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ANN ARBOR

PROGRESS REPORT NO. 3

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Project M898

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SUMMARY

I Detonation

The work on detonation during this quarter concentrated largely on obtaining detonation velocities for various fuel-oxygen and fuel-air mixtures. A spark schlieren system with the necessary delay circuit, was designed, fabricated, and used for photographing hydrogen-oxygen detonations.

II Instrumentation

Assembly of interferometer continued.

A focusing schlieren system was set up and tested on optical bench.

PROGRESS REPORT NO. 3

DETTONATION

A spark schlieren system utilizing a pair of achromatic lenses was set up and used to photograph various hydrogen-oxygen detonations. A schematic

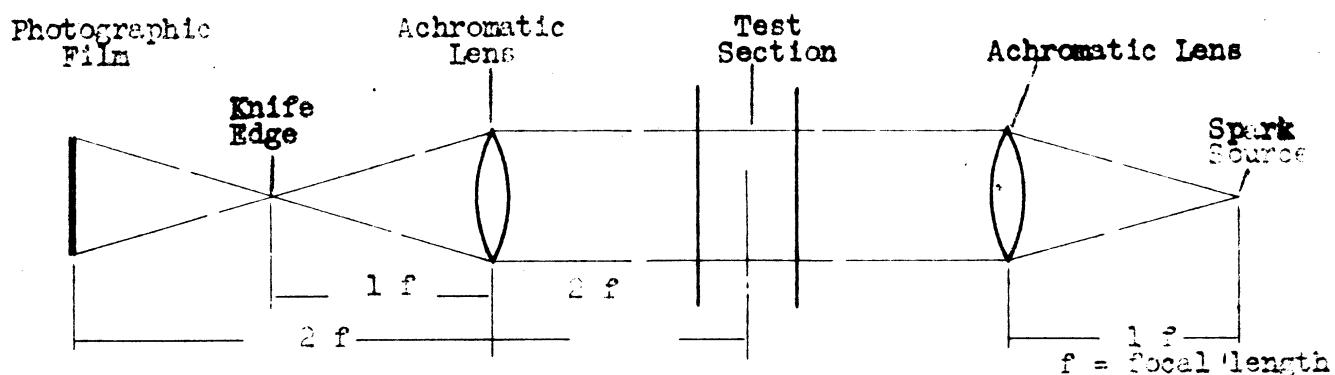
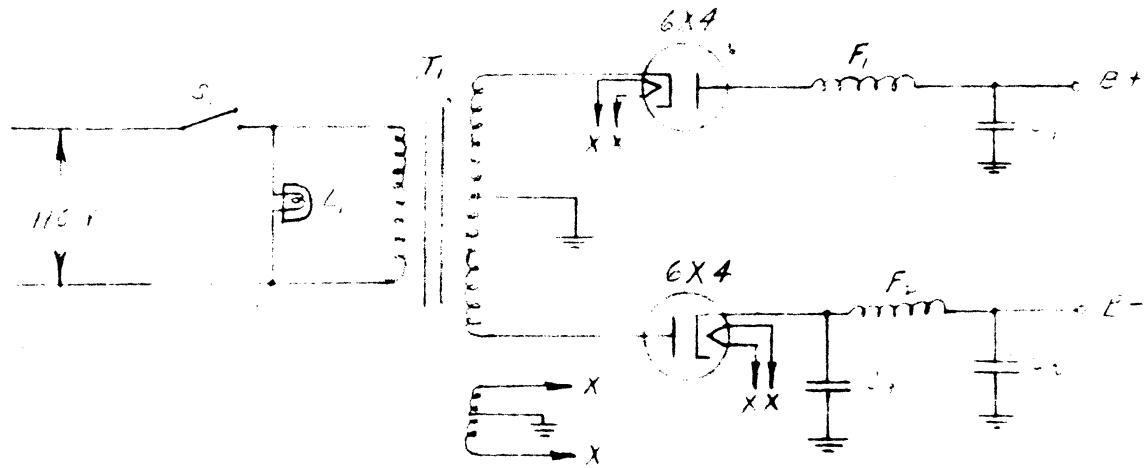


Fig. 1

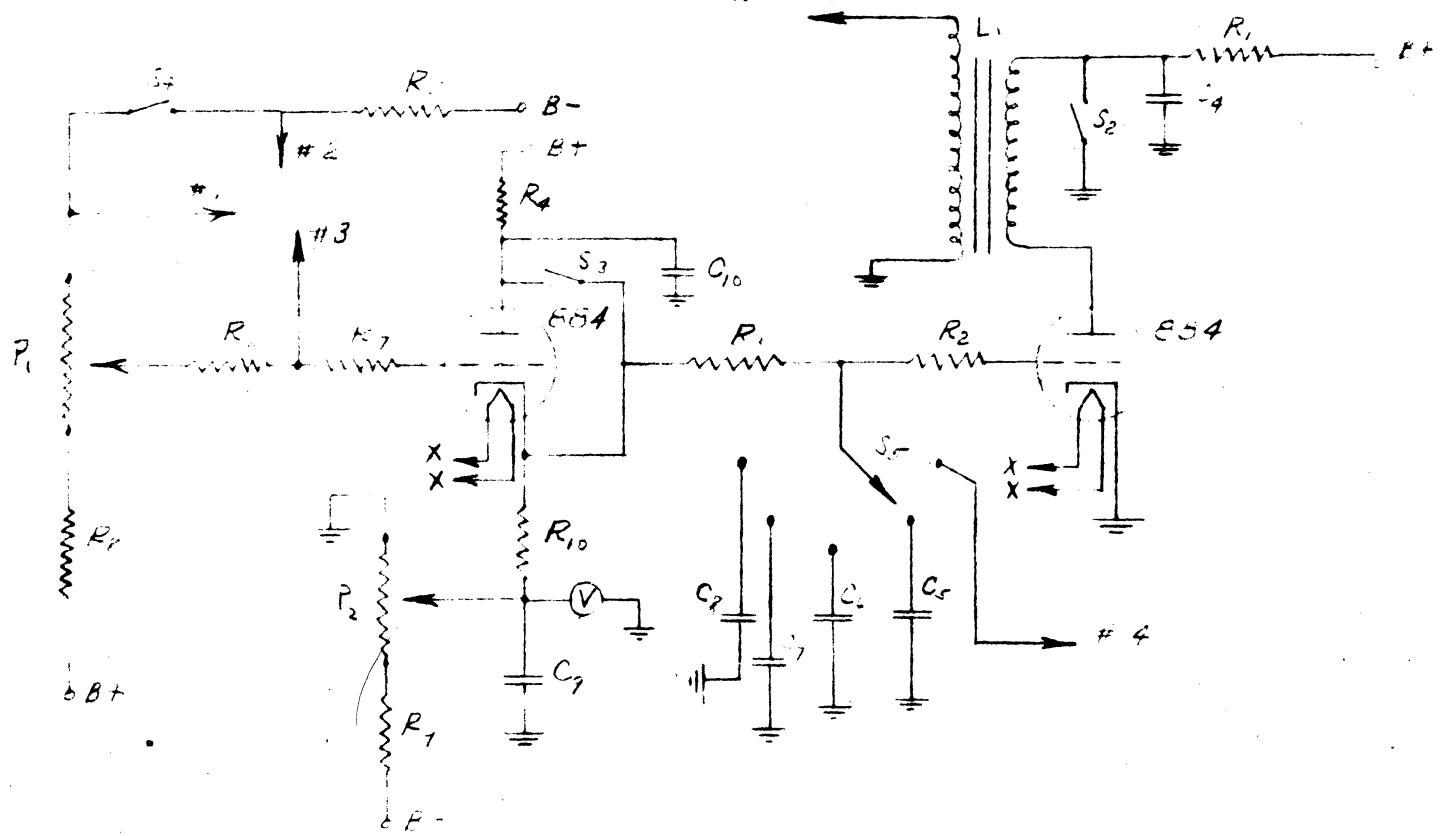
diagram of the experimental set up is shown in Fig. 1.

In order to photograph the detonation wave at various stations in the test chamber, a time delay circuit was designed and fabricated.

TIME DELAY



MAIN SPARK



XX - 6.3 VOLTS

#1, 2, 3, 4 - JACKS

L1 - PILOT LIGHT

 F_1, F_2 - FILTER CHOKE S_1, S_2, S_3, S_4 - SPST SWITCH S_5 - FIVE POSITION SWITCH $C_1 = 20 \mu\text{fd}$ 450 V $C_2 = 20 \mu\text{fd}$ 450 V $C_3 = 1 \mu\text{fd}$ 450 V $C_4 = 1 \mu\text{fd}$ 250 V $C_5 = .0001 \mu\text{fd}$ $C_6 = .01 \mu\text{fd}$ 600 V $C_7 = .01 \mu\text{fd}$ 600 V $C_8 = .1 \mu\text{fd}$ 600 V $C_9 = 20 \mu\text{fd}$ 450 V $C_{10} = 20 \mu\text{fd}$ 450 V

V - VOLTMETER

 L_1 - AUTOMATIC

F500 TUBE

 $R_1 = 23,000 \Omega$ $R_2 = 25,000 \Omega$ $R_3 = 100,000 \Omega$ $R_4 = 390 \Omega$ $R_5 = 25,000 \Omega$ $R_6 = 10,000 \Omega$ $R_7 = 25,000 \Omega$ $R_8 = 25,000 \Omega$ $R_9 = 10,000 \Omega$ $R_{10} = 10,000 \Omega$

E.P. 10 220 V

FIG. 2

The principle of operation of the time-delay circuit is as follows: (See Fig. 2)

1. A pulse is received from the ionization probe (see reference in Progress Report No. 2) on the grid of the first thyratron. (No. 3 Jack)
2. The firing of the first thyratron from the above pulse starts a charge on a condenser (C_5 , C_6 , C_7 , or C_8) through the resistor R_3 .

By means of the potentiometer, P_2 , the voltage on the latter condenser was previously set at some negative bias in excess of that required to hold the second thyratron from firing.

3. When the voltage on condenser C_5 , C_6 , C_7 , or C_8 drops to the critical bias voltage for the second thyratron, the tube fires, sending a pulse through the primary of an automotive-type spark coil.
4. The pulse from the secondary of the spark coil triggers the spark of the main spark gap. (Progress Report No. 1)

S_5 serves as a decade switch for selection of various time intervals. Voltmeter, V , indicates the bias on the second thyratron. S_2 and S_3 are restoring switches for the thyratrons.

Photographs of the shock tube and the experimental setup for the timing and photographing of the detonation waves are shown in Figs. 21, 22, 23, and 24.

INSTRUMENTATION

Besides the spark schlieren apparatus described above, a sharp-focusing schlieren system has been set, and initial studies of such a system have been made. A sharp-focusing schlieren system permits making an image confined to a narrow depth of field of the investigated region and eliminates the integrated effects of density changes over a large region, including wall effects, and effects of regions outside the area of investigation. The narrow depth of field is accomplished by

1. large size of light source
2. multiple light sources
3. corresponding multiple knife-edges

The diagram of the system is shown below:

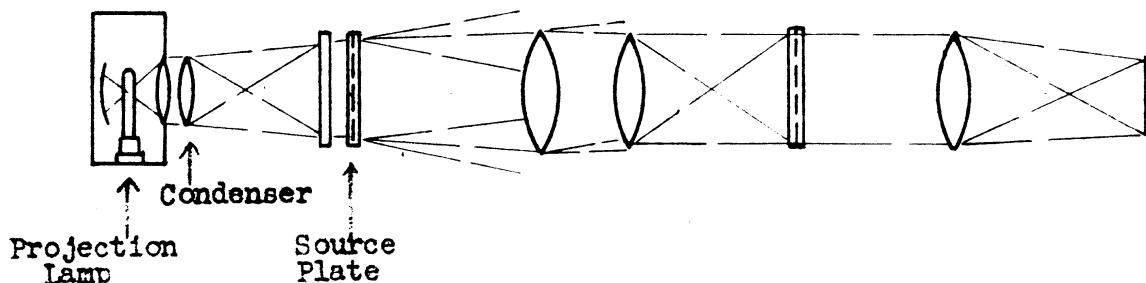


Fig. 3

This system will be used for photographing combustion phenomena, and should help in isolating undesired disturbances.

The equipment is on loan, and work with it has been described in Report No. WTM-186, "A Study of Sharp Focus Schlieren Systems," by E. Turner.

The interferometer assembly is continuing, although at a rather slow pace due to priority requirements on manpower. The instrument is totally assembled, except for the control system and photographic setup. The main interferometer plates were sent back to the manufacturer for final surface coating. A proposal for utilizing the interferometer in flame studies has been completed and submitted.

EXPERIMENTAL RESULTS

The same experimental equipment and methods as were reported in Progress Reports No. 1 and No. 2 were used to obtain detonation velocities for various fuel-oxygen and fuel-air mixtures. These velocities for oxygen mixtures of methane, ethane, propane, butane, and hexane are plotted in Figs. 4, 5, 6, 7, and 8, respectively. It is interesting to note that these graphs of detonation velocities for this hydrocarbon series tend to normalize when plotted vs. actual fuel-oxygen mixture ratio divided by the fuel-oxygen mixture ratio at stoichiometric conditions (see Figs. 9 and 10). Graphs of detonation velocities for hydrogen-oxygen, hydrogen-air, and ether-oxygen mixtures appear in Figs. 11, 12, and 13. Detonation velocities for acetylene-oxygen mixtures are shown in Fig. 14. Figs. 15 and 16 illustrate the effect of ambient pressure on acetylene-oxygen detonation velocities.

Detonation velocities as a function of distance in a 21-ft shock tube are shown in Fig. 17. A 51 per cent mixture of hydrogen and oxygen was used in these tests. The dispersion in data can be attributed to photo-cell probes that were used for these runs. The response times for these cells were unequal and could not be readily reproduced. To eliminate the unequal response times the probes were reversed after each run and the run duplicated. An average of the times in the two runs was used. It is apparent that within the accuracy of these experiments the detonation velocity remains substantially unchanged as a function of distance.

A series of spark schlieren detonation photographs for hydrogen-oxygen mixtures are shown in Figs. 18, 19, and 20. At approximately 40 per cent mixtures (by volume) of hydrogen and oxygen the clean detonation front normally encountered is changed into an interacting and ~~more~~ ^{more} homogeneous region of shocks and combustion. From the small amount of evidence that the photographs give it is felt that the combustion behind the shocks of these lean detonations is quite unstable, continually lagging, and catching up to the shock. By the same reasoning the shocks would also be unstable. Further investigation of this phenomenon is being made.

Fig. 18 shows a sequence of spark schlieren photographs for a detonation wave of hydrogen and oxygen as the wave approaches and breaks over a wedge inserted in the test section of the shock tube.

Fig. 19 is included to show the intermingling and nonhomogeneity of the shock and combustion areas for lean hydrogen-oxygen mixtures. It is evident from these photographs that the combustion zones can lag the shock fronts by an appreciable distance.

Fig. 20 illustrates the effect of knife-edge orientation in the schlieren photographs of detonation waves. The light area in the upper photograph of this series indicates that a strong, adverse density gradient is present after the front.

For a matter of reference the top-to-bottom dimensions of all these photographs is 1/2 inch. The waves in all cases are moving from left to right.

DETROITATION VELOCITY OF A METHANE - OXYGEN MIXTURE
VERSUS MIXTURE RATIO

VELOCITY IN FEET PER SECOND $\times 10^{-3}$

0 1 2 3 4 5 6 7 8 9 10

STOICHIOMETRIC

0 10 14 16 22 26 30 34 38

PER CENT FUEL BY VOLUME

3-2-b1

Mixture Ratio (Per Cent Fuel by Volume)	Velocity ($\times 10^3$ ft/sec)
10	10
12	18
14	28
16	25
18	22
20	25
22	38
24	35
26	32
28	28
30	25
32	22
34	18
36	15
38	12

DETONATION VELOCITY OF AN ETIENE - OXYGEN MIXTURE
VERSUS MIXTURE RATIO

VELOCITY IN FEET PER SECOND X 10

Atmospheric

0 4 8 12 16 20 24 28 32 36

PER CENT FUEL BY VOLUME

Fig. 3
3-2-51

FUEL - PER CENT BY VOLUME

FIG. 6

DETONATION VELOCITY OF A PROPANE - OXYGEN MIXTURE
VERSUS MIXTURE RATIO

STOICHIOMETRIC

VELOCITy IN FEET PER SECOND X 10^{-3}

2 - 24 - 51

DETTONATION VELOCITY OF A BUTANE - OXYGEN MIXTURE
VERSUS MIXTURE RATIO

VELOCITY IN FEET PER SECOND $\times 10^{-3}$

9 8 7 6 5 4 3 2 1 0

FUEL - PER CENT BY VOLUME
30 25 20 15 10 5 0

STOICHIOMETRIC

9

8

7

6

5

4

3

2

1

0

9

8

7

6

5

4

3

2

1

0

9

8

7

6

5

4

3

2

1

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9

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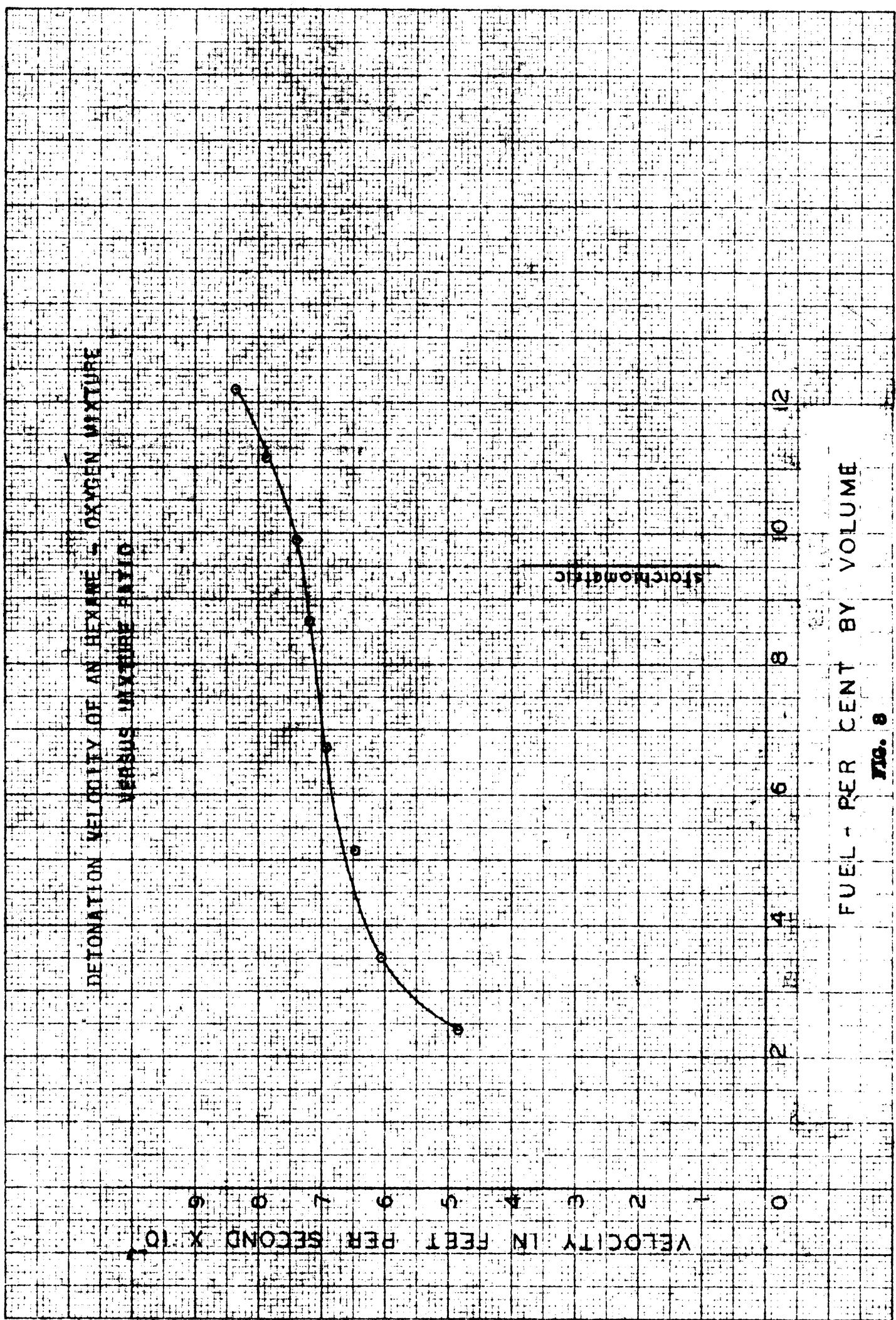
4

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2

1

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DETONATION VELOCITY OF HYDROCARBON BASES
VERSUS MIXTURE RATIO

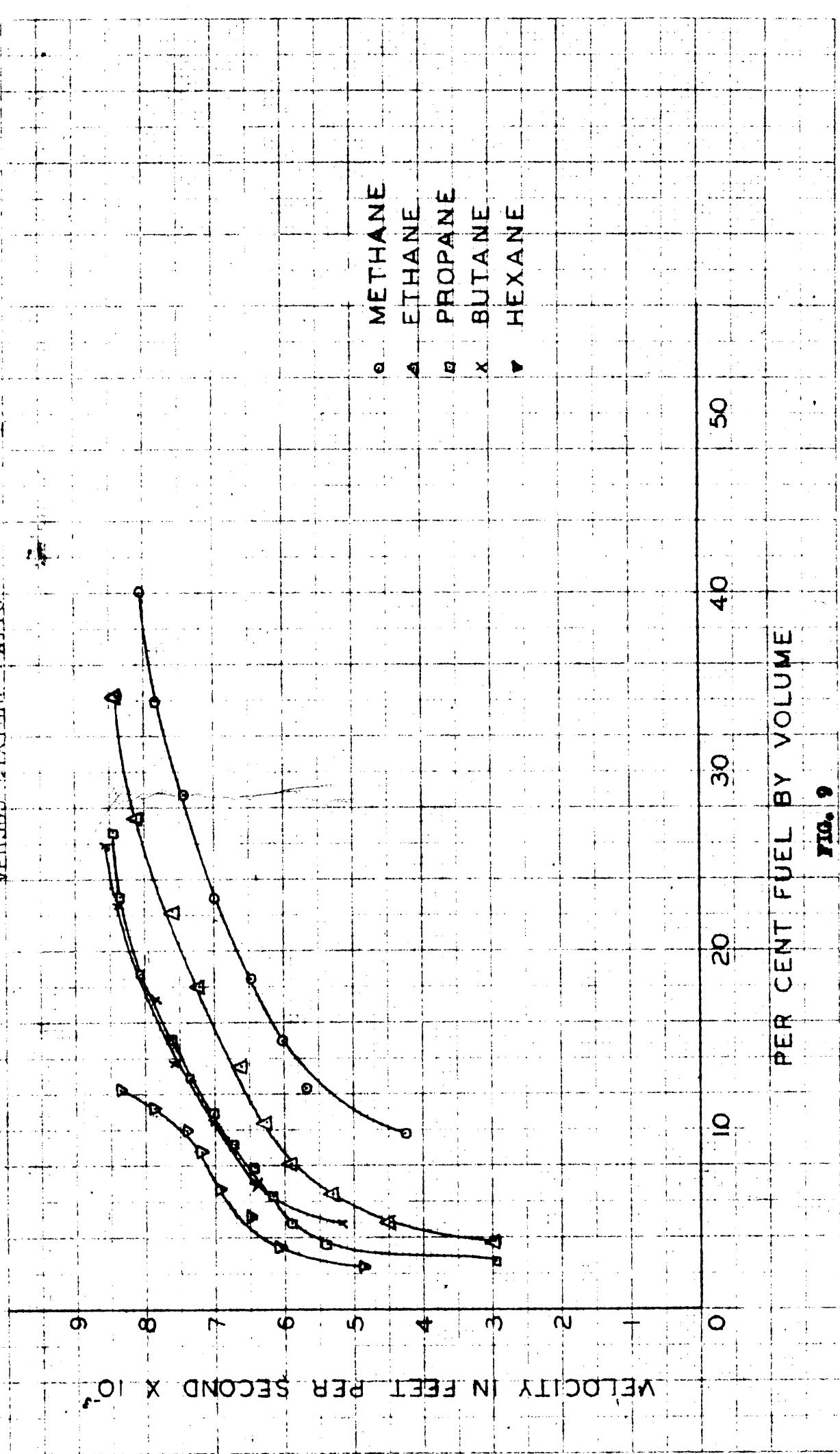


FIG. 9

DETTONATION VELOCITY OF HYDROCARBON GASES
VERSUS NORMALIZED MIXTURE RATIO

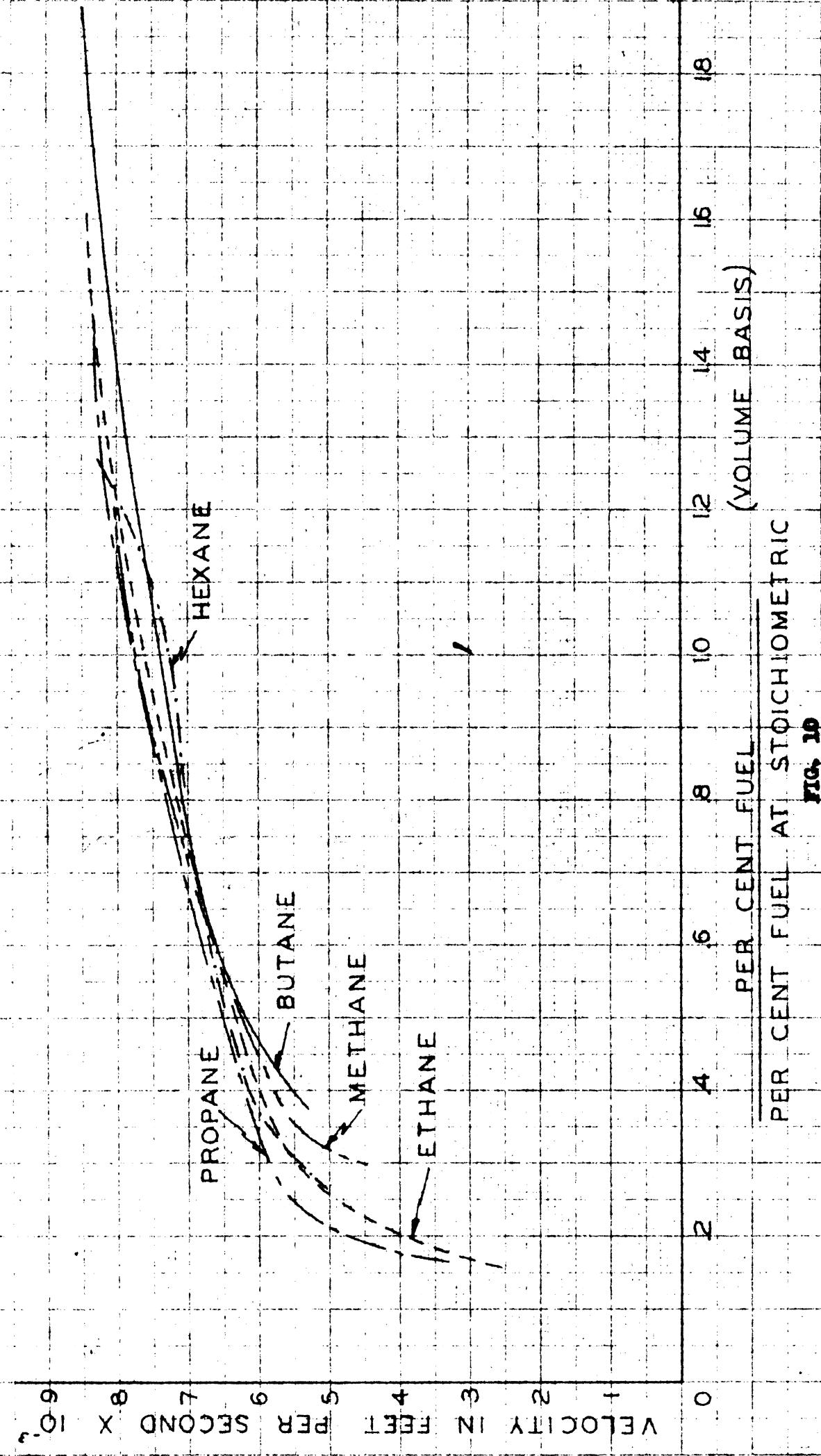


FIG. 19

PER CENT FUEL AT STOICHIOMETRIC

(VOLUME BASIS)

DETONATION VELOCITY OF AN HYDROGEN - OXYGEN MIXTURE
VERSUS MIXTURE RATIO

VELOCITY IN FEET PER SECOND $\times 10^{-3}$

10

20

30

40

50

60

70

80

90

100

110

120

130

140

150

160

170

180

190

200

210

220

230

240

250

260

270

280

290

300

310

320

330

340

350

360

370

380

390

400

410

420

430

440

450

460

470

480

490

500

510

520

530

540

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570

580

590

600

610

620

630

640

650

660

670

680

690

700

710

720

730

740

750

760

770

780

790

800

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830

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850

860

870

880

890

900

910

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940

950

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970

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990

1000

1010

1020

1030

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1070

1080

1090

1100

1110

1120

1130

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1190

1200

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3140

3150

3160

3170

3180

3190

3200

3210

3220

3230

3240

3250

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3270

3280

3290

3300

3310

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3330

3340

3350

3360

3370

DETTONATION VELOCITY OF AN HYDROGEN - AIR MIXTURE
VERSUS MIXTURE RATIO

VELOCITY IN FEET PER SECOND X 10³

8 7 6 5 4 3 2 1 0

STOICHIOMETRIC

PER CENT FUEL BY VOLUME

40 35 30 25 20

18



FUEL - PER CENT BY VOLUME
No. 13

10 20 30 40

10

10

10

10

10

10

10

10

10

10

10

10

10

10

WATER VAPOR CONCENTRATION IN PERCENTAGE OF AN ETHER-OXYGEN MIXTURE

VELOCITY IN FEET PER SECOND X 10⁻³

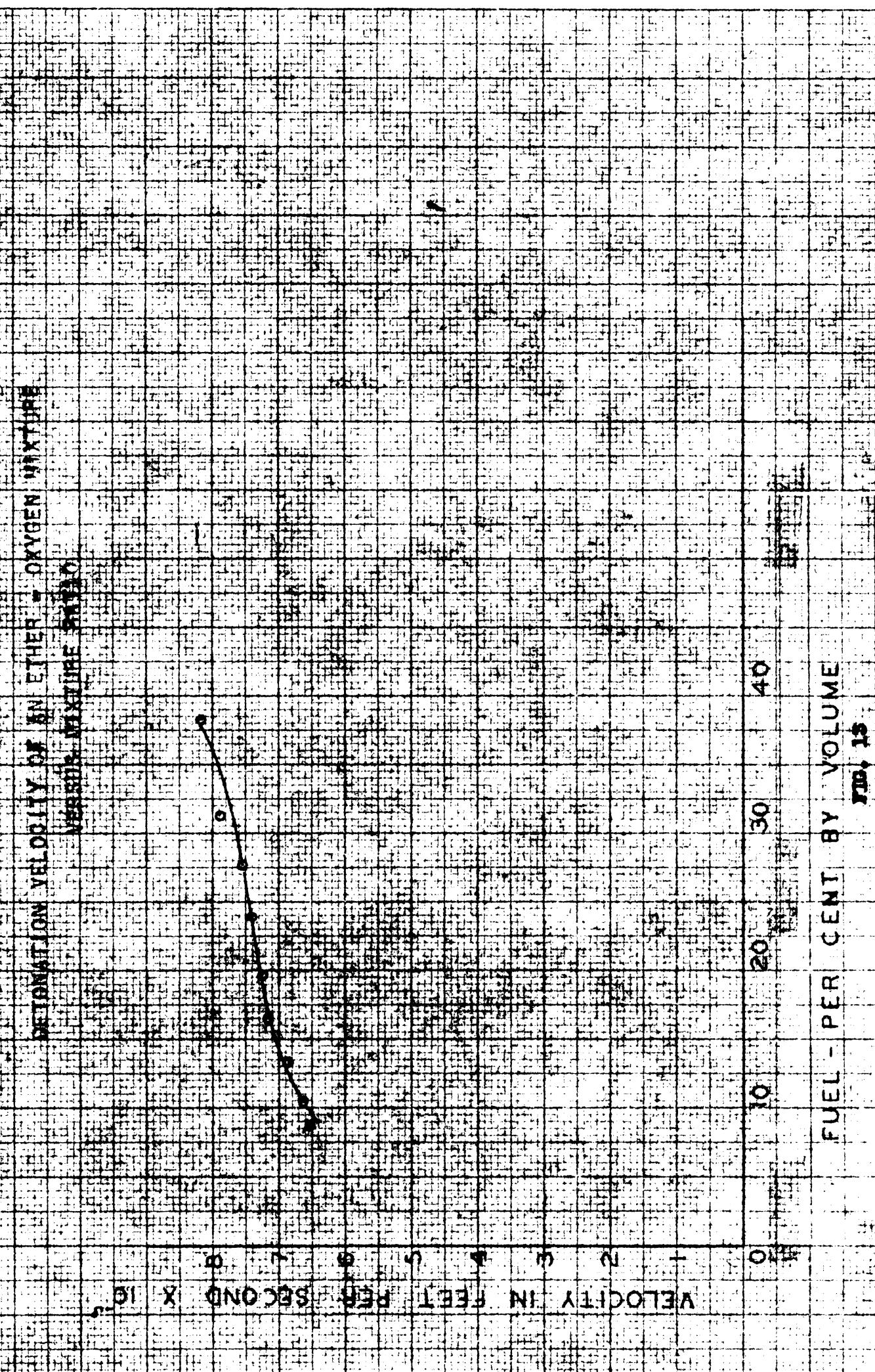
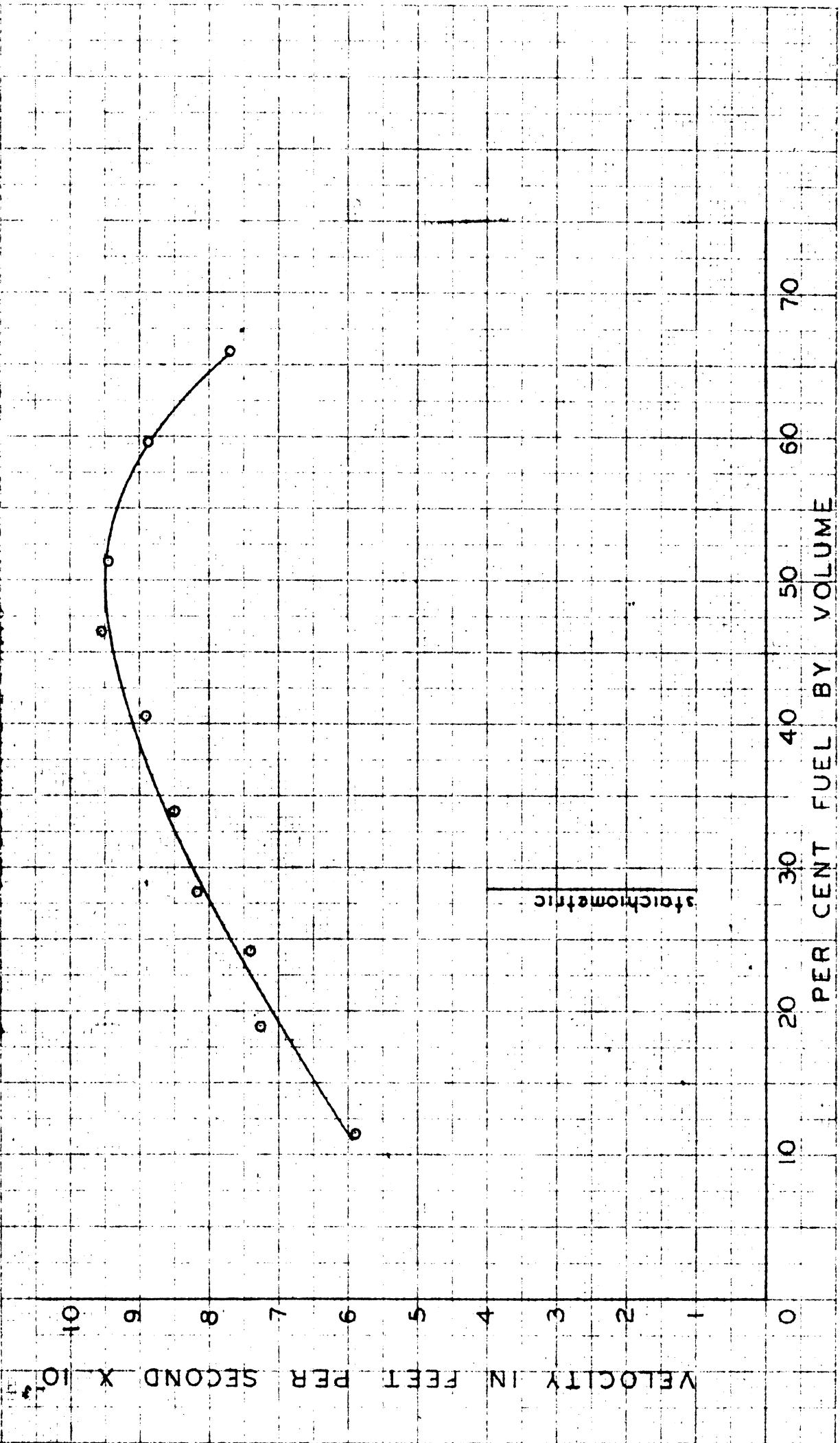


FIG. 14

DETONATION VELOCITY OF AN ACETYLENE - OXYGEN MIXTURE
VERSUS MIXTURE RATIO



DETONATION VELOCITY OF VARIOUS ACETYLENE - OXYGEN MIXTURES
AT REDUCED PRESSURES

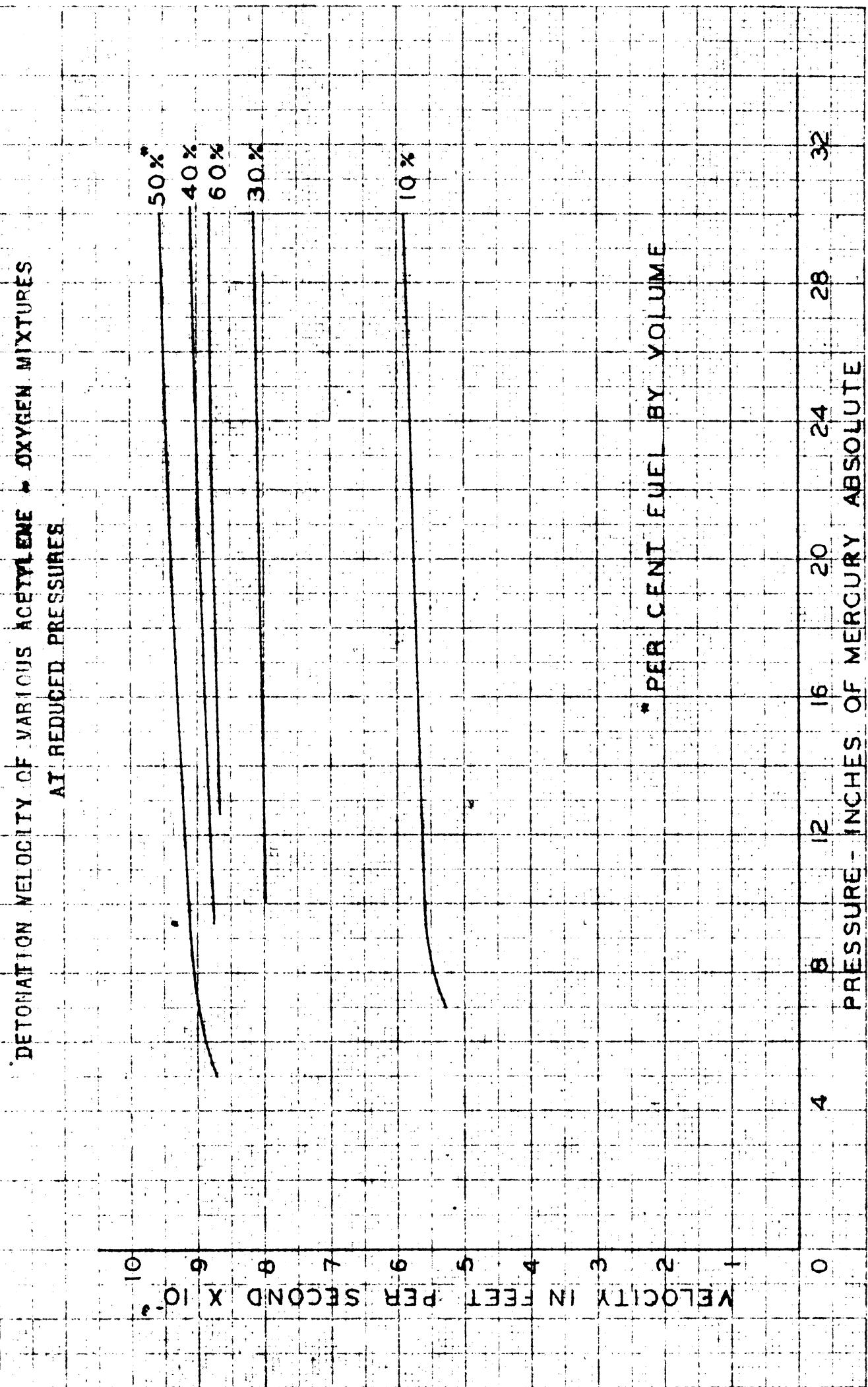
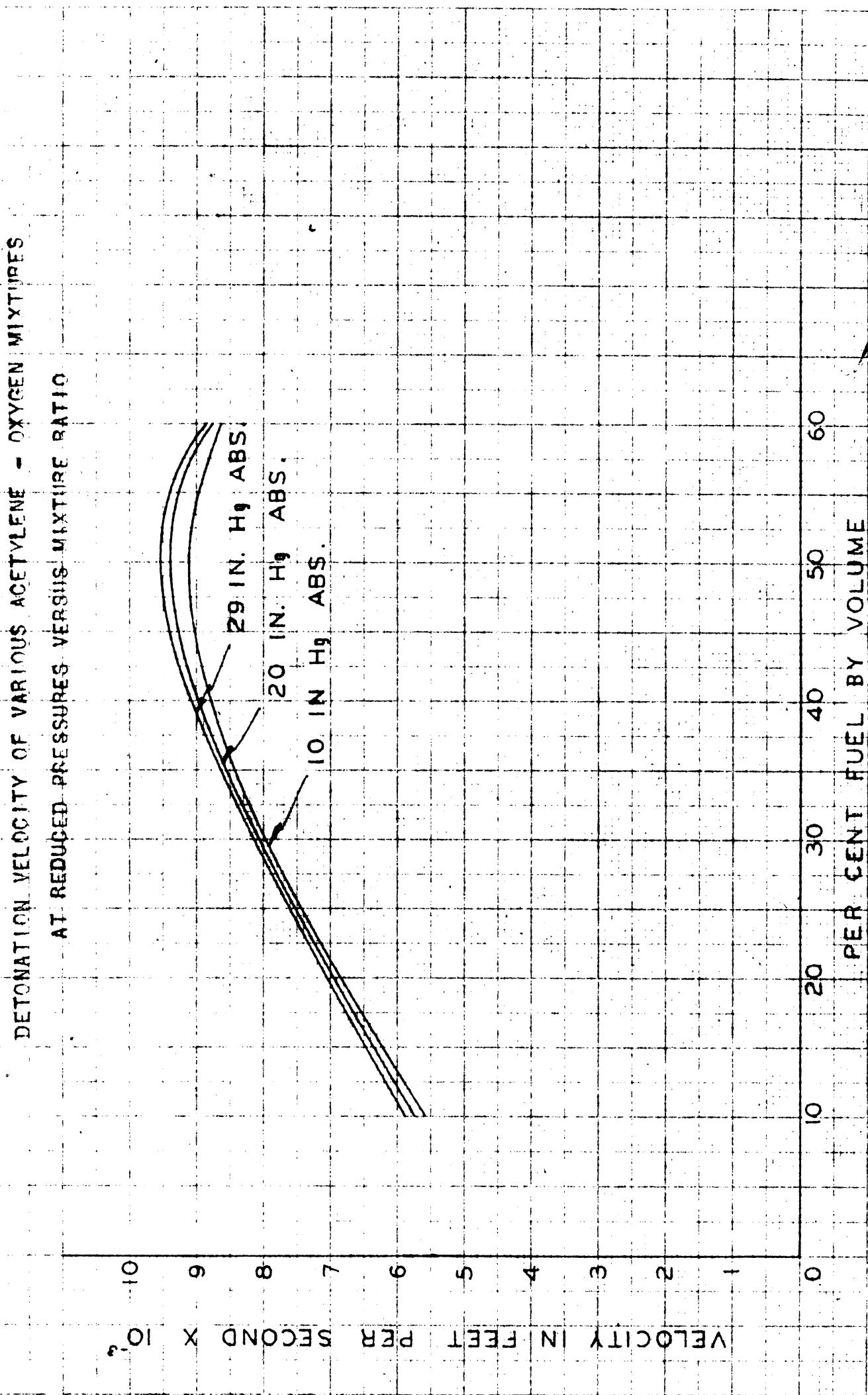


FIG. 15

DETONATION VELOCITY OF VARIOUS ACETYLENE - OXYGEN MIXTURES
AT REDUCED PRESSURES VERSUS MIXTURE RATIO



DETONATION VELOCITY OF A 51.3% HYDROGEN - OXYGEN MIXTURE
VERSUS DISTANCE FROM DIAPHRAGM

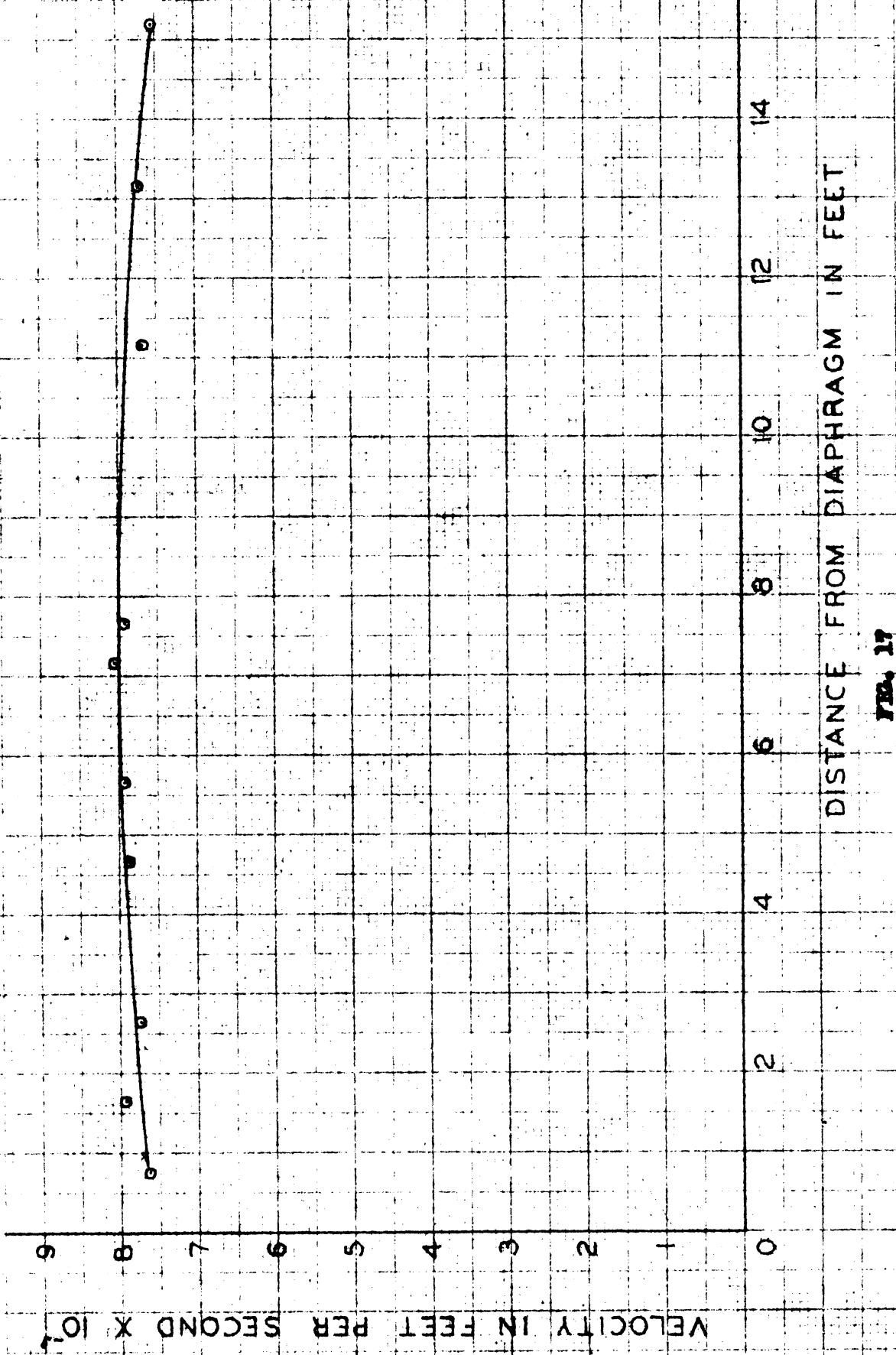


Fig. 17

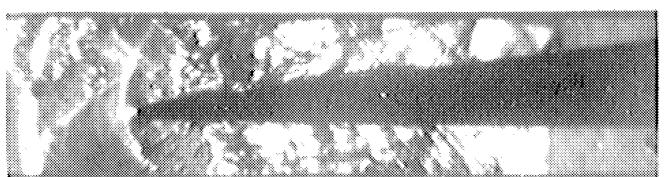
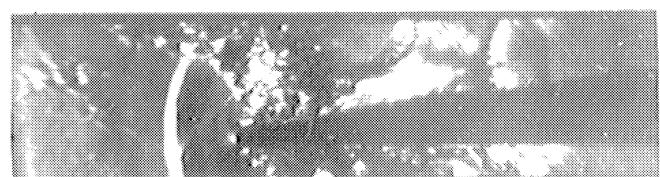
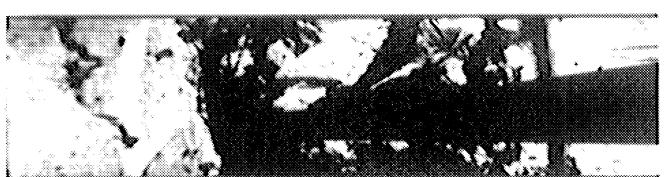
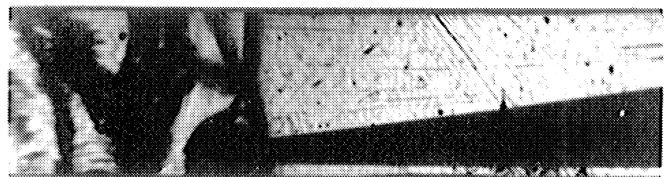
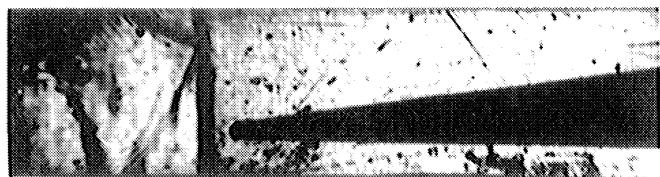
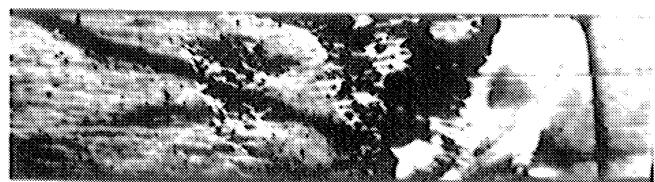
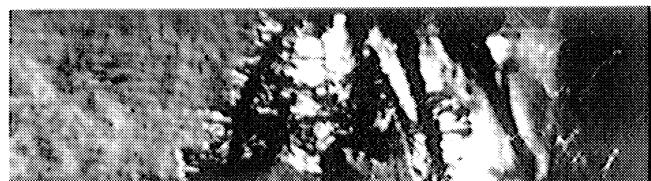
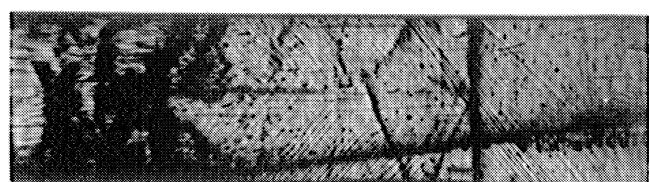


FIG. 18 - 25 % H₂O₂ DETONATION WAVE - SPARK SCHLIEREN



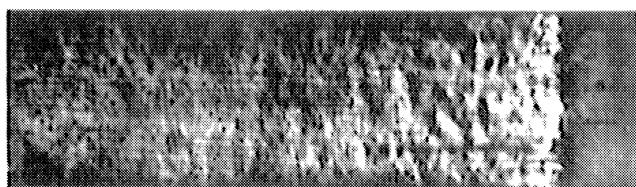
HORIZONTAL KNIFE EDGE



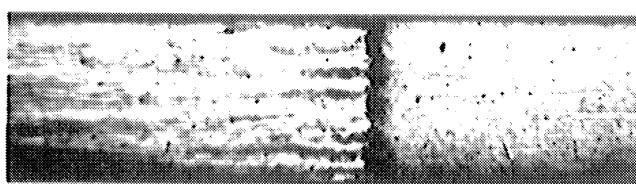
VERTICAL KNIFE EDGE

FIG. 19 - SPARK SCHLIEREN PHOTOGRAPHS

25 % H₂-O₂ DETONATIONS



41 % $\text{H}_2\text{-O}_2$
VERTICAL KNIFE EDGE



50 % $\text{H}_2\text{-O}_2$
HORIZONTAL KNIFE EDGE

FIG. 20 - SCHLIEREN PHOTOGRAPH OF A
DETONATION WAVE

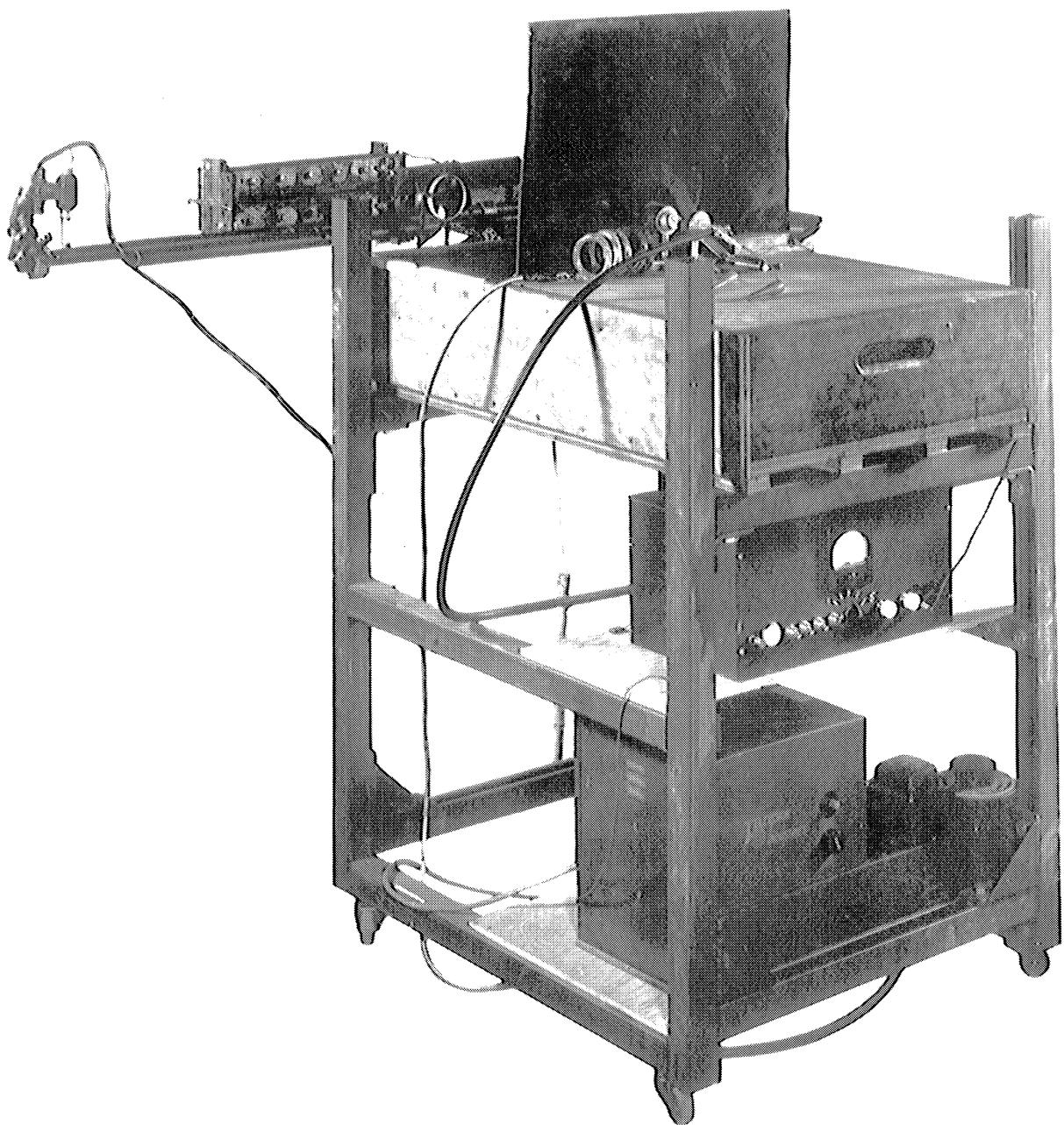


FIG. 21 -- HIGH VOLTAGE SPARK GAP WITH TIME DELAY

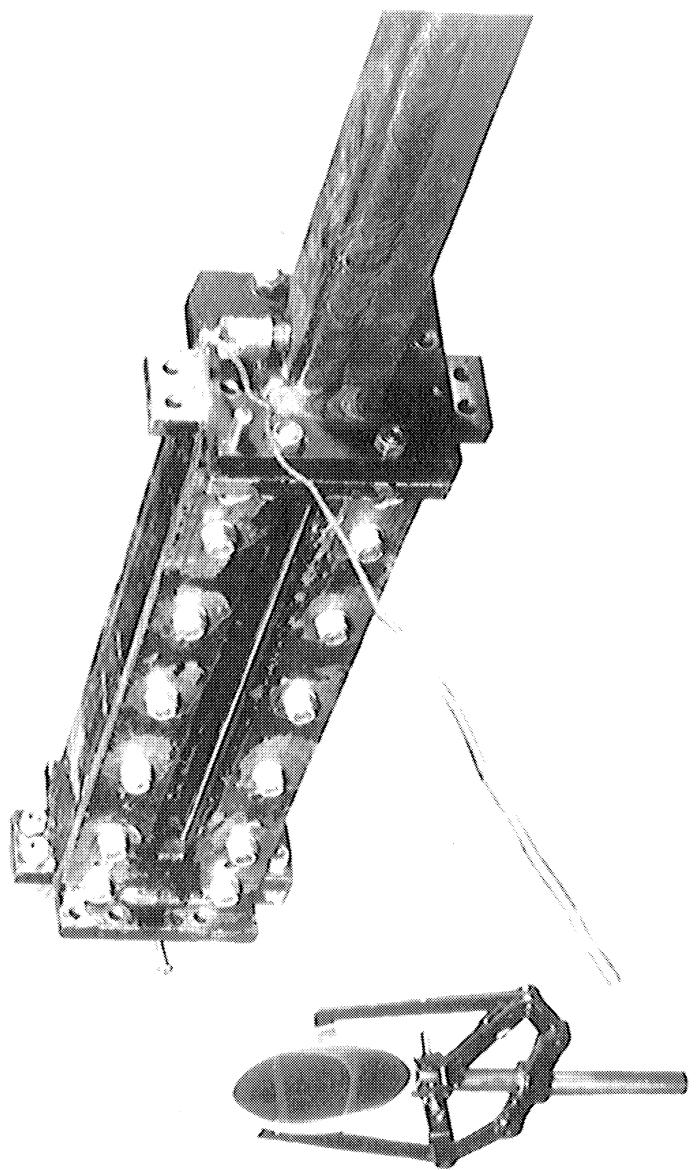
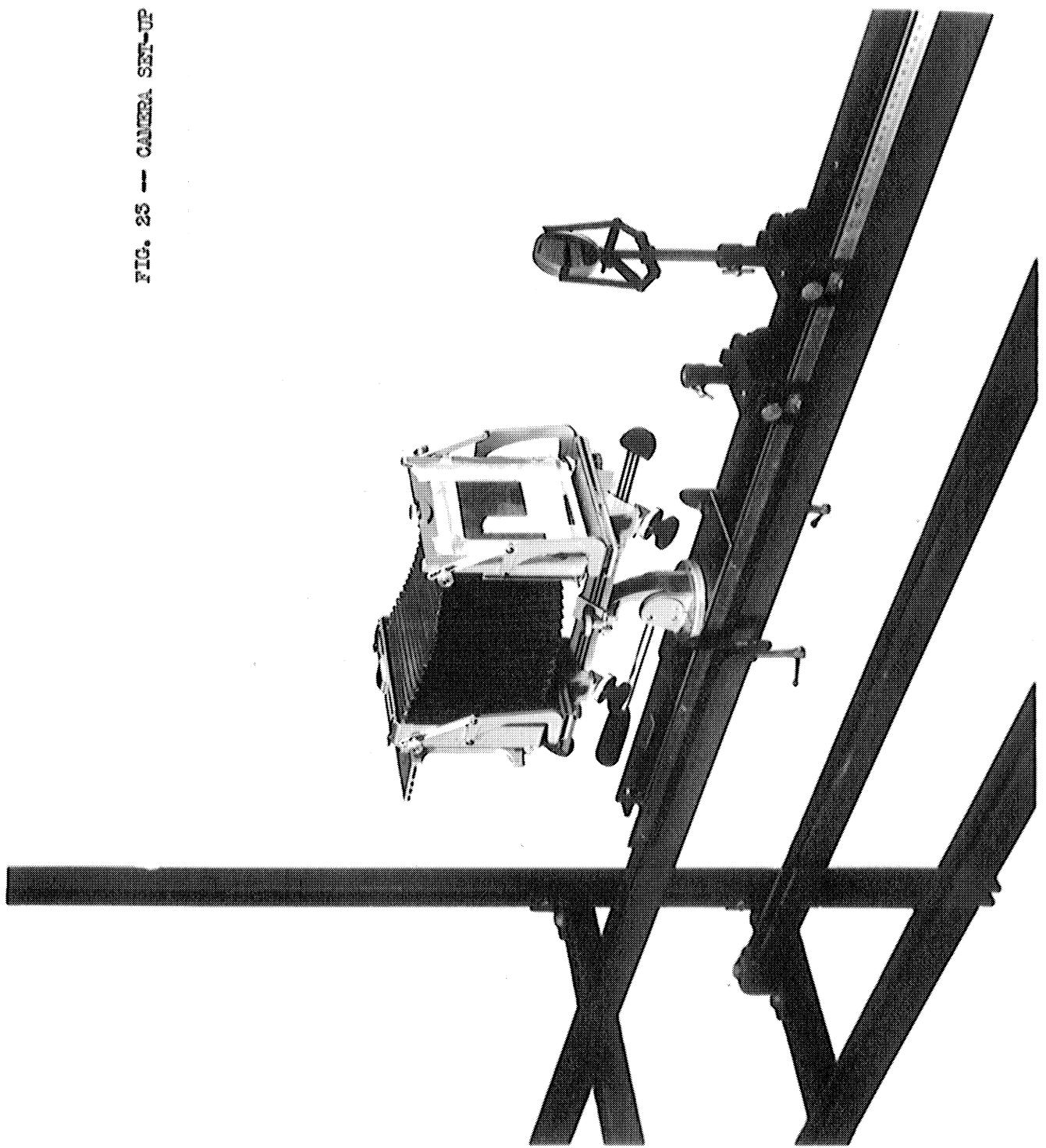


FIG. 28 - - TURST SECTION AND CUTTING PLATE

FIG. 25 — CAMERA SET-UP



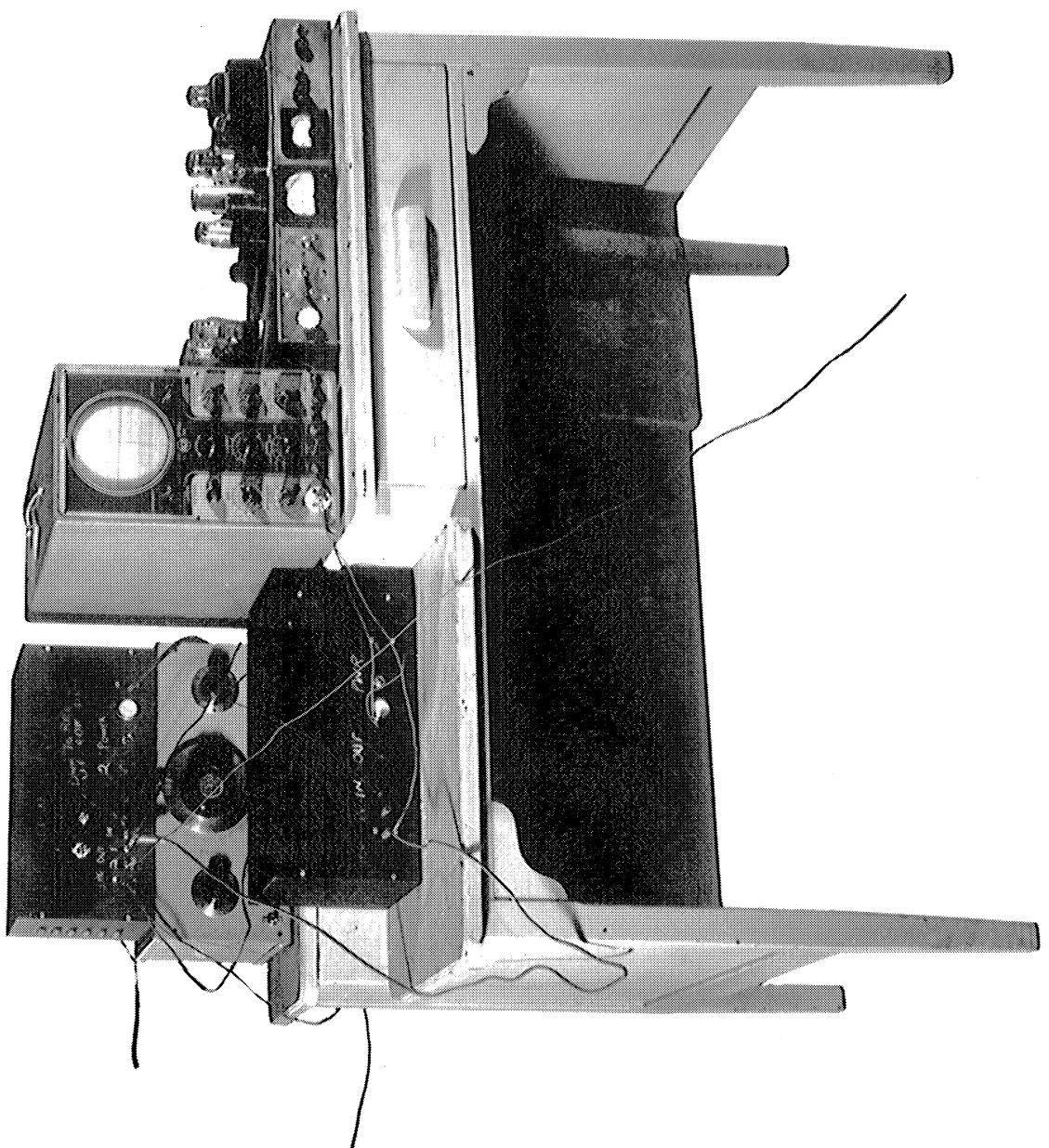


FIG. 24 — TUNING CIRCUIT (on right) WITH ASSOCIATED CALIBRATION EQUIPMENT