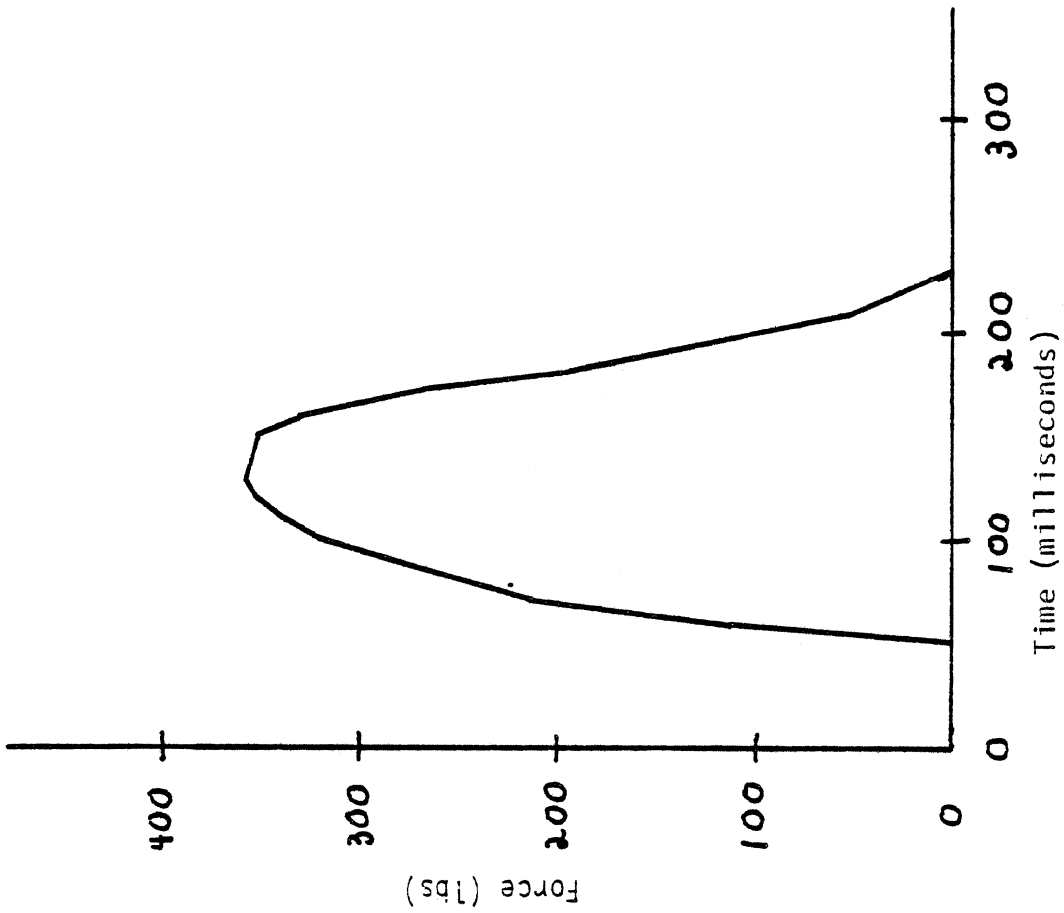


Fig. 21. Contact Force. Lower Torso/Grille.

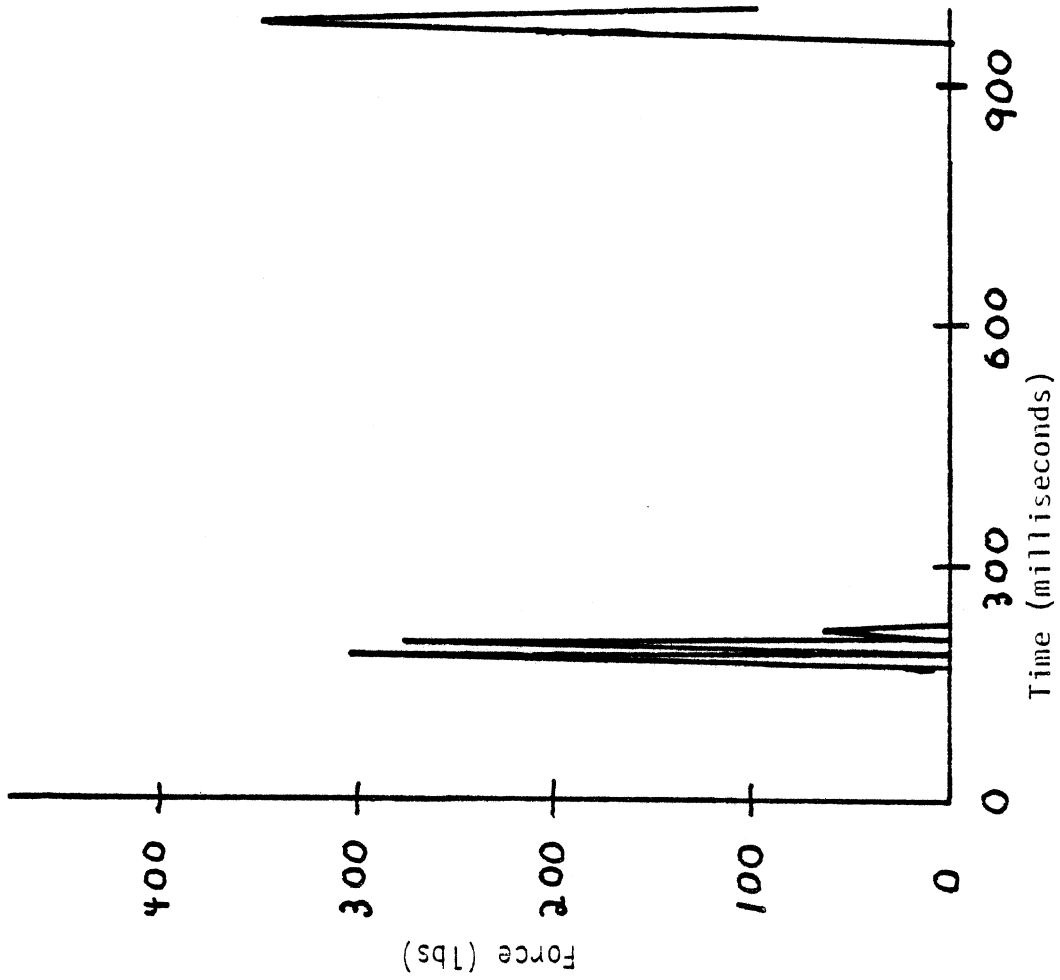


Fig. 22. Contact Force. Right Upper Arm/Hood.

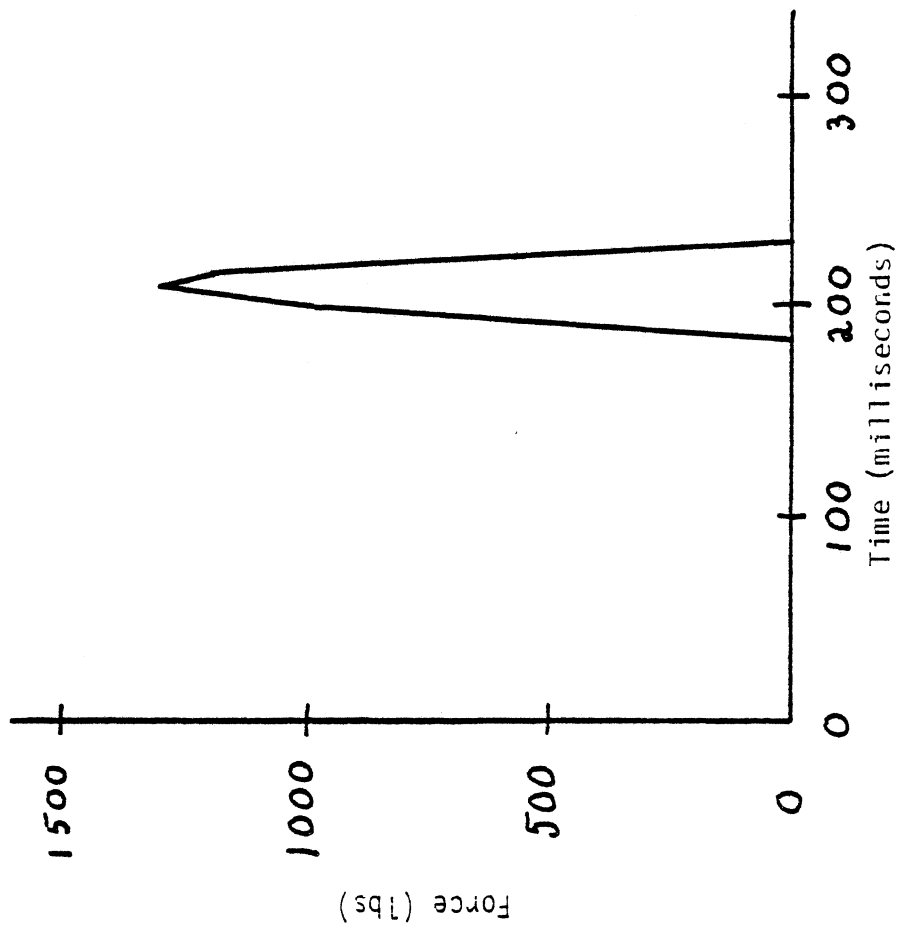


Fig. 23. Contact Force. Upper Torso/Hood.

## 6.0 REFERENCES

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