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An Investigation into the Possibility of Developing Straight Line Time Trends Based on Basal Area To Aid in Determining Costs in the Logging Industry

Prepared by
Barclay Keith Bowman

This paper is respectfully submitted in partial fulfillment of the requirements for the degree of Master of Forestry from the School of Forestry end Conservation, University of Michigan


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In this writing, basal area of diameter breast high has been used as the basis of determining the time necessary to complete the various operations in converting standing timber to rough lumber. It is hoped that the basal area concept as a means of determining costs will prove satisfactory. Since a certain amount of work is necessary to sever the wood fibers of any specified crosssectional area of any particular species, it is conceivable that some unit of this area, i.e. basal area in square feet would be a logical approach to cost analysis. This theory was originally advanced by the late Professor D. M. Matthews and in response to his request these additional investigations have been made.

It is a well known fact that basal area as a measurement of timber is relatively new and is not in use by the logging industry. This paper shall endeavor to present an acceptable method of converting basal area to volume in terms of the Scribner and Doyle log rules for mature northern hardwoods in Iron County, Michigan, or any similar area. A volume table for this forest type and area is also developed and presented here.

Quadratic equations and curves act as barriers in attempting to get new ideas accepted, therefore, here an attempt is made to develop straight line trends.

Naturally this gives linear equations which are more easily presented. It follows that constant variation from size class to size class could be given with the time required at some specific diameter. This rule of thumb, if you will, would be usable by the layman in the woods; therefore, if such trends can be developed for various species and areas, a new operator in an area would have some basis for estimating probable costs on a contemplated operation.

I would like to acknowledge the aid given me in the preparation of this paper. The late Professor D. M. Matthews stimulated my original interest and provided me with the original time studies used in this report. Data collected by the students of the Forestry school on northern hardwood species was used to make the form class volume table. Cruise data from Gogebic County, Michigan, by Mr. Frank Murray was used to make the stand tables. Many stimulating discussions and suggestions were received from Mr. George Banzaf, Mr. Thomas Hellings and Mr. John Carow.

Barclay K. Bowman
Ann Arbor, Michigan
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To conduct any time or cost study, suitable volume and stand tables must be available. After doing some searching for applicable tables, it was decided to construct originals for use in this investigation. The accuracy of these tables can be no better than the original data; therefore, it was necessary to locate reliable data.

## Volume Table Construction

The volume table was constructed from data collected by the students of the School of Forestry and Conservation at summer camp in 1947. The original measurements were made on felled hardwood trees in the vicinity of Camp Filibert Roth, Iron County, Michigan. Diameter outside bark at 4.5 feet from the ground was taken as diameter breast height. The scaling diameter of each 16 foot $\log$ of each tree was recorded. All diameters were measured to the nearest 0.1 inch on each of the 70 trees used. This data was then sorted into 3 broad diameter groups. The breakdown was by 12 to 16 inch diameter class inclusive, 18 to 22 inch inclusive, and 24 to 28 inch inclusive.

After sorting this data, the taper of each log was determined and these tapers, to the nearest 0.1 inch were averaged for each log, i.e. first log, 2nd. log, etc. by
group breakdown. The form class of any tree is found by multiplying the quotient of the top diameter inside bark divided by the diameter breast height outside bark by 100. To ascertain the form class for each group the form class of each individual tree was calculated and the average for each group determined. These figures were entered into Table 1 and were used to determine the top diameters inside bark and volumes in both the Scribner and Doyle log rules. The volumes in Scribner were read from the volume table page 408 in Forest Mensuration by Bruce and Schumacher, and those in the Doyle rule were calculated by the formula for that rule.

These volumes were then plotted over tree lengths in 16 foot logs. From the curves fitted to these points the volumes could be read by 0.5 log lengths and plotted over the diameters breast height. The results of this plotting is shown in Figures $1,2,3$ and 4. It was from the graphs in Figures 3 and 4 that the volumes for the volume tables were read. Upon checking the aggregate difference of these tables it was found that the Scribner volume table was $2.9 \%$ higher than that of the actual volumes and 1.28\% low in the Doyle table. Appendix A includes these volume tables.

Mr. Frank Murray provided the basic data for the construction of the stand table. Cruise sheets from Gogebic County, Michigan, were used in the development of the stand and stock tables in appendix B. These tables include not only the diameter breast height, number of trees per acre, basal area per acre and volumes in both Scribner and Doyle, but the board feet per square foot of basal area.

The total number of trees tallied were of two classes, some were in the form of a cruise of about $10 \%$ of the residual stand and the others were a $100 \%$ cruise of the trees which had been marked for cutting. The various totals by diameter classes and log lengths were multiplied by the appropriate factor and these figures in turn added to the totals of the trees marked for cutting. These totals divided by the number of acres in the area concerned provided the figures in the column-Number of trees per acre. The number of trees per acre times the basal area per tree gave the basal area per acre and the number of trees multiplied by the average volume per tree, which was determined by using the previously prepared volume table, gave the volume per acre.

In that the time basis used later in this study is man minutes per square foot of basal area, it is necessary to know the volume per square foot of basal area so that a
conversion may be made from basal area to board feet. This figure was obtained by dividing the volume per class by the corresponding basal area.

Table 1
Compilation of Data for Making Northern Hardwood Volume Tables

| D.B.H. Class | $\begin{aligned} & \text { D.B.H. } \\ & \text { Used } \end{aligned}$ | $\begin{aligned} & A D . \\ & F \cdot C . \end{aligned}$ |  | Merchantable Helght in 16-foot Logs |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | 1 | $1{ }^{1} \frac{1}{2}$ | 2 | $2 \frac{1}{2}$ | 3 | 3 ${ }^{\frac{1}{2}}$ | 4 |
|  |  |  |  | $\log$ | 10 g | $\log$ | 10 g | 10 g | $\log$ | $\log$ |
| 12-16 | 14 | 78.0 | Taper |  | 0.8 | 0.8 | 0.9 | 0.9 |  |  |
|  |  |  | Top dib. | 10.9 | 10.1 | 9.3 | 8.4 | 7.5 |  |  |
|  |  |  | Vol.Scrib. | 6.8 | 93 | 114 | 129 | 139 |  |  |
|  |  |  | Vol. Doyle | 48 | 67 | 76 | 86 | 88 |  |  |
| 18-22 | 20 | 78.1 | Taper |  | 0.9 | 0.9 | 1.0 | 1.1 | 1.2 | 1.2 |
|  |  |  | Top dib. | 15.6 | 14.7 | 13.8 | 12.1 | 11.7 | 10.5 | 9.3 |
|  |  |  | Vol.Scrib. | 157 | 222 | 276 | 325 | 362 | 390 | 409 |
|  |  |  | Vol.Doyle | 135 | 192 | 231 | 264 | 290 | 311 | 318 |
| 24-28 | 26 | 78.6 | Taper |  | 1.0 | 1.0 | 1.3 | 1.4 | 1.4 | 1.5 |
|  |  |  | Top dib. | 20.4 | 19.4 | 18.4 | 17.1 | 15.7 | 14.3 | 12.8 |
|  |  |  | Vol.Scrib. | 284 | 404 | 511 | 600 | 670 | 727 | 770 |
|  |  |  | Vol. Doyle | 279 | 398 | 487 | 573 | 624 | 677 | 701 |



Volume Curves Doyle




## Chapter 2

It is well known that basal area as a unit of measurement is not in use in the field. To date so many square feet of basal area is used in the laboratory or research office only. In that in this study the time required to perform the various operations of logging and milling is in terms of man-minutes per square foot of basal area, it is necessary to devise some means of converting basal area to board foot volume. Without a way of making this conversion such a study would be of use only to the technically trained man and of no use to the untrained operator who this is intended to help.

In order to develop a method of making this conversion it was necessary to construct the stand and stock tables referred to in the preceding chapter. The basal areas and volumes were totaled for all species by diameter classes. This gives weighted totals which in turn gives proper weights to each species. The total basal area was then divided into the total volume which gave a volume per square foot of basal area figure. Upon plotting these volume figures over diameter breast height a definite trend could be seen. Figures 5 and 6.

These trends seemed to be straight lines, therefore an attempt was made to fit straight lines to the data. The data carried sufficient weight from the 10 inch to the 24 inch class. For the Doyle rule one straight line fit
the diameter range of 10 to 21 inches well. From the 20 inch class up there seems to be a smaller increase in volume per square foot of basal area which was fitted with one straight line. The data from 30 to 36 inches was very erratic and light so no fact can be drawn from this range.

When the Scribner volumes were plotted it was noted they run relatively higher than the Doyle values with a tendency to come together. about the 30 inch-0less. The initial rate of rather fast increase in volume appears to taper off at about the 18 inch class. At this point the Scribner rule levels off more than does the Doyle rule at the 21 inch class so that they cross at about the 30 inch class.

Even though these graphs are easily readable, it seems advantageous to state the conversion factors in terms of linear equations. To do this it was necessary to determine the slope of the line which is the rise divided by the horizontal run. The volume intercepts of the trend lines were read off and both of these figures substituted in the general formula of a straight line which is $y=a x+c$. In this formula we let $y=V=$ volume, $a=$ the slope of the trend, $x=$ the diameter breast height, and $c=$ the intercept on the volume axis. Rewriting the formula using symbols suitable to forestry, we get the equation $V$. $(\mathrm{a} \times \mathrm{DBH})+\mathrm{c}$.

The graphs and formula for the trend lines developed
here are given in Appendix 0 .
To check the soundness of these trend lines a series of calculations are in order. Using the stand table for hard maple in Appendix $B$ as a source for the basal area per acre and the volumes as read from the trend lines just developed the following computations are made. First using the Doyle values for sugar maple we have:

| 0.90 | x | 31.2 | $=$ | 28.08 |
| :---: | :---: | :---: | :---: | :---: |
| 2.85 | X | 44.5 | = | 127.27 |
| 4.42 | x | 57.5 | $=$ | 254.15 |
| 5.66 | x | 70.5 | $=$ | 399.03 |
| 6.23 | x | 83.5 | $=$ | 521.27 |
| 4.40 | x | 96.7 | $=$ | 425.48 |
| 2.86 | x | 104.7 | - | 299.44 |
| 2.42 | x | 107.5 | = | 260.15 |
| 0.63 | x | 110.2 | = | 69.33 |
| 0.38 | x | 113.0 | = | 42.94 |
| 0.05 | x | 115.8 | = | 5.79 |

Volume 10-30 inch classes from stand table 2502.54 Volume 10-30 inch classes from above table $\frac{2427.93}{74.61}$

This is 2.98\% low.
Now using the Scribner values we have:

| 0.90 | x | 62.2 | $=$ | 55.98 |
| ---: | ---: | ---: | ---: | ---: |
| 2.86 | x | 74.0 | $=$ | 211.64 |
| 4.42 | x | 85.6 | $=$ | 378.35 |
| 5.66 | x | 97.5 | $=$ | 551.85 |
| 6.23 | x | 109.2 | $=$ | 680.32 |
| 4.40 | x | 110.3 | $=$ | 485.32 |
| 2.86 | x | 111.7 | $=$ | 319.46 |
| 2.42 | x | 113.1 | $=$ | 273.70 |
| 0.63 | x | 114.5 | $=$ | 72.14 |
| 0.38 | x | 115.9 | $=$ | 44.04 |
| 0.05 | x | 117.3 | $=$ | 5.87 |

Volume 10-30 inch classes from stand table 3278.97 Volume 10-30 inch classes from above table $\frac{3078.67}{200.30}$ This is $6.11 \%$ low.

Now using the stand table for yellow birch and the volume per square foot basal area values for the Scribner rule we have:

| 1.04 | x | 62.2 | $=$ | 64.69 |
| ---: | ---: | ---: | :--- | ---: |
| 1.81 | x | 74.0 | $=$ | 113.94 |
| 3.23 | x | 85.6 | $=$ | 276.49 |
| 3.74 | x | 97.5 | $=$ | 364.65 |
| 4.24 | x | 109.2 | $=$ | 463.01 |
| 4.14 | x | 110.3 | $=$ | 456.64 |
| 3.02 | x | 111.7 | $=$ | 337.33 |
| 4.20 | x | 113.1 | $=$ | 475.02 |
| 1.37 | x | 114.5 | $=$ | 156.87 |
| 1.11 | x | 115.9 | $=$ | 128.65 |
| 1.08 | x | 117.3 | $=$ | 126.68 |
|  |  |  |  | 2983.97 |

Volume 10-30 inch classes from stand table 2724.80 Volume 10-30 inch classes,ambove table $\frac{2983.97}{259.17}$
This is $9.51 \%$ high.
Now using thesstand table for yellow birch and the volume per square foot basal are values for the Doyle rule we have:

| 1.04 | x | 31.2 | $=$ | 32.45 |
| ---: | :--- | ---: | :--- | ---: |
| 1.81 | x | 44.5 | $=$ | 82.55 |
| 3.23 | x | 57.5 | $=$ | 185.73 |
| 3.74 | x | 70.5 | $=$ | 263.67 |
| 4.24 | x | 83.5 | $=$ | 354.04 |
| 4.14 | x | 96.7 | $=$ | 400.34 |
| 3.02 | x | 104.7 | $=$ | 316.19 |
| 4.20 | x | 107.5 | $=$ | 451.50 |
| 1.37 | x | 110.2 | $=$ |  |
| 1.11 | x | 113.0 | $=$ |  |
| 1.08 | x | 115.8 | $=\frac{125.97}{2487.06}$ |  |

Volume 10-30 inch classes from stand table 2295.00 Volume 10-30 inch classes from above table 2487.93

This is 8.38\% high.

If the basswood stand table is used, the volume by the Doyle rule will be:

| 0.10 | x | 31.2 | $=$ | 3.12 |
| ---: | :--- | ---: | :--- | ---: |
| 0.31 | x | 44.5 | $=$ | 13.80 |
| 0.21 | x | 57.5 | $=$ | 12.08 |
| 0.42 | x | 70.5 | $=$ | 29.61 |
| 0.55 | x | 83.5 | $=$ | 10.93 |
| 0.11 | x | 96.7 | $=$ | 32.46 |
| 0.31 | x | 104.7 | $=$ | 7.71 |
| 0.53 | x | 107.5 | $=$ | 46.98 |
| 0.07 | x | 110.2 | $=$ | 5.79 |
| 0.04 | x | 113.0 | $=$ | 224.64 |

Volume 10-30 inch classes from stand table 273.50 Volume 10-30 inch classes from above table
$\frac{224.64}{48.86}$
This is $17.9 \%$ low.
Now using the Scribner rule we have:

| 0.10 | x | 62.2 | 6.22 |
| :---: | :---: | :---: | :---: |
| 0.31 | x | 74.0 | 23.94 |
| 0.21 | x | 85.6 | 17.98 |
| 0.42 | x | 97.5 | 40.95 |
| 0.55 | x | 109.2 | 60.06 |
| 0.11 | x | 110.3 | 12.13 |
| 0.31 | x | 111.7 | 34.63 |
| 0.53 | x | 113.1 | 59.94 |
| 0.07 | x | 114.5 | 8.02 |
| 0.04 | x | 115.9 | 4.64 |
| 0.05 | x | 117.3 | 5.87 |
|  |  |  | 274.48 |

Volume 10-30 inch classes from stand table 335.10 Volume 10-30 inch classes from above table $\frac{274.48}{60.62}$ This is 18.1\% low.

As will be noticed in the foregoing calculations there is considerable error in any oner ${ }^{\text {Species }}$ in that the original conversion of these should have been done as one calculation. Therefore if we consolidate the previous work we will get the following result.

| Species | Scribner |  | Doyle |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Stand Table | Conversion | Stand Table | Conversion |
| Hard Maple | 3278.97 | 3078.67 | 2502.54 | 2427.93 |
| Yellow Birch | 2724.80 | 2983.97 | 2295.00 | 2487.93 |
| Basswood | 335.10 | 274.48 | 273.50 | 224.64 |
|  | 6338.87 | 6287.12 | 5071.04 | 5140.50 |

Which gives us a $0.82 \%$ lower figure by using the conversion formula in conjunction with the Scribner rule. With the Doyle rule the conversion is $1.37 \%$ higher. These percentages certainly indicate that it is entirely possible to develop reliable conversion formula. These could be worked out for any number of species in all areas, or could be worked out for different forest types in the different areas. For the purpose of this study the formula developed so far will serve to prove the point.

## Chapter 3

The principle objective of this investigation is to determine the possibility of using straight line trends based on basal area as a means of estimating the probable time or cost of a logging or milling operation. Since the wood fibers are uniform in any particular species it is quite conceivable that a certain amount of energy is required to break the fibers of any specified cross sectional area. In that basal area breast height would be relatively easy to determine and has been used in research and taught in the technical training given potential foresters, it will be the basic unit upom which the time required will be calculated.

The original data was provided by the late Professor D. M. Matthews. These data were unpublished time studies made by the U. S. Forest Service. Of the time studies available, seven were chosen to be worked up in this investigation.

There were three studies conducted in the states of New York, New Hampshire and Vermont in 1936-37. The study made in Vermont occupied a median position so it was used. In addition to the three predominant species used in this investigation, the stands included white ash, red spruce, hemlock, balsam fir and basswood in small quantities.

The felling and bucking was performed by two crews of two men each. There were two units skidding each com-
posed of one man and one horse. The hauling was done by one $20 \mathrm{H} . \mathrm{P}$. caterpillar tractor and scoot over an average estimated distance of 2500 feet. Included in this operation was part of the road work, loading and hauling. In the milling phase of the operation a portable mill was operated by a crew consisting of a head sawyer, one deckman, one offbearer, one marker and one fireman.

The original study in northern Wisconsin was made by Raymond H. Miller and associates in 1935-36. The stand here studied also included hemlock as well as the yellow birch, sugar maple, elm and basswood which are incorporated in this report.

The operations of skidding, loading and hauling overlapped. These operations were performed by a crew composed of one and a half truck drivers, two teamsters and two swampers. There is no statement available as to the manner of organization for the felling and bucking. On this operation the sawmilling was done by a single band mill with shotgun feed. The 38 men employed, operated this mill and its equipment which included a pond, edger, trimmer, green chain and lumber yard space.

There are sixteen columns in the work sheets, Appendix 0, Tables 4-10 inclusive, of time per unit for the various operations, etc. A general discussion at this point on the derivation of the various columns will give an insight into the following discussion. Column 2
was taken from basal area tables. Columns 1, 3, 5, 8, 11 and 14 were taken from the original time study sheets. To determine the basal area per M, column 4, the volume per tree was divided unto the basal area per tree and this quotient multiplied by 1000. The man hours per square foot of basal area columns under each of the major operations was calculated by dividing the basal area per $M$ into the man hours per $M$ in each of the operations. These last figures multiplied by 60 minutes gave the last column under each operation heading.

The first step in attempting to develop these straight line trends after acquiring the original data was determining the man-minutes per square foot of basal area. These values were then plotted over d.b.h. in the graphs in Appendix 0. Smooth curves were adjusted by halves so that each end ofthe curve is better fitted and therefore more accurately placed on the data. After plotting the curves as well as possible straight lines were then fitted to the data. These straight lines are the potential trend lines, if you will, that we are looking for.

When the curves had been plotted many things were noted, among which was the similarity of curves for one operation in each of the two areas under consideration. The curves for the Vermont studies were not as uniform as those from Northern Wisconsin. The maximum diameter range used in the Vermont study was from 11 inches to 23 inches inclusive. The original data covered a wider
range but the relative weights of the end points which were dropped were of little importance. This is evidenced by the small weights shown on the end points of the graphs.

Upon examining the curves plotted for felling and bucking, Figures 7, 11 and 15, we find the sugar maple shows the same relative hump at about the 14 inch class. The yellow birch and beech on the other hand show a rather steady downward trend throughout the diameter ranges under consideration. In both of the later cases this drop is about 0.44 minute per diameter class, for the yellow birch it is 0.45 minutes and for the beech it is 0.43 minutes. The actual time ranges are for the yellow birch 18.1 minutes to 23.5 minutes, for the beech 19.1 minutes to 23 minutes over a range of 9 inches which is well within the 12 inch range of the yellow birch. The variation in the sugar maple curve is about 0.27 minutes per diameter class from the 14 inch class up. These figures on variation per size class are fairly close to one another and further investigation may show a more definite trend. It will be noted though that the time for sugar maple is consistently a little higher than the other species. This may be due to the higher specific gravity or density of this species.

The skidding curves, Figures 8,12 and 16 , show very similar characteristics in that they all drop steadily over most of the diameter ranges being studied. They
also show a tendency to level off in the larger sizes. The drop per inch of increase in diameter class of the sugar maple is 0.56 man-minutes. For the yellow birch we find a decrease of 0.58 man-minutes for each inch of diameter increase. In this respect the beech is slightly lower. It's decrease for each inch of increase of diameter class is 0.53 man-minutes per square foot of basal area. Should the curves of skidding in northern Wisconsin show close similarities to these curves it may be concluded that the skidding time per square foot of basal area has a definite trend. It will be noted that the straight lines as fitted to these data fit remarkably well and easy on the graphs.

All three of the hauling curves, Figures 9, 13 and 17, have different trends. Both the yellow birch and sugar maple curves show an increase in the lower diameter with a decrease in the upper diameter. The increase in the sugar maple data is more rapid than in the yellow birch where as the decrease is gentler. From 14 inches to 23 inches inclusive on the sugar maple graph, the time plotted starts at 19.1 man-minutes rises to 19.7 man-minutes at 17 inches and then drops back to 19.0 man-minutes. That is a 0.15 man-minute increase and a 0.10 man-minute drop. For most purposes this might be interpreted as a horizontal line. The yellow birch starts at 17.9 man-minutes in the 11 inch class then rises to 18.6 man-minutes at the 14
inch class or 0.18 man-minutes per one inch increase in diameter and drops off to 17.5 man-mingtes in the 22 inch class, 0.12 man-minutes per inch. In contrast to the rising then falling curve of the two above mentioned species the beech curve steadily rises from 16.0 manminutes at the 12 inch diameter to 17.3 man-minutes at the 20 inch diameter, which is 0.13 man minutes per inch increase in diameter. This increase tends to counter balance the drops in the other curves and if the weighted average were calculated it would be found to be 18.43 man minutes per square foot of basal area.

The milling curves, Figures 10, 14, 18, show a downward trend from about the 13 inch class up on the hard maple and yellow birch studies. The general lay of the data seems to indicate a rise in time to this point or at least in the lower diameter classes. This might indicate that the milling practice was to saw the smaller trees with increasing care as to quality outurn up to the point where the time starts to come down. These indications are not found in the curve for milling of the beech. In this curve we see a fairly steady increase in time per square foot of basal area with the larger sizes. It might be found if these studies were carried farther that a horizontal or slightly descending trend would be developed. The maximum differential in the plotted data is only 2.8 man-minutes per square foot of basal area for
a ll inch range in the yellow birch. This would show only about a 0.25 minute differential, from size class to size class. Upon considering the three species together there is a maximum differential of 4.6 man-minutes over a range of 12 inches even this gives about a drop of 0.40 minute from one diameter to the next larger.

Northern Wisconsin Study

It will be noted that the felling and bucking curves Figures 19, 23, 27, 31, for this operation show decided inclinations toward a decrease in time with an increase of diameter breast high. In one case this decline is shown only in the 10 to 28 inch diameter. This curve for the elm shows an increase of about 1 man-minute from 14 inches to 20 inches inclusive. The decrease is about 2 man-minutes for the diameter range from 20 inches to 28 inches. These figures show a general decrease for the entire range being studied, which correlates with the curves for the other species. The curve for the felling and bucking of yellow birch shows an increase in the lower three diameters but from 14 inches up to the 24 inches class there is a decrease of 4.5 man-minutes per square foot of basal area. This gives a net fall of about 0.45 manminutes per inch increase in diameter. The felling and bucking curve for sugar maple drops from 22.3 man-minutes
to 17.4 man-minutes over a range of 15 inches or a decrease of 0.35 man-minutes per square foot of basal area for each inch of increased diameter. These decreases are upheld by the basswood curve. It drops from 19.4 man-minutes at 13 inches to 14 man-minutes at 27 inches. This is a drop of 0.39 man-minutes per inch of increase in diameter. It is interesting to note that this particular curve is encouraging as an indication that the straight line trend may prove applicable. A slight $S$ curve could have been fitted to the data of the basswood felling and bucking time but the curvature would have been practically negligible. Three of the skidding curves, Figures 20, 24, 28, 32, have two separate slopes. The basswood curve for instance drops from 27.2 man-minutes at the 13 inch class to 17.7 man-minutes at the 20 inch class for an average drop per diameter class of 1.36 man-minutes. The diameter range of 20 inches to 27 inches has a decrease from size class to size class of 0.83 man-minutes. Sugar maple most closely resembles the basswood in respect to time. The average drop over the 12 to 20 inch classes is 1.19 manminutes per inch of increase in diameter. For the upper diameter range of 20 inches to 26 inches, the average decrease in time is 0.67 man-minutes per square foot of basal area for eabh inch increase in diameter breast high. The other curve showing two separate slopes is the one for elma. Here too the break in slope is at 20 inches.

For diameter below this point, we have an average decrease in man-minutes of 0.63 for every inch of diameter. The diameter larger than 20 inches have about 0.21 man-minutes fall in time per inch of diameter increase. In this series we find the yellow birch curve assumes a definite $S$ pattmrn. Because of the location of the data here we find that one straight line or rather one continuous slope is best suited for discussion. Considering this as a one slope line we have a drop of 0.78 man-minutes per square foot of basal area for the diameter range of 12 to 24 inches inclusive.

It is very interesting to see that part of the loading and hauling curve for the basswood, Figure 29, also plots as a straight line. The part of the curve from 13 inches to 18 inches inclusive rises then falls with the high point being at 15 inches. The rise is only 0.40 manminutes and the drop over the above range is 0.50 manperinch. minutes. Under examination we find that the drop per inch of diameter breast high for the straight line range of this curve is 0.43 man-minutes. The loading and hauling curve for elm Figure 33 and the other two has the same general shape as the basswood in that it rises through the lower diameter classes and then falls off to the end of the range. The rise in this case is from 14 inches to 19 inches inclusive. The net change over this range is plus 2.3 man-minutes or about 0.46 man-minutes per inch of
increased diameter. From 19 inches to 28 inches the data drops 2.5 man-minutes per class. The sugar maple curve, Figure 21, rises from the 12 inch class to the 14 inch one inclusive. Over these diameters the rise 0.80 man minutes or 0.40 man-minutes per inch increase in diameter. From 15 inches to 26 inches the trend is down with a drop of 4.6 man-minutes. This gives us a decrease in time of 0.42 man-minutes for each inch of diameter increase. All of these trends are very similar as is also the one for yellow birch. The yellow birch curve, figure 25, rises from 12 inches to 15 inches at the rate of 0.50 man-minutes per inch of diameter increase. The slope down starts with the 16 inch class and continues through the 24 inch diameter. Over this range of diameter there is a drop of 0.35 manminutes for each inch.

The most strikingly similar curves in this study are those pertaining to milling, Figures $22,26,30,34$. They all rise rapidly and reach a high point around the 18 to 20 inch class, from which they rapidly drop off. This high point probably is at the point where the height growth of . the tree slows to practically nothing, that is the length in logs comes to a standstill. This would cause a rapid increase in time in that the number of logs increases more rapidly than the basal area. For each of the logs the time necessary for turning would be about constant so this time would vary directly as to the number of logs in a tree.

Since these curves have such a high point in the middle, it is practically impossible to fit two straight lines to the data. Because of this, three lines would be necessary to make a reasonable fit and this would cause much confusion in the use of these trend lines. Perhaps further study of this type of operation would disclose facts which tend to support or disprove this tendency for the curves to rise and then fall rapidly.

For the basswood milling curve it rises from 76.1 manminutes at 13 inches to 83.7 man-minutes at 18 inches and then drops to 70.0 man-minutes at 27 inches. This gives a net difference of 13.7 man-minutes over a range of 10 inches which is a sizable variation. The rapid change would have a marked effect on the costs of milling various sizes of trees. Upon examination the sugar maple curves starts at 45.5 man-minutes at 12 inches and ends at 46.5 man-minutes at 26 inches with the high point at 17 inches and a value of 54.9 man-minutes. Once again the variation from inch class to inch class is marked and would seriously effect the milling cost. The elm curve shows the same rapid change in time from one diameter class to the next. A low point of 47.7 man-minutes at 14 inches is at one end of the curve, at 20 inches the high point is reached with a point of about 59.0 man-minutes. When we get to the 28 inch the man-minutes are down to 48.2. The milling curve of the yellow birch shows the same general
trend except the decrease from the high point is more gentle. Here we have a value of 39 man-minutes for the 12 inch class which rises to 50.6 man-minutes at the 19 inch diameter. The decline from this point is rather gradual to a point at 24 inches where the time value is 47.7 man-minutes. From the original data it is not possible to determine if the practice of the mill may have had some important influence on these curves. If the head sawyer had instructions to saw more for quality as size increased, the time element would increase to some point where quality was at a premium and then gradually taper off. Such a practice would tend to accentuate the hump in these curves.

## Determination of Error Induced

In all of the above discussions of the graphs of man-minutes over diameter breast high, I have used the values as actually plotted. Of course these would change if either of the other two possible sets of values were used but the relations would remain practically constant. The other values could have been those read from the curves themselves or the straight lines.

To see if the straight lines induce much error in the time necessary and hence the cost of logging a stand, the following calculations are in order. For the purpose of these computations the values read from the fitted
curves and straight lines will be used. There is little net difference between the values on the curve and the plotted points as the curve was balanced in by weighted values. The following form of calculations will be used for determining the error induced if the Northern Wisconsin time study is used.

Yellow Birch -- Felling and Bucking

| D.B.H. | Man-minutes per <br> Square foot of BA |  |  | B.A. per <br> Acre |  |
| :---: | :---: | :---: | :---: | :---: | :---: | | Time per |
| :---: |
| Acre |

In using the above form for computations we find the totals for the following to be:

| Felling and Bucking |  | Curve | Trend line | \% of Error |
| :--- | ---: | :---: | :---: | :---: |
| Yellow Birch |  | 440.7 |  | 442.5 |
| Sugar Maple | 593.8 | 594.5 | +.41 |  |
| Basswood | 36.9 | 36.9 | +.12 |  |
| Elm | 9.8 | 9.8 | .00 |  |
|  | 1081.2 | 1083.7 | .00 |  |
| Skidding |  |  | +.23 |  |
| Yellow Birch | 360.0 | 359.0 | -.28 |  |
| Sugar Maple | 534.2 | 536.9 | +.51 |  |
| Basswood | 42.2 | 42.1 | -.24 |  |
| Elm | 8.8 | 8.8 | .00 |  |
|  | 945.2 | 946.8 | +.17 |  |
| Loading and Hauling |  |  |  |  |
| Yellow Birch | 299.2 | 298.8 | -.13 |  |
| Sugar Maple | 416.1 | 418.0 | +.46 |  |
| Basswood | 33.6 | 33.7 | +.30 |  |
| Elm | 5.6 | 5.6 | .00 |  |
|  | 754.5 | 756.1 | +.21 |  |

I have not seen filt to try to balance in straight lines to the milling curves due to their extreme curvature. For trend lines to be of use they should be relatively simple. In the case of these curves as has been stated before, it would take at least three straight lines to even faintly follow the trend indicated by the curves. This would complicate matters beyond practicability.

- From the above tabulations it will be noted that the percentage error induced by using the trend lines as plotted is very small. The most extreme error for all species is less than a quarter of one percent. An operator could hardly hope to estimate costs of an operation closer than this figure. Should we compute the error on an operation which delivers logs to a mill we find the over all error is about $0.20 \%$. This is negligible in the light that it is an estimation.

We have determined several things in this investigation, some of which are conclusive and others which are only indicative. The indications are primarily that further study is necessary to definitely fix the location of the trend lines and those used in making the conversions from basal area to board foot volumes.

The conversion formulae set forth in this study definitely show that it is possible to correlate basal area at breast height with board foot volume. The data used herein is definitely limited which tends to cast a shadow as to the precise accuracy of these formulae. To accurately develop the necessary formulae, it would be necessary to run a study such as the one conducted in Chapter 2 of this paper on a much larger number of trees. It would also be necessary to broaden the coverage of such investigations to include other species and timber types, as those produced here deal only with the northern hardwoods in the northern hardwood-hemlock type.

In respect to the trend line development it may be stated that they can be developed satisfactorily. We have here shown that such trend lines developed with one set of data applied to a stand table which had been constructed from different data, induced very little error. Although these lines have been determined for the species and area covered in this study it is self-evident
that such trends are not fixed in respect to their time values. It is quite likely that these trends could be consolidated by species so as to come up with a heavier weighted trend. If this were to be done, more time study data would have to be consulted.

I have not developed the formulae for the various trend lines as plotted, because I feel there is a need for further study to more specifically locate the lines. Such formulae could be written by the method given in Chapter 2. They could then be stated either in symbols or words for use by the layman as well as the trained man.

It is evident that the felling and bucking operation has a declining time trend per square foot of basal area as the diameter increases. The rate of decrease varies from species to species as does the time required at any specific diameter. As was stated previously, the board foot volume per square foot of basal area increases with diameter. If the time per square foot of basal area was converted to time per $M$ the decrease would be more pronounced thereby getting confirmation from the experience of contract loggers. These loggers have found through selective logging that costs decrease per $M$ as you cut larger sized timber.

Of all the operations, skidding shows the most similarity. For this operation all of the curves have a definite decrease in time with the increase in diameter.

This trend would hold as long as the equipment being used was not made to work outside its load limits. In the Vermont study this trend seems to be a single straight line, but in the Northern Wisconsin study there seems to be a sag at about the 20 inch class, causing two separate trend lines to be used. One may definitely say in the face of the evidence shown in this study that trend lines are applicable to skidding operations.

The time required to load and haul logs tends to increase in the lower diameter ranges then taper off as the larger diameters are reached. This could be partially caused by the relation between height and diameter growth. It has been determined that the maximum merchantable height of lake states hardwoods is usually reached at about the 18 inch class. This would cause the relationship between the number of logs and basal area to level off when this diameter was reached, and therefore the fixed time of hooking and unhooking would become constant on a per tree basis. The one exception to the general trend stated above is the tractor hauling curve for beech in Vermont. This hauling curve climbs throughout the diameter range under consideration. Both the yellow birch and sugar maple curves for the Vermont study turns down in the largerdiameter classes. I am unable to correlate this variation in that my knowledge of that area is nil.

The milling phase of the operation presents the most variation. The curves for milling in the northern Wisconsin study are very similar in that they all rise rapidly in the lower diameters, level off around the 18 to 20 inch class, and then decline rapidly to the upper diameter limit of the species studied. As stated before, it is impractical to try to develop trend lines for this operation. The curves for the Vermont study presents three distinct types of curves. For yellow birch, there is a relatively steady decrease throughout the diameter range with the increase in diameter. The curve for the beech shows the opposite trend, that is a steady increase in time with the increase in diameter. The sugar maple curve starts as the beech with rising time values with increasing diameter then a reversal of slope to a decreasing time per square foot of basal area which is similar to the yellow birch curve. Because of these erratic curves it is impossible to draw any conclusions from the milling curves except that further study is needed.

It must be noted that the trend lines here-in developed had the human factor in the original data. How efficient the original workers were is debatable. We can probably conclude that the equipment in use then was not nearly as efficient as that in use today. Because of these factors there probably is need for adjustment in the loeations of these trend lines. Quite likely with power saws the felling and bucking trend lines would tend to become
more horizontal with a general decrease in the man-minutes per square foot of basal area values. Other improvements in equipment will in turn influence the time values for the operations on which they are used.

To summarize briefly, we have found that trend lines of man-minutes per square foot of basal area over diameter breast high can be developed and induce very slight errors in determining the time necessary to accomplish different operations. A satisfactory method of converting basal area at diameter breast height to board foot volume in either the Doyle or Scribner rule has been developed. The two principle problems of this investigation have therefore been acoomplished.

Appendix A

Northern Hardwood Volume Tables



Prepared by Form class - taper method.
Block indicates extent of basic data.
Aggregate difference - $-1.28 \%$

Appendix B

Northern Hardwood stand Tables

Stand and Stock Table, Hard Maple, Mature Hardwood - Hemlock, Gogebic County

Michigan
Typical Acre

| DBH | \#Trees/a | B.A./a | Vol.Scrib. | Bd.ft./ <br> Sq.ft.B.A. | Vol. <br> Doyle | Bd.ft/ <br> sq.ft.B.A. |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 10 | 1.64 | 0.90 | 57.40 | 63.78 | 19.68 | 21.87 |
| 12 | 3.64 | 2.86 | 203.48 | 71.15 | 112.48 | 39.33 |
| 14 | 4.11 | 4.42 | 383.05 | 86.44 | 265.92 | 60.16 |
| 16 | 4.04 | 5.66 | 557.92 | 98.57 | 422.58 | 74.48 |
| 18 | 3.53 | 6.23 | 739.89 | 118.76 | 596.22 | 95.70 |
| 20 | 2.00 | 4.40 | 534.60 | 121.50 | 447.60 | 101.73 |
| 22 | 1.10 | 2.86 | 350.57 | 122.58 | 319.44 | 111.69 |
| 24 | 0.77 | 2.42 | 311.46 | 128.70 | 288.29 | 119.12 |
| 26 | 0.17 | 0.63 | 85.58 | 135.84 | 69.56 | 110.41 |
| 28 | 0.09 | 0.38 | 55.50 | 145.78 | 54.90 | 144.47 |
| 30 | 0.01 | 0.05 | 5.52 | 110.40 | 58.50 | 117.00 |
| 32 | 0.01 | 0.06 | 5.01 | 83.50 | 55.10 | 91.83 |
| 34 | 0.01 | 0.06 | 9.28 | 154.67 | 108.50 | 180.83 |
|  | 21.12 | 30.93 | 3293.26 |  | 2518.9 |  |

Stand and Stock Table, Xellow Birch Mature Hardwood - Hemlock, Gogebic County Michigan

Typleal sere

| DBH | \#Tree/a | BA/a | Vol.Scrib. | Bd.ft/ |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Sq.ft.BA |  |  |  |  |$\quad$ Vol.Doyle | Bd.ft/. |
| :--- |
| Sq.ft./BA |

Stand and Stock Table, Besswood Mature Hardwood - Eemlock, Gogebic County

Miehigan
Typiepl Acre

| DBH | \#Trees/a | BA/a | Vol.Scrib. | $\begin{aligned} & \mathrm{Bd} \cdot \mathrm{ft} \cdot / \\ & \mathrm{sq} \cdot \mathrm{ft} \cdot \mathrm{BA} \end{aligned}$ | Vol.Doyle | $\begin{aligned} & \mathrm{Bd} \cdot \mathrm{Ft} \cdot / \\ & \text { sq.ft. } \mathrm{BA} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 10 | 0.19 | 0.10 | 7.0 | 70.0 | 2.3 | 23.0 |
| 12 | 0.40 | 0.31 | 24.6 | 79.4 | 13.3 | 42.9 |
| 14 | 0.19 | 0.21 | 21.7 | 103.3 | 14.4 | 68.6 |
| 16 | 0.31 | 0.42 | 54.6 | 130.1 | 40.0 | 95.3 |
| 18 | 0.31 | 0.55 | 65.1 | 118.4 | 55.5 | 101.0 |
| 20 | 0.05 | 0.11 | 12.2 | 111.0 | 10.2 | 92.7 |
| 22 | 0.12 | 0.31 | 46.2 | 149.0 | 41.1 | 132.8 |
| 24 | 0.17 | 0.53 | 76.2 | 143.9 | 69.6 | 131.3 |
| 26 | 0.02 | 0.07 | 12.0 | 171.4 | 11.5 | 164.2 |
| 28 | 0.01 | 0.04 | 7.1 | 177.6 | 7.1 | 177.5 |
| 30 | 0.01 | 0.05 | 8.4 | 167.1 | 8.5 | 170.0 |
|  | 1.78 | 2.70 | 335.1 |  | $\overline{273.5}$ |  |

Stand and Stock Table, Red Maple,
Mature Hardwood - Hemlock, Gogebic County Michigan

Typicalacne
$\left.\begin{array}{ccccccc}\text { DBH \#Trees/a } & \text { BA/a } & \text { Vol.Scrib. Bd.ft./ } & \text { Vol.Doyle Bd.ft./ } \\ \text { sq.ft.BA }\end{array}\right]$

Stand and Stock Table, Black Ash, Hature Hardwood - Hemlock, Gogebic County Michigan

Typical Aere

| DBH \#Trees/a BA/a | Vol.Scrib. Bd.ft/ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| sq.ft.BA |  | Vol.Doyle | Bd.ft./ |
| :---: |
| sq.ft.BA |

Stand and Stock Table, Elm
Mature Hardwood - Hemlock, Gogebic County Michigan
Typicalacre

| DBH \#Trees/a | BA/a | Vol.Scrib. | Bd.ft./ <br> Sq.Ft.BA | Vol.Doyle Bd.ft./ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| sq.ft.BA |  |  |  |  |

Appendix C

Time Study Tables and Graphs


*All volumes are board feet mill tally.

| $\begin{gathered} \text { (1) } \\ \text { D. B. н. } \end{gathered}$ | $\begin{aligned} & \text { (2) } \\ & \text { B. A. } \\ & \text { per } \\ & \text { Tree } \end{aligned}$ | $\begin{aligned} & \text { (3) } \\ & \text { Vol. } \% \\ & \text { per } \\ & \text { Tree } \end{aligned}$ | $\begin{aligned} & \text { (4) } \\ & \text { B. A. } \\ & \text { per } \\ & \text { M } \end{aligned}$ | FELLINg and bucking |  |  | SKIDDING |  |  | HAULING |  |  | Milling |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | $\begin{gathered} \hline(5) \\ \begin{array}{c} \text { Mon Hrs. } \\ \text { per } \\ M \end{array} \\ \hline \end{gathered}$ | $\begin{gathered} \text { (6) } \\ \text { Man } \begin{array}{c} \text { Mrs. } \\ \text { Per Sq. } \\ \text { Ft. B. A. } \end{array} \end{gathered}$ | $\begin{gathered} \text { (7) } \\ \begin{array}{c} \text { Mon Min. } \\ \text { Pet. } \\ \text { Pat. } \\ \text { ft. B. A. } \end{array} \\ \hline \end{gathered}$ | $\begin{gathered} \text { (8) } \\ \substack{\text { Man Hrs. } \\ \text { Per } \\ M} \\ \hline \end{gathered}$ | $\begin{aligned} & \text { Per Sq. } \\ & \text { ft. B. A. } \end{aligned}$ $\begin{gathered} \text { (9) } \\ \text { Man Hrs. } \\ \text { Per Sq. } \end{gathered}$ | $\begin{gathered} (10) \\ \text { Man Min. } \\ \text { Per } \\ \text { Pt. S. } \\ \text { St. A. } \end{gathered}$ | (11) Man Hrs. per $M$ | $\begin{gathered} \hline \text { (12) } \\ \substack{\text { Men Hss. } \\ \text { Per } \\ \text { for. } \\ \text { ft. B. A. }} \end{gathered}$ | (13) <br> Man Min. Per Sq. Ft. B. A. . | $\underset{\text { Mon Hrs. }}{(14)}$ $\begin{aligned} & \text { per } \\ & M \end{aligned}$ |  | (16) Man Min. Man Per Sa. Min. Ft. B. A. |
| 12 | 0.785 | 68 | 11.55 | 4.43 | 0.384 | 23.0 | 2.50 | 0.217 | 13.0 | 3.09 | 0.268 | 16.0 | 4.42 | 0.382 | 23.0 |
| 13 | 0.922 | 82 | 11.25 | 4.21 | 0.374 | 22.4 | 2.28 | 0.203 | 12.3 | 3.03 | 0.269 | 16.1 | 4.28 | 0.380 | 22.8 |
| 14 | 1.069 | 97 | 11.00 | 4.00 | 0.364 | 21.8 | 2.10 | 0.191 | 11.4 | 2.98 | 0.271 | 16.2 | 4.17 | 0.379 | 22.8 |
| 15 | 1.227 | 114 | 10.75 | 3.80 | 0.354 | 21.2 | 1.95 | 0.181 | 10.9 | 2.93 | 0.272 | 16.4 | 4.07 | 0.378 | 22.7 |
| 16 | 1.396 | 134 | 10.41 | -3.62 | 0.347 | 20.8 | 1.80 | 0.173 | 10.4 | 2.89 | 0.278 | 16.6 | 4.01 | 0.385 | 23.1 |
| 17 | 1.576 | 155 | 10.17 | 3.46 | 0.340 | 20.4 | 1.69 | 0.166 | 10.0 | 2.86 | 0.282 | 16.9 | 3.95 | 0.389 | 23.3 |
| 18 | 1.767 | 177 | 9.99 | 3.32 | 0.333 | 20.0 | 1.59 | 0.159 | 9.6 | 2.83 | 0.284 | 17.0 | 3.90 | 0.391 | 23.4 |
| 19 | 1.969 | 201 | 9.79 | 3.19 | 0.326 | 19.6 | 1.50 | 0.153 | 9.2 | 2.80 | 0.286 | 17.1 | 3.87 | 0.395 | 23.7 |
| 20 | 2.182 | 226 | 9.66 | 3.08 | 0.319 | 19.1 | 1.41 | 0.146 | 8.8 | 2.78 | 0.288 | 17.3 | 3.83 | 0.396 | 23.8 |
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| SKIDDING |  |  | HAULING |  |  | MILLING |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| (8) | (9) | (10) | (11) | (12) | (13) | (14) | (15) | (16) |
| Man Hrs. Per M | Man Hrs. Per Sq. <br> Ft. B. A. | Man Min. Per Sq. <br> Ft. B. A | Man His. per M | Man Hrs. Per Sq. <br> Ft. B. A. | Man Min. <br> Per Sq. <br> Ft. B. A | Man Hrs. per $M$ | Man Hrs. Per Sq. <br> Ft. B. A | Man Min. Per Sq. Ft. B. A. |
| 3.90 | . 407 | 24.4 | 2.35 | . 245 | 14.7 | 7.27 | . 760 | 45.5 |
| 3.60 | . 402 | 24.2 | 2.28 | . 255 | 15.3 | 7.30 | . 816 | 49.0 |
| 3.29 | . 386 | 23.1 | 2.21 | . 259 | 15.5 | 7.30 | . 855 | 51.3 |
| 2.99 | .364 | 21.6 | 2.13 | . 259 | 15.5 | 7.34 | . 891 | 53.5 |
| 2.71 | . 347 | 20.8 | 2.05 | . 253 | 15.2 | 7.37 | . 909 | 54.5 |
| 2.47 | . 306 | 18.3 | 1.99 | . 246 | 14.8 | 7.34 | . 909 | 54.5 |
| 2.29 | . 297 | 17.8 | 1.92 | . 249 | 14.9 | 7.30 | . 945 | 56.7 |
| 2.15 | . 268 | 16.1 | 1.86 | . 232 | 13.9 | 7.27 | . 905 | 54.3 ' |
| 2.01 | . 248 | 14.9 | 1.81 | . 224 | 13.4 | 7.24 | . 894 | 53.6 |
| 1.91 | . 234 | 14.1 | 1.76 | . 216 | 13.0 | 7.21 | . 885 | 53.1 |
| 1.83 | . 221 | 13.3 | 1.72 | . 208 | 12.5 | 7.14 | . 863 | 51.7 |
| 1.76 | . 208 | 12.5 | 1.70 | . 201 | 12.1 | 7.11 | . 842 | 50.5 |
| 1.65 | . 192 | 11.5 | 1.67 | . 194 | 11.7 | 7.05 | .820 | 49.2 |
| 1.66 | . 189 | 11.4 | 1.65 | . 188 | 11.3 | 7.01 | . 800 | 48.0 |
| 1.63 | . 181 | 10.9 | 1.64 | . 182 | 10.9 | 6.95 | . 772 | 46.3 |




|  | $\begin{gathered} \text { (2) } \\ \text { B. A. } \\ \text { per } \\ \text { Tree } \end{gathered}$ | $\begin{aligned} & \text { (3) } \\ & \text { Vol. } * \\ & \text { per } \\ & \text { Tree } \end{aligned}$ | (4) <br> B. A. $\stackrel{\text { per }}{M}$ | FELLING and BUCKING |  |  | SKIDDING |  |  | HAULING |  |  | MILLING |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | (5) <br> Man Hrs. per $M$ | (6) <br> Man Hrs. Per Sq. Fi. B. A. | (7) Man Min. Per Sq. F. B. A. | (8) Man Hrs. Per M | (9) <br> Man Hrs. Per Sq. Ft. B. A. | (10) <br> Man Min. Per Sq. <br> Fr. B. A. | (11) <br> Man Hrs. <br> $\substack{\text { per } \\ M}$ | (12) <br> Man Hrs. Per Sq. <br> Ft. B. A. | (13) <br> Man Min. Per Sq. Ft. B. A. | (14) <br> Man Hrs. per M | (15) <br> Man Hrs. Per Sq. Ft. B. A. | (16) <br> Man Min. Ft. B. A. |
| 13 | . 922 | 107 | 8.61 | 2.78 | . 323 | 19.4 | 3.91 | . 454 | 27.2 | 2.34 | . 272 | 16.3 | 10.91 | 1.268 | 76.1 |
| 14 | 1.069 | 131 | 8.16 | 2.60 | . 319 | 19.1 | 3.60 | . 441 | 26.5 | 2.25 | . 276 | 16.5 | 10.71 | 1.313 | 78.9 |
| 15 | 1.227 | 157 | 7.81 | 2.40 | . 308 | 18.4 | 3.30 | . 423 | 25.4 | 2.17 | . 278 | 16.7 | 10.52 | 1.349 | 80.9 |
| 16 | 1.396 | 184 | 7.58 | 2.29 | . 302 | 18.1 | 3.00 | .396 | 23.8 | 2.10 | . 277 | 16.6 | 10.39 | 1.370 | 82.2 |
| 17 | 1.576 | 214 | 7.37 | 2.18 | . 296 | 17.8 | 2.74 | .372 | 22.3 | 2.01 | . 273 | 16.4 | 10.23 | 1.389 | 83.4 |
| 18 | 1.767 | 243 | 7.27 | 2.09 | . 288 | 17.3 | 2.48 | . 342 | 20.5 | 1.94 | . 267 | 16.0 | 10.10 | 1.390 | 83.4 |
| 19 | 1.969 | 274 | 7.19 | 2.03 | . 282 | 16.9 | 2.26 | . 314 | 18.9 | 1.88 | . 262 | 15.7 | 10.01 | 1.391 | 83.5 |
| 20 | 2.182 | 305 | 7.17 | 2.00 | . 279 | 16.7 | 2.11 | . 294 | 17.7 | 1.82 | . 254 | 15.2 | 9.91 | 1.381 | 83.0 |
| 21 | 2.405 | 335 | 7.18 | 1.96 | .273 | 16.4 | 2.00 | . 279 | 16.7 | 1.77 | . 247 | 14.8 | 9.81 | 1.357 | 82.0 |
| 22 | 2.640 | 366 | 7.22 | 1.94 | . 269 | 16.1 | 1.90 | . 264 | 15.8 | 1.74 | . 241 | 14.5 | 9.72 | 1.347 | 80.8 |
| 23 | 2.885 | 395 | 7.31 | 1.92 | . 263 | 15.8 | 1.83 | .252 | 15.0 | 1.71 | . 234 | 14.0 | 9.62 | 1.316 | 79.0 |
| 24 | 3.142 | 422 | 7.45 | 1.91 | .256 | 15.4 | 1.75 | . 235 | 14.1 | 1.68 | . 226 | 13.5 | 9.56 | 1.284 | 77.1 |
| 25 | 3.409 | 449 | 7.60 | 1.89 | . 249 | 14.9 | 1.67 | . 220 | 13.2 | 1.66 | . 218 | 13.1 | 9.49 | 1.249 | 75.0 |
| 26 | 3.687 | 474 | 7.79 | 1.86 | . 239 | 14.3 | 1.62 | . 211 | 12.6 | 1.64 | . 211 | 12.6 | 9.39 | 1.206 | 72.4 |
| 27 | 3.976 | 496 | 8.01 | 1.87 | . 234 | 14.0 | 1.59 | . 199 | 11.9 | 1.63 | . 204 | 12.2 | 9.33 | 1.166 | 69.9 |
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|  | (2) <br> B. A. <br> per | (3) <br> Vol. * <br> per <br> Tree | (4) <br> B. A. <br> per <br> M | FELLING and BUCKING |  |  | SKIDDING |  |  | HAULING |  |  | MILLING |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | (5) | (6) | (7) |  |  |  |  |  |  |  |  |  |
|  |  |  |  | Man Hrs. M | Man Hrs. <br> Per Sq. <br> Ft. B. A. | Man Min. Per Sq. Ft. B. A. | Man Hrs. Per M | Man Hrs. Per Sq. Ft. B. A | Man Min. Per Sq. <br> Ft. B. A | Man Hrs. per M |  | (13) <br> Man Min. Per Sq. Ft. B. A. | (14) <br> Man Hrs per $M$ | (15) <br> Man Hrs. Per Sq. <br> Ft. B. | (16) <br> Man Min. Per Sq. |
| 14 | 1.069 | 112 | 9.54 | 2.69 | . 282 | 16.9 | 3.13 |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  | . 328 | 19.7 | 2.13 | . 224 | 13.4 | 7.56 | . 794 | 47.6 |
| 15 | 1.227 | 143 | 8.57 | 2.50 | . 291 | 17.5 | 2.81 | . 328 | 19.7 | 2.06 | . 240 | 14.4 | 7.40 | 863 | 51.8 |
| 16 | 1.396 | 176 | 7.93 | 2.35 | . 297 | 17.8 |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  | 17.8 | 2.50 | . 316 | 18.9 | 1.98 | . 250 | 15.0 | 7.21 | . 910 | 54.6 |
| 17 | 1.576 | 212 | 7.44 | 2.22 | . 298 | 17.9 | 2.25 | . 303 | 18.2 | 1.91 | . 257 | 15.4 | 7.01 | 943 |  |
| 18 | 1.767 | 248 | 7.12 | 2.12 | . 298 | 17.9 |  |  |  |  |  |  |  |  | 56.6 |
|  |  |  |  |  |  | 17.9 | 2.04 | . 287 | 17.2 | 1.84 | . 258 | 15.5 | 6.85 | . 962 | 57.7 |
| 19 | 1.969 | 287 | 6.86 | 2.06 | . 300 | 18.0 | 1.89 | . 276 | 16.5 | 1.79 | . 261 | 15.7 | 6.69 |  |  |
| 20 | 2.182 | 328 | 6.66 | 2.02 | . 303 | 18.2 |  |  |  |  |  |  |  |  | 58.5 |
|  |  |  |  |  |  |  | 1.77 | .266 | 15.9 | 1.73 | . 260 | 15.6 | 6.50 | . 975 | 58.5 |
| 21 | 2.405 | 374 | 6.44 | 1.93 | . 299 | 17.9 | 1.68 | . 261 | 15.6 | 1.68 | . 261 | 15.7 | 6.38 | . 985 |  |
| 22 | 2.640 | 417 | 6.34 | 1.88 | . 297 | 17.8 |  |  |  |  |  |  |  |  | 59.1 |
|  |  |  |  |  |  |  | 1.62 | . 256 | 15.3 | 1.64 | . 259 | 15.5 | 6.18 | . 975 | 58.5 |
| 23 | 2.885 | 455 | 6.35 | 1.85 | . 291 | 17.5 | 1.57 | . 247 | 14.8 | 1.62 | . 255 | 15.3 | 6.02 | 949 |  |
| 24 | 3.142 | 496 | 6.35 | 11.82 | . 287 | 17.2 |  |  |  |  |  |  |  | . 949 | 57.9 |
|  |  |  |  |  |  |  | 1.52 | . 240 | 14.4 | 1.59 | . 251 | 15.0 | 5.86 | . 924 | 55.4 |
| 25 | 3.409 | 436 | 7.82 | 1.81 | . 232 | 13.9 | 1.49 | . 191 | 11.4 |  |  |  |  |  |  |
| 26 | 3.687 | 575 | 6.42 | 1.81 |  |  |  |  |  | 1.57 | . 201 | 12.0 | 5.69 | . 728 | 43.7 |
|  |  |  |  |  | . 282 | 16.9 | 1.45 | . 226 | 13.6 | 1.56 | . 243 | 14.6 | 5.57 | . 868 | 52.0 |
| 27 | 3.976 | 611 | 6.50 | 1.81 | . 279 | 16.7 | 1.44 |  |  |  |  |  |  |  |  |
| 28 | 4.276 | 647 |  |  |  |  |  |  |  | 1.56 | . 240 | 14.4 | 5.44 | . 837 | 50.2 |
|  |  |  | 6.61 | 1.77 | . 268 | 16.1 | 1.46 | . 221 | 13.2 | 1.56 | . 236 | 14.2 | 5.31 | . 803 |  |
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## Tractor Hauling Curve of

Maniminules per Soguare toot of Basal Area- D.B.H.
Beech, Vermont

Manminules per Square Foot of Basal Area- D.B.K.

Shidting Curve of
Man-minutes perSquare- Fool of Besal Area-D.B.H
Yellow Birch. Vermont
$700_{4}^{2}$ - $10{ }^{2} 5_{5}$
Man-minutes per
D. B.H.-inches

Tractor Hauling Curve of
Man minutes per Square fíoot of Basal Area D.B.H. Yellow Birch, Vermont


Figure 14

Milling Curve of
Man -minutes per Square Fool of Basal Area D.B.H.
Yellow Birch Vermont

Man-minutes per Square Foot of Basal Area.D.B.H.



Skidding Curves of
Man minutes per Square Foot of Basal Area -D.B.H. Sugar Maple, Vermont

Man -minutes per Square Foot of Basal Area- D.B. H.
Hauling Curves of
Man minutes per Square Foot of Basal Area -D.B.H. Sugar Maple, Vermont
Milling Curves of
Man-mmutes per Square foot of Basal Area-D.B.H. Sugar Maple Vermont
Man-minutes per Square Foot of Basal
Fëlling and Buching Curve of
Man-minuter per Sare fóot or Baval Area. D.B.H.
Yellow Birch, Northern Wisconsin



> Skidding Curve or
> Man minutes per Square Pot of Basal Area-D.B.H. Yellow Burch, Northern Wisconsin


> Loading and Hauling Curve of
> Manminules per Square Foot of Basal Area -D.B.L Yellow Birch, Northern Wisconsin

Fuelling and Bucking Curve of
Man-minules per Sure Pool or Basal Area D.B.H.
Sugar Maple, Northern Wisconsm
$H 8 O^{\circ}$
0


## Loading and Hauling Curve or <br> Man minutes per Square foot of Basal Area D.B.L. Sugar Maple, Northern Wisconsin



MiNna Curve of
Man-minuter per SQuare fool of Basal Area -D.B.H. Sugar Maple, Northern Wisconsin


> Felling and Bucking Curve of
> Man-minutes per Square Foot of Basal Area-D.BH. Basswood, Northern Wisconsin



Loading and Hauling Curve of
Man-minutes per Square föot of Basal Area-D.B.H. Basswood, Northern Wisconsin



> Fielling and Bucting Curve of
> Manminutesper Souare foot of Basal Area-D.B.H. E'lm-Northern Wisconsun
D.B.H.
 Man-minutes per Souare



Standeng Curve or
Manminules per Souare fäotor Bosal Area-D.B.H. Eilm-Northenn Wisconsin

Man-minutes per Souare Foot of Boal Arean $0 . B_{i} H$ H.


> Looding ond Hauling Curves of
> Man-minutes per Square FÖotol Basal Area-DBH Élm- WhorthernWisonsun



> Appendix D

Basal Area - Volume Conversion Formulae and Graphs



Conversion Formulae
Doyle Rule
10" to 21" diameters
$V=6.5 \mathrm{D} \mathrm{B} \mathrm{H}-33.3$
21" to $30^{\prime \prime}$ diameters
$V=1.39 \mathrm{DBH}+74$

Saribner Rule
10" to 18" aiameters
$V=5.9 \mathrm{DBH}+3$
18" to $30^{\prime \prime}$ diameters
$V=0.7$ D B H +96.5


## ACCOPRESS BINDEA

BD 2507 EMB
Manufactured By
ACCOPRODUCTS.Inc.
Ogdensburg, N. Y., U.S.A.

