

74412

UMTRI-86-26/II

Improving the Dynamic Performance of Multitrailer Vehicles: A Study of Innovative Dollies

Volume II

Appendices

**C. B. Winkler
P. S. Fancher
O. Carsten
A. Mathew
P. Dill**

July 1986

**UMTRI The University of Michigan
 Transportation Research Institute**

NOTICE

This document is disseminated under the sponsorship of the Department of Transportation in the interest of information exchange. The United States Government assumes no liability for its contents or use thereof.

The contents of this report reflect the views of the contractor who is responsible for the facts and the accuracy of the data presented herein. The contents do not necessarily reflect the official policy of the Department of Transportation.

This report does not constitute a standard, specification, or regulation.

The United States Government does not endorse products or manufacturers. Trademarks or manufacturers' names appear herein only because they are considered essential to the object of this document.

Technical Report Documentation Page

1. Report No. FHWA/RD-86/162	2. Government Accession No.	3. Recipient's Catalog No.	
4. Title and Subtitle IMPROVING THE DYNAMIC PERFORMANCE OF MULTITRAILER VEHICLES: A STUDY OF INNOVATIVE DOLLIES - Volume II Appendices		5. Report Date July 1986	
7. Author(s) C.B. Winkler, P.S. Fancher, O. Carsten, A. Mathew, P. Dill		6. Performing Organization Code	
9. Performing Organization Name and Address The University of Michigan Transportation Research Institute 2901 Baxter Road, Ann Arbor, Michigan 48109		8. Performing Organization Report No. UMTRI-86-26/II	
12. Sponsoring Agency Name and Address Federal Highway Administration U.S. Department of Transportation Washington, D.C. 20590		10. Work Unit No. (TRAIS) 3104-112	
		11. Contract or Grant No. DTFH61-84-C-00026	
		13. Type of Report and Period Covered Final May 1984-July 1986	
15. Supplementary Notes Contracting Officer's Technical Representative: Mr. Martin Hargrave (HSR-20)		14. Sponsoring Agency Code	
16. Abstract <p>This study of the dynamic performance of multitrailer articulated vehicles has led to the development of guidelines for the design of innovative dollies that will improve the roll stability and trailing fidelity of doubles combinations. The major effort of this project involved identification, analysis, and further development of innovative dolly and trailer hitching hardware showing potential for the reduction of rearward amplification and prevention of rollover of the second trailer. Specifically, the project (1) reviewed the current state-of-the-art in innovative coupling mechanisms, (2) performed a parametric sensitivity study, based on computer simulation techniques, on combination vehicles using existing and proposed coupling mechanisms, and incorporating various combinations of 96- and 102-in-width hardware, (3) developed a new type of dolly believed to provide superior safety performance, (4) conducted full-scale tests of combination vehicles using various dollies, including a prototype of the new dolly, and (5) examined the potential safety and economic impacts of the use of innovative dolly hardware.</p>			
<p>This volume is the second in a series. The others in the series are: FHWA No. _____ Vol. No. _____ Title _____</p> <p>RD-86/162 I Final Technical Report</p>			
17. Key Words Innovative dollies, Doubles, Roll stability Rearward amplification, Trailing fidelity, B-dollies		18. Distribution Statement No restrictions. This document is available to the public through the National Technical Information Service, Springfield, VA 22161	
19. Security Classif. (of this report) Unclassified	20. Security Classif. (of this page) Unclassified	21. No. of Pages 58	22. Price

TABLE OF CONTENTS

VOLUME I: FINAL TECHNICAL REPORT

<u>Section</u>	<u>Page</u>
INTRODUCTION.....	1
A REVIEW OF INNOVATIVE DOLLIES AND COUPLING MECHANISMS	5
1. Modified A-Dollies	8
2. B-Dollies	25
THE SIMULATION STUDY.....	32
1. The "Test" Vehicle	32
2. Findings with Respect to the Use of Innovative Coupling Mechanisms	33
3. Findings with Respect to the Use of Mixed-Width Axles	121
THE VEHICLE TEST PROGRAM	129
1. Test Dollies	133
2. Test Program Findings	149
OPERATIONAL IMPACTS	183
1. Accident Studies	183
2. Economic Analysis	204
CONCLUSIONS AND RECOMMENDATIONS	228
1. Dolly Performance and Design Guidelines	228
2. Further Development of Innovative Dollies	232
REFERENCES.....	234

VOLUME II: APPENDICES

<u>Section</u>	<u>Page</u>
APPENDIX A: EXAMPLE LISTINGS OF SIMULATED VEHICLE PARAMETERS FOR THE YAW/ROLL SIMULATION.....	1
APPENDIX B: LISTINGS OF EQUATIONS AND VARIABLES USED IN THE FINANCIAL MODEL.....	39

LIST OF TABLES

<i>Table</i>	<i>Page</i>
1. Innovative Dollies and Hitching Hardware Identified in Task A	6
2. The Screening Study Vehicles	38
3. Significant Dimensions of the Simulated Vehicle of Figures 31 and 32	60
4. Effective Damping Ratio of the Test Vehicle in a 55 mi/h (88.5 km/h) Pulse-Steer Maneuver, Equipped with the Improved Dollies and Under Differing Load Conditions	99
5. The Influence of Dolly Drawbar Length and Steering Properties on the Damping Ratio of Test Vehicle Equipped with the B-Dollies	103
6. Maximum Absolute Drawbar Hitch Loads in Emergency Lane-Change Maneuvers at the Rollover Threshold	111
7. Combinations of Axle Widths Simulated	123
8. Rollover Thresholds of A-Trains - Static Roll Model	124
9. Maximum Lateral Acceleration (in g's) Developed at the Tractor During a 2 Radian/Second Lane-Change Maneuver - A-Train: Yaw/Roll Model	125
10. Maximum Lateral Acceleration (in g's) Developed at the Tractor During a 2 Radian/Second Lane-Change Maneuver - B-Train: Yaw/Roll Model	126
11. Side Slope and Road Sinkage (25 ft (7.62 m) Distance Constant): Sinkage Constrained to the Right Side of the Vehicle - A-Trains with a Forward Velocity of 27.72 mi/h (44.60 km/h)	127
12. Test Vehicle Wheel Loads	134
13. Variables Transduced and Recorded During Testing	134
14. Test Dolly Weights	150
15. Constants Used in Correcting Rearward Amplification Measures for Variations of Test Velocity from 55 mi/h (88.5 km/h)	150
16. Damping Ratios Measured in the Vehicle Testing Program	157
17. Maximum Loadings	181
18. Tractor-Trailer Accident Involvements by Data Source and Number of Trailers	189
19. ICC-Authorized Tractor-Trailer Accident Involvements by Data Source and Number of Trailers	189
20. Tractor-Trailer Fatal Accident Involvement Rates by Data Source and Number of Trailers	192
21. Tractor-Trailer Injury (Incl. Fatal) Accident Involvement Rates by Data Source and Number of Trailers	192
22. TIFA 1980-82: Tractor-Trailer Fatal Accident Involvements by Road Class and Number of Trailers	194
23. BMCS 1984: ICC-Authorized Tractor-Trailer Accident Involvements by Road Class and Number of Trailers	194

24.	TIFA 1980-82: Tractor-Trailer Involvements by Number of Vehicles Involved and Number of Trailers	196
	25.BMCS 1984: ICC-Authorized Tractor-Trailer Accident Involvements by Number of Vehicles Involved and Number of Trailers	196
26.	TIFA 1980-82: Tractor-Trailer Involvements by First Harmful Event and Number of Trailers	197
27.	TIFA 1980-82: Tractor-Trailer Involvements by Most Harmful Event and Number of Trailers	197
28.	TIFA 1980-82: Tractor-Trailer Involvements by Rollover and Number of Trailers	198
29.	TIFA 1980-82: Tractor-Trailer Involvements by Jackknife and Number of Trailers	198
	30.BMCS 1984: ICC-Authorized Tractor-Trailer Accident Involvements by Non-Collision Type and Number of Trailers	199
31.	BMCS 1984: ICC-Authorized Tractor-Trailer Property-Damage Accident Involvements by Non-Collision Type and Number of Trailers	199
32.	NASS 1981-84: Maximum AIS (MAIS) for Injury-Level Tractor-Trailer Involvements by Number of Trailers	201
33.	The Variables Used in the Financial Model	211
34.	The Reference Condition, Results Correspond to the Purchase of Six B-Dollies	212
35.	Variations Used in Sensitivity Analysis	215
36.	The Hypothetical Situation	219
37.	Values of the Variables Used in the Hypothetical Situation	221
38.	Another Reference Condition: Lighter B-Dolly	222
39.	Lighter B-Dolly Results	223
40.	Variations Used in Sensitivity Analysis: Lighter B-Dolly	225
41.	Worst-Case Loading Values	231

VOLUME II: APPENDICES

42.	Yaw/Roll Simulation Data Echo for the Fully Loaded Double Equipped with the A-Dolly	2
43.	Yaw/Roll Simulation Data Echo for the Fully Loaded Double Equipped with the Asymmetric Trapezoidal Dolly in the Forward IC Condition	9
44.	Yaw/Roll Simulation Data Echo for the Fully Loaded Double Equipped with the Linked-Articulation Dolly with 0.44 System Gain	16
45.	Yaw/Roll Simulation Data Echo for the Fully Loaded Double Equipped with the Self-Steering B-Dolly with Full Resistance Steering	23
46.	Yaw/Roll Simulation Data Echo for the Fully Loaded Double Equipped with the Controlled-Steering B-Dolly with 0.30 Steering Gain	31
47.	Variables Used in the Operational Impacts Study	41
48.	Key to the Variables Used in the Operational Impacts Study	42
49.	Economic Issues Considered in the Operational Impacts Study	43
50.	Equations Used for the Year Zero in the Operational Impacts Study	44

51. Equations Used for Years One, Five and Nine in the Operational Impacts Study	45
52. Equations Used for Years Two, Four, Six and Eight in the Operational Impacts Study	46
53. Equations Used for Years Three and Seven in the Operational Impacts Study	47

LIST OF FIGURES

<i>Figure</i>		
	<i>Page</i>	
1. Project flow chart	4	
2. The A-dolly and B-dolly	9	
3. The symmetric, trapezoidal dolly	11	
4. A trapezoidal dolly and the equivalent, imaginary A-dolly	12	
5. The asymmetric, trapezoidal dolly	14	
6. The converter, trapezoidal dolly	15	
7. The double-cross drawbar	16	
8. The A-dolly with roller cam hitch	16	
9a. Two European, force-steer dollies	18	
9b. A Canadian forced-steer dolly	18	
10. Linked articulation dolly with telescoping member	19	
11. The skid-steer dolly	21	
12. Two extending drawbar dollies	23	
13. The locking A-dolly	24	
14. A B-train is composed of a tractor towing two or more semitrailers. The towing trailers have an extended 5th wheel for attaching the next trailer made of a B-dolly and semitrailer	26	
15a. Converter style B-dolly	27	
15b. Turntable style B-dolly	27	
16. Auto-steering B-dolly	29	
17. Turntable-steering B-dolly	29	
18. Three types of centering devices for the auto-steering axle	30	
19. The baseline simulation test vehicle: the western double	34	
20. Two modifications to the baseline vehicle	35	
21. Characteristic parameters of three types of screening study dollies	40	
a. The shifted IC dollies	40	
b. The forced-steer dollies	41	
c. The linked-articulation dolly	41	
22. Steering resistance performance of the reference self-steering axle	42	
23. Example path and acceleration data from a lane-change maneuver performed with the Yaw/Roll model	45	
24. Rearward amplification in the frequency domain: the shifted IC dollies	46	
25. Rearward amplification in the frequency domain: forced-steer dollies	47	
26. Rearward amplification in the frequency domain: the roll-stiffened pintle hitches	48	
27. Rearward amplification in the frequency domain: the linked-articulation dollies	49	
28. Rearward amplification in the frequency domain: the skid-steer dollies	50	
29. Rearward amplification in the frequency domain:		

the roll-compliant B-dollies	51
30. Rearward amplification in the frequency domain:	
the self-steering B-dollies	52
31. Peak rearward amplification of all the screening study vehicles	56
32. Schematic diagram illustrating the location of the steer point for forced-steer dollies	58
33. Rearward amplification as a function of steer-point position	61
34. Low-speed offtracking in a 50-ft (15.24-m) turn as a function of steer point position	62
35. Dynamic rollover threshold in an emergency lane change: the shifted-steer-point dollies	65
36. Dynamic rollover threshold in an emergency lane change: the roll-stiffened pintle hitches	66
37. Dynamic rollover threshold in an emergency lane change: the linked-articulation dollies	67
38. Dynamic rollover threshold in an emergency lane change: the skid-steer dollies	68
39. Dynamic rollover threshold in an emergency lane change: the roll-compliant B-dollies	69
40. Dynamic rollover threshold in an emergency lane change: the self-steering B-dollies	71
41. Dynamic rollover threshold in an emergency lane change of all the screening study dollies	72
42. Maximum offtracking performance of the screening study vehicles in a 50-ft- (15.24-m-) radius turn	74
43. Offtracking behavior with the skid-steer dolly	75
44. Ackerman steer geometry applied to the linked-articulation dolly	80
45. Ackerman steer geometry applied to the controlled-steering dolly	83
46. Comparison of the rearward amplification of the improved dollies under four loading conditions	85
a. Trailer loading conditions: full/full	85
b. Trailer loading conditions: full/empty	85
c. Trailer loading conditions: empty/full	86
d. Trailer loading conditions: empty/empty	86
47. The influence of loading condition on the rearward amplification of the improved dollies	87
a. The trapezoidal dolly, forward IC position	87
b. The linked-articulation dolly, 0.44 system gain	87
c. The self-steering B-dolly, full steering resistance	88
d. The CSB-dolly, 0.30 steering gain	88
48. Less favorable rearward amplification performance	89
a. The trapezoidal dolly, rearward IC position	89
b. The self-steering B-dolly, low steering resistance	89
49. The influence of forward velocity on rearward amplification	90
a. The A-train	90
b. The trapezoidal dolly, forward IC position	90

c. The trapezoidal dolly, rearward IC position	91
d. The linked-articulation dolly, 0.44 system gain	91
e. The self-steering B-dolly, full resistance steering	92
f. The self-steering B-dolly, low resistance steering	92
g. The CSB-dolly, 0.30 steering gain	93
50. Dynamic rollover threshold of the improved dollies	95
51. Low-speed offtracking performance of the selected dollies	96
52. Lateral acceleration response to a steering pulse: the reference A-train	97
53. Lateral acceleration response to a steering pulse: the linked- articulation dolly, 0.44 system gain	100
54. Lateral acceleration response to a steering pulse: the CSB-dolly, 0.30 steering gain	101
55. Lateral acceleration response to a steering pulse: the self-steering B-dolly, full steering resistance	102
56. Lateral acceleration response to a steering pulse: the self-steering B-dolly, low steering resistance	104
57. Lateral acceleration response to a steering pulse: the self-steering B-dolly, long drawbar, low steering resistance	105
58. Lateral acceleration response to a steering pulse: the CSB-dolly, long drawbar, 0.30 steering gain	106
59. Lateral acceleration response to a steering pulse: the CSB-dolly, long drawbar, 0.43 steering gain	107
60a. The A-dolly hitch loads	109
60b. The trapezoidal dolly hitch loads	109
60c. Linked articulation dolly hitch loads	110
60d. B-dolly hitch loads	110
61. Straight-line braking (wet surface), deceleration at the occurrence of wheel lock, empty vehicles	113
62. Straight-line braking (wet surface), deceleration at the occurrence of 10° articulation angles, empty vehicles	115
63. Braking in a turn (wet surface), deceleration at the occurrence of wheel lock, empty vehicles	116
64. Braking in a turn (wet surface), deceleration at the occurrence of 10° articulation angles, empty vehicles	117
65. Braking in a turn (dry surface), deceleration at the occurrence of axle lock, loaded vehicles	118
66. Braking in a turn (dry surface), deceleration at the occurrence of 10° articulation angles, loaded vehicles	119
67. Straight-line braking (split surface), deceleration at the occurrence of wheel lock, loaded vehicles	120
68. The geometry of the test vehicle	130
69. The test vehicle	131
70. Test vehicle loading	132
71. The drawbar hitch load transducer	135
72. The A-dolly	136

73.	The asymmetric trapezoidal dolly	137
74.	The linked-articulation dolly	138
75.	The auto-steering B-dolly	139
76.	The controlled-steering B-dolly	140
77.	The forward and rearward IC position of the trapezoidal dolly hitch	142
	a. The forward IC position	142
	b. The rearward IC position	142
78.	Castered steering system kingpin of the auto-steer-style dolly	143
79.	The centering mechanism of the self-steering B-dolly	144
80.	Schematic diagram of the CSB-dolly steering linkage	145
81.	Schematic diagram of the CSB-dolly steering connection with its trailer	146
82.	A top view of the CSB-dolly upper steering arm	147
83.	The CSB-dolly steering linkage	148
84.	Rearward amplification performance results for all of the test dollies	151
85.	Comparison of test and simulation rearward amplification performance measures	151
	a. A-train	151
	b. Linked-articulation dolly	152
	c. Trapezoidal dolly, forward position	152
	d. Self-steering B-dolly, full resistance steering	153
	e. Controlled steering B-dolly, 0.30 steering system gain	153
86.	Rollover threshold of the test vehicle equipped with the various test dollies	155
87.	Example pulse-steer time histories of steering and lateral acceleration response	156
88.	Example pulse-steer response for each test dolly	158
	a. The LA.8 dolly	158
	b. The TRAP.F dolly	158
	c. The TRAP.R dolly	159
	d. The SA.60 dolly	159
	e. The SA.0 dolly	160
	f. The CSB.30 dolly	160
89.	Low-speed offtracking in a 50-ft- (15.24-m-) radius turn	162
	a. 50-ft- (15.24-m-) radius, 90 degree arc	162
	b. 50-ft- (15.24-m-) radius, 180 degree arc	162
90.	High-speed offtracking in a 1000-ft- (304.8-m-) radius turn at 45 mi/h (72.42 km/h)	163
	a. Absolute outboard offtracking	163
	b. High-speed outboard offtracking component	163
91.	Brake pressure and longitudinal deceleration time histories during braking-in-a-turn: run number 443	165
92.	Articulation angle and steering wheel angle time histories during braking-in-a-turn: run number 443	166
93.	Articulation angle and steering wheel angle time histories during braking-in-a-turn: run number 442	167

94.	Articulation angle and steering wheel angle time histories during braking-in-a-turn: run number 460	169
95.	Articulation angle and steering wheel angle time histories during braking-in-a-turn: run number 466	170
96.	Articulation angle and steering wheel angle time histories during braking-in-a-turn: run number 465	171
97.	Articulation angle and steering wheel angle time histories during braking-in-a-turn: run number 437	172
98.	Articulation angle and steering wheel angle time histories during braking-in-a-turn: run number 447	173
99.	Articulation angle and steering wheel angle time histories during braking-in-a-turn: run number 450	174
100.	Articulation angle and steering wheel angle time histories during braking-in-a-turn: run number 131	176
101.	Articulation angle and steering wheel angle time histories during braking-in-a-turn: run number 132	177
102.	The curb-climbing test	178
103.	The severe steer test	180
104.	Operating cost sensitivities for a current small fleet (the more important variables)	216
105.	Operating cost sensitivities for a current small fleet (the less important variables)	217
106.	Operating cost sensitivities for a lighter B-dolly	226

ACKNOWLEDGEMENTS

The success of this project is the result of the cooperation of a number of individuals and organizations, too numerous to allow a complete listing here. Special thanks are due, however, to the following: Mr. Norman Gallatin of the Trapezoid Corporation; Mr. William Feight Sr. of Truck Safety Systems; Mr. N. Royce Curry (formerly of ASTL) and Mr. Mike Krymski of Auto Steering Trailers Limited; Mr. Adrian Hulverson and Mr. Phil Pierce of the Fruehauf Corporation; Mr. Norman Burns of Highways and Transportation of the Province of Saskatchewan; Mr. Jack Baynes of the Department of Transportation of the Province of Alberta; Mr. Wayne Kaldestead and Mr. Fred Kearns of TRIMAC Transportation Services; Mr. Roy Margenau and Mr. Elmer Kiel of Chrysler Proving Grounds; and Mr. Martin Hargrave who served as the Contracting Officer's Technical Representative for FHWA.

The authors wish to thank John Koch, Tom Dixon, Michael Hagan, Michael Campbell, Jeannette Leveille, Kathy Richards, and David Toepler of the UMTRI staff for their efforts in this project.

Appendix A

Example Listings of Simulated Vehicle Parameters For the Yaw/Roll Simulation

Table 42. Yaw/Roll Simulation Data Echo for the Fully Loaded Double Equipped with the A-dolly.

DIRECTIONAL RESPONSE SIMULATION

FHWA FIVE-AXLE DOUBLE / 27-Ft TRAILERS (A-TRAIN, FULL/FULL)

# OF SPRUNG MASSES	=	4
TOTAL # OF AXLES	=	5
GROSS VEHICLE WEIGHT	=	80000.00 L.B.
FORWARD VELOCITY	=	55.00 M.P.H
PEAK FRICTIONAL COEFFICIENT	=	1.00

	DISTANCE AHEAD OF SPRUNG MASS C.G. (INCHES)	HEIGHT BELOW SPRUNG MASS C.G. (INCHES)	ROLL STIFFNESS (IN.LB/DEG)	TYPE OF CONSTRAINT
ARTICULATION PT # 1 ON UNIT # 1	-87.27	-4.00	999999.00	1
ARTICULATION PT # 2 ON UNIT # 2	138.40	33.30		
ARTICULATION PT # 2 ON UNIT # 2	-159.63	37.30	0.0	1
ARTICULATION PT # 3 ON UNIT # 3	80.00	0.0	-4.00	1
ARTICULATION PT # 3 ON UNIT # 3	0.0	0.0	999999.00	
ARTICULATION PT # 4 ON UNIT # 4	136.20	32.70		
TYPE OF CONSTRAINT :	O1 CONVENTIONAL 5TH WHEEL O2 INVERTED 5TH WHEEL O3 PINNLE HOOK O4 KING PIN(RIGID IN ROLL & PITCH)			

Table 42 (continued). Yaw/Roll Simulation Data Echo
for the Fully Loaded Double Equipped with the A-dolly.

FHWA FIVE-AXLE DOUBLE / 27-FT TRAILERS (A-TRAIN, FULL/FULL)

UNIT # 1

OF AXLES ON THIS UNIT = 2

WEIGHT OF SPRUNG MASS = 9700.00 LB.

ROLL MOMENT OF INERTIA OF SPRUNG MASS = 15000.00 LB.IN.SEC**2

PITCH MOMENT OF INERTIA OF SPRUNG MASS = 75000.00 LB.IN.SEC**2

YAW MOMENT OF INERTIA OF SPRUNG MASS = 75000.00 LB.IN.SEC**2

HEIGHT OF SPRUNG MASS CG ABOVE GROUND = 44.00 INCHES

AXLE # 1 AXLE # 2 AXLE #

***** ***** ***** ***** ***** *****

LOAD ON EACH AXLE (LB.) 10000.00 17500.00

AXLE WEIGHT (LB.) 1200.00 2300.00

AXLE ROLL M.I (LB.IN.SEC**2) 3719.00 4458.00

X DIST FROM SP MASS CG (IN) 24.00 -96.00

HEIGHT OF AXLE C.G. ABOVE GROUND (INCHES) 19.50 19.50

HEIGHT OF ROLL CENTER ABOVE GROUND (INCHES) 23.00 29.00

HALF SPRING SPACING (IN) 16.00 19.00

HALF TRACK - INNER TIRES (IN) 40.00 29.50

DUAL TIRE SPACING (IN) 0.0 13.00

STIFFNESS OF EACH TIRE (LB/IN) 4500.00 4500.00

ROLL STEER COEFFICIENT 0.0 0.0

AUX ROLL STIFFNESS (IN.LB/DEG) 1500.00 8000.00

SPRING COULOMB FRICTION - PER SPRING (LB) 300.00 1000.00

VISCOUS DAMPING PER SPRING (LB.SEC/IN) 0.0 0.0

SPRING TABLE # 1 2

CORNERING FORCE TABLE # 1 1

ALIGNING TORQUE TABLE # 1 1

Table 42 (continued). Yaw/Roll Simulation Data Echo
for the Fully Loaded Double Equipped with the A-dolly.

FHWA FIVE-AXLE DOUBLE / 27-FT TRAILERS (A-TRAIN, FULL/FULL)

UNIT # 2

OF AXLES ON THIS UNIT = 1

WEIGHT OF SPRUNG MASS = 30300.00 LB.

ROLL MOMENT OF INERTIA OF SPRUNG MASS = 101204.00 LB.IN.SEC**2

PITCH MOMENT OF INERTIA OF SPRUNG MASS = 475638.00 LB.IN.SEC**2

YAW MOMENT OF INERTIA OF SPRUNG MASS = 469434.00 LB.IN.SEC**2

HEIGHT OF SPRUNG MASS CG ABOVE GROUND = 81.30 INCHES

AXLE # 3 AXLE #

***** * ***** ***** ***** ***** *****

LOAD ON EACH AXLE (LB.) 17500.00

AXLE WEIGHT (LB.) 1500.00

AXLE ROLL M.I (LB.IN.SEC**2) 4100.00

X DIST FROM SP MASS CG (IN) -123.70

HEIGHT OF AXLE C.G. ABOVE GROUND (INCHES) 19.50

HEIGHT OF ROLL CENTER ABOVE GROUND (INCHES) 29.00

HALF SPRING SPACING (IN) 19.00

HALF TRACK - INNER TIRES (IN) 29.50

DUAL TIRE SPACING (IN) 13.00

STIFFNESS OF EACH TIRE (LB/IN) 4500.00

ROLL STEER COEFFICIENT 0.0

AUX ROLL STIFFNESS (IN.LB/DEG) 10000.00

SPRING COULOMB FRICTION - PER SPRING (LB) 1000.00

VISCOSUS DAMPING PER SPRING (LB.SEC/IN) 0.0

SPRING TABLE # 3

CORNERING FORCE TABLE # 1

ALIGNING TORQUE TABLE # 1

Table 42 (continued). Yaw/Roll Simulation Data Echo
for the Fully Loaded Double Equipped with the A-dolly.

FHWA FIVE-AXLE DOUBLE / 27-FT TRAILERS (A-TRAIN, FULL/FULL)	
UNIT # 3	

# OF AXLES ON THIS UNIT =	1
WEIGHT OF SPRUNG MASS =	1000.00 LB.
ROLL MOMENT OF INERTIA OF SPRUNG MASS =	1900.00 LB.IN.SEC**2
PITCH MOMENT OF INERTIA OF SPRUNG MASS =	2560.00 LB.IN.SEC**2
YAW MOMENT OF INERTIA OF SPRUNG MASS =	2560.00 LB.IN.SEC**2
HEIGHT OF SPRUNG MASS CG ABOVE GROUND =	44.00 INCHES
AXLE # 4	AXLE #
*****	*****
LOAD ON EACH AXLE (LB.)	17500.00
AXLE WEIGHT (LB.)	1500.00
AXLE ROLL M.I (LB.IN.SEC**2)	4100.00
X DIST FROM SP MASS CG (IN)	0.0
HEIGHT OF AXLE C.G. ABOVE GROUND (INCHES)	19.50
HEIGHT OF ROLL CENTER ABOVE GROUND (INCHES)	29.00
HALF SPRING SPACING (IN)	19.00
HALF TRACK - INNER TIRES (IN)	29.50
DUAL TIRE SPACING (IN)	13.00
STIFFNESS OF EACH TIRE (LB/IN)	4500.00
ROLL STEER COEFFICIENT	0.0
AUX ROLL STIFFNESS (IN.LB/DEG)	10000.00
SPRING COULOMB FRICTION - PER SPRING (LB)	1000.00
VISCOUS DAMPING PER SPRING (LB.SEC/IN)	0.0
SPRING TABLE #	3
CORNERING FORCE TABLE #	1
ALIGNING TORQUE TABLE #	1

Table 42 (continued). Yaw/Roll Simulation Data Echo
for the Fully Loaded Double Equipped with the A-dolly.

FHWA FIVE-AXLE DOUBLE / 27-FT TRAILERS (A-TRAIN, FULL/FULL)

UNIT # 4

OF AXLES ON THIS UNIT = 1

WEIGHT OF SPRUNG MASS = 31000.00 LB.

ROLL MOMENT OF INERTIA OF SPRUNG MASS = 108375.00 LB.IN.SEC**2

PITCH MOMENT OF INERTIA OF SPRUNG MASS = 497375.00 LB.IN.SEC**2

YAW MOMENT OF INERTIA OF SPRUNG MASS = 490000.00 LB.IN.SEC**2

HEIGHT OF SPRUNG MASS CG ABOVE GROUND = 80.70 INCHES

AXLE # 5 AXLE #

***** ***** ***** ***** ***** *****

LOAD ON EACH AXLE (LB.) 17500.00

AXLE WEIGHT (LB.) 1500.00

AXLE ROLL M.I (LB.IN.SEC**2) 4100.00

X DIST FROM SP MASS CG (IN) -127.80

HEIGHT OF AXLE C.G. ABOVE GROUND (INCHES) 19.50

HEIGHT OF ROLL CENTER ABOVE GROUND (INCHES) 29.00

HALF SPRING SPACING (IN) 19.00

HALF TRACK - INNER TIRES (IN) 29.50

DUAL TIRE SPACING (IN) 13.00

STIFFNESS OF EACH TIRE (LB/IN) 4500.00

ROLL STEER COEFFICIENT 0.0

AUX ROLL STIFFNESS (IN.LB/DEG) 10000.00

SPRING COULOMB FRICTION - PER SPRING (LB) 1000.00

VISCOUS DAMPING PER SPRING (LB.SEC/IN) 0.0

SPRING TABLE # 3

CORNERING FORCE TABLE # 1

ALIGNING TORQUE TABLE # 1

Table 42 (continued). Yaw/Roll Simulation Data Echo
for the Fully Loaded Double Equipped with the A-dolly.

SPRING TABLE # 1

FORCE LB	DEFLECTION INCHES
-------------	----------------------

-20000.00	-20.00
0.0	0.0
8645.00	7.20
25000.00	7.50

SPRING TABLE # 2

FORCE LB	DEFLECTION INCHES
-------------	----------------------

-29800.00	-11.00
0.0	-1.00
0.0	0.0
4650.00	1.00
7650.00	1.50
11650.00	2.00
16300.00	2.50
21600.00	3.00
59500.00	4.00

SPRING TABLE # 3

FORCE LB	DEFLECTION INCHES
-------------	----------------------

-40500.00	-11.00
0.0	-1.50
0.0	0.0
2812.00	0.50
7188.00	1.00
12175.00	1.50

17913.00	2.00
24063.00	2.50
56000.00	3.00

Table 42 (continued). Yaw/Roll Simulation Data Echo
for the Fully Loaded Double Equipped with the A-dolly.

CORNERING FORCE TABLE # 1

LATERAL FORCE VS. SLIP ANGLE

0.0	1.00	2.00	4.00	6.00	12.00
3000.00	540.00	990.00	1710.00	2130.00	2490.00
6000.00	840.00	1500.00	2760.00	3480.00	4140.00
9000.00	990.00	1710.00	3420.00	4680.00	6210.00

ALIGNING TORQUE TABLE # 1

ALIGNING TORQUE VS. SLIP ANGLE

0.0	1.00	3.00	4.00	5.00	7.00	10.00
3000.00	660.00	1104.00	1200.00	1440.00	1500.00	1200.00
6000.00	1560.00	3132.00	3600.00	4248.00	4476.00	3984.00
9000.00	2400.00	5424.00	6396.00	7500.00	7800.00	6780.00

Table 43. Yaw/Roll Simulation Data Echo for the Fully Loaded Double Equipped
with the Asymmetric Trapezoidal Dolly in the Forward IC Condition.

DIRECTIONAL RESPONSE SIMULATION

FIVIA FIVE-AXLE DOUBLE / 27-Ft TRAILERS (4-BAR FORWARD, FUL/FULL)

# OF SPRUNG MASSES	=	4
TOTAL # OF AXLES	=	5
GROSS VEHICLE WEIGHT	=	80000.00 LB.
FORWARD VELOCITY	=	55.00 M.P.H

PEAK FRICTIONAL COEFFICIENT = 1.00

	DISTANCE AHEAD OF SPRUNG MASS C.G. (INCHES)	HEIGHT BELOW SPRUNG MASS C.G. (INCHES)	ROLL STIFFNESS (IN.LB/DEG)	TYPE OF CONSTRAINT
ARTICULATION PT # 1	-87.27	-4.00	999999.98	1
	138.40	33.30		
ARTICULATION PT # 2	-41.00	37.30	0.0	1
	198.50	0.0		
ARTICULATION PT # 3	0.0	-4.00	999999.98	1
	136.20	32.70		
TYPE OF CONSTRAINT :	O1 CONVENTIONAL 5TH WHEEL O2 INVERTED 5TH WHEEL O3 PINTLE HOOK O4 KING PIN(RIGID IN ROLL & PITCH)			

Table 43 (continued). Yaw/Roll Simulation Data Echo
for the Fully Loaded Double Equipped with the Asymmetric Trapezoidal
Dolly in the Forward IC Condition.

FHWA FIVE-AXLE DOUBLE / 27-FT TRAILERS (4-BAR FORWARD, FULL/FULL)		
UNIT # 1		

# OF AXLES ON THIS UNIT =	2	
WEIGHT OF SPRUNG MASS =	9700.00 LB.	
ROLL MOMENT OF INERTIA OF SPRUNG MASS =	15000.00 LB.IN.SEC**2	
PITCH MOMENT OF INERTIA OF SPRUNG MASS =	75000.00 LB.IN.SEC**2	
YAW MOMENT OF INERTIA OF SPRUNG MASS =	75000.00 LB.IN.SEC**2	
HEIGHT OF SPRUNG MASS CG ABOVE GROUND =	44.00 INCHES	
	AXLE # 1	AXLE # 2
	*****	*****
LOAD ON EACH AXLE (LB.)	10000.00	17500.00
AXLE WEIGHT (LB.)	1200.00	2300.00
AXLE ROLL M.I (LB.IN.SEC**2)	3719.00	4458.00
X DIST FROM SP MASS CG (IN)	24.00	-96.00
HEIGHT OF AXLE C.G. ABOVE GROUND (INCHES)	19.50	19.50
HEIGHT OF ROLL CENTER ABOVE GROUND (INCHES)	23.00	29.00
HALF SPRING SPACING (IN)	16.00	19.00
HALF TRACK - INNER TIRES (IN)	40.00	29.50
DUAL TIRE SPACING (IN)	0.0	13.00
STIFFNESS OF EACH TIRE (LB/IN)	4500.00	4500.00
ROLL STEER COEFFICIENT	0.0	0.0
AUX ROLL STIFFNESS (IN.LB/DEG)	1500.00	8000.00
SPRING COULOMB FRICTION - PER SPRING (LB)	300.00	1000.00
VISCOUS DAMPING PER SPRING (LB.SEC/IN)	0.0	0.0
SPRING TABLE #	1	2
CORNERING FORCE TABLE #	1	1
ALIGNING TORQUE TABLE #	1	1

Table 43 (continued). Yaw/Roll Simulation Data Echo
for the Fully Loaded Double Equipped with the Asymmetric Trapezoidal
Dolly in the Forward IC Condition.

FHWA FIVE-AXLE DOUBLE / 27-FT TRAILERS (4-BAR FORWARD, FULL/FULL)

UNIT # 2

OF AXLES ON THIS UNIT = 1

WEIGHT OF SPRUNG MASS = 30300.00 LB.

ROLL MOMENT OF INERTIA OF SPRUNG MASS = 101204.00 LB.IN.SEC**2

PITCH MOMENT OF INERTIA OF SPRUNG MASS = 475638.00 LB.IN.SEC**2

YAW MOMENT OF INERTIA OF SPRUNG MASS = 469434.00 LB.IN.SEC**2

HEIGHT OF SPRUNG MASS CG ABOVE GROUND = 81.30 INCHES

AXLE # 3

LOAD ON EACH AXLE (LB.) 17500.00

AXLE WEIGHT (LB.) 1500.00

AXLE ROLL M.I (LB.IN.SEC**2) 4100.00

X DIST FROM SP MASS CG (IN) -123.70

HEIGHT OF AXLE C.G. ABOVE GROUND (INCHES) 19.50

HEIGHT OF ROLL CENTER ABOVE GROUND (INCHES) 29.00

HALF SPRING SPACING (IN) 19.00

HALF TRACK - INNER TIRES (IN) 29.50

DUAL TIRE SPACING (IN) 13.00

STIFFNESS OF EACH TIRE (LB/IN) 4500.00

ROLL STEER COEFFICIENT 0.0

AUX ROLL STIFFNESS (IN.LB/DEG) 10000.00

SPRING COULOMB FRICTION - PER SPRING (LB) 1000.00

VISCOS DAMPING PER SPRING (LB.SEC/IN) 0.0

SPRING TABLE # 3

CORNERING FORCE TABLE # 1

ALIGNING TORQUE TABLE # 1

Table 43 (continued). Yaw/Roll Simulation Data Echo
for the Fully Loaded Double Equipped with the Asymmetric Trapezoidal
Dolly in the Forward IC Condition.

FHWA FIVE-AXLE DOUBLE / 27-FT TRAILERS (4-BAR FORWARD, FULL/FULL)

UNIT # 3

OF AXLES ON THIS UNIT = 1

WEIGHT OF SPRUNG MASS = 1000.00 LB.

ROLL MOMENT OF INERTIA OF SPRUNG MASS = 1900.00 LB.IN.SEC**2

PITCH MOMENT OF INERTIA OF SPRUNG MASS = 2560.00 LB.IN.SEC**2

YAW MOMENT OF INERTIA OF SPRUNG MASS = 2560.00 LB.IN.SEC**2

HEIGHT OF SPRUNG MASS CG ABOVE GROUND = 44.00 INCHES

AXLE # 4

LOAD ON EACH AXLE (LB.) 17500.00

AXLE WEIGHT (LB.) 1500.00

AXLE ROLL M.I (LB.IN.SEC**2) 4100.00

X DIST FROM SP MASS CG (IN) 0.0

HEIGHT OF AXLE C.G. ABOVE GROUND (INCHES) 19.50

HEIGHT OF ROLL CENTER ABOVE GROUND (INCHES) 29.00

HALF SPRING SPACING (IN) 19.00

HALF TRACK - INNER TIRES (IN) 29.50

DUAL TIRE SPACING (IN) 13.00

STIFFNESS OF EACH TIRE (LB/IN) 4500.00

ROLL STEER COEFFICIENT 0.0

AUX ROLL STIFFNESS (IN.LB/DEG) 10000.00

SPRING COULOMB FRICTION - PER SPRING (LB) 1000.00

VISCOUS DAMPING PER SPRING (LB.SEC/IN) 0.0

SPRING TABLE # 3

CORNERING FORCE TABLE # 1

ALIGNING TORQUE TABLE # 1

Table 43 (continued). Yaw/Roll Simulation Data Echo
for the Fully Loaded Double Equipped with the Asymmetric Trapezoidal
Dolly in the Forward IC Condition.

FHWA FIVE-AXLE DOUBLE / 27-FT TRAILERS (4-BAR FORWARD, FULL/FULL)

UNIT # 4

OF AXLES ON THIS UNIT = 1

WEIGHT OF SPRUNG MASS = 31000.00 LB.

ROLL MOMENT OF INERTIA OF SPRUNG MASS = 108375.00 LB.IN.SEC**2

PITCH MOMENT OF INERTIA OF SPRUNG MASS = 497375.00 LB.IN.SEC**2

YAW MOMENT OF INERTIA OF SPRUNG MASS = 490000.00 LB.IN.SEC**2

HEIGHT OF SPRUNG MASS CG ABOVE GROUND = 80.70 INCHES

AXLE # 5

LOAD ON EACH AXLE (LB.) 17500.00

AXLE WEIGHT (LB.) 1500.00

AXLE ROLL M.I (LB.IN.SEC**2) 4100.00

X DIST FROM SP MASS CG (IN) -127.80

HEIGHT OF AXLE C.G. ABOVE GROUND (INCHES) 19.50

HEIGHT OF ROLL CENTER ABOVE GROUND (INCHES) 29.00

HALF SPRING SPACING (IN) 19.00

HALF TRACK - INNER TIRES (IN) 29.50

DUAL TIRE SPACING (IN) 13.00

STIFFNESS OF EACH TIRE (LB/IN) 4500.00

ROLL STEER COEFFICIENT 0.0

AUX ROLL STIFFNESS (IN.LB/DEG) 10000.00

SPRING COULOMB FRICTION - PER SPRING (LB) 1000.00

VISCOUS DAMPING PER SPRING (LB.SEC/IN) 0.0

SPRING TABLE # 3

CORNERING FORCE TABLE # 1

ALIGNING TORQUE TABLE # 1

Table 43 (continued). Yaw/Roll Simulation Data Echo
for the Fully Loaded Double Equipped with the Asymmetric Trapezoidal
Dolly in the Forward IC Condition.

SPRING TABLE # 1

FORCE LB	DEFLECTION INCHES
-------------	----------------------

-20000.00	-20.00
-----------	--------

0.0	0.0
-----	-----

8645.00	7.20
---------	------

25000.00	7.50
----------	------

SPRING TABLE # 2

FORCE LB	DEFLECTION INCHES
-------------	----------------------

-29800.00	-11.00
-----------	--------

0.0	-1.00
-----	-------

0.0	0.0
-----	-----

4650.00	1.00
---------	------

7650.00	1.50
---------	------

11650.00	2.00
----------	------

16300.00	2.50
----------	------

21600.00	3.00
----------	------

59500.00	4.00
----------	------

SPRING TABLE # 3

FORCE LB	DEFLECTION INCHES
-------------	----------------------

-40500.00	-11.00
-----------	--------

0.0	-1.50
-----	-------

0.0	0.0
-----	-----

2812.00	0.50
---------	------

7188.00	1.00
---------	------

12175.00	1.50
----------	------

17913.00	2.00
----------	------

24063.00	2.50
----------	------

56000.00	3.00
----------	------

Table 43 (continued). Yaw/Roll Simulation Data Echo
 for the Fully Loaded Double Equipped with the Asymmetric Trapezoidal
 Dolly in the Forward IC Condition.

CORNERING FORCE TABLE # 1

LATERAL FORCE VS. SLIP ANGL

0.0	1.00	2.00	4.00	6.00	12.00
3000.00	540.00	990.00	1710.00	2130.00	2490.00
6000.00	840.00	1500.00	2760.00	3480.00	4140.00
9000.00	990.00	1710.00	3420.00	4680.00	6210.00

ALIGNING TORQUE TABLE # 1

ALIGNING TORQUE VS. SLIP ANGLE

0.0	1.00	3.00	4.00	5.00	7.00	10.00
3000.00	660.00	1104.00	1200.00	1440.00	1500.00	1200.00
6000.00	1560.00	3132.00	3600.00	4248.00	4476.00	3984.00
9000.00	2400.00	5424.00	6396.00	7500.00	7800.00	6780.00

Table 44. Yaw/Roll Simulation Data Echo for the Fully Loaded Double Equipped with the Linked-Articulation Dolly with 0.44 System Gain.

 DIRECTIONAL RESPONSE SIMULATION

FHWA FIVE-AXLE DOUBLE / 27-FT TRAILERS (LINKED ARTIC GAIN .44 FULL/FULL)

OF SPRUNG MASSES = 4
 TOTAL # OF AXLES = 5
 GROSS VEHICLE WEIGHT = 80000.00 LB.
 FORWARD VELOCITY = 55.00 M.P.H

PEAK FRICTIONAL COEFFICIENT = 1.00

	DISTANCE AHEAD OF SPRUNG MASS C.G. (INCHES)	HEIGHT BELOW SPRUNG MASS C.G. (INCHES)	ROLL STIFFNESS (IN.LB/DEG)	TYPE OF CONSTRAINT
ARTICULATION PT # 1 ON UNIT # 1	-87.27	-4.00	999999.88	1
ON UNIT # 2	138.40	33.30		
ARTICULATION PT # 2 ON UNIT # 2	-159.63	37.30	0.0	1
ON UNIT # 3	80.00	0.0		
ARTICULATION PT # 3 ON UNIT # 3	0.0	-4.00	999999.88	1
ON UNIT # 4	136.20	32.70		

LINKED ARTICULATION: GAIN: 0.44 STIFFNESS: 10000000.00 (IN-LB/DEG GAMMA2)

TYPE OF CONSTRAINT :
 01 CONVENTIONAL 5TH WHEEL
 02 INVERTED 5TH WHEEL
 03 PINTLE HOOK
 04 KING PIN(RIGID IN ROLL & PITCH)

Table 44 (continued). Yaw/Roll Simulation Data Echo for the Fully Loaded Double Equipped with the Linked-Articulation Dolly with 0.44 System Gain.

FHWA FIVE-AXLE DOUBLE / 27-FT TRAILERS (LINKED ARTIC GAIN .44 FULL/FULL)

UNIT # 1		

# OF AXLES ON THIS UNIT =	2	
WEIGHT OF SPRUNG MASS =	9700.00 LB.	
ROLL MOMENT OF INERTIA OF SPRUNG MASS =	15000.00 LB.IN.SEC**2	
PITCH MOMENT OF INERTIA OF SPRUNG MASS =	75000.00 LB.IN.SEC**2	
YAW MOMENT OF INERTIA OF SPRUNG MASS =	75000.00 LB.IN.SEC**2	
HEIGHT OF SPRUNG MASS CG ABOVE GROUND =	44.00 INCHES	
AXLE # 1	AXLE # 2	
*****	*****	
LOAD ON EACH AXLE (LB.)	10000.00	17500.00
AXLE WEIGHT (LB.)	1200.00	2300.00
AXLE ROLL M.I (LB.IN.SEC**2)	3719.00	4458.00
X DIST FROM SP MASS CG (IN)	24.00	-96.00
HEIGHT OF AXLE C.G. ABOVE GROUND (INCHES)	19.50	19.50
HEIGHT OF ROLL CENTER ABOVE GROUND (INCHES)	23.00	29.00
HALF SPRING SPACING (IN)	16.00	19.00
HALF TRACK - INNER TIRES (IN)	40.00	29.50
DUAL TIRE SPACING (IN)	0.0	13.00
STIFFNESS OF EACH TIRE (LB/IN)	4500.00	4500.00
ROLL STEER COEFFICIENT	0.0	0.0
AUX ROLL STIFFNESS (IN.LB/DEG)	1500.00	8000.00
SPRING COULOMB FRICTION - PER SPRING (LB)	300.00	1000.00
VISCOUS DAMPING PER SPRING (LB.SEC/IN)	0.0	0.0
SPRING TABLE #	1	2
CORNERING FORCE TABLE #	1	1
ALIGNING TORQUE TABLE #	1	1

Table 44 (continued). Yaw/Roll Simulation Data Echo for the Fully Loaded Double Equipped with the Linked-Articulation Dolly with 0.44 System Gain.

FHWA FIVE-AXLE DOUBLE / 27-FT TRAILERS (LINKED ARTIC GAIN .44 FULL/FULL)

UNIT # 2	

# OF AXLES ON THIS UNIT =	1
WEIGHT OF SPRUNG MASS =	30300.00 LB.
ROLL MOMENT OF INERTIA OF SPRUNG MASS =	101204.00 LB.IN.SEC**2
PITCH MOMENT OF INERTIA OF SPRUNG MASS =	475638.00 LB.IN.SEC**2
YAW MOMENT OF INERTIA OF SPRUNG MASS =	469434.00 LB.IN.SEC**2
HEIGHT OF SPRUNG MASS CG ABOVE GROUND =	81.30 INCHES
AXLE # 3	

LOAD ON EACH AXLE (LB.)	17500.00
AXLE WEIGHT (LB.)	1500.00
AXLE ROLL M.I (LB.IN.SEC**2)	4100.00
X DIST FROM SP MASS CG (IN)	-123.70
HEIGHT OF AXLE C.G. ABOVE GROUND (INCHES)	19.50
HEIGHT OF ROLL CENTER ABOVE GROUND (INCHES)	29.00
HALF SPRING SPACING (IN)	19.00
HALF TRACK - INNER TIRES (IN)	29.50
DUAL TIRE SPACING (IN)	13.00
STIFFNESS OF EACH TIRE (LB/IN)	4500.00
ROLL STEER COEFFICIENT	0.0
AUX ROLL STIFFNESS (IN.LB/DEG)	10000.00
SPRING COULOMB FRICTION - PER SPRING (LB)	1000.00
VISCOUS DAMPING PER SPRING (LB.SEC/IN)	0.0
SPRING TABLE #	3
CORNERING FORCE TABLE #	1
ALIGNING TORQUE TABLE #	1

Table 44 (continued). Yaw/Roll Simulation Data Echo for the Fully Loaded Double Equipped with the Linked-Articulation Dolly with 0.44 System Gain.

FHWA FIVE-AXLE DOUBLE / 27-FT TRAILERS (LINKED ARTIC GAIN .44 FULL/FULL)

UNIT # 3	

# OF AXLES ON THIS UNIT =	1
WEIGHT OF SPRUNG MASS =	1000.00 LB.
ROLL MOMENT OF INERTIA OF SPRUNG MASS =	1900.00 LB.IN.SEC**2
PITCH MOMENT OF INERTIA OF SPRUNG MASS =	2560.00 LB.IN.SEC**2
YAW MOMENT OF INERTIA OF SPRUNG MASS =	2560.00 LB.IN.SEC**2
HEIGHT OF SPRUNG MASS CG ABOVE GROUND =	44.00 INCHES
AXLE # 4	

LOAD ON EACH AXLE (LB.)	17500.00
AXLE WEIGHT (LB.)	1500.00
AXLE ROLL M.I (LB.IN.SEC**2)	4100.00
X DIST FROM SP MASS CG (IN)	0.0
HEIGHT OF AXLE C.G. ABOVE GROUND (INCHES)	19.50
HEIGHT OF ROLL CENTER ABOVE GROUND (INCHES)	29.00
HALF SPRING SPACING (IN)	19.00
HALF TRACK - INNER TIRES (IN)	29.50
DUAL TIRE SPACING (IN)	13.00
STIFFNESS OF EACH TIRE (LB/IN)	4500.00
ROLL STEER COEFFICIENT	0.0
AUX ROLL STIFFNESS (IN.LB/DEG)	10000.00
SPRING COULOMB FRICTION - PER SPRING (LB)	1000.00
VISCOUS DAMPING PER SPRING (LB.SEC/IN)	0.0
SPRING TABLE #	3
CORNERING FORCE TABLE #	1
ALIGNING TORQUE TABLE #	1

Table 44 (continued). Yaw/Roll Simulation Data Echo for the Fully Loaded Double Equipped with the Linked-Articulation Dolly with 0.44 System Gain.

FHWA FIVE-AXLE DOUBLE / 27-FT TRAILERS (LINKED ARTIC GAIN .44 FULL/FULL)

	UNIT # 4 *****
# OF AXLES ON THIS UNIT =	1
WEIGHT OF SPRUNG MASS =	31000.00 LB.
ROLL MOMENT OF INERTIA OF SPRUNG MASS =	108375.00 LB.IN.SEC**2
PITCH MOMENT OF INERTIA OF SPRUNG MASS =	497375.00 LB.IN.SEC**2
YAW MOMENT OF INERTIA OF SPRUNG MASS =	490000.00 LB.IN.SEC**2
HEIGHT OF SPRUNG MASS CG ABOVE GROUND =	80.70 INCHES
	AXLE # 5 *****
LOAD ON EACH AXLE (LB.)	17500.00
AXLE WEIGHT (LB.)	1500.00
AXLE ROLL M.I (LB.IN.SEC**2)	4100.00
X DIST FROM SP MASS CG (IN)	-127.80
HEIGHT OF AXLE C.G. ABOVE GROUND (INCHES)	19.50
HEIGHT OF ROLL CENTER ABOVE GROUND (INCHES)	29.00
HALF SPRING SPACING (IN)	19.00
HALF TRACK - INNER TIRES (IN)	29.50
DUAL TIRE SPACING (IN)	13.00
STIFFNESS OF EACH TIRE (LB/IN)	4500.00
ROLL STEER COEFFICIENT	0.0
AUX ROLL STIFFNESS (IN.LB/DEG)	10000.00
SPRING COULOMB FRICTION - PER SPRING (LB)	1000.00
VISCOUS DAMPING PER SPRING (LB.SEC/IN)	0.0
SPRING TABLE #	3
CORNERING FORCE TABLE #	1
ALIGNING TORQUE TABLE #	1

Table 44 (continued). Yaw/Roll Simulation Data Echo for the Fully Loaded Double Equipped with the Linked-Articulation Dolly with 0.44 System Gain.

SPRING TABLE # 1

FORCE LB	DEFLECTION INCHES
-------------	----------------------

-20000.00	-20.00
0.0	0.0
8645.00	7.20
25000.00	7.50

SPRING TABLE # 2

FORCE LB	DEFLECTION INCHES
-------------	----------------------

-29800.00	-11.00
0.0	-1.00
0.0	0.0
4650.00	1.00
7650.00	1.50
11650.00	2.00
16300.00	2.50
21600.00	3.00
59500.00	4.00

SPRING TABLE # 3

FORCE LB	DEFLECTION INCHES
-------------	----------------------

-40500.00	-11.00
0.0	-1.50
0.0	0.0
2812.00	0.50
7188.00	1.00
12175.00	1.50
17913.00	2.00
24063.00	2.50
56000.00	3.00

Table 44 (continued). Yaw/Roll Simulation Data Echo for the Fully Loaded Double Equipped with the Linked-Articulation Dolly with 0.44 System Gain.

CORNERING FORCE TABLE # 1

LATERAL FORCE VS. SLIP ANGL

0.0	1.00	2.00	4.00	6.00	12.00
3000.00	540.00	990.00	1710.00	2130.00	2490.00
6000.00	840.00	1500.00	2760.00	3480.00	4140.00
9000.00	990.00	1710.00	3420.00	4680.00	6210.00

ALIGNING TORQUE TABLE # 1

ALIGNING TORQUE VS. SLIP ANGLE

0.0	1.00	3.00	4.00	5.00	7.00	10.00
3000.00	660.00	1104.00	1200.00	1440.00	1500.00	1200.00
6000.00	1560.00	3132.00	3600.00	4248.00	4476.00	3984.00
9000.00	2400.00	5424.00	6396.00	7500.00	7800.00	6780.00

Table 45. Yaw/Roll Simulation Data Echo for the Fully Loaded Double Equipped with the Self-Steering B-Dolly with Full Resistance Steering.

* DIRECTIONAL RESPONSE SIMULATION *

FHWA FIVE-AXLE DOUBLE / 27-FT TRAILERS (SAI FULL/FULL)

# OF SPRUNG MASSES	=	4
TOTAL # OF AXLES	=	5
GROSS VEHICLE WEIGHT	=	80000.00 LB.
FORWARD VELOCITY	=	55.00 M.P.H
PEAK FRICTIONAL COEFFICIENT = 1.00		

	ON UNIT # 1	ON SPRUNG MASS C.G. (INCHES)	DISTANCE AHEAD OF SPRUNG MASS C.G. (INCHES)	HEIGHT BELOW C.G. (INCHES)	ROLL STIFFNESS (IN-LB/DEG)	TYPE OF CONSTRAINT
ARTICULATION PT # 1	0	-87.27	-4.00	999999.88	1	
ON UNIT # 2	138.40	138.40	33.30			
ARTICULATION PT # 2	0	-159.63	37.30	59999.99	1	
ON UNIT # 3	80.00	80.00	0.0			
ARTICULATION PT # 3	0	0.0	-4.00	999999.88	1	
ON UNIT # 4	136.20	136.20	32.70			
LINKED ARTICULATION: GAIN:	0.00	STIFFNESS: 1000000.00 (IN-LB/DEG GAMMA2)				
TYPE OF CONSTRAINT :	O1 CONVENTIONAL 5TH WHEEL O2 INVERTED 5TH WHEEL O3 PINTLE HOOK O4 KING PIN(RIGID IN ROLL & PITCH)					

Table 45 (continued). Yaw/Roll Simulation Data Echo for the Fully Loaded Double Equipped with the Self-Steering B-Dolly with Full Resistance Steering.

FHWA FIVE-AXLE DOUBLE / 27-FT TRAILERS (SA1 FULL/FULL)		
UNIT # 1		

# OF AXLES ON THIS UNIT =	2	
WEIGHT OF SPRUNG MASS =	9700.00 LB.	
ROLL MOMENT OF INERTIA OF SPRUNG MASS =	15000.00 LB.IN.SEC**2	
PITCH MOMENT OF INERTIA OF SPRUNG MASS =	75000.00 LB.IN.SEC**2	
YAW MOMENT OF INERTIA OF SPRUNG MASS =	75000.00 LB.IN.SEC**2	
HEIGHT OF SPRUNG MASS CG ABOVE GROUND =	44.00 INCHES	
AXLE # 1	AXLE # 2	
*****	*****	
LOAD ON EACH AXLE (LB.)	10000.00	17500.00
AXLE WEIGHT (LB.)	1200.00	2300.00
AXLE ROLL M.I (LB.IN.SEC**2)	3719.00	4458.00
X DIST FROM SP MASS CG (IN)	24.00	-96.00
HEIGHT OF AXLE C.G. ABOVE GROUND (INCHES)	19.50	19.50
HEIGHT OF ROLL CENTER ABOVE GROUND (INCHES)	23.00	29.00
HALF SPRING SPACING (IN)	16.00	19.00
HALF TRACK - INNER TIRES (IN)	40.00	29.50
DUAL TIRE SPACING (IN)	0.0	13.00
STIFFNESS OF EACH TIRE (LB/IN)	4500.00	4500.00
ROLL STEER COEFFICIENT	0.0	0.0
AUX ROLL STIFFNESS (IN.LB/DEG)	1500.00	8000.00
SPRING COULOMB FRICTION - PER SPRING (LB)	300.00	1000.00
VISCOUS DAMPING PER SPRING (LB.SEC/IN)	0.0	0.0
SPRING TABLE #	1	2
CORNERING FORCE TABLE #	1	1
ALIGNING TORQUE TABLE #	1	1

Table 45 (continued). Yaw/Roll Simulation Data Echo for the Fully Loaded Double Equipped with the Self-Steering B-Dolly with Full Resistance Steering.

FHWA FIVE-AXLE DOUBLE / 27-FT TRAILERS (SA1 FULL/FULL)

UNIT # 2

OF AXLES ON THIS UNIT = 1

WEIGHT OF SPRUNG MASS = 30300.00 LB.

ROLL MOMENT OF INERTIA OF SPRUNG MASS = 101204.00 LB.IN.SEC**2

PITCH MOMENT OF INERTIA OF SPRUNG MASS = 475638.00 LB.IN.SEC**2

YAW MOMENT OF INERTIA OF SPRUNG MASS = 469434.00 LB.IN.SEC**2

HEIGHT OF SPRUNG MASS CG ABOVE GROUND = 81.30 INCHES

AXLE # 3

LOAD ON EACH AXLE (LB.) 17500.00

AXLE WEIGHT (LB.) 1500.00

AXLE ROLL M.I (LB.IN.SEC**2) 4100.00

X DIST FROM SP MASS CG (IN) -123.70

HEIGHT OF AXLE C.G. ABOVE GROUND (INCHES) 19.50

HEIGHT OF ROLL CENTER ABOVE GROUND (INCHES) 29.00

HALF SPRING SPACING (IN) 19.00

HALF TRACK - INNER TIRES (IN) 29.50

DUAL TIRE SPACING (IN) 13.00

STIFFNESS OF EACH TIRE (LB/IN) 4500.00

ROLL STEER COEFFICIENT 0.0

AUX ROLL STIFFNESS (IN.LB/DEG) 10000.00

SPRING COULOMB FRICTION - PER SPRING (LB) 1000.00

VISCOUS DAMPING PER SPRING (LB.SEC/IN) 0.0

SPRING TABLE # 3

CORNERING FORCE TABLE # 1

ALIGNING TORQUE TABLE # 1

Table 45 (continued). Yaw/Roll Simulation Data Echo for the Fully Loaded Double Equipped with the Self-Steering B-Dolly with Full Resistance Steering.

FHWA FIVE-AXLE DOUBLE / 27-FT TRAILERS (SA1 FULL/FULL)	
UNIT # 3	

# OF AXLES ON THIS UNIT =	1
WEIGHT OF SPRUNG MASS =	1000.00 LB.
ROLL MOMENT OF INERTIA OF SPRUNG MASS =	1900.00 LB.IN.SEC**2
PITCH MOMENT OF INERTIA OF SPRUNG MASS =	2560.00 LB.IN.SEC**2
YAW MOMENT OF INERTIA OF SPRUNG MASS =	2560.00 LB.IN.SEC**2
HEIGHT OF SPRUNG MASS CG ABOVE GROUND =	44.00 INCHES
AXLE # 4	

LOAD ON EACH AXLE (LB.)	17500.00
AXLE WEIGHT (LB.)	1500.00
AXLE ROLL M.I (LB.IN.SEC**2)	4100.00
X DIST FROM SP MASS CG (IN)	0.0
HEIGHT OF AXLE C.G. ABOVE GRDUND (INCHES)	19.50
HEIGHT OF ROLL CENTER ABOVE GROUND (INCHES)	29.00
HALF SPRING SPACING (IN)	19.00
HALF TRACK - INNER TIRES (IN)	29.50
DUAL TIRE SPACING (IN)	13.00
STIFFNESS OF EACH TIRE (LB/IN)	4500.00
ROLL STEER COEFFICIENT	0.0
AUX ROLL STIFFNESS (IN.LB/DEG)	10000.00
SPRING COULOMB FRICTION - PER SPRING (LB)	1000.00
VISCOUS DAMPING PER SPRING (LB.SEC/IN)	0.0
SPRING TABLE #	3
CORNERING FORCE TABLE #	1
ALIGNING TORQUE TABLE #	1

Table 45 (continued). Yaw/Roll Simulation Data Echo for the Fully Loaded Double Equipped with the Self-Steering B-Dolly with Full Resistance Steering.

AXLE 4 IS SELF STEERING

PRIMARY STIFFNESS, IN-LB/DEG: 1000000.00
COULOMB FRICTION, IN-LB: 30000.00
MECHANICAL TRAIL, INCHES: 5.00

STEERING TORQUE AND DISPLACEMENT BOUNDRIES

TORQUE, IN-LB	ANGLE, DEG
-26000.00	-20.000
-6250.00	-0.250
6250.00	0.250
26000.00	20.000

Table 45 (continued). Yaw/Roll Simulation Data Echo for the Fully Loaded Double Equipped with the Self-Steering B-Dolly with Full Resistance Steering.

FHWA FIVE-AXLE DOUBLE / 27-FT TRAILERS (SA1 FULL/FULL)

UNIT # 4

OF AXLES ON THIS UNIT = 1

WEIGHT OF SPRUNG MASS = 31000.00 LB.

ROLL MOMENT OF INERTIA OF SPRUNG MASS = 108375.00 LB.IN.SEC**2

PITCH MOMENT OF INERTIA OF SPRUNG MASS = 497375.00 LB.IN.SEC**2

YAW MOMENT OF INERTIA OF SPRUNG MASS = 490000.00 LB.IN.SEC**2

HEIGHT OF SPRUNG MASS CG ABOVE GROUND = 80.70 INCHES

AXLE # 5

LOAD ON EACH AXLE (LB.) 17500.00

AXLE WEIGHT (LB.) 1500.00

AXLE ROLL M.I (LB.IN.SEC**2) 4100.00

X DIST FROM SP MASS CG (IN) -127.80

HEIGHT OF AXLE C.G. ABOVE GROUND (INCHES) 19.50

HEIGHT OF ROLL CENTER ABOVE GROUND (INCHES) 29.00

HALF SPRING SPACING (IN) 19.00

HALF TRACK - INNER TIRES (IN) 29.50

DUAL TIRE SPACING (IN) 13.00

STIFFNESS OF EACH TIRE (LB/IN) 4500.00

ROLL STEER COEFFICIENT 0.0

AUX ROLL STIFFNESS (IN.LB/DEG) 10000.00

SPRING COULOMB FRICTION - PER SPRING (LB) 1000.00

VISCOS DAMPING PER SPRING (LB.SEC/IN) 0.0

SPRING TABLE # 3

CORNERING FORCE TABLE # 1

ALIGNING TORQUE TABLE # 1

Table 45 (continued). Yaw/Roll Simulation Data Echo for the Fully Loaded Double Equipped with the Self-Steering B-Dolly with Full Resistance Steering.

SPRING TABLE # 1

FORCE LB	DEFLECTION INCHES
-------------	----------------------

-20000.00	-20.00
0.0	0.0
8645.00	7.20
25000.00	7.50

SPRING TABLE # 2

FORCE LB	DEFLECTION INCHES
-------------	----------------------

-29800.00	-11.00
0.0	-1.00
0.0	0.0
4650.00	1.00
7650.00	1.50
11650.00	2.00
16300.00	2.50
21600.00	3.00
59500.00	4.00

SPRING TABLE # 3

FORCE LB	DEFLECTION INCHES
-------------	----------------------

-40500.00	-11.00
0.0	-1.50
0.0	0.0
2812.00	0.50
7188.00	1.00
12175.00	1.50
17913.00	2.00
24063.00	2.50

56000.00	3.00
----------	------

Table 45 (continued). Yaw/Roll Simulation Data Echo for the Fully Loaded Double Equipped with the Self-Steering B-Dolly with Full Resistance Steering.

CORNERING FORCE TABLE # 1

LATERAL FORCE VS. SLIP ANGL

0.0	1.00	2.00	4.00	6.00	12.00
3000.00	540.00	990.00	1710.00	2130.00	2490.00
6000.00	840.00	1500.00	2760.00	3480.00	4140.00
9000.00	990.00	1710.00	3420.00	4680.00	6210.00

ALIGNING TORQUE TABLE # 1

ALIGNING TORQUE VS. SLIP ANGLE

0.0	1.00	3.00	4.00	5.00	7.00	10.00
3000.00	660.00	1104.00	1200.00	1440.00	1500.00	1200.00
6000.00	1560.00	3132.00	3600.00	4248.00	4476.00	3984.00
9000.00	2400.00	5424.00	6396.00	7500.00	7800.00	6780.00

**Table 46. Yaw/Roll Simulation Data Echo for the Fully Loaded Double Equipped
with the Controlled-Steering B-Dolly with 0.30 Steering Gain.**

* DIRECTIONAL RESPONSE SIMULATION *

FHWA FIVE-AXLE DOUBLE / 27-FT TRAILERS (PRO.30 FULL/FULL)

# OF SPRUNG MASSES	=	4
TOTAL # OF AXLES	=	5
GROSS VEHICLE WEIGHT	=	80000.00 LB.
FORWARD VELOCITY	=	55.00 M.P.H
 PEAK FRICTIONAL COEFFICIENT = 1.00		

	DISTANCE AHEAD OF SPRUNG MASS C.G. (INCHES)	HEIGHT BELOW SPRUNG MASS C.G. (INCHES)	ROLL STIFFNESS (IN.LB/DEG)	TYPE OF CONSTRAINT
ARTICULATION PT # 1 ON UNIT # 1	-87.27	-4.00	999999.88	1
ARTICULATION PT # 2 ON UNIT # 2	130.40	33.30		
ARTICULATION PT # 2 ON UNIT # 2	-159.63	37.30	59999.99	1
ARTICULATION PT # 3 ON UNIT # 3	80.00	0.0		
ARTICULATION PT # 3 ON UNIT # 3	0.0	-4.00	999999.88	1
ARTICULATION PT # 4 ON UNIT # 4	136.20	32.70		
LINKED ARTICULATION: GAIN:	0.00	STIFFNESS:	1000000.00 (IN-LB/DEG GAMMA2)	
TYPE OF CONSTRAINT :	O1 CONVENTIONAL 5TH WHEEL O2 INVERTED 5TH WHEEL O3 PINTLE HOOK O4 KING PIN(RIGID IN ROLL & PITCH)			

Table 46 (continued). Yaw/Roll Simulation Data Echo for the Fully Loaded Double Equipped with the Controlled-Steering B-Dolly with 0.30 Steering Gain.

FHWA FIVE-AXLE DOUBLE / 27-FT TRAILERS (PRO.30 FULL/FULL)

FORCED STEER RATIOS

	FRT WHEEL	ARTC # 1	ARTC # 2	ARTC # 3
	*****	*****	*****	*****
AXLE # 2	0.0	0.0	0.0	0.0
AXLE # 3	0.0	0.0	0.0	0.0
AXLE # 4	0.0	0.0	0.0	-0.30
AXLE # 5	0.0	0.0	0.0	0.0

Table 46 (continued). Yaw/Roll Simulation Data Echo for the Fully Loaded Double Equipped with the Controlled-Steering B-Dolly with 0.30 Steering Gain.

FHWA FIVE-AXLE DOUBLE / 27-FT TRAILERS (PRO.30 FULL/FULL)

UNIT # 1

OF AXLES ON THIS UNIT = 2

WEIGHT OF SPRUNG MASS = 9700.00 LB.

ROLL MOMENT OF INERTIA OF SPRUNG MASS = 15000.00 LB.IN.SEC**2

PITCH MOMENT OF INERTIA OF SPRUNG MASS = 75000.00 LB.IN.SEC**2

YAW MOMENT OF INERTIA OF SPRUNG MASS = 75000.00 LB.IN.SEC**2

HEIGHT OF SPRUNG MASS CG ABOVE GROUND = 44.00 INCHES

AXLE # 1 AXLE # 2

***** *****

LOAD ON EACH AXLE (LB.)	10000.00	17500.00
AXLE WEIGHT (LB.)	1200.00	2300.00
AXLE ROLL M.I (LB.IN.SEC**2)	3719.00	4458.00
X DIST FROM SP MASS CG (IN)	24.00	-96.00
HEIGHT OF AXLE C.G. ABOVE GROUND (INCHES)	19.50	19.50
HEIGHT OF ROLL CENTER ABOVE GROUND (INCHES)	23.00	29.00
HALF SPRING SPACING (IN)	16.00	19.00
HALF TRACK - INNER TIRES (IN)	40.00	29.50
DUAL TIRE SPACING (IN)	0.0	13.00
STIFFNESS OF EACH TIRE (LB/IN)	4500.00	4500.00
ROLL STEER COEFFICIENT	0.0	0.0
AUX ROLL STIFFNESS (IN.LB/DEG)	1500.00	8000.00
SPRING COULOMB FRICTION - PER SPRING (LB)	300.00	1000.00
VISCOUS DAMPING PER SPRING (LB.SEC/IN)	0.0	0.0
SPRING TABLE #	1	2
CORNERING FORCE TABLE #	1	1
ALIGNING TORQUE TABLE #	1	1

Table 46 (continued). Yaw/Roll Simulation Data Echo for the Fully Loaded Double Equipped with the Controlled-Steering B-Dolly with 0.30 Steering Gain.

FHWA FIVE-AXLE DOUBLE / 27-FT TRAILERS (PRO.30 FULL/FULL)	
UNIT # 2	

# OF AXLES ON THIS UNIT =	1
WEIGHT OF SPRUNG MASS =	30300.00 LB.
ROLL MOMENT OF INERTIA OF SPRUNG MASS =	101204.00 LB.IN.SEC**2
PITCH MOMENT OF INERTIA OF SPRUNG MASS =	475638.00 LB.IN.SEC**2
YAW MOMENT OF INERTIA OF SPRUNG MASS =	469434.00 LB.IN.SEC**2
HEIGHT OF SPRUNG MASS CG ABOVE GROUND =	81.30 INCHES
AXLE # 3	

LOAD ON EACH AXLE (LB.)	17500.00
AXLE WEIGHT (LB.)	1500.00
AXLE ROLL M.I (LB.IN.SEC**2)	4100.00
X DIST FROM SP MASS CG (IN)	-123.70
HEIGHT OF AXLE C.G. ABOVE GROUND (INCHES)	19.50
HEIGHT OF ROLL CENTER ABOVE GROUND (INCHES)	29.00
HALF SPRING SPACING (IN)	19.00
HALF TRACK - INNER TIRES (IN)	29.50
DUAL TIRE SPACING (IN)	13.00
STIFFNESS OF EACH TIRE (LB/IN)	4500.00
ROLL STEER COEFFICIENT	0.0
AUX ROLL STIFFNESS (IN.LB/DEG)	10000.00
SPRING COULOMB FRICTION - PER SPRING (LB)	1000.00
VISCOUS DAMPING PER SPRING (LB.SEC/IN)	0.0
SPRING TABLE #	3
CORNERING FORCE TABLE #	1
ALIGNING TORQUE TABLE #	1

Table 46 (continued). Yaw/Roll Simulation Data Echo for the Fully Loaded Double Equipped with the Controlled-Steering B-Dolly with 0.30 Steering Gain.

FHWA FIVE-AXLE DOUBLE / 27-FT TRAILERS (PRO.30 FULL/FULL)	
UNIT # 3	

# OF AXLES ON THIS UNIT =	1
WEIGHT OF SPRUNG MASS =	1000.00 LB.
ROLL MOMENT OF INERTIA OF SPRUNG MASS =	1900.00 LB.IN.SEC**2
PITCH MOMENT OF INERTIA OF SPRUNG MASS =	2560.00 LB.IN.SEC**2
YAW MOMENT OF INERTIA OF SPRUNG MASS =	2560.00 LB.IN.SEC**2
HEIGHT OF SPRUNG MASS CG ABOVE GROUND =	44.00 INCHES
AXLE # 4	

LOAD ON EACH AXLE (LB.)	17500.00
AXLE WEIGHT (LB.)	1500.00
AXLE ROLL M.I (LB.IN.SEC**2)	4100.00
X DIST FROM SP MASS CG (IN)	0.0
HEIGHT OF AXLE C.G. ABOVE GROUND (INCHES)	19.50
HEIGHT OF ROLL CENTER ABOVE GROUND (INCHES)	29.00
HALF SPRING SPACING (IN)	19.00
HALF TRACK - INNER TIRES (IN)	29.50
DUAL TIRE SPACING (IN)	13.00
STIFFNESS OF EACH TIRE (LB/IN)	4500.00
ROLL STEER COEFFICIENT	0.0
AUX ROLL STIFFNESS (IN.LB/DEG)	10000.00
SPRING COULOMB FRICTION - PER SPRING (LB)	1000.00
VISCOUS DAMPING PER SPRING (LB.SEC/IN)	0.0
SPRING TABLE #	3
CORNERING FORCE TABLE #	1
ALIGNING TORQUE TABLE #	1

Table 46 (continued). Yaw/Roll Simulation Data Echo for the Fully Loaded Double Equipped with the Controlled-Steering B-Dolly with 0.30 Steering Gain.

FHWA FIVE-AXLE DOUBLE / 27-FT TRAILERS (PRO.30 FULL/FULL)

UNIT # 4

OF AXLES ON THIS UNIT = 1

WEIGHT OF SPRUNG MASS = 31000.00 LB.

ROLL MOMENT OF INERTIA OF SPRUNG MASS = 108375.00 LB.IN.SEC**2

PITCH MOMENT OF INERTIA OF SPRUNG MASS = 497375.00 LB.IN.SEC**2

YAW MOMENT OF INERTIA OF SPRUNG MASS = 490000.00 LB.IN.SEC**2

HEIGHT OF SPRUNG MASS CG ABOVE GROUND = 80.70 INCHES

AXLE # 5

LOAD ON EACH AXLE (LB.) 17500.00

AXLE WEIGHT (LB.) 1500.00

AXLE ROLL M.I (LB.IN.SEC**2) 4100.00

X DIST FROM SP MASS CG (IN) -127.80

HEIGHT OF AXLE C.G. ABOVE GROUND (INCHES) 19.50

HEIGHT OF ROLL CENTER ABOVE GROUND (INCHES) 29.00

HALF SPRING SPACING (IN) 19.00

HALF TRACK - INNER TIRES (IN) 29.50

DUAL TIRE SPACING (IN) 13.00

STIFFNESS OF EACH TIRE (LB/IN) 4500.00

ROLL STEER COEFFICIENT 0.0

AUX ROLL STIFFNESS (IN.LB/DEG) 10000.00

SPRING COULOMB FRICTION - PER SPRING (LB) 1000.00

VISCOUS DAMPING PER SPRING (LB.SEC/IN) 0.0

SPRING TABLE # 3

CORNERING FORCE TABLE # 1

ALIGNING TORQUE TABLE # 1

Table 46 (continued). Yaw/Roll Simulation Data Echo for the Fully Loaded Double Equipped with the Controlled-Steering B-Dolly with 0.30 Steering Gain.

SPRING TABLE # 1

FORCE LB	DEFLECTION INCHES
-------------	----------------------

-20000.00	-20.00
-----------	--------

0.0	0.0
-----	-----

8645.00	7.20
---------	------

25000.00	7.50
----------	------

SPRING TABLE # 2

FORCE LB	DEFLECTION INCHES
-------------	----------------------

-29800.00	-11.00
-----------	--------

0.0	-1.00
-----	-------

0.0	0.0
-----	-----

4650.00	1.00
---------	------

7650.00	1.50
---------	------

11650.00	2.00
----------	------

16300.00	2.50
----------	------

21600.00	3.00
----------	------

59500.00	4.00
----------	------

SPRING TABLE # 3

FORCE LB	DEFLECTION INCHES
-------------	----------------------

-40500.00	-11.00
-----------	--------

0.0	-1.50
-----	-------

0.0	0.0
-----	-----

2812.00	0.50
---------	------

7188.00	1.00
---------	------

12175.00	1.50
----------	------

17913.00	2.00
----------	------

24063.00	2.50
----------	------

56000.00	3.00
----------	------

Table 46 (continued). Yaw/Roll Simulation Data Echo for the Fully Loaded Double Equipped with the Controlled-Steering B-Dolly with 0.30 Steering Gain.

CORNERING FORCE TABLE # 1

LATERAL FORCE VS. SLIP ANGLL

0.0	1.00	2.00	4.00	6.00	12.00
3000.00	540.00	990.00	1710.00	2130.00	2490.00
6000.00	840.00	1500.00	2760.00	3480.00	4140.00
9000.00	990.00	1710.00	3420.00	4680.00	6210.00

ALIGNING TORQUE TABLE # 1

ALIGNING TORQUE VS. SLIP ANGLE

0.0	1.00	3.00	4.00	5.00	7.00	10.00
3000.00	660.00	1104.00	1200.00	1440.00	1500.00	1200.00
6000.00	1560.00	3132.00	3600.00	4248.00	4476.00	3984.00
9000.00	2400.00	5424.00	6396.00	7500.00	7800.00	6780.00

Appendix B

Listings of Equations and Variables Used in the Financial Model

This appendix contains a listing of the rules (equations) and variables used to compute the results given in the tables of incremental costs and/or benefits in Section 5.2. The input variables to the model are displayed in Table 47, with the reference values of the variables shown on the right. Where the value of the input variable is calculated from other input variables, the equation is shown. A key to the input variables appears in Table 48, with a short explanation of each variable name. Table 49 displays a list which indicates the change in cost/benefit values between A and B dollies that are being computed in each row of the model. These equations are shown in Table 50 through Table 53. Different sets of equations were used for calculating the cost/benefit values in different years due to the periodic nature of some of the variables associated with the use of the B-dolly as opposed to the use of the A-dolly. For example, A-dollies require a major overhaul every four years, whereas B-dollies require one every two years. The relationships between these input variables and the resulting cost/benefit values were discussed in the The Financial Model section. Table 50 displays the equations used for computing values for Year 0 (the first year of the project). Table 51 displays the equations used in Years 1, 5, and 9. The equations in Table 52 were used in computing the cost/benefit values for Years 2, 4, 6, and 8. Table 53 displays the equations used for the Years 3 and 7.

The financial model was implemented using the Microsoft spreadsheet program "Excel" on an Apple Macintosh computer.

Table 47. Variables Used in the Operational Impacts Study.

Variables	Reference Case Values
PER GROSS OUT GROSSED OUT	0.6 TRUE
DOLLY WEIGHT	1000
MILES PER YEAR	100000
COST/LB MILE	0.0000894
BLADDED DOLLIES OWNED	6
DOLLIES OWNED =B_BLADDED*DOLLIES OWNED	15
B PERCENT	100000
MILES/PER TIRE	0.15
PER TIRE WEAR	0.2
PER COST/OVERTIME	500
PREV MAINTENANCE	TRUE
BACKUP	1
BREAK UPS	0.008
ACC SAVE/PER MILE	0.008
INTEREST RATE	0.1
SCHEDULING BASE	0
SCHEDULING CURVE BASE	1000 =(SCHEDULING_CURVE_BASE*(1-2*ABS(0.5-B_PERCENT)))/EXP(-1)
TRAINING BASE	1000 =TRAINING_BASE/EXP(-1)
SCHEDULING CURVE TRAINING CURVE	1000 =TRAINING_CURVE/EXP(-1)
LOCALS	TRUE
LOCAL DROPS	500
ALLOW OVER WEIGHT	FALSE
OVER WEIGHT YEAR	0 1 -IF(MILES_PER_YEAR+0>=MILES_PER_TIRE_MILES_PER_YEAR-MILES_PER_TIRE_MILES_PER_YEAR,0,MILES_PER_TIRE_MILES_PER_YEAR)
TIRE MILES LEFT	

Table 48. Key to the Variables Used in the Operational Impacts Study.

Variables	Explanation
PER GROSS	Percentage of trips made at GVW
GROSSED OUT	True or False : Are vehicles with B-dollies operating at GVW?
DOLLY WEIGHT	Additional weight of B-dolly over A-dolly
MILES PER YEAR	Miles traveled per year by vehicle
COST LB MILE	Price charged by trucking company to haul freight (price per lb per mile)
B ADDED	Number of B-dollies added to the fleet
DOLLIES OWNED	Total number of A and B dollies owned
B PERCENT	Percentage of B-dollies in the fleet
MILES PER TIRE	Number of miles a set of tires will run before replacement
PER TIRE WEAR	Percent increase in the wear by B-dollies over A-dollies
PER COST OVERHAUL	Percent increase in the cost of a major over haul for B-dollies over A-dollies
PREV MAINTENANCE	Increase in the cost of preventive maintenance for B-dollies over A-dollies
BACKUP	True or False : Will the vehicles with B-dollies be backed up?
BREAK UPS	Number of times the unit is backed up per day
ACC SAVE PER MILE	Accident saving per dolly per mile traveled
INTEREST RATE	Discount Rate after taxes
SCHEDULING BASE	One time cost of updating computer programs used in scheduling
SCHEDULING CURVE BASE	Variable used in calculating scheduling learning curve
TRAINING BASE	Variable used in calculating training learning curve
SCHEDULING CURVE	Equation to determine coefficient for scheduling Learning Curve
TRAINING CURVE	Equation to determine coefficient for training Learning Curve
LOCALS	True or False : Are vehicles with B-dollies allowed on secondary roads to make deliveries?
LOCAL DROPS	Number of local deliveries made per year
ALLOW OVER WEIGHT	True or False : Are vehicles with B-dollies allowed a higher GVW to account for the additional weight of the dolly?
OVER WEIGHT	Amount of additional weight vehicles with B-dollies are allowed to carry
YEAR	Variable that indicates the year of the project - one entry for each year
TIRE MILES LEFT	Variable that indicates the number of miles left until replacement on the current sets of tires - one entry for each year

Table 49. Economic Issues Considered in the Operational Impacts Study.

Δ costs/benefits between A and B dollies
Initial cost of dollies
Converting existing equipment
Major overhauls
Tire wear
Preventive maintenance
Scheduling
Training
Ability to back up
Less weight hauled
Fewer accidents
Ability to operate on secondary roads
Allow higher GVW
Total
Net Present Value
Cost increase to cover loss /1000 lb/mile
Change in operating cost/dolly/mile

-B ADDDED,3000	-500,B ADDDED,IR(BACKUP,INT(BRAKE, UPS,B ADDDED/60),15000,0)	-INT(0) ADDDED,MILES PER YEAR,MILES PER TIRE,900,PER TIRE_WEAR	-PREV MAINTENANCE,B ADDDED,MILES PER YEAR,B ADDDED,BREAK UPS,T200M	-IF(BACKUP,B ADDDED,BREAK UPS,T200M)	-IF(ANNUALMILES >0,TRAINING CURVE,B ADDDED,EXTR-YEAR),0	-MILES PER YEAR,B ADDDED,ACC SAVE PER MILE	-IF(ANNUALMILES >0,OVER WEIGHT,GROSSED OUT,COST_LB_MILE,B ADDDED,BOLLY_WEIGHT,MILES_PER_YEAR,PER_GROSS,0)	-IF(ULOCAL DRIVERS,B ADDDED,0)	-IRANANDGROSSED OUTALLOW OVER WEIGHT,DOLLY_WEIGHT,COST_LB_MILE,MILES PER YEAR,B ADDDED,PER_GROSS,0)	-SMOOTH,0)	-IN(VIN)PRESENT KATEESTNS,D15	-IN(VIN)PRESENT VALUE(0),IN(VIN)DOLLIES OWNED,0,(B ADDDED,0),SCIDEULNG BASE,0),(100,B ADDDED,MILES PER YEAR)	-IN(VIN)PRESENT VALUE(0),IN(VIN)PRESENT VALUE(0)/PER_GROSS,30000,(PER_GROSS,25000,MILES PER YEAR),100,0)	-NET PRESENT VALUE(0),IN(VIN)ADDED,(PER_GROSS,30000,(PER_GROSS,25000,MILES PER YEAR))100,0)
----------------	--	--	--	--------------------------------------	---	--	---	--------------------------------	---	------------	-------------------------------	--	--	---

Table 50. Equations Used for the Year Zero in the Operational Impacts Study.

Table 51. Equations Used for Years One, Five and Nine in the Operational Impacts Study.

Year 1
<pre> -0 -IF(BACKUP,INT(BREAK_UPS*B_ADDED/60)*15000,0) -PER COST OVERHAUL,7225*B_ADDED -INT((B_ADDED*MILES_PER_YEAR*TIRE_MILES_LEFT)/MILES_PER_TIRE)*900*PER_TIRE_WEAR -PREV MAINTENANCE*B_ADDED -SCHEDULING_CURVE*EXP(-YEAR) -IF(B_ADDED>0,TRAINING_CURVE*B_ADDED*EXP(-YEAR),0) -IF(BACKUP,B_ADDED*BREAK_UPS*7260,0) -IF(AND(NOT(ALLOW_OVER_WEIGHT),GROSSED_OUT),COST_LB_MILE*B_ADDED*DOLLY_WEIGHT*MILES_PER_YEAR*PER_GROSS,0) -MILES_PER_YEAR*B_ADDED*ACC_SAVE_PER_MILE -IF(LOCALS30*LOCAL_DROPS*B_ADDED,0) -IF(AND(GROSSED_OUT,ALLOW_OVER_WEIGHT),(OVER_WEIGHT*DOLLY_WEIGHT)*COST_LB_MILE*MILES_PER_YEAR*B_ADDED*PER_GROSS,0) -SUM(E1:E14) </pre>

Table 52. Equations Used for Years Two, Four, Six and Eight in the Operational Impacts Study.

Year2
<pre> =0 =IF(BACKUP,INT(BREAK_UPS*B_ADDED/60)*15000,0) =0 =INT((B_ADDED*MILES_PER_YEAR*TIRE_MILES_LEFT)/MILES_PER_TIRE)*900*PER_TIRE_WEAR =PREV_MAINTENANCE*B_ADDED =SCHEDULING_CURVE*EXP(-YEAR) =IF(B_ADDED>0,TRAINING_CURVE*B_ADDED*EXP(-YEAR),0) =IF(BACKUP,B_ADDED*BREAK_UPS*7260,0) =IF(AND(NOT(ALLOW_OVER_WEIGHT),GROSSED_OUT),COST_LB_MILE*B_ADDED*DOLLY_WEIGHT*MILES_PER_YEAR*PER_GROSS,0) =MILES_PER_YEAR*B_ADDED*ACC_SAVE_PER_MILE =IF(LOCALS_30*LOCAL_DROPS*B_ADDED,0) =IF(AND(GROSSED_OUT,ALLOW_OVER_WEIGHT),(OVER_WEIGHT-DOLLY_WEIGHT)*COST_LB_MILE*MILES_PER_YEAR*B_ADDED*PER_GROSS,0) =SUM(F3:F14) </pre>

Table 53. Equations Used for Years Three and Seven in the Operational Impacts Study.

Year 3
$=0$ $=\text{IF}(BACKUP1 \neq \text{BREAK_UPS}, \text{ADDED}(\text{GO} * 15000)$ $= \text{PER_COST_OVERHAUL} * 725 \text{ PER_COST_OVERHAUL}, 3000)$ B_ADDED $=\text{INT}((\text{B_ADDED_MILES} \text{ PER_YEAR} * \text{TIRE_MILES_LEFT}) / \text{MILES_PER_TIRE}) * 900 \text{ PER_TIRE_WEAR}$ $=\text{PREV_MAINTENANCE} \text{ B_ADDED}$ $=\text{SCHEDULING_CURVE} \text{ (EXY_YEAR)}$ $=\text{IF}(\text{B_ADDED} > \text{TRAINING_CURVE}, \text{B_ADDED} * \text{EXY_YEAR}), 0)$ $=\text{IF}(BACKUP1 \neq \text{BREAK_UPS}, \text{PT2600})$ $=\text{IF}(\text{AND}(\text{NOT}(\text{ALLOW_OVER_WEIGHT}), \text{GROSSED_OUT}), \text{COST_LB_MILE} * \text{B_ADDED} * \text{DOLLY_WEIGHT} * \text{MILES_PER_YEAR} \text{ PER_GROSS}, 0)$ $=\text{MILES_PER_YEAR} * \text{B_ADDED} * \text{ACC_SAVE_PER_MILE}$ $=\text{IF}(\text{LOCAL_MILES} > 0, \text{LOCAL_DROPS} * \text{B_ADDED}, 0)$ $=\text{IF}(\text{AND}(\text{GROSSED_OUT}, \text{ALLOW_OVER_WEIGHT}), \text{DOLLY_WEIGHT} * \text{COST_LB_MILE} * \text{MILES_PER_YEAR} * \text{B_ADDED} * \text{PER_GROSS}, 0)$ $=\text{SUM}(\text{G14})$

