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RADIAL-PLY CARCASS SHAPES UNDER INFLATION

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NOMENCLATURE

English Letters

- a, A - half rim-width
- b, B - rim radius
- C - constant of integration
- E, F - elliptic integrals of first and second kind
- E_θ, E_ϕ - elastic moduli in the circumferential and meridional directions, respectively
- H - tire section height
- I, J - definite integrals used in the analysis
- K - modulus of an elliptic integral
- L - arc length of tire meridian section
- N_θ, N_ϕ - stress resultant, or force per unit length, in circumferential and meridional direction respectively
- p - inflation pressure
- r - radial dimension to a point on the tire from the axis of revolution
- r_1 - radius of curvature of the cross section in its own plane
- t - variable of integration
- w - tire section width
- x, y - cartesian co-ordinate

Greek Letters

- α - variable of integration
- ψ - variable of integration

NOMENCLATURE (CONCLUDED)

λ - constant

ϕ - angle of meridian as measured from a tangent

ϕ_0 - rim tangent angle measured from horizontal line

Φ - amplitude of elliptic integral

ρ - $\phi + \pi/2$

γ - $b^2/2\lambda + \cos \phi_0$

I. INTRODUCTION

In the process of manufacturing a tire it is desirable to know the shape which the inflated tire carcass will take in order to be able to determine

- (1) the overall dimensions such as the maximum height and width, as well as the volume of material required
- (2) the shape of the lower surface of the tread, in order to minimize residual stresses created during the process of bonding the tread to the carcass.

The shape of the radial-ply carcass, because of its special construction, is particularly amenable to solution. This report deals with the calculation of the equilibrium shape of the carcass of a radial-ply tire subjected to internal pressure.

II. SUMMARY

The equilibrium equations giving the shape of a toroidal tire carcass under internal pressure were solved, using the particular assumption that the circumferential elastic modulus (E_θ) is negligible with respect to the radial elastic modulus (E_ϕ). This corresponds physically to a case in which tire cords run in a purely radial fashion, from rim to rim, similar to those in the basic carcass plies of some radial tires. A computer program was written to calculate the coordinates of the inflated tire cross section as a function of the ratio of rim-width to rim-diameter and also as a function of the maximum tire height. Results are presented in both tabular and graphical forms.

III. DISCUSSION OF ANALYSIS, COMPUTER PROGRAM, AND RESULTS

A detailed analysis of the shape of the inflated carcass of a radial-ply tire is presented in Appendix A. The assumptions, resulting equations, and the computer program which is needed to compute the coordinates of the tire cross section are reviewed below. The geometry of the inflated shape and the definition of terms used in the analysis are given in Figure 1.

The basic assumption made in the analysis is that the stiffness of the radial reinforcement is so much greater than the circumferential stiffness that the stress resultants developed in the circumferential direction are negligible, i.e. $N_\theta \approx 0$. Hence, only stress resultants N_ϕ along the meridional direction can be developed. This leads directly to the result that

$$rr_1 = \lambda \quad (5)*$$

in which r is the radial distance from the axis of revolution, r_1 is the local radius of curvature in the plane of the cross section, and λ is an undetermined constant. Then, introduction of the boundary conditions results in the following three equations

$$\sqrt{\lambda/a} (2E - F) - 1 = 0 \quad (30)$$

$$K^2 = \frac{(b/a)^2}{4(\sqrt{\lambda/a})^2} + \cos^2 \frac{\Phi_0}{2} \quad (31)$$

$$K \cos \frac{\Phi_0}{2} = \frac{(b/a)}{2(\sqrt{\lambda/a})} \quad (32)$$

which must be satisfied simultaneously, where b/a is the given ratio of rim-width to rim-diameter, and Φ_0 is the given angle that the tangent to the carcass at the rim makes with the horizontal (axis of revolution). K and Φ_0 are the modulus and amplitude respectively, of the elliptic integrals of the first and second kind, i.e.

$$F = \int_0^{\Phi_0} \frac{d\Phi}{\sqrt{1 - K^2 \sin^2 \Phi}} = F(K, \Phi_0)$$

*Equation numbers are as assigned in Appendix A.

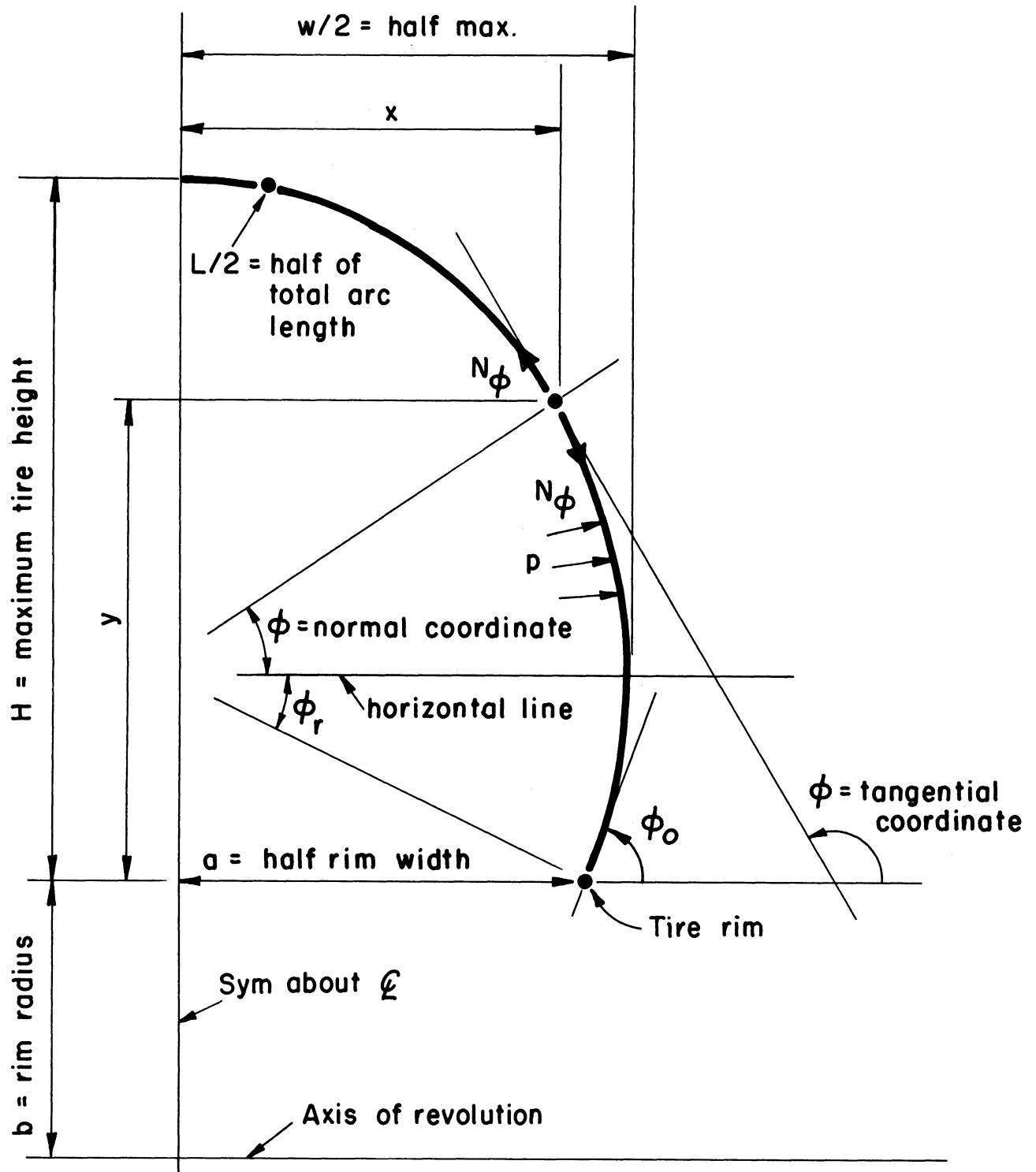


Figure 1. Inflated carcass notation.

and

$$E = \int_{\phi_0}^{\Phi_0} (1 - K^2 \sin^2 \phi) d\phi = E(K, \Phi_0)$$

The value of $\sqrt{\lambda}/a$ which satisfies Eqs. (30), (31), and (32) is found by an iterative procedure in which b/a and ϕ_0 are fixed and various values of $\sqrt{\lambda}/a$ are tried until Eq. (30) is satisfied. This procedure has been programmed in the MAD language for solution at The University of Michigan's computer facilities at Ann Arbor. Then, with this value of $\sqrt{\lambda}/a$ which satisfies Eqs. (30), (31) and (32) the ratio of total-arc-length to rim-width (L/a) is computed from Eq. (29) as follows:

$$\frac{L}{a} = 2 \frac{\sqrt{\lambda}}{a} F(K, \Phi_0) \quad (29)$$

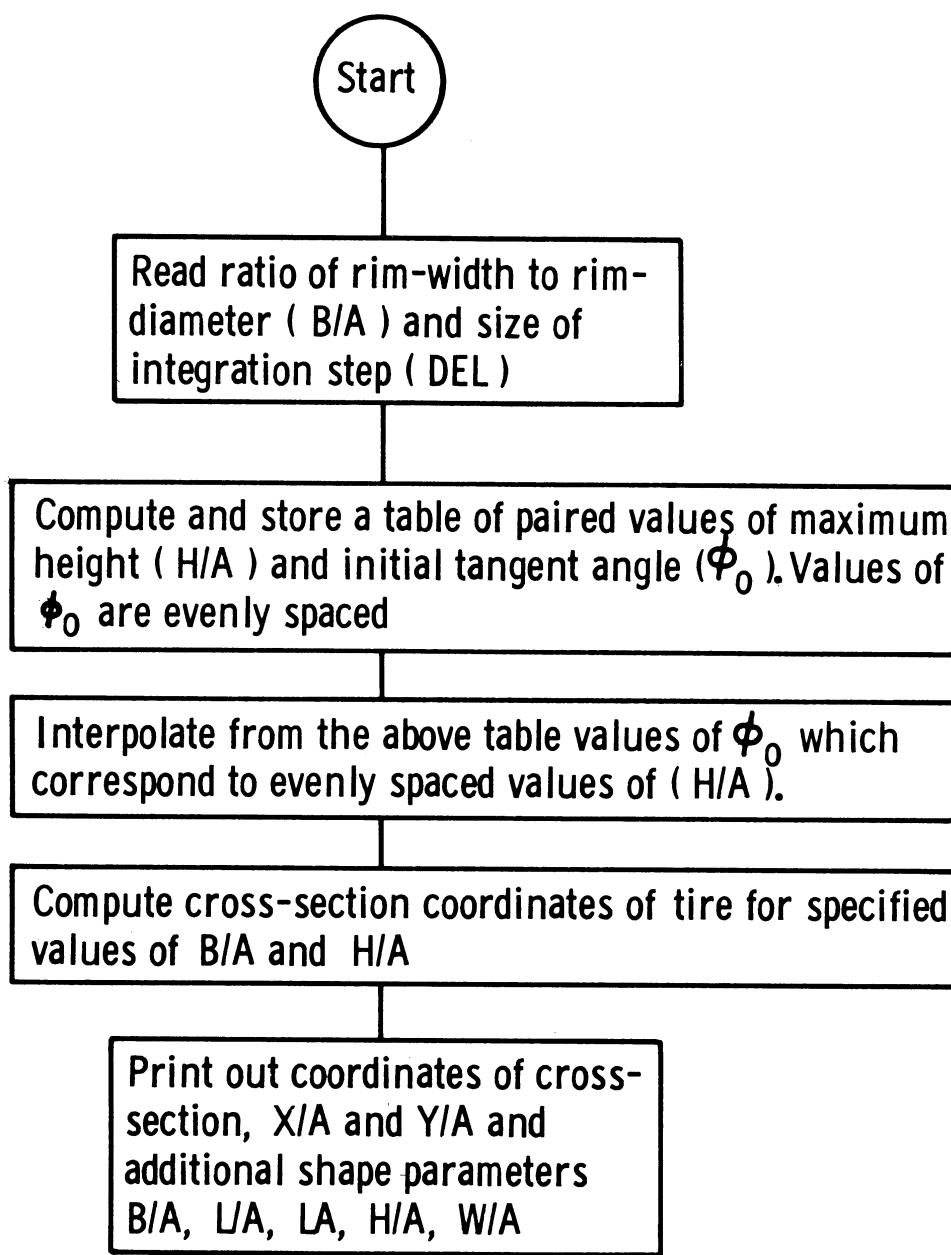
The ratio of maximum tire section height to rim-width (H/a) is computed from Eq. (38), where

$$\frac{H}{a} = \sqrt{2} \left(\frac{\sqrt{\lambda}}{a} \right) \left[\frac{(b/a)^2}{2(\sqrt{\lambda}/a)^2} + 1 + \cos \phi_0 \right]^{1/2} - (b/a) \quad (38)$$

Since for a specified (b/a) it is of more practical interest to specify (H/a) , rather than ϕ_0 , values of ϕ_0 were first specified and then stored in the computer with their corresponding values of (H/a) , as computed from Eq. (38). Then the subroutine TAB. was used to interpolate values of ϕ_0 for specified values of (H/a) . These values of ϕ_0 were then used in Eqs. (30), (31), and (32) to compute the corresponding values of $\sqrt{\lambda}/a$. New (H/a) values were computed from Eq. (38) and compared to the prescribed value to check the accuracy of the interpolation subroutine.

A simplified flow chart showing the essential features of the digital computer program is given in Figure 2. The program itself is given in Appendix B and has been written in the MAD* language for solution at the com-

*MAD (Michigan Algorithm Decoder) is an algebraic statement language designed by members of The University of Michigan Computing Center originally for the IBM 704 Computer and now available for the IBM 709 and 7090. The main features of MAD are very-high-speed compilation and a very general language. Programs produced by MAD are not as fast in execution as those produced by some other compilers; however, this disadvantage can be partially overcome by appropriate programming.



Φ_0 = tangent angle at rim
 LA = section constant
 B = rim diameter
 A = half rim-width
 L = total arc length in the plane of the cross-section
 H = distance from rim to crown
 W = width

Figure 2. Flow chart of computer program.

puting center of The University of Michigan.

Results are presented in tabular and graphical form. Each table is headed by the following tire carcass cross section parameters:

B/A, the ratio of rim-diameter to rim-width,

P, the program name for ϕ_0 , the tangent angle at the rim,

LA, the program name for $\sqrt{\lambda}/a$, the constant which simultaneously satisfies Eqs. (30), (31), and (32),

L/A, the ratio of total arc length to half the rim-width,

H/A, the ratio of maximum tire section height to half the rim-width,

and W/A, the ratio of tire section width to half the rim-width.

Then, below each heading are given the dimensionless coordinates (X/A) and (Y/A) which correspond to specified values of (B/A) and (H/A). A table of coordinates is given for each combination of (B/A) and (H/A) with (B/A) taking the values

1.00	2.00	3.00	7.00
1.25	2.25	4.00	8.00
1.50	2.50	5.00	9.00
1.75	2.75	6.00	10.00

and (H/A) taking the values 1.0 to 3.0 in 0.10 increments. The curves shown in Figures 3 and 4 are plots of some of the data given in the above tables and clearly show how the dimensionless shape of the inflated radial-ply tire carcass varies with the (B/A) and (H/A) ratios.

In the practical application of the tabular and graphical results, one will invariably need to establish some reasonably good method for interpolating shapes for (B/A) and (H/A) ratios not given. Owing to the relatively close spacing of the (B/A) ratios, it is hoped that interpolation with respect to (B/A) will not be necessary. For example, there is little noticeable difference in the dimensionless shapes given for (B/A) = 8 and the shapes given for (B/A) = 9. Graphical interpolation of shapes for arbitrary (H/A) ratios will probably provide sufficient accuracy for practical applications. It should be noted that all tabular data presented is in dimensionless form and can be plotted to any convenient scale for purposes of interpolation. In some instances (H/A) ratios do not precisely correspond to the evenly spaced prescribed values. This can be attributed to error in the interpolation routine used in the computer program. However, the X/A and Y/A coordinate data generated by the program are correct for whatever the H/A ratio actually is; the graphs of the shapes will just not have nice evenly spaced intercepts at

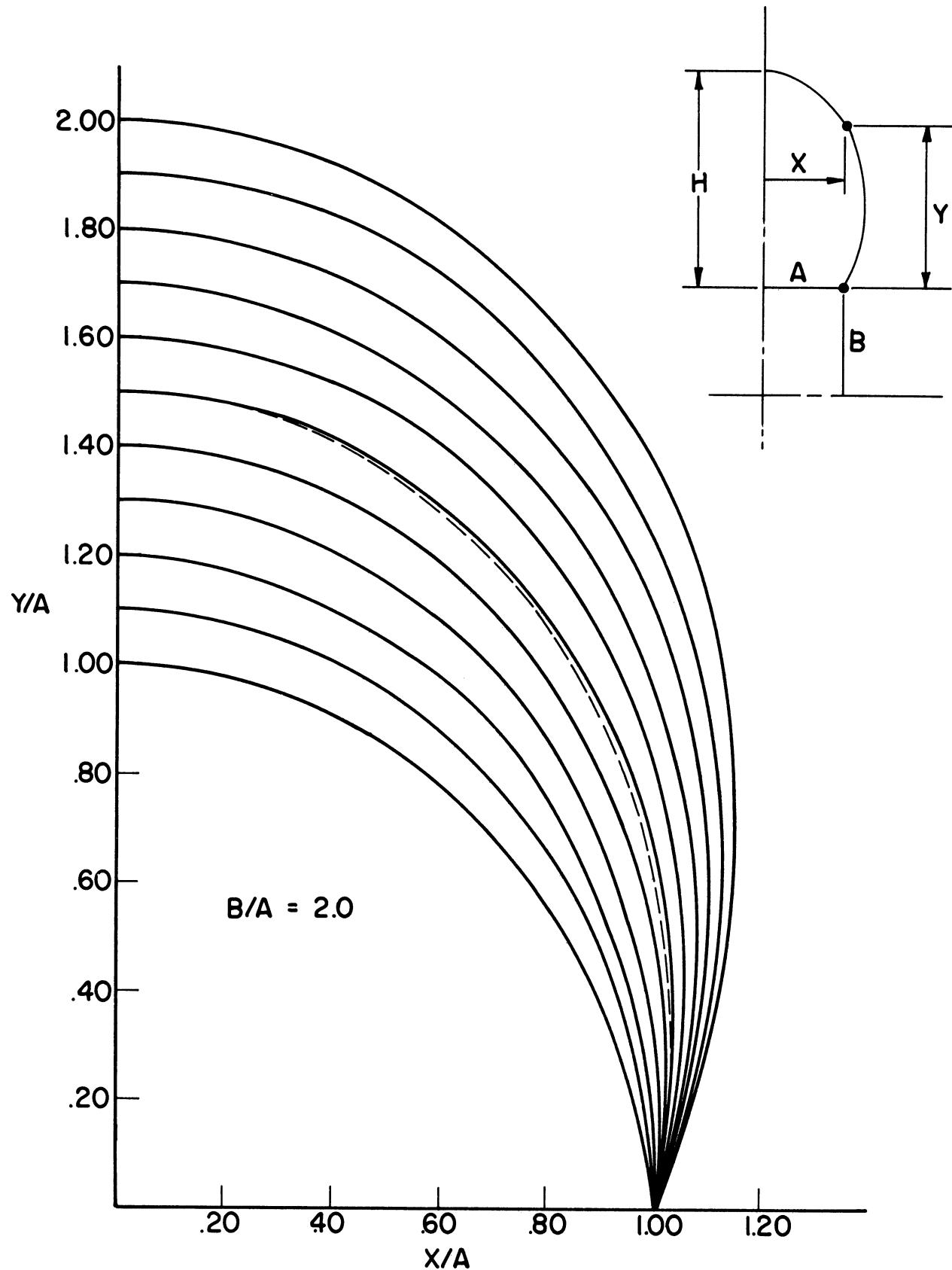


Figure 3. Meridian shapes for $B/a = 2.0$.

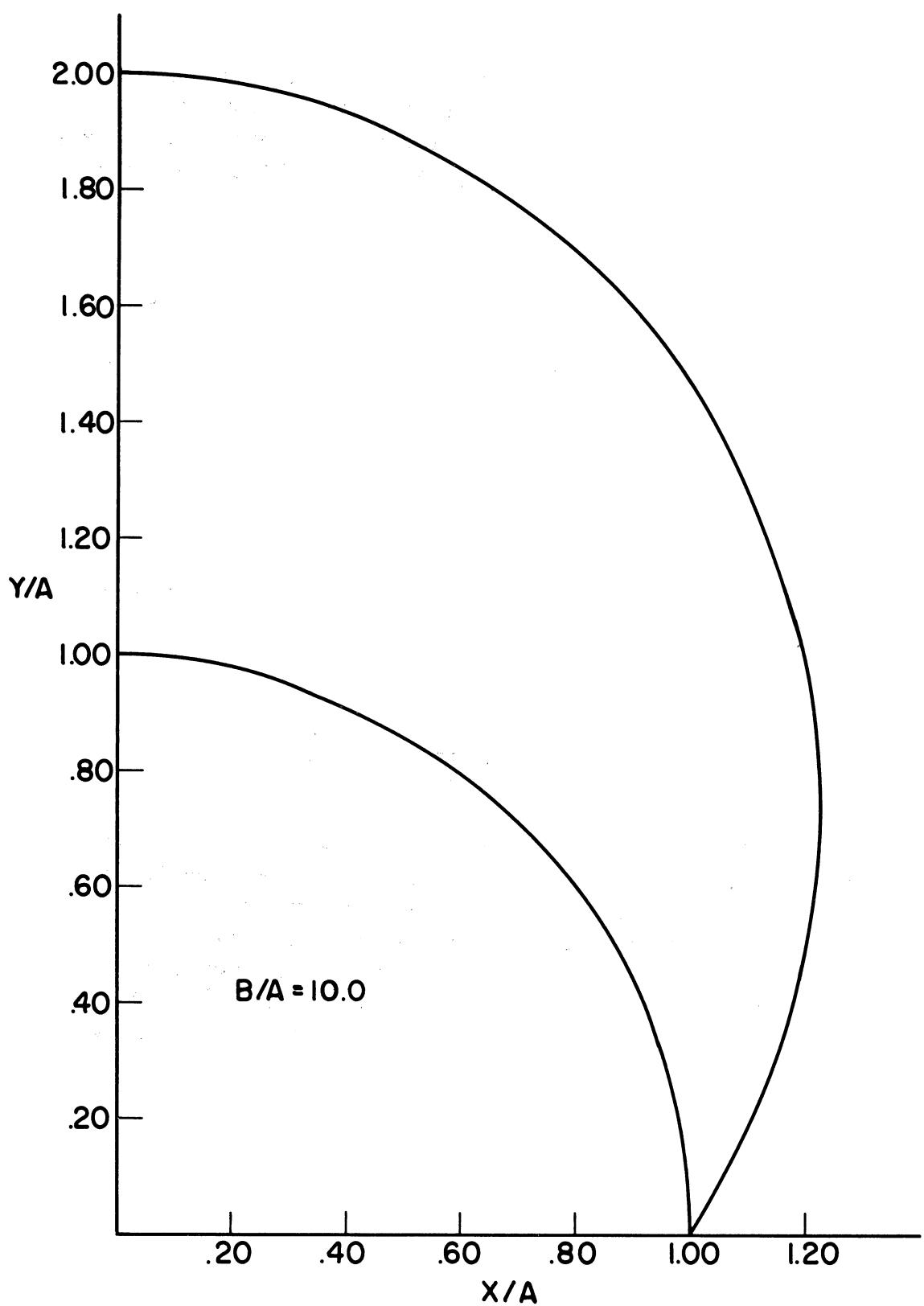


Figure 4. Meridian shapes for $B/a = 10.0$.

the crown, such as 1.300, 1.400, etc.

In instances where the tire width, rather than the tire height, is specified, a plot of width-vs-height can be made from the tabular data and the height which corresponds to the specified width can be picked off the resultant curve. Then the desired shape corresponding to this height can be obtained by graphical interpolation.

In addition to the tabular and graphical form of the inflated carcass shape, it may also be desirable to know the local radius of curvature at any point on the cross section. This is obtained from Eq. (5), which, in terms of parameters given at the heading of each table of coordinates, can be expressed as

$$\left(\frac{r_1}{a} \right) = \frac{(LA)^2}{(B/A + Y/A)}$$

for example, for $(B/A) = 2.0$ and $(H/A) = 2.00$, we see from Figure 10k that $LA = 5.322$.

Therefore, $\left(\frac{r_1}{a} \right) = \frac{(5.322)^2}{(2.00 + Y/A)} = \frac{28.4}{2 + Y/A}$

In general examination of the shape curves plotted in Figures 6a through 23v shows that for increasing (B/A) values the cross section of a radial-ply carcass approaches closer and closer to circular, so that one might expect an extreme case of this, such as a narrow bicycle tire, to be essentially circular. On the other hand, very wide tires will show considerable deviation from this as is evidenced by the plots of data for $(B/A) = 1.0$ to 2.0 . There, the shape becomes "higher" than a circle in appearance, and begins to take on characteristics of an ellipse on end.

APPENDIX A

ANALYSIS OF SHAPE OF INFLATED RADIAL-PLY CARCASS.

The applicable membrane equilibrium equations for a toroidal shell (shell of revolution) as given by Flugge (1)* are

$$\frac{d}{d\phi} (rN_\phi) - r_1 N_\theta \cos \phi = - P_\phi rr_1 \quad (1)$$

$$\frac{N_\phi}{r_1} + \frac{N_\theta}{r_2} = P_r = P \quad (2)$$

where the nomenclature is that found in Ref. (1). Let half the rim-width be a , and the rim radius be b , as shown in Figure 1.

If we assume that the radial reinforcement is many times stiffer than the circumferential stiffness, i.e. $E_\phi \gg E_\theta$, then we can take the stress resultant N_θ equal to zero. Furthermore, P_ϕ is zero since all pressure is normal. Hence, Eq. (2) reduces to

$$N_\phi = r_1 p \quad (3)$$

and Eq. (1) becomes

$$\frac{d}{d\phi} (rN_\phi) = 0. \quad (4)$$

Putting Eq. (3) into (4)

$$\frac{d}{d\phi} (rr_1 p) = 0,$$

or

$$rr_1 p = c$$

where c is a constant. Now since p , the internal pressure, is just some constant, we have

*Numbers in parenthesis refer to references given in the bibliography.

$$rr_1 = \lambda = \text{constant} \quad (5)$$

Introducing the Gauss relationship

$$dr = r_1 \cos\phi d\phi$$

or

$$\frac{dr}{d\phi} = r_1 \cos\phi \quad (6)$$

and differentiating Eq. (5) gives

$$r \frac{dr_1}{d\phi} + r_1 \frac{dr}{d\phi} = 0 = r \frac{dr_1}{d\phi} + r_1^2 \cos\phi \quad (7)$$

But from Eq. (5)

$$r = \lambda/r_1.$$

Hence, Eq. (7) becomes

$$\lambda \frac{dr_1}{d\phi} + r_1^3 \cos\phi = 0 \quad (8)$$

The solution of Eq. (8)

$$r_1 = \frac{1}{\sqrt{\frac{2}{\lambda_1} \sin\phi + c_2}} \quad (9)$$

where c_2 is another constant of integration and ϕ is the normal coordinate of a point on the meridian.

Equation (9) is subject to the following conditions, as shown in Figure 1:

(A) Setting r equal to b and putting Eq. (9) into Eq. (5) we get

$$\lambda = \frac{b}{\sqrt{\frac{2}{\lambda_1} \sin\phi_r + c_2}}$$

or

$$c_2 = \frac{b^2}{\lambda^2} - \frac{2}{\lambda} \sin \phi_r \quad (10)$$

(B) The length $L/2$ is known, i.e.

$$\int_{\phi_r}^{\pi/2} r_1 d\phi = \frac{L}{2} = \int_{\phi_r}^{\pi/2} \frac{d\phi}{\sqrt{\frac{2}{\lambda} \sin \phi + c_2}} = \int_{\phi_r}^{\pi/2} \frac{d\phi}{\sqrt{\frac{b^2}{\lambda^2} - \frac{2}{\lambda} \sin \phi_r + \frac{2}{\lambda} \sin \phi}} \quad (11)$$

(C) The dimension a is known, i.e.

$$a = \int_{\phi_r}^{\pi/2} r_1 \sin \phi d\phi = \int_{\phi_r}^{\pi/2} \frac{\sin \phi d\phi}{\sqrt{\frac{b^2}{\lambda^2} - \frac{2}{\lambda} \sin \phi_r + \frac{2}{\lambda} \sin \phi}} \quad (12)$$

We now deal with Eqs. (11) and (12) by changing to a tangential coordinate system to describe the independent variable as shown in Figure 1. From that figure, we have

$$\frac{\pi}{2} + \phi = \varphi$$

$$\sin \phi = -\cos \varphi$$

$$d\phi = d\varphi$$

$$\text{when } \phi = \frac{\pi}{2}, \quad \varphi = \pi$$

$$\text{when } \phi = \phi_r, \quad \varphi = \varphi_o$$

Making the above changes of independent variable, Eqs. (11) and (12) become

$$\frac{L}{2} = \int_{\varphi_o}^{\pi} \frac{d\varphi}{\sqrt{\frac{b^2}{\lambda^2} + \frac{2}{\lambda} (\cos \varphi_o - \cos \varphi)}} \quad (13)$$

$$-a = \int_{\varphi_0}^{\pi} \frac{\cos \varphi d\varphi}{\sqrt{\frac{b^2}{\lambda^2} + \frac{2}{\lambda} (\cos \varphi_0 - \cos \varphi)}} \quad (14)$$

Defining $\gamma = \frac{b^2}{2\lambda} + \cos \varphi_0$, then Eqs. (13) and (14) become

$$\sqrt{\frac{\lambda}{2}} \int_{\varphi_0}^{\pi} \frac{d\varphi}{\sqrt{\gamma - \cos \varphi}} = \frac{L}{2} \quad (15)$$

$$\sqrt{\frac{\lambda}{2}} \int_{\varphi_0}^{\pi} \frac{\cos \varphi d\varphi}{\sqrt{\gamma - \cos \varphi}} = -a \quad (16)$$

Defining the integrals

$$I = \int_{\varphi_0}^{\pi} \frac{d\varphi}{\sqrt{\gamma - \cos \varphi}} ; \quad J = \int_{\varphi_0}^{\pi} \sqrt{\gamma - \cos \varphi} d\varphi$$

Then

$$\int_{\varphi_0}^{\pi} \frac{\cos \varphi d\varphi}{\sqrt{\gamma - \cos \varphi}} = \gamma I - J$$

so that Eqs. (15) and (16) become

$$\sqrt{\frac{\lambda}{2}} (J - \gamma I) = a \quad (17)$$

$$\sqrt{\frac{\lambda}{2}} I = \frac{L}{2} \quad (18)$$

we now express I and J in terms of the standard incomplete elliptic integrals $F(K, x)$ and $E(K, x)$ where

$$F(K, x) = \int_0^x \frac{dt}{\sqrt{1 - K^2 \sin^2 t}} ; \quad E(K, x) = \int_0^x \sqrt{1 - K^2 \sin^2 t} dt$$

with the restriction that $K^2 \sin^2 x < 1$. Using the trigonometric relation that $\cos \varphi = 2 \cos^2 \varphi/2 - 1$, and changing the variable of integration from φ to ψ by means of

$$\frac{\varphi}{2} = \frac{\pi}{2} - \psi ,$$

then I and J become

$$I = 2 \int_0^{\frac{\pi - \varphi_0}{2}} \frac{d\psi}{\sqrt{\psi + 1 - 2 \sin^2 \psi}} \quad (19)$$

$$J = 2 \int_0^{\frac{\pi - \varphi_0}{2}} \sqrt{\psi + 1 - 2 \sin^2 \psi} d\psi \quad (20)$$

Making the change in variable

$$\sqrt{2} \sin \psi = \sqrt{\gamma + 1} \sin t ,$$

from which

$$d\psi = \sqrt{\frac{\gamma + 1}{2}} \frac{\cos t dt}{\sqrt{1 - (\frac{\gamma + 1}{2}) \sin^2 t}} ,$$

and substituting this into Eq. (19) yields

$$I = \sqrt{2} \int_0^{\sin^{-1}(\sqrt{\frac{2}{\gamma + 1}} \cos \frac{\varphi_0}{2})} \frac{dt}{\sqrt{1 - (\gamma + 1/2) \sin^2 t}}$$

or

$$I = \sqrt{2} \cdot F(K, \varphi_0) \quad (21)$$

where

$$K^2 = \frac{\gamma + 1}{2} = \frac{b^2}{4\lambda} + \cos^2 \frac{\varphi_0}{2} \text{ and}$$

$$K \sin \varphi_0 = \cos \frac{\varphi_0}{2}$$

Similarly,

$$J = \sqrt{2} (\gamma + 1) \int_0^{\Phi_0} \frac{\cos^2 t dt}{\sqrt{1 - \frac{(\gamma + 1)}{2} \sin^2 t}}$$

or

$$J = \sqrt{2} [(\gamma - 1) F(K, \Phi_0) + 2E(K, \Phi_0)] \quad (22)$$

Equations (17) and (18) now become

$$\sqrt{\lambda} (2E - F) = a \quad (23)$$

$$\sqrt{\lambda} F = L/2 \quad (24)$$

now add (23) and (24) to get

$$2\sqrt{\lambda} E = a + L/2 \quad (25)$$

where, to repeat,

$$E = E(K, \Phi_0); \quad F = F(K, \Phi_0)$$

and

$$K \sin \Phi_0 = \cos \frac{\Phi_0}{2} \quad (26)$$

$$K^2 = \frac{b^2}{4\lambda} + \cos^2 \frac{\Phi_0}{2} \quad (27)$$

Dividing Eqs. (23) and (24) by a, they become

$$\frac{2\sqrt{\lambda}}{a} E = 1 + \frac{1}{2} \left(\frac{L}{a} \right) \quad (28)$$

$$\frac{\sqrt{\lambda}}{a} F = \frac{1}{2} \left(\frac{L}{a} \right) \quad (29)$$

Eliminating (L/a) between Eqs. (28) and (29) gives

$$\frac{\sqrt{\lambda}}{a} (2E - F) - 1 = 0 \quad (30)$$

Equation (27) can be rewritten as

$$K^2 = \frac{(b/a)^2}{4(\frac{\sqrt{\lambda}}{a})^2} + \cos^2 \frac{\Phi_0}{2} \quad (31)$$

Squaring Eq. (26), subtracting it from Eq. (27) and noting that $1 - \sin^2 \Phi_0 = \cos^2 \Phi_0$, we get

$$K \cos \Phi_0 = \frac{(b/a)}{2(\sqrt{\lambda}/a)} \quad (32)$$

The equations which must be simultaneously satisfied are Eqs. (29), (30), (31), and (32). We do this by working first with only Eqs. (30), (31), and (32) in the following sequence

- (1) Fix (b/a) (ratio of rim-width to rim-diameter)
- (2) Fix Φ_0 (angle between tangent to carcass at the rim and the axis of revolution)
- (3) Choose a value of $\sqrt{\lambda}/a$
 - (a) Calculate K from Eq. (31)
 - (b) Calculate Φ_0 from Eq. (32)
- (4) Check (30) to see if it is satisfied. If it is then $\sqrt{\lambda}/a$ is correctly chosen. If not, choose a new value and try again until we have a value which works.

Now use Eq. (29) to calculate (L/a) , the dimensionless arc length from rim-to-rim. It should be emphasized that $\sqrt{\lambda}/a$ is a function of Φ_0 and (b/a) and must be obtained by trial and error in such a way as to satisfy the boundary conditions. However, once it is found and substituted back into

$$rr_1 = \lambda \quad (5')$$

then all other characteristics of the carcass shape can be computed in a straightforward manner.

Finally, we need to calculate the section height H and the section width W . To obtain the section height we return to Eq. (5') from which

$$r = \lambda/r_1 \quad (33)$$

But, from Eq. (11),

$$r_1 = \frac{1}{\sqrt{\frac{b^2}{\lambda^2} - \frac{2}{\lambda} \sin \phi_r + \frac{2}{\lambda} \sin \phi}}$$

or

$$r_1 = \frac{\sqrt{\lambda/2}}{\sqrt{\frac{b^2}{2\lambda} - \sin \phi_r + \sin \phi}}$$

Now, change variables by letting

$$\frac{\pi}{2} + \phi = \varphi$$

from which

$$\sin \phi = -\cos \varphi$$

Then

$$r_1 = \frac{\sqrt{\frac{\lambda}{2}}}{\sqrt{\frac{b^2}{2\lambda} + \cos \phi_o - \cos \varphi}} \quad (35)$$

Noting that the independent variable is now φ , the tangent to the carcass at any point, we can obtain the maximum distance r_{\max} from the axis of revolution by setting $\varphi = \pi$. Then

$$(r_1)_{\varphi=\pi} = \frac{\sqrt{\frac{\lambda}{2}}}{\sqrt{\frac{(b/a)^2}{2} + 1 + \cos \phi_o}} \quad (36)$$

Therefore, from Eqs. (33) and (36)

$$r_{\max} = (r)_{\varphi = \pi} = \sqrt{2} \sqrt{\lambda} \sqrt{\frac{(\frac{b}{a})^2}{2(\frac{\sqrt{\lambda}}{a})^2} + 1 + \cos \varphi_0} \quad (37)$$

But, as can be seen from Figure 1,

$$(r)_{\varphi = \pi} = b + H$$

from which

$$\frac{H}{a} = \frac{(r)_{\varphi = \pi}}{a} - \frac{b}{a}$$

or

$$\frac{H}{a} = \sqrt{2} \left(\frac{\sqrt{\lambda}}{a} \right) \sqrt{\frac{(\frac{b}{a})^2}{2(\frac{\sqrt{\lambda}}{a})^2} + 1 + \cos \varphi_0} - \frac{b}{a} \quad (38)$$

Equation (38) gives the dimensionless height as a function of the (b/a) ratio, the initial tangent angle φ_0 and a constant $\sqrt{\lambda}/a$ which was previously determined in such a way that the boundary conditions of the problem were satisfied.

The half section width $W/2$ is given by

$$\frac{W}{2} = \int_{\pi/2}^{\pi} \frac{\cos \varphi d\varphi}{\sqrt{\frac{b^2}{\lambda^2} + \frac{2}{\lambda} (\cos \varphi_0 - \cos \varphi)}}$$

Let

$$\gamma = \frac{b^2}{2\lambda} + \cos \varphi_0 = \frac{(\frac{b}{a})^2}{2(\frac{\sqrt{\lambda}}{a})^2} + \cos \varphi_0 .$$

Then Eq. (39) becomes

$$\frac{W}{2} = \sqrt{\frac{\lambda}{2}} \int_{\pi/2}^{\pi} \frac{\cos \varphi d\varphi}{\sqrt{\gamma - \cos \varphi}} \quad (40)$$

Now let $\varphi = \pi - \psi$

$$\text{when } \varphi = \pi, \quad \psi = 0$$

When $\varphi = \pi/2$, $\psi = \pi/2$

Consider the integrals \tilde{I} and \tilde{J} where

$$\tilde{I} = \int_{\pi/2}^{\pi} \frac{d\varphi}{\sqrt{\gamma - \cos \varphi}} ; \quad \tilde{J} = \int_{\pi/2}^{\pi} \sqrt{\gamma - \cos \varphi} d\varphi$$

Then

$$\int_{\pi/2}^{\pi} \frac{\cos \varphi d\varphi}{\sqrt{\gamma - \cos \varphi}} = \gamma \tilde{I} - \tilde{J} \quad (41)$$

Noting that $d\varphi = -d\psi$, and using the trigonometric relationships

$$\cos \varphi = 2 \cos^2 \frac{\varphi}{2} - 1$$

and

$$\cos \frac{\varphi}{2} = \cos \left(\frac{\pi}{2} - \frac{\psi}{2} \right) = \sin \frac{\psi}{2}$$

we find that

$$\cos \varphi = 2 \sin^2 \frac{\psi}{2} - 1$$

Thus the integrals \tilde{I} and \tilde{J} can be written

$$\tilde{I} = \int_{\pi/2}^0 \frac{-d\psi}{\sqrt{\gamma + 1 - 2 \sin^2 \psi/2}} = 2 \int_0^{\pi/2} \frac{d(\frac{\psi}{2})}{\sqrt{\gamma + 1 - 2 \sin^2 \psi/2}}$$

Making the substitution $\alpha = \psi/2$,

$$\tilde{I} = \frac{2}{\sqrt{\gamma + 1}} \int_0^{\pi/2} \frac{d\alpha}{\sqrt{1 - \left(\frac{2}{\gamma + 1} \right) \sin^2 \alpha}}$$

or

$$\tilde{I} = \frac{2}{\sqrt{\gamma + 1}} F \left(\sqrt{\frac{2}{\gamma + 1}} \right) \quad (42)$$

Similarly

$$J = 2\sqrt{\gamma + 1} \int_0^{\pi/2} \sqrt{1 - \left(\frac{2}{\gamma + 1}\right) \sin^2 \alpha} d\alpha$$

or

$$\tilde{J} = 2\sqrt{\gamma + 1} \left[E\left(\sqrt{\frac{2}{\gamma + 1}}\right) \right] \quad (43)$$

Note that $F(\sqrt{2/\gamma + 1})$ and $E(\sqrt{2/\gamma + 1})$ are the complete elliptic integrals of the first and second kind respectively, with modulus $K = \sqrt{2/\gamma + 1}$. By virtue of Eqs. (40) and (41)

$$\frac{W}{2} = \sqrt{\frac{\lambda}{2}} (\gamma \tilde{I} - \tilde{J})$$

From which

$$\frac{W}{a} = \sqrt{2} \left(\frac{\sqrt{\lambda}}{a} \right) [\gamma \tilde{I} - \tilde{J}] \quad (44)$$

where I and J are given by Eqs. (42) and (43). Again, the solution is in terms of the parameter $\sqrt{\lambda}/a$. Once the term $\sqrt{\lambda}/a$ has been determined for particular values of (b/a) and φ_0 , it is possible to calculate the radial shape of the carcass in a straightforward way. For some point on the cross section of the inflated carcass, let

x = distance from vertical plane of symmetry

y = vertical distance from rim

r = radial distance from axis of revolution.

as shown in Figure 1.

To get the y coordinate in terms of the independent variable φ , we put Eq. (5') into Eq. (35) to get

$$r = \frac{\lambda}{r_1} = \sqrt{2} \sqrt{\lambda} \sqrt{\frac{b^2}{2} + \cos \varphi_0 - \cos \varphi}$$

which can be written as

$$\frac{r}{a} = \sqrt{\left(\frac{b}{a}\right)^2 + 2\left(\frac{\sqrt{\lambda}}{a}\right)^2 (\cos \varphi_0 + \sin \phi)} . \quad (45)$$

Then, from the relation

$$y + b = r$$

we get

$$\frac{y}{a} = \frac{r}{a} - \frac{b}{a} ,$$

which when put into Eq. (45) yields

$$\frac{y}{a} = \sqrt{\left(\frac{b}{a}\right)^2 + 2\left(\frac{\sqrt{\lambda}}{a}\right)^2 (\cos \varphi_0 + \sin \phi)} \quad (46)$$

To get the x coordinate as a function of ϕ , we have the relations

$$x = a - \int_{\phi_r}^{\phi} r_1 \sin \phi \, d\phi . \quad (47)$$

Rewriting Eq. (35) in the form

$$r_1 = \frac{\sqrt{\lambda/a}}{\sqrt{\frac{(b/a)^2}{(\sqrt{\lambda}/a)^2} + 2(\cos \varphi_0 + \sin \phi)}}$$

and putting this into Eq. (47), we get

$$x = a - \int_{\phi_r}^{\phi} \frac{\sqrt{\lambda} \sin \phi \, d\phi}{\sqrt{\frac{(b/a)^2}{(\sqrt{\lambda}/a)^2} + 2(\cos \varphi_0 + \sin \phi)}} \quad (48)$$

or

$$\frac{x}{a} = 1 - \int_{\phi_r}^{\phi} \frac{(\sqrt{\lambda}/a) \sin \phi \, d\phi}{\sqrt{\frac{(b/a)^2}{(\sqrt{\lambda}/a)^2} + 2(\cos \varphi_0 + \sin \phi)}} \quad (49)$$

Equation (49) can be put in the form of an elliptic integral, requiring certain changes of variables. However, with the use of the digital computer it can be numerically integrated as it stands by some method such as Simpsons' rule. Equations (46) and (49) give the y and x coordinates of a point, respectively, for any specified value of the independent variable φ . As a check, $(x/a)_{\max}$ from Eq. (49) should be equal to (W/a) as given by Eq. (44), and $(y/a)_{\max}$ from Eq. (46) should be equal to (H/a) as given by Eq. (38).

APPENDIX B

DIGITAL COMPUTER PROGRAM TO DETERMINE SHAPE OF RADIAL-PLY CARCASS

The basic program flow chart is given in Figure 2. Figure 5 is a detailed program listing, while Figures 6 and 7 give similar listings for the two major subroutines used in the execution of the calculations.

\$COMPILE MAD, EXECUTE, DUMP, PRINT OBJECT, PUNCH OBJECT

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```
MAD (29 APR 1966 VERSION) PROGRAM LISTING . . . . .  
  
START  
    INTEGER N,N1,J,Q,ZZ,LO,HI,$  
    DIMENSION XA(360),YA(360),SUM(360),P(20),HA(20)  
    READ AND PRINT DATA BA,DEL  
    THROUGH LOOP1, FOR S=1,1, S.6.10  
    P(S)=1.9-.1*S  
    PRINT RESULTS P(S)  
    C1=COS.(P(S)/2)*COS.(P(S)/2)  
    C=BA/(2.*SQR(.1.0.-C1))  
    WHENEVER BA.G.2.0  
    A=5.0  
    OTHERWISE  
    A=C+6.0  
    END OF CONDITIONAL  
    B=1.0  
    DELLA=0.50  
    PRINT RESULTS C,A,B,DELLA  
    EXECUTE UINTR2.(A,DELLA,B,.001,.0001,256,LA)  
    K = SQR((BA*BA)/(4.*LA*LA)) + C1  
    PHI = ARCCOS.(BA/(2.*K*LA))  
    F=ELLIPT.(K,PHI,1.0)  
    E=ELLIPT.(K,PHI,2.0)  
    FCN=LA*(12.*E-F)-1.0  
    I=UINTR2A.(FCN)  
    WHENEVER I.E.1.C, TRANSFER TO GO  
    ZZ=S  
    WHENEVER I.E.2.0  
    PRINT COMMENT $ NC ROOT FOUND$  
    ZZ=S-1  
    PRINT RESULTS LA,P(1)...P(ZZ),HA(1)...HA(ZZ)  
    TRANSFER TO SKIP  
    END OF CONDITIONAL  
    WHENEVER I.E.3.C  
    PRINT COMMENT $ NO. OF ITERATIONS EXCEEDED$  
    TRANSFER TO START  
    END OF CONDITIONAL  
    PRINT RESULTS LA,K,PHI  
    HA(S)=1.414214*(LA*SQR(.BA*BA/(2.*LA*LA)+COS.(P(S))+1.0)-BA  
    PRINT RESULTS P(1)...P(ZZ),HA(1)...HA(ZZ)  
    LO=(HA(1)+.1)*10.  
    WHENEVER LO.L.10,LO=10  
    HI=10.*HA(ZZ)  
    WHENEVER HI.G.20,HI=20  
    THROUGH TASK, FOR Q=LO,1,Q.G.HI  
    HA=G/10.0  
    P=TAB.(HA,HA(1),P(1),1,1,5,ZZ,SW)  
    WHENEVER SW.E.2.0  
    PRINT COMMENT $ INTERPOLATION ROUTINE FAILS$  
    PRINT RESULTS HA  
    TRANSFER TO TASK  
    END OF CONDITIONAL  
    PRINT RESULTS HA,P  
    C1 = COS.(P/2)*COS.(P/2)  
    C=BA/(2.*SQR(.1.0.-C1))
```

Figure 5. Listing of computer main program.

```

PRINT RESULTS C,A,B,DELLA
EXECUTE UINTR2.(A,DELLA,B,*001,*0001,256,LA)
GONE
K = SQR1.((BA*BA)/(4.*LA*LA) + C1)
PHI = ARCCOS.(BA*(2.*K*LA))
F=ELLIPT.(K,PHI,1.0)
E=ELLIPT.(K,PHI,2.0)
FCN=LA*(2.*E-F)-1.0
I=UINTR2A.(FCN)
WHENEVER I.E.1.0, TRANSFER TO GONE
WHENEVER I.E.2.0
PRINT COMMENT $ NO. OF ITERATIONS EXCEEDED$
PRINT COMMENT $ NO ROOT FOUND$
PRINT RESULTS LA,P
TRANSFER TO TASK
END OF CONDITIONAL
WHENEVER I.E.3.0
PRINT COMMENTS OF CROSS-SECTION OF TIRE
TRANSFER TO TASK
END OF CONDITIONAL
PRINT RESULTS LA,K,PHI
HA=+4*14214*LA*SQRT.(BA*BA/(2.*LA*LA)+COS.(P)+1.0)-BA
L=2.*F*LA
COORDINATES OF CROSS-SECTION OF TIRE
R=3.14159-P
D=P-1.570796
N=R/(2.*DEL)
N=2*N1
INC=R/N
SUM(0)=0.0
XA(0)=1.0
YA(0)=0.0
WA=2.0
THROUGH LOOP10, FOR J=1,1,J.G.N1
YA(J)=SQR1.(BA*BA + 2.*LA*LA*(COS.(P)+SIN.(D+2.*J*R/N))) - BA
FO=LA*LA*SIN.(D+2.*J-2.*R/N)/SQRT.(BA*BA + 2.*LA*LA*)
1.(COS.(P)+SIN.(D+2.*J-2.*R/N))-
F1=LA*LA*SIN.(D+2.*J-1.*R/N)/SQRT.(BA*BA + 2.*LA*LA*)
1.(COS.(P)+SIN.(D+2.*J-1.*R/N))-
F2=LA*LA*SIN.(D+2.*J*R/N)/SQRT.(BA*BA + 2.*LA*LA*(COS.(P)+SIN.
1.(D+2.*J*R/N))-
SUM(J)=SUM(J-1)+(INC/3.)*(FO+4.*F1+F2)
XA(J)=1.0-SUM(J)
WHENEVER J.G.-1 AND YA(J-1).G.XA(J-2).AND.XA(J-1).G.XA(J)
WA = 2.*XA(J-1)
END OF CONDITIONAL
HA = YA(N1)
LOOP10
PRINT COMMENT $1$  

PRINT FORMAT HEADS
VECTOR VALUES HEADS = $S16,3HB/A,S8,1HP,S9,2H LA,S7,
1.3HL/A,S7,3HH/A,S7,3HW/A*$  

PRINT FORMAT CON,BAP,LA,L,HA,WA  

VECTOR VALUES CUN = $S10,6F10.3//*$  

PRINT FORMAT TABLE
VECTOR VALUES TABLE = $S36,3HX/A,S7,3HY/A/*$  

THROUGH TASK, FOR J=0,1,J.G.N1
PRINT FORMAT COORD,XA(J),YA(J)
VECTOR VALUES COORD = $S30,2F10.3*$  

CONTINUE
TRANSFER TO START
END OF PROGRAM

```

Figure 5. Concluded.

UITR2

SINGLE ITERATION - INTERVAL HALVING

PURPOSE GIVEN $F(X) = 0$ TO FIND A VALUE FOR X WITHIN A GIVEN ERROR IN A SPECIFIED INTERVAL (A,B) .

CALLING SEQUENCES

MAD EXECUTE UITR2.(A,DELX,B,EPS1,EPS2,K,X)
I = UITR2A.(F)

FORTRAN CALL UITR2(A,DELX,B,EPS1,EPS2,K,X)
I = UITR2A(F)

UMAP CALL UITR2
PAR A
PAR DELX
PAR B
PAR EPS1
PAR EPS2
PAR K
PAR X
NORMAL RETURN
COMPUTE F
CALL UITR2A
PAR F
NORMAL RETURN - I IN THE ACCUMULATOR

ARGUMENTS

A FLOATING POINT LOWER LIMIT OF THE INTERVAL (A,B) .

B FLOATING POINT UPPER LIMIT OF THE INTERVAL (A,B) .

DELX THE INTERVAL (A,B) IS STEPPED ACROSS FROM A, IN INCREMENTS OF DELX, UNTIL A CHANGE OF SIGN OCCURS IN THE FUNCTION $F(X)$. THEN THIS INTERVAL IS HALVED A SPECIFIED NUMBER OF TIMES UNTIL THE RCOT IS FOUND OR THE ITERATION COUNT IS EXCEEDED. DELX IS FLOATING POINT.

EPS1 EPSILON VALUES FOR CONVERGENCE TESTS.

EPS2 (SEE UITR1 WRITE-UP.)

K INTEGER NUMBER OF ITERATIONS TO BE ALLOWED.

X FLOATING POINT INDEPENDENT VARIABLE. X IS THE DESIRED RCOT AFTER SUCCESSFUL EXECUTION OF THE SUBROUTINE.

F IN FORTRAN AND MAD, THE FLOATING POINT EXPRESSION WHICHSE VALUE IS $F(X)$. IN UMAP, F IS THE LOCATION OF THE VALUE OF THIS FUNCTION. F MUST BE COMPUTED BEFORE INITIAL ENTRY INTO UITR2A.

Figure 6. Iteration subroutine.

I COMPUTATION SWITCH - FLOATING POINT
I = 1.0 NEW ITERATION REQUIRED. IN MAD OR FORTRAN,
RETURN TO UITR2A. IN UMAP, RECOMPUTE THE FUNCTION
F AND THEN RETURN TO UITR2A.
I = 2.0 THE INTERVAL (A,B) HAS BEEN COMPLETELY SCANNED
AND NO ROOT WAS FOUND.
I = 3.0 NUMBER OF ITERATIONS (K) EXCEEDED WITHOUT MEET-
ING THE TEST. THE CURRENT APPROXIMATE OF THE
ROOT IS IN X.
I = 4.0 NORMAL RETURN, COMPUTATION SUCCESSFUL.

CODING INFORMATION

STORAGE REQUIRED

UITR2,UITR2A	322
ERASABLE	0

NOTE.....FOR A DISCUSSION OF THE CONVERGENCE TESTS
UTILIZED IN UITR2, SEE THE WRITE-UP ENTITLED
UITR CONVERGENCE TESTING IN ITERATION
SUBROUTINES.

Figure 6. Concluded.

TAB

SINGLE TABLE INTERPOLATION

PURPOSE GIVEN THE VALUE OF AN INDEPENDENT ARGUMENT X, PERFORM A KTH ORDER INTERPOLATION ON A TABLE OF (X(I),Y(I)) VALUES FOR THE CORRESPONDING DEPENDENT ARGUMENT Y.

CALLING SEQUENCES

MAD	Y = TAB.(X,XT,YT,M1,M2,K,N,SW)
FORTRAN	Y = TAB(X,XT,YT,M1,M2,K,N,SW)
UMAP	CALL TAB
PAR	X
PAR	XT
PAR	YT
PAR	M1
PAR	M2
PAR	K
PAR	N
PAR	SW

NORMAL RETURN - Y IN THE ACCUMULATOR

ARGUMENTS

X	INDEPENDENT FLOATING POINT ARGUMENT X FOR WHICH THE CORRESPONDING VALUE Y IS DESIRED.
XT	NAME OF THE FIRST ENTRY IN THE TABLE OF FLOATING POINT INDEPENDENT VARIABLES, X(I).
YT	NAME OF THE FIRST ENTRY IN THE TABLE OF FLOATING POINT DEPENDENT VARIABLES, Y(I).
M1	INTEGRAL NUMBER OF STORAGE LOCATION STEPS BETWEEN EACH ENTRY OF THE INDEPENDENT VARIABLE TABLE. NORMALLY M1 = 1 WHEN THE VARIABLES ARE STORED IN SEQUENTIAL LOCATIONS.
M2	INTEGRAL NUMBER OF LOCATIONS BETWEEN EACH ENTRY OF THE DEPENDENT VARIABLE TABLE. NORMALLY M2 = 1.
K	INTEGRAL ORDER OF INTERPOLATION DESIRED, K .LE. 5.
N	INTEGRAL NUMBER OF ENTRIES IN THE INDEPENDENT VARIABLE TABLE (NUMBER OF PAIRS (X(I),Y(I))).
SW	FLOATING POINT COMPUTATION SWITCH
	SW = 1.0 NORMAL RETURN, INTERPOLATION SUCCESSFUL.
	SW = 2.0 AC OR MQ OVERFLOW OR UNDERFLOW OR DIVIDE CHECK -- ERROR RETURN.
Y	FLOATING POINT DEPENDENT VARIABLE, THE INTERPOLATED VALUE FOR THE INDEPENDENT VARIABLE X.

CODING INFORMATION

STORAGE REQUIRED

TAB	307
ERASABLE	22

Figure 7. Interpolation subroutine.

APPENDIX C

DIGITAL AND GRAPHICAL PRESENTATION OF INFLATED SHAPES

The computed meridian shapes for various (B/a) ratios are given for discrete values of (H/a) in Figures 8a through 23v. Two methods are chosen for presenting the information. In the first method direct numerical data is given from the computer output in the form of (x/a) vs. (y/a) co-ordinates defining the inflated meridian shape. This information is carried to three significant figures and is useful for layout work or further interpolation. Secondly the (x/a) vs. (y/a) data is plotted to scale and may be used to visualize quickly the effect of changes in a particular parameter.

Figures 8-23

Numerical and graphical inflated radial-ply carcass shapes for various (B/a) and (H/a) values.

B/A 1.000	P 1.729	L/A 1.335	L/A 3.091	H/A 1.001	W/A 2.000
		X/A	Y/A		
		1.000	.000		
		.971	.144		
		.933	.269		
		.890	.379		
		.840	.477		
		.786	.565		
		.727	.644		
		.664	.713		
		.598	.775		
		.530	.829		
		.458	.875		
		.385	.913		
		.310	.945		
		.233	.969		
		.156	.987		
		.077	.997		
		-.001	1.001		

Figure 8. (a)

B/A 1.000	P 1.653	L/A 1.363	L/A 3.280	H/A 1.100	W/A 2.000
		X/A	Y/A		
		1.000	.000		
		.981	.150		
		.953	.281		
		.917	.397		
		.874	.501		
		.826	.594		
		.773	.678		
		.716	.754		
		.654	.821		
		.590	.880		
		.522	.932		
		.452	.977		
		.380	1.015		
		.306	1.046		
		.230	1.070		
		.154	1.087		
		.077	1.097		
		-.000	1.100		

Figure 8. Continued. (b)

B/A 1.000	P 1.587	L/A 1.398	L/A 3.481	H/A 1.201	W/A 2.000
--------------	------------	--------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
.990	.165
.968	.308
.937	.434
.897	.547
.851	.649
.799	.740
.741	.823
.679	.896
.613	.961
.544	1.018
.471	1.067
.396	1.108
.319	1.142
.241	1.168
.161	1.186
.080	1.197
-.001	1.201

Figure 8. Continued. (c)

B/A 1.000	P 1.528	L/A 1.434	L/A 3.683	H/A 1.300	W/A 2.000
--------------	------------	--------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.000	.170
.986	.317
.963	.449
.930	.566
.890	.673
.843	.769
.791	.856
.734	.935
.672	1.005
.607	1.068
.538	1.123
.466	1.170
.392	1.210
.316	1.242
.238	1.267
.160	1.285
.080	1.296
-.000	1.300

Figure 8. Continued. (d)

B/A <u>1.000</u>	P <u>1.476</u>	LA <u>1.475</u>	L/A <u>3.897</u>	H/A <u>1.400</u>	W/A <u>2.000</u>
---------------------	-------------------	--------------------	---------------------	---------------------	---------------------

X/A	Y/A
1.000	.000
1.009	.175
1.004	.327
.987	.463
.961	.585
.927	.696
.885	.797
.838	.889
.786	.973
.728	1.048
.667	1.116
.601	1.176
.533	1.229
.462	1.275
.388	1.313
.313	1.345
.236	1.369
.157	1.386
.078	1.397
-.001	1.400

Figure 8. Continued. (e)

B/A <u>1.000</u>	P <u>1.429</u>	LA <u>1.516</u>	L/A <u>4.109</u>	H/A <u>1.499</u>	W/A <u>2.040</u>
---------------------	-------------------	--------------------	---------------------	---------------------	---------------------

X/A	Y/A
1.000	.000
1.019	.188
1.020	.351
1.008	.496
.985	.627
.953	.745
.913	.853
.867	.951
.814	1.041
.756	1.121
.693	1.194
.626	1.258
.555	1.315
.482	1.364
.405	1.405
.327	1.439
.247	1.465
.165	1.484
.083	1.495
-.000	1.499

Figure 8. Continued. (f)

B/A <u>1.000</u>	P <u>1.387</u>	L/A <u>1.560</u>	L/A <u>4.331</u>	H/A <u>1.599</u>	W/A <u>2.073</u>
---------------------	-------------------	---------------------	---------------------	---------------------	---------------------

X/A	Y/A
1.000	.000
1.027	.193
1.036	.360
1.031	.508
1.015	.643
.988	.765
.954	.877
.912	.980
.864	1.073
.811	1.159
.752	1.236
.689	1.305
.622	1.367
.551	1.422
.478	1.469
.402	1.509
.324	1.541
.244	1.566
.163	1.584
.082	1.595
-.000	1.599

Figure 8. Continued. (g)

B/A <u>1.000</u>	P <u>1.349</u>	L/A <u>1.605</u>	L/A <u>4.556</u>	H/A <u>1.699</u>	W/A <u>2.105</u>
---------------------	-------------------	---------------------	---------------------	---------------------	---------------------

X/A	Y/A
1.000	.000
1.037	.206
1.053	.384
1.052	.542
1.039	.684
1.016	.814
.983	.933
.942	1.041
.894	1.141
.839	1.231
.779	1.313
.715	1.387
.646	1.453
.573	1.511
.497	1.561
.418	1.603
.337	1.638
.254	1.665
.170	1.684
.085	1.696
-.000	1.699

Figure 8. Continued. (h)

B/A	P	LA	L/A	H/A	W/A
<u>1.000</u>	<u>1.316</u>	<u>1.653</u>	<u>4.787</u>	<u>1.800</u>	<u>2.149</u>

X/A	Y/A
1.000	.000
1.047	.220
1.070	.408
1.074	.575
1.065	.726
1.043	.863
1.012	.989
<u>.971</u>	<u>1.104</u>
.923	1.209
.868	1.305
.807	1.392
.741	1.470
.670	1.539
.595	1.601
.516	1.654
.435	1.699
.350	1.735
.264	1.764
.177	1.784
.088	1.796
<u>-.001</u>	<u>1.800</u>

Figure 8. Continued. (i)

B/A	P	LA	L/A	H/A	W/A
<u>1.000</u>	<u>1.285</u>	<u>1.701</u>	<u>5.018</u>	<u>1.901</u>	<u>2.192</u>

X/A	Y/A
1.000	.000
<u>1.055</u>	<u>.223</u>
1.085	.415
1.096	.585
1.093	.739
<u>1.077</u>	<u>.879</u>
1.051	1.008
1.016	1.126
.972	1.235
.922	1.335
.866	1.426
.804	1.509
.737	1.584
.665	1.651
.590	1.709
.512	1.760
.431	1.803
.347	1.838
.262	1.866
.175	1.885
.088	1.897
<u>-.000</u>	<u>1.901</u>

Figure 8. Continued. (j)

B/A 1.000	P 1.258	L/A 1.749	L/A 5.250	H/A 2.000	W/A 2.236
--------------	------------	--------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.065	.236
1.102	.438
1.118	.617
1.118	.779
1.105	.926
1.080	1.061
1.046	1.186
1.003	1.300
.952	1.405
.895	1.501
.831	1.588
.763	1.667
.689	1.737
.612	1.799
.531	1.852
.447	1.897
.360	1.934
.272	1.963
.182	1.983
.091	1.996
-0.000	2.000

Figure 8. Continued. (k)

B/A 1.000	P 1.233	L/A 1.798	L/A 5.487	H/A 2.100	W/A 2.288
--------------	------------	--------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.076	.250
1.119	.462
1.140	.650
1.144	.819
1.133	.974
1.110	1.116
1.076	1.246
1.033	1.366
.982	1.476
.924	1.577
.859	1.668
.789	1.751
.713	1.824
.633	1.889
.550	1.945
.463	1.993
.373	2.031
.282	2.062
.188	2.083
.094	2.096
-0.000	2.100

Figure 8. Continued. (l)

B/A	P	LA	L/A	H/A	W/A
<u>1.000</u>	<u>1.211</u>	<u>1.849</u>	<u>5.725</u>	<u>2.201</u>	<u>2.339</u>

X/A	Y/A
<u>1.000</u>	<u>.000</u>
<u>1.083</u>	<u>.253</u>
<u>1.133</u>	<u>.468</u>
<u>1.161</u>	<u>.658</u>
<u>1.170</u>	<u>.829</u>
<u>1.164</u>	<u>.986</u>
<u>1.147</u>	<u>1.131</u>
<u>1.118</u>	<u>1.264</u>
<u>1.080</u>	<u>1.388</u>
<u>1.034</u>	<u>1.501</u>
<u>.981</u>	<u>1.606</u>
<u>.921</u>	<u>1.701</u>
<u>.855</u>	<u>1.788</u>
<u>.783</u>	<u>1.867</u>
<u>.707</u>	<u>1.937</u>
<u>.628</u>	<u>1.999</u>
<u>.544</u>	<u>2.052</u>
<u>.458</u>	<u>2.098</u>
<u>.369</u>	<u>2.135</u>
<u>.278</u>	<u>2.164</u>
<u>.186</u>	<u>2.184</u>
<u>.093</u>	<u>2.196</u>
<u>-.001</u>	<u>2.201</u>

Figure 8. Continued. (m)

B/A	P	LA	L/A	H/A	W/A
<u>1.000</u>	<u>1.190</u>	<u>1.898</u>	<u>5.959</u>	<u>2.299</u>	<u>2.390</u>

X/A	Y/A
<u>1.000</u>	<u>.000</u>
<u>1.094</u>	<u>.266</u>
<u>1.151</u>	<u>.491</u>
<u>1.182</u>	<u>.689</u>
<u>1.195</u>	<u>.868</u>
<u>1.192</u>	<u>1.032</u>
<u>1.176</u>	<u>1.183</u>
<u>1.149</u>	<u>1.322</u>
<u>1.111</u>	<u>1.450</u>
<u>1.065</u>	<u>1.569</u>
<u>1.010</u>	<u>1.678</u>
<u>.949</u>	<u>1.778</u>
<u>.882</u>	<u>1.868</u>
<u>.809</u>	<u>1.950</u>
<u>.731</u>	<u>2.024</u>
<u>.648</u>	<u>2.088</u>
<u>.562</u>	<u>2.144</u>
<u>.473</u>	<u>2.191</u>
<u>.382</u>	<u>2.230</u>
<u>.288</u>	<u>2.260</u>
<u>.193</u>	<u>2.281</u>
<u>.097</u>	<u>2.294</u>
<u>-.000</u>	<u>2.299</u>

Figure 8. Continued. (n)

B/A	P	LA	L/A	H/A	W/A
1.000	1.172	1.949	6.200	2.399	2.442

X/A	Y/A
1.000	.000
1.104	.280
1.168	.515
1.205	.722
1.221	.908
1.221	1.079
1.206	1.236
1.179	1.381
1.142	1.515
1.095	1.638
1.040	1.752
.978	1.856
.909	1.950
.834	2.036
.754	2.112
.669	2.179
.580	2.237
.489	2.287
.394	2.327
.297	2.358
.199	2.381
.099	2.394
-.001	2.399

Figure 8. Continued. (o)

B/A	P	LA	L/A	H/A	W/A
1.000	1.155	2.000	6.438	2.497	2.498

X/A	Y/A
1.000	.000
1.115	.293
1.186	.538
1.227	.754
1.247	.948
1.249	1.125
1.236	1.288
1.210	1.439
1.173	1.578
1.126	1.706
1.070	1.824
1.006	1.932
.936	2.031
.859	2.119
.777	2.199
.690	2.269
.599	2.329
.504	2.381
.407	2.423
.307	2.455
.205	2.479
.103	2.493
-.000	2.497

Figure 8. Continued. (p)

B/A	P	L/A	L/A	H/A	W/A
1.000	1.139	2.051	6.679	2.596	2.555

X/A	Y/A
1.000	.000
1.126	.307
1.204	.563
1.250	.786
1.273	.988
1.278	1.172
1.266	1.341
1.241	1.497
1.204	1.642
1.157	1.775
1.100	1.897
1.035	2.009
.963	2.112
.884	2.204
.800	2.285
.711	2.359
.617	2.422
.520	2.475
.419	2.519
.317	2.553
.212	2.577
.106	2.591
-.000	2.596

Figure 8. Continued. (q)

B/A	P	L/A	L/A	H/A	W/A
1.000	1.125	2.103	6.922	2.696	2.613

X/A	Y/A
1.000	.000
1.132	.309
1.216	.565
1.268	.791
1.297	.993
1.307	1.179
1.300	1.350
1.281	1.508
1.249	1.655
1.207	1.791
1.156	1.917
1.097	2.033
1.030	2.139
.956	2.236
.877	2.323
.792	2.402
.703	2.471
.610	2.530
.513	2.581
.414	2.622
.312	2.655
.209	2.678
.105	2.691
-.000	2.696

Figure 8. Continued. (r)

B/A 1.000	P 1.111	LA 2.155	L/A 7.169	H/A 2.797	W/A 2.671
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.143	.323
1.234	.590
1.291	.823
1.323	1.033
1.336	1.225
1.331	1.403
1.312	1.567
1.281	1.719
1.239	1.859
1.187	1.990
1.127	2.110
1.058	2.220
.983	2.320
.902	2.411
.815	2.492
.723	2.563
.628	2.625
.528	2.677
.426	2.720
.322	2.754
.215	2.778
.108	2.792
.000	2.797

Figure 8. Continued. (s)

B/A 1.000	P 1.099	LA 2.210	L/A 7.424	H/A 2.900	W/A 2.731
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.155	.338
1.253	.615
1.315	.857
1.351	1.075
1.365	1.274
1.362	1.457
1.345	1.627
1.314	1.784
1.271	1.930
1.219	2.065
1.157	2.189
1.088	2.303
1.011	2.407
.927	2.501
.838	2.584
.744	2.658
.645	2.723
.543	2.777
.438	2.821
.331	2.856
.221	2.881
.111	2.895
.000	2.900

Figure 8. Continued. (t)

B/A <u>1.000</u>	P <u>1.090</u>	L/A <u>2.247</u>	L/A <u>7.597</u>	H/A <u>2.971</u>	W/A <u>2.772</u>
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X/A	Y/A
<u>1.000</u>	<u>.000</u>
<u>1.163</u>	<u>.348</u>
<u>1.266</u>	<u>.632</u>
<u>1.332</u>	<u>.880</u>
<u>1.370</u>	<u>1.103</u>
<u>1.386</u>	<u>1.306</u>
<u>1.384</u>	<u>1.494</u>
<u>1.367</u>	<u>1.667</u>
<u>1.337</u>	<u>1.828</u>
<u>1.294</u>	<u>1.977</u>
<u>1.241</u>	<u>2.115</u>
<u>1.179</u>	<u>2.242</u>
<u>1.108</u>	<u>2.359</u>
<u>1.030</u>	<u>2.465</u>
<u>.945</u>	<u>2.561</u>
<u>.855</u>	<u>2.647</u>
<u>.759</u>	<u>2.723</u>
<u>.659</u>	<u>2.789</u>
<u>.555</u>	<u>2.844</u>
<u>.448</u>	<u>2.890</u>
<u>.338</u>	<u>2.925</u>
<u>.227</u>	<u>2.950</u>
<u>.114</u>	<u>2.965</u>
<u>.001</u>	<u>2.971</u>

Figure 8. Continued. (u)

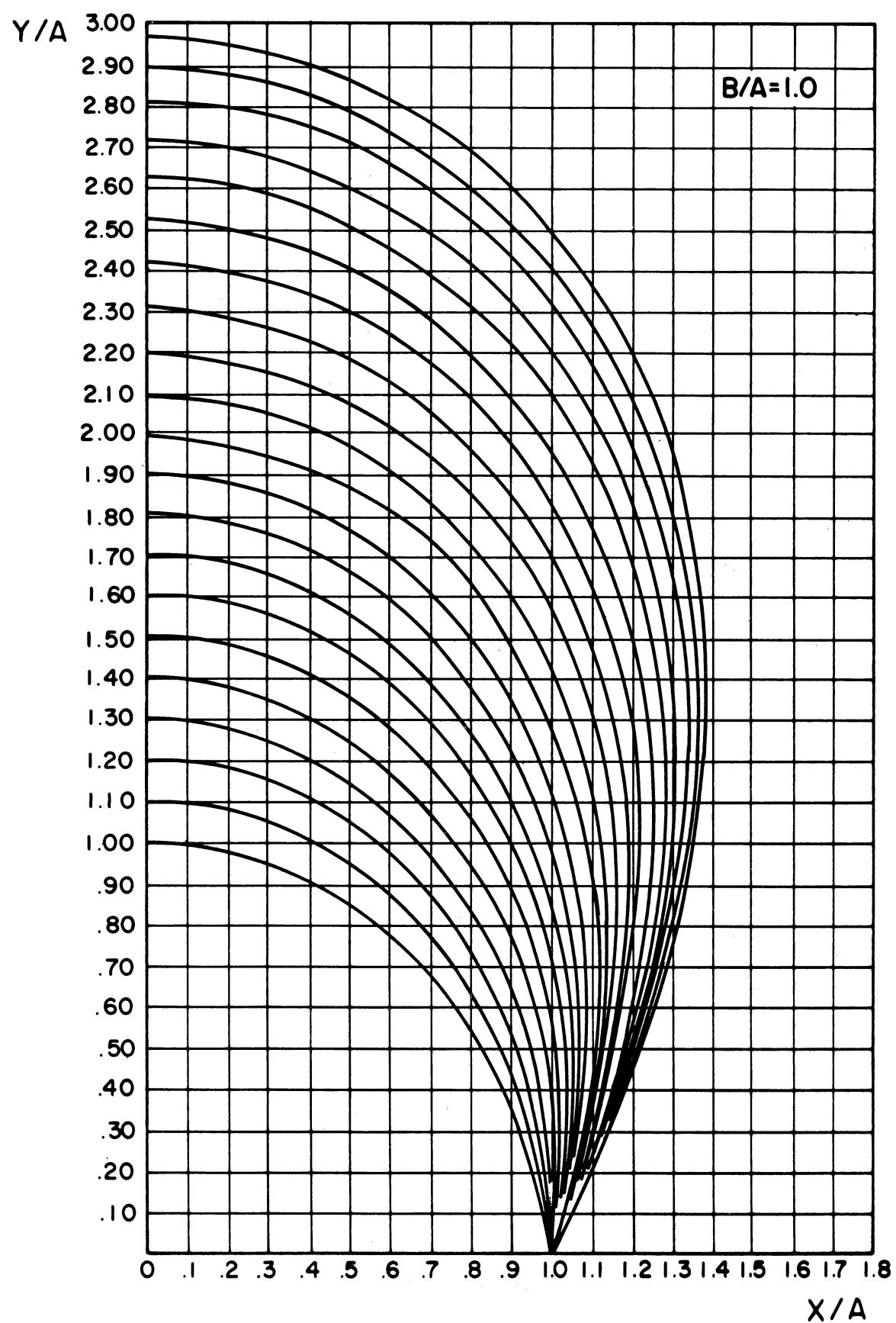


Figure 8. Concluded. (v)

B/A	P	LA	L/A	H/A	W/A
<u>1.250</u>	1.708	<u>1.425</u>	<u>3.097</u>	<u>1.001</u>	<u>2.000</u>

X/A	Y/A
1.000	.000
.975	.136
<u>.941</u>	<u>.257</u>
.900	.366
.853	.464
.800	.553
.741	.632
<u>.679</u>	<u>.704</u>
.613	.767
.543	.822
.471	.870
<u>.396</u>	<u>.910</u>
.319	.943
.241	.968
.161	.987
.081	.997
<u>.000</u>	<u>1.001</u>

Figure 9. (a)

B/A	P	LA	L/A	H/A	W/A
<u>1.250</u>	1.632	<u>1.453</u>	<u>3.287</u>	<u>1.100</u>	<u>2.000</u>

X/A	Y/A
1.000	.000
.985	.141
<u>.960</u>	<u>.267</u>
.927	.382
.887	.485
.840	.579
.788	.665
<u>.731</u>	<u>.742</u>
.669	.811
.604	.872
.536	.926
.464	.972
.391	1.012
<u>.315</u>	<u>1.044</u>
.238	1.068
.159	1.086
.080	1.097
<u>.000</u>	<u>1.100</u>

Figure 9. Continued (b)

B/A	P	LA	L/A	H/A	W/A
1.250	1.564	1.485	3.485	1.199	2.000

X/A	Y/A
1.000	.000
.995	.146
.978	.277
.953	.396
.919	.504
.879	.604
.832	.694
.780	.776
.724	.851
.663	.918
.598	.977
.530	1.029
.460	1.075
.387	1.113
.312	1.144
.235	1.168
.158	1.186
.079	1.196
.000	1.199

Figure 9. Continued. (c)

B/A	P	LA	L/A	H/A	W/A
1.250	1.504	1.521	3.691	1.299	2.007

X/A	Y/A
1.000	.000
1.004	.158
.994	.300
.973	.429
.943	.548
.905	.653
.859	.751
.808	.840
.751	.921
.689	.993
.623	1.058
.553	1.114
.480	1.164
.404	1.205
.326	1.239
.246	1.265
.165	1.284
.083	1.295
.001	1.299

Figure 9. Continued. (d)

B/A	P	LA	L/A	H/A	W/A
<u>1.250</u>	<u>1.450</u>	<u>1.561</u>	<u>3.906</u>	<u>1.400</u>	<u>2.025</u>

X/A	Y/A
<u>1.000</u>	<u>.000</u>
<u>1.013</u>	<u>.162</u>
<u>1.011</u>	<u>.308</u>
<u>.997</u>	<u>.441</u>
<u>.974</u>	<u>.563</u>
<u>.942</u>	<u>.674</u>
<u>.902</u>	<u>.777</u>
<u>.856</u>	<u>.870</u>
<u>.804</u>	<u>.956</u>
<u>.747</u>	<u>1.034</u>
<u>.685</u>	<u>1.104</u>
<u>.619</u>	<u>1.166</u>
<u>.549</u>	<u>1.221</u>
<u>.476</u>	<u>1.269</u>
<u>.401</u>	<u>1.309</u>
<u>.323</u>	<u>1.342</u>
<u>.244</u>	<u>1.367</u>
<u>.164</u>	<u>1.385</u>
<u>.082</u>	<u>1.396</u>
<u>.000</u>	<u>1.400</u>

Figure 9. Continued. (e)

B/A	P	LA	L/A	H/A	W/A
<u>1.250</u>	<u>1.402</u>	<u>1.603</u>	<u>4.125</u>	<u>1.500</u>	<u>2.053</u>

X/A	Y/A
<u>1.000</u>	<u>.000</u>
<u>1.022</u>	<u>.175</u>
<u>1.027</u>	<u>.331</u>
<u>1.018</u>	<u>.473</u>
<u>.998</u>	<u>.603</u>
<u>.969</u>	<u>.722</u>
<u>.931</u>	<u>.832</u>
<u>.885</u>	<u>.932</u>
<u>.833</u>	<u>1.024</u>
<u>.775</u>	<u>1.107</u>
<u>.712</u>	<u>1.182</u>
<u>.644</u>	<u>1.249</u>
<u>.572</u>	<u>1.308</u>
<u>.490</u>	<u>1.359</u>
<u>.418</u>	<u>1.402</u>
<u>.338</u>	<u>1.437</u>
<u>.255</u>	<u>1.465</u>
<u>.171</u>	<u>1.484</u>
<u>.086</u>	<u>1.498</u>
<u>.000</u>	<u>1.500</u>

Figure 9. Continued. (f)

B/A	P	LA	L/A	H/A	W/A
1.250	1.360	1.647	4.348	1.600	2.085

X/A	Y/A
1.000	.000
1.030	.178
1.043	.338
1.041	.483
1.028	.617
1.004	.740
.972	.853
.931	.958
.884	1.054
.831	1.142
.772	1.222
.708	1.294
.640	1.358
.568	1.415
.493	1.464
.415	1.506
.335	1.540
.253	1.566
.169	1.585
.085	1.596
.000	1.600

Figure 9. Continued. (g)

B/A	P	LA	L/A	H/A	W/A
1.250	1.322	1.693	4.576	1.701	2.125

X/A	Y/A
1.000	.000
1.039	.190
1.059	.360
1.062	.514
1.053	.656
1.031	.786
1.001	.907
.961	1.018
.914	1.120
.860	1.213
.800	1.298
.735	1.375
.665	1.443
.590	1.504
.512	1.556
.432	1.600
.348	1.636
.263	1.665
.176	1.685
.088	1.697
.000	1.701

Figure 9. Continued. (h)

B/A <u>1.250</u>	P <u>1.229</u>	LA <u>1.835</u>	L/A <u>5.270</u>	H/A <u>1.999</u>	W/A <u>2.261</u>
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X/A	Y/A
1.000	.000
1.066	.216
1.106	.408
1.127	.583
1.130	.743
1.120	.891
1.098	1.028
1.066	1.155
1.025	1.272
.975	1.380
.918	1.480
.854	1.570
.784	1.651
.710	1.724
.631	1.789
.548	1.845
.461	1.892
.372	1.931
.281	1.961
.189	1.982
.095	1.995
.001	1.999

Figure 9. Continued. (k)

B/A <u>1.250</u>	P <u>1.204</u>	LA <u>1.885</u>	L/A <u>5.508</u>	H/A <u>2.100</u>	W/A <u>2.312</u>
---------------------	-------------------	--------------------	---------------------	---------------------	---------------------

X/A	Y/A
1.000	.000
1.073	.218
1.120	.413
1.146	.590
1.156	.752
1.152	.903
1.135	1.043
1.108	1.173
1.072	1.293
1.027	1.405
.975	1.508
.916	1.603
.851	1.689
.780	1.767
.705	1.837
.626	1.898
.543	1.952
.457	1.997
.369	2.034
.278	2.063
.186	2.083
.094	2.096
.000	2.100

Figure 9. Continued. (l)

B/A <u>1.250</u>	P <u>1.180</u>	LA <u>1.938</u>	L/A <u>5.759</u>	H/A <u>2.205</u>	W/A <u>2.366</u>
---------------------	-------------------	--------------------	---------------------	---------------------	---------------------

X/A	Y/A
1.000	.000
1.084	.231
1.138	.435
1.169	.621
1.183	.791
1.181	.949
1.167	1.096
1.141	1.232
1.105	1.359
1.060	1.476
1.007	1.584
.947	1.683
.880	1.774
.808	1.856
.730	1.929
.648	1.993
.563	2.049
.474	2.097
.383	2.136
.289	2.166
.194	2.188
.097	2.201
.000	2.205

Figure 9. Continued. (m)

B/A <u>1.250</u>	P <u>1.158</u>	LA <u>1.992</u>	L/A <u>6.014</u>	H/A <u>2.311</u>	W/A <u>2.422</u>
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X/A	Y/A
1.000	.000
1.094	.243
1.155	.458
1.192	.653
1.210	.831
1.211	.996
1.198	1.150
1.174	1.292
1.138	1.425
1.093	1.547
1.039	1.660
.978	1.764
.909	1.859
.835	1.945
.755	2.021
.671	2.089
.583	2.148
.491	2.197
.396	2.238
.299	2.270
.201	2.292
.101	2.306
.000	2.311

Figure 9. Continued. (n)

B/A 1.250	P 1.139	LA 2.044	L/A 6.263	H/A 2.413	W/A 2.481
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.104	.256
1.173	.481
1.215	.684
1.237	.870
1.241	1.043
1.230	1.203
1.206	1.351
1.171	1.489
1.125	1.617
1.071	1.735
1.008	1.843
.938	1.942
.862	2.032
.780	2.112
.693	2.182
.602	2.243
.507	2.295
.410	2.338
.309	2.371
.207	2.394
.104	2.409
.001	2.413

Figure 9. Continued. (o)

B/A 1.250	P 1.122	LA 2.095	L/A 6.503	H/A 2.512	W/A 2.538
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.111	.257
1.185	.483
1.233	.687
1.260	.875
1.269	1.049
1.264	1.211
1.245	1.362
1.215	1.502
1.175	1.633
1.126	1.754
1.069	1.866
1.004	1.969
.933	2.063
.856	2.148
.773	2.225
.687	2.292
.596	2.350
.502	2.399
.405	2.440
.306	2.471
.205	2.494
.103	2.507
.001	2.512

Figure 9. Continued. (p)

B/A	P	LA	L/A	H/A	W/A
1.250	1.107	2.144	6.732	2.606	2.592

X/A	Y/A
1.000	.000
1.120	.268
1.201	.503
1.254	.715
1.284	.910
1.296	1.090
1.292	1.258
1.275	1.414
1.245	1.560
1.205	1.695
1.155	1.821
1.097	1.937
1.031	2.044
.959	2.141
.880	2.229
.795	2.308
.706	2.378
.613	2.438
.516	2.489
.417	2.531
.315	2.564
.211	2.587
.106	2.601
.001	2.606

Figure 9. Continued. (q)

B/A	P	LA	L/A	H/A	W/A
1.250	1.095	2.191	6.952	2.695	2.643

X/A	Y/A
1.000	.000
1.129	.279
1.216	.523
1.273	.742
1.307	.944
1.321	1.130
1.319	1.303
1.303	1.464
1.274	1.615
1.233	1.754
1.183	1.884
1.124	2.004
1.057	2.114
.983	2.215
.902	2.306
.816	2.387
.724	2.459
.629	2.522
.530	2.575
.427	2.618
.323	2.652
.216	2.676
.109	2.690
.001	2.695

Figure 9. Continued. (r)

B/A	P	LA	L/A	H/A	W/A
1.250	1.084	2.234	7.153	2.777	2.690

X/A	Y/A
1.000	.000
1.138	.289
1.231	.541
1.292	.767
1.328	.974
1.345	.166
1.344	1.344
1.328	1.510
1.300	1.665
1.259	1.809
1.209	1.942
1.149	2.066
1.081	2.179
1.005	2.283
.923	2.376
.835	2.460
.741	2.534
.644	2.598
.542	2.653
.438	2.697
.330	2.732
.222	2.757
.111	2.772
.001	2.777

Figure 9. Continued. (s)

B/A	P	LA	L/A	H/A	W/A
1.250	1.074	2.275	7.345	2.854	2.735

X/A	Y/A
1.000	.000
1.146	.299
1.244	.558
1.309	.791
1.349	1.004
1.367	1.201
1.368	1.384
1.353	1.554
1.324	1.713
1.284	1.860
1.233	1.998
1.172	2.124
1.103	2.241
1.026	2.347
.942	2.443
.852	2.529
.757	2.605
.657	2.671
.554	2.727
.447	2.773
.337	2.808
.226	2.834
.114	2.849
.000	2.854

Figure 9. Continued. (t)

B/A	P	L/A	L/A	H/A	W/A
<u>1.250</u>	<u>1.065</u>	<u>2.314</u>	<u>7.527</u>	<u>2.928</u>	<u>2.780</u>

X/A	Y/A
1.000	.000
1.153	.308
1.257	.575
1.326	.813
1.368	1.032
1.388	1.234
1.390	1.421
1.376	1.596
1.348	1.758
1.307	1.910
1.256	2.050
1.194	2.180
1.124	2.299
1.046	2.408
.961	2.507
.869	2.595
.772	2.673
.670	2.740
.565	2.798
.456	2.845
.344	2.881
.231	2.907
.116	2.923
.000	2.928

Figure 9. Continued. (u)

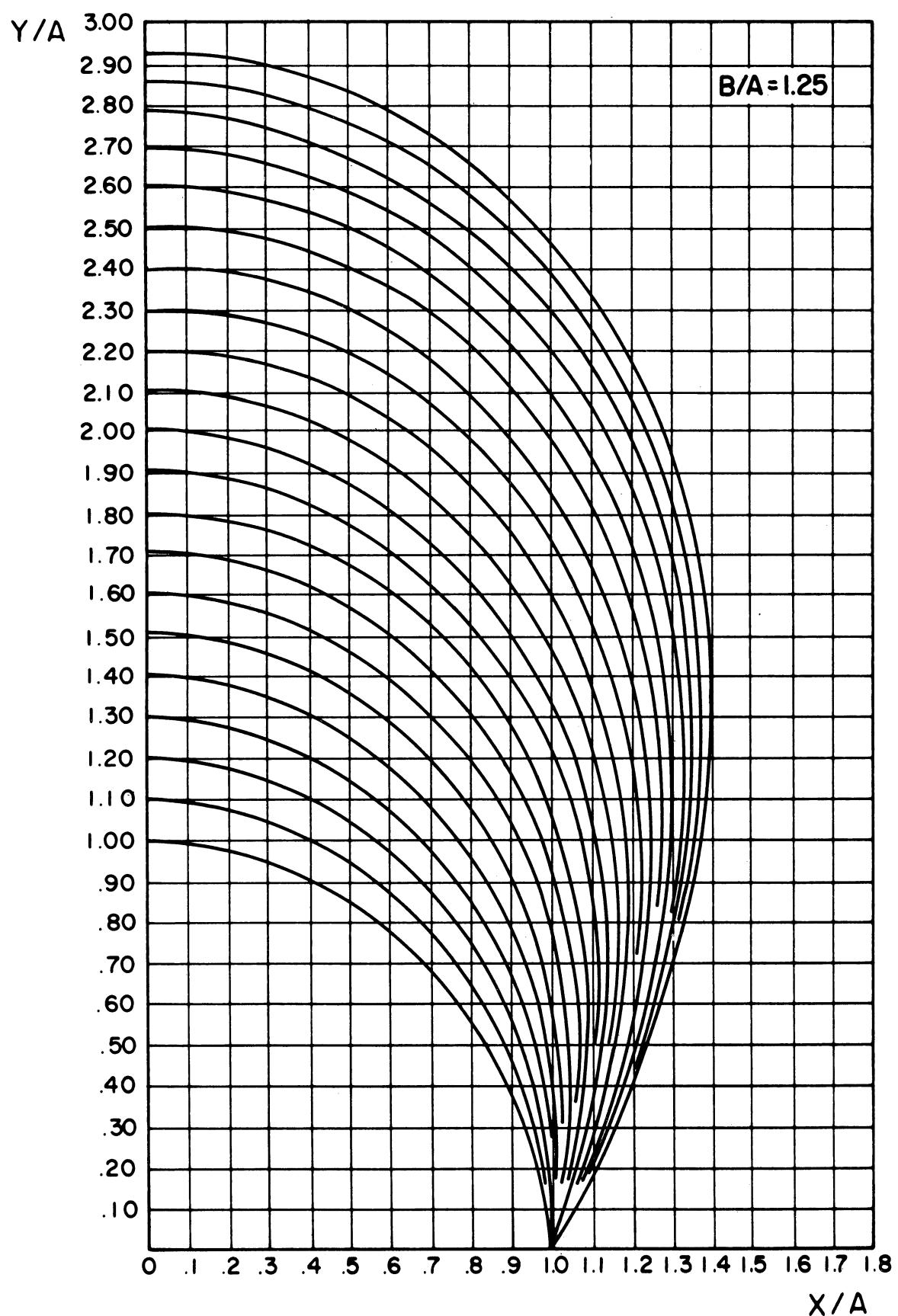


Figure 9. Concluded. (v)

B/A	P	LA	L/A	H/A	W/A
<u>1.500</u>	<u>1.694</u>	<u>1.509</u>	<u>3.098</u>	<u>1.000</u>	<u>2.000</u>

X/A	Y/A
1.000	.000
.978	.130
.947	.248
.908	.355
.862	.453
.810	.542
.752	.623
.690	.695
.623	.759
.553	.816
.480	.865
.404	.906
.326	.940
.246	.966
.165	.985
.083	.996
.001	1.000

Figure 10. (a)

B/A	P	LA	L/A	H/A	W/A
<u>1.500</u>	<u>1.615</u>	<u>1.537</u>	<u>3.293</u>	<u>1.101</u>	<u>2.000</u>

X/A	Y/A
1.000	.000
.988	.135
.966	.258
.935	.370
.896	.474
.851	.568
.799	.654
.742	.732
.681	.803
.615	.866
.546	.921
.474	.969
.399	1.009
.322	1.042
.243	1.068
.163	1.086
.082	1.097
.000	1.101

Figure 10. Continued. (b)

B/A	P	LA	L/A	H/A	W/A
<u>1.500</u>	<u>1.546</u>	<u>1.569</u>	<u>3.496</u>	<u>1.201</u>	<u>2.000</u>

X/A	Y/A
1.000	.000
.997	.139
<u>.984</u>	<u>.266</u>
.960	.384
.929	.492
.890	.591
.844	.682
<u>.793</u>	<u>.766</u>
.736	.842
.675	.910
.610	.972
.541	1.025
.470	1.072
<u>.395</u>	<u>1.112</u>
.319	1.144
.241	1.169
.161	1.187
.081	1.197
.000	1.201

Figure 10. Continued. (c)

B/A	P	LA	L/A	H/A	W/A
<u>1.500</u>	<u>1.485</u>	<u>1.604</u>	<u>3.701</u>	<u>1.300</u>	<u>2.012</u>

X/A	Y/A
1.000	.000
<u>1.006</u>	<u>.150</u>
.999	.288
.981	.414
.953	.531
.916	.639
.872	.737
<u>.821</u>	<u>.828</u>
.765	.910
.703	.984
.636	1.051
.565	1.109
.491	1.160
<u>.414</u>	<u>1.203</u>
.334	1.238
.252	1.265
.169	1.284
.085	1.296
.001	1.300

Figure 10. Continued. (d)

B/A	P	LA	L/A	H/A	W/A
1.500	1.430	1.643	3.915	1.399	2.031

X/A	Y/A
1.000	.000
1.015	.153
1.016	.295
1.005	.425
.983	.545
.953	.657
.915	.760
.870	.855
.818	.943
.761	1.022
.693	1.094
.632	1.158
.561	1.214
.487	1.264
.410	1.305
.331	1.339
.250	1.365
.180	1.384
.084	1.390
.001	1.399

Figure 10. Continued. (e)

B/A	P	LA	L/A	H/A	W/A
1.500	1.382	1.685	4.135	1.500	2.063

X/A	Y/A
1.000	.000
1.023	.157
1.031	.301
1.027	.435
1.012	.559
.988	.674
.955	.782
.916	.881
.869	.973
.816	1.057
.758	1.134
.696	1.203
.625	1.263
.553	1.320
.484	1.365
.408	1.408
.329	1.441
.248	1.467
.166	1.485
.084	1.496
.000	1.500

Figure 10. Continued. (f)

B/A	P	LA	L/A	H/A	W/A
1.500	1.338	1.729	4.360	1.600	2.096

X/A	Y/A
1.000	.000
1.032	.167
1.047	.321
1.048	.463
1.037	.596
1.016	.719
.985	.833
.946	.939
.899	1.037
.846	1.127
.787	1.209
.723	1.283
.654	1.349
.581	1.408
.505	1.459
.425	1.502
.343	1.537
.259	1.564
.174	1.584
.087	1.596
.000	1.600

Figure 10. Continued. (g)

B/A	P	LA	L/A	H/A	W/A
1.500	1.299	1.775	4.589	1.701	2.139

X/A	Y/A
1.000	.000
1.040	.170
1.062	.326
1.069	.472
1.065	.607
1.049	.734
1.024	.851
.990	.961
.949	1.063
.901	1.157
.846	1.244
.786	1.323
.721	1.395
.652	1.459
.579	1.515
.502	1.564
.423	1.606
.341	1.640
.257	1.666
.173	1.685
.087	1.697
.000	1.701

Figure 10. Continued. (h)

B/A	P	LA	L/A	H/A	W/A
<u>1.500</u>	<u>1.264</u>	<u>1.822</u>	<u>4.820</u>	<u>1.800</u>	<u>2.181</u>

X/A	Y/A
1.000	.000
<u>1.048</u>	<u>.180</u>
<u>1.078</u>	<u>.346</u>
<u>1.090</u>	<u>.500</u>
<u>1.090</u>	<u>.643</u>
<u>1.077</u>	<u>.777</u>
<u>1.054</u>	<u>.901</u>
<u>1.021</u>	<u>1.017</u>
.980	1.125
.931	1.225
.876	1.317
.815	1.400
.748	1.476
<u>.677</u>	<u>1.544</u>
.601	1.604
.522	1.656
.440	1.700
.355	1.736
.268	1.764
.180	1.784
.090	1.796
.001	1.800

Figure 10. Continued. (i)

B/A	P	LA	L/A	H/A	W/A
<u>1.500</u>	<u>1.233</u>	<u>1.871</u>	<u>5.057</u>	<u>1.902</u>	<u>2.230</u>

X/A	Y/A
1.000	.000
<u>1.058</u>	<u>.191</u>
<u>1.094</u>	<u>.366</u>
<u>1.112</u>	<u>.528</u>
<u>1.115</u>	<u>.679</u>
<u>1.105</u>	<u>.820</u>
<u>1.083</u>	<u>.952</u>
<u>1.052</u>	<u>1.074</u>
1.011	1.188
.962	1.293
.906	1.390
.844	1.479
.775	1.559
.702	1.630
.624	1.694
.542	1.749
.456	1.795
.368	1.834
.278	1.863
.186	1.885
.093	1.897
.000	1.902

Figure 10. Continued. (j)

B/A	P	L/A	L/A	H/A	W/A
1.500	1.205	1.919	5.290	2.000	2.280

X/A	Y/A
1.000	.000
1.064	.193
1.107	.370
1.131	.534
1.140	.687
1.136	.831
1.120	.965
1.093	1.090
1.058	1.207
1.014	1.316
.963	1.417
.905	1.510
.841	1.595
.772	1.671
.698	1.740
.620	1.801
.538	1.854
.453	1.898
.365	1.935
.276	1.963
.185	1.984
.093	1.996
.000	2.000

Figure 10. Continued. (k)

B/A	D	L/A	L/A	H/A	W/A
1.500	1.179	1.971	5.538	2.104	2.332

X/A	Y/A
1.000	.000
1.074	.203
1.123	.390
1.153	.563
1.166	.724
1.165	.875
1.151	1.016
1.126	1.147
1.091	1.270
1.047	1.385
.995	1.491
.936	1.588
.871	1.677
.800	1.758
.723	1.830
.642	1.894
.558	1.950
.470	1.997
.379	2.035
.286	2.065
.192	2.087
.096	2.100
.000	2.104

Figure 10. Continued. (l)

B/A	P	LA	L/A	H/A	W/A
1.500	1.155	2.022	5.781	2.205	2.387

X/A	Y/A
1.000	.000
1.083	.214
1.140	.410
1.175	.591
1.192	.760
1.194	.917
1.182	1.065
1.158	1.203
1.124	1.332
1.080	1.452
1.027	1.563
.967	1.665
.900	1.758
.827	1.843
.749	1.918
.665	1.985
.578	2.044
.487	2.093
.393	2.133
.297	2.165
.199	2.187
.100	2.201
.001	2.205

Figure 10. Continued. (m)

B/A	P	LA	L/A	H/A	W/A
1.500	1.134	2.074	6.031	2.308	2.446

X/A	Y/A
1.000	.000
1.090	.216
1.152	.413
1.193	.596
1.216	.767
1.223	.927
1.217	1.077
1.198	1.217
1.169	1.349
1.131	1.472
1.083	1.587
1.028	1.693
.966	1.790
.897	1.880
.823	1.961
.744	2.033
.661	2.098
.573	2.153
.483	2.200
.389	2.239
.294	2.269
.197	2.291
.099	2.304
.000	2.308

Figure 10. Continued. (n)

B/A 1.500	P 1.115	LA 2.125	L/A 6.270	H/A 2.406	W/A 2.502
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.099	.226
1.168	.432
1.214	.623
1.241	.801
1.251	.967
1.246	1.124
1.229	1.270
1.201	1.407
1.162	1.536
1.114	1.655
1.058	1.765
.995	1.867
.925	1.960
.849	2.045
.767	2.120
.681	2.187
.592	2.245
.498	2.294
.402	2.335
.304	2.366
.203	2.388
.102	2.402
.000	2.406

Figure 10. Continued. (o)

B/A 1.500	P 1.099	LA 2.174	L/A 6.500	H/A 2.500	W/A 2.555
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.108	.236
1.184	.451
1.235	.649
1.265	.834
1.277	1.007
1.275	1.169
1.259	1.321
1.231	1.463
1.192	1.596
1.144	1.720
1.087	1.835
1.023	1.941
.951	2.037
.873	2.125
.790	2.203
.701	2.273
.609	2.333
.513	2.384
.414	2.426
.313	2.458
.210	2.482
.105	2.496
.000	2.500

Figure 10. Continued. (p)

B/A	P	LA	L/A	H/A	W/A
1.500	1.084	2.221	6.721	2.590	2.606

X/A	Y/A
1.000	.000
1.117	.246
1.199	.469
1.254	.674
1.288	.866
1.303	1.045
1.302	1.212
1.287	1.370
1.260	1.517
1.221	1.655
1.173	1.783
1.115	1.901
1.049	2.011
.976	2.111
.896	2.201
.811	2.282
.721	2.354
.626	2.417
.527	2.469
.425	2.513
.321	2.546
.215	2.570
.108	2.585
.001	2.590

Figure 10. Continued.. (q)

B/A	P	LA	L/A	H/A	W/A
1.500	1.072	2.266	6.931	2.675	2.657

X/A	Y/A
1.000	.000
1.125	.255
1.213	.486
1.273	.698
1.310	.896
1.328	1.081
1.328	1.254
1.314	1.416
1.288	1.568
1.249	1.710
1.200	1.842
1.141	1.965
1.074	2.078
1.000	2.181
.919	2.274
.831	2.358
.739	2.432
.642	2.496
.541	2.551
.437	2.596
.330	2.630
.221	2.655
.111	2.670
.001	2.675

Figure 10. Continued. (r)

B/A	P	L/A	L/A	H/A	W/A
<u>1.500</u>	<u>1.060</u>	<u>2.311</u>	<u>7.142</u>	<u>2.760</u>	<u>2.709</u>

X/A	Y/A
<u>1.000</u>	<u>.000</u>
<u>1.133</u>	<u>.264</u>
<u>1.227</u>	<u>.503</u>
<u>1.292</u>	<u>.723</u>
<u>1.332</u>	<u>.926</u>
<u>1.352</u>	<u>1.117</u>
<u>1.354</u>	<u>1.295</u>
<u>1.341</u>	<u>1.463</u>
<u>1.315</u>	<u>1.619</u>
<u>1.276</u>	<u>1.766</u>
<u>1.227</u>	<u>1.902</u>
<u>1.167</u>	<u>2.028</u>
<u>1.099</u>	<u>2.144</u>
<u>1.023</u>	<u>2.250</u>
<u>.941</u>	<u>2.347</u>
<u>.851</u>	<u>2.433</u>
<u>.757</u>	<u>2.510</u>
<u>.657</u>	<u>2.576</u>
<u>.554</u>	<u>2.632</u>
<u>.447</u>	<u>2.678</u>
<u>.338</u>	<u>2.714</u>
<u>.226</u>	<u>2.740</u>
<u>.114</u>	<u>2.755</u>
<u>.000</u>	<u>2.760</u>

Figure 10. Continued. (s)

B/A	P	L/A	L/A	H/A	W/A
<u>1.500</u>	<u>1.049</u>	<u>2.356</u>	<u>7.352</u>	<u>2.845</u>	<u>2.761</u>

X/A	Y/A
<u>1.000</u>	<u>.000</u>
<u>1.142</u>	<u>.274</u>
<u>1.242</u>	<u>.520</u>
<u>1.311</u>	<u>.747</u>
<u>1.354</u>	<u>.957</u>
<u>1.376</u>	<u>1.153</u>
<u>1.380</u>	<u>1.337</u>
<u>1.368</u>	<u>1.509</u>
<u>1.342</u>	<u>1.670</u>
<u>1.304</u>	<u>1.821</u>
<u>1.254</u>	<u>1.961</u>
<u>1.194</u>	<u>2.091</u>
<u>1.124</u>	<u>2.211</u>
<u>1.047</u>	<u>2.320</u>
<u>.962</u>	<u>2.419</u>
<u>.871</u>	<u>2.508</u>
<u>.775</u>	<u>2.587</u>
<u>.673</u>	<u>2.655</u>
<u>.567</u>	<u>2.713</u>
<u>.458</u>	<u>2.760</u>
<u>.346</u>	<u>2.797</u>
<u>.232</u>	<u>2.824</u>
<u>.117</u>	<u>2.840</u>
<u>.000</u>	<u>2.845</u>

Figure 10. Continued. (t)

B/A	P	L/A	L/A	H/A	W/A
1.500	1.039	2.403	7.571	2.933	2.816

X/A	Y/A
1.000	.000
1.145	.273
1.250	.518
1.323	.744
1.371	.954
1.399	1.150
1.408	1.334
1.402	1.507
1.381	1.670
1.348	1.822
1.304	1.964
1.250	2.097
1.187	2.220
1.116	2.333
1.037	2.437
.951	2.530
.860	2.615
.764	2.689
.663	2.754
.558	2.808
.450	2.853
.340	2.888
.228	2.913
.115	2.928
.001	2.933

Figure 10. Continued. (u)

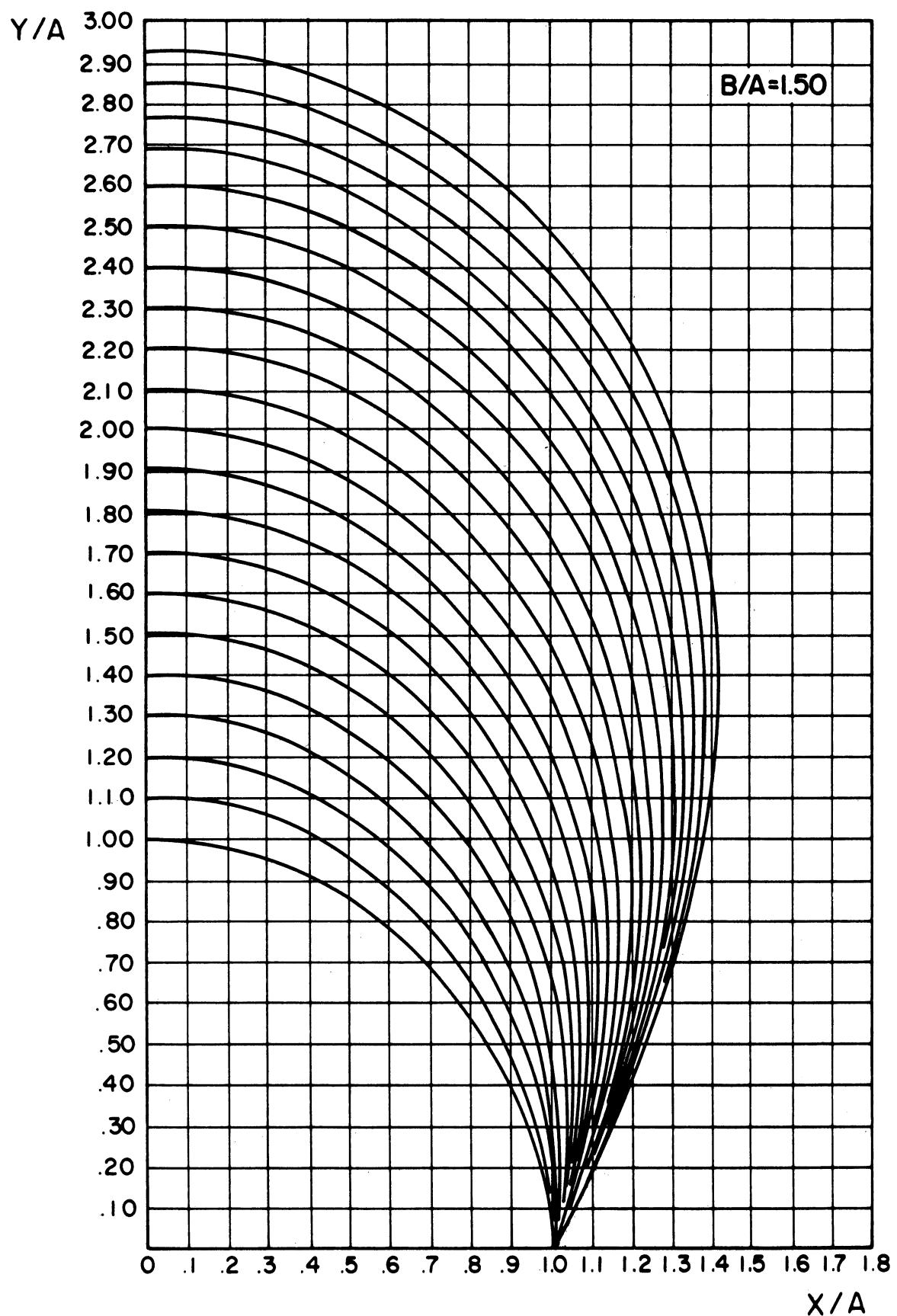


Figure 10. Concluded. (v)

B/A	P	LA	L/A	H/A	W/A
1.750	1.681	1.591	3.104	1.000	2.000

X/A	Y/A
1.000	.000
.980	.126
.951	.242
.914	.348
.869	.446
.818	.535
.760	.616
.698	.690
.632	.755
.561	.813
.487	.862
.410	.905
.331	.939
.250	.966
.168	.985
.084	.997
.000	1.000

Figure 11. (a)

B/A	P	LA	L/A	H/A	W/A
1.750	1.602	1.616	3.296	1.100	2.000

X/A	Y/A
1.000	.000
.990	.130
.970	.250
.941	.361
.903	.464
.859	.559
.808	.645
.752	.724
.690	.796
.624	.860
.555	.916
.482	.965
.406	1.006
.328	1.040
.247	1.066
.166	1.085
.083	1.096
.001	1.100

Figure 11. Continued. (b)

B/A	P	LA	L/A	H/A	W/A
1.750	1.532	1.647	3.499	1.200	2.000

X/A	Y/A
1.000	.000
.999	.134
.988	.258
.966	.373
.936	.480
.898	.580
.853	.672
.803	.756
.746	.833
.685	.903
.620	.965
.550	1.020
.478	1.068
.402	1.108
.325	1.141
.245	1.167
.165	1.185
.083	1.196
.001	1.200

Figure 11. Continued. (c)

B/A	P	LA	L/A	H/A	W/A
1.750	1.469	1.684	3.710	1.301	2.016

X/A	Y/A
1.000	.000
1.008	.137
1.004	.265
.990	.384
.967	.496
.935	.599
.896	.696
.851	.785
.800	.867
.743	.942
.682	1.010
.616	1.071
.547	1.125
.475	1.171
.400	1.211
.323	1.243
.244	1.268
.163	1.286
.082	1.297
.000	1.301

Figure 11. Continued. (d)

B/A	P	LA	L/A	H/A	W/A
<u>1.750</u>	<u>1.414</u>	<u>1.723</u>	<u>3.926</u>	<u>1.400</u>	<u>2.039</u>

X/A	Y/A
1.000	.000
1.017	.147
1.019	.284
1.010	.412
.991	.532
.962	.644
.925	.748
.881	.844
.829	.932
.772	1.013
.710	1.087
.642	1.152
.571	1.210
.496	1.261
.418	1.303
.337	1.338
.255	1.365
.171	1.385
.086	1.397
.000	1.400

Figure 11. Continued. (e)

B/A	P	LA	L/A	H/A	W/A
<u>1.750</u>	<u>1.364</u>	<u>1.764</u>	<u>4.144</u>	<u>1.499</u>	<u>2.070</u>

X/A	Y/A
1.000	.000
1.025	.149
1.035	.289
1.033	.421
1.020	.544
.997	.659
.966	.767
.927	.867
.881	.960
.829	1.046
.771	1.124
.708	1.195
.640	1.259
.569	1.315
.494	1.364
.416	1.405
.338	1.439
.254	1.465
.170	1.484
.086	1.496
.001	1.499

Figure 11. Continued. (f)

B/A	P	LA	L/A	H/A	W/A
<u>1.750</u>	<u>1.32C</u>	<u>1.808</u>	<u>4.369</u>	<u>1.599</u>	<u>2.107</u>

X/A	Y/A
1.000	.000
<u>1.033</u>	<u>.159</u>
1.050	.308
1.054	.448
1.045	.579
1.025	.702
.996	.817
.958	.924
.912	1.023
.859	1.114
.800	1.198
.736	1.274
.666	1.342
.592	1.402
.515	1.454
.434	1.498
.350	1.535
<u>.265</u>	<u>1.563</u>
.178	1.583
.089	1.595
.001	1.599

Figure 11. Continued. (g)

B/A	P	LA	L/A	H/A	W/A
<u>1.750</u>	<u>1.281</u>	<u>1.853</u>	<u>4.599</u>	<u>1.699</u>	<u>2.149</u>

X/A	Y/A
1.000	.000
<u>1.041</u>	<u>.161</u>
1.065	.313
1.074	.455
1.072	.589
<u>1.058</u>	<u>.715</u>
1.035	.833
1.002	.944
.962	1.047
.914	1.143
.860	1.231
.799	1.312
.734	1.385
.664	1.451
.590	1.509
.512	1.559
.431	1.602
.348	1.637
.263	1.664
<u>.176</u>	<u>1.684</u>
.089	1.696
.000	1.699

Figure 11. Continued. (h)

B/A	P	LA	L/A	H/A	W/A
1.750	1.245	1.900	4.830	1.799	2.194

X/A	Y/A
1.000	.000
1.049	.171
1.080	.331
1.095	.481
1.097	.623
1.086	.756
1.064	.881
1.033	.998
.993	1.107
.945	1.209
.890	1.302
.829	1.388
.762	1.465
.690	1.535
.613	1.597
.533	1.650
.449	1.696
.362	1.733
.274	1.762
.184	1.782
.092	1.795
.001	1.799

Figure 11. Continued. (i)

B/A	P	LA	L/A	H/A	W/A
1.750	1.213	1.949	5.067	1.900	2.244

X/A	Y/A
1.000	.000
1.056	.172
1.093	.334
1.115	.487
1.122	.631
1.117	.767
1.101	.895
1.075	1.015
1.040	1.123
.998	1.233
.947	1.331
.891	1.421
.828	1.503
.760	1.576
.687	1.645
.610	1.705
.530	1.756
.446	1.800
.360	1.836
.272	1.864
.182	1.884
.091	1.896
.000	1.900

Figure 11. Continued. (j)

B/A	P	LA	L/A	H/A	W/A
<u>1.750</u>	<u>1.185</u>	<u>1.998</u>	<u>5.303</u>	<u>1.999</u>	<u>2.294</u>

X/A	Y/A
1.000	.000
<u>1.065</u>	<u>.182</u>
1.109	.352
1.136	.513
1.147	.664
1.145	.807
1.131	.941
<u>1.107</u>	<u>1.068</u>
1.072	1.186
<u>1.030</u>	<u>1.297</u>
.979	1.400
.921	1.495
.857	1.581
.787	1.660
.712	1.731
.633	1.793
.549	1.848
.463	1.894
.374	1.932
.282	1.961
.189	1.982
.095	1.995
.001	1.999

Figure 11. Continued. (k)

B/A	P	LA	L/A	H/A	W/A
<u>1.750</u>	<u>1.158</u>	<u>2.050</u>	<u>5.551</u>	<u>2.102</u>	<u>2.349</u>

X/A	Y/A
1.000	.000
<u>1.074</u>	<u>.191</u>
1.125	.371
<u>1.157</u>	<u>.540</u>
1.173	.699
<u>1.174</u>	<u>.849</u>
1.163	.990
<u>1.139</u>	<u>1.123</u>
1.106	1.248
<u>1.063</u>	<u>1.364</u>
<u>1.012</u>	<u>1.472</u>
.953	1.572
.887	1.663
.815	1.746
.738	1.820
.656	1.886
.570	1.943
.481	1.992
.388	2.031
.293	2.062
.197	2.084
.099	2.098
.001	2.102

Figure 11. Continued. (l)

B/A <u>1.750</u>	P <u>1.134</u>	LA <u>2.102</u>	L/A <u>5.800</u>	H/A <u>2.205</u>	W/A <u>2.407</u>
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X/A	Y/A
<u>1.000</u>	<u>.000</u>
<u>1.080</u>	<u>.193</u>
<u>1.137</u>	<u>.374</u>
<u>1.175</u>	<u>.544</u>
<u>1.197</u>	<u>.705</u>
<u>1.204</u>	<u>.857</u>
<u>1.197</u>	<u>1.001</u>
<u>1.180</u>	<u>1.137</u>
<u>1.151</u>	<u>1.265</u>
<u>1.114</u>	<u>1.384</u>
<u>1.068</u>	<u>1.496</u>
<u>1.014</u>	<u>1.600</u>
<u>.953</u>	<u>1.695</u>
<u>.885</u>	<u>1.783</u>
<u>.812</u>	<u>1.863</u>
<u>.735</u>	<u>1.934</u>
<u>.652</u>	<u>1.997</u>
<u>.566</u>	<u>2.052</u>
<u>.477</u>	<u>2.099</u>
<u>.385</u>	<u>2.137</u>
<u>.290</u>	<u>2.167</u>
<u>.194</u>	<u>2.188</u>
<u>.098</u>	<u>2.201</u>
<u>.000</u>	<u>2.205</u>

Figure 11. Continued. (m)

B/A <u>1.750</u>	P <u>1.113</u>	LA <u>2.151</u>	L/A <u>6.033</u>	H/A <u>2.301</u>	W/A <u>2.462</u>
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X/A	Y/A
<u>1.000</u>	<u>.000</u>
<u>1.089</u>	<u>.202</u>
<u>1.153</u>	<u>.391</u>
<u>1.196</u>	<u>.569</u>
<u>1.221</u>	<u>.737</u>
<u>1.231</u>	<u>.895</u>
<u>1.227</u>	<u>1.045</u>
<u>1.210</u>	<u>1.187</u>
<u>1.183</u>	<u>1.320</u>
<u>1.145</u>	<u>1.444</u>
<u>1.099</u>	<u>1.561</u>
<u>1.044</u>	<u>1.669</u>
<u>.982</u>	<u>1.769</u>
<u>.913</u>	<u>1.860</u>
<u>.839</u>	<u>1.943</u>
<u>.759</u>	<u>2.018</u>
<u>.674</u>	<u>2.084</u>
<u>.585</u>	<u>2.141</u>
<u>.493</u>	<u>2.190</u>
<u>.398</u>	<u>2.230</u>
<u>.301</u>	<u>2.261</u>
<u>.202</u>	<u>2.283</u>
<u>.102</u>	<u>2.296</u>
<u>.001</u>	<u>2.301</u>

Figure 11. Continued. (n)

B/A	P	LA	L/A	H/A	W/A
1.750	1.095	2.202	6.271	2.398	2.516

X/A	Y/A
1.000	.000
<u>1.097</u>	<u>.211</u>
1.168	.408
1.216	.594
1.245	.769
1.258	.934
1.256	1.090
<u>1.241</u>	<u>1.238</u>
1.214	1.376
1.177	1.506
1.130	1.627
1.074	1.740
1.011	1.844
.940	1.939
.864	2.026
.782	2.103
.694	2.172
.603	2.232
.508	2.282
.410	2.324
.310	2.356
.208	2.379
.104	2.393
.000	2.398

Figure 11. Continued. (o)

B/A	P	LA	L/A	H/A	W/A
1.750	1.078	2.249	6.492	2.488	2.568

X/A	Y/A
1.000	.000
<u>1.106</u>	<u>.220</u>
1.183	.425
1.236	.617
1.268	.799
1.284	.970
1.284	1.132
<u>1.270</u>	<u>1.285</u>
1.244	1.429
1.206	1.563
1.159	1.689
1.103	1.806
1.038	1.914
.967	2.012
.888	2.102
.804	2.182
.715	2.254
.621	2.316
.523	2.368
.422	2.411
.319	2.445
.214	2.469
.108	2.483
.001	2.488

Figure 11. Continued. (p)

B/A <u>1.750</u>	P <u>1.064</u>	LA <u>2.298</u>	L/A <u>6.720</u>	H/A <u>2.580</u>	W/A <u>2.623</u>
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X/A	Y/A
<u>1.000</u>	<u>.000</u>
<u>1.114</u>	<u>.229</u>
<u>1.197</u>	<u>.442</u>
<u>1.255</u>	<u>.642</u>
<u>1.292</u>	<u>.830</u>
<u>1.310</u>	<u>1.008</u>
<u>1.312</u>	<u>1.176</u>
<u>1.299</u>	<u>1.334</u>
<u>1.273</u>	<u>1.483</u>
<u>1.236</u>	<u>1.622</u>
<u>1.189</u>	<u>1.752</u>
<u>1.131</u>	<u>1.873</u>
<u>1.066</u>	<u>1.985</u>
<u>.992</u>	<u>2.087</u>
<u>.912</u>	<u>2.180</u>
<u>.826</u>	<u>2.264</u>
<u>.734</u>	<u>2.337</u>
<u>.638</u>	<u>2.402</u>
<u>.538</u>	<u>2.456</u>
<u>.434</u>	<u>2.501</u>
<u>.328</u>	<u>2.535</u>
<u>.220</u>	<u>2.560</u>
<u>.110</u>	<u>2.575</u>
<u>.000</u>	<u>2.580</u>

Figure 11. Continued. (q)

B/A <u>1.750</u>	P <u>1.050</u>	LA <u>2.345</u>	L/A <u>6.941</u>	H/A <u>2.669</u>	W/A <u>2.678</u>
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X/A	Y/A
<u>1.000</u>	<u>.000</u>
<u>1.123</u>	<u>.238</u>
<u>1.212</u>	<u>.459</u>
<u>1.275</u>	<u>.665</u>
<u>1.315</u>	<u>.860</u>
<u>1.336</u>	<u>1.044</u>
<u>1.339</u>	<u>1.217</u>
<u>1.328</u>	<u>1.381</u>
<u>1.303</u>	<u>1.535</u>
<u>1.266</u>	<u>1.679</u>
<u>1.218</u>	<u>1.813</u>
<u>1.160</u>	<u>1.938</u>
<u>1.093</u>	<u>2.054</u>
<u>1.018</u>	<u>2.160</u>
<u>.936</u>	<u>2.256</u>
<u>.848</u>	<u>2.342</u>
<u>.754</u>	<u>2.418</u>
<u>.655</u>	<u>2.484</u>
<u>.552</u>	<u>2.541</u>
<u>.446</u>	<u>2.587</u>
<u>.337</u>	<u>2.623</u>
<u>.226</u>	<u>2.648</u>
<u>.114</u>	<u>2.664</u>
<u>.001</u>	<u>2.669</u>

Figure 11. Continued. (r)

B/A	P	LA	L/A	H/A	W/A
1.750	1.037	2.395	7.177	2.764	2.737

X/A	Y/A
1.000	.000
1.127	.237
1.221	.458
1.288	.665
1.333	.860
1.359	1.044
1.368	1.219
1.362	1.383
1.343	1.539
1.312	1.685
1.270	1.822
1.217	1.950
1.156	2.069
1.087	2.179
1.011	2.280
.928	2.371
.839	2.453
.745	2.526
.647	2.589
.545	2.642
.439	2.686
.332	2.720
.222	2.744
.112	2.759
.000	2.764

Figure 11. Continued. (s)

B/A	P	LA	L/A	H/A	W/A
1.750	1.024	2.448	7.424	2.863	2.798

X/A	Y/A
1.000	.000
1.136	.247
1.237	.476
1.310	.691
1.359	.893
1.388	1.084
1.399	1.264
1.394	1.435
1.376	1.596
1.345	1.747
1.302	1.889
1.249	2.021
1.187	2.144
1.116	2.258
1.038	2.362
.953	2.456
.862	2.541
.766	2.616
.665	2.681
.560	2.737
.452	2.782
.341	2.817
.229	2.843
.115	2.858
.000	2.863

Figure 11. Continued. (t)

B/A	P	L/A	L/A	H/A	W/A
1.750	1.011	2.509	7.706	2.976	2.867

X/A	Y/A
1.000	.000
1.147	.259
1.256	.498
1.334	.721
1.388	.931
1.420	1.129
1.433	1.317
1.430	1.494
1.413	1.661
1.382	1.818
1.339	1.965
1.285	2.102
1.222	2.230
1.150	2.348
1.069	2.456
.982	2.554
.889	2.642
.789	2.720
.686	2.787
.578	2.845
.466	2.892
.352	2.928
.236	2.955
.119	2.970
.000	2.976

Figure 11. Continued. (u)

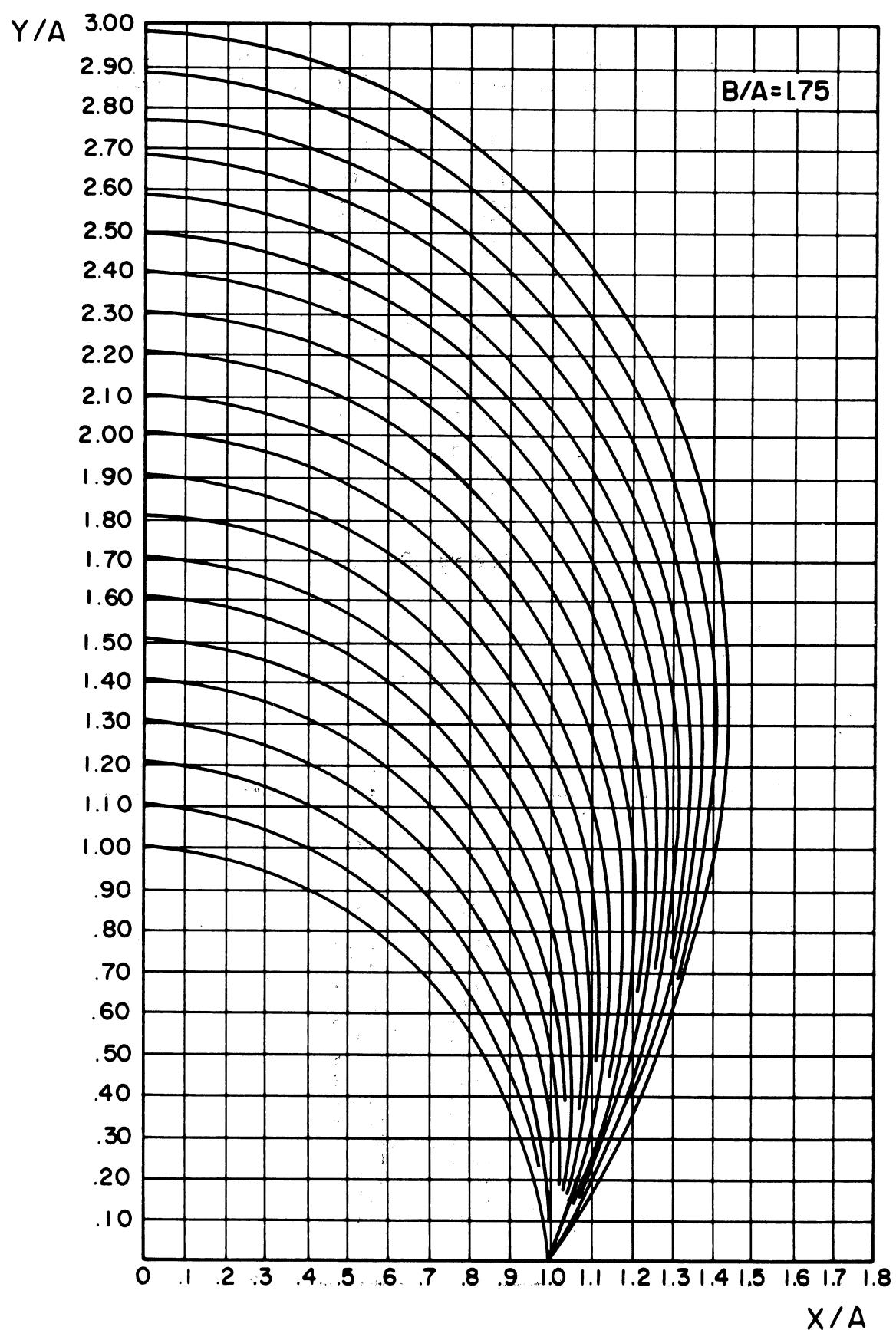


Figure 11. Concluded. (v)

B/A	P	L/A	L/A	H/A	W/A
2.000	1.672	1.667	3.105	1.000	2.000

X/A	Y/A
1.000	.000
.982	.122
.954	.236
.918	.342
.874	.439
.824	.529
.767	.610
.705	.684
.639	.750
.568	.809
.493	.859
.416	.902
.336	.937
.254	.965
.170	.984
.085	.996
.001	1.000

Figure 12. (a)

B/A	P	L/A	L/A	H/A	W/A
2.000	1.591	1.692	3.300	1.100	2.000

X/A	Y/A
1.000	.000
.992	.126
.973	.244
.945	.354
.909	.457
.866	.551
.815	.638
.759	.718
.698	.790
.632	.855
.562	.912
.488	.962
.412	1.004
.332	1.038
.251	1.065
.168	1.085
.085	1.096
.001	1.100

Figure 12. Continued. (b)

B/A	P	LA	L/A	H/A	W/A
2.000	1.520	1.723	3.504	1.200	2.002

X/A	Y/A
1.000	.000
1.001	.129
.991	.251
.971	.365
.942	.472
.905	.571
.861	.664
.811	.749
.755	.826
.693	.897
.628	.960
.558	1.016
.484	1.065
.408	1.106
.330	1.140
.249	1.166
.167	1.185
.084	1.196
.000	1.200

Figure 12. Continued. (c)

B/A	P	LA	L/A	H/A	W/A
2.000	1.457	1.758	3.714	1.299	2.018

X/A	Y/A
1.000	.000
1.009	.132
1.007	.257
.994	.375
.972	.485
.942	.589
.904	.686
.859	.776
.809	.858
.752	.934
.691	1.003
.625	1.065
.555	1.120
.482	1.167
.406	1.208
.328	1.241
.248	1.266
.166	1.285
.083	1.296
.000	1.299

Figure 12. Continued. (d)

B/A 2.000	P 1.400	LA 1.797	L/A 3.932	H/A 1.400	W/A 2.045
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.018	.142
1.022	.276
1.015	.402
.997	.521
.970	.633
.934	.737
.890	.834
.839	.923
.782	1.005
.719	1.079
.652	1.146
.580	1.205
.504	1.257
.425	1.300
.343	1.336
.259	1.364
.174	1.384
.087	1.396
.000	1.400

Figure 12. Continued. (e)

B/A 2.000	P 1.350	LA 1.839	L/A 4.152	H/A 1.500	W/A 2.075
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.026	.144
1.038	.280
1.037	.409
1.026	.532
1.005	.647
.975	.755
.937	.856
.891	.950
.839	1.036
.781	1.116
.718	1.188
.650	1.253
.578	1.311
.502	1.360
.423	1.403
.342	1.438
.258	1.465
.173	1.484
.087	1.496
.001	1.500

Figure 12. Continued. (f)

B/A	P	LA	L/A	H/A	W/A
2.000	1.305	1.883	4.380	1.600	2.116

X/A	Y/A
1.000	.000
1.033	.146
1.052	.285
1.058	.417
1.053	.542
1.038	.660
1.014	.771
.981	.876
.941	.974
.894	1.066
.840	1.150
.781	1.227
.717	1.297
.648	1.360
.576	1.416
.500	1.465
.421	1.506
.340	1.540
.257	1.566
.172	1.585
.086	1.596
.000	1.600

Figure 12. Continued. (g)

B/A	P	LA	L/A	H/A	W/A
2.000	1.265	1.929	4.610	1.700	2.158

X/A	Y/A
1.000	.000
1.041	.155
1.067	.302
1.079	.441
1.078	.574
1.066	.700
1.044	.818
1.012	.929
.973	1.034
.925	1.131
.871	1.220
.811	1.303
.745	1.377
.675	1.445
.600	1.504
.521	1.556
.439	1.600
.354	1.636
.268	1.664
.179	1.684
.090	1.696
.000	1.700

Figure 12. Continued. (h)

B/A	P	LA	L/A	H/A	W/A
2.000	1.228	1.977	4.846	1.801	2.206

X/A	Y/A
1.000	.000
1.050	.164
1.083	.319
1.100	.467
1.103	.607
1.094	.740
1.074	.865
1.044	.983
1.005	1.094
.958	1.197
.903	1.292
.841	1.379
.774	1.458
.701	1.530
.623	1.593
.542	1.648
.457	1.694
.369	1.732
.279	1.762
.187	1.783
.094	1.796
.000	1.801

Figure 12. Continued. (i)

B/A	P	LA	L/A	H/A	W/A
2.000	1.196	2.024	5.077	1.898	2.256

X/A	Y/A
1.000	.000
1.057	.165
1.095	.321
1.119	.471
1.128	.613
1.125	.748
1.111	.876
1.086	.997
1.052	1.111
1.010	1.217
.961	1.316
.904	1.408
.841	1.492
.773	1.569
.699	1.637
.621	1.698
.540	1.751
.455	1.796
.367	1.833
.278	1.861
.186	1.882
.094	1.894
.001	1.898

Figure 12. Continued. (j)

B/A	P	LA	L/A	H/A	W/A
<u>2.000</u>	<u>1.167</u>	<u>2.075</u>	<u>5.320</u>	<u>2.000</u>	<u>2.306</u>

X/A	Y/A
1.000	.000
1.065	.173
1.111	.339
1.140	.496
1.153	.646
1.153	.788
1.141	.923
1.118	1.050
1.085	1.170
1.043	1.282
.993	1.386
.935	1.483
.871	1.572
.800	1.652
.725	1.725
.644	1.789
.560	1.845
.472	1.892
.381	1.931
.288	1.961
.193	1.983
.097	1.996
.000	2.000

Figure 12. Continued. (k)

B/A	P	LA	L/A	H/A	W/A
<u>2.000</u>	<u>1.139</u>	<u>2.128</u>	<u>5.573</u>	<u>2.105</u>	<u>2.366</u>

X/A	Y/A
1.000	.000
1.074	.183
1.127	.356
1.162	.522
1.179	.679
1.183	.829
1.173	.971
1.151	1.105
1.119	1.231
1.077	1.349
1.026	1.459
.968	1.560
.902	1.654
.829	1.738
.751	1.815
.668	1.882
.581	1.941
.490	1.991
.395	2.032
.299	2.064
.200	2.087
.100	2.100
.000	2.105

Figure 12. Continued. (l)

B/A	P	LA	L/A	H/A	W/A
<u>2.000</u>	<u>1.116</u>	<u>2.179</u>	<u>5.814</u>	<u>2.204</u>	<u>2.422</u>

X/A	Y/A
1.000	.000
1.080	.183
1.139	.358
1.178	.525
1.202	.683
1.211	.835
1.207	.978
1.191	1.115
1.164	1.244
1.127	1.365
1.082	1.478
1.028	1.584
.967	1.681
.900	1.771
.826	1.852
.748	1.926
.664	1.990
.577	2.047
.486	2.095
.392	2.134
.296	2.164
.198	2.186
.099	2.199
.000	2.204

Figure 12. Continued. (m)

B/A	P	LA	L/A	H/A	W/A
<u>2.000</u>	<u>1.095</u>	<u>2.228</u>	<u>6.045</u>	<u>2.298</u>	<u>2.476</u>

X/A	Y/A
1.000	.000
1.088	.191
1.153	.374
1.198	.547
1.226	.713
1.238	.871
1.236	1.021
1.221	1.163
1.195	1.297
1.159	1.423
1.113	1.541
1.059	1.652
.997	1.753
.928	1.847
.853	1.932
.772	2.008
.686	2.076
.596	2.135
.502	2.184
.405	2.225
.306	2.257
.205	2.280
.103	2.294
.001	2.298

Figure 12. Continued. (n)

B/A 2.000	P 1.076	LA 2.279	L/A 6.283	H/A 2.395	W/A 2.530
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.097	.200
1.168	.390
1.218	.571
1.250	.744
1.265	.908
1.265	1.064
1.252	1.212
1.227	1.352
1.190	1.483
1.144	1.606
1.089	1.721
1.026	1.827
.955	1.925
.878	2.013
.795	2.092
.707	2.163
.614	2.224
.517	2.276
.418	2.319
.316	2.352
.211	2.376
.106	2.390
.000	2.395

Figure 12. Continued. (o)

B/A 2.000	P 1.060	LA 2.328	L/A 6.512	H/A 2.488	W/A 2.587
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.105	.208
1.183	.406
1.238	.594
1.274	.773
1.291	.944
1.294	1.106
1.282	1.260
1.257	1.405
1.221	1.541
1.175	1.669
1.119	1.788
1.055	1.898
.982	1.999
.903	2.091
.818	2.174
.728	2.247
.632	2.310
.533	2.364
.430	2.409
.325	2.443
.218	2.468
.109	2.483
.000	2.488

Figure 12. Continued. (p)

B/A 2.000	P 1.044	LA 2.377	L/A 6.741	H/A 2.580	W/A 2.646
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.109	.208
1.192	.405
1.252	.593
1.292	.773
1.315	.944
1.323	1.107
1.317	1.262
1.298	1.408
1.267	1.547
1.226	1.677
1.176	1.799
1.117	1.913
1.051	2.018
.977	2.114
.897	2.202
.811	2.281
.721	2.350
.626	2.411
.527	2.462
.425	2.505
.321	2.538
.215	2.561
.108	2.575
.001	2.580

Figure 12. Continued. (q)

B/A 2.000	P 1.029	LA 2.429	L/A 6.987	H/A 2.678	W/A 2.706
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.118	.216
1.207	.422
1.272	.617
1.317	.804
1.343	.981
1.353	1.150
1.348	1.311
1.330	1.463
1.300	1.607
1.259	1.742
1.208	1.869
1.148	1.987
1.080	2.096
1.005	2.196
.923	2.287
.835	2.368
.742	2.440
.644	2.503
.543	2.557
.438	2.600
.331	2.635
.222	2.659
.111	2.674
.001	2.678

Figure 12. Continued. (r)

B/A	P	LA	L/A	H/A	W/A
2.000	1.014	2.486	7.251	2.784	2.770

X/A	Y/A
1.000	.000
1.127	.226
1.224	.440
1.295	.643
1.344	.837
1.373	1.022
1.385	1.197
1.382	1.364
1.365	1.522
1.335	1.672
1.294	1.812
1.242	1.943
1.181	2.066
1.112	2.179
1.034	2.283
.950	2.377
.860	2.462
.764	2.537
.664	2.602
.559	2.658
.451	2.703
.341	2.738
.229	2.764
.115	2.779
.000	2.784

Figure 12. Continued. (s)

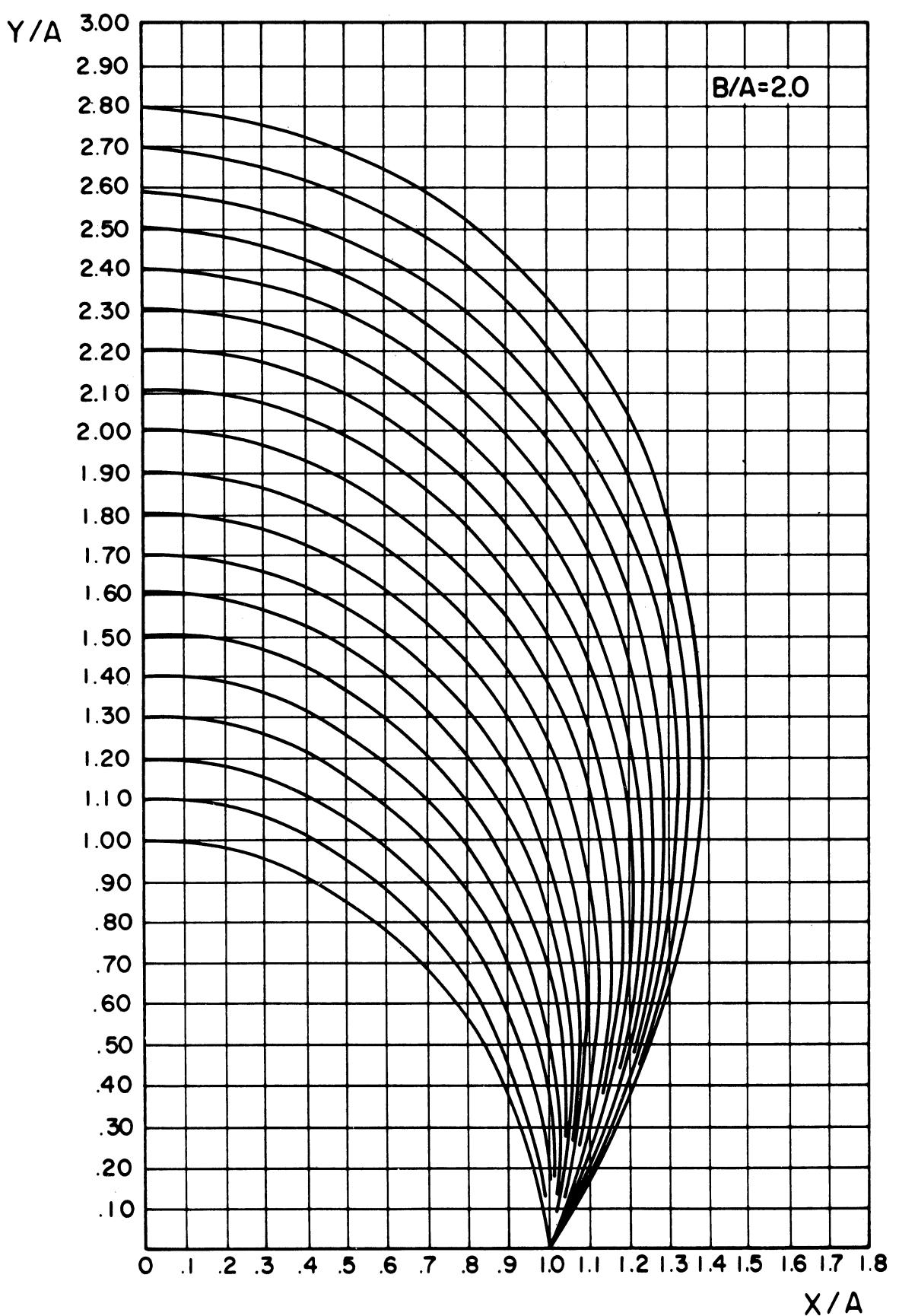


Figure 12. Concluded. (t)

B/A 2.250	P 1.664	LA 1.741	L/A 3.110	H/A 1.000	W/A 2.000
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
.983	.120
.957	.232
.922	.337
.879	.434
.829	.524
.773	.606
.711	.680
.644	.747
.573	.806
.498	.857
.420	.901
.339	.937
.256	.964
.172	.984
.086	.996
.000	1.000

Figure 13. (a)

B/A 2.250	P 1.582	LA 1.765	L/A 3.304	H/A 1.100	W/A 2.000
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
.993	.123
.976	.239
.949	.349
.914	.450
.871	.545
.821	.633
.766	.713
.704	.786
.638	.851
.568	.909
.494	.959
.416	1.002
.336	1.037
.254	1.065
.171	1.084
.086	1.096
.001	1.100

Figure 13. Continued. (b)

B/A	P	LA	L/A	H/A	W/A
<u>2.250</u>	<u>1.509</u>	<u>1.795</u>	<u>3.511</u>	<u>1.201</u>	<u>2.004</u>

X/A	Y/A
1.000	.000
<u>1.092</u>	<u>.126</u>
.993	.246
.974	.359
.947	.405
.911	.565
.857	.657
<u>.818</u>	<u>.743</u>
.762	.821
.700	.893
.634	.957
.564	1.014
.493	1.063
<u>.413</u>	<u>1.125</u>
.334	1.139
.252	1.165
.169	1.185
.085	1.197
<u>.000</u>	<u>1.201</u>

Figure 13. Continued. (c)

B/A	P	LA	L/A	H/A	W/A
<u>2.250</u>	<u>1.445</u>	<u>1.831</u>	<u>3.721</u>	<u>1.301</u>	<u>2.021</u>

X/A	Y/A
1.000	.000
<u>1.010</u>	<u>.129</u>
1.009	.251
.993	.368
.977	.475
.948	.581
.911	.678
.867	.769
.816	.852
.760	.929
.698	.999
.632	1.062
.562	1.117
<u>.488</u>	<u>1.156</u>
.411	1.207
.332	1.241
.251	1.257
.168	1.285
.084	1.297
<u>.000</u>	<u>1.301</u>

Figure 13. Continued. (d)

B/A	P	LA	L/A	H/A	W/A
2.250	1.389	1.869	3.936	1.399	2.049

X/A	Y/A
1.000	.000
1.018	.131
1.025	.256
1.020	.375
1.006	.489
.983	.596
.952	.697
.913	.791
.868	.880
.816	.961
.759	1.036
.697	1.104
.631	1.166
.561	1.220
.487	1.267
.410	1.308
.331	1.340
.250	1.366
.168	1.384
.084	1.395
.001	1.399

Figure 13. Continued. (e)

B/A	P	LA	L/A	H/A	W/A
2.250	1.337	1.911	4.159	1.499	2.082

X/A	Y/A
1.000	.000
1.027	.139
1.040	.273
1.041	.400
1.031	.521
1.011	.636
.982	.744
.945	.846
.900	.940
.848	1.028
.790	1.109
.726	1.182
.658	1.248
.585	1.306
.509	1.357
.429	1.400
.346	1.436
.262	1.464
.176	1.483
.088	1.495
.000	1.499

Figure 13. Continued. (f)

B/A 2.250	P 1.292	LA 1.955	L/A 4.385	H/A 1.599	W/A 2.123
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.034	.141
1.054	.276
1.062	.406
1.058	.530
1.044	.648
1.021	.759
.989	.865
.950	.963
.903	1.055
.850	1.141
.791	1.219
.726	1.290
.657	1.355
.584	1.411
.508	1.461
.428	1.503
.345	1.537
.261	1.564
.175	1.583
.088	1.595
.001	1.599

Figure 13. Continued. (g)

B/A 2.250	P 1.251	LA 2.002	L/A 4.619	H/A 1.700	W/A 2.166
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.042	.149
1.069	.293
1.082	.430
1.083	.562
1.072	.687
1.051	.805
1.021	.917
.982	1.022
.935	1.120
.882	1.211
.821	1.295
.755	1.371
.684	1.439
.608	1.500
.529	1.552
.440	1.597
.360	1.634
.272	1.663
.182	1.683
.092	1.696
.000	1.700

Figure 13. Continued. (h)

B/A 2.250	P 1.214	LA 2.049	L/A 4.850	H/A 1.798	W/A 2.216
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.049	.150
1.082	.295
1.101	.435
1.108	.568
1.103	.696
1.088	.817
1.063	.932
1.030	1.040
.988	1.142
.939	1.237
.884	1.325
.822	1.406
.755	1.480
.683	1.546
.607	1.605
.527	1.656
.444	1.699
.359	1.735
.271	1.763
.182	1.782
.092	1.794
.001	1.798

Figure 13. Continued. (i)

B/A 2.250	P 1.181	LA 2.098	L/A 5.087	H/A 1.898	W/A 2.266
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.057	.158
1.097	.311
1.122	.458
1.133	.598
1.131	.733
1.118	.861
1.095	.982
1.062	1.097
1.021	1.204
.972	1.305
.915	1.398
.852	1.483
.783	1.561
.709	1.631
.631	1.693
.548	1.747
.462	1.793
.373	1.831
.282	1.860
.189	1.881
.096	1.894
.001	1.898

Figure 13. Continued. (j)

B/A 2.250	P 1.151	LA 2.148	L/A 5.330	H/A 1.999	W/A 2.320
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.065	.167
1.112	.327
1.143	.481
1.158	.629
1.160	.771
1.149	.906
1.128	1.033
1.096	1.154
1.054	1.267
1.005	1.373
.947	1.471
.883	1.561
.812	1.643
.736	1.717
.654	1.783
.569	1.840
.480	1.888
.388	1.928
.293	1.959
.197	1.981
.099	1.994
.001	1.999

Figure 13. Continued. (k)

B/A 2.250	P 1.124	LA 2.201	L/A 5.580	H/A 2.102	W/A 2.378
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.072	.167
1.124	.329
1.161	.485
1.182	.635
1.189	.778
1.184	.915
1.168	1.046
1.142	1.170
1.106	1.286
1.061	1.396
1.009	1.498
.949	1.593
.883	1.680
.811	1.759
.734	1.831
.652	1.894
.566	1.949
.477	1.995
.385	2.034
.291	2.064
.195	2.085
.098	2.098
.001	2.102

Figure 13. Continued. (l)

B/A 2.250	P 1.100	LA 2.252	L/A 5.820	H/A 2.200	W/A 2.434
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.080	.175
1.139	.344
1.181	.507
1.206	.664
1.217	.814
1.214	.958
1.200	1.094
1.174	1.224
1.139	1.346
1.094	1.461
1.041	1.568
.980	1.667
.912	1.758
.838	1.841
.759	1.916
.675	1.982
.586	2.040
.494	2.088
.399	2.129
.302	2.160
.202	2.182
.102	2.196
.001	2.200

Figure 13. Continued. (m)

B/A 2.250	P 1.079	LA 2.303	L/A 6.058	H/A 2.297	W/A 2.488
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.088	.183
1.154	.360
1.201	.530
1.230	.693
1.244	.850
1.244	1.000
1.231	1.142
1.206	1.278
1.171	1.405
1.126	1.525
1.072	1.637
1.010	1.740
.941	1.835
.865	1.922
.783	2.000
.697	2.069
.605	2.129
.510	2.180
.412	2.222
.312	2.255
.209	2.278
.105	2.292
.001	2.297

Figure 13. Continued. (n)

B/A <u>2.250</u>	P <u>1.060</u>	LA <u>2.354</u>	L/A <u>6.296</u>	H/A <u>2.393</u>	W/A <u>2.547</u>
---------------------	-------------------	--------------------	---------------------	---------------------	---------------------

X/A	Y/A
1.000	.000
1.096	.191
1.169	.375
1.221	.552
1.254	.723
1.271	.886
1.274	1.042
1.262	1.190
1.238	1.331
1.203	1.464
1.158	1.589
1.103	1.705
1.040	1.813
.969	1.912
.892	2.002
.808	2.084
.718	2.156
.625	2.218
.527	2.271
.425	2.315
.321	2.349
.215	2.374
.108	2.388
.000	2.393

Figure 13. Continued. (o)

B/A <u>2.250</u>	P <u>1.042</u>	LA <u>2.404</u>	L/A <u>6.533</u>	H/A <u>2.489</u>	W/A <u>2.607</u>
---------------------	-------------------	--------------------	---------------------	---------------------	---------------------

X/A	Y/A
1.000	.000
1.101	.191
1.178	.375
1.235	.552
1.274	.723
1.296	.887
1.303	1.044
1.298	1.194
1.279	1.336
1.250	1.472
1.210	1.599
1.161	1.719
1.103	1.830
1.038	1.934
.965	2.029
.887	2.115
.802	2.193
.713	2.262
.619	2.322
.521	2.372
.421	2.414
.318	2.447
.213	2.470
.107	2.484
.001	2.489

Figure 13. Continued. (p)

B/A <u>2.250</u>	P <u>1.026</u>	LA <u>2.457</u>	L/A <u>6.779</u>	H/A <u>2.587</u>	W/A <u>2.667</u>
---------------------	-------------------	--------------------	---------------------	---------------------	---------------------

X/A	Y/A
1.000	.000
1.109	.199
1.193	.390
1.255	.575
1.298	.752
1.324	.923
1.334	1.086
1.329	1.242
1.312	1.390
1.283	1.530
1.243	1.663
1.194	1.787
1.135	1.903
1.068	2.010
.994	2.109
.913	2.199
.826	2.280
.734	2.351
.638	2.413
.537	2.466
.434	2.510
.328	2.544
.220	2.568
.110	2.582
.001	2.587

Figure 13. Continued. (q)

B/A <u>2.250</u>	P <u>1.010</u>	LA <u>2.514</u>	L/A <u>7.042</u>	H/A <u>2.692</u>	W/A <u>2.732</u>
---------------------	-------------------	--------------------	---------------------	---------------------	---------------------

X/A	Y/A
1.000	.000
1.118	.207
1.209	.407
1.277	.599
1.324	.784
1.353	.961
1.366	1.131
1.363	1.293
1.347	1.447
1.318	1.593
1.278	1.731
1.228	1.860
1.168	1.981
1.100	2.092
1.024	2.195
.941	2.288
.852	2.372
.757	2.447
.658	2.512
.554	2.567
.448	2.612
.338	2.647
.227	2.672
.114	2.687
.000	2.692

Figure 13. Continued. (r)

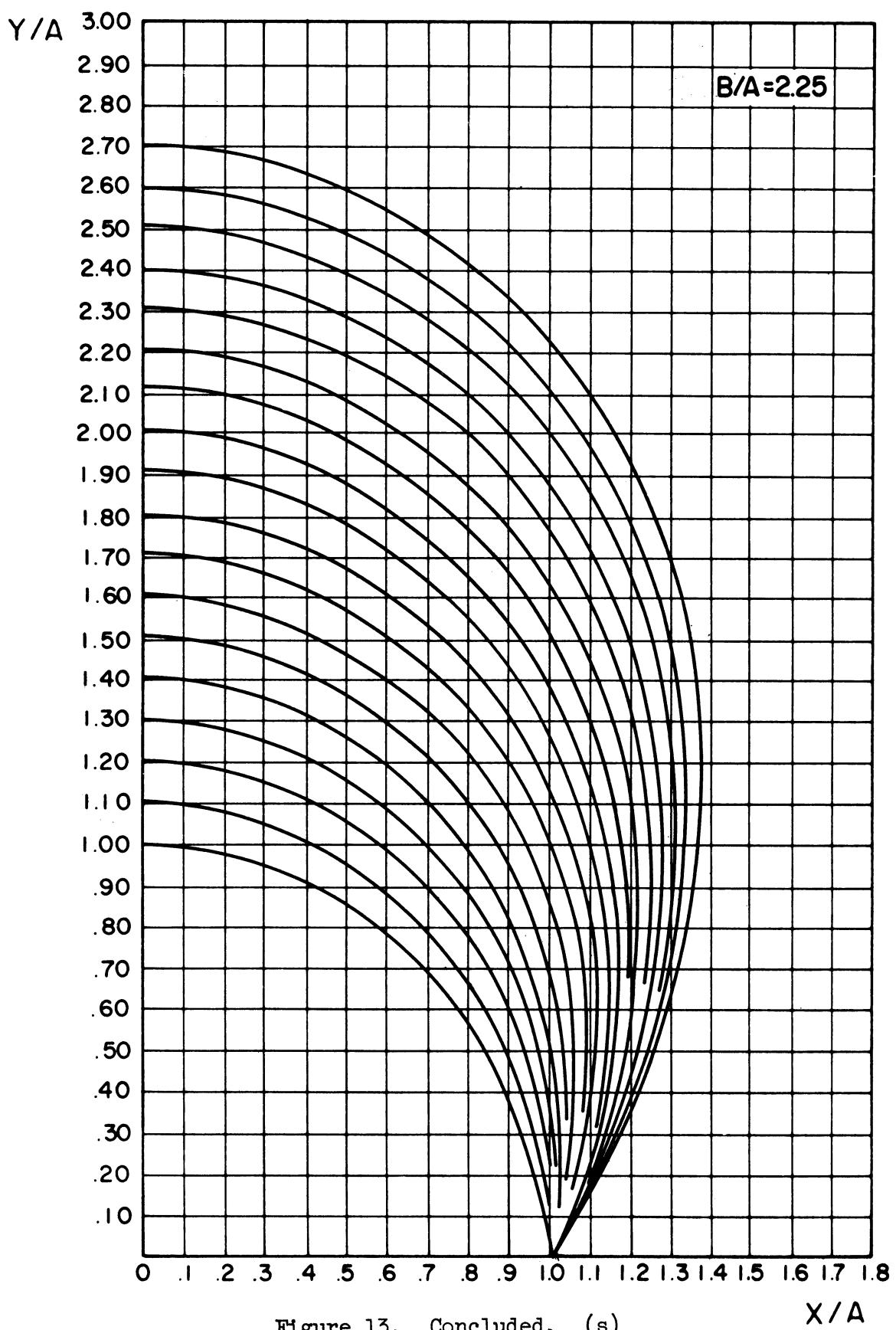


Figure 13. Concluded. (s)

B/A	P	LA	L/A	H/A	W/A
<u>2.500</u>	<u>1.656</u>	<u>1.811</u>	<u>3.110</u>	<u>1.000</u>	<u>2.000</u>

X/A	Y/A
1.000	.000
.986	.111
.962	.216
.932	.315
.893	.407
.849	.494
.798	.573
.742	.646
.681	.713
.616	.773
.547	.826
.475	.872
.400	.911
.323	.943
.244	.968
.164	.985
.082	.996
.001	1.000

Figure 14. (a)

B/A	P	LA	L/A	H/A	W/A
<u>2.500</u>	<u>1.574</u>	<u>1.835</u>	<u>3.308</u>	<u>1.100</u>	<u>2.000</u>

X/A	Y/A
1.000	.000
.994	.121
.978	.236
.952	.344
.918	.445
.876	.540
.826	.628
.771	.709
.710	.782
.643	.848
.573	.907
.498	.958
.420	1.001
.339	1.037
.256	1.064
.172	1.084
.086	1.096
.000	1.100

Figure 14. Continued. (b)

B/A <u>2.500</u>	P <u>1.501</u>	LA <u>1.865</u>	L/A <u>3.514</u>	H/A <u>1.201</u>	W/A <u>2.006</u>
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X/A	Y/A
1.000	.000
1.003	.124
.995	.242
.977	.354
.951	.459
.915	.559
.873	.651
.823	.737
.768	.816
.706	.888
.640	.953
.570	1.011
.495	1.061
.418	1.103
.337	1.138
.255	1.165
.171	1.185
.086	1.197
.000	1.201

Figure 14. Continued. (c)

B/A <u>2.500</u>	P <u>1.436</u>	LA <u>1.900</u>	L/A <u>3.724</u>	H/A <u>1.300</u>	W/A <u>2.023</u>
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X/A	Y/A
1.000	.000
1.011	.126
1.011	.246
1.001	.362
.981	.471
.953	.574
.916	.671
.873	.762
.823	.846
.766	.924
.705	.994
.638	1.058
.568	1.114
.493	1.163
.416	1.205
.336	1.239
.254	1.266
.170	1.285
.086	1.296
.000	1.300

Figure 14. Continued. (d)

B/A <u>2.500</u>	P <u>1.378</u>	LA <u>1.938</u>	L/A <u>3.940</u>	H/A <u>1.399</u>	W/A <u>2.053</u>
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X/A	Y/A
1.000	.000
<u>1.019</u>	<u>.128</u>
<u>1.027</u>	<u>.251</u>
<u>1.023</u>	<u>.368</u>
<u>1.010</u>	<u>.481</u>
<u>.988</u>	<u>.588</u>
<u>.958</u>	<u>.689</u>
<u>.920</u>	<u>.784</u>
<u>.875</u>	<u>.873</u>
<u>.824</u>	<u>.955</u>
<u>.767</u>	<u>1.031</u>
<u>.704</u>	<u>1.100</u>
<u>.638</u>	<u>1.162</u>
<u>.567</u>	<u>1.217</u>
<u>.493</u>	<u>1.265</u>
<u>.415</u>	<u>1.306</u>
<u>.335</u>	<u>1.339</u>
<u>.253</u>	<u>1.365</u>
<u>.170</u>	<u>1.384</u>
<u>.086</u>	<u>1.395</u>
<u>.001</u>	<u>1.399</u>

Figure 14. Continued. (e)

B/A <u>2.500</u>	P <u>1.326</u>	LA <u>1.980</u>	L/A <u>4.163</u>	H/A <u>1.499</u>	W/A <u>2.088</u>
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X/A	Y/A
1.000	.000
<u>1.027</u>	<u>.136</u>
<u>1.042</u>	<u>.267</u>
<u>1.044</u>	<u>.392</u>
<u>1.035</u>	<u>.513</u>
<u>1.016</u>	<u>.627</u>
<u>.988</u>	<u>.735</u>
<u>.952</u>	<u>.837</u>
<u>.907</u>	<u>.932</u>
<u>.856</u>	<u>1.021</u>
<u>.798</u>	<u>1.102</u>
<u>.734</u>	<u>1.176</u>
<u>.666</u>	<u>1.243</u>
<u>.592</u>	<u>1.302</u>
<u>.515</u>	<u>1.354</u>
<u>.435</u>	<u>1.398</u>
<u>.351</u>	<u>1.434</u>
<u>.266</u>	<u>1.462</u>
<u>.179</u>	<u>1.482</u>
<u>.090</u>	<u>1.495</u>
<u>.001</u>	<u>1.499</u>

Figure 14. Continued. (f)

B/A 2.500	P 1.280	LA 2.025	L/A 4.395	H/A 1.600	W/A 2.130
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.035	.137
1.050	.270
1.065	.398
1.063	.521
1.050	.638
1.028	.750
.997	.856
.958	.955
.911	1.048
.858	1.134
.799	1.214
.735	1.286
.665	1.351
.592	1.409
.514	1.459
.434	1.502
.350	1.537
.265	1.565
.178	1.584
.090	1.596
.001	1.600

Figure 14. Continued. (g)

B/A 2.500	P 1.238	LA 2.072	L/A 4.628	H/A 1.700	W/A 2.175
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.043	.145
1.071	.286
1.085	.421
1.088	.551
1.078	.676
1.058	.795
1.029	.907
.991	1.013
.944	1.112
.891	1.203
.831	1.288
.764	1.365
.693	1.435
.616	1.496
.536	1.550
.452	1.596
.365	1.633
.276	1.662
.186	1.683
.094	1.696
.001	1.700

Figure 14. Continued. (h)

B/A 2.500	P 1.201	LA 2.120	L/A 4.862	H/A 1.800	W/A 2.225
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.049	.146
1.084	.288
1.104	.425
1.112	.557
1.109	.684
1.095	.805
1.071	.921
1.038	1.030
.997	1.133
.949	1.229
.893	1.318
.832	1.400
.764	1.475
.692	1.542
.615	1.602
.535	1.654
.451	1.698
.364	1.735
.275	1.763
.185	1.783
.093	1.796
.001	1.800

Figure 14. Continued. (i)

B/A 2.500	P 1.168	LA 2.170	L/A 5.101	H/A 1.900	W/A 2.274
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.058	.153
1.099	.303
1.125	.447
1.137	.587
1.137	.720
1.126	.848
1.103	.970
1.072	1.086
1.031	1.194
.982	1.296
.925	1.390
.862	1.477
.793	1.556
.719	1.627
.639	1.691
.558	1.746
.469	1.792
.379	1.831
.286	1.861
.192	1.882
.097	1.895
.001	1.900

Figure 14. Continued. (j)

B/A	P	LA	L/A	H/A	W/A
<u>2.500</u>	<u>1.138</u>	<u>2.221</u>	<u>5.344</u>	<u>2.000</u>	<u>2.331</u>

X/A	Y/A
1.000	.000
1.066	.161
1.114	.318
1.145	.472
1.162	.616
1.166	.757
1.157	.892
1.138	1.020
1.105	1.142
1.064	1.256
1.015	1.363
.958	1.463
.893	1.554
.822	1.638
.745	1.713
.663	1.780
.577	1.858
.486	1.887
.393	1.928
.297	1.959
.199	1.982
.100	1.990
.000	2.000

Figure 14. Continued. (k)

B/A	P	LA	L/A	H/A	W/A
<u>2.500</u>	<u>1.110</u>	<u>2.273</u>	<u>5.593</u>	<u>2.102</u>	<u>2.389</u>

X/A	Y/A
1.000	.000
1.072	.162
1.125	.319
1.163	.472
1.186	.621
1.195	.763
1.191	.900
1.176	1.031
1.151	1.155
1.116	1.273
1.072	1.384
1.020	1.487
.960	1.584
.894	1.672
.821	1.753
.744	1.825
.661	1.890
.574	1.946
.484	1.993
.391	2.033
.295	2.063
.198	2.085
.099	2.098
.000	2.102

Figure 14. Continued. (l)

B/A	P	LA	L/A	H/A	W/A
<u>2.500</u>	<u>1.086</u>	<u>2.324</u>	<u>5.832</u>	<u>2.200</u>	<u>2.445</u>

X/A	Y/A
-----	-----

1.000	.000
1.086	.169
1.140	.334
1.183	.494
1.210	.649
1.222	.793
1.221	.941
1.208	1.078
1.184	1.208
1.149	1.331
1.105	1.447
1.052	1.556
.991	1.656
.924	1.749
.849	1.833
.769	1.909
.684	1.977
.595	2.036
.501	2.086
.405	2.127
.306	2.159
.205	2.182
.103	2.195
.001	2.200

Figure 14. Continued. (m)

B/A	P	LA	L/A	H/A	W/A
<u>2.500</u>	<u>1.064</u>	<u>2.375</u>	<u>6.070</u>	<u>2.296</u>	<u>2.503</u>

X/A	Y/A
-----	-----

1.000	.000
1.088	.176
1.155	.348
1.203	.515
1.234	.676
1.250	.832
1.251	.982
1.240	1.125
1.216	1.260
1.182	1.389
1.138	1.510
1.084	1.623
1.022	1.728
.953	1.825
.877	1.913
.794	1.993
.707	2.063
.615	2.125
.518	2.177
.419	2.220
.317	2.253
.212	2.277
.107	2.291
.001	2.296

Figure 14. Continued. (n)

B/A	P	LA	L/A	H/A	W/A
<u>2.500</u>	<u>1.045</u>	<u>2.428</u>	<u>6.315</u>	<u>2.395</u>	<u>2.564</u>

X/A	Y/A
1.000	.000
1.092	.176
1.164	.348
1.218	.516
1.254	.678
1.275	.835
1.282	.985
1.276	1.130
1.258	1.268
1.229	1.399
1.190	1.523
1.142	1.640
1.086	1.749
1.022	1.850
.951	1.943
.873	2.027
.790	2.104
.702	2.171
.610	2.230
.514	2.280
.415	2.321
.313	2.353
.210	2.376
.105	2.390
.000	2.395

Figure 14. Continued. (o)

B/A	P	LA	L/A	H/A	W/A
<u>2.500</u>	<u>1.026</u>	<u>2.480</u>	<u>6.560</u>	<u>2.493</u>	<u>2.624</u>

X/A	Y/A
1.000	.000
1.101	.184
1.179	.363
1.238	.537
1.278	.706
1.303	.869
1.312	1.026
1.308	1.176
1.291	1.320
1.263	1.456
1.224	1.586
1.175	1.707
1.118	1.820
1.052	1.926
.980	2.022
.900	2.111
.815	2.190
.724	2.260
.629	2.322
.530	2.374
.428	2.417
.323	2.450
.217	2.474
.109	2.488
.000	2.493

Figure 14. Continued. (p)

B/A	P	L/A	L/A	H/A	W/A
<u>2.500</u>	<u>1.009</u>	<u>2.537</u>	<u>6.822</u>	<u>2.597</u>	<u>2.688</u>

X/A	Y/A
1.000	.000
1.109	.191
1.195	.378
1.259	.560
1.304	.736
1.332	.906
1.344	1.069
1.342	1.226
1.326	1.376
1.298	1.518
1.259	1.652
1.210	1.779
1.152	1.897
1.085	2.006
1.010	2.107
.928	2.199
.841	2.282
.747	2.355
.649	2.419
.547	2.473
.442	2.518
.334	2.553
.224	2.578
.112	2.593
.000	2.597

Figure 14. Continued. (q)

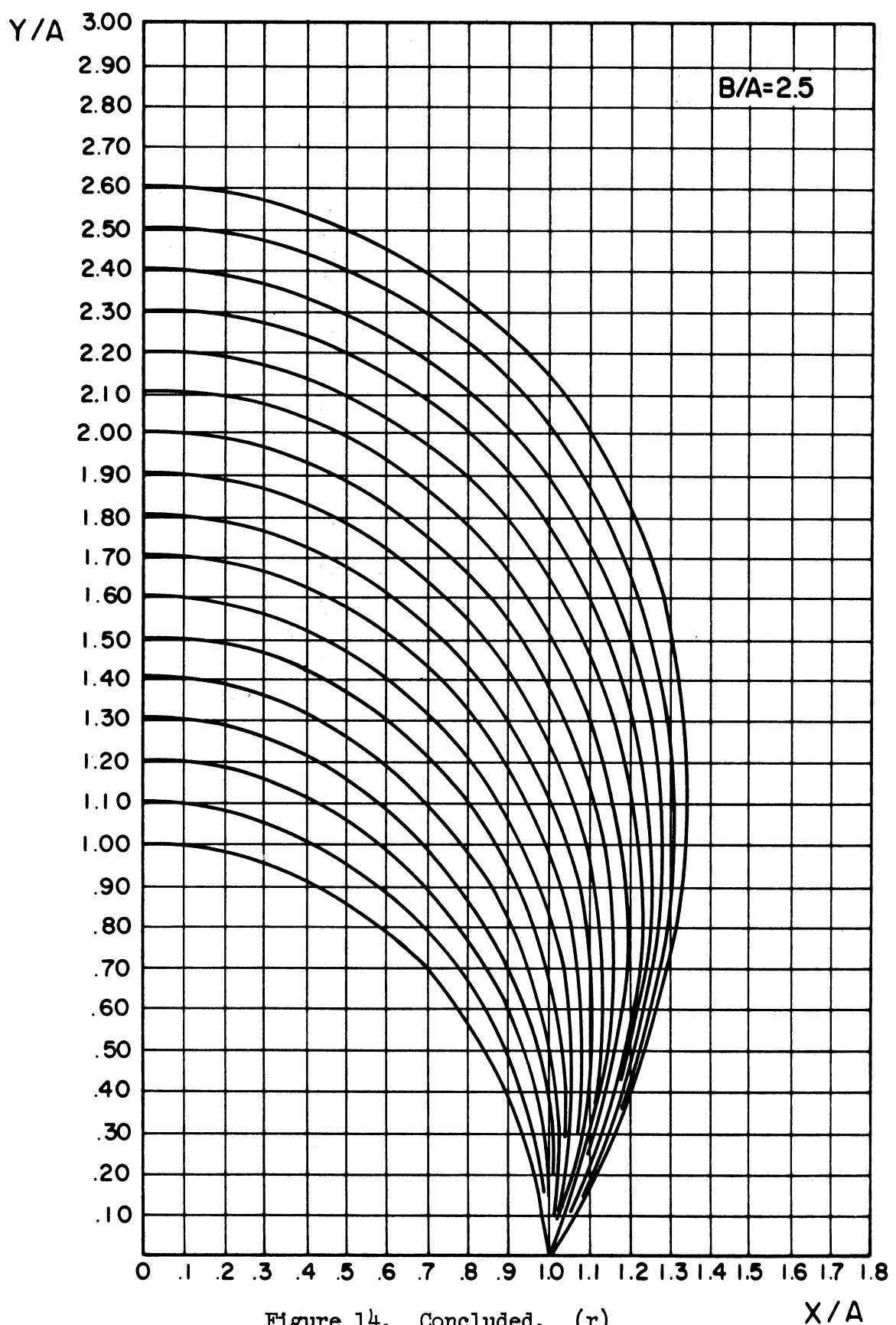


Figure 14. Concluded. (r)

B/A <u>2.750</u>	P <u>1.650</u>	LA <u>1.880</u>	L/A <u>3.115</u>	H/A <u>1.001</u>	W/A <u>2.000</u>
---------------------	-------------------	--------------------	---------------------	---------------------	---------------------

X/A	Y/A
1.000	.000
.986	.110
.964	.214
.934	.312
.896	.404
.852	.490
.802	.570
.746	.644
.685	.711
.620	.771
.551	.824
.479	.871
.403	.910
.325	.943
.246	.968
.165	.986
.083	.997
.000	1.001

Figure 15. (a)

B/A <u>2.750</u>	P <u>1.567</u>	LA <u>1.902</u>	L/A <u>3.311</u>	H/A <u>1.100</u>	W/A <u>2.000</u>
---------------------	-------------------	--------------------	---------------------	---------------------	---------------------

X/A	Y/A
1.000	.000
.996	.113
.982	.220
.959	.323
.929	.419
.892	.510
.848	.595
.798	.674
.742	.747
.682	.813
.617	.873
.548	.926
.476	.972
.401	1.011
.324	1.043
.245	1.068
.164	1.086
.083	1.097
.000	1.100

Figure 15. Continued. (b)

B/A	P	LA	L/A	H/A	W/A
2.750	1.494	1.932	3.515	1.200	2.008

X/A	Y/A
1.000	.000
1.004	.121
.997	.238
.930	.349
.954	.454
.919	.553
.877	.646
.828	.732
.772	.812
.711	.884
.645	.950
.574	1.008
.499	1.058
.421	1.101
.340	1.137
.257	1.164
.172	1.184
.087	1.196
.000	1.200

Figure 15. Continued. (c)

B/A	P	LA	L/A	H/A	W/A
2.750	1.428	1.937	3.729	1.300	2.026

X/A	Y/A
1.000	.000
1.012	.124
1.013	.242
1.004	.356
.985	.465
.957	.568
.921	.666
.878	.757
.828	.841
.772	.919
.710	.991
.644	1.055
.573	1.112
.498	1.161
.420	1.204
.339	1.238
.256	1.265
.172	1.285
.086	1.296
.000	1.300

Figure 15. Continued. (d)

B/A	P	LA	L/A	H/A	W/A
2.750	1.369	2.005	3.945	1.399	2.057

X/A	Y/A
1.000	.000
1.020	.125
1.028	.246
1.026	.363
1.014	.475
.993	.581
.963	.682
.926	.778
.881	.867
.830	.950
.773	1.026
.711	1.096
.644	1.159
.573	1.215
.498	1.263
.420	1.305
.339	1.339
.257	1.365
.172	1.384
.087	1.396
.001	1.399

Figure 15. Continued. (e)

B/A	P	LA	L/A	H/A	W/A
2.750	1.316	2.049	4.174	1.501	2.094

X/A	Y/A
1.000	.000
1.028	.133
1.043	.262
1.047	.386
1.039	.506
1.021	.620
.994	.729
.958	.831
.914	.927
.863	1.016
.805	1.098
.741	1.173
.672	1.241
.598	1.301
.520	1.354
.439	1.398
.355	1.435
.268	1.464
.180	1.484
.091	1.497
.001	1.501

Figure 15. Continued. (f)

B/A 2.750	P 1.270	LA 2.094	L/A 4.404	H/A 1.601	W/A 2.135
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.035	.134
1.057	.265
1.067	.391
1.066	.513
1.054	.630
1.033	.742
1.003	.848
.964	.948
.918	1.042
.865	1.129
.806	1.209
.742	1.282
.672	1.348
.598	1.407
.519	1.458
.433	1.502
.354	1.537
.267	1.565
.179	1.585
.090	1.597
.000	1.601

Figure 15. Continued. (g)

B/A 2.750	P 1.228	LA 2.141	L/A 4.037	H/A 1.701	W/A 2.182
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.043	.142
1.072	.280
1.088	.413
1.091	.543
1.083	.667
1.064	.786
1.035	.898
.993	1.005
.952	1.104
.893	1.197
.838	1.282
.772	1.361
.700	1.431
.623	1.494
.542	1.548
.457	1.595
.369	1.633
.279	1.663
.187	1.684
.094	1.697
.000	1.701

Figure 15. Continued. (h)

B/A	P	LA	L/A	H/A	W/A
2.750	1.190	2.189	4.873	1.800	2.232

X/A	Y/A
1.000	.000
1.050	.142
1.085	.281
1.107	.417
1.116	.548
1.114	.674
1.101	.795
1.078	.911
1.046	1.021
1.005	1.124
.957	1.221
.901	1.311
.840	1.395
.772	1.470
.699	1.539
.622	1.599
.541	1.652
.450	1.697
.368	1.734
.278	1.763
.187	1.784
.094	1.796
.000	1.800

Figure 15. Continued. (i)

B/A	P	LA	L/A	H/A	W/A
2.750	1.156	2.239	5.111	1.900	2.284

X/A	Y/A
1.000	.000
1.058	.149
1.100	.295
1.127	.438
1.141	.576
1.142	.709
1.132	.837
1.110	.959
1.079	1.075
1.039	1.185
.990	1.287
.934	1.382
.871	1.470
.802	1.551
.727	1.623
.647	1.687
.562	1.743
.474	1.791
.383	1.830
.290	1.861
.194	1.883
.098	1.896
.001	1.900

Figure 15. Continued. (j)

B/A	P	LA	L/A	H/A	W/A
<u>2.750</u>	<u>1.126</u>	<u>2.290</u>	<u>5.353</u>	<u>2.000</u>	<u>- - -</u>

X/A	Y/A
1.000	.000
1.034	.150
1.111	.297
1.144	.440
1.164	.580
1.171	.715
1.166	.845
1.150	.970
1.125	1.088
1.090	1.201
1.047	1.307
.995	1.407
.937	1.499
.872	1.584
.802	1.662
.726	1.732
.645	1.794
.561	1.848
.473	1.895
.382	1.932
.288	1.962
.194	1.983
.097	1.996
.001	2.000

Figure 15. Continued. (k)

B/A	P	LA	L/A	H/A	W/A
<u>2.750</u>	<u>1.098</u>	<u>2.342</u>	<u>5.598</u>	<u>2.100</u>	<u>2.398</u>

X/A	Y/A
1.000	.000
1.072	.157
1.126	.311
1.165	.461
1.189	.607
1.199	.749
1.197	.886
1.183	1.017
1.159	1.141
1.124	1.260
1.081	1.371
1.029	1.476
.970	1.573
.903	1.663
.831	1.745
.752	1.818
.669	1.884
.582	1.941
.490	1.989
.396	2.029
.299	2.060
.201	2.082
.101	2.096
.001	2.100

Figure 15. Continued. (l)

B/A 2.750	P 1.073	LA 2.395	L/A 5.845	H/A 2.200	W/A 2.456
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.080	.164
1.141	.325
1.185	.482
1.213	.635
1.227	.784
1.228	.927
1.216	1.064
1.193	1.195
1.159	1.319
1.115	1.436
1.063	1.545
1.002	1.647
.934	1.741
.859	1.827
.779	1.904
.693	1.973
.603	2.033
.508	2.084
.411	2.126
.310	2.158
.208	2.182
.105	2.196
.001	2.200

Figure 15. Continued. (m)

B/A 2.750	P 1.050	LA 2.449	L/A 6.098	H/A 2.302	W/A 2.518
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.088	.171
1.156	.339
1.206	.504
1.239	.664
1.256	.819
1.259	.969
1.249	1.112
1.227	1.249
1.193	1.379
1.150	1.502
1.096	1.616
1.034	1.723
.965	1.821
.888	1.911
.805	1.992
.717	2.064
.623	2.127
.526	2.180
.425	2.224
.321	2.258
.215	2.283
.108	2.297
.000	2.302

Figure 15. Continued. (n)

B/A 2.750	P 1.030	LA 2.502	L/A 6.343	H/A 2.401	W/A 2.580
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.093	.171
1.166	.339
1.220	.504
1.259	.664
1.281	.820
1.290	.971
1.286	1.116
1.269	1.255
1.241	1.387
1.203	1.513
1.156	1.631
1.099	1.742
1.035	1.844
.964	1.939
.886	2.025
.802	2.103
.713	2.172
.619	2.232
.522	2.283
.422	2.325
.319	2.358
.214	2.382
.107	2.396
.001	2.401

Figure 15. Continued. (o)

B/A 2.750	P 1.011	LA 2.557	L/A 6.596	H/A 2.501	W/A 2.642
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.101	.178
1.180	.353
1.241	.525
1.283	.692
1.310	.854
1.321	1.012
1.318	1.163
1.303	1.307
1.276	1.445
1.238	1.576
1.190	1.699
1.132	1.814
1.067	1.921
.993	2.020
.913	2.110
.827	2.191
.735	2.263
.639	2.326
.539	2.379
.435	2.423
.329	2.457
.220	2.481
.111	2.496
.000	2.501

Figure 15. Continued. (p)

B/A <u>2.750</u>	P <u>.994</u>	LA <u>2.609</u>	L/A <u>6.840</u>	H/A <u>2.598</u>	W/A <u>2.702</u>
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X/A	Y/A
1.000	.000
1.109	.185
1.195	.367
1.261	.545
1.308	.719
1.337	.888
1.351	1.051
1.350	1.208
1.336	1.358
1.310	1.501
1.272	1.637
1.223	1.765
1.165	1.885
1.098	1.996
1.023	2.098
.941	2.192
.852	2.276
.758	2.351
.659	2.416
.556	2.471
.449	2.517
.339	2.552
.228	2.578
.115	2.593
.001	2.598

Figure 15. Continued. (q)

B/A <u>2.750</u>	P <u>.979</u>	LA <u>2.664</u>	L/A <u>7.091</u>	H/A <u>2.698</u>	W/A <u>2.766</u>
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X/A	Y/A
1.000	.000
1.117	.192
1.210	.381
1.281	.566
1.332	.747
1.366	.922
1.382	1.091
1.383	1.254
1.370	1.410
1.344	1.559
1.306	1.700
1.257	1.833
1.198	1.957
1.129	2.072
1.053	2.179
.968	2.276
.878	2.363
.781	2.441
.679	2.509
.572	2.566
.462	2.613
.350	2.650
.234	2.676
.118	2.692
.001	2.698

Figure 15. Continued. (r)

B/A <u>2.750</u>	P <u>.965</u>	LA <u>2.719</u>	L/A <u>7.343</u>	H/A <u>2.797</u>	W/A <u>2.831</u>
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X/A	Y/A
<u>1.000</u>	<u>.000</u>
<u>1.125</u>	<u>.199</u>
<u>1.225</u>	<u>.395</u>
<u>1.302</u>	<u>.587</u>
<u>1.357</u>	<u>.775</u>
<u>1.394</u>	<u>.956</u>
<u>1.413</u>	<u>1.132</u>
<u>1.416</u>	<u>1.301</u>
<u>1.404</u>	<u>1.463</u>
<u>1.378</u>	<u>1.617</u>
<u>1.340</u>	<u>1.763</u>
<u>1.290</u>	<u>1.900</u>
<u>1.230</u>	<u>2.029</u>
<u>1.160</u>	<u>2.149</u>
<u>1.082</u>	<u>2.259</u>
<u>.996</u>	<u>2.360</u>
<u>.903</u>	<u>2.450</u>
<u>.803</u>	<u>2.531</u>
<u>.698</u>	<u>2.601</u>
<u>.589</u>	<u>2.660</u>
<u>.476</u>	<u>2.709</u>
<u>.360</u>	<u>2.748</u>
<u>.241</u>	<u>2.775</u>
<u>.121</u>	<u>2.791</u>
<u>.000</u>	<u>2.797</u>

Figure 15. Continued. (s)

B/A <u>2.750</u>	P <u>.952</u>	LA <u>2.773</u>	L/A <u>7.594</u>	H/A <u>2.896</u>	W/A <u>2.897</u>
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X/A	Y/A
<u>1.000</u>	<u>.000</u>
<u>1.129</u>	<u>.198</u>
<u>1.232</u>	<u>.394</u>
<u>1.314</u>	<u>.585</u>
<u>1.374</u>	<u>.772</u>
<u>1.416</u>	<u>.954</u>
<u>1.440</u>	<u>1.130</u>
<u>1.449</u>	<u>1.300</u>
<u>1.442</u>	<u>1.462</u>
<u>1.423</u>	<u>1.618</u>
<u>1.391</u>	<u>1.766</u>
<u>1.347</u>	<u>1.907</u>
<u>1.293</u>	<u>2.039</u>
<u>1.230</u>	<u>2.162</u>
<u>1.157</u>	<u>2.277</u>
<u>1.077</u>	<u>2.382</u>
<u>.990</u>	<u>2.478</u>
<u>.896</u>	<u>2.565</u>
<u>.796</u>	<u>2.642</u>
<u>.691</u>	<u>2.709</u>
<u>.583</u>	<u>2.766</u>
<u>.470</u>	<u>2.812</u>
<u>.355</u>	<u>2.849</u>
<u>.238</u>	<u>2.875</u>
<u>.120</u>	<u>2.890</u>
<u>.000</u>	<u>2.896</u>

Figure 15. Continued. (t)

B/A <u>2.750</u>	P <u>.940</u>	L/A <u>2.828</u>	L/A <u>7.845</u>	H/A <u>2.994</u>	W/A <u>2.962</u>
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X/A	Y/A
1.000	.000
1.137	.206
1.247	.408
1.334	.606
1.398	.799
1.444	.987
1.470	1.169
1.481	1.345
1.476	1.513
1.457	1.674
1.425	1.827
1.381	1.972
1.326	2.109
1.262	2.236
1.188	2.355
1.106	2.464
1.016	2.563
.920	2.653
.818	2.732
.710	2.801
.599	2.860
.483	2.908
.365	2.946
.245	2.973
.123	2.989
.001	2.994

Figure 15. Continued. (u)

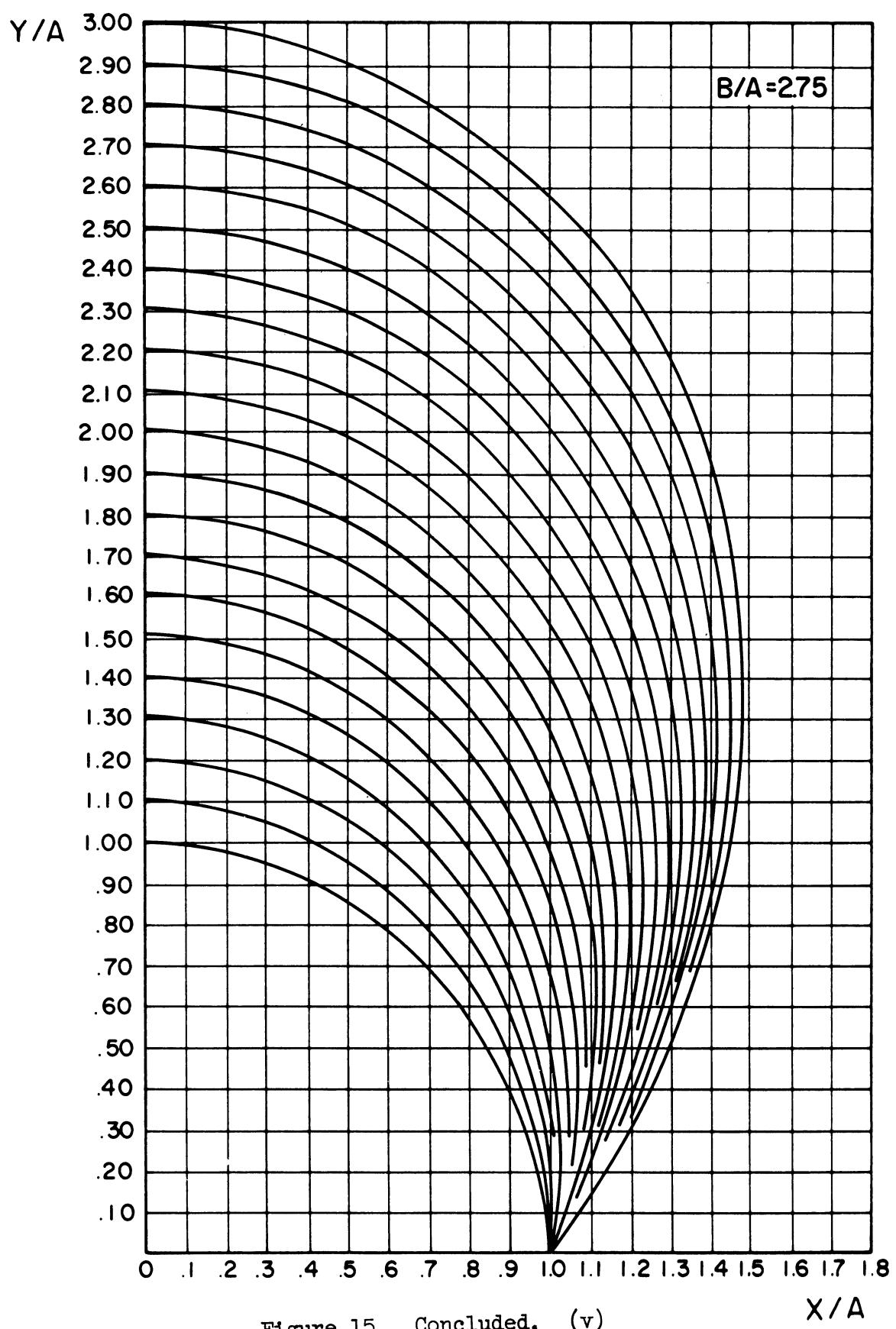


Figure 15. Concluded. (v)

B/A	P	LA	L/A	H/A	W/A
3.000	1.645	1.945	3.116	1.001	2.000

X/A	Y/A
1.000	.000
.987	.108
.966	.211
.936	.309
.899	.401
.855	.487
.805	.567
.750	.641
.689	.708
.624	.769
.555	.823
.482	.870
.406	.909
.328	.942
.248	.968
.166	.986
.084	.997
.000	1.001

Figure 16. (a)

B/A	P	LA	L/A	H/A	W/A
3.000	1.561	1.966	3.311	1.100	2.000

X/A	Y/A
1.000	.000
.996	.111
.983	.218
.962	.319
.932	.415
.895	.506
.852	.592
.802	.671
.747	.744
.687	.810
.622	.870
.553	.924
.480	.970
.405	1.010
.327	1.042
.243	1.067
.166	1.085
.084	1.096
.001	1.100

Figure 16. Continued. (b)

B/A	P	LA	L/A	H/A	W/A
3.000	1.486	1.996	3.519	1.200	2.010

X/A	Y/A
1.000	.000
1.005	.120
.999	.235
.982	.345
.957	.450
.923	.549
.882	.642
.833	.729
.778	.808
.715	.882
.650	.947
.579	1.006
.504	1.057
.425	1.101
.344	1.137
.260	1.164
.175	1.184
.088	1.196
.001	1.200

Figure 16. Continued. (c)

B/A	P	LA	L/A	H/A	W/A
3.000	1.420	2.032	3.734	1.301	2.029

X/A	Y/A
1.000	.000
1.013	.122
1.015	.239
1.006	.352
.983	.461
.961	.564
.926	.661
.883	.752
.833	.837
.777	.916
.716	.988
.649	1.052
.578	1.110
.502	1.160
.424	1.203
.343	1.238
.259	1.266
.174	1.285
.087	1.297
.001	1.301

Figure 16. Continued. (d)

B/A	P	LA	L/A	H/A	W/A
3.000	1.361	2.072	3.955	1.401	2.060

X/A	Y/A
1.000	.000
1.021	.123
1.030	.243
1.028	.358
1.017	.470
.996	.576
.967	.677
.930	.773
.886	.863
.835	.946
.778	1.024
.716	1.094
.649	1.158
.577	1.214
.502	1.263
.423	1.305
.342	1.340
.258	1.367
.173	1.386
.087	1.398
.000	1.401

Figure 16. Continued. (e)

B/A	P	LA	L/A	H/A	W/A
3.000	1.308	2.113	4.176	1.500	2.098

X/A	Y/A
1.000	.000
1.028	.124
1.044	.246
1.049	.363
1.044	.477
1.030	.587
1.007	.691
.975	.791
.937	.884
.891	.972
.839	1.054
.781	1.130
.717	1.199
.650	1.261
.578	1.316
.502	1.365
.423	1.406
.342	1.440
.258	1.480
.173	1.485
.087	1.496
.001	1.500

Figure 16. Continued. (f)

B/A	P	LA	L/A	H/A	W/A
3.000	1.261	2.159	4.463	1.600	2.139

X/A	Y/A
1.000	.000
1.036	.131
1.058	.260
1.069	.385
1.069	.506
1.058	.623
1.037	.734
1.008	.840
.970	.941
.924	1.035
.871	1.123
.812	1.203
.747	1.277
.677	1.344
.603	1.404
.524	1.455
.442	1.499
.357	1.536
.270	1.564
.181	1.584
.091	1.596
.000	1.600

Figure 16. Continued. (g)

B/A	P	LA	L/A	H/A	W/A
3.000	1.219	2.205	4.638	1.699	2.188

X/A	Y/A
1.000	.000
1.042	.132
1.071	.262
1.088	.388
1.094	.511
1.089	.630
1.074	.744
1.051	.854
1.018	.958
.978	1.056
.930	1.148
.876	1.233
.815	1.312
.749	1.384
.679	1.449
.603	1.507
.524	1.558
.442	1.600
.357	1.636
.270	1.663
.181	1.683
.092	1.695
.001	1.699

Figure 16. Continued. (h)

B/A	P	LA	L/A	H/A	W/A
3.000	1.180	2.256	4.882	1.801	2.238

X/A	Y/A
1.000	.000
1.050	.139
1.086	.276
1.109	.410
1.119	.540
1.118	.666
1.106	.787
1.083	.903
1.052	1.013
1.012	1.117
.964	1.215
.909	1.306
.847	1.390
.779	1.466
.706	1.536
.628	1.597
.546	1.651
.460	1.697
.372	1.734
.281	1.764
.188	1.785
.095	1.797
.000	1.801

Figure 16. Continued. (i)

B/A	P	LA	L/A	H/A	W/A
3.000	1.146	2.306	5.120	1.900	2.292

X/A	Y/A
1.000	.000
1.058	.146
1.101	.289
1.129	.430
1.144	.567
1.146	.700
1.137	.827
1.116	.950
1.086	1.066
1.046	1.176
.998	1.279
.942	1.376
.879	1.464
.809	1.546
.734	1.619
.653	1.684
.568	1.741
.479	1.789
.387	1.829
.293	1.860
.197	1.882
.099	1.896
.001	1.900

Figure 16. Continued. (j)

B/A 3.000	P 1.115	LA 2.356	L/A 5.358	H/A 1.998	W/A 2.349
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.064	.146
1.112	.290
1.146	.431
1.166	.569
1.174	.704
1.171	.833
1.156	.958
1.131	1.077
1.097	1.190
1.054	1.297
1.003	1.397
.945	1.491
.880	1.577
.809	1.656
.733	1.726
.652	1.790
.567	1.845
.478	1.891
.386	1.930
.292	1.960
.196	1.981
.099	1.994
.001	1.998

Figure 16. Continued. (k)

B/A 3.000	P 1.087	LA 2.410	L/A 5.610	H/A 2.101	W/A 2.406
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.072	.153
1.127	.304
1.166	.452
1.191	.597
1.203	.738
1.202	.874
1.189	1.005
1.166	1.131
1.132	1.250
1.089	1.362
1.037	1.468
.978	1.566
.912	1.657
.839	1.740
.760	1.814
.676	1.881
.588	1.939
.496	1.988
.400	2.028
.302	2.060
.203	2.083
.102	2.096
.000	2.101

Figure 16. Continued. (l)

B/A	P	LA	L/A	H/A	W/A
3.000	1.062	2.463	5.856	2.200	2.466

X/A	Y/A
1.000	.000
1.080	.159
1.141	.317
1.187	.472
1.216	.624
1.231	.771
1.233	.914
1.222	1.051
1.200	1.182
1.167	1.307
1.124	1.425
1.071	1.536
1.011	1.639
.943	1.734
.868	1.821
.787	1.899
.700	1.969
.609	2.030
.514	2.082
.415	2.124
.314	2.157
.210	2.181
.106	2.195
.000	2.200

Figure 16. Continued. (m)

B/A	P	LA	L/A	H/A	W/A
3.000	1.039	2.516	6.100	2.298	2.528

X/A	Y/A
1.000	.000
1.084	.159
1.151	.317
1.201	.472
1.236	.624
1.257	.773
1.264	.917
1.259	1.056
1.242	1.189
1.215	1.316
1.177	1.437
1.131	1.551
1.076	1.658
1.013	1.758
.943	1.850
.867	1.933
.785	2.009
.698	2.076
.606	2.135
.511	2.184
.413	2.225
.312	2.257
.209	2.280
.105	2.294
.001	2.298

Figure 16. Continued. (n)

B/A	P	LA	L/A	H/A	W/A
<u>3.000</u>	<u>1.018</u>	<u>2.570</u>	<u>6.352</u>	<u>2.399</u>	<u>2.590</u>

X/A	Y/A
1.000	.000
1.092	.166
1.166	.330
1.222	.492
1.261	.651
1.285	.806
1.295	.956
1.292	<u>1.101</u>
1.276	1.240
1.250	1.373
1.212	1.499
1.165	1.619
1.109	1.730
1.045	1.834
.973	1.930
.895	2.018
.811	2.097
.721	2.167
.627	2.228
.528	2.280
.427	2.323
.322	2.356
.216	2.380
.109	2.394
.001	2.399

Figure 16. Continued. (e)

B/A	P	LA	L/A	H/A	W/A
<u>3.000</u>	<u>.999</u>	<u>2.625</u>	<u>6.604</u>	<u>2.499</u>	<u>2.652</u>

X/A	Y/A
1.000	.000
1.100	.172
1.180	.343
1.242	.512
1.286	.677
1.313	.838
1.326	.995
1.325	<u>1.146</u>
1.311	1.291
1.284	1.430
1.247	1.561
1.200	1.685
1.143	1.802
1.077	1.910
1.004	2.010
.923	2.101
.837	2.184
.744	2.257
.647	2.320
.546	2.375
.441	2.419
.333	2.454
.224	2.479
.112	2.494
.001	2.499

Figure 16. Continued. (p)

B/A	P	LA	L/A	H/A	W/A
3.000	.982	2.682	6.863	2.601	2.717

X/A	Y/A
1.000	.000
1.109	.179
1.195	.357
1.262	.533
1.311	.705
1.342	.873
1.358	1.035
1.358	1.193
1.345	1.344
1.320	1.488
1.283	1.625
1.235	1.754
1.177	1.876
1.110	1.988
1.035	2.092
.952	2.187
.863	2.273
.768	2.349
.667	2.416
.563	2.472
.455	2.518
.344	2.555
.230	2.581
.116	2.596
.000	2.601

Figure 16. Continued. (q)

B/A	P	LA	L/A	H/A	W/A
3.000	.966	2.736	7.114	2.700	2.783

X/A	Y/A
1.000	.000
1.117	.186
1.210	.371
1.283	.553
1.336	.731
1.371	.906
1.389	1.075
1.392	1.238
1.380	1.395
1.355	1.545
1.318	1.687
1.269	1.821
1.210	1.947
1.142	2.064
1.065	2.172
.980	2.271
.889	2.360
.791	2.439
.688	2.508
.581	2.566
.469	2.614
.355	2.652
.238	2.679
.120	2.695
.001	2.700

Figure 16. Continued. (r)

B/A	P	LA	L/A	H/A	W/A
3.000	.951	2.793	7.373	2.802	2.851

X/A	Y/A
1.000	.000
1.120	.185
1.218	.369
1.296	.551
1.353	.730
1.394	.904
1.417	1.074
1.425	1.238
1.420	1.396
1.401	1.548
1.369	1.693
1.327	1.830
1.274	1.959
1.212	2.080
1.141	2.192
1.062	2.296
.976	2.391
.884	2.476
.785	2.552
.682	2.618
.575	2.674
.464	2.720
.351	2.756
.235	2.782
.118	2.797
.001	2.802

Figure 16. Continued. (s)

B/A	P	LA	L/A	H/A	W/A
3.000	.937	2.850	7.632	2.904	2.917

X/A	Y/A
1.000	.000
1.129	.192
1.233	.383
1.316	.572
1.378	.757
1.422	.938
1.448	1.113
1.459	1.284
1.454	1.447
1.436	1.605
1.405	1.754
1.362	1.896
1.309	2.030
1.245	2.156
1.173	2.272
1.092	2.379
1.004	2.477
.909	2.566
.808	2.644
.702	2.712
.592	2.771
.478	2.818
.361	2.856
.242	2.882
.122	2.898
.001	2.904

Figure 16. Continued. (t)

B/A <u>3.000</u>	P <u>.925</u>	L/A <u>2.906</u>	L/A <u>7.890</u>	H/A <u>3.005</u>	W/A <u>2.984</u>
---------------------	------------------	---------------------	---------------------	---------------------	---------------------

X/A	Y/A
<u>1.000</u>	<u>.000</u>
<u>1.137</u>	<u>.199</u>
<u>1.248</u>	<u>.397</u>
<u>1.336</u>	<u>.592</u>
<u>1.403</u>	<u>.784</u>
<u>1.450</u>	<u>.971</u>
<u>1.479</u>	<u>1.153</u>
<u>1.492</u>	<u>1.329</u>
<u>1.489</u>	<u>1.499</u>
<u>1.471</u>	<u>1.661</u>
<u>1.440</u>	<u>1.816</u>
<u>1.397</u>	<u>1.963</u>
<u>1.343</u>	<u>2.101</u>
<u>1.278</u>	<u>2.231</u>
<u>1.204</u>	<u>2.352</u>
<u>1.121</u>	<u>2.463</u>
<u>1.031</u>	<u>2.564</u>
<u>.934</u>	<u>2.655</u>
<u>.830</u>	<u>2.736</u>
<u>.722</u>	<u>2.807</u>
<u>.608</u>	<u>2.867</u>
<u>.491</u>	<u>2.916</u>
<u>.371</u>	<u>2.955</u>
<u>.249</u>	<u>2.983</u>
<u>.125</u>	<u>2.999</u>
<u>.000</u>	<u>3.005</u>

Figure 16. Continued. (u)

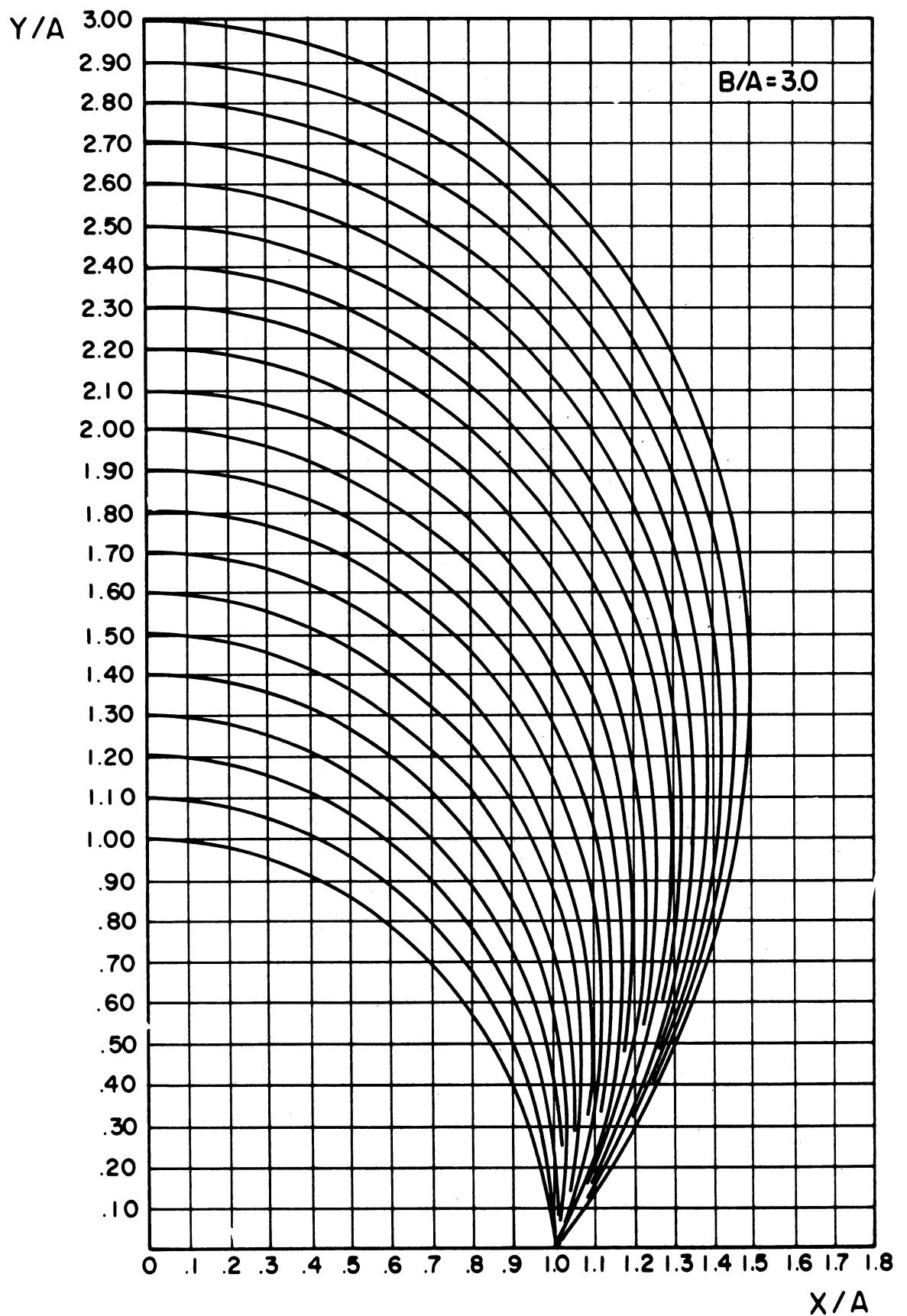


Figure 16. Concluded. (v)

B/A	P	LA	L/A	H/A	W/A
4.000	1.629	2.186	3.119	1.000	2.000

X/A	Y/A
1.000	.000
.989	.104
.970	.205
.942	.301
.907	.392
.864	.478
.816	.558
.761	.632
.700	.701
.635	.762
.565	.817
.492	.865
.415	.906
.336	.940
.254	.966
.171	.985
.086	.996
.001	1.000

Figure 17. (a)

B/A	P	LA	L/A	H/A	W/A
4.000	1.543	2.207	3.319	1.100	2.000

X/A	Y/A
1.000	.000
.998	.107
.987	.210
.968	.310
.940	.405
.905	.495
.862	.581
.813	.661
.759	.735
.698	.802
.633	.864
.564	.918
.490	.966
.414	1.007
.335	1.040
.253	1.066
.170	1.085
.086	1.096
.001	1.100

Figure 17. Continued. (b)

B/A	P	LA	L/A	H/A	W/A
<u>4.000</u>	<u>1.467</u>	<u>2.236</u>	<u>3.526</u>	<u>1.200</u>	<u>2.013</u>

X/A	Y/A
1.000	.000
<u>1.006</u>	<u>.108</u>
<u>1.003</u>	<u>.214</u>
.991	.317
.971	.416
.942	.510
.907	.600
<u>.864</u>	<u>.685</u>
.814	.764
.759	.837
.699	.904
<u>.633</u>	<u>.965</u>
.564	1.019
<u>.490</u>	<u>1.067</u>
.413	1.107
.334	1.140
.253	1.166
.170	1.185
.086	1.196
.001	1.200

Figure 17. Continued. (c)

B/A	P	LA	L/A	H/A	W/A
<u>4.000</u>	<u>1.399</u>	<u>2.271</u>	<u>3.740</u>	<u>1.299</u>	<u>2.037</u>

X/A	Y/A
1.000	.000
<u>1.015</u>	<u>.116</u>
<u>1.019</u>	<u>.229</u>
<u>1.012</u>	<u>.339</u>
.996	.446
.971	.548
.938	.645
.896	.737
.847	.823
.792	.903
.730	.976
.663	1.043
.591	1.102
<u>.515</u>	<u>1.154</u>
.435	1.198
.352	1.234
.266	1.263
.179	1.283
.090	1.295
.001	1.299

Figure 17. Continued. (d)

B/A	P	L/A	L/A	H/A	W/A
4.000	1.338	2.313	3.965	1.400	2.069

X/A	Y/A
1.000	.000
1.022	.117
1.033	.232
1.034	.344
1.025	.453
1.007	.559
.980	.660
.944	.756
.901	.840
.851	.931
.794	1.010
.732	1.082
.664	1.148
.591	1.206
.515	1.257
.434	1.300
.351	1.336
.265	1.364
.178	1.384
.089	1.396
.000	1.400

Figure 17. Continued. (e)

B/A	P	L/A	L/A	H/A	W/A
4.000	1.283	2.355	4.190	1.499	2.110

X/A	Y/A
1.000	.000
1.029	.117
1.047	.234
1.055	.348
1.052	.459
1.040	.567
1.019	.671
.990	.771
.953	.866
.908	.955
.856	1.039
.798	1.116
.735	1.187
.666	1.251
.593	1.309
.516	1.359
.435	1.401
.352	1.436
.266	1.464
.178	1.484
.090	1.495
.001	1.499

Figure 17. Continued. (f)

B/A	P	LA	L/A	H/A	W/A
4.000	1.234	2.402	4.423	1.600	2.155

X/A	Y/A
1.000	.000
1.037	.124
1.062	.246
1.075	.367
1.073	.486
1.069	.601
1.051	.712
1.024	.818
.987	.920
.943	1.015
.891	1.105
.832	1.188
.767	1.264
.696	1.333
.620	1.395
.540	1.448
.456	1.494
.368	1.532
.279	1.562
.187	1.583
.094	1.595
.001	1.600

Figure 17. Continued. (g)

B/A	P	LA	L/A	H/A	W/A
4.000	1.190	2.451	4.660	1.700	2.206

X/A	Y/A
1.000	.000
1.043	.124
1.075	.247
1.094	.369
1.103	.489
1.101	.607
1.089	.720
1.067	.830
1.036	.934
.997	1.034
.951	1.128
.897	1.216
.836	1.297
.770	1.372
.698	1.439
.621	1.499
.540	1.552
.456	1.597
.369	1.634
.279	1.662
.187	1.683
.094	1.695
.001	1.700

Figure 17. Continued. (h)

B/A 4.000	P 1.150	LA 2.502	L/A 4.900	H/A 1.799	W/A 2.259
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.051	.130
1.089	.259
1.114	.388
1.128	.514
1.129	.638
1.120	.758
1.101	.874
1.071	.985
1.033	1.091
.986	1.191
.931	1.284
.870	1.371
.801	1.450
.727	1.522
.648	1.586
.564	1.642
.476	1.690
.385	1.729
.291	1.760
.196	1.782
.099	1.795
.001	1.799

Figure 17. Continued. (i)

B/A 4.000	P 1.114	LA 2.555	L/A 5.144	H/A 1.900	W/A 2.316
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.057	.130
1.100	.260
1.132	.389
1.151	.517
1.158	.642
1.155	.764
1.141	.883
1.117	.997
1.084	1.106
1.043	1.209
.994	1.307
.937	1.398
.873	1.482
.803	1.560
.728	1.630
.648	1.692
.564	1.747
.475	1.793
.384	1.831
.290	1.861
.195	1.882
.098	1.895
.001	1.900

Figure 17. Continued. (j)

B/A <u>4.000</u>	P <u>1.082</u>	LA <u>2.609</u>	L/A <u>5.393</u>	H/A <u>2.001</u>	W/A <u>2.373</u>
---------------------	-------------------	--------------------	---------------------	---------------------	---------------------

X/A	Y/A
1.000	.000
1.064	.135
1.115	.271
1.152	.407
1.175	.541
1.187	.673
1.136	.801
1.175	.926
1.152	1.046
1.120	1.161
1.079	1.271
1.029	1.374
.971	1.470
.906	1.559
.834	1.641
.756	1.715
.673	1.781
.586	1.839
.494	1.888
.399	1.928
.302	1.960
.202	1.983
.101	1.996
.000	2.001

Figure 17. Continued. (k)

B/A <u>4.000</u>	P <u>1.053</u>	LA <u>2.664</u>	L/A <u>5.642</u>	H/A <u>2.101</u>	W/A <u>2.436</u>
---------------------	-------------------	--------------------	---------------------	---------------------	---------------------

X/A	Y/A
1.000	.000
1.072	.141
1.129	.283
1.172	.425
1.200	.565
1.215	.703
1.218	.838
1.208	.969
1.188	1.096
1.156	1.217
1.115	1.332
1.065	1.440
1.006	1.542
.939	1.636
.865	1.722
.785	1.800
.699	1.869
.609	1.930
.514	1.982
.415	2.025
.314	2.058
.210	2.082
.106	2.096
.000	2.101

Figure 17. Continued. (l)

B/A 4.000	P 1.026	LA 2.719	L/A 5.890	H/A 2.200	W/A 2.499
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.077	.140
1.139	.282
1.187	.424
1.221	.565
1.241	.704
1.249	.840
1.246	.973
1.231	1.101
1.205	1.225
1.170	1.343
1.125	1.455
1.071	1.560
1.010	1.659
.941	1.750
.866	1.833
.785	1.909
.698	1.976
.607	2.035
.512	2.085
.414	2.126
.313	2.159
.210	2.182
.105	2.196
.000	2.200

Figure 17. Continued. (m)

B/A 4.000	P 1.002	LA 2.775	L/A 6.145	H/A 2.301	W/A 2.562
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.084	.146
1.153	.293
1.206	.441
1.245	.588
1.270	.734
1.281	.876
1.279	1.015
1.266	1.149
1.241	1.279
1.206	1.402
1.161	1.520
1.107	1.630
1.044	1.733
.974	1.829
.896	1.917
.813	1.996
.723	2.066
.629	2.128
.531	2.181
.429	2.224
.324	2.258
.217	2.282
.109	2.296
.000	2.301

Figure 17. Continued. (n)

B/A	P	LA	L/A	H/A	W/A
4.000	.980	2.832	6.400	2.401	2.627

X/A	Y/A
1.000	.000
1.092	.151
1.167	.305
1.226	.459
1.270	.612
1.298	.763
1.312	.912
1.313	1.057
1.301	1.197
1.278	1.332
1.243	1.461
1.197	1.584
1.142	1.700
1.078	1.808
1.006	1.908
.927	1.999
.840	2.082
.748	2.156
.651	2.220
.549	2.275
.444	2.320
.336	2.356
.225	2.381
.113	2.396
.000	2.401

Figure 17. Continued. (e)

B/A	P	LA	L/A	H/A	W/A
4.000	.960	2.889	6.654	2.501	2.695

X/A	Y/A
1.000	.000
1.096	.151
1.176	.303
1.239	.457
1.288	.610
1.321	.762
1.341	.911
1.348	1.057
1.341	1.199
1.323	1.336
1.294	1.467
1.255	1.593
1.206	1.712
1.147	1.824
1.081	1.928
1.007	2.025
.926	2.114
.838	2.193
.746	2.265
.648	2.327
.547	2.380
.442	2.423
.334	2.457
.224	2.482
.113	2.496
.001	2.501

Figure 17. Continued. (p)

B/A	P	LA	L/A	H/A	W/A
<u>4.000</u>	<u>.941</u>	<u>2.947</u>	<u>6.915</u>	<u>2.603</u>	<u>2.763</u>

X/A	Y/A
1.000	.000
1.104	.156
1.190	.315
1.259	.474
1.312	.634
1.350	.791
1.372	.947
<u>1.381</u>	<u>1.099</u>
1.377	1.246
1.360	1.389
1.331	1.526
1.291	1.657
1.242	1.781
1.182	1.897
1.114	2.006
1.038	2.107
.955	2.199
.865	2.282
.770	2.357
.669	2.421
.564	2.477
.456	2.522
.344	2.557
.231	2.583
.116	2.598
.000	2.603

Figure 17. Continued. (q)

B/A	P	LA	L/A	H/A	W/A
<u>4.000</u>	<u>.925</u>	<u>3.004</u>	<u>7.169</u>	<u>2.702</u>	<u>2.829</u>

X/A	Y/A
1.000	.000
1.111	.162
1.204	.326
1.278	.491
1.336	.656
1.378	.820
1.403	.981
1.414	1.139
1.412	1.292
1.396	1.440
1.367	1.583
1.327	1.719
1.277	1.847
1.217	1.969
1.147	2.082
1.069	2.186
.984	2.282
.892	2.369
.794	2.446
.690	2.513
.582	2.570
.470	2.617
.356	2.654
.238	2.681
.120	2.697
.001	2.702

Figure 17. Continued. (r)

B/A	P	LA	L/A	H/A	W/A
<u>4.000</u>	<u>.909</u>	<u>3.063</u>	<u>7.430</u>	<u>2.803</u>	<u>2.896</u>

X/A	Y/A
1.000	.000
1.119	.167
1.218	.337
1.298	.509
1.361	.680
1.406	.850
1.434	1.017
1.448	1.181
1.447	1.340
1.432	1.494
1.404	1.641
1.364	1.782
1.313	1.916
1.251	2.042
1.180	2.159
1.100	2.268
1.013	2.367
.918	2.457
.817	2.537
.711	2.607
.599	2.666
.484	2.715
.366	2.754
.245	2.781
.123	2.797
.000	2.803

Figure 17. Continued. (s)

B/A	P	LA	L/A	H/A	W/A
<u>4.000</u>	<u>.896</u>	<u>3.119</u>	<u>7.683</u>	<u>2.901</u>	<u>2.961</u>

X/A	Y/A
1.000	.000
1.126	.173
1.232	.349
1.317	.526
1.384	.703
1.433	.879
1.465	1.052
1.480	1.221
1.481	1.386
1.467	1.545
1.439	1.698
1.399	1.844
1.347	1.983
1.285	2.113
1.212	2.234
1.131	2.347
1.041	2.450
.944	2.543
.840	2.625
.731	2.698
.616	2.759
.498	2.810
.376	2.850
.252	2.878
.127	2.895
.000	2.901

Figure 17. Continued. (t)

B/A	P	L/A	L/A	H/A	W/A
4.000	.883	3.174	7.927	2.995	3.028

X/A	Y/A
1.000	.000
1.133	.178
1.245	.360
1.336	.543
1.408	.725
1.460	.907
1.495	1.086
1.512	1.261
1.514	1.431
1.501	1.595
1.474	1.753
1.433	1.904
1.381	2.047
1.317	2.181
1.244	2.307
1.160	2.423
1.069	2.529
.969	2.625
.863	2.711
.751	2.786
.633	2.849
.512	2.902
.387	2.942
.260	2.972
.130	2.989
.000	2.995

Figure 17. Continued. (u)

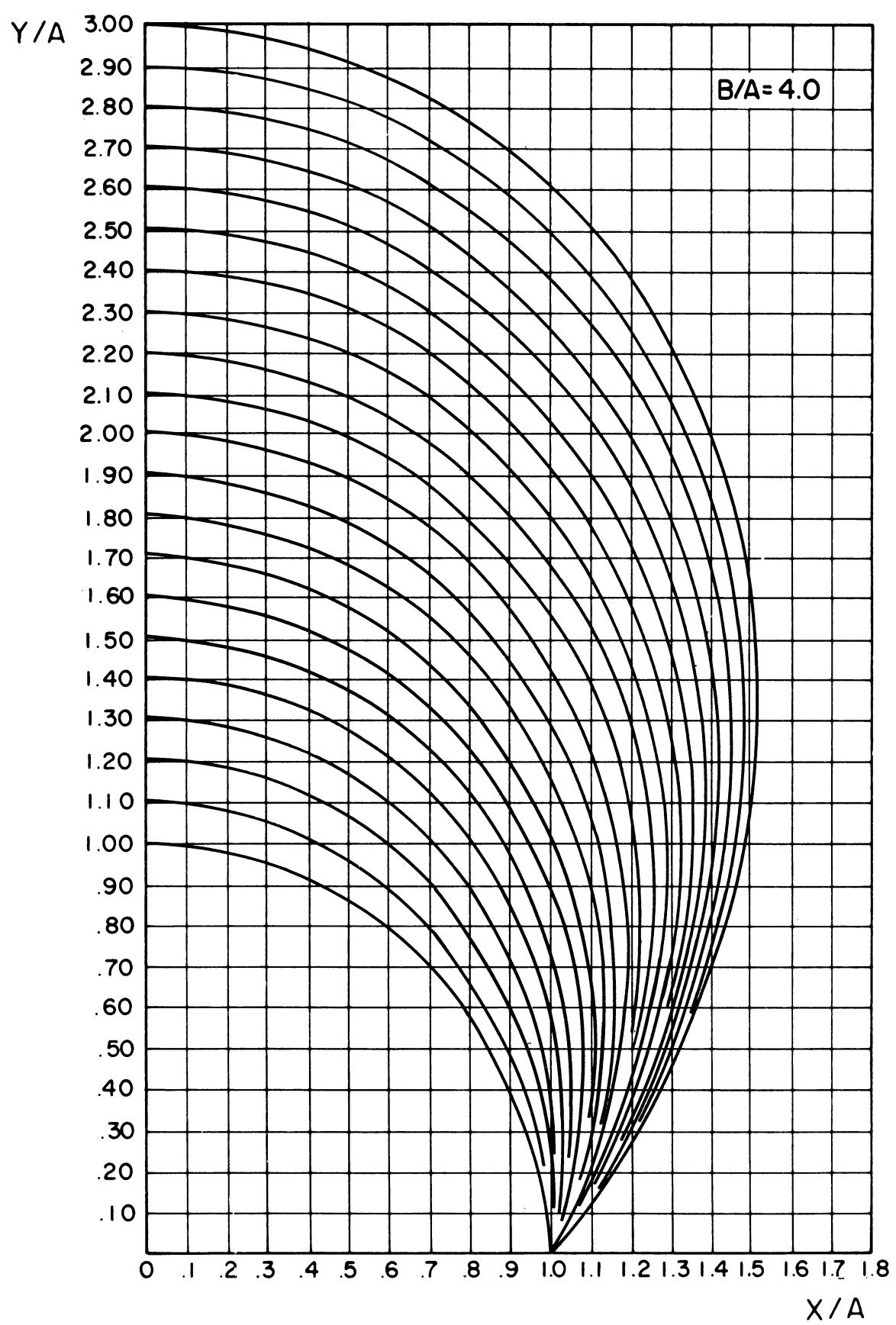


Figure 17. Concluded. (v)

B/A	P	LA	L/A	H/A	W/A
5.000	1.619	2.405	3.126	1.001	2.000

X/A	Y/A
1.000	.000
.991	.102
.972	.201
.946	.296
.912	.387
.870	.473
.822	.553
.767	.628
.707	.697
.641	.759
.571	.815
.497	.864
.420	.905
.339	.939
.257	.966
.172	.986
.086	.997
.000	1.001

Figure 18. (a)

B/A	P	LA	L/A	H/A	W/A
5.000	1.532	2.425	3.324	1.100	2.000

X/A	Y/A
1.000	.000
.999	.104
.990	.205
.971	.304
.945	.398
.910	.489
.869	.574
.821	.654
.766	.729
.706	.797
.641	.859
.571	.915
.497	.963
.419	1.005
.339	1.039
.256	1.066
.172	1.085
.087	1.096
.000	1.100

Figure 18. Continued. (b)

B/A 5.000	P 1.454	LA 2.452	L/A 3.529	H/A 1.199	W/A 2.016
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.008	.105
1.006	.209
.995	.310
.976	.408
.949	.502
.914	.591
.872	.676
.823	.756
.768	.830
.707	.898
.642	.960
.572	1.015
.498	1.063
.420	1.104
.340	1.138
.257	1.165
.173	1.184
.087	1.195
.001	1.199

Figure 18. Continued. (c)

B/A 5.000	P 1.384	LA 2.490	L/A 3.750	H/A 1.300	W/A 2.042
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.015	.107
1.021	.212
1.018	.315
1.005	.416
.985	.514
.956	.607
.920	.696
.877	.781
.827	.860
.771	.934
.710	1.001
.644	1.063
.573	1.117
.499	1.165
.421	1.206
.340	1.240
.257	1.266
.173	1.285
.087	1.297
.000	1.300

Figure 18. Continued. (d)

B/A	P	LA	L/A	H/A	W/A
5.000	1.322	2.530	3.971	1.399	2.077

X/A	Y/A
1.000	.000
1.023	.113
1.036	.225
1.038	.335
1.031	.443
1.014	.547
.988	.648
.954	.744
.912	.835
.862	.921
.806	1.001
.743	1.074
.675	1.141
.602	1.200
.524	1.252
.443	1.297
.358	1.334
.271	1.362
.182	1.383
.092	1.395
.001	1.399

Figure 18. Continued. (e)

B/A	P	LA	L/A	H/A	W/A
5.000	1.266	2.576	4.203	1.501	2.118

X/A	Y/A
1.000	.000
1.030	.113
1.050	.226
1.059	.338
1.058	.448
1.048	.555
1.028	.659
1.000	.759
.963	.854
.919	.944
.868	1.029
.810	1.128
.747	1.180
.678	1.246
.603	1.304
.525	1.356
.443	1.400
.358	1.436
.271	1.464
.182	1.484
.091	1.496
.000	1.501

Figure 18. Continued. (f)

B/A	P	LA	L/A	H/A	W/A
5.000	1.216	2.624	4.437	1.500	2.167

X/A	Y/A
1.000	.000
1.037	.113
1.062	.227
1.078	.340
1.083	.452
1.079	.561
1.066	.668
1.043	.771
1.013	.869
.974	.964
.928	1.053
.875	1.136
.816	1.214
.751	1.285
.681	1.350
.636	1.408
.527	1.458
.445	1.501
.359	1.537
.272	1.564
.182	1.534
.092	1.596
.000	1.600

Figure 18. Continued. (g)

B/A	P	LA	L/A	H/A	W/A
5.000	1.170	2.676	4.677	1.701	2.217

X/A	Y/A
1.000	.000
1.044	.119
1.077	.238
1.098	.357
1.108	.475
1.108	.591
1.098	.704
1.078	.814
1.048	.919
1.010	1.020
.984	1.115
.911	1.204
.850	1.287
.784	1.353
.711	1.433
.633	1.494
.551	1.548
.465	1.595
.376	1.633
.284	1.662
.191	1.684
.096	1.697
.000	1.701

Figure 18. Continued. (h)

B/A	P	LA	L/A	H/A	W/A
5.000	1.129	2.728	4.918	1.800	2.275

X/A	Y/A
1.000	.000
1.050	.119
1.088	.238
1.116	.358
1.132	.477
1.137	.595
1.133	.710
1.119	.822
1.095	.930
1.063	1.034
1.022	1.133
.974	1.226
.918	1.314
.856	1.395
.788	1.470
.714	1.538
.636	1.598
.553	1.651
.467	1.696
.377	1.734
.285	1.763
.191	1.784
.096	1.796
.001	1.800

Figure 18. Continued. (i)

B/A	P	LA	L/A	H/A	W/A
5.000	1.092	2.784	5.169	1.902	2.333

X/A	Y/A
1.000	.000
1.057	.124
1.103	.249
1.135	.375
1.157	.500
1.166	.624
1.165	.745
1.153	.863
1.131	.978
1.100	1.088
1.059	1.193
1.010	1.292
.954	1.385
.890	1.472
.820	1.551
.744	1.623
.662	1.687
.576	1.744
.486	1.792
.393	1.831
.297	1.862
.199	1.884
.100	1.898
.000	1.902

Figure 18. Continued. (j)

B/A	P	LA	L/A	H/A	W/A
5.000	1.059	2.838	5.412	2.000	2.393

X/A	Y/A
1.000	.000
1.065	.129
1.116	.259
1.155	.390
1.181	.522
1.195	.651
1.197	.779
1.187	.903
1.167	1.024
1.136	1.140
1.096	1.251
1.047	1.355
.989	1.454
.924	1.545
.852	1.629
.774	1.705
.689	1.773
.600	1.832
.507	1.883
.410	1.925
.310	1.958
.208	1.981
.105	1.995
.001	2.000

Figure 18. Continued. (k)

B/A	P	LA	L/A	H/A	W/A
5.000	1.028	2.895	5.662	2.100	2.457

X/A	Y/A
1.000	.000
1.070	.128
1.126	.258
1.170	.390
1.202	.521
1.221	.652
1.228	.780
1.225	.907
1.210	1.029
1.185	1.148
1.151	1.262
1.107	1.370
1.055	1.472
.995	1.568
.928	1.657
.855	1.739
.775	1.813
.690	1.879
.600	1.937
.506	1.986
.409	2.027
.309	2.059
.208	2.081
.105	2.095
.001	2.100

Figure 18. Continued. (l)

B/A 5.000	P 1.001	LA 2.953	L/A 5.917	H/A 2.201	W/A 2.520
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.077	.133
1.140	.268
1.190	.405
1.226	.543
1.249	.679
1.260	.814
1.259	.946
1.246	1.075
1.222	1.200
1.188	1.319
1.144	1.433
1.092	1.541
1.030	1.641
.961	1.735
.886	1.821
.803	1.899
.715	1.968
.622	2.029
.525	2.081
.424	2.124
.321	2.157
.215	2.181
.108	2.196
-.000	2.201

Figure 18. Continued. (m)

B/A 5.000	P .976	LA 3.010	L/A 6.166	H/A 2.298	W/A 2.584
--------------	-----------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.084	.137
1.154	.278
1.209	.421
1.250	.564
1.277	.706
1.291	.847
1.292	.985
1.281	1.119
1.258	1.250
1.225	1.375
1.181	1.494
1.128	1.606
1.065	1.712
.995	1.810
.917	1.900
.832	1.982
.741	2.055
.645	2.119
.545	2.173
.440	2.218
.333	2.253
.223	2.278
.112	2.293
.000	2.298

Figure 18. Continued. (n)

B/A	P	LA	L/A	H/A	W/A
5.000	.954	3.068	6.421	2.398	2.653

X/A	Y/A
1.000	.000
1.088	.137
1.162	.276
1.222	.418
1.268	.561
1.300	.704
1.320	.845
1.326	.984
1.321	1.120
1.304	1.252
1.277	1.380
1.239	1.502
1.191	1.618
1.134	1.728
1.069	1.833
.997	1.926
.917	2.013
.831	2.092
.740	2.163
.643	2.224
.542	2.277
.438	2.320
.331	2.354
.222	2.378
.112	2.393
.000	2.398

Figure 18. Continued. (o)

B/A	P	LA	L/A	H/A	W/A
5.000	.933	3.127	6.676	2.497	2.720

X/A	Y/A
1.000	.000
1.095	.141
1.176	.286
1.241	.433
1.292	.582
1.328	.730
1.351	.877
1.360	1.022
1.356	1.164
1.341	1.301
1.314	1.434
1.276	1.562
1.228	1.683
1.170	1.797
1.104	1.905
1.029	2.004
.947	2.095
.859	2.178
.765	2.251
.665	2.316
.561	2.371
.453	2.416
.343	2.451
.230	2.477
.116	2.492
.000	2.497

Figure 18. Continued. (p)

B/A	P	LA	L/A	H/A	W/A
<u>5.000</u>	<u>.913</u>	<u>3.188</u>	<u>6.939</u>	<u>2.599</u>	<u>2.788</u>

X/A	Y/A
1.000	.000
1.103	.146
1.189	.296
1.260	.449
1.316	.603
1.356	.757
1.382	.910
1.394	1.061
1.392	1.209
1.378	1.352
1.352	1.490
1.314	1.623
1.265	1.750
1.206	1.869
1.139	1.981
1.062	2.084
.978	2.179
.887	2.265
.790	2.342
.687	2.409
.580	2.467
.469	2.514
.354	2.551
.237	2.577
.119	2.593
.000	2.599

Figure 18. Continued. (q)

B/A	P	LA	L/A	H/A	W/A
<u>5.000</u>	<u>.895</u>	<u>3.248</u>	<u>7.203</u>	<u>2.700</u>	<u>2.858</u>

X/A	Y/A
1.000	.000
1.110	.151
1.203	.306
1.280	.465
1.341	.624
1.385	.784
1.414	.943
1.429	1.100
1.429	1.254
1.416	1.403
1.390	1.547
1.352	1.685
1.303	1.816
1.243	1.940
1.174	2.057
1.096	2.165
1.009	2.264
.916	2.353
.815	2.433
.710	2.503
.599	2.563
.484	2.612
.366	2.650
.246	2.678
.123	2.695
.000	2.700

Figure 18. Continued. (r)

B/A	P	LA	L/A	H/A	W/A
5.000	.879	3.311	7.475	2.804	2.932

X/A	Y/A
1.000	.000
1.118	.156
1.218	.317
1.300	.481
1.366	.647
1.414	.813
1.447	.978
1.464	1.141
1.466	1.300
1.454	1.455
1.429	1.605
1.391	1.748
1.341	1.885
1.281	2.014
1.210	2.135
1.130	2.247
1.041	2.350
.945	2.444
.842	2.527
.732	2.600
.618	2.662
.500	2.713
.378	2.753
.254	2.781
.127	2.799
.001	2.804

Figure 18. Continued. (s)

B/A	P	LA	L/A	H/A	W/A
5.000	.863	3.375	7.755	2.912	3.009

X/A	Y/A
1.000	.000
1.121	.155
1.225	.315
1.312	.478
1.382	.643
1.436	.809
1.474	.974
1.497	1.137
1.505	1.298
1.499	1.454
1.480	1.606
1.448	1.752
1.405	1.891
1.351	2.024
1.287	2.149
1.213	2.266
1.130	2.375
1.040	2.474
.942	2.564
.838	2.645
.729	2.715
.615	2.774
.497	2.824
.375	2.862
.252	2.889
.126	2.906
.000	2.912

Figure 18. Continued. (t)

B/A 5.000	P .848	L/A 3.441	L/A 8.044	H/A 3.022	W/A 3.087
--------------	-----------	--------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.129	.160
1.240	.326
1.333	.495
1.408	.666
1.466	.838
1.508	1.009
1.533	1.179
1.543	1.345
1.539	1.508
1.521	1.665
1.489	1.817
1.446	1.962
1.391	2.100
1.325	2.230
1.249	2.352
1.165	2.464
1.072	2.568
.971	2.661
.864	2.744
.752	2.817
.634	2.879
.512	2.930
.387	2.970
.259	2.999
.130	3.016
-.000	3.022

Figure 18. Continued. (u)

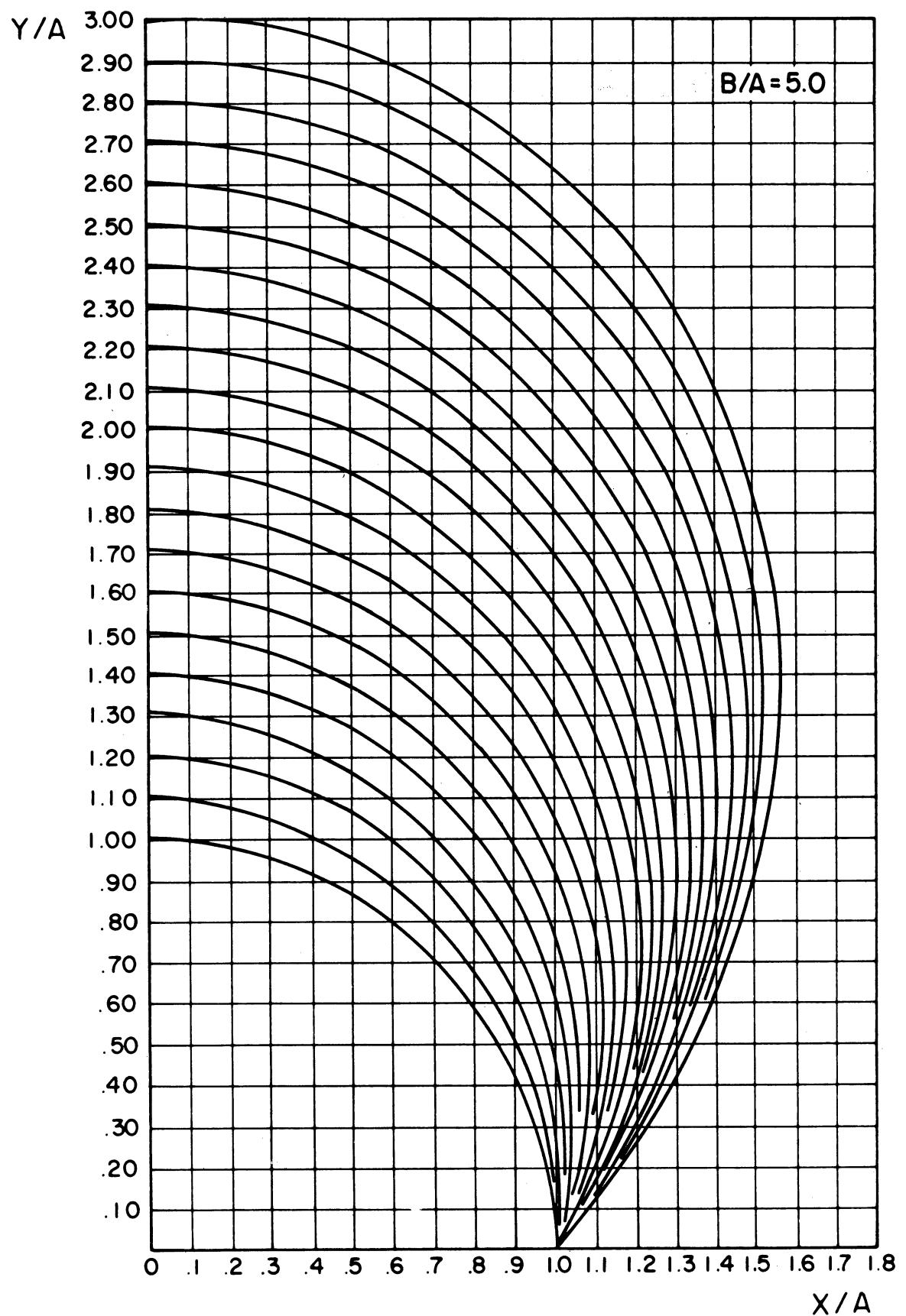


Figure 18. Concluded. (v)

B/A	P	LA	L/A	H/A	W/A
6.000	1.612	2.634	3.126	1.000	2.000

X/A	Y/A
1.000	.000
.991	.100
.974	.198
.948	.292
.915	.382
.874	.468
.826	.549
.772	.624
.712	.693
.646	.755
.576	.812
.502	.861
.424	.903
.343	.938
.259	.965
.174	.984
.088	.996
.001	1.000

Figure 19. (a)

B/A	P	LA	L/A	H/A	W/A
6.000	1.524	2.623	3.326	1.100	2.000

X/A	Y/A
1.000	.000
1.000	.102
.991	.202
.974	.300
.948	.394
.915	.484
.874	.569
.826	.649
.772	.724
.712	.793
.646	.856
.576	.912
.502	.961
.424	1.003
.343	1.038
.259	1.065
.174	1.084
.088	1.096
.001	1.100

Figure 19. Continued. (b)

B/A 6.000	P 1.445	LA 2.652	L/A 3.536	H/A 1.200	W/A 2.017
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.008	.103
1.008	.205
.998	.305
.980	.403
.953	.496
.919	.586
.877	.671
.829	.751
.774	.826
.714	.895
.648	.957
.577	1.013
.503	1.062
.425	1.104
.343	1.138
.260	1.165
.174	1.184
.088	1.196
.001	1.200

Figure 19. Continued. (c)

B/A 6.000	P 1.374	LA 2.689	L/A 3.756	H/A 1.301	W/A 2.046
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.016	.104
1.023	.208
1.020	.310
1.009	.410
.989	.507
.962	.600
.926	.690
.884	.775
.834	.854
.779	.929
.717	.997
.651	1.059
.580	1.115
.505	1.163
.426	1.205
.344	1.239
.261	1.266
.175	1.285
.088	1.297
.000	1.301

Figure 19. Continued. (d)

B/A 6.000	P 1.310	LA 2.732	L/A 3.983	H/A 1.402	W/A 2.083
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.024	.110
1.038	.220
1.041	.329
1.035	.436
1.019	.540
.994	.641
.961	.737
.919	.829
.870	.916
.814	.996
.751	1.070
.682	1.138
.609	1.198
.530	1.252
.448	1.297
.362	1.334
.274	1.364
.184	1.385
.092	1.397
.000	1.402

Figure 19. Continued. (e)

B/A 6.000	P 1.253	LA 2.777	L/A 4.209	H/A 1.500	W/A 2.124
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.031	.110
1.051	.221
1.062	.331
1.062	.440
1.053	.546
1.034	.649
1.007	.749
.971	.845
.928	.936
.877	1.021
.819	1.101
.756	1.174
.686	1.240
.612	1.300
.533	1.352
.450	1.397
.364	1.434
.276	1.462
.185	1.483
.093	1.496
.001	1.500

Figure 19. Continued. (f)

B/A 6.000	P 1.202	LA 2.828	L/A 4.446	H/A 1.600	W/A 2.174
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.037	.110
1.064	.221
1.081	.333
1.087	.443
1.084	.551
1.072	.657
1.051	.760
1.021	.859
.983	.954
.937	1.044
.885	1.128
.826	1.207
.761	1.279
.690	1.345
.615	1.404
.535	1.455
.451	1.499
.365	1.535
.276	1.564
.185	1.584
.093	1.596
.000	1.600

Figure 19. Continued. (g)

B/A 6.000	P 1.156	LA 2.881	L/A 4.686	H/A 1.700	W/A 2.227
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.045	.115
1.078	.232
1.101	.349
1.112	.465
1.113	.560
1.104	.692
1.085	.802
1.057	.907
1.020	1.008
.974	1.104
.921	1.194
.861	1.279
.794	1.356
.721	1.426
.643	1.489
.560	1.544
.473	1.591
.382	1.630
.289	1.661
.194	1.683
.098	1.696
.000	1.700

Figure 19. Continued. (h)

B/A 6.000	P 1.114	LA 2.936	L/A 4.929	H/A 1.800	W/A 2.285
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.050	.115
1.090	.231
1.113	.349
1.135	.466
1.143	.582
1.139	.697
1.126	.808
1.104	.917
1.073	1.021
1.033	1.121
.985	1.215
.929	1.304
.867	1.387
.799	1.463
.725	1.532
.645	1.593
.562	1.648
.474	1.694
.383	1.732
.290	1.762
.195	1.783
.098	1.796
.001	1.800

Figure 19. Continued. (i)

B/A 6.000	P 1.076	LA 2.992	L/A 5.177	H/A 1.900	W/A 2.343
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.058	.119
1.104	.241
1.138	.364
1.160	.487
1.171	.609
1.172	.730
1.161	.848
1.140	.962
1.110	1.073
1.071	1.179
1.022	1.279
.966	1.373
.902	1.461
.832	1.542
.755	1.615
.673	1.686
.586	1.738
.495	1.787
.400	1.828
.303	1.859
.203	1.882
.102	1.896
.001	1.900

Figure 19. Continued. (j)

B/A	P	LA	L/A	H/A	W/A
<u>6.000</u>	<u>1.041</u>	<u>3.051</u>	<u>5.429</u>	<u>2.001</u>	<u>2.408</u>

X/A	Y/A
1.000	.000
<u>1.063</u>	<u>.119</u>
1.114	.240
1.153	.363
1.181	.487
1.198	.610
1.204	.732
<u>1.199</u>	<u>.852</u>
1.185	.969
1.160	1.082
1.126	1.191
1.083	1.295
1.032	1.393
<u>.974</u>	<u>1.486</u>
.908	1.572
.836	1.651
.758	1.723
.675	1.787
.587	1.843
<u>.496</u>	<u>1.891</u>
.401	1.930
.303	1.961
.203	1.983
.102	1.997
.000	2.001

Figure 19. Continued. (k)

B/A	P	LA	L/A	H/A	W/A
<u>6.000</u>	<u>1.011</u>	<u>3.109</u>	<u>5.680</u>	<u>2.100</u>	<u>2.471</u>

X/A	Y/A
1.000	.000
<u>1.070</u>	<u>.123</u>
1.127	.249
1.172	.378
1.205	.507
1.226	.636
1.236	.763
<u>1.233</u>	<u>.889</u>
1.220	1.012
1.197	1.131
1.164	1.246
1.121	1.355
1.069	1.459
<u>1.010</u>	<u>1.556</u>
.942	1.647
.868	1.730
.788	1.806
.702	1.874
.611	1.933
<u>.516</u>	<u>1.984</u>
.417	2.025
.315	2.058
.211	2.081
.106	2.095
.000	2.100

Figure 19. Continued. (l)

B/A 6.000	P .982	LA 3.170	L/A 5.937	H/A 2.201	W/A 2.536
--------------	-----------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.077	.128
1.141	.259
1.192	.392
1.230	.527
1.255	.662
1.267	.795
1.268	.927
1.257	1.056
1.235	1.181
1.202	1.301
1.159	1.416
1.107	1.526
1.046	1.628
.977	1.724
.900	1.811
.817	1.891
.728	1.962
.634	2.025
.535	2.078
.433	2.122
.327	2.156
.219	2.181
.110	2.196
-.000	2.201

Figure 19. Continued. (m)

B/A 6.000	P .956	LA 3.229	L/A 6.187	H/A 2.298	W/A 2.605
--------------	-----------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.081	.126
1.150	.257
1.205	.390
1.248	.524
1.278	.659
1.296	.793
1.302	.926
1.297	1.056
1.281	1.183
1.254	1.305
1.217	1.423
1.170	1.536
1.115	1.643
1.052	1.743
.981	1.835
.903	1.921
.819	1.998
.729	2.067
.634	2.128
.535	2.179
.432	2.222
.327	2.255
.219	2.279
.110	2.294
.001	2.298

Figure 19. Continued. (n)

B/A 6.000	P .933	LA 3.291	L/A 6.450	H/A 2.400	W/A 2.673
--------------	-----------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.088	.131
1.163	.266
1.224	.404
1.272	.544
1.306	.684
1.328	.824
1.337	.963
1.333	1.099
1.318	1.231
1.292	1.360
1.255	1.483
1.208	1.601
1.152	1.713
1.087	1.817
1.015	1.915
.934	2.004
.847	2.085
.755	2.158
.656	2.221
.554	2.275
.448	2.320
.338	2.355
.227	2.380
.114	2.395
.000	2.400

Figure 19. Continued. (o)

B/A 6.000	P .911	LA 3.352	L/A 6.707	H/A 2.499	W/A 2.741
--------------	-----------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.095	.135
1.176	.275
1.243	.418
1.296	.563
1.334	.709
1.359	.854
1.371	.998
1.369	1.140
1.356	1.278
1.330	1.412
1.293	1.541
1.246	1.664
1.189	1.781
1.123	1.890
1.048	1.992
.966	2.085
.876	2.170
.781	2.246
.679	2.312
.573	2.369
.464	2.415
.351	2.452
.235	2.478
.118	2.494
.000	2.499

Figure 19. Continued. (p)

B/A 6.000	P .891	LA 3.414	L/A 6.970	H/A 2.600	W/A 2.811
--------------	-----------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.102	.139
1.190	.284
1.262	.432
1.320	.582
1.363	.734
1.391	.885
1.405	1.035
1.406	1.183
1.393	1.327
1.369	1.467
1.332	1.601
1.284	1.729
1.226	1.851
1.159	1.965
1.082	2.071
.997	2.168
.905	2.257
.807	2.336
.702	2.405
.593	2.464
.479	2.513
.362	2.551
.243	2.578
.122	2.594
.000	2.600

Figure 19. Continued. (q)

B/A 6.000	P .873	LA 3.477	L/A 7.234	H/A 2.701	W/A 2.884
--------------	-----------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.110	.143
1.204	.293
1.282	.446
1.344	.602
1.391	.759
1.423	.917
1.439	1.072
1.442	1.226
1.431	1.376
1.407	1.521
1.371	1.661
1.323	1.794
1.264	1.920
1.194	2.039
1.116	2.150
1.029	2.251
.934	2.343
.833	2.425
.725	2.497
.612	2.559
.495	2.610
.374	2.649
.251	2.678
.126	2.695
-.000	2.701

Figure 19. Continued. (r)

B/A <u>6.000</u>	P .856	LA 3.539	L/A 7.499	H/A 2.801	W/A
---------------------	-----------	-------------	--------------	--------------	-----

X/A	Y/A
1.000	.000
1.113	.142
1.210	.290
1.292	.442
1.359	.597
1.411	.754
1.448	.910
1.470	1.066
1.479	1.220
1.474	1.371
1.456	1.518
1.426	1.660
1.384	1.796
1.332	1.925
1.269	2.048
1.197	2.163
1.116	2.270
1.028	2.368
.932	2.457
.829	2.536
.721	2.606
.609	2.665
.492	2.714
.372	2.752
.249	2.779
.125	2.796
-.000	2.801

Figure 19. Continued. (s)

B/A <u>6.000</u>	P .841	LA 3.602	L/A 7.764	H/A 2.902	W/A 3.029
---------------------	-----------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.120	.146
1.223	.299
1.311	.456
1.383	.616
1.439	.778
1.479	.941
1.504	1.102
1.515	1.261
1.511	1.418
1.494	1.570
1.465	1.717
1.423	1.858
1.370	1.993
1.306	2.120
1.232	2.240
1.149	2.350
1.058	2.452
.960	2.544
.854	2.627
.743	2.699
.627	2.760
.507	2.811
.383	2.851
.257	2.879
.129	2.896
.000	2.902

Figure 19. Continued. (t)

B/A <u>6.000</u>	P <u>.827</u>	L/A <u>3.664</u>	L/A <u>8.029</u>	H/A <u>3.002</u>	W/A <u>3.101</u>
---------------------	------------------	---------------------	---------------------	---------------------	---------------------

X/A	Y/A
<u>1.000</u>	<u>.000</u>
<u>1.127</u>	<u>.150</u>
<u>1.237</u>	<u>.308</u>
<u>1.330</u>	<u>.470</u>
<u>1.406</u>	<u>.635</u>
<u>1.466</u>	<u>.803</u>
<u>1.510</u>	<u>.971</u>
<u>1.538</u>	<u>1.138</u>
<u>1.551</u>	<u>1.303</u>
<u>1.549</u>	<u>1.465</u>
<u>1.532</u>	<u>1.622</u>
<u>1.503</u>	<u>1.775</u>
<u>1.461</u>	<u>1.921</u>
<u>1.407</u>	<u>2.060</u>
<u>1.342</u>	<u>2.192</u>
<u>1.267</u>	<u>2.316</u>
<u>1.182</u>	<u>2.431</u>
<u>1.089</u>	<u>2.536</u>
<u>.988</u>	<u>2.632</u>
<u>.879</u>	<u>2.717</u>
<u>.765</u>	<u>2.792</u>
<u>.646</u>	<u>2.855</u>
<u>.522</u>	<u>2.908</u>
<u>.394</u>	<u>2.949</u>
<u>.264</u>	<u>2.978</u>
<u>.133</u>	<u>2.996</u>
<u>.000</u>	<u>3.002</u>

Figure 19. Continued. (u)

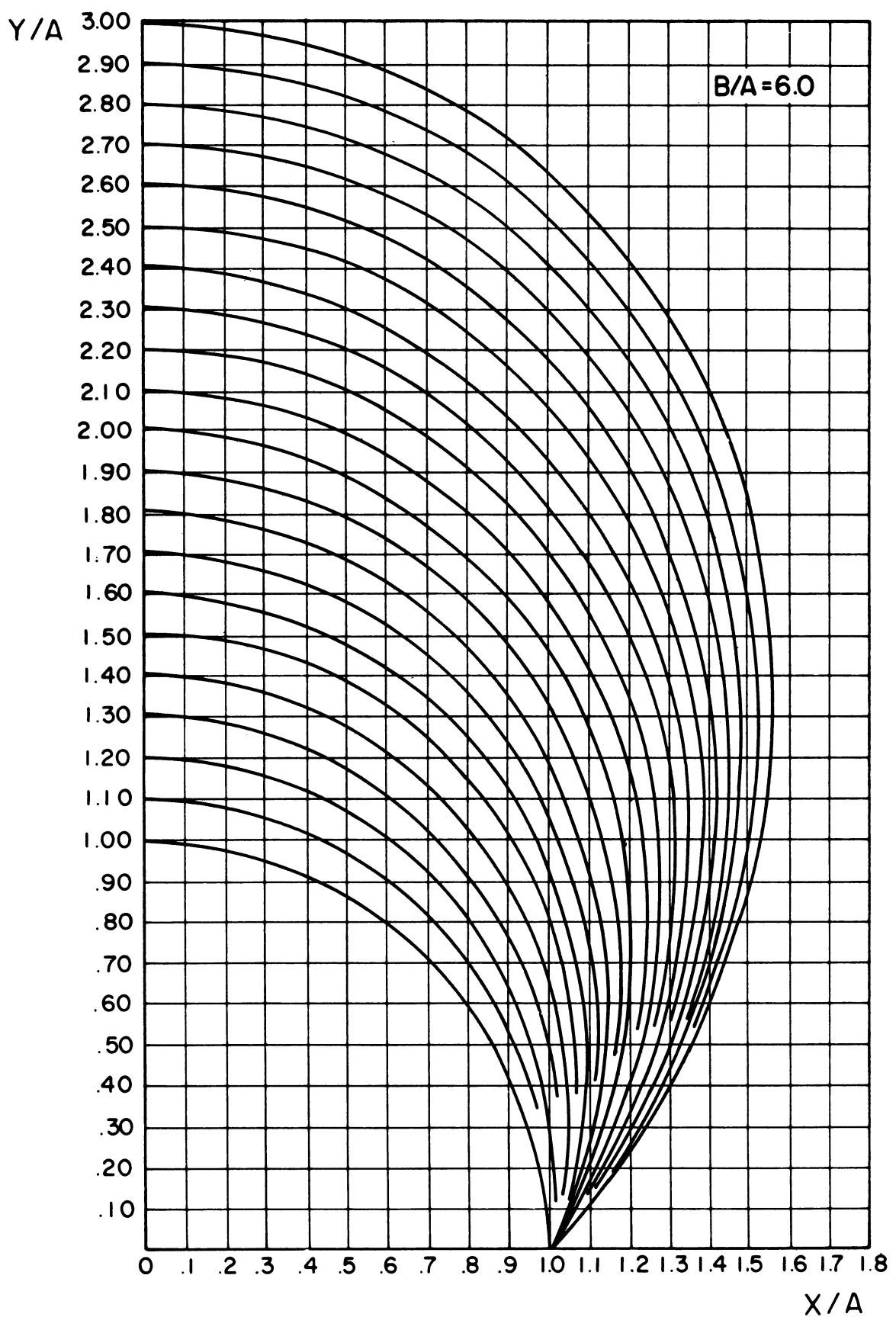


Figure 19. Concluded. (v)

B/A	P	LA	L/A	H/A	W/A
7.000	1.607	2.789	3.127	.999	2.000

X/A	Y/A
1.000	.000
.992	.099
.975	.196
.950	.290
.917	.379
.877	.465
.829	.545
.775	.621
.715	.690
.650	.753
.579	.809
.505	.859
.426	.901
.345	.936
.261	.964
.175	.984
.088	.995
.001	.999

Figure 20. (a)

B/A	P	LA	L/A	H/A	W/A
7.000	1.518	2.809	3.329	1.100	2.002

X/A	Y/A
1.000	.000
1.001	.101
.993	.200
.976	.297
.951	.390
.917	.480
.877	.565
.829	.646
.775	.721
.715	.790
.650	.853
.579	.910
.505	.959
.426	1.002
.345	1.037
.261	1.064
.175	1.084
.088	1.096
.000	1.100

Figure 20. Continued. (b)

B/A	P	LA	L/A	H/A	W/A
7.000	1.438	2.838	3.540	1.200	2.018

X/A	Y/A
1.000	.000
1.009	.102
1.009	.203
1.000	.302
.982	.399
.956	.492
.923	.582
.881	.667
.833	.747
.779	.822
.718	.892
.652	.954
.582	1.011
.507	1.060
.428	1.103
.346	1.137
.262	1.165
.176	1.184
.088	1.196
.000	1.200

Figure 20. Continued. (c)

B/A	P	LA	L/A	H/A	W/A
7.000	1.366	2.875	3.759	1.300	2.048

X/A	Y/A
1.000	.000
1.017	.103
1.024	.205
1.022	.306
1.012	.405
.993	.502
.966	.595
.931	.685
.888	.770
.839	.850
.784	.924
.723	.993
.656	1.056
.585	1.112
.509	1.161
.430	1.203
.348	1.238
.263	1.265
.177	1.285
.089	1.296
.001	1.300

Figure 20. Continued. (d)

B/A 7.000	P 1.302	LA 2.918	L/A 3.983	H/A 1.400	W/A 2.086
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.024	.103
1.038	.206
1.043	.309
1.039	.410
1.027	.509
1.006	.606
.977	.699
.941	.788
.897	.873
.847	.952
.790	1.027
.728	1.095
.660	1.157
.588	1.213
.512	1.262
.432	1.303
.350	1.338
.264	1.365
.178	1.384
.089	1.396
.001	1.400

Figure 20. Continued. (e)

B/A 7.000	P 1.244	LA 2.967	L/A 4.216	H/A 1.500	W/A 2.129
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.031	.108
1.052	.217
1.063	.326
1.065	.434
1.056	.540
1.038	.643
1.012	.743
.977	.838
.934	.930
.883	1.016
.826	1.096
.762	1.170
.692	1.237
.617	1.297
.538	1.350
.454	1.396
.367	1.433
.278	1.462
.186	1.483
.094	1.496
.000	1.500

Figure 20. Continued. (f)

B/A	P	LA	L/A	H/A	W/A
7.000	1.192	3.018	4.450	1.599	2.180

X/A	Y/A
1.000	.000
1.038	.108
1.065	.217
1.082	.327
1.090	.436
1.088	.544
1.076	.649
1.056	.752
1.027	.851
.989	.946
.944	1.036
.892	1.121
.833	1.201
.768	1.274
.697	1.340
.621	1.400
.541	1.452
.457	1.496
.369	1.533
.279	1.562
.188	1.583
.094	1.595
.001	1.599

Figure 20. Continued. (g)

B/A	P	LA	L/A	H/A	W/A
7.000	1.145	3.072	4.692	1.699	2.234

X/A	Y/A
1.000	.000
1.045	.113
1.079	.227
1.103	.342
1.115	.457
1.117	.571
1.109	.683
1.091	.793
1.063	.898
1.027	1.000
.982	1.096
.929	1.187
.869	1.272
.802	1.350
.728	1.421
.650	1.485
.566	1.541
.478	1.589
.387	1.628
.293	1.659
.197	1.682
.099	1.695
.001	1.699

Figure 20. Continued. (h)

B/A 7.000	P 1.102	LA 3.129	L/A 4.936	H/A 1.799	W/A 2.292
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.051	.112
1.091	.226
1.120	.342
1.138	.458
1.146	.573
1.144	.687
1.132	.798
1.110	.906
1.080	1.011
1.041	1.111
.993	1.207
.938	1.296
.876	1.380
.807	1.457
.733	1.526
.653	1.589
.569	1.644
.480	1.691
.388	1.730
.294	1.760
.197	1.782
.099	1.795
.001	1.799

Figure 20. Continued. (i)

B/A 7.000	P 1.063	LA 3.189	L/A 5.190	H/A 1.901	W/A 2.353
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.058	.117
1.105	.236
1.140	.357
1.163	.478
1.175	.600
1.177	.720
1.167	.837
1.148	.952
1.118	1.063
1.079	1.169
1.031	1.270
.975	1.365
.912	1.454
.841	1.536
.764	1.611
.681	1.677
.593	1.736
.501	1.786
.405	1.827
.306	1.859
.206	1.882
.103	1.896
.000	1.901

Figure 20. Continued. (j)

B/A 7.000	P 1.028	LA 3.248	L/A 5.438	H/A 1.999	W/A 2.418
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.063	.116
1.115	.234
1.155	.355
1.184	.477
1.202	.599
1.209	.720
1.205	.839
1.192	.956
1.168	1.069
1.135	1.179
1.093	1.283
1.042	1.383
.984	1.476
.918	1.563
.846	1.643
.768	1.716
.684	1.781
.595	1.838
.502	1.887
.406	1.927
.307	1.959
.206	1.981
.104	1.995
.001	1.999

Figure 20. Continued. (k)

B/A 7.000	P .997	LA 3.311	L/A 5.696	H/A 2.101	W/A 2.482
--------------	-----------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.070	.120
1.128	.243
1.174	.369
1.208	.496
1.231	.624
1.241	.751
1.240	.876
1.228	.999
1.206	1.118
1.174	1.234
1.131	1.344
1.080	1.449
1.021	1.547
.954	1.639
.879	1.724
.798	1.801
.711	1.870
.619	1.930
.523	1.982
.423	2.024
.320	2.058
.214	2.082
.108	2.096
.000	2.101

Figure 20. Continued. (l)

B/A 7.000	P .968	LA 3.373	L/A 5.953	H/A 2.201	W/A 2.550
--------------	-----------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.077	.124
1.142	.252
1.194	.383
1.233	.515
1.259	.649
1.273	.781
1.275	.913
1.265	1.041
1.244	1.167
1.212	1.288
1.170	1.404
1.119	1.514
1.058	1.618
.989	1.715
.912	1.804
.829	1.885
.739	1.958
.643	2.021
.543	2.076
.439	2.121
.332	2.156
.223	2.181
.112	2.196
-.000	2.201

Figure 20. Continued. (m)

B/A 7.000	P .941	LA 3.436	L/A 6.210	H/A 2.301	W/A 2.620
--------------	-----------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.081	.123
1.150	.250
1.207	.380
1.251	.512
1.283	.645
1.302	.779
1.310	.911
1.306	1.041
1.291	1.168
1.265	1.292
1.229	1.411
1.183	1.525
1.128	1.632
1.065	1.734
.994	1.828
.915	1.915
.830	1.994
.739	2.065
.643	2.126
.543	2.179
.439	2.223
.332	2.257
.222	2.281
.112	2.296
-.000	2.301

Figure 20. Continued. (n)

B/A	P	LA	L/A	H/A	W/A
<u>7.000</u>	<u>.917</u>	<u>3.498</u>	<u>6.468</u>	<u>2.400</u>	<u>2.688</u>

X/A	Y/A
1.000	.000
1.088	.126
1.163	.258
1.226	.393
1.275	.530
1.311	.669
1.334	.808
1.344	.945
1.342	1.081
1.328	1.214
1.303	1.343
1.268	1.468
1.222	1.587
1.166	1.699
1.101	1.806
1.028	1.905
.947	1.996
.860	2.078
.766	2.152
.667	2.217
.563	2.272
.455	2.318
.344	2.354
.231	2.379
.116	2.395
.000	2.400

Figure 20. Continued. (o)

B/A	P	LA	L/A	H/A	W/A
<u>7.000</u>	<u>.895</u>	<u>3.561</u>	<u>6.725</u>	<u>2.498</u>	<u>2.757</u>

X/A	Y/A
1.000	.000
1.095	.130
1.177	.266
1.244	.406
1.298	.548
1.338	.692
1.365	.836
1.378	.980
1.378	1.121
1.366	1.260
1.342	1.394
1.306	1.524
1.260	1.648
1.203	1.766
1.137	1.877
1.062	1.980
.980	2.076
.889	2.162
.793	2.239
.690	2.307
.583	2.365
.471	2.413
.357	2.450
.239	2.477
.120	2.493
.000	2.498

Figure 20. Continued. (p)

B/A 7.000	P .875	LA 3.625	L/A 6.989	H/A 2.599	W/A 2.830
--------------	-----------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.102	.134
1.190	.274
1.263	.419
1.322	.566
1.367	.716
1.397	.866
1.413	1.015
1.415	1.162
1.404	1.307
1.381	1.447
1.345	1.582
1.299	1.712
1.241	1.835
1.174	1.950
1.097	2.058
1.012	2.157
.919	2.248
.819	2.328
.714	2.399
.603	2.459
.487	2.509
.369	2.548
.247	2.576
.124	2.593
.000	2.599

Figure 20. Continued. (q)

B/A 7.000	P .856	LA 3.689	L/A 7.254	H/A 2.699	W/A 2.903
--------------	-----------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.105	.133
1.197	.271
1.274	.415
1.337	.561
1.387	.710
1.422	.860
1.444	1.009
1.452	1.157
1.447	1.302
1.430	1.444
1.401	1.581
1.361	1.714
1.310	1.840
1.248	1.960
1.178	2.072
1.099	2.177
1.012	2.273
.918	2.360
.817	2.438
.711	2.506
.600	2.565
.485	2.613
.366	2.650
.246	2.677
.123	2.694
-.000	2.699

Figure 20. Continued. (r)

B/A	P	L/A	L/A	H/A	W/A
7.000	.839	3.754	7.519	2.799	2.976

X/A	Y/A
1.000	.000
1.112	.136
1.210	.279
1.293	.427
1.361	.579
1.414	.733
1.453	.888
1.478	1.043
1.488	1.196
1.485	1.347
1.469	1.494
1.440	1.637
1.400	1.775
1.348	1.906
1.286	2.030
1.214	2.147
1.133	2.256
1.043	2.356
.947	2.447
.843	2.528
.734	2.599
.619	2.659
.500	2.709
.378	2.749
.254	2.777
.127	2.794
-.000	2.799

Figure 20. Continued. (s)

B/A	P	L/A	L/A	H/A	W/A
7.000	.823	3.818	7.785	2.899	3.049

X/A	Y/A
1.000	.000
1.119	.140
1.223	.287
1.311	.440
1.385	.597
1.442	.756
1.484	.917
1.512	1.077
1.524	1.236
1.523	1.392
1.508	1.545
1.479	1.693
1.439	1.836
1.386	1.972
1.323	2.101
1.250	2.222
1.167	2.335
1.075	2.439
.975	2.533
.869	2.618
.756	2.691
.638	2.754
.516	2.806
.390	2.847
.262	2.876
.131	2.894
.000	2.899

Figure 20. Continued. (t)

B/A	P	L/A	L/A	H/A	W/A
<u>7.000</u>	<u>.808</u>	<u>3.885</u>	<u>8.059</u>	<u>3.002</u>	<u>3.123</u>

X/A	Y/A
<u>1.000</u>	<u>.000</u>
<u>1.126</u>	<u>.144</u>
<u>1.236</u>	<u>.296</u>
<u>1.331</u>	<u>.454</u>
<u>1.409</u>	<u>.615</u>
<u>1.471</u>	<u>.780</u>
<u>1.516</u>	<u>.946</u>
<u>1.547</u>	<u>1.112</u>
<u>1.561</u>	<u>1.277</u>
<u>1.561</u>	<u>1.439</u>
<u>1.547</u>	<u>1.597</u>
<u>1.519</u>	<u>1.751</u>
<u>1.479</u>	<u>1.899</u>
<u>1.426</u>	<u>2.040</u>
<u>1.361</u>	<u>2.174</u>
<u>1.286</u>	<u>2.300</u>
<u>1.201</u>	<u>2.417</u>
<u>1.107</u>	<u>2.525</u>
<u>1.005</u>	<u>2.622</u>
<u>.895</u>	<u>2.710</u>
<u>.779</u>	<u>2.786</u>
<u>.658</u>	<u>2.852</u>
<u>.532</u>	<u>2.906</u>
<u>.402</u>	<u>2.948</u>
<u>.269</u>	<u>2.978</u>
<u>.135</u>	<u>2.996</u>
<u>-.000</u>	<u>3.002</u>

Figure 20. Continued. (u)

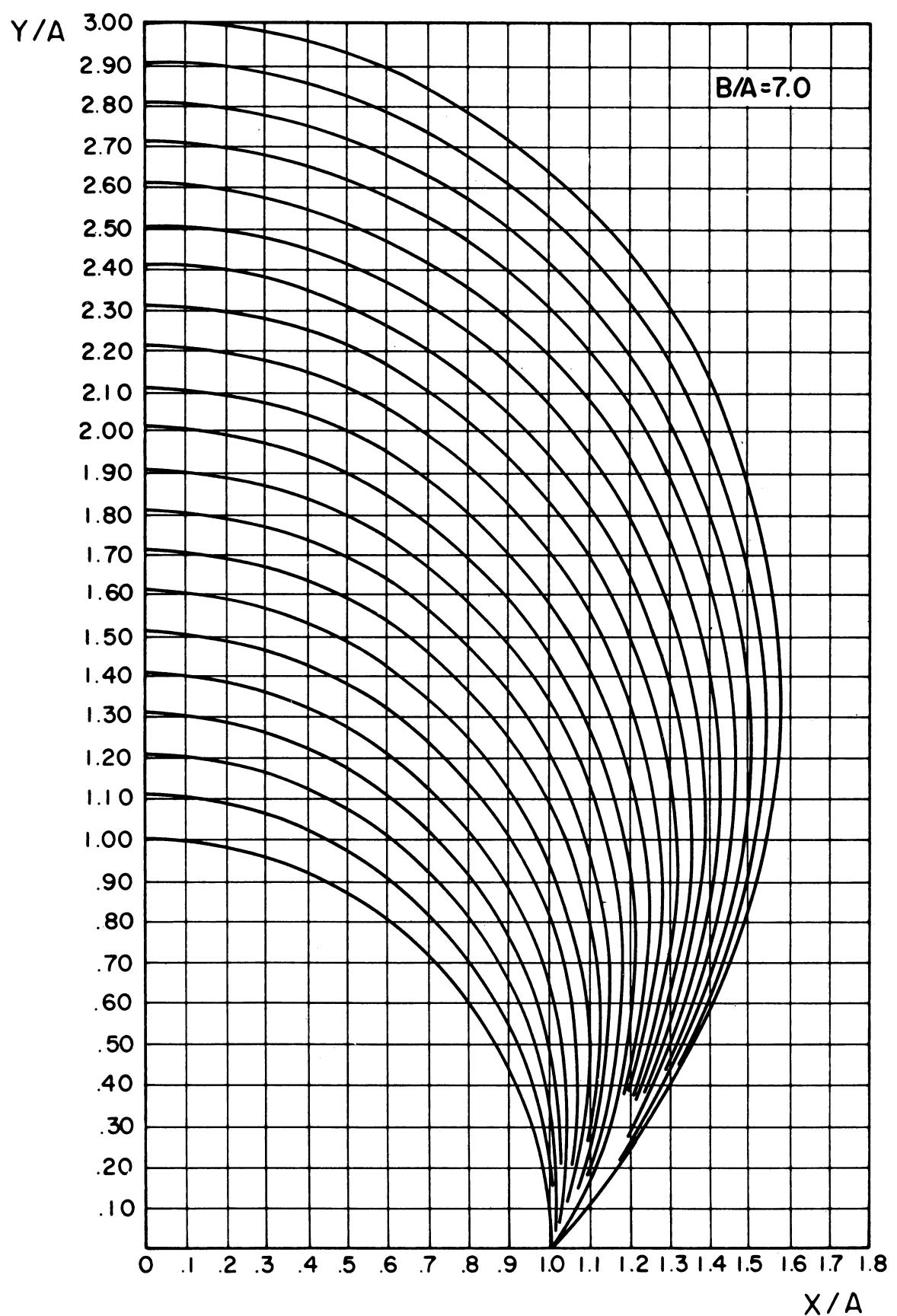


Figure 20. Concluded. (v)

B/A	P	LA	L/A	H/A	W/A
8.000	1.602	2.963	3.130	1.000	2.000

X/A	Y/A
1.000	.000
.992	.098
.976	.195
.952	.268
.919	.377
.879	.463
.832	.544
.778	.619
.718	.688
.653	.752
.582	.809
.507	.859
.429	.901
.347	.937
.263	.964
.176	.984
.089	.996
.001	1.000

Figure 21. (a)

B/A	P	LA	L/A	H/A	W/A
8.000	1.513	2.982	3.332	1.100	2.002

X/A	Y/A
1.000	.000
1.001	.100
.994	.198
.977	.294
.952	.388
.920	.477
.880	.563
.832	.643
.778	.719
.718	.788
.653	.852
.582	.909
.507	.959
.429	1.001
.347	1.037
.262	1.064
.176	1.084
.088	1.096
.000	1.100

Figure 21. Continued. (b)

B/A	P	L/A	L/A	H/A	W/A
8.000	1.433	3.012	3.542	1.200	2.020

X/A	Y/A
1.000	.000
1.009	.101
1.010	.201
1.001	.299
.984	.396
.959	.489
.925	.576
.884	.664
.837	.744
.782	.819
.722	.889
.656	.952
.585	1.009
.509	1.059
.430	1.101
.348	1.137
.263	1.164
.177	1.184
.089	1.196
.000	1.200

Figure 21. Continued. (c)

B/A	P	L/A	L/A	H/A	W/A
8.000	1.360	3.049	3.760	1.299	2.050

X/A	Y/A
1.000	.000
1.017	.101
1.025	.203
1.024	.303
1.014	.402
.995	.498
.969	.591
.934	.680
.892	.765
.843	.846
.783	.921
.727	.990
.660	1.053
.589	1.109
.513	1.159
.433	1.201
.350	1.236
.265	1.264
.178	1.284
.090	1.296
.001	1.299

Figure 21. Continued. (d)

B/A 8.000	P 1.295	LA 3.094	L/A 3.987	H/A 1.400	W/A 2.089
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.024	.102
1.039	.204
1.045	.306
1.041	.406
1.030	.505
1.009	.601
.981	.694
.945	.784
.902	.869
.851	.949
.795	1.023
.733	1.092
.665	1.155
.593	1.211
.516	1.260
.436	1.303
.352	1.337
.267	1.365
.179	1.384
.090	1.396
.001	1.400

Figure 21. Continued. (e)

B/A 8.000	P 1.236	LA 3.145	L/A 4.222	H/A 1.501	W/A 2.134
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.032	.107
1.053	.214
1.065	.322
1.067	.429
1.059	.535
1.042	.638
1.016	.738
.981	.834
.939	.925
.888	1.012
.831	1.092
.767	1.167
.697	1.235
.622	1.296
.542	1.349
.458	1.395
.370	1.433
.280	1.463
.188	1.484
.094	1.497
.000	1.501

Figure 21. Continued. (f)

B/A 8.000	P 1.184	LA 3.197	L/A 4.458	H/A 1.600	W/A 2.184
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.038	.106
1.066	.214
1.084	.323
1.092	.431
1.091	.538
1.080	.643
1.060	.746
1.031	.846
.994	.941
.950	1.032
.898	1.117
.839	1.197
.773	1.271
.702	1.338
.626	1.398
.545	1.451
.460	1.496
.372	1.533
.282	1.562
.189	1.583
.095	1.596
.000	1.600

Figure 21. Continued. (g)

B/A 8.000	P 1.136	LA 3.254	L/A 4.700	H/A 1.700	W/A 2.240
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.045	.111
1.080	.224
1.104	.338
1.117	.452
1.120	.565
1.113	.677
1.095	.786
1.068	.892
1.032	.994
.988	1.090
.935	1.182
.875	1.268
.808	1.346
.734	1.418
.655	1.483
.571	1.540
.483	1.588
.390	1.628
.295	1.659
.198	1.682
.100	1.696
.000	1.700

Figure 21. Continued. (h)

B/A 8.000	P 1.093	LA 3.313	L/A 4.946	H/A 1.800	W/A 2.298
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.051	.110
1.091	.223
1.121	.337
1.140	.452
1.149	.566
1.148	.679
1.137	.791
1.116	.899
1.086	1.004
1.047	1.105
1.000	1.201
.945	1.291
.883	1.375
.814	1.453
.739	1.523
.659	1.587
.574	1.642
.484	1.690
.392	1.729
.296	1.760
.199	1.782
.100	1.795
.000	1.800

Figure 21. Continued. (i)

B/A 8.000	P 1.054	LA 3.373	L/A 5.195	H/A 1.900	W/A 2.361
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.058	.114
1.105	.231
1.141	.351
1.165	.471
1.178	.591
1.180	.711
1.172	.828
1.153	.943
1.124	1.054
1.086	1.160
1.038	1.262
.982	1.358
.919	1.447
.848	1.530
.771	1.605
.688	1.673
.599	1.732
.506	1.782
.410	1.824
.310	1.857
.208	1.881
.105	1.895
.000	1.900

Figure 21. Continued. (j)

B/A	P	LA	L/A	H/A	W/A
<u>8.000</u>	<u>1.018</u>	<u>3.436</u>	<u>5.448</u>	<u>2.000</u>	<u>2.426</u>

X/A	Y/A
1.000	.000
<u>1.063</u>	<u>.113</u>
1.115	.230
<u>1.156</u>	<u>.349</u>
1.186	.469
<u>1.205</u>	<u>.590</u>
1.213	.711
<u>1.210</u>	<u>.830</u>
1.197	.946
<u>1.174</u>	<u>1.060</u>
1.142	1.170
<u>1.100</u>	<u>1.275</u>
1.050	1.375
<u>.992</u>	<u>1.470</u>
.926	1.557
<u>.853</u>	<u>1.638</u>
.775	1.712
<u>.690</u>	<u>1.778</u>
.601	1.836
<u>.507</u>	<u>1.885</u>
.410	1.926
<u>.310</u>	<u>1.958</u>
.208	1.981
<u>.105</u>	<u>1.995</u>
.000	2.000

Figure 21. Continued. (k)

B/A	P	LA	L/A	H/A	W/A
<u>8.000</u>	<u>.986</u>	<u>3.498</u>	<u>5.701</u>	<u>2.099</u>	<u>2.490</u>

X/A	Y/A
1.000	.000
<u>1.070</u>	<u>.117</u>
1.129	.238
<u>1.175</u>	<u>.362</u>
1.210	.487
<u>1.233</u>	<u>.614</u>
1.245	.740
<u>1.245</u>	<u>.865</u>
1.234	.987
<u>1.213</u>	<u>1.107</u>
1.181	1.223
<u>1.139</u>	<u>1.333</u>
1.089	1.439
<u>1.029</u>	<u>1.538</u>
.962	1.631
<u>.887</u>	<u>1.717</u>
.806	1.795
<u>.719</u>	<u>1.864</u>
.626	1.926
<u>.529</u>	<u>1.978</u>
.428	2.021
<u>.324</u>	<u>2.055</u>
.217	2.079
<u>.109</u>	<u>2.094</u>
.001	2.099

Figure 21. Continued. (l)

B/A	P	LA	L/A	H/A	W/A
8.000	.956	3.563	5.959	2.199	2.561

X/A	Y/A
1.000	.000
1.074	.116
1.137	.236
1.189	.359
1.229	.485
1.258	.611
1.275	.738
1.281	.864
1.275	.988
1.260	1.110
1.234	1.228
1.198	1.342
1.153	1.451
1.100	1.555
1.038	1.652
.968	1.743
.892	1.827
.809	1.903
.721	1.971
.627	2.030
.529	2.081
.428	2.123
.324	2.156
.217	2.180
.109	2.194
.001	2.199

Figure 21. Continued. (m)

B/A	P	LA	L/A	H/A	W/A
8.000	.929	3.629	6.224	2.301	2.631

X/A	Y/A
1.000	.000
1.081	.120
1.151	.244
1.208	.372
1.253	.502
1.286	.634
1.307	.767
1.315	.898
1.313	1.028
1.298	1.156
1.273	1.280
1.238	1.399
1.193	1.514
1.138	1.623
1.075	1.725
1.004	1.821
.925	1.909
.839	1.989
.748	2.060
.651	2.123
.550	2.177
.444	2.221
.336	2.256
.225	2.281
.113	2.296
.000	2.301

Figure 21. Continued. (n)

B/A 8.000	P .904	LA 3.695	L/A 6.488	H/A 2.402	W/A 2.701
--------------	-----------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.088	.123
1.164	.252
1.227	.384
1.277	.520
1.314	.657
1.339	.795
1.350	.933
1.350	1.068
1.337	1.201
1.313	1.331
1.278	1.456
1.232	1.576
1.177	1.690
1.112	1.798
1.039	1.898
.958	1.990
.870	2.074
.775	2.150
.675	2.215
.570	2.272
.461	2.318
.349	2.355
.234	2.381
.117	2.397
-.000	2.402

Figure 21. Continued. (o)

B/A 8.000	P .881	LA 3.760	L/A 6.747	H/A 2.500	W/A 2.773
--------------	-----------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.095	.127
1.177	.259
1.246	.397
1.301	.537
1.342	.680
1.370	.823
1.385	.966
1.386	1.107
1.375	1.246
1.352	1.381
1.318	1.512
1.272	1.637
1.216	1.756
1.150	1.869
1.075	1.973
.992	2.070
.901	2.158
.803	2.236
.709	2.305
.591	2.364
.478	2.413
.362	2.451
.243	2.478
.122	2.495
.000	2.500

Figure 21. Continued. (p)

B/A <u>8.000</u>	P .860	LA <u>3.828</u>	L/A <u>7.019</u>	H/A <u>2.603</u>	W/A <u>2.848</u>
---------------------	-----------	--------------------	---------------------	---------------------	---------------------

X/A	Y/A
1.000	.000
1.099	.125
1.184	.257
1.257	.393
1.317	.533
1.363	.675
1.397	.818
1.417	.961
1.424	1.103
1.419	1.243
1.402	1.380
1.374	1.513
1.334	1.641
1.285	1.764
1.225	1.881
1.156	1.990
1.078	2.092
.993	2.186
.901	2.271
.802	2.347
.698	2.414
.589	2.471
.476	2.518
.360	2.555
.241	2.582
.121	2.598
-.000	2.603

Figure 21. Continued. (q)

B/A <u>8.000</u>	P .841	LA <u>3.893</u>	L/A <u>7.278</u>	H/A <u>2.701</u>	W/A <u>2.920</u>
---------------------	-----------	--------------------	---------------------	---------------------	---------------------

X/A	Y/A
1.000	.000
1.105	.129
1.197	.264
1.275	.404
1.340	.549
1.391	.696
1.427	.844
1.450	.993
1.460	1.140
1.457	1.285
1.441	1.428
1.413	1.566
1.374	1.700
1.323	1.827
1.263	1.948
1.192	2.062
1.113	2.168
1.025	2.266
.930	2.355
.829	2.434
.722	2.504
.609	2.563
.492	2.613
.372	2.651
.250	2.679
.125	2.695
.000	2.701

Figure 21. Continued. (r)

B/A 8.000	P .824	LA 3.957	L/A 7.537	H/A 2.798	W/A 2.992
--------------	-----------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.112	.132
1.210	.271
1.294	.416
1.363	.565
1.418	.717
1.458	.870
1.484	1.024
1.496	1.177
1.495	1.328
1.480	1.476
1.452	1.619
1.413	1.758
1.362	1.890
1.300	2.016
1.228	2.134
1.147	2.245
1.057	2.346
.960	2.439
.855	2.521
.745	2.594
.629	2.655
.509	2.706
.385	2.746
.258	2.775
.130	2.792
.001	2.798

Figure 21. Continued. (s)

B/A 8.000	P .807	LA 4.023	L/A 7.803	H/A 2.898	W/A 3.065
--------------	-----------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.119	.136
1.223	.279
1.312	.428
1.386	.582
1.445	.739
1.489	.898
1.518	1.057
1.532	1.215
1.532	1.372
1.519	1.525
1.492	1.674
1.452	1.817
1.400	1.955
1.338	2.086
1.264	2.209
1.181	2.323
1.089	2.428
.989	2.524
.881	2.610
.767	2.685
.648	2.749
.524	2.802
.396	2.844
.266	2.874
.134	2.892
.001	2.898

Figure 21. Continued. (t)

B/A 8.000	P .793	L/A 4.090	L/A 8.070	H/A 2.997	W/A 3.140
--------------	-----------	--------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.125	.139
1.236	.286
1.330	.440
1.409	.599
1.473	.761
1.520	.925
1.552	1.090
1.568	1.254
1.570	1.416
1.557	1.574
1.531	1.728
1.491	1.877
1.439	2.020
1.375	2.155
1.300	2.283
1.215	2.401
1.120	2.511
1.017	2.610
.907	2.699
.790	2.777
.667	2.843
.539	2.898
.408	2.941
.274	2.972
.137	2.991
.000	2.997

Figure 21. Continued. (u)

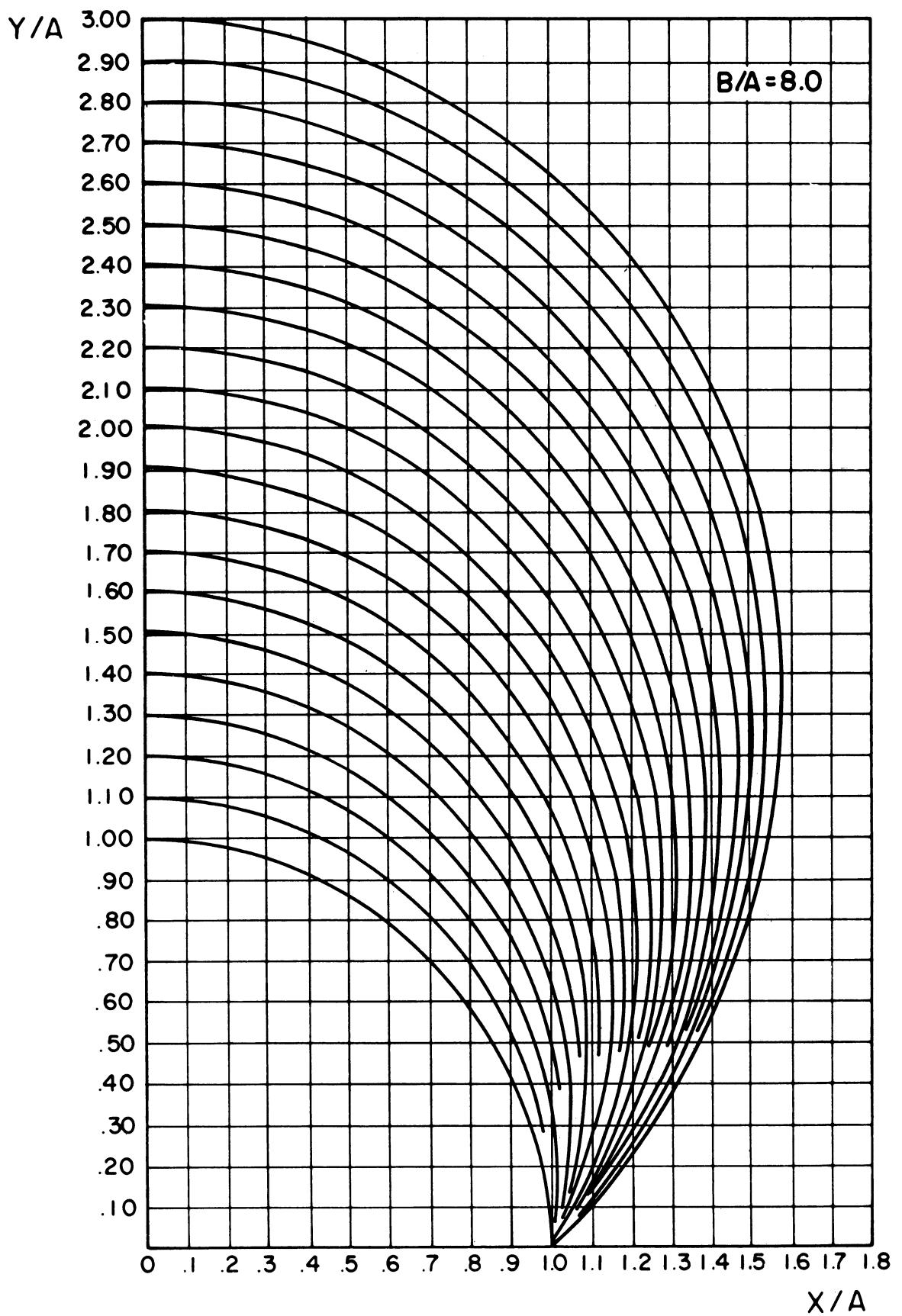


Figure 21. Concluded. (v)

B/A 9.000	P 1.599	LA 3.127	L/A 3.130	H/A 1.000	W/A 2.000
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
.993	.098
.977	.193
.953	.286
.920	.376
.881	.461
.834	.542
.780	.617
.720	.687
.655	.750
.584	.807
.509	.858
.431	.901
.348	.936
.264	.964
.177	.984
.089	.996
.001	1.000

Figure 22. (a)

B/A 9.000	P 1.509	LA 3.146	L/A 3.334	H/A 1.101	W/A 2.003
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.002	.099
.994	.197
.978	.293
.954	.386
.922	.475
.882	.561
.835	.641
.781	.717
.721	.787
.656	.851
.585	.908
.510	.958
.431	1.001
.349	1.037
.264	1.064
.177	1.084
.089	1.097
.000	1.101

Figure 22. Continued. (b)

<u>B/A</u>	<u>P</u>	<u>L/A</u>	<u>L/A</u>	<u>H/A</u>	<u>W/A</u>
<u>9.000</u>	<u>1.428</u>	<u>3.175</u>	<u>3.544</u>	<u>1.200</u>	<u>2.021</u>

X/A	Y/A
1.000	.000
1.010	.100
1.011	.199
1.002	.297
.996	.393
.961	.486
.928	.576
.887	.661
.839	.742
.785	.817
.725	.887
.659	.951
.583	1.008
.512	1.058
.433	1.101
.350	1.136
.265	1.164
.178	1.184
.090	1.196
.000	1.200

Figure 22. Continued. (c)

<u>B/A</u>	<u>P</u>	<u>L/A</u>	<u>L/A</u>	<u>H/A</u>	<u>W/A</u>
<u>9.000</u>	<u>1.355</u>	<u>3.215</u>	<u>3.764</u>	<u>1.300</u>	<u>2.051</u>

X/A	Y/A
1.000	.000
1.017	.100
1.025	.201
1.025	.301
1.015	.399
.997	.495
.971	.588
.937	.678
.895	.763
.846	.843
.791	.919
.730	.988
.663	1.052
.591	1.109
.515	1.159
.435	1.201
.352	1.237
.266	1.264
.179	1.284
.090	1.296
.000	1.300

Figure 22. Continued. (d)

B/A	P	LA	L/A	H/A	W/A
9.000	1.289	3.262	3.994	1.401	2.092

X/A	Y/A
1.000	.000
1.024	.101
1.040	.202
1.046	.303
1.043	.404
1.032	.502
1.012	.598
.984	.691
.948	.781
.905	.866
.855	.947
.799	1.022
.736	1.091
.668	1.154
.596	1.211
.519	1.260
.438	1.303
.354	1.338
.268	1.366
.180	1.385
.090	1.397
-.000	1.401

Figure 22. Continued. (e)

B/A	P	LA	L/A	H/A	W/A
9.000	1.230	3.313	4.226	1.501	2.137

X/A	Y/A
1.000	.000
1.032	.106
1.054	.212
1.066	.319
1.069	.426
1.061	.531
1.045	.634
1.019	.734
.985	.830
.942	.921
.892	1.008
.835	1.089
.771	1.164
.701	1.233
.626	1.294
.545	1.348
.461	1.394
.373	1.432
.282	1.462
.189	1.484
.095	1.497
.000	1.501

Figure 22. Continued. (f)

B/A 9.000	P 1.177	LA 3.367	L/A 4.463	H/A 1.601	W/A 2.188
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.038	.105
1.057	.212
1.085	.319
1.094	.427
1.093	.534
1.083	.639
1.063	.742
1.035	.841
.999	.937
.954	1.028
.902	1.114
.843	1.194
.778	1.268
.706	1.336
.630	1.396
.549	1.450
.464	1.495
.375	1.533
.284	1.562
.190	1.583
.096	1.596
.000	1.601

Figure 22. Continued. (g)

B/A 9.000	P 1.129	LA 3.426	L/A 4.707	H/A 1.701	W/A 2.245
--------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.044	.105
1.078	.211
1.103	.319
1.117	.428
1.123	.536
1.118	.643
1.105	.748
1.083	.850
1.052	.949
1.013	1.044
.966	1.135
.912	1.220
.852	1.299
.785	1.373
.712	1.440
.634	1.499
.552	1.552
.466	1.597
.377	1.634
.285	1.663
.191	1.684
.096	1.696
-.000	1.701

Figure 22. Continued. (h)

B/A	P	LA	L/A	H/A	W/A
9.000	1.086	3.486	4.953	1.800	2.303

X/A	Y/A
1.000	.000
1.051	.109
1.092	.220
1.122	.333
1.142	.447
1.152	.561
1.151	.674
1.140	.785
1.120	.893
1.090	.998
1.052	1.099
1.005	1.196
.950	1.287
.888	1.371
.819	1.450
.744	1.521
.663	1.585
.578	1.641
.488	1.689
.395	1.729
.299	1.760
.200	1.782
.101	1.796
.000	1.800

Figure 22. Continued. (i)

B/A	P	LA	L/A	H/A	W/A
9.000	1.046	3.549	5.203	1.900	2.368

X/A	Y/A
1.000	.000
1.056	.108
1.102	.218
1.138	.331
1.164	.446
1.179	.560
1.184	.675
1.179	.788
1.165	.898
1.141	1.006
1.108	1.110
1.067	1.210
1.017	1.306
.960	1.395
.896	1.479
.826	1.556
.749	1.626
.667	1.689
.581	1.744
.490	1.791
.396	1.830
.300	1.861
.201	1.883
.101	1.896
.000	1.900

Figure 22. Continued. (j)

B/A	P	LA	L/A	H/A	W/A
9.000	1.010	3.613	5.458	2.000	2.432

X/A	Y/A
1.000	.000
1.063	.111
1.116	.226
1.157	.344
1.188	.464
1.208	.584
1.216	.704
1.214	.822
1.202	.939
1.180	1.053
1.148	1.163
1.107	1.269
1.057	1.369
.999	1.464
.933	1.553
.860	1.635
.781	1.709
.696	1.776
.606	1.835
.512	1.885
.414	1.926
.313	1.958
.210	1.982
.106	1.996
.000	2.000

Figure 22. Continued. (k)

B/A	P	LA	L/A	H/A	W/A
9.000	.977	3.680	5.717	2.101	2.499

X/A	Y/A
1.000	.000
1.070	.115
1.129	.234
1.177	.357
1.212	.481
1.236	.607
1.249	.733
1.250	.857
1.240	.980
1.219	1.100
1.188	1.216
1.146	1.328
1.096	1.434
1.037	1.534
.969	1.628
.895	1.714
.813	1.793
.725	1.864
.631	1.926
.533	1.979
.431	2.023
.326	2.057
.219	2.082
.110	2.096
- 000	2.101

Figure 22. Continued. (l)

B/A 9.000	P .947	LA 3.746	L/A 5.976	H/A 2.201	W/A 2.570
--------------	-----------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.075	.114
1.138	.232
1.190	.354
1.231	.478
1.260	.604
1.278	.730
1.285	.856
1.281	.980
1.266	1.102
1.241	1.220
1.206	1.335
1.161	1.445
1.108	1.549
1.046	1.647
.976	1.739
.899	1.824
.816	1.901
.727	1.970
.633	2.030
.534	2.082
.432	2.125
.326	2.158
.219	2.182
.110	2.197
-.000	2.201

Figure 22. Continued. (m)

B/A 9.000	P .919	LA 3.813	L/A 6.234	H/A 2.300	W/A 2.639
--------------	-----------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.081	.117
1.151	.239
1.209	.366
1.255	.495
1.288	.626
1.310	.757
1.320	.888
1.318	1.018
1.304	1.145
1.280	1.270
1.245	1.390
1.201	1.505
1.146	1.615
1.083	1.718
1.012	1.814
.933	1.903
.847	1.984
.755	2.057
.657	2.120
.555	2.175
.449	2.220
.339	2.255
.228	2.280
.114	2.295
-.000	2.300

Figure 22. Continued. (n)

B/A	P	LA	L/A	H/A	W/A
<u>9.000</u>	<u>.894</u>	<u>3.879</u>	<u>6.493</u>	<u>2.399</u>	<u>2.709</u>

X/A	Y/A
1.000	.000
1.088	.120
1.164	.247
1.228	.377
1.278	.511
1.316	.647
1.341	.784
1.354	.921
1.354	1.056
1.343	1.189
1.320	1.319
1.285	1.444
1.246	1.565
1.185	1.680
1.121	1.788
1.048	1.889
.966	1.982
.878	2.067
.783	2.143
.682	2.210
.576	2.267
.466	2.314
.352	2.351
.236	2.378
.119	2.394
.000	2.399

Figure 22. Continued. (o)

B/A	P	LA	L/A	H/A	W/A
<u>9.000</u>	<u>.871</u>	<u>3.945</u>	<u>6.752</u>	<u>2.497</u>	<u>2.784</u>

X/A	Y/A
1.000	.000
1.092	.119
1.171	.244
1.239	.373
1.294	.506
1.337	.641
1.368	.778
1.386	.915
1.392	1.051
1.386	1.185
1.369	1.316
1.341	1.444
1.302	1.567
1.253	1.686
1.195	1.798
1.128	1.904
1.052	2.002
.969	2.093
.879	2.175
.783	2.249
.682	2.314
.575	2.369
.465	2.415
.352	2.451
.236	2.476
.119	2.492
.001	2.497

Figure 22. Continued. (p)

B/A <u>9.000</u>	P <u>.850</u>	LA <u>4.016</u>	L/A <u>7.023</u>	H/A <u>2.599</u>	W/A <u>2.858</u>
---------------------	------------------	--------------------	---------------------	---------------------	---------------------

X/A	Y/A
1.000	.000
1.098	.122
1.184	.251
1.257	.385
1.318	.522
1.365	.663
1.399	.805
1.420	.947
1.429	1.089
1.425	1.228
1.409	1.365
1.381	1.499
1.342	1.628
1.293	1.751
1.234	1.868
1.165	1.979
1.087	2.082
1.002	2.176
.909	2.263
.810	2.340
.705	2.408
.595	2.466
.481	2.513
.364	2.551
.244	2.578
.122	2.594
-.000	2.599

Figure 22. Continued. (q)

B/A <u>9.000</u>	P <u>.830</u>	LA <u>4.082</u>	L/A <u>7.284</u>	H/A <u>2.697</u>	W/A <u>2.930</u>
---------------------	------------------	--------------------	---------------------	---------------------	---------------------

X/A	Y/A
1.000	.000
1.105	.125
1.197	.258
1.276	.396
1.341	.538
1.392	.683
1.430	.830
1.454	.978
1.465	1.125
1.463	1.270
1.448	1.412
1.421	1.551
1.382	1.685
1.333	1.813
1.272	1.935
1.202	2.050
1.123	2.158
1.035	2.256
.939	2.346
.837	2.427
.729	2.497
.616	2.558
.498	2.607
.377	2.646
.253	2.674
.127	2.691
.001	2.697

Figure 22. Continued. (r)

B/A	P	LA	L/A	H/A	W/A
9.000	.812	4.152	7.558	2.799	3.005

X/A	Y/A
1.000	.000
1.112	.129
1.210	.265
1.294	.407
1.364	.554
1.420	.705
1.462	.857
1.489	1.010
1.503	1.163
1.502	1.313
1.489	1.462
1.462	1.606
1.423	1.745
1.373	1.879
1.311	2.006
1.240	2.126
1.158	2.237
1.068	2.340
.970	2.434
.865	2.518
.753	2.591
.636	2.654
.514	2.706
.389	2.746
.261	2.776
.131	2.793
.000	2.799

Figure 22. Continued. (s)

B/A	P	LA	L/A	H/A	W/A
9.000	.795	4.223	7.833	2.902	3.084

X/A	Y/A
1.000	.000
1.119	.132
1.223	.272
1.313	.419
1.388	.571
1.449	.726
1.494	.884
1.525	1.043
1.540	1.201
1.542	1.357
1.529	1.511
1.503	1.661
1.465	1.806
1.414	1.945
1.351	2.077
1.278	2.201
1.194	2.317
1.102	2.424
1.001	2.521
.892	2.609
.777	2.685
.657	2.751
.531	2.805
.402	2.847
.270	2.877
.135	2.895
.000	2.902

Figure 22. Continued. (t)

B/A 9.000	P .779	L/A 4.293	L/A 8.110	H/A 3.004	W/A 3.164
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X/A	Y/A
1.000	.000
1.121	.130
1.229	.269
1.322	.414
1.402	.564
1.467	.718
1.517	.875
1.553	1.033
1.575	1.191
1.582	1.348
1.576	1.502
1.557	1.653
1.525	1.800
1.481	1.942
1.425	2.077
1.359	2.206
1.282	2.327
1.196	2.440
1.102	2.543
1.000	2.637
.890	2.722
.775	2.796
.654	2.859
.529	2.911
.400	2.951
.268	2.981
.135	2.998
.001	3.004

Figure 22. Continued. (u)

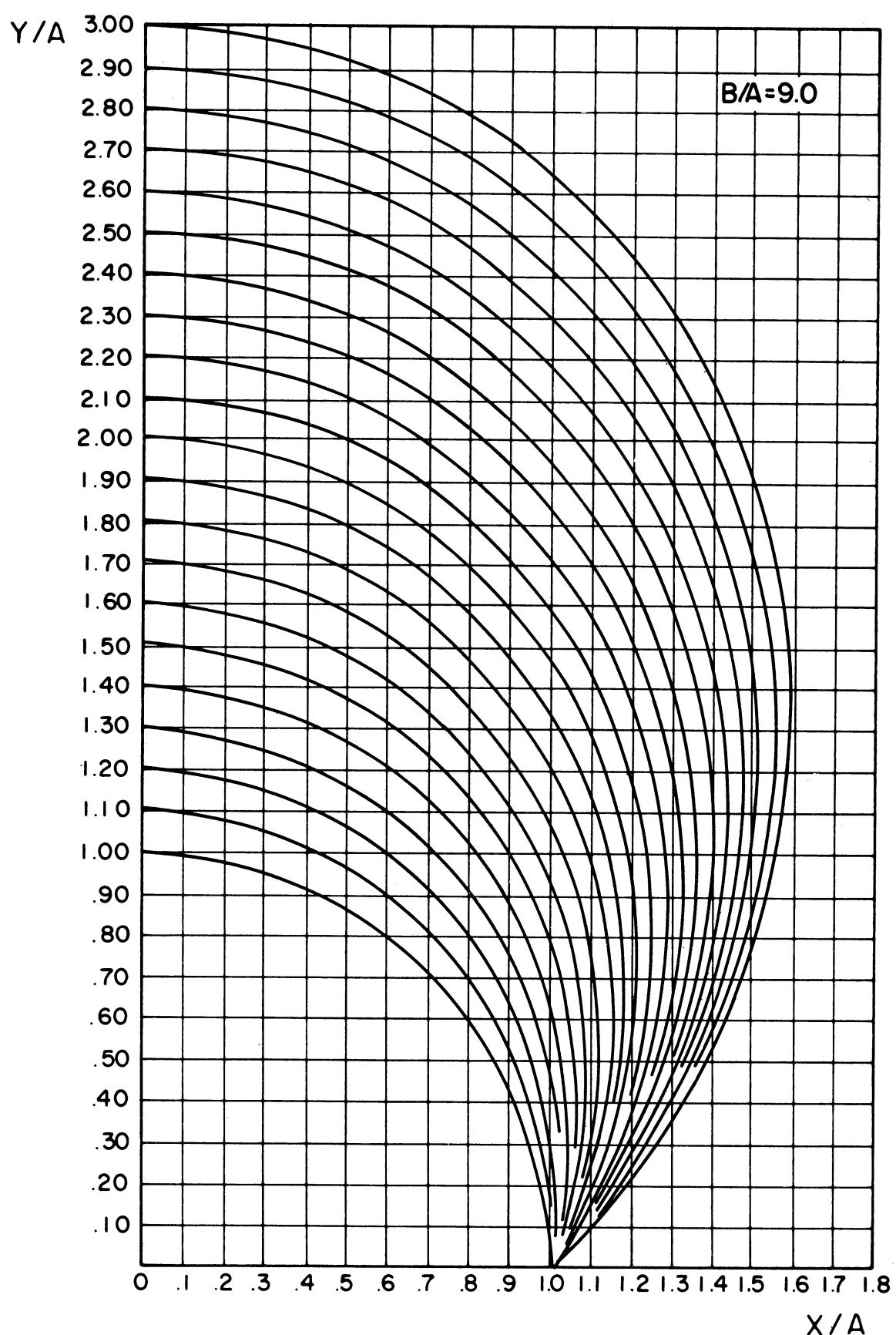


Figure 22. Concluded. (v)

B/A	P	LA	L/A	H/A	W/A
10.000	1.547	3.282	3.130	1.000	2.000

X/A	Y/A
1.000	.000
.993	.097
.978	.192
.954	.285
.922	.374
.882	.459
.835	.540
.782	.616
.722	.685
.657	.749
.586	.806
.511	.857
.432	.900
.350	.935
.265	.963
.178	.984
.090	.996
.001	1.000

Figure 23. (a)

B/A	P	LA	L/A	H/A	W/A
10.000	1.506	3.302	3.335	1.100	2.004

X/A	Y/A
1.000	.000
1.002	.099
.995	.196
.979	.291
.955	.384
.923	.473
.883	.559
.837	.640
.783	.715
.723	.785
.657	.849
.587	.906
.511	.957
.432	1.000
.350	1.036
.265	1.064
.178	1.084
.089	1.096
.000	1.100

Figure 23. Continued. (b)

B/A	P	LA	L/A	H/A	W/A
10.000	1.424	3.332	3.547	1.200	2.022

X/A	Y/A
1.000	.000
1.010	.099
1.011	.198
1.003	.296
.957	.391
.962	.484
.930	.574
.889	.669
.842	.740
.787	.816
.727	.886
.661	.949
.590	1.007
.514	1.057
.434	1.100
.352	1.136
.266	1.164
.179	1.184
.090	1.196
.000	1.200

Figure 23. Continued. (c)

B/A	P	LA	L/A	H/A	W/A
10.000	1.351	3.372	3.768	1.301	2.053

X/A	Y/A
1.000	.000
1.018	.100
1.026	.200
1.026	.299
1.017	.397
.999	.493
.973	.586
.939	.675
.893	.761
.849	.842
.794	.917
.733	.987
.663	1.051
.594	1.108
.517	1.158
.437	1.201
.354	1.237
.268	1.265
.180	1.285
.090	1.297
.000	1.301

Figure 23. Continued. (d)

B/A	P	LA	L/A	H/A	W/A
10.000	1.285	3.419	3.995	1.401	2.093

X/A	Y/A
1.000	.000
1.025	.100
1.040	.200
1.047	.301
1.044	.401
1.033	.499
1.014	.595
.986	.688
.951	.778
.908	.863
.858	.944
.802	1.019
.739	1.089
.671	1.152
.599	1.209
.521	1.259
.440	1.302
.356	1.337
.269	1.365
.181	1.385
.091	1.397
.000	1.401

Figure 23. Continued. (e)

B/A	P	LA	L/A	H/A	W/A
10.000	1.226	3.471	4.227	1.500	2.140

X/A	Y/A
1.000	.000
1.032	.104
1.055	.210
1.067	.317
1.070	.423
1.063	.527
1.047	.630
1.022	.730
.983	.826
.945	.918
.895	1.005
.838	1.086
.774	1.161
.704	1.230
.629	1.292
.548	1.346
.463	1.392
.375	1.431
.284	1.461
.191	1.483
.096	1.496
.000	1.500

Figure 23. Continued. (f)

B/A	P	LA	L/A	H/A	W/A
10.000	1.172	3.527	4.463	1.599	2.190

X/A	Y/A
1.000	.000
1.038	.104
1.067	.210
1.086	.317
1.095	.424
1.095	.530
1.085	.635
1.066	.737
1.038	.836
1.002	.932
.957	1.023
.906	1.109
.847	1.190
.781	1.265
.710	1.333
.633	1.394
.552	1.447
.466	1.493
.377	1.531
.286	1.561
.192	1.582
.097	1.595
.001	1.599

Figure 23. Continued. (g)

B/A	P	LA	L/A	H/A	W/A
10.000	1.124	3.587	4.707	1.699	2.249

X/A	Y/A
1.000	.000
1.044	.103
1.079	.209
1.103	.316
1.119	.424
1.124	.531
1.121	.638
1.108	.743
1.086	.845
1.055	.944
1.017	1.039
.970	1.130
.916	1.215
.856	1.295
.769	1.369
.716	1.436
.638	1.496
.556	1.549
.469	1.594
.380	1.632
.287	1.661
.193	1.682
.097	1.695
.001	1.699

Figure 23. Continued. (h)

B/A	P	LA	L/A	H/A	W/A
10.000	1.079	3.651	4.958	1.800	2.307

X/A	Y/A
1.000	.000
1.051	.107
1.092	.217
1.123	.330
1.144	.443
1.154	.556
1.153	.669
1.143	.780
1.123	.888
1.094	.993
1.056	1.095
1.009	1.191
.955	1.282
.893	1.368
.824	1.446
.748	1.518
.668	1.583
.582	1.639
.491	1.688
.398	1.728
.301	1.759
.202	1.782
.101	1.796
.000	1.800

Figure 23. Continued. (i)

B/A	P	LA	L/A	H/A	W/A
10.000	1.039	3.716	5.211	1.901	2.373

X/A	Y/A
1.000	.000
1.056	.106
1.103	.216
1.139	.328
1.165	.441
1.181	.556
1.187	.669
1.182	.782
1.168	.893
1.145	1.001
1.113	1.105
1.072	1.206
1.022	1.301
.960	1.391
.901	1.476
.831	1.553
.754	1.624
.672	1.687
.585	1.743
.494	1.791
.399	1.830
.302	1.861
.202	1.883
.102	1.896
.000	1.901

Figure 23. Continued. (j)

B/A 10.000	P 1.002	LA 3.783	L/A 5.466	H/A 2.001	W/A 2.438
---------------	------------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.063	.110
1.116	.224
1.158	.340
1.189	.459
1.210	.578
1.219	.698
1.218	.816
1.206	.933
1.184	1.047
1.153	1.157
1.112	1.263
1.062	1.365
1.004	1.460
.938	1.549
.865	1.632
.786	1.707
.701	1.774
.610	1.833
.516	1.884
.417	1.926
.315	1.958
.212	1.982
.106	1.996
.000	2.001

Figure 23. Continued. (k)

B/A 10.000	P .969	LA 3.850	L/A 5.721	H/A 2.100	W/A 2.506
---------------	-----------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.070	.113
1.130	.231
1.177	.352
1.214	.476
1.238	.601
1.251	.726
1.253	.850
1.243	.973
1.223	1.092
1.192	1.209
1.152	1.321
1.102	1.427
1.043	1.528
.975	1.622
.900	1.709
.818	1.789
.730	1.860
.636	1.923
.538	1.976
.435	2.020
.329	2.055
.221	2.080
.111	2.095
.000	2.100

Figure 23. Continued. (l)

B/A	P	LA	L/A	H/A	W/A
10.000	.939	3.918	5.981	2.200	2.577

X/A	Y/A
1.000	.000
1.075	.112
1.138	.229
1.191	.349
1.232	.472
1.262	.597
1.281	.722
1.288	.848
1.285	.971
1.271	1.093
1.246	1.212
1.211	1.327
1.167	1.437
1.114	1.542
1.052	1.641
.982	1.733
.906	1.819
.822	1.896
.733	1.966
.638	2.027
.539	2.079
.436	2.122
.329	2.156
.221	2.180
.111	2.195
.000	2.200

Figure 23. Continued. (m)

B/A	P	LA	L/A	H/A	W/A
10.000	.911	3.988	6.246	2.301	2.647

X/A	Y/A
1.000	.000
1.081	.115
1.152	.236
1.210	.361
1.256	.489
1.291	.619
1.313	.749
1.323	.880
1.322	1.010
1.310	1.137
1.286	1.262
1.252	1.382
1.207	1.498
1.153	1.609
1.090	1.713
1.019	1.810
.940	1.900
.854	1.981
.761	2.055
.663	2.119
.560	2.174
.453	2.219
.342	2.255
.230	2.281
.115	2.296
-.000	2.301

Figure 23. Continued. (n)

B/A 10.000	P .840	LA 4.199	L/A 7.044	H/A 2.602	W/A 2.869
---------------	-----------	-------------	--------------	--------------	--------------

X/A	Y/A
1.000	.000
1.098	.120
1.185	.247
1.259	.379
1.320	.515
1.368	.654
1.403	.796
1.425	.937
1.435	1.079
1.432	1.219
1.417	1.356
1.390	1.490
1.351	1.620
1.302	1.744
1.243	1.862
1.174	1.974
1.097	2.078
1.011	2.174
.918	2.261
.818	2.339
.712	2.408
.601	2.466
.486	2.515
.367	2.553
.246	2.580
.123	2.597
-.000	2.602

Figure 23. Continued. (q)

B/A 10.000	P .820	LA 4.270	L/A 7.311	H/A 2.702	W/A 2.943
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X/A	Y/A
1.000	.000
1.105	.123
1.197	.253
1.277	.390
1.343	.530
1.395	.675
1.434	.821
1.460	.968
1.472	1.115
1.471	1.260
1.457	1.403
1.430	1.543
1.392	1.678
1.343	1.807
1.282	1.930
1.212	2.046
1.133	2.155
1.044	2.255
.949	2.346
.846	2.427
.736	2.499
.622	2.560
.503	2.611
.380	2.650
.255	2.679
.128	2.696
-.000	2.702

Figure 23. Continued. (r)

B/A 10.000	P .801	LA 4.340	L/A 7.579	H/A 2.801	W/A 3.019
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X/A	Y/A
1.000	.000
1.112	.126
1.210	.260
1.295	.400
1.366	.546
1.423	.695
1.466	.846
1.494	.999
1.509	1.151
1.509	1.302
1.497	1.451
1.471	1.595
1.433	1.736
1.383	1.870
1.322	1.998
1.250	2.119
1.168	2.232
1.078	2.336
.979	2.431
.873	2.516
.761	2.590
.643	2.654
.520	2.707
.393	2.748
.264	2.778
.132	2.795
.000	2.801

Figure 23. Continued. (s)

B/A 10.000	P .784	LA 4.410	L/A 7.848	H/A 2.901	W/A 3.098
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X/A	Y/A
1.000	.000
1.114	.124
1.216	.256
1.304	.395
1.379	.539
1.441	.686
1.488	.837
1.522	.989
1.542	1.141
1.549	1.292
1.543	1.441
1.524	1.587
1.492	1.730
1.449	1.867
1.395	1.998
1.330	2.123
1.255	2.241
1.171	2.350
1.078	2.451
.978	2.543
.871	2.625
.758	2.697
.640	2.759
.517	2.810
.391	2.850
.262	2.878
.132	2.895
.000	2.901

Figure 23. Continued. (t)

B/A <u>10.000</u>	P .768	L/A 4.484	L/A 8.131	H/A 3.005	W/A 3.177
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X/A	Y/A
1.000	.000
1.121	.127
1.229	.263
1.323	.406
1.403	.554
1.469	.707
1.520	.863
1.557	1.020
1.580	1.177
1.588	1.334
1.583	1.489
1.565	1.641
1.534	1.788
1.490	1.931
1.435	2.067
1.369	2.197
1.292	2.319
1.206	2.433
1.111	2.538
1.008	2.633
.898	2.719
.782	2.794
.660	2.858
.533	2.910
.403	2.952
.270	2.982
.135	2.999
-.001	3.005

Figure 23. Continued. (u)

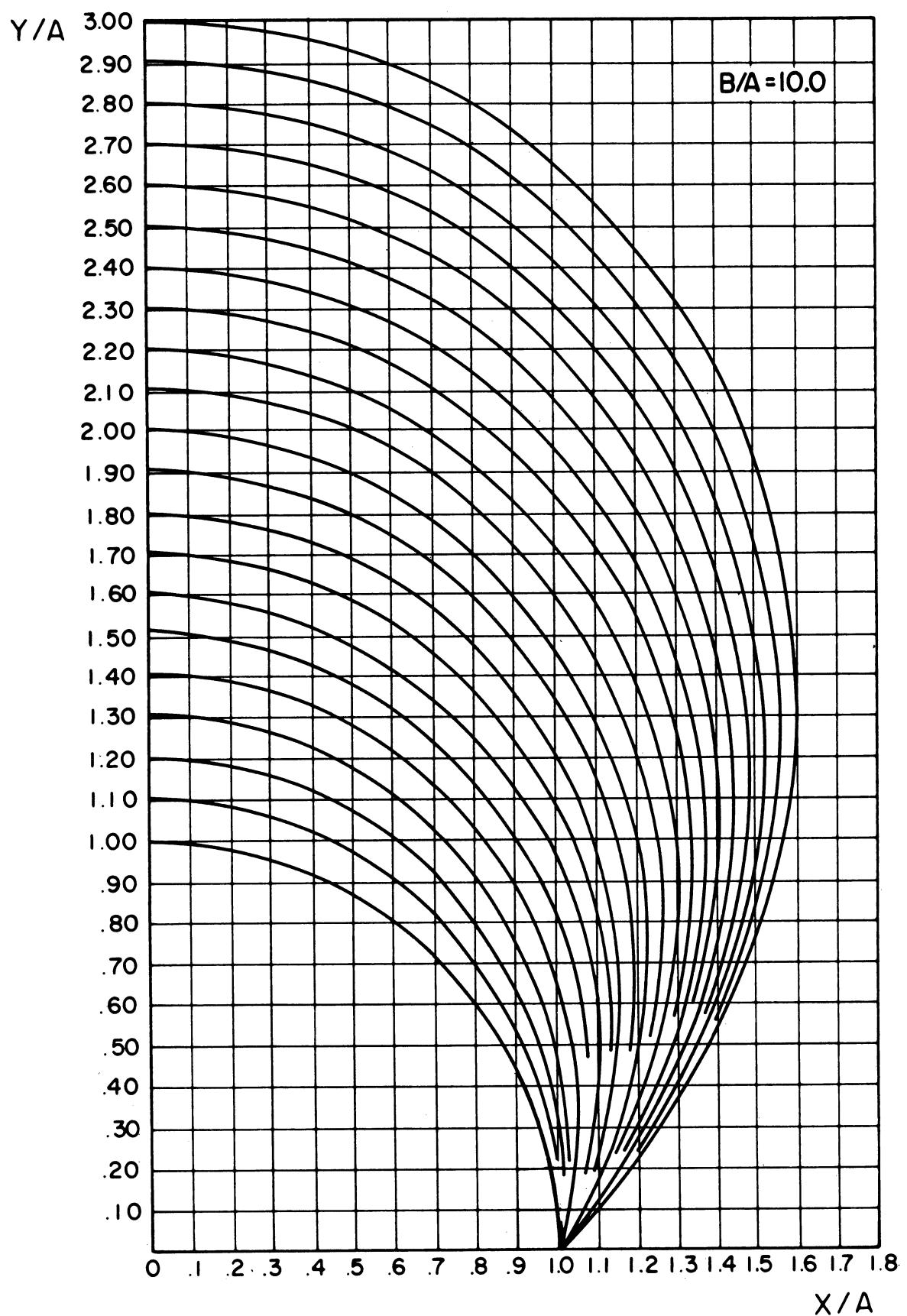


Figure 23. Concluded. (v)

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