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THREE-DIMENSIONAL OCCUPANT DYNAMICS SOFTWARE:
BELT MODEL USE

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<p>16. Abstract</p> <p>The University of Michigan Transportation Research Institute (UMTRI) conducted a study of seat belt modeling for use with the CAL 3-D crash victim simulation code. The objective was to examine the capabilities of existing software and to improve the codes insofar as possible. The work included:</p> <ul style="list-style-type: none"> - Implementation of the CAL 3-D (Version 20) at UMTRI - Study of the experimental basis for seat belt analytical modeling - Development of belt slip and submarining models using the existing code - Development and testing of an analytical basis and software for the transfer of belt material across body surfaces - Review of the status of the HARNESS sub-program 			
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1.0 INTRODUCTION

The University of Michigan Transportation Research Institute has conducted a study of seat belt modeling for use with three-dimensional crash victim simulation codes. The objective was to examine the capabilities of existing software and to improve the codes insofar as possible.

The restraint belt algorithm of the Calspan CVS, Version 20 (Fleck et al. 1981), defines a restraint belt in terms of two anchor points and a fixed point on the surface of a contact ellipsoid. The belt is presumed to lie entirely within the belt plane defined by these three points in space. The two anchor points are restricted to be attached to any one segment (usually the vehicle) while the contact ellipsoid, and along with it the fixed point, is restricted to be attached to any other segment (usually one of the body segments). Up to eight belts are allowed but each is totally independent of the other.

British Leyland developed a model for slipping between two belts for the case in which one anchor of one of the belts was coincident with one anchor of the other belt (Newman et al. 1981). Butler et al. (1980, 1983) developed a major new sub-program (HARNESS) which allowed both slipping of the belt over the surface of the occupant and penetration of the belt into the body.

General Motors Research Laboratories made modifications to the Version 20 code particularly in the area of problem size. The University of Michigan Transportation Research Institute reorganized the output sections to reduce the amount of storage required and simultaneously installed some of the output features from the updated version of Version 18A (Bennett et al. 1982).

The remainder of the report describes the work conducted during the project:

- Development of experimental basis for seat belt modeling
- Development of belt slip and submarining models using the existing codes

- Development and testing of an analytical basis for the transfer of belt material across body surfaces
- Review of the status of the HARNESS sub-program
- The UMTRI implementation of the CVS

2.0 BACKGROUND AND BASICS FOR SEAT BELT MODELING

2.1 Review of Impact Test Data

In order to understand the physical phenomena which should be incorporated in a model of seat belt interaction with a motor vehicle occupant during a crash, a review was conducted of impact test data. The two questions posed were:

1. Did the belt move or slip over the surface of the test subject; and,
2. Did the belt compress the chest structures during load application?

Two papers by Biomedical Science Department staff at the General Motors Research Laboratories were reviewed in this context. A Part 572 dummy was used in a study of test dummy interactions with a shoulder or lap belt by Viano and Culver (1981). These frontal impact tests were conducted with the thorax skin removed in order to better visualize the geometry of the interactions. The major phases of the dummy's interaction with the restraint system involved: "(1) forward movement of the dummy and take up of belt slack; (2) initial belt slip and adjustment to the thoracic structure; (3) inertial acceleration of the thorax with primarily planar thoracic compression; and, (4) substantial non-symmetric deformation of the thoracic structure as the chest rotates about the belt. . . ." An independent review of these movies revealed some slipping of the belt across the surface of the thorax during the loading phase. This was particularly marked where the lower portion of the shoulder belt interacted with the lower right side of the dummy's rib cage. Also, the stalk where the three-point attachment is routed to vehicle structures is observed to rotate.

Horsch (1980) reported a study of occupant dynamics as a function of impact angle and belt restraint. Tests were conducted at impact angles of 0, ± 30 , ± 45 , ± 60 , and ± 90 degrees. The test velocities were 35 km/hr. In "opposite side" impacts, the body escaped from under the

torso belt at 60 and 90 degrees but importantly it was noted that much of the impact energy had already been absorbed.

The observation of belt sliding across the surface of the Part 572 thorax in the frontal impacts caused consternation among the present researchers. The reason was that a foundation of the original Calspan 3-D CVS model was attachment of the belt at a fixed point on the thorax. Because of this a further review of test movies using Hybrid III dummies and cadavers was conducted. The data were obtained from the whole body response study, a major effort at UMTRI funded by General Motors and reported by Alem et al. (1977). The test buck was provided by General Motors and test velocities at 16, 22, and 33 mph were used. A schematic of the test setup is shown in Figure 2.1.

A quick look at the cadaver movies revealed what appears to be considerable slipping of the belt over the torso, perhaps 10 inches or more. In the eight side views of a low-level test (16 mph), there seemed to be some sliding of the torso belt as it penetrated down and into the lower right-hand side of the subject. From the left side, the belt slid over the shoulder. This apparent extensive amount of slipping occurred at the same time the belt appeared to be compressing the center of the torso. This was confirmed in a front view of the test. In this view, the belt appeared to slide a little bit initially as if the belt were using up slack while adjusting to the surface of the body before applying any significant loads. As the load was applied, there was a tremendous compression of the chest, during which time the belt was pocketed by the surrounding tissue. No slipping along the belt line was observed. Side slipping was virtually impossible because of the pocketing. It should be noted that the shoulder complex rotated around the thorax and belt to accentuate this effect. The same pattern of behavior was observed in the higher velocity impacts (22 and 33 mph).

The tests at UMTRI using the Hybrid III were conducted using General Motors equipment (test buck and dummies). Tests were reviewed at three velocities (16 mph, 22 mph, 33 mph). With respect to belt slipping, the results were similar to those observed in the cadaver tests. The major difference was the lack of shoulder complex forward

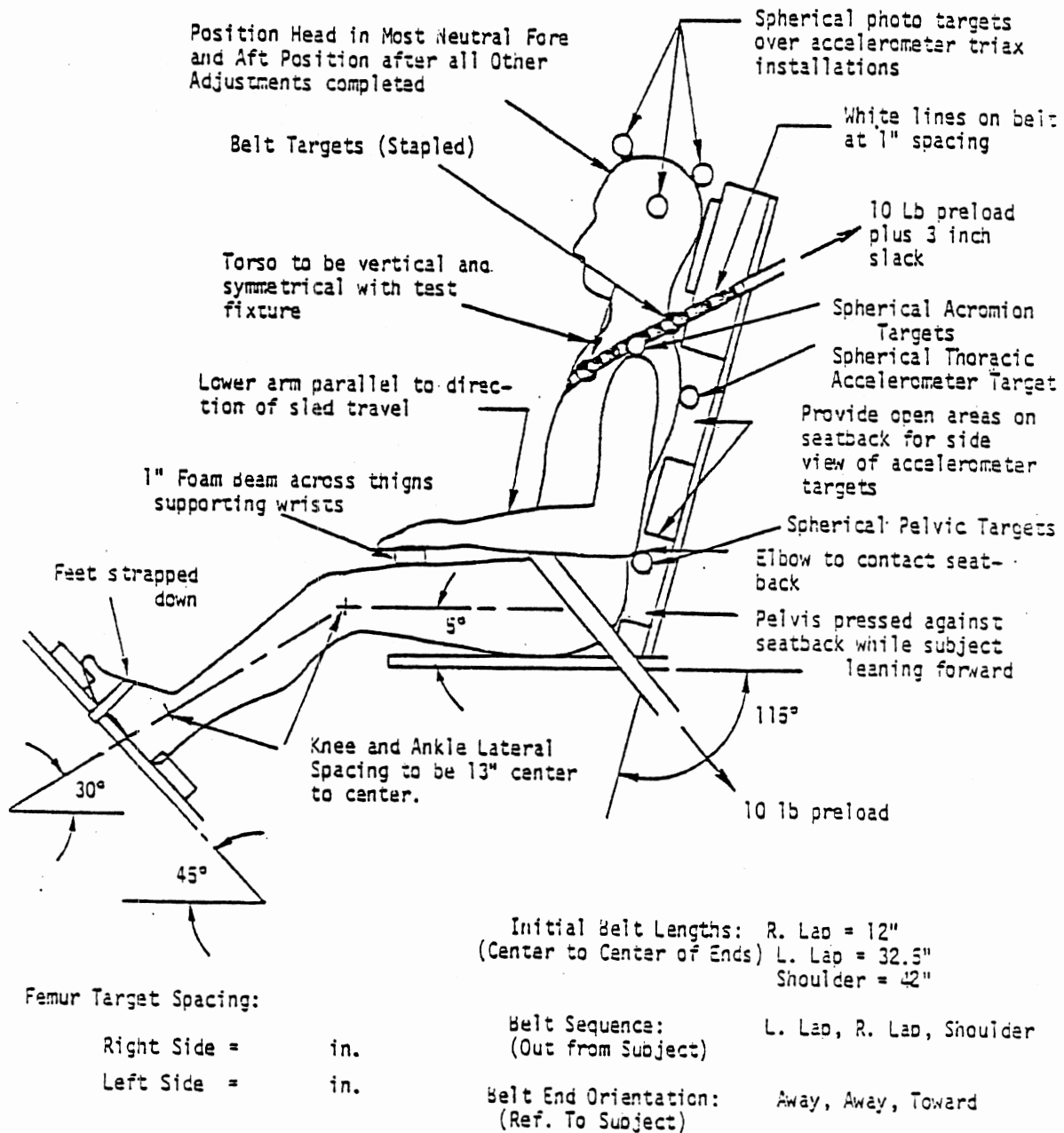


Figure 2.1. Schematic of Test Setup

rotation and the general apparent excessive stiffness of the thoracic structure and spine. Some chest compression was observed.

In conclusion, the following observations can be made in answer to the questions posed at the beginning of this section.

1. Most of the slippage of the belt over the surface of the subject was observed to occur in the initial phase of the test in order to take up slack which may exist in any of the belt segments.

2. Apparent slippage is observed in the upper and lower torso belt segments as body loads are applied. This is primarily the result of thorax compression and, to a lesser extent, belt stretch.

3. During application of a frontal impact load to a subject having a well-positioned belt system, it appears that there is no slippage for one point on the thorax.

4. While the belt interaction with Hybrid III and cadaver test subjects are similar, the Hybrid II response appears to be rather different.

2.2 Limitations of Existing BELT Code

In the BELT subprogram, each of the restraint belts is assumed to lie in a plane defined by two anchor points attached to a segment (usually the vehicle) and by a fixed point on a contact ellipsoid rigidly attached to some other segment (see Figure 2.2). The calculation of the belt length from the fixed point to the two anchor points is done separately. The friction of the contact between the belt and the segment ellipsoid may be assumed to be either zero or infinite. In the zero friction option the total belt length is used to compute the strain and a single force-strain history is used to determine the force which is applied equally at each of the tangent points. In the infinite friction option each of the partial belt lengths (one from the fixed point to anchor point A and the other from the fixed point to anchor point B) are treated independently. Separate force-strain histories are carried for each part resulting in different forces. It is assumed that the force-strain functions are defined in such a manner as to account for deformation of the contact ellipsoid.

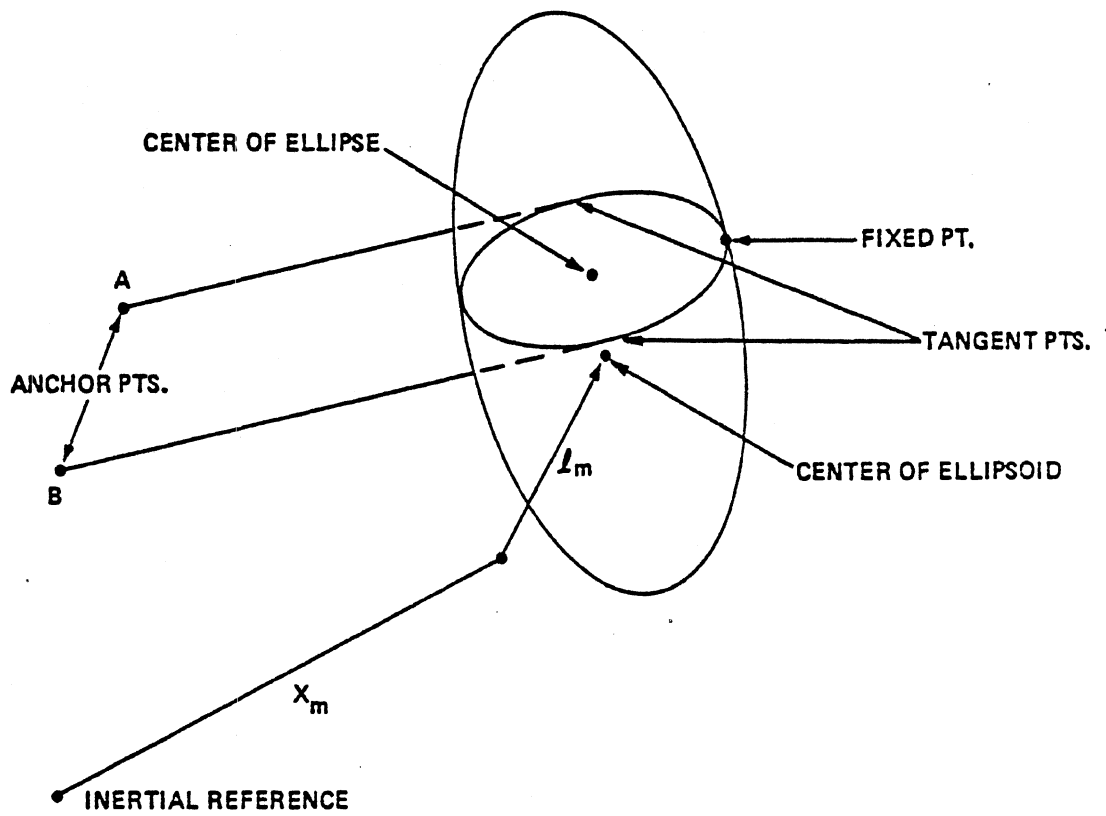


Figure 2.2. Restraint Belt Geometry

Based on the observations put forth in Section 2.1, the BELT code is deficient in three ways:

1. There is no capability to transfer material from one side of the belt segment to the other. The only mechanism is force equalization which, rather than feeding slack material from one side to the other, computes the average of the non-zero force on one side with the zero force on the slack side. Based on the observation of adjustment of the belt to fit the shape of the occupant just discussed in Section 2.1, this assumption is inadequate.

2. It is not possible to model a three-point belt. In other words, it is not possible to connect two belts, such as those defined in Figure 2.2, together in order to represent the torso and lap sections of a seat belt assembly. Even if this were possible, the rotation of the stalk attached to the D-ring could not be represented.

3. It is not possible to allow migration of the fixed point on the segment ellipsoid. Although this assumption appears to be good for frontal impact (in the case where there is little transfer of slack belt material), it is not valid for opposite side lateral or oblique impacts where the occupant can slip completely out of the belt.

3.0 BELT SLIP AND SUBMARINING MODELS USING EXISTING CODES

This section of the report discusses the use of the original BELT software to simulate sliding of the belt over body surfaces and penetration of the belt into body surfaces during dynamic loading. Section 3.1 shows the modeling differences between applications to various conceptual problems. Section 3.2 summarizes various simple restraint models and their effectiveness. Section 3.3 presents a full-scale example of a submarining model which appears to work well and which should be laboratory tested for general use.

3.1 Sequence of Seat Belt Model Development

Figure 3.1 is a schematic which shows a variety of modeling concepts including:

- Current BELT code
- Modifications to the code generated by British Leyland
- Further new modifications by UMTRI, made during the present project, suggested for complete implementation

The two drawings in the upper-left section of the figure represent the current state. The two ends of any belt segment are fixed to the vehicle. The belt itself is constrained to conform to an ellipsoid attached to the occupant. This belt is rigidly attached to a point on the surface of the ellipsoid. The forces in the two separate elements of the belt can either be equalized or totally independent. To model a three-point belt system, two independent sets of belts must be used. Each of the four belt ends is fixed independently to the vehicle and each pair has a fixed attachment to a body ellipsoid. This concept is most relevant to the older four-point belt system.

The modifications made to the BELT code by British Leyland (Newman et al. 1981) have the effect illustrated in the upper right portion of Figure 3.1. This allows the transfer of material between pairs of belts and is intended to represent this effect at the D-ring. However, no slippage across the occupant is allowed as the fixed points on the ellipsoid surfaces are still required.

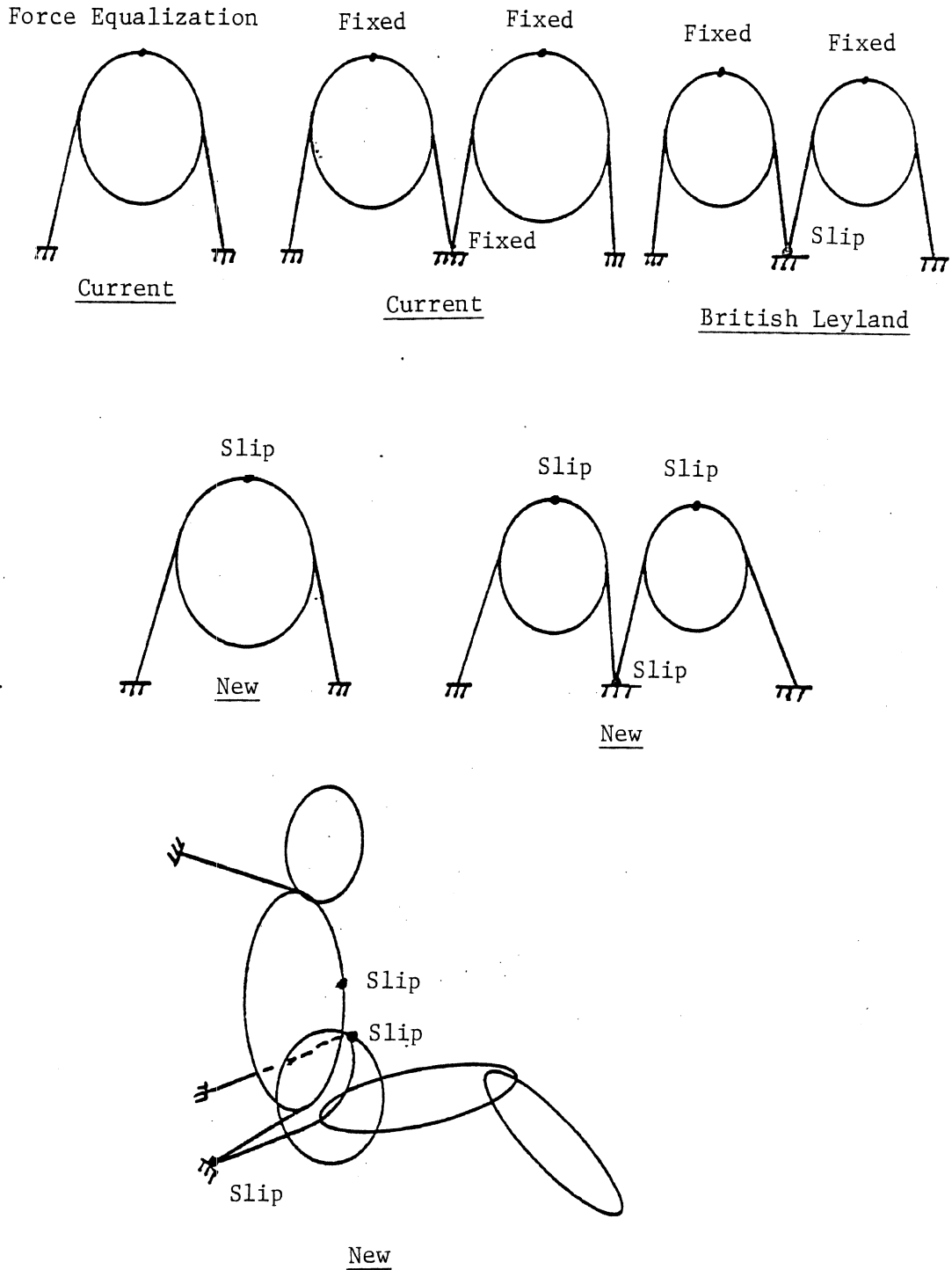


Figure 3.1. Sequence of Belt Models

The new UMTRI concepts, implemented and tested at the subroutine level, but not yet integrated into the CAL 3-D code, are illustrated in the bottom three drawings in Figure 3.1. In these cases, slipping of material is allowed across slip points which are rigidly attached to the surface of body ellipsoids, as before. Further, slipping can occur at the point where pairs of belts are connected, as is the case with the British Leyland improvements. Because of this general capability to slip, or transfer material, between all the belt segments, the take-up of initial slack discussed in Section 2 of this report is accommodated. The potential application to the three-point belt system is shown in the bottom section of Figure 3.1. It should be noted, however, that mobility of the stalk into which the D-ring is inserted is not accommodated.

More advanced belt modeling concepts are discussed in Section 5 where the HARNESS sub-program is described.

3.2 Test Cases Using Various Simple Concepts

Simple modeling concepts have been used to study various potential methods of simulating belt slip and submarining. The first of these, shown in Figure 3.2, is intended to demonstrate slipping of a belt either over the thorax or lower torso pelvic region. The mass and geometry of the spherical shaped segment is intended to represent the thorax restrained by an upper torso belt, as shown. A contact surface below the sphere represents the interaction of the lower portion of the body with seat structures. The sphere can slide on, and penetrate, the surface.

To represent slipping of the belt over this surface, a second mass (10% of the first mass) was superimposed and pin-jointed at their mutual centers-of-mass. The belt was attached to the second, and smaller, mass. In order to simulate resistance to the slipping, a moment resistance is added at the pin joint as a function of the relative angle between the two masses.

This modeling concept appeared to function properly. It worked especially well when some resistance to the motion between the two segments was added. Because of the ability to control the slipping over

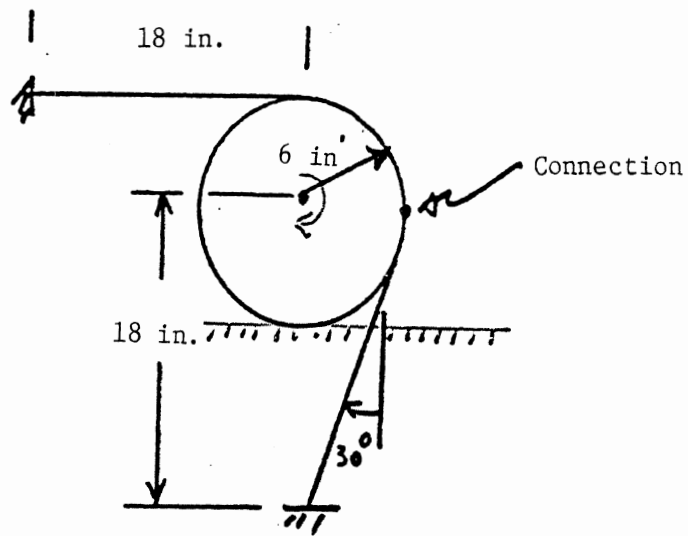


Figure 3.2. Superimposed Segments for Representation of Slip

a surface in this manner, it was felt that this model concept could be adapted to use as a submarining indicator.

A second series of simple modeling concepts was explored based on the geometry of Figure 3.3. As before, a spherical mass was used to simulate the thorax or lower torso region. The general placement of belt attachments to the vehicle was also as before. In these cases, however, a second mass (small) was located at the point where the belt would pass over the primary body segment. The belt was then attached to a separate ellipsoid on this new small mass.

Three options available with the CAL 3-D were tested as means of attachment of the small mass to the larger primary mass to simulate slippage between the two. These were the fixed distance constraint, the fixed point constraint, and the massless link. The fixed distance constraint is designed to keep a point on one mass a fixed distance from a point on the other. The fixed point constraint is intended to keep a point on one mass at the same point in inertial space as a point on the other mass. These constraints are approximate and use force to maintain the geometry rather than changing the number of degrees of freedom.

The two constraint concepts exhibited problems with instability due to a trading of energy and oscillation from one side of the belt to the other. The only way to damp this behavior was to alter the belt properties. This was considered a poor method because alterations to damp this spurious behavior would also affect the primary properties of the belt which are to stop the forward motion of the primary mass.

The massless link idea does alter the equations of motion. This concept appears to be sound based on the work of Fleck et al. (1975) and Wittenberg (1977). However, in practice, the software did not work.

A final attempt to use the geometric ideas of Figure 3.3 was to employ the traditionally jointed superimposed masses of Figure 3.2. As was the case with the original Figure 3.2 models already described, this concept worked well. It was possible to control the motion of the forward mass. These controls could be based on test data defining the direction and magnitude of forces associated with movement of the belt over the pelvis. These data could be represented as a torque-angle

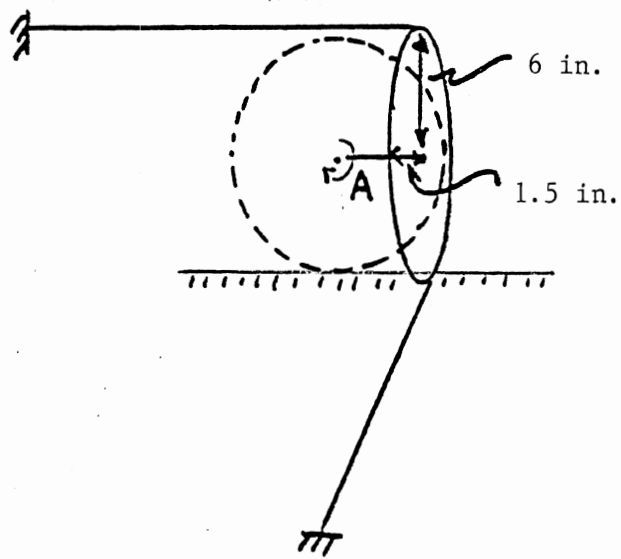


Figure 3.3. Attachment of Belt to Mass which Moves Relative to Primary Segment

curve. Because of the promise of this technique, the full-scale exercise discussed in Section 3.3 was conducted.

3.3 Full-Scale Testing of Submarining Model

A basic data set provided by General Motors was modified to include a prototype lap belt submarining indicator. Figure 3.4 is a schematic of this data set at the initial time. An overlay of the general shape of the pelvis is included to show the orientation of the lap belts. They are well positioned initially to take crash loading. The pelvic overlay is based on the positions specified in the data set of the joints connecting the pelvis to the spine and the femurs. The point labelled with an "X" on the front of the ellipsoid representing the lower torso is the attachment point for the two elements in the lower torso belt.

The data structure for the submarining indicator is based on the concept described in Section 3.3 where two masses are superimposed at a pinned joint. The small mass, representing a portion of the pelvic mass, is attached to the belt while the primary pelvic mass is attached normally to the remainder of the body linkage. The two masses are connected at a pinned joint which resists relative rotation by the mechanism of a torque-angle resistance.

Table 3.1 is the input data set for the full-scale submarining model using the UMTRI version of the CAL 3-D. Each line in the data file has a number. Those which define changes for the implementation of the submarining indicator are as follows:

Line 24.5. B2 Card. This defines the mass, inertial, and ellipsoid properties of the overlaid mass, named BPEL.

Line 56.1, 56.2. B3 Cards. The attachment of BPEL to the lower torso mass, LT, is defined.

Line 80.1. B4 Card. The torque-angle resistance of the mass to which the belt is attached (BPEL) with respect to the primary mass (LT) is defined. Values have been selected without the aid of experimental information. They are consistent with other properties of the dummy.

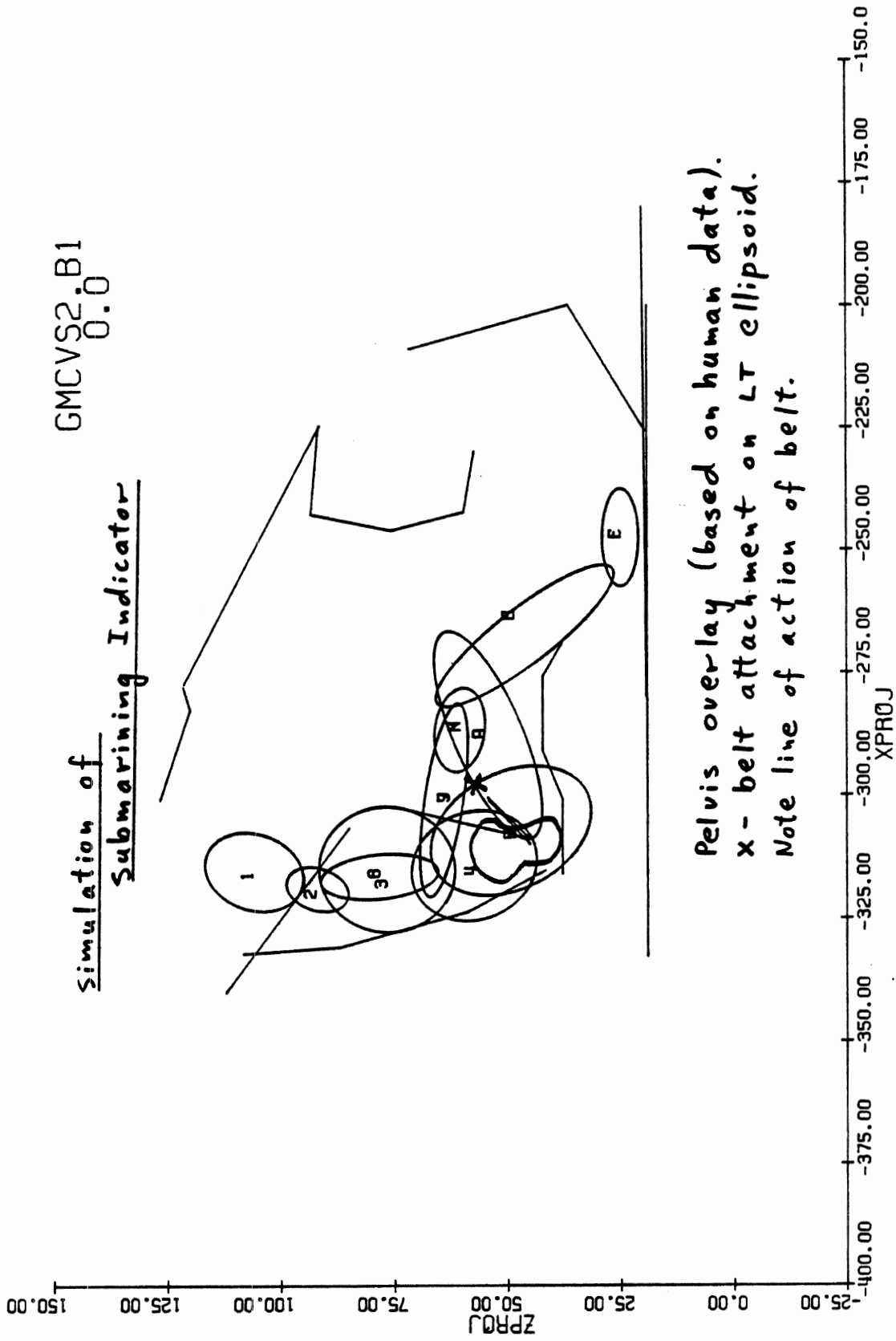


Figure 3.4. Simulation of Submarining Indicator (t = 0 ms)

17

1	04 NOV 1983																			
2	TRIAL DATASET FOR SEAT BELT GRAPHICS ALGORITHM																			
3	RESTR PASSR,FRONTAL BARRIER IMPACT, NO PITCH																			
4	CM. KG.SEC.	0.0	0.0	980.66																
5	6 150 0.00100 0.00025 0.001 0.00025																			
6	00 005 0 0 0 0 000 0 0 0 00000 0 1																			
7	18 17 GM HYB3 50 R10.27.82																			
8	LT 517.331 2.479 2.479 1.468 12.00 12.50 18.50 1.70 0.000 -.350																			
9	CT 4 5.760 .3650 .3650 .2790 11.00 11.00 14.00 1.660 0.000 0.000																			
10	UT 317.227 2.504 2.504 2.170 12.75 12.75 15.00 3.610 0.000 0.000																			
11	N 2 1.545 0.060 0.060 0.006 4.30 4.30 7.00 1.670 .0000 0.000																			
12	H 1 4.545 .2190 .2060 .2060 7.75 7.75 11.00 1.500 .0000 0.000																			
13	LUL A 6.091 .6860 .6860 .1310 7.50 7.50 23.10 -0.94 .0000 .0000																			
14	LLL B 3.300 .7650 .7650 .0970 5.75 5.75 23.70 -4.22 .0000 .0000																			
15	LF C 1.227 .0550 .0550 .0150 4.00 4.00 10.00 .0000 .0000 .0000																			
16	RUL D 6.091 .6860 .6860 .1310 7.50 7.50 23.10 -.940 .0000 .0000																			
17	RLL E 3.300 .7650 .7650 .0970 5.75 5.75 23.70 -4.22 .0000 .0000																			
18	RF F 1.227 .0550 .0550 .0150 4.00 4.00 10.00 .0000 .0000 .0000																			
19	LUA 6 2.000 .1160 .1160 .0250 4.50 4.50 13.00 0000 .000 .0000																			
20	LLA 7 2.273 .3600 .3600 .0320 4.25 4.25 20.80 1.15 .0000 .0000																			
21	RUA 8 2.000 .1160 .1160 .0250 4.50 4.50 13.00 .0000 0.00 .0000																			
22	RLA 9 2.273 .3600 .3600 .0320 4.25 4.25 20.80 1.15 .0000 .0000																			
23	LH N 0.800 .0115 .0115 .0012 5.50 3.05 9.00 .000 .000 .0000																			
24	RH M 0.80 .0115 .0115 .0012 5.50 3.05 9.00 .000 .000 .0000																			
24.5	BP EL P4.	2.479 2.479 1.468 12.			12.5 18.5 1.7 0.															
25	P O 1 -2 -4.25			-4.32		.0000 6.53														
26		0.0 0.0 0.0		0.0 0.0 0.0		0.0 0.0 0.0														
27	W P 2 -2 -1.60			-6.48		.0000 13.93														
28		0.0 0.0 0.0		0.0 0.0 0.0		0.0 0.0 0.0														
29	NP Q 3 -2 -2.54			-15.59		.0000 .0000														
30																				
31	HP R 4 -2 0.000			-9.59		.0000 4.780														
32																				
33	LH W 1 -4 -2.45 -8.85 2.57			0.0 .0000-23.99																
34		-90. 90.		4.76		27.0 -70.0														
35	LK X 6 1 0.00 .0000 16.18			0.0 .0000-16.36																
36				43.0																
37	LA G 7 -4-0.250 .0000 22.04			5.36 .0000 -4.09																
38		90.		90.		79.0														
39	RH Y 1 -4 -2.45 8.85 2.57			0.00.0000-23.99																
40		90. 90.		4.76		-27. 70.														
41	RK Z 9 1 0.0 .0000 16.18			0.0 .0000-16.36																
42				43.0																
43	RA H 10 -4-0.250 .0000 22.04			5.36 .0000 -4.09																
44		90.		90.		79.0														
45	LS S 3 -4 0.45-18.00-14.59			0.0 .0000-13.06																
46				90.		-55. -65.														
47	LE T 12 -4 0.0 .0000 13.07			0.0 .0000-15.11																
48		90.0		90.		8.0 70.														
49	RS U 3 -4 0.45 18.00-14.59			0.0 .0000-13.06																
50				-90.		55.0 65.														
51	RE V 14 -4 0.0 .0000 13.07			0.0 .0000-15.11																
52		90.		90.		-8. 70.														
53	LW J 13 1 0.0 .0000 10.20			0.0 .0000 -5.11																
54		0.0 .0000		-10. 00.0																
55	RW K 15 1 0.0 .0000 10.20			0.0 .0000 -5.11																
56		0.0 .0000		-10. 00.0																
56.1	PELJ P 1 10. 0. 0. 0. 0. 0. 0.																			

Table 3.1. Input Data Set for Full-scale Submarining Model (Page 1 of 10)

56.2																						
57	115.8	0.000	2000	0.500	90.000					115.8	.0000	.2000	0.500	70.000								
58	115.8	0.500	90.000							115.8	.000	0.200	0.5	70.0								
59	30.0	.108	.0000	0.500	60.000					150.	.108	.0000	0.500	60.000								
60	30.0	.108	.0000	0.500	60.000					150.	.108	.0000	0.500	60.000								
61	6.000	.2500	.0000	0.500	10.000					2.972	.1088	0.000	0.500	100.00								
62	16.0	160.	160.	0.5	60.0					0.	-90.0	0.0										
63	0.00	10.00	10.0	0.950	45.000					0.000	.000	0.000	0.950									
64	1.00	10.00	10.00	0.950	50.000					1.0	10.0	10.	0.950	42.								
65	0.	0.																				
66	6.000	.2500	.0000	0.500	10.000					2.972	.1088	0.000	.500	100.								
67	16.0	160.	160.0	.5	60.0					0.0	0.											
68	10.00	10.00	10.00	0.950	45.000								0.950	0.000								
69	1.00	10.00	10.00	0.950	50.000					1.0	10.0	10.	0.950	42.								
70	0.	0.																				
71	14.	00.0	00.0	0.950	125.00								0.950	60.0								
72	0.	0.																				
73	20.0	20.0	20.0	0.950	45.000								0.950	70.000								
74	0.	0.																				
75	14.	00.0	00.0	0.950	125.00								0.950	60.0								
76	0.	0.	00.0																			
77	20.0	20.0	20.0	0.950	45.000								0.950	70.00								
78	0.	0.																				
79	14.	20.	0.	.5	60.					14.	20.	0.	.5	60.								
80	14.	20.	0.	.5	60.					14.	20.	0.	.5	60.								
80.1	50.	10.	10.	.95	30.																	
81	0.0	1000.	200.0	174.5	.0								0.0	0.0								
82	0.0	1000.	200.0	105.0	.0								0.0	0.0								
83	0.0	20.0	200.0	174.5	.0								0.0	0.0								
84	0.0	20.0	200.0	180.9	.0								0.0	0.0								
85	0.0	500.0	200.0	180.9	.0								0.0	0.0								
86	0.0	500.0	200.0	180.9	.0								0.0	0.0								
87	0.0	500.0	200.0	180.9	.0								0.0	0.0								
88	0.0	125.0	10.0	15.4	.0								0.0	0.0								
89	0.0	20.0	10.0	30.	.0								0.0	0.0								
90	0.0	20.0	10.0	30.	.0								0.0	0.0								
91	0.0	0.0	10.0																			
92	0.0	500.0	200.0	180.9	0.0								0.0	0.0								
93	0.0	500.0	200.0	180.9	0.0								0.0	0.0								
94	0.0	500.0	200.0	180.9	0.0								0.0	0.0								
95	0.0	125.0	10.0	15.4	.0								0.0	0.0								
96	0.0	20.0	10.0	30.	.0								0.0	0.0								
97	0.0	20.0	10.0	30.	.0								0.0	0.0								
98	0.0	0.0	10.0																			
99	0.0	125.0	400.0	65.0	0.0								0.0	0.0								
100	0.0	50.0	400.0	65.0																		
101	0.0	0.0	400.0	0.0																		
102	0.0	175.0	100.0	16.3	0.0								0.0	0.0								
103	0.0	175.0	100.0	16.3																		
104	0.0	0.0	100.0																			
105	0.0	120.0	400.0	65.0	0.0								0.0	0.0								
106	0.0	50.0	400.0	65.0																		
107	0.0	0.0	400.0	0.0																		
108	0.0	175.0	100.0	16.3	0.0								0.0	0.0								
109	0.0	175.0	100.0	16.3																		
110	0.0	0.0	100.0																			
111	.1	50.	100.	25.	0.																	
112	.1	50.	100.	25.	0.																	

112.1	0.	50.	50.	50.	0.								
113						00.1	00.10	00.10	00.01	00.01	00.01		
114						00.1	00.10	00.1					
115						00.1	00.10	00.10					
116						00.1	00.10	00.10					
117						00.1	00.10	00.10					
118						00.1	00.10	00.10					
119						00.1	00.10	00.10					
120						00.1	00.10	00.10					
121						00.1	00.10	00.10					
122						00.1	00.10	00.10					
123						00.1	00.10	00.10					
124						00.1	00.10	00.10					
125						00.1	00.1	00.1					
126						00.1	00.1	00.1					
127						00.1	00.1	00.1					
128						00.1	00.1	00.1					
129						00.1	00.1	00.1					
129.1						.1	.1	.1					
130													
131	0.0	0.0	0.0	1369.	0.000	0.0	0.0	0.0	59	0.0	0.002		00
132	0.0	0.0	1.0	7.0	17.0	19.0	18.0	12.5	8.5	5.0	2.0	22.5	
133	27.5	15.0	18.0	20.5	37.0	33.0	22.5	14.5	15.5	20.0	22.0	25.0	
134	23.0	25.5	26.0	25.5	22.5	21.5	21.0	25.0	24.0	23.0	22.0	20.0	
135	17.0	15.0	12.5	10.5	10.0	10.0	7.5	5.0	1.0	0.0	-3.0	-3.0	
136	-2.5	-2.0	-2.0	-1.5	-1.0	-0.5	0.0	0.0	0.0	0.0	0.0	0.0	
137	23	2	0	0									
138	1												
139	-224.8		50.0										
140	-277.5		50.0										
141	-224.8		-50.0										
142	2												
143	-200.1		50.0										
144	-209.2		50.0										
145	-200.1		-50.0										
146	3												
147	-230.0		50.										
148	-242.4		50.										
149	-230.0		-50.										
150	4												
151	-242.4		50.										
152	-246.2		50.										
153	-242.4		-50.										
154	5												
155	-246.2		50.										
156	-242.9		50.										
157	-246.2		-50.										
158	6												
159	-323.8		20.0										
160	-315.3		20.0										
161	-323.8		-20.0										
162	7												
163	-330.9		20.0										
164	-323.8		20.0										
165	-330.9		-20.0										
166	8												
167	-316.0		25.0										
168	-301.0		25.0										

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Table 3.1. Input Data Set for Full-Scale Model (Page 3 of 10)

169	-316.0	-25.0	-37.72
170	9	FLOORBOARD	
171	-280.	50.0	-19.2
172	-180.0	50.0	-20.1
173	-280.	-50.0	-19.2
174	10	TOEBOARD	
175	-225.8	50.0	-19.5
176	-200.1	50.0	-36.4
177	-225.8	-50.0	-19.50
178	11	UPPER I.P.	
179	-242.9	50.0	-93.1
180	-224.8	50.0	-91.4
181	-242.9	-50.	-93.1
182	12	FRONT SEAT BACK3	
183	-332.2	20.0	-108.12
184	-330.9	20.0	-86.72
185	-332.2	-20.0	-108.12
186	13	LOWER I.P.	
187	-242.4	50.	-59.5
188	-246.2	50.	-75.5
189	-242.4	-50.	-59.5
190	14	MID I.P.	
191	-246.2	50.	-75.5
192	-242.9	50.	-93.1
193	-246.2	-50.	-75.5
194	15	FR SEAT CUSHION2	
195	-301.0	25.0	-37.72
196	-291.0	25.0	-42.12
197	-301.0	-25.0	-37.72
198	16	FR SEAT CUSHION3	
199	-291.0	25.0	-42.12
200	-276.0	25.0	-42.12
201	-291.0	-25.0	-42.12
202	17	FR SEAT CUSHION4	
203	-276.0	25.0	-42.12
204	-268.9	25.0	-37.72
205	-276.0	-25.0	-42.12
206	18	SILL	
207	-332.8	50.0	-19.0
208	-200.1	50.0	-19.0
209	-332.8	-50.0	-19.00
210	19	ROOF PANEL 1	
211	-282.6	50.0	-119.8
212	-277.9	50.0	-121.3
213	-282.6	-50.0	-119.8
214	20	ROOF PANEL 2	
215	-282.6	50.	-119.8
216	-301.0	50.	-126.5
217	-282.6	-50.	-119.8
218	21	BOTTOM I.P.	
219	-230.0	50.	-57.2
220	-242.4	50.	-59.5
221	-230.0	-50.	-57.2
222	22	LOWER I.P.	
223	-242.4	50.	-59.5
224	-246.2	50.	-75.5
225	-242.4	-50.	-59.5
226	23	MID I.P.	

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Table 3.1. Input Data Set for Full-scale Submarining Model (Page 4 of 10)

227	-246.2	50.	-75.5				
228	-242.9	50.	-93.1				
229	-246.2	-50.	-75.5				
230	LAP BELT						
231	-310.	-20.00	-45.00	-309.	21.00	-45.00	
232	12.0		-4.000		0.010		
233	SHOULDER BELT						
234	-340.0	-24.	-112.	-309.	21.00	-45.	
235	11.9	0.000	1.0000.		1.000		
236							
237	1 HEADREST FORCE(KG)		0.0		0.0		
238	0.0	-15.					
239	4						
240	0.0	0.0	5.0	100.	10.0	200.	
241	15.0	300.					
242	2 SEAT CUSHION FORCE(KG)						
243	0.0	-14.	0.0	1.0			
244	8						
245	0.0	0.0	2.0	20.	4.0	45.	
246	6.0	80.	8.0	130.	10.0	200.	
247	12.0	300.	14.0	450.			
248	3 SEATBACK FORCE(KG)						
249	0.0	-16.	0.0	1.0			
250	8						
251	0.0	0.0	1.0	7.5	2.	20.	
252	3.	50.	4.	90.	6.	200.	
253	10.	500.	16.	1000.			
254	4 TOE BRD FORCE(KG)						
255	0.0	-10.		1.0			
256	18						
257	0.0	0.0	0.1	14.0	0.2	22.	
258	0.3	40.	0.4	56.	0.5	74.	
259	0.6	95.	0.7	115.	0.8	145.	
260	1.0	150.	2.0	240.	3.0	300.	
261	4.0	350.	5.0	500.	6.0	900.	
262	7.0	1300.	9.0	1650.	10.0	1800.	
263	5 WND SHLD R FUNCTION						
264	0.0	-20.	0.0				
265	4						
266	0.0	1.0	2.0	0.5	9.0	0.25	
267	20.	0.0					
268	6 WND SHLD G FUNCTION						
269	0.0	-20.	0.0				
270	4						
271	0.0	0.0	2.0	.75	9.0	0.95	
272	20.	0.95					
273	8 MID I.P. LOADING(KG)						
274	0.0	-20.	0.		0.0		
275	9						
276	0.0	0.0	1.0	1200.	1.5	1620.	
277	2.	1800.	2.5	1860.	3.0	1910.	
278	4.	2010.	6.0	2055.	20.	2160.	
279	9 CONSTANT F=0.40						
280	0.0	0.0	0.40				
281	10 CONSTANT F=0.1						
282	0.0	0.0	0.1				
283	11 UPP I.P. LOAD(KG)						
284	0.0	-24.	0.0		1.0		

Table 3.1. Input Data Set for Full-scale Submarining Model (Page 5 of 10)

285	7	0.0	0.0	3.0	80.	6.	120.
286	9.	240.	12.	18.	560.		1150.
288	24.	1800.					
289	12	CONSTANT F=0.9					
290	13	TOEBRD F	0.9				
292	14	CONSTANT F=0.95	0.95				
293	14	CONSTANT F=0.67	0.67				
294	15	UNLOADING G FUNCTION	0.0				
296	4	-1000.	0.0				
297	4	0.0	0.5	0.6	0.0	0.95	
298	1000.	0.95					
299	16	UNLOADING R FUNCTION					
300	16	-1000.	0.0				
301	4	1.0	0.5	0.6	1.0	0.05	
302	4	0.05					
303	1000.	0.05					
304	17	WINDSHLD FORCE(KG)	0.0				
305	17	-20.	1.0				
306	16	0.0	0.0	1.0			
307	16	0.0	1.	2.	70.		110.
308	3.	145.	4.	5.	170.		182.
309	6.	188.	7.	8.	190.		189.
310	9.	176.	10.	11.	166.		153.
311	12.	130.	13.	15.	90.		0.
312	20.	0.					
313	18	WSHLD SPIKE(KG)					
314	13	-2.5	0.0	1.0	1.5		
315	13	0.0	0.4	0.5	60.		120.
316	0.0	0.0	0.9	1.0	190.		200.
317	0.7	160.	1.4	1.5	160.		130.
318	1.2	190.	2.0	2.2	40.		20.
319	1.7	80.					
320	2.5	0.					
321	19	LWR IP LOAD(KG)					
322	17	-40.	0.0	0.0			
323	0.0	0.0	1.	2.	20.		50.
324	3.	100.	4.	5.	200.		300.
325	6.	400.	7.	8.	485.		495.
326	11.	525.	13.	15.	550.		600.
327	17.	700.	19.	20.	900.		1070.
328	21.	1300.	40.5		160000.		
329	20	HEADER LOAD(KG)					
330	6	-40.	0.0	0.0			
331	6	0.0	5.08	7.62	445.		980.
332	12.7	980.	20.3	40.5	2225.		16000.
333	21	TOEBRD G					
334	8	-10.	0.0	0.0			
335	8	0.0	0.2	0.4	0.05		0.13
336	0.65	0.22	1.50	2.20	0.55		0.80
337	2.8	0.92	10.0		0.99		
338	22	TOEBRD R					
339	8	0.0					
340	0.65	0.22	1.50	2.20	0.55		0.80
341	2.8	0.92	10.0		0.99		
342	22	TOEBRD R					

Table 3.1. Input Data Set for Full-scale Submerging Model (Page 6 of 10)

Listing of GMCVS2.B1 at 03:24:15 on JAN 31, 1986 for CC1d=SU33

343	0.0	-10.	0.0	0.0	0.0	0.0	0.0	0.0	0.0
344	8								
345	0.0	0.0	0.2	0.47	0.4	0.4	0.37		
346	0.65	0.31	1.50	0.26	2.20	2.20	0.24		
347	2.8	0.22	10.0	0.01					
348	23	WINDSHLD F							
349	0.0	10.0							
350	0.76	0.156	0.0						
351	24	ROOF PAN F							
352	0.0	0.0	0.80						
353	25	SEAT F							
354	0.0	10.0							
355	0.30	0.1	0.0						
356	26	BODY FORCES(KG)							
357	0.0	-4.5	0.0		1.0				
358	6								
359	0.0	0.0	0.4	1.	1.0		2.		
360	1.5	3.	2.0	4.	4.5		6.		
361	27	LAP BELT FDF							
362	0.0	-1.50							
363	5								
364	0.00	0.0	.125	70.0	.254		400.		
365	1.25	800.0	1.50	800.0					
366	28	SHOULDER BELT FDF							
367	0.0	-1.25							
368	5								
369	0.00	0.0	.0254	44.0	0.25		800.0		
370	0.950	900.0	1.25	900.0					
371	29	BELT R							
372	0.0	0.0	0.750						
373	30	BELT G							
374	0.0	0.0	0.150						
375	31	BELT CF							
376			1.0						
377	32	BELT SEGMENT CF							
378			1.0	0.0	0.5				
379	33	TIE POINT CF							
380			0.5	0.	0.5				
381	999								
382	1	2	5	3	1	2	4	4	3
383	1	2	2	2	1	2	2	3	1
384	1	5	5	17	18	5	6	23	
385	2	19	5	11	16	15	24		
386	3	19	7	19	0	16	15	12	
387	3	19	10	19	0	16	15	12	
388	4	19	6	19	0	16	15	12	
389	4	19	7	19	0	16	15	9	
390	4	19	9	19	0	16	15	9	
391	4	19	10	19	0	16	15	9	
392	4	19	1	8	16	15	12		
393	5	19	1	8	0	16	15	12	
394	5	19	2	8	0	16	15	12	
395	5	19	3	8	0	16	15	12	
396	5	19	13	19	16	15	12		
397	5	19	15	19	16	15	12		
398	6	19	1	3	0	16	15	10	
399	6	19	2	3	0	16	15	10	
400	6	19	3	3	16	15	10		

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401	7	19	1	1	3		16	15	10										
402	7	19	2	2	3	0	16	15	10										
403	7	19	3	3	3	0	16	15	14										
404	8	19	1	1	2		16	15	25										
405	9	19	8	8	4		22	21	13										
406	9	19	11	11	4	0	22	21	13										
407	10	19	8	8	4		22	21	13										
408	10	19	11	11	4		22	21	13										
409	11	19	5	5	11		16	15	10										
410	11	19	3	3	11		16	15	10										
411	12	19	5	5	1		16	15	10										
412	12	19	1	1	2		16	15	25										
413	12	19	2	2	2		16	15	25										
414	12	19	3	3	2		16	15	25										
415	13	19	12	12	19		16	15	12										
416	13	19	14	14	19		16	15	12										
417	13	19	13	13	19		16	15	12										
418	13	19	15	15	19		16	15	12										
419	14	19	12	12	19		16	15	12										
420	14	19	14	14	19		16	15	12										
421	15	19	1	1	2		16	15	25										
422	15	19	6	6	2		16	15	25										
423	15	19	9	9	2		16	15	25										
424	16	19	1	1	2		16	15	25										
425	16	19	6	6	2		16	15	10										
426	16	19	9	9	2		16	15	10										
427	17	19	1	1	2		16	15	10										
428	19	19	5	5	10		16	15	24										
429	20	19	5	5	20		16	15	24										
430	21	19	6	6	19		16	15	24										
431	21	19	9	9	19		16	15	24										
432	22	19	17	17	19		16	15	10										
433	22	19	16	16	19		16	15	10										
434	23	19	16	16	19		16	15	10										
435	23	19	17	17	19		16	15	10										
436	1	1																	
437	1	19	18	18	27		29	30	31										
438	2	19	3	3	28		29	30	31										
439	2	2	4	4	0	1	0	0	1	0	0	5	3	3	1	0	0	0	
440	1	1	13	13	4		16	15	10										
441	1	1	15	15	4		16	15	10										
442	2	2	16	16	26		16	15	10										
443	2	2	17	17	26		16	15	10										
444	3	3	13	13	4		16	15	10										
445	3	3	15	15	4		16	15	10										
446	3	3	16	16	26		16	15	10										
447	3	3	17	17	26		16	15	10										
448	4	4	12	12	26		16	15	12										
449	4	4	13	13	26		16	15	12										
450	4	4	14	14	26		16	15	12										
451	4	4	15	15	26		16	15	12										
452	6	6	16	16	26		16	15	12										
453	9	9	17	17	26		16	15	12										
454	12	12	14	14	26		16	15	12										
455	12	12	15	15	26		16	15	12										
456	12	12	1	1	26		16	15	12										
457	12	12	2	2	26		16	15	12										
458	12	12	3	3	26		16	15	12										

Table 3.1. Input Data Set for Full-scale Submarining Model (Page 8 of 10)

459	13	13	14	14	26	16	15	12			
460	13	13	15	15	26	16	15	12			
461	13	13	2	2	26	16	15	12			
462	14	14	1	1	26	16	15	12			
463	14	14	2	2	26	16	15	12			
464	14	14	3	3	26	16	15	12			
465	15	15	2	2	26	16	15	12			
466											
467	10.0		30.0		1.0			18			
468	-308.71		0.0		-48.19						
469	0.0		22.50		0.0						
470	0.0		15.00		0.0						
471	0.0		-2.00		0.0						
472	0.0		-15.00		0.0						
473	0.0		-15.0		0.0						
474	0.0		115.00		0.0						
475	0.0		35.000		0.0						
476	0.0		90.0		0.0						
477	0.0		115.00		0.0						
478	0.0		35.000		0.0						
479	0.0		90.0		0.0						
480	0.0		5.0		0.0						
481	17.5		81.0		0.0			0.0		0.0	3 2 1
482	0.0		5.0		0.0						
483	-17.5		81.0		0.0						3 2 1
484	17.5		81.0		0.0						3 2 1
485	-17.5		81.0		0.0						3 2 1
486	0.		22.5		0.						
1000											
1001	0.	150.	1.			0					
1002											
1003											
1004	18	0	10.								0.
1005	0	0	20.								0.
1006	0	0	30.								0.
1007	0	0	40.								0.
1008	0	0	50.								0.
1009	0	0	60.								0.
1010	0	0	70.								0.
1011	0	0	80.								0.
1012	0	0	90.								0.
1013	0	0	100.								0.
1014	0	0	110.								0.
1015	0	0	120.								0.
1016	0	0	130.								0.
1017	0	0	140.								0.
1018	0	0	150.								0.
1019	0	0	160.								0.
1020	0	0	170.								0.
1020.5	0	0	180.								0.
1021	18	0	10.								0.
1022	0	0	20.								0.
1023	0	0	30.								0.
1024	0	0	40.								0.
1025	0	0	50.								0.
1026	0	0	60.								0.
1027	0	0	70.								0.
1028	0	0	80.								0.

Table 3.1. Input Data Set for Full-scale Submerging Model (Page 9 of 10)

1029	0	90.	0.	0.										
1030	0	100.	0.	0.										
1031	0	110.	0.	0.										
1032	0	120.	0.	0.										
1033	0	130.	0.	0.										
1034	0	140.	0.	0.										
1035	0	150.	0.	0.										
1036	0	160.	0.	0.										
1037	0	170.	0.	0.										
1037.5	0	180.	0.	0.										
1038	18	0	10.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
1039	0	20.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
1040	0	30.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
1041	0	40.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
1042	0	50.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
1043	0	60.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
1044	0	70.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
1045	0	80.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
1046	0	90.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
1047	0	100.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
1048	0	110.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
1049	0	120.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
1050	0	130.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
1051	0	140.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
1052	0	150.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
1053	0	160.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
1054	0	170.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
1054.5	0	180.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
1055	18	1	2	3	4	5	6	7	8	9	10	11		
1056		12	13	14	15	16	17	18						
1057	18	1	2	3	4	5	6	7	8	9	10	11		
1058		12	13	14	15	16	17	18						
1059	18	1	2	3	4	5	6	7	8	9	10	11		
1060		12	13	14	15	16	17	18						
1061	17	1	2	3	4	5	6	7	8	9	10	11		
1062		12	13	14	15	16	17							
1063	5	3												
2001	0	1	1	1	0	1	1	0						
2002	0.	.15	.01											
2003	0	0.	0.											
2004	1.	0.	0.											
2005	0.	1.	0.											
2006	0.	0.	1.											
2007	1.	0.	0.											
2008	0.	1.	0.											
2009	0.	0.	1.											
2010	.5	.5	11.	8.5										
2011	.5	.5	10.	7.										
2012	-400.	-150.	250.	175.	.3									
2013	GMCVS2.D	XZ												

26

\$EMP GUC7
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However, when specific data are obtained which can directly relate pelvic orientation to belt placement and submarining, they should be used.

Line 112.1. B5 Card. The second card describing the torque-angle data.

Line 129.1. B6 Card. The three quantities included are magnitude, absolute error, and relative error tests for angular acceleration of BPEL. The values chosen are the same as for the other variables.

Line 437. F2 Card. This is a variation of the card used in the original data set. The belt attachment for the occupant is shifted from the lower torso (segment 1) to the overlay mass (segment 18).

NOTE: Many lines in the data set use the number of segments included in the model. The segment number representing the vehicle has been changed to 19 with BPEL, the new mass in the occupant linkage, now being assigned to segment 18.

Figure 3.5 is a schematic showing the occupant at 80 milliseconds into simulation. It should be noted that the overlay mass has rotated backward toward the seat back. The original position of the belt attachment to the lower torso is indicated by an "X" with a circle around it. This point has migrated upward, in the direction of submarining, to the point indicated with an "X." Some penetration into the original lower torso mass has also occurred.

A summary of the general results from this simulation are as follows:

- Velocity: 1369 cm/sec
- Deceleration: Peak of 37 g and duration of 90 ms
- Peak Head Deceleration: 61 g's at 74 ms
- Peak Thorax Deceleration: 65 g's at 71 ms
- Peak Pelvis Deceleration: 64 g's at 73 ms
- Upper Torso Belt: 487 kg at 84 ms
- Lower Torso Belt: 471 kg at 84 ms
- Lap Belt A: 809 kg at 75 ms
- Lap Belt B: 808 kg at 78 ms

This simulation has demonstrated the capabilities of the existing BELT subprogram to model submarining without changes to the code. In

Simulation of
Submarining Indicator

GMCV52:B1
80:0

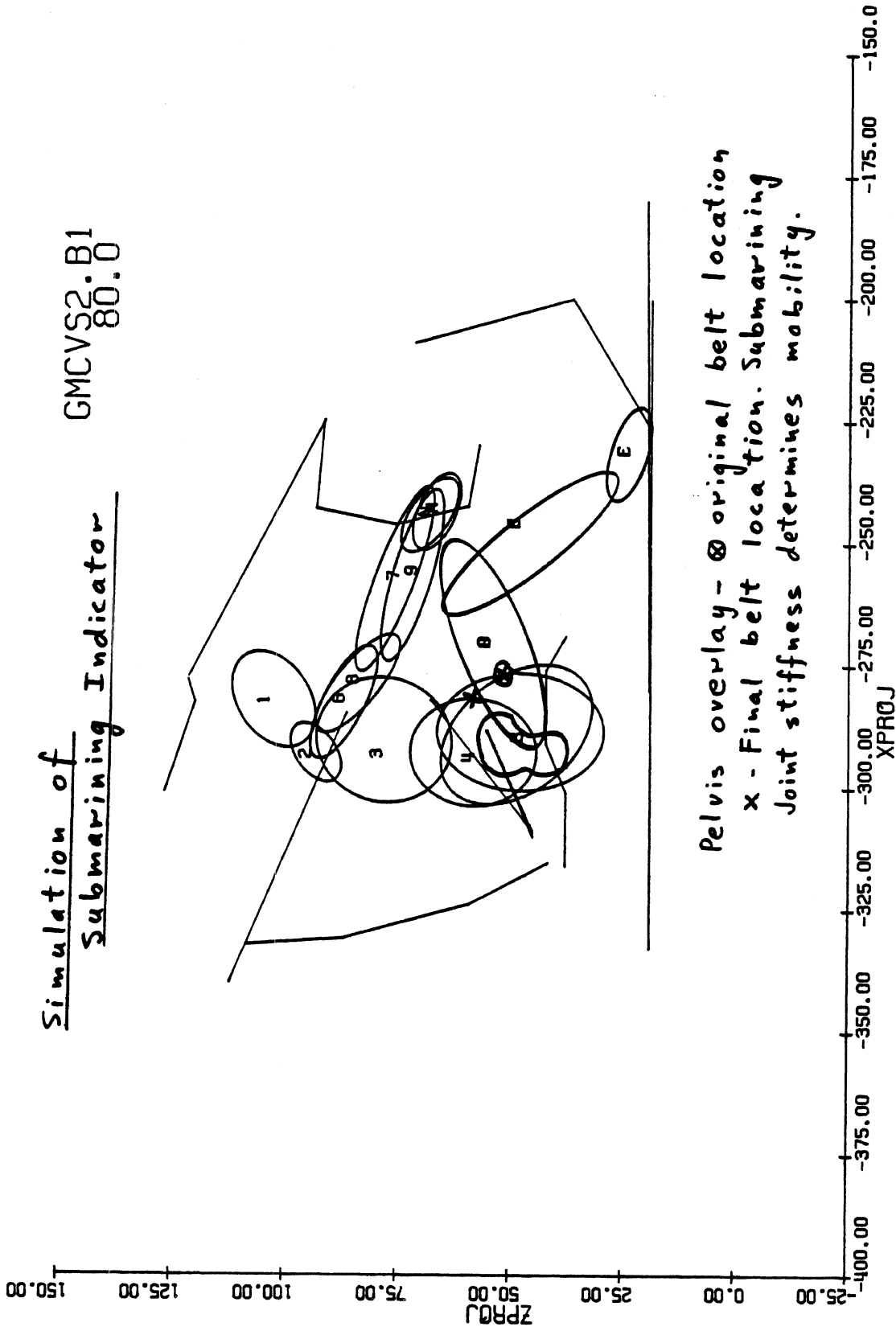


Figure 3.5. Simulation of Submarining Indicator (t = 80 ms)

order to use it in realistic design studies, impact studies should be conducted to refine the following input quantities:

- Location of the joint on the overlay mass.
- Properties of the torque-angle resistance.
- Shape and location of the overlap ellipsoid.

This will require new kinds of tests and analyses of results which graphically document the position of the belt on the pelvic region as a function of the pelvic structure of the test dummy.

4.0 ANALYSIS OF BELT MATERIAL TRANSFER ACROSS SURFACES

4.1 The Belt Slip Model Developed by British Leyland

As was mentioned in Section 3.1, each belt has a plane called the belt plane which is defined by the positions of two belt anchor points and the fixed point in inertial space. The intersection of the belt plane and the belt contact ellipsoid is the belt ellipse within the belt plane. This situation is pictured in Figure 4.1. From each slip point the belt proceeds as a straight line in the belt plane until it intersects the belt ellipse at a tangent point and then conforms to the belt ellipse to the fixed point. In the case that the belt ellipse is oriented so that there exists line-of-sight between one or both anchors and the fixed point, the belt is assumed to proceed along the line-of-sight and of course no tangent point exists on that side of the fixed point. Figure 4.2 illustrates several such cases. In the original Calspan report, this figure illustrated the algorithm for choosing the belt path from the two tangent lines to an ellipse through any point outside of the ellipse. In the cases where no actual tangent point exists, the term "tangent point" will be defined to mean "fixed point."

A point at which anchors from two belts coincide lies in a plane defined by the common anchor and the near tangent point or fixed point from each of the two belts. We will call this plane the anchor slip plane. In general the anchor slip plane will not coincide with the belt planes of either belt and may or may not contain the fixed points of the two belts. This definition will be used in cases where webbing material passes through a ring. However, in all cases the points at which the belts proceeding from the common anchor first intersect the two belt ellipses will be within the belt slip plane by definition. If the belt is imagined to fasten to the anchor point, then the force vector representing the belt tension's action upon the belt anchor will lie along the belt from the anchor to the nearer tangent point with a magnitude equal to the belt tension. The resultant of both belts upon the common anchor will be the vector sum of the two belt vectors. The

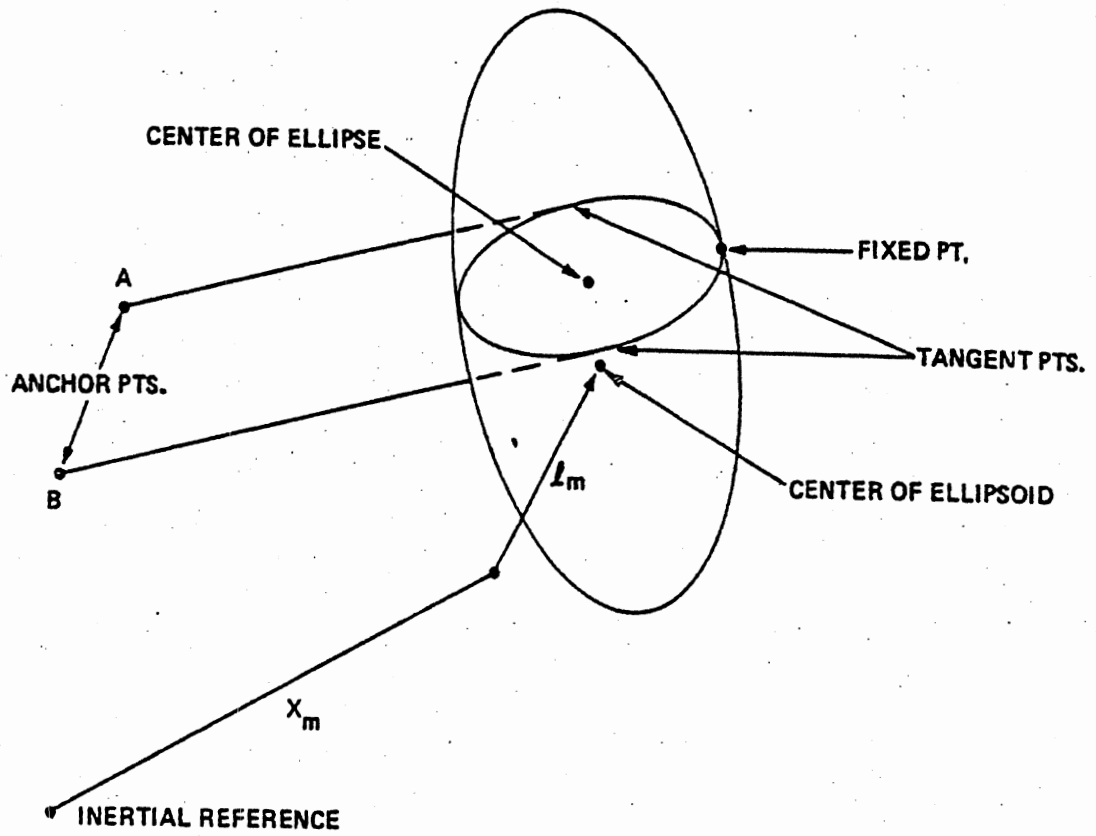


Figure 4.1. The Belt Plane in Inertial Space.

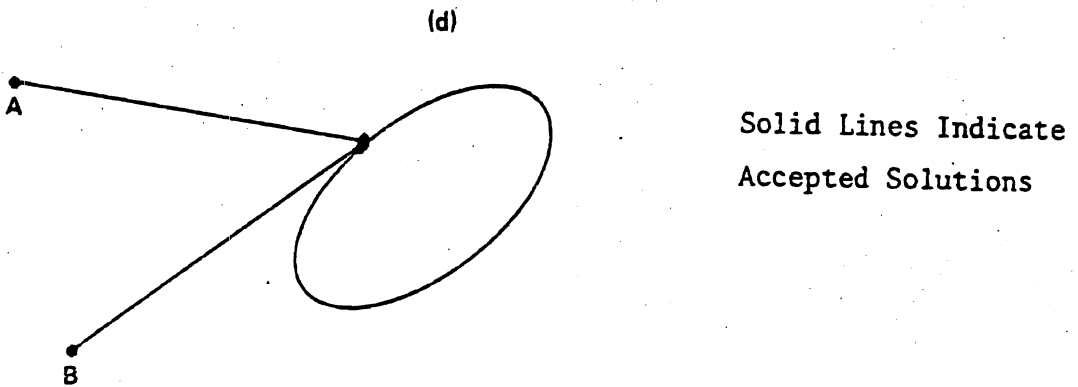
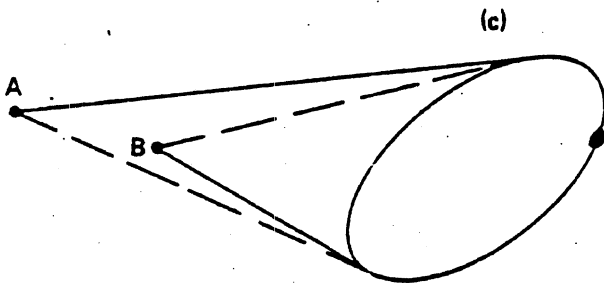
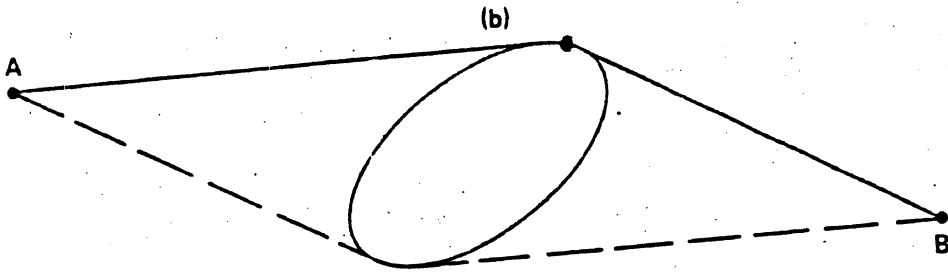
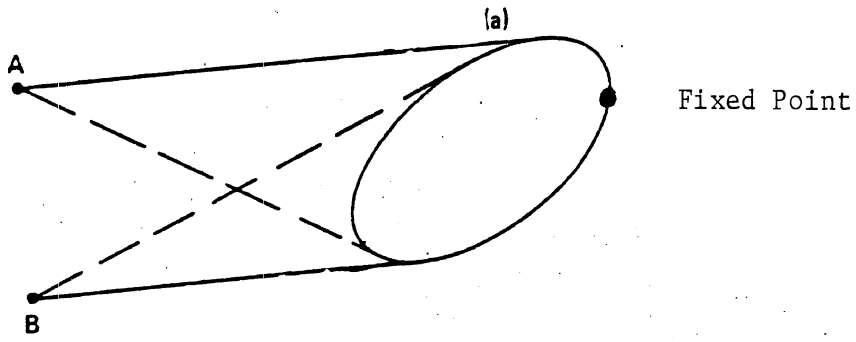


Figure 4.2. Belt Layout Examples.

resultant belt force is broken into "normal" and "tangential" components. The "normal" direction is defined by the unit vector at the common anchor point for which the scalar products with the unit vectors along the two belt force vectors at the same point are equal. The "tangential" direction is defined as an unit vector at the common anchor which is perpendicular. There are two unit vectors which satisfy both the "normal" and "tangential" definitions. In each case the unit vector is chosen for which the component of the resultant force is positive. Figure 4.3 shows the various vectors in the belt slip plane within the belt segment on one side labeled "A" and on the other side labeled "B."

The component of the resultant force in the tangential direction is called the "slip force." The slip force is assumed to be opposed by a "slip friction force" and a "threshold force." The slip friction force is modelled as kinetic friction while the larger effect of static friction is modelled as a threshold force. If slip force exceeds the sum of slip friction force and threshold force then the unstrained belt lengths are modified until slip force is reduced below this sum but not below slip friction force. The satisfaction of this criterion will be referred to as reaching "equilibrium." Note that equilibrium is used relative to the iteration which takes place at each point in time in order to calculate what would physically be seen at that time. Equilibrium is not used in the usual physical sense.

4.2 UMTRI Extensions to the British Leyland Slip Algorithm

Friction-opposed slipping was desired at both fixed points on segments and at vehicle anchors for as many belt segments as were considered to be defined by a single piece of webbing. This was done in order to consider a complete three-point belt system which consists of two lap and shoulder sections with the potential for slipping across the lap, through the ring connecting the lap and shoulder sections, and across the chest. The first extension required was to find corresponding definitions for normal direction, tangential direction, and slip force for the case of the fixed point on a belt ellipse. It is clear that the direction of belt tension at the fixed point itself is

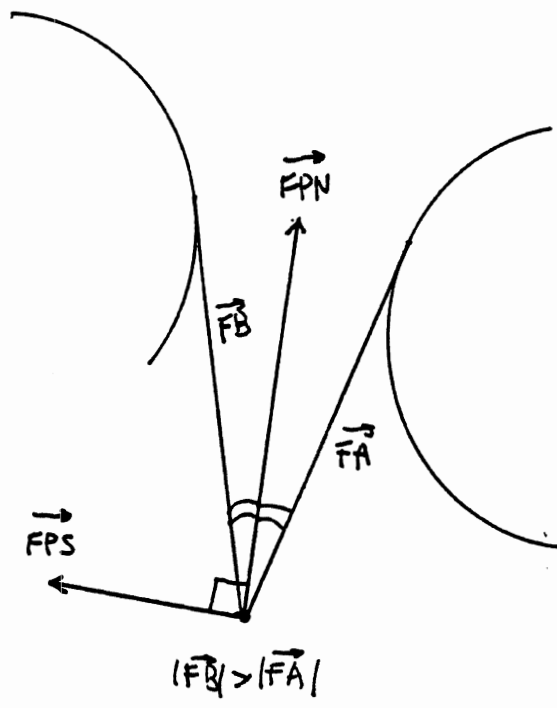


Figure 4.3. British Leyland Slippage Between Belts

irrelevant to the effect of the belt on the contact ellipse and on the tendency of the belt to slip over the contact ellipse. The directions of the force vectors at the fixed point for the purposes of determining slip force were defined as parallel to the directions of the corresponding anchor points as seen from the two tangent points (with the line-of-sight exception raised in the last section). All the other definitions are carried over from the previous section in terms of these two new force vectors and their resultant. Figure 4.4 illustrates the situation at the fixed point and how it corresponds to the situation pictured in Figure 4.3 at the common anchor point.

UMTRI also adapted the "F.9" data cards which were added by British Leyland to input slip algorithm quantities, as well as made other necessary input changes. Appendix A presents the updated Input Description pages covering these changes.

4.2.1 Definition of Terms for Belt Slip Algorithm. It is useful to define four new terms with which to describe the combining of multiple CVS belts.

1. **Belt Node** is either any belt anchor point or any belt fixed point for which infinite friction is prescribed. There is a maximum of 24 belt nodes (two or three per belt). Any belt node is characterized by the number of the belt on which the point is situated together with an indicator designating which point (A = Anchor A, F = Fixed Point, or B = Anchor B).

2. **Belt Segment** is the portion of any belt which connects any two consecutive belt nodes. There is a maximum of 16 belt segments (one or two per belt). Any belt segment can be characterized by the designation of the belt nodes which it connects; however, usually a belt segment will be characterized by its number in the ordered list of belt segments which comprise a belt loop (see remaining definitions).

3. **Slip Point** is either a terminating belt node (Anchor B) of one belt segment which is coincident in both location and attachment system with the initial belt node (Anchor A) of another belt segment or a fixed point on any belt segment and in either case for which slipping is prescribed. There is a maximum of 15 slip points for all belts. Slip Points can be characterized by the belt nodes which form them or, as in the case of belt segments, by its number in the ordered list of slip points which connect the ordered list of belt segments, respectively.

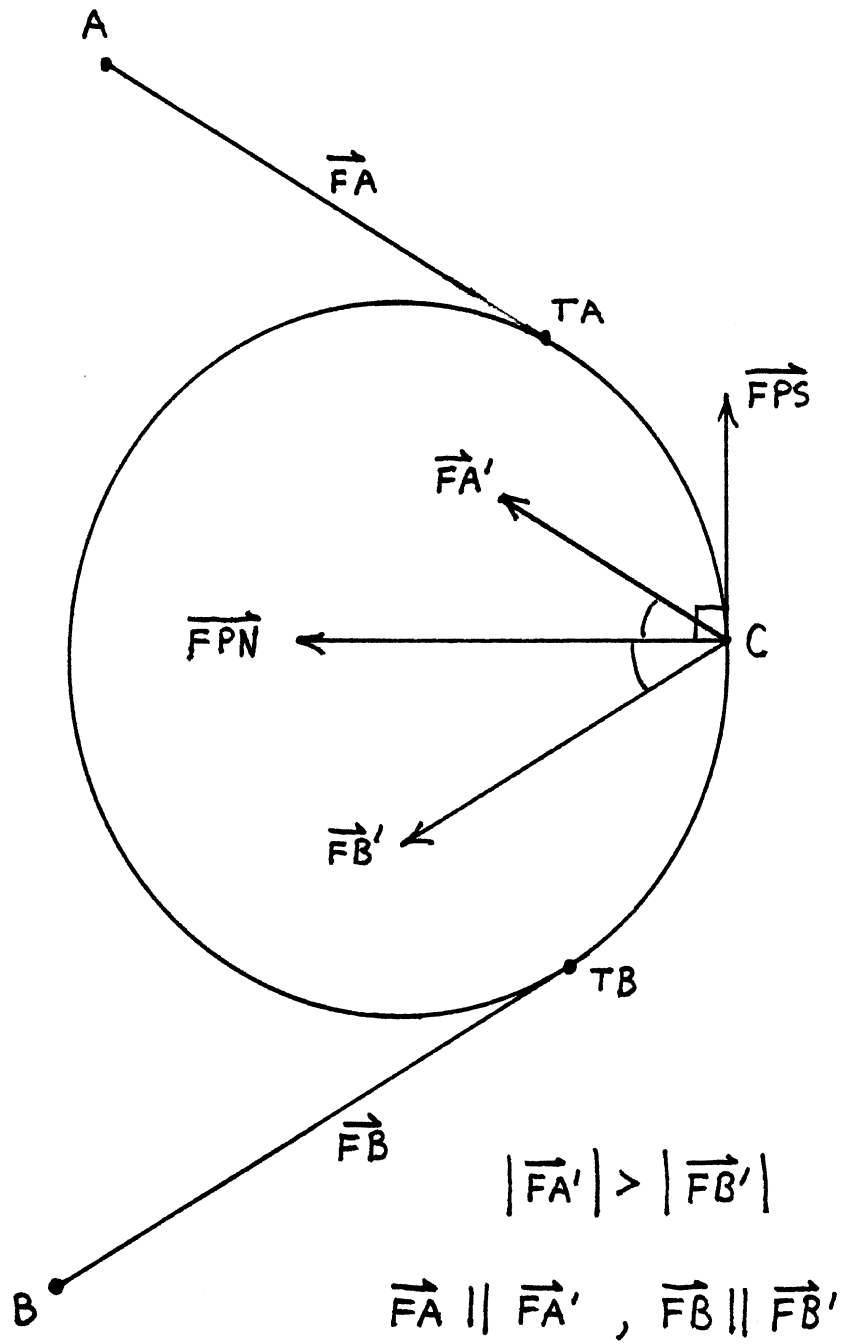


Figure 4.4 Modified Slippage at Fixed Point

4. **Belt Loop** is any group of belt segments for which all but exactly two of their constituent belt nodes are slip points connecting belt segments within the group. The two belt nodes which are not slip points within the loop can not be slip points at all and are called loop anchors. There is a maximum of eight belt loops. Belt loops are characterized by the two loop anchors, by the ordered list of belt segments which comprise it, or by the ordered list of slip points which hold it together. Every belt loop is necessarily independent. The typical belt loop in what follows will consist of N belt segments and N-1 slip points.

4.2.2 Belt Slip in the Presence of Slack. Observations of sled tests appear to reveal the characteristic that belts freely slip until all slack is taken up. At this time the slipping mechanism changes and becomes very restricted. This type of slipping behavior has been added by UMTRI by looking at each belt segment individually and prorating unstrained total belt length for the entire belt loop to the belt segment according to the ratio of the belt segment's strained length to the total strained belt length for the entire belt loop. Expressed in equation form, let l_k be the strained belt length for the "k-th" belt segment in the loop. Let L_k be the unstrained belt length for the "k-th" belt segment in the loop.

Let l_T be the total strained belt length over the entire belt loop.

Let L_T be the total unstrained belt length over the entire belt loop.

Then if $L_T \geq l_T$, the unstrained segment lengths are determined by

$$L_k = \lambda l_k \quad \text{for } k = 1, \dots, N$$

where

$$\lambda = \frac{L_T}{l_T}$$

and all belt forces are defined to be zero. If this free-slipping condition is not met, then the methods of the succeeding subsections are used.

4.2.3 Belt Slip Under Load at a Typical Slip Point. Belt segment k-1 will connect to belt segment k at slip point k-1 where k can be any of 2, ... , N. Assume that the belt segments are both producing belt

tension. The following equation represents the relationship between the belt segment tension forces at the slip point which is necessary to achieve slip equilibrium. (See Appendix B for the derivation of this expression.) Figure 4.5 shows the typical slip point and pertinent quantities.

$$\lambda_{A,k-1} \tilde{F}_{k-1} + \lambda_{B,k-1} \tilde{F}_k + \lambda_{C,k-1} = 0$$

where the tilde written over any variables signifies "at equilibrium"

$$\lambda_{A,k-1} = \sin(\Omega_{k-1}) + \eta_{k-1} h_{1,k-1} \cos(\Omega_{k-1})$$

$$\lambda_{B,k-1} = -\sin(\Omega_{k-1}) + \eta_{k-1} h_{1,k-1} \cos(\Omega_{k-1})$$

$$\lambda_{C,k-1} = \eta_{k-1} h_{2,k-1}$$

Ω_{k-1} = one-half of included angle between belt segments

$$h_{1,k-1} = \mu_{k-1} + \frac{1}{2} C_{1,k-1}$$

$$h_{2,k-1} = \frac{1}{2} C_{2,k-1}$$

η_{k-1} = relative direction indicator for slip resistance

μ_{k-1} = coefficient of friction

$C_{1,k-1}$ = coefficient of threshold force

$C_{2,k-1}$ = constant threshold force

This is the characteristic equation of belt slipping equilibrium at each slip point. The computational problem is to adjust the unstrained belt segment lengths throughout the belt loop so that this characteristic equilibrium equation is simultaneously satisfied at all slip points in the belt loop. In what follows, consideration is limited to a maximum of three slip points and four belt segments for each belt loop. Figure 4.6 illustrates one such configuration for a belt loop involving two belt contact ellipsoids.

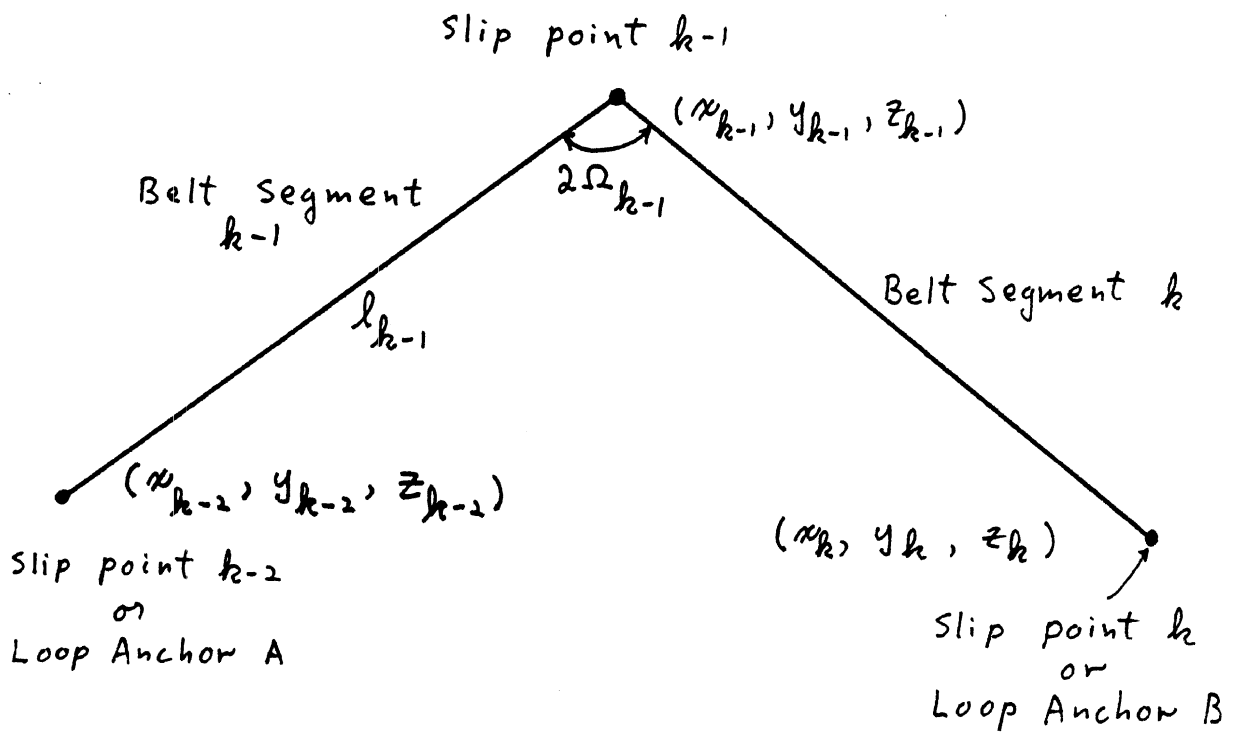


Figure 4.5. The Typical Slip Point $k-1$

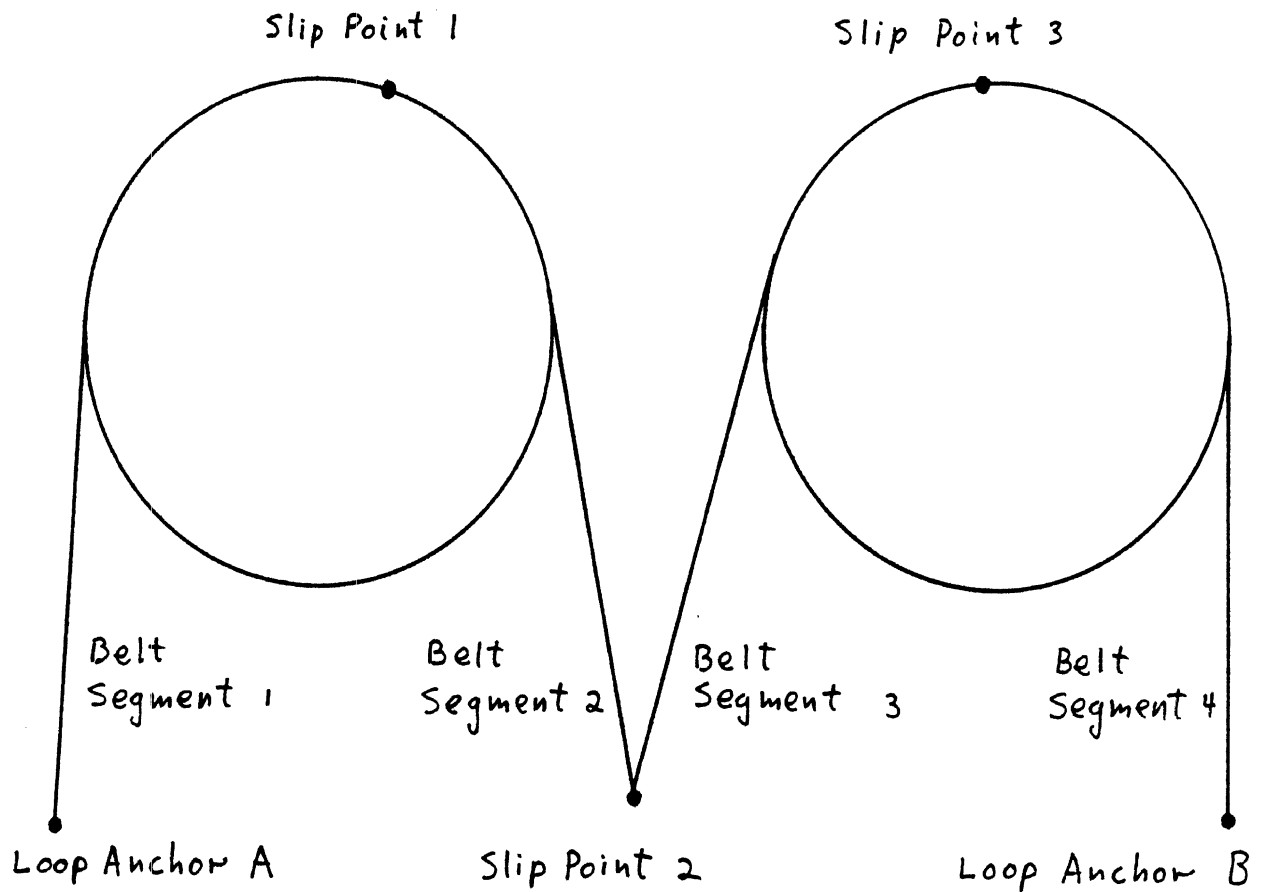


Figure 4.6. A Maximum Belt Loop Configuration

4.2.4 The Progressive Solution Approach. Belt slipping over a whole belt loop can be conceived as a sequence of slips at individual slip points. If this approach were valid, then the computational problem would be reduced to several simpler tasks (searching for the zero of a non-linear equation in one variable).

The non-linear equation is simply the equilibrium condition equation for the slip point k-1. The force for belt segment k-1 is a function of the strained and unstrained belt lengths for belt segment k-1, of which only the unstrained belt length is subject, during the iteration process. Likewise, the force for belt segment k is a function of the strained and unstrained belt lengths for belt segment k of which only the unstrained belt length is subject to change in the iteration. By looking at slipping only at slip point k-1, it follows that the change in the unstrained belt length for segment k-1 must be equal and opposite to the change in the unstrained belt length for segment k. The following can then be written:

$$\tilde{L}_{k-1} = L_{k-1} + \Delta L_{k-1}$$

$$\tilde{L}_k = L_k - \Delta L_{k-1}$$

where ΔL_{k-1} is the unstrained belt length added to belt segment k-1 by slipping and is the only unknown.

An effective algorithm for the solution of the non-linear equation was put together from similar work in earlier models and makes use of the methods of Newton, the secant, and halving the interval.

This approach worked very well for single slip point belt loops with all possible belt material properties, but it was very capricious in cases involving more than one slip point. Sometimes the results would converge very quickly and smoothly and other times the results would oscillate chaotically. The apparent flaw in this approach was the selection criterion for determining the order to do the slip points. Although this problem is completely analogous to the selection problem occurring during the relaxation method, no attempt was made to investigate selection from this point of view since the needed partial derivatives are both complex and difficult to obtain accurately when

involving tabular information. It was that there must be some appropriate order of individual slip point adjustments that would converge for any given case since the actual slipping (at least at the quantum level) theoretically occurs this way. It was also felt that some other approaches which seemed to promise a quicker solution should be tried.

4.2.5 The Simultaneous Solution Based on Change in Unstrained Length for Belt Segment 1. A linear approximation to the belt material properties yields:

$$F_{k-1} = K_{k-1} \left(\frac{l_{k-1} - L_{k-1}}{L_{k-1}} \right)$$

and

$$F_k = K_k \left(\frac{l_k - L_k}{L_k} \right)$$

where K_{k-1} , K_k are the effective linear coefficients of force versus strain. Note that while there is only one set of material properties over both belt segments, it is likely that the two belt segments will be in different strain ranges and therefore will need separate linear approximation.

For each belt segment k , a variable Δ_k can be defined as

$$\Delta_k = \tilde{l}_k - L_k$$

Δ_k is the amount of additional unstrained belt segment length for each belt segment in order to reach equilibrium (may be positive or negative). Since the total unstrained belt length over each loop is invariant during this iteration, therefore it is true that

$$\sum_{k=1}^N \Delta_k = 0$$

We can write

$$\lambda_{A,k-1} \left(\frac{l_{k-1} - L_{k-1} - \Delta_{k-1}}{L_{k-1} + \Delta_{k-1}} \right) + \lambda_{B,k-1} \left(\frac{l_k - L_k - \Delta_k}{L_k + \Delta_k} \right) + \lambda_{C,k-1} = 0$$

and solving for Δ_k , we get

$$\Delta_k = \frac{a_{2,k-1} \Delta_{k-1} + a_{4,k-1}}{a_{1,k-1} \Delta_{k-1} + a_{3,k-1}}$$

where

$$a_{1,k-1} = \lambda_{A,k-1} K_{k-1} + \lambda_{B,k-1} K_k - \lambda_{C,k-1}$$

$$a_{2,k-1} = a_{A,k-1} L_k - \lambda_{B,k-1} K_k l_k$$

$$a_{3,k-1} = -a_{1,k-1} l_{k-1} + \lambda_{A,k-1} K_{k-1} l_{k-1}$$

$$a_{4,k-1} = -a_{1,k-1} L_{k-1} L_k + \lambda_{A,k-1} K_{k-1} L_k l_{k-1} + \lambda_{B,k-1} K_k L_{k-1} l_k$$

Since this is a forward recursion relationship, it can be used to solve for each Δ_k in terms of Δ_1 and then these can be substituted into

$\sum_{k=1}^N \Delta_k = 0$ to get a polynomial in terms of Δ_1 . For $N=2$, the expression is a quadratic; for $N=3$, it is a cubic; for $N=4$, a quartic. For the last case with reasonably typical values of physical quantities the coefficients of the quartic ranged from 10^{44} to 10^{23} . These were big enough to cause exponent overflow using a good real polynomial solver on the University of Michigan Amdahl. When the coefficients were scaled by the leading coefficient, good zeroes were always obtained even through an occasional false "lack of convergence" was indicated. It was possible to demonstrate that there was loss of significance of at least eight, and as much as twelve, places during this calculation; however, since sixteen places were carried, the results were good enough.

It was necessary to devise an algorithm to select the appropriate root. This turned out to be easily done by choosing a real root which yielded a positive unstrained belt length which was not greater than the total unstrained belt length.

For materials which were linear, the results were always correct. For non-linear materials, the results always overshoot. This type of behavior was expected since it was anticipated that this linear approximation based on the first derivative would act like Newton's Method. This did not turn out to be the case since when repeated applications of this algorithm were tried, cyclical behavior was noted which after a point did not improve the results further.

4.2.6 The Simultaneous Solution Based on Deflection of Belt Segments. It was felt that perhaps the numerical properties could be improved if we were to solve for optimal deflection instead of the change in unstrained belt segment length unless the coefficients were driven still larger. While it is true that physically the length of webbing which slips is the variable to be determined, mathematically we could choose any variable in terms of which we could write the unstrained belt length. So force was taken to be

$$F_k = K_k \left(\frac{\delta_k}{l_k - \delta_k} \right)$$

and substitute as before to come up with another forward recursion relationship in δ_k

$$\delta_k = \frac{a_{1,k-1} \delta_{k-1} + a_{2,k-1}}{a_{3,k-1} \delta_{k-1} + a_{4,k-1}}$$

where

$$a_{1,k-1} = l_k [\lambda_{C,k-1} - \lambda_{A,k-1} K_{k-1}]$$

$$a_{2,k-1} = -\lambda_{C,k-1} l_{k-1} l_k$$

$$a_{3,k-1} = -\lambda_{A,k-1} K_{k-1} - \lambda_{B,k-1} K_{k-1} + \lambda_{C,k-1}$$

$$a_{4,k-1} = l_{k-1} [\lambda_{B,k-1} K_{k-1} - \lambda_{C,k-1}]$$

As before this expression was used to write all δ 's in terms of δ_1 and then substituted into the equation resulting from the fact that the sum of all deflections over the loop is invariant during the iteration.

This approach caused a small improvement in coefficient size and in loss of significance but no improvement in non-linear behavior. It was realized that the huge coefficients were due to many applications of the recursion relationship and it was decided that the number of applications could be reduced by starting in the middle and working both ways instead of starting at one end and working across. So the forward recursion relationship was solved backwards to obtain:

$$\delta_{k-1} = \frac{a_{4,k-1}\delta_k - a_{2,k-1}}{-a_{3,k-1}\delta_k + a_{1,k-1}}$$

where the a's are the same as before.

This made a dramatic improvement in coefficient size (now ranging 10^{23} to 10^{12} and in loss of significance to only four or five places, but did not completely solve the non-linear convergence problem.

4.2.7 The Simultaneous Solution Based on Strain for Belt Segment 2. It was felt that the lack of convergence for linear approximations of non-linear material properties was probably due to the form of the definition of force since it was force which was being controlled. It was decided to solve directly in terms of strain and then compute unstrained belt length and deflection from the expressions:

$$L_{k-1} = \frac{l_{k-1}}{1+S_{k-1}}$$

and

$$\delta_{k-1} = \frac{S_{k-1}l_{k-1}}{1+S_{k-1}}$$

where S_{k-1} is strain for belt segment k.

The force equation was greatly simplified as

$$F_{k-1} = K_{k-1} S_{k-1}$$

and the recursion relationships became

$$S_k = a_{1,k-1} + a_{2,k-1} S_{k-1}$$

and

$$S_{k-1} = \frac{1}{a_{2,k-1}(S_k - a_{1,k-1})}$$

where

$$a_{1,k-1} = \frac{-\lambda_{C,k-1}}{K_k \lambda_{B,k-1}}$$

and

$$a_{2,k-1} = \frac{-\lambda_{A,k-1} K_{k-1}}{\lambda_{B,k-1} K_k}$$

This leads to easy solution of all strained in terms of S_2 , but now the invariant takes a more complex form

$$\sum_{k=1}^N \left(\frac{S_k l_k}{1+S_k} \right) = \delta_T$$

This yields coefficient expressions which are as complex as those from the other approaches but promise to yield smaller sizes for coefficients. Unfortunately, it was not possible to finish and test this approach within the resources of the project and extension. The original equations were developed. A satisfactory hand case for the $N=2$ linear case was done. However, a dimensional check and rederivation of the equations were not accomplished.

4.2.8 Set Up of the Slip Resistance Direction Factors. In the proceeding several sections, we have made use of the Y_{k-1} slip resistance direction factors saying only that they must be properly chosen for a valid solution. In this section, the algorithm for determining the proper choice of these factors is discussed.

For the $N=2$ case, it is clear that the proper choice is to oppose belt slip from the lower tension belt segment to the higher tension belt segment (since slipping would stop before it would overshoot).

Likewise it is clear that any monotonic arrangement of belt segment tensions in a multiple slip point case would remain in that configuration at equilibrium (with reduced tension differences). It is also clear that there are arrangements in which two relatively small belt tensions could be reversed by the presence of a much larger belt tension nearby on the way to equilibrium.

The approach used was to evaluate the given configuration, find the maximum tension belt segment and proceed in both directions from there searching for reversals in monotonicity (which for the $N = 4$ case can be a maximum of two). For each of these reversals, the problem is solved with both choices of y_k for the affected belt segments (a maximum of four solutions). Finally, the single solution is chosen which minimizes total belt slipping as the correct solution. This approach may be more laborious than necessary, but until an algorithm which would give good results was developed, it was not possible to investigate improvements in this procedure.

4.3 Summary of Progress

While a major portion of the effort in this project was spent investigating a suitable general method for the solution of the slip equilibrium equations at all slip points, several other tasks were necessary to integrate any such algorithm in the Calspan CVS, Version 20 code. A new Slip Input routine along with modifications to other input routines was also necessary. These have been coded and tested both in isolation and within the model.

It was also necessary to modify the belt routines so that they would work along with the new belt slip routines. The belt slip routines determine the situation, handle any slack, set up the problem for solution, do the solution for slipping, compute the quantities to be outputted and records these for later printing. These routines have also been coded and tested in isolation and also with a dummy solution routine within the CVS model. Finally, the output changes necessary to print the output quantities have been coded and tested.

It was necessary to write a separate test program for the various approaches to the equilibrium equation solution routine and determine the numerical characteristics of each approach. The plan was that when the slip solver was satisfactory in isolation, it would be inserted into the CVS code and final testing of the whole package would take place.

4.4 Recommendations

It is recommended that the strain approach discussed in Section 4.2.7 be implemented, tested, and the numerical characteristics determined.

If this fails, it is felt that an incremental approach should be tried where controlled steps are taken in the direction determined by a Newton-type or secant-type method. The numerical studies already done give some hope that this approach could be successful.

If both of these approaches fail, it is felt that everything done to this point should be reviewed and carefully reevaluated before anything else is considered.

The reasoning behind these recommendations is that the concept and the algorithms are inherently simpler than those used in the more sophisticated HARNESS routines which are not yet working entirely satisfactorily. It is estimated that these concepts are satisfactory for many standard three-point belt applications, and when completely installed and debugged, should be relatively inexpensive and easy to use.

5.0 THE HARNESS ALGORITHM

An advanced restraint system submodel (HARNESS) has been under development of a number of years by Fleck and associates (Butler et al. 1975, 1980, 1983). The model requires the user to specify a set of potential reference points on ellipsoids which are in contact with the belts comprising the harness (see Figure 5.1). The anchor points do not have to be fixed to the same segment. They can also be attached to another belt. Each belt may pass over more than one ellipsoid. Major aspects of this code are described as follows.

1. The position of the reference points is mobile. That is, they can move over the surface of the ellipsoid to represent belt sliding. This sliding can include frictional effects.

2. The reference points can penetrate the ellipsoid to represent the deformation of the non-rigid body based on its force-deformation characteristics.

3. If the force is removed from the belt at a reference point, the belt can lift off from contact.

This subprogram has potential, not present in the older BELT subprogram, to overcome problems observed (see Section 2) in laboratory tests of belt hardware. These include:

1. Slippage of belt over the surface in non-frontal impacts and release from contact if the occupant slips out of the belt.
2. Modeling of submarining.
3. Modeling of the complete three-point belt system in three dimensions.
4. Modeling of the belt/chest interaction.
5. Attachment of belts to non-rigid anchors.

During the early stages of the project, UMTRI was informed by the sponsor of development (USAF) that the software was essentially non-frictional. By the end of 1984, some modest successes were reported. By the end of 1985, UMTRI was provided with a short report (Obergefell and Kaleps 1984) and a list of code modifications to Version 20 of the CVS software. An example was included for a rather sophisticated Air Force harness (see Figure 5.2). It was indicated that

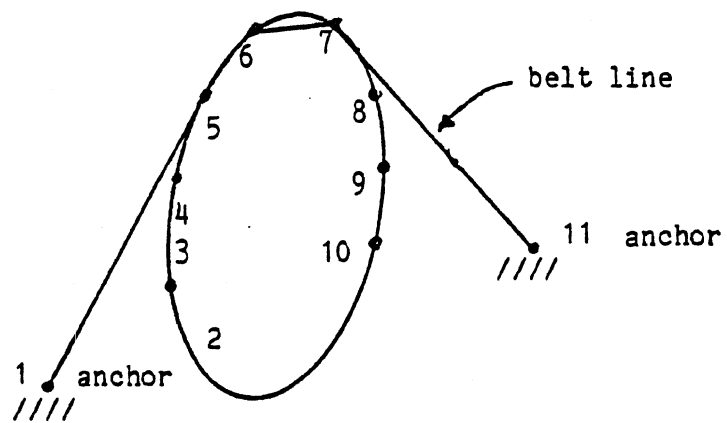


Figure 5.1. Points on Simple Harness.

most features worked but that great care had to be used in developing data sets. It is clear that a body of user knowledge must be developed before this code is ready for general use.

It is the recommendations of UMTRI that a considerable effort be expended to build a body of user knowledge on real problems, starting with a matrix of simple test cases. Most design problems involving belts can be handled with this code. Because the code was not recommended for use during the formal work on the project without a considerable expenditure of time and money, no effort was made to exercise it.

HARNES MODEL - MIGRATION AND PENETRATION
 POSSIBLE (WITH GREAT CARE).
 CODE CAN BE OBTAINED

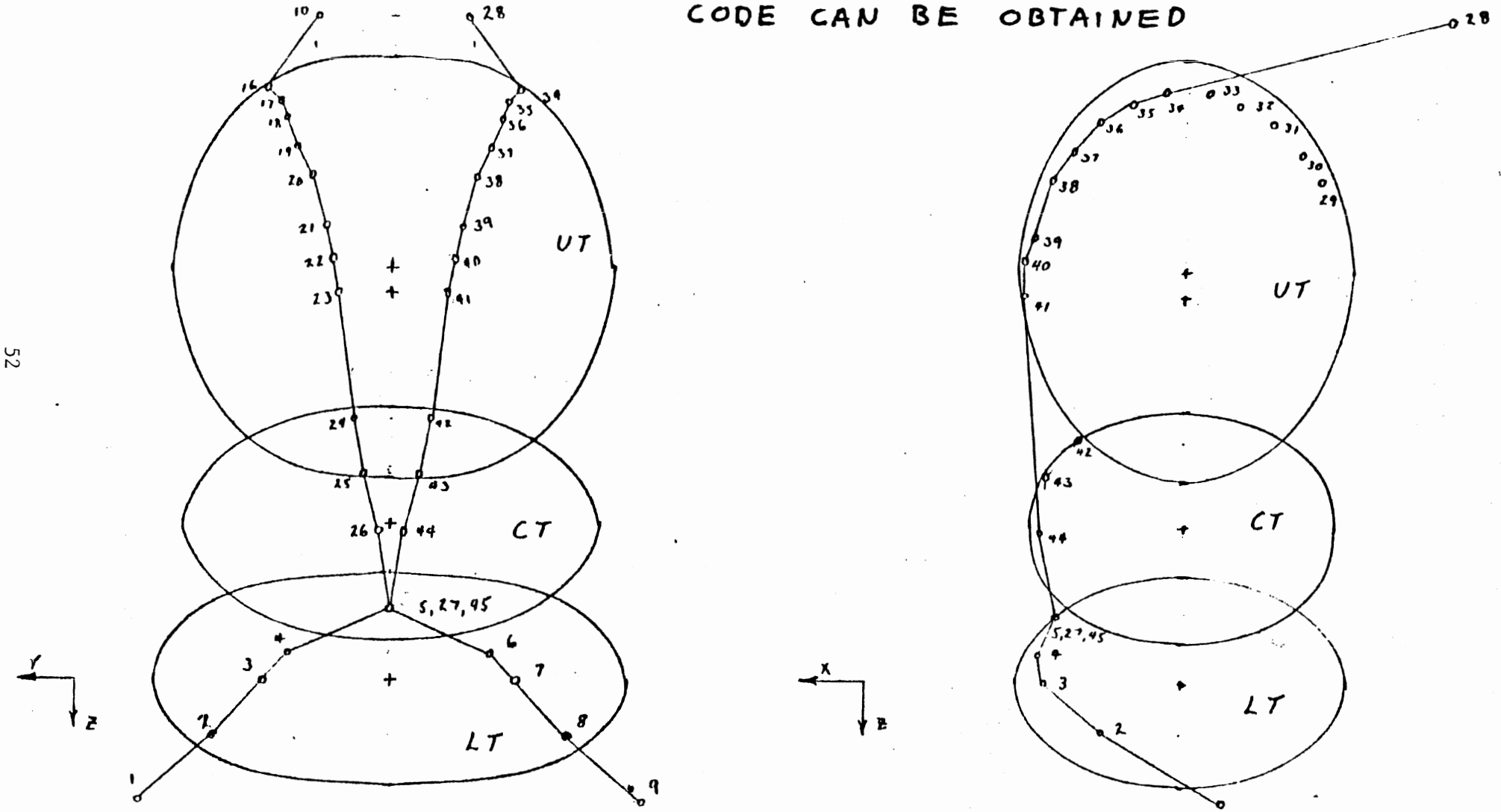


Figure 5.2. Air Force Harness Simulation Using HARNES.

6.0 UMTRI VERSION OF GMCVS

The UMTRI version of GMCVS includes a variety of improvements as well as modifications which were required in order for the program to function on MTS. In particular, the program was split into two separate processors. The first one was used to produce output. Most of these improvements and changes had already been developed during a previous contract with NHTSA (Bennett and Robbins 1982).

The Calspan 3-D CVS, Version 20, as it came to UMTRI from GM, made use of well over three megabytes of virtual storage. This large use of storage is considered excessive on the MTS System and usually causes job cancellation. Also, previous versions of the Calspan 3-D CVS made use of a separate logical device number for each output page as a means of sorting information into output pages as the run proceeded. This practice was not permitted on the MTS System. To cope with these problems during previous contracts with NHTSA, UMTRI reorganized the output sections using direct access (or indexed) input/output to achieve the sorting of information into pages. This reorganization was easily achieved in the past.

In recent versions such as CVS18 and CVS19, new output options were added requiring access to output quantities from previous time points in the simulation and so storage arrays were set up to hold this information. The options of printing all pages on one logical device number at the end of the run and of recording the information in an exterior file (sequentially in simulated time) were also added while keeping the ability to output on multiple logical device numbers. The increased complexity of the output sections and the huge amount of information now stored required the alternate use of three direct access hold files (due to file size restrictions) and multiplied the amount of effort required for the reorganization at UMTRI.

While the necessary reorganization was being carried out, UMTRI installed a number of useful output options which had already been developed in our previous work with NHTSA. As well as the two output recording options supported in Version 20 (every integration step or

every evaluation) it is now possible to record in output at equal increments of time. Regardless of which information recording concept is used, it is possible to print output in equal increments of integral multiples of DT or to print all information present.

The kinematics printout controlled by the "H" cards now allow the user several new options including:

- Specification of the coordinate system in which each output quantity is printed with the original conventions being used as a default;
- Optional printout of contact information both as to category of information and individual interaction; and
- Specifications of the order of printing by category of information.

Discrete use of these options enable the user to cheaply determine the important trends in a run and then set up more detailed printout and graphic displays of pertinent information. This is now possible because the output sections of the program are in a separate processor and can be rerun as often as useful as long as the hold files are kept intact.

Several parts of the general CVS program were not implemented in the UMTRI versions. These included HIC, SI, the variable graphics printer plots, the equilibrium positioning software, the RESTART option, and the VIEW graphics postprocessor. The first four were not implemented since alternatives such as the Validation Command Language Postprocessor (Bennett et al. 1979, Bennett 1983) were available from previous NHTSA work as part of the reorganization of output storage and processing.

The RESTART option was not implemented in GMCVS and so was left out of the UMTRI version. However, it is strongly recommended that this software be implemented as it gives the user the capability to interactively run the program and change the input data structure as simulation proceeds. This can be very useful, particularly in controlling integration time step, during long simulations such as rollovers. Interim graphic output should also be available at local workstations to determine whether to continue, change data and continue, or stop.

The connection to the VIEW postprocessor was also not implemented as the required DISSPLA software package was not installed on at The University of Michigan mainframe. The alternative was the Ellipsoidal Man Plot Postprocessor (Lehman et al. 1983) which was developed under NHTSA contract. It should be noted that the VIEW program cannot include more than one ellipsoid per segment. This limitation has been recently illustrated in attempts to compare graphic results of steering column simulations generated by GMCVS with those generated at UMTRI using the simpler, but more flexible, software.

One code modification was made in the UMTRI version in order to meet the need for a general vehicle motion input vector in simulations of general vehicle rollovers (Robbins 1986).

7.0 REFERENCES

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APPENDIX A

REVISION PAGES TO GMCVS INPUT DESCRIPTION

The following pages are replacement pages for the Calspan CVS model, Version 20, Input Description covering the changes made to the input sections of the model in order to provide a structure for the algorithms presented in Part 4 of this report.

IF NBLT IS NONZERO ON CARD D.1, NBLT SETS OF CARDS D.3 ARE REQUIRED.

CARD D.3.A	FORMAT (5A4)
BLTTTL(I,J), I=1,5	A 20 CHARACTER DESCRIPTION OF THE JTH BELT.
CARD D.3.B	FORMAT (6F12.0)
BELT(I,J), I=1,3	POSITION OF ANCHOR POINT A FOR THE JTH BELT W.R.T. SEGMENT NSEGA (SPECIFIED ON CARD F.2.B IN NS(1) FIELD). X, Y, AND Z COORDINATES (IN.)
BELT(I,J), I=4,6	POSITION OF ANCHOR POINT B FOR THE JTH BELT W.R.T. SEGMENT NSEGB (SPECIFIED ON CARD F.2.B IN NS(1) FIELD). X, Y, AND Z COORDINATES (IN.)

NOTE: THE PROGRAM MUST PASS A PLANE THROUGH THE THREE POINTS, ANCHOR POINT A, ANCHOR POINT B, AND A FIXED POINT ON THE CONTACTED BODY SEGMENT. IF ANCHOR POINTS A AND B COINCIDE, THEY MUST BE SEPARATED SLIGHTLY FOR INPUT SUCH THAT THE DESIRED BELT PLANE WILL BE DEFINED.

CARD D.3.C

FORMAT (5F12.0)

BELT(I,J), I=7,9

POSITION OF BELT FIXED CONTACT POINT WITH RESPECT TO SYSTEM THAT HAS ORIGIN AT ELLIPSOID CENTER AND IS PARALLEL TO LOCAL BODY SEGMENT SYSTEM. (X, Y, AND Z COORDINATES (IN.))

NSLPBL(J)

NUMBER OF SLIP POINTS FOR THIS BELT. SLIP POINTS MAY OCCUR AT EITHER BELT ANCHOR IF THERE IS ANOTHER BELT WHICH HAS A COINCIDENT ANCHOR WHICH IS ALSO SPECIFIED AS A SLIP POINT. SLIP POINTS MAY ALSO OCCUR AT FIXED POINTS FOR BELTS. (MAXIMUM VALUE IS 3; ENTER AS REAL NUMBER.)

BELT(11,J)

BELT SLACK (IN). THE SLACK IS ADDED TO THE INITIAL GEOMETRIC LENGTH TO OBTAIN THE INITIAL BELT LENGTH. IF NEGATIVE NUMBER IS ENTERED, IT WILL BE INTERPRETED AS INITIAL BELT LENGTH FROM WHICH THE PROGRAM WILL COMPUTE THE SLACK.

NOTE: NSPT IS DEFINED AS THE SUM OF ALL FIXED POINTS PLUS ONE HALF OF ALL ANCHOR POINTS SPECIFIED IN THE NSLPBL FIELDS OF ALL D.3.C CARDS, IN OTHER WORDS, THE TOTAL NUMBER OF INDIVIDUAL SLIP POINTS FOR ALL BELTS.

IF NBLT (THE NUMBER OF BELTS) IS NONZERO ON CARD D.1, CARDS F.2 ARE REQUIRED.

CARD F.2.A FORMAT (8I4)

MNBLT(J), J=1, NBLT FOR BELT J, THE NUMBER OF SEGMENTS FOR WHICH
SEGMENT-BELT INTERACTION IS ALLOWED (0 OR 1
ONLY).

FOR EACH BELT J, MNBLT(J) CARDS OF THE FOLLOWING MUST BE SUPPLIED.

CARDS F.2.B - F.2.N FORMAT (9I4)

NJ THE BELT NUMBER TO BE CONTACTED, MUST CORRESPOND
TO J ABOVE. THERE MUST BE MNBLT(J) CARDS WITH
THE SAME NJ. IF MNBLT(J) = 0, NO NJ = J SHOULD
BE PRESENT.

NS(1) SUPPLY NSEGA + 100 * NSEGB WHERE NSEGA IS THE
SEGMENT NUMBER FOR ANCHOR A AND NSEGB IS THE
SEGMENT NUMBER FOR ANCHOR B. IF NSEGA AND NSEGB
ARE THE SAME, SUPPLY ONLY NSEGA. (NOTE 1
APPLIES TO BOTH NSEGA AND NSEGB)

NS(2) SUPPLY NOBODY WHICH IS THE NUMBER OF THE SEGMENT
TO WHICH THE CONTACT ELLIPSOID IS
ATTACHED. (NOTE 1 APPLIES TO NOBODY).

NS(3) THE NUMBER OF THE CONTACT ELLIPSOID ATTACHED TO
THE SEGMENT NOBODY.

NF(1) THE FUNCTION NUMBER FROM CARD E.1 TO DEFINE THE
FORCE-DEFLECTION FUNCTION FOR THIS CONTACT. THE
ABSCISSA FOR THIS FUNCTION SHOULD BE STRAIN
(IN/IN).

NF(I), I=2, 4 SAME DEFINITION AS ON CARD F.1.B ABOVE.

NF(5) IF NON-ZERO, FULL BELT FRICTION IS ASSUMED,
I.E., FORCES ARE COMPUTED FOR EACH HALF OF THE
BELT SEPARATELY. IF ZERO, ZERO BELT FRICTION IS
ASSUMED I.E., BELT TENSION IS THE SAME AT BOTH
BELT ANCHOR POINTS. IF THE FIXED POINT FOR BELT
NJ IS SPECIFIED AS A SLIP POINT ON A F.9 CARD,
THIS FIELD IGNORED.

NOTES:

1. ONE OF THREE OPTIONS IS CHOSEN BY USER:
(A) THE CARD NUMBER I UNDER CARD B.2.A FOR ANY BODY SEGMENT,
(B) NVEH FOR THE PRINCIPAL VEHICLE, OR
(C) NGRND FOR THE INERTIAL FRAME (GROUND).
2. THE USE OF RATE DEPENDENT FUNCTION AS DEFINED UNDER CARDS F.1.B.
ARE NOT CURRENTLY OPERATIONAL FOR BELT-SEGMENT CONTACTS.

F.9 SUBROUTINE SLPINP - CARD INPUT FOR SEAT BELT FEED THROUGH DATA.
(NSPT CARDS REQUIRED, SEE NOTE ON CARD D.3.C.)

CARDS F.9 FORMAT (I4,3X,A1,I4,3X,A1,5F10.0)

NBSP(I,J),I=1,4 TWO PAIRS OF VALUES SPECIFYING THE BELT
 NUMBER AND POINT CODE FOR EACH BELT NODE
 COINCIDENT AT SLIP POINT J.
 POINT CODES: A = ANCHOR A
 B = ANCHOR B
 F = FIXED POINT
 (ONLY ONE BELT INVOLVED IF POINT CODE
 "F".)

SFRICT(1,J) IF POSITIVE, THE FRICTION COEFFICIENT AT
 SLIP POINT J. (LBS/LBS). IF NEGATIVE, THE
 FUNCTION NUMBER FOR FRICTION FORCE (MUST
 BE NON-NEGATIVE) VS NORMAL FORCE.

SFRICT(2,J) THE CONSTANT TERM OF THRESHOLD FORCE (MUST
 BE NON-NEGATIVE). (LBS.) THIS ACTS
 TOGETHER WITH NEXT QUANTITY.

SFRICT(3,J) THE COEFFICIENT OF THRESHOLD FORCE (LBS/
 LBS). THE TOTAL THRESHOLD FORCE IS
 OBTAINED BY MULTIPLYING THIS BY SLIP
 NORMAL FORCE AND ADDING SFRICT(2,J).

SFRICT(4,J) THE INITIAL SLIP INCREMENT TO BE
 USED. (IN.) (UNUSED AT PRESENT TIME)

SFRICT(5,J) MAXIMUM RATE OF SLIP WHICH IS ALLOWABLE
 (IN./SEC.). (UNUSED AT PRESENT TIME)

NOTES: 91. BELT NODES SPECIFIED MUST BE EITHER ONE FIXED POINT
OR TWO ANCHOR POINTS WHICH MUST BE COINCIDENT IN BOTH POSITION
AND SPECIFICATION OF ATTACHMENT SEGMENT.

92. SFRICT(1,J) AND SFRICT(2,J) CAN NOT BOTH BE SPECIFIED ZERO.

APPENDIX B

DERIVATION OF THE SLIP FORCE EQUILIBRIUM EQUATION

This appendix refers to and amplifies Section 4.2.3 and Figure 4.5. Slip point k-1 is located at $(x_{k-1}, y_{k-1}, z_{k-1})$ in inertial space. Belt segment k-1 terminates at slip point k-1 and begins at slip point k-2 or loop anchor A which is located at $(x_{k-2}, y_{k-2}, z_{k-2})$ in inertial space. Belt segment k begins at slip point k-1 and terminates at slip point k or loop anchor B which is located at (x_k, y_k, z_k) in inertial space. As before let l_k be the strained belt length of belt segment k and let L_k be the unstrained belt length of belt segment k. The strained belt lengths are determined geometrically. Total unstrained belt length for any loop is determined from the initial conditions supplied by the user. Individual unstrained belt lengths are determined to meet the slip equilibrium requirements and maintain the user-specified total unstrained belt length of the loop.

So

$$l_{k-1} = \sqrt{(x_{k-1} - x_{k-2})^2 + (y_{k-1} - y_{k-2})^2 + (z_{k-1} - z_{k-2})^2}$$

and

$$l_k = \sqrt{(x_k - x_{k-1})^2 + (y_k - y_{k-1})^2 + (z_k - z_{k-1})^2}$$

Define

$$\bar{f}_{k-1} = \begin{pmatrix} a_{k-1} \\ \beta_{k-1} \\ \gamma_{k-1} \end{pmatrix} \quad \text{and} \quad \bar{f}_k = \begin{pmatrix} a_k \\ \beta_k \\ \gamma_k \end{pmatrix}$$

where

$$\begin{aligned}
 a_{k-1} &= \frac{1}{l_{k-1}}(x_{k-2} - x_{k-1}) & a_k &= \frac{1}{l_k}(x_k - x_{k-1}) \\
 \beta_{k-1} &= \frac{1}{l_{k-1}}(y_{k-2} - y_{k-1}) & \beta_k &= \frac{1}{l_k}(y_k - y_{k-1}) \\
 \gamma_{k-1} &= \frac{1}{l_{k-1}}(z_{k-2} - z_{k-1}) & \gamma_k &= \frac{1}{l_k}(z_k - z_{k-1})
 \end{aligned}$$

These are the unit vectors along the two belt segments k-1 and k, respectively based at the slip point and pointing toward the respective anchors.

Now

$$\cos(2\Omega_{k-1}) = \bar{f}_{k-1} \cdot \bar{f}_k = a_{k-1}a_k + \beta_{k-1}\beta_k + \gamma_{k-1}\gamma_k$$

Define

$$\bar{F}_{k-1} = F_{k-1}\bar{f}_{k-1} \quad \text{and} \quad \bar{F}_k = F_k\bar{f}_k$$

These are the belt tension force vectors at the slip point along the two belt segments, respectively. British Leyland defines the normal direction as a unit vector called $f_{n,k-1}$ where

$$\bar{f}_{n,k-1} = \frac{\bar{f}_{k-1} + \bar{f}_k}{|\bar{f}_{k-1} + \bar{f}_k|}$$

and the tangential direction as

$$\bar{f}_{s,k-1} = \frac{\bar{f}_{k-1} - \bar{f}_k}{|\bar{f}_{k-1} - \bar{f}_k|}$$

Note that

$$|\bar{f}_{k-1} + \bar{f}_k| = \pm 2 \cos(\Omega_{k-1})$$

and

$$|\bar{f}_{k-1} - \bar{f}_k| = \pm 2 \sin(\Omega_{k-1})$$

These expressions are determined by substitution of components into the definitions of vector magnitudes and application of trigonometric identities. British Leyland defined the normal and tangential force magnitudes as the scalar product of the force resultant vector with the two direction vectors.

$$F_{n,k-1} = (\bar{F}_{k-1} + \bar{F}_k) \cdot \bar{f}_{n,k-1}$$

and

$$F_{s,k-1} = (\bar{F}_{k-1} + \bar{F}_k) \cdot \bar{f}_{s,k-1}$$

Substituting definitions and simplifying, the normal force magnitude becomes

$$\begin{aligned} F_{n,k-1} &= (F_{k-1} \bar{f}_{k-1} + F_k \bar{f}_k) \cdot \frac{\bar{f}_{k-1} + \bar{f}_k}{|\bar{f}_{k-1} + \bar{f}_{k-1}|} \\ &= \frac{(F_{k-1} + F_k) (1 + \cos(2\Omega_{k-1}))}{\pm 2 \cos(\Omega_{k-1})} \\ &= \pm (F_{k-1} + F_k \cos(\Omega_{k-1})) \end{aligned}$$

Likewise for tangential or slip force magnitude,

$$\begin{aligned} F_{s,k-1} &= \frac{(F_{k-1} - F_k) (1 - \cos(2\Omega_{k-1}))}{\pm 2 \sin(\Omega_{k-1})} \\ &= \pm (F_{k-1} - F_k) \sin(\Omega_{k-1}) \end{aligned}$$

The slip resistance force vector at the slip point ($\bar{F}_{R,k-1}$) is assumed to be due to friction force at the slip point ($\bar{F}_{F,k-1}$) and threshold force at the slip point ($F_{T,k-1}$). Threshold force includes the differences between static and kinetic friction while friction force is includes kinetic effects only.

So that

$$F_{R,k-1} = F_{F,k-1} + F_{T,k-1}$$

where

$$F_{F,k-1} = \mu_{k-1} F_{n,k-1}$$

and

$$F_{t,k-1} = C_{1,k-1} F_{n,k-1} + C_{2,k-1}$$

μ_{k-1} is the inputted coefficient of friction,

$C_{1,k-1}$ is the inputted coefficient of threshold force, and

$C_{2,k-1}$ is the inputted constant threshold force.

The direction of $\bar{F}_{R,k-1}$ is opposite to that of $\bar{F}_{S,k-1}$.

In the British Leyland algorithm, slipping will occur if

$$F_{S,k-1} > F_{F,k-1} + F_{T,k-1}$$

and the iteration to adjust the unstrained lengths in order to reduce $F_{S,k-1}$ until $F_{F,k-1} < F_{S,k-1} < F_{F,k-1} + F_{T,k-1}$. This is the interval of convergence.

We will define a target variable V_{k-1} which assumes the value of zero in the center of the interval of convergence as

$$V_{k-1} = F_{S,k-1} + \eta_{k-1} F_{R,k-1}$$

where η_{k-1} is assigned the value of +1 or -1 depending on the relative direction of slip resistance forces when equilibrium is reached. Note that slip resistance will always oppose slip force, but if the equation is to predict equilibrium, then it must reflect the direction of slip resistance at equilibrium which may or may not be the same as the direction of slip resistance where the iteration is started.

The equilibrium condition then is taken to be $V_{k-1}=0$.

When computed during the iteration, convergence is defined as

$$|V_{k-1}| \leq \frac{1}{2} F_{T,k-1}$$

Note that this condition corresponds to the previous interval of convergence. Now substituting the previously developed expressions

$$V_{k-1} = 0 = (F_{k-1} - F_k) \sin(\Omega_{k-1}) + \eta_{k-1} [h_{1,k-1}(F_{k-1} + F_k) \cos(\Omega_{k-1}) + h_{2,k-1}]$$

and collecting on F_{k-1} and F_k ,

$$\lambda_{A,k-1} F_{k-1} + \lambda_{B,k-1} F_k + \lambda_{C,k-1} = 0$$

where

$$\lambda_{A,k-1} = \sin(\Omega_{k-1}) + \eta_{k-1} h_{1,k-1} \cos(\Omega_{k-1})$$

$$\lambda_{B,k-1} = -\sin(\Omega_{k-1}) + \eta_{k-1} h_{1,k-1} \cos(\Omega_{k-1})$$

$$\lambda_{C,k-1} = \eta_{k-1} h_{2,k-1}$$

APPENDIX C

TAPE DESCRIPTION AND INSTALLATION NOTES

C.1 Introduction

The software produced as part of the CVS belt software project is submitted in the form of magnetic tape number BSC023. The remaining sections of this appendix present a description of the physical layout of tape BSC023, a description of each piece of software included on the tape, and notes concerning installation of this software at GMR including a summary of changes made in the UMTRI version (GUCVS) of the GMR version (GMCVS) of the Calspan CVS, Version 20.

C.2 Tape Description of Tape BSC023

Tape BSC023 is an unlabelled, EBCD, nine-track magnetic tape with eleven files and the following properties: RECFM = FB, BLKSIZE = 2400, and LRECL = 80 written at 6250 BPI. Table C.1 summarizes the contents by file.

TABLE C.1

DESCRIPTION OF TAPE BSC023

File No.	Code Name	Description	Seq ID (col 73-74)	No. of Records	No. of Blocks
1	ODIC1.FORT	GMCVS Part I	num 73-80	6,824	228
2	ODIC3.FORT	GMCVS Part II	num 73-80	6,443	215
3	CIGS	GUCVS Part I	IG	13,080	436
4	CUTS	GUCVS Part II	UT	1,363	46
5	ROBMULTESTS	Deflection 2 Code	ED	830	28
6	ROBEPLMULT	Unstrained Change	EP	792	27
7	ROBDELOMULT	Deflection 1 Code	DZ	811	28
8	RIGS	Slip GUCVS Part I	RI	3,395	114
9	RUTS	Slip GUCVS Part II	RU	353	12
10	ROBPLOTCS.S	Ellip Man Plotter	CS	1,330	45
11	ROBMULTEST.D	Test Data for 5-7	None	168	6

C.3 Software Descriptions

ODIC1.FORT and ODIC3.FORT are duplicates of the GMCVS files from which UMTRI started. They are included to serve as a reference point from which to understand the updates which UMTRI made in creating GUCVS. It may be useful to compare these two old GM files with the corresponding current GM files in order to pinpoint where the changes reported in the next section relative to these two old files fit relative to current GM files.

While ODIC1.FORT and ODIC3.FORT were just the GMCVS divided into two rather equal files for ease of handling, CIGS and CUTS represent a division of the model into two processors to be run usually in succession. This division was made for two reasons: first, it makes recovering printout on an aborted run easier (sometimes automatic if the model is run under procedure control), and secondly, it reduces the total virtual memory needed to run the model without either reducing model features or increasing the cost of a model run. Part 6 of this report gives a short discussion of model improvements incorporated in GUCVS.

ROBMULTESTS, ROBEPLMULT, and ROBDELOMULT are three stand alone packages which consist of a test main, a trial version of the new CVS model subprogram, "BLTSOL" (which has the task of obtaining a solution to the belt slip equilibrium equations, see Section 4.2.3), and needed service routines either pulled from the model intact or dummied. Each of these packages use the same data formats to describe the desired test cases. ROBMULTEST.D is the data for the standard group of tests which was used to test these three approaches.

ROBEPLMULT is the approach discussed in Section 4.2.5 . This package contains one coding error which invalidates the results for the N=4 cases. Since it was clear from the N=2 and N=3 cases that the approach had failed, there was no purpose in finding and correcting this error.

ROBDELOMULT and ROBMULTESTS are the two approaches discussed in Section 4.6 of Part I. There are no known coding errors in these two packages.

RIGS and RUTS contain replacement and new subprograms for GUCVS to implement the new belt slip algorithms. The subprograms in CIGS for which changes were required (and for which changed versions are included in RIGS) are BELTRT, CINPUT, CONTCT, OUTREC, OUTPUT, SINPUT, and UPDATE. Table C.2 contains a short description of the functions of each of the new subprograms included in RIGS. The subprograms in CUTS for which changes were required (and for which changed versions are included in RUTS) are BLOCK DATA, HEDING, and PRTLIN. All these routines are only partially tested and are subject to further changes.

ROBPLOTCS.S is the source for the Ellipsoid Man Plotting Program which UMTRI used instead of the VIEW Plotting Program. GUCVS will optionally produce the exterior binary hold files required by both/ either/neither of these plotting programs. ROBPLOTCS.S makes use of the regular Calcomp Plotting Routines whereas VIEW makes use of the DISSPLA plotting routines.

TABLE C.2

NEW BELT SLIP ALGORITHM ROUTINES

Routine Name	Description of Function
BLDERV	Obtains approximations to belt material derivatives for one specified belt loop and one specified unstrained belt length configuration of four possible unstrained belt length configurations.
BLEVL	Evaluates belt tension, normal forces, and slip forces for all slip points in all belt loops for one specified unstrained belt length configuration.
BLTSLP	Is the main control routine for the belt slip algorithm. It calls the other belt slip routines as necessary to handle for each belt loop separately the applicable cases of non-slipping belts, free-slipping belts under slack, or slipping under friction. The last case is handled by setting up and solving up to four belt configurations in order to determine the minimum amount of belt slip which satisfies the belt slip equilibrium equations.
BLTSOL	Solves for unstrained belt lengths which satisfy the belt slip equilibrium equations for a specified belt loop and a specified belt configuration.
BLTUPD	Updates the unstrained belt lengths for which values at current and last previous simulated times are maintained.
BLTVAL	Evaluates belt tension forces for a specified regular belt or around a specified belt slip point.
POLRT	Computes real and complex roots of a real polynomial by the Newton-Raphson iterative technique.
SLPINP	Reads the F.9 input data cards and sets up the appropriate control and data internal storage arrays.

C.4 Installation Notes

This section documents the updates necessary to turn the GMCVS presented on tape BSC023 into the GUCVS also presented on this tape. Table C.3 is the index of the collected output of several runs of a comparison program on the MTS System of the files CVSA and CVSB (which are MTS line file versions of tape files ODIC1.FORT and ODIC3.FORT, respectively) and the files CIGS and CUTS (which are MTS line file versions of tape files CIGS and CUTS, respectively). The collected output is included as Table C.5. In all cases the sequence fields have been stripped off to enable the comparisons to be based solely on program content.

Line files are characterized by line numbers which identify each line of information separately from line contents. This allows sequencing to be maintained without disturbing comparisons of content. Line numbers in the file listings which accompany tape BSC023 correspond to the number of the record in the tape file in each case. These tape file listings show the line number for each tape record on the left followed by the 80 characters of contents which includes the sequencing information.

Table C.3 also shows the line number for each displayed line at the left. The output of the comparison program shows lines from the two files being compared side by side on as many printout lines as required to display the total contents of both lines. Every pair of lines which are the same character by character and which are displayed are designated by "=" on the extreme left and right of each printout line required to display the entire lines. The only equal lines which are displayed are those which begin the interval of comparison, end the interval of comparison, precede an unequal line, or follow an unequal line. The equal lines which are not displayed are counted in a summary of omitted lines which is printed in the place of the omitted equal lines. Every line in either file for which a difference is found or for which no corresponding line is found is displayed without the "=" on the extreme left and right of each printout line.

The output of the several comparison runs are ordered in Table C.3 on the sequence of the line intervals in CVSA and CVSB. Any line

intervals which are missing in Table C.3 are either exactly the same, or bear no relationship to the other file. A list of the sections of the code which have been changed are included as Table C.4. The changed listings are included as Table C.6.

TABLE C.3

COMPARISON OF GUCVS WITH GMCVS

GUCVS Lines	GMCVS Lines
CVSA(1,249)	CIGS(1,246)
CVSA(250,856)	CIGS(247,856)
CVSA(861,1778)	CIGS(857,1781)
CVSA(1779,3506)	CIGS(1782,3508)
CVSA(3507,3781)	CIGS(3509,3782)
CVSA(5235,6258)	CIGS(5257,6304)
CVSA(6420,6824)	CUTS(835,1122)
CVSB(166,1501)	CIGS(6527,7862)
CVSB(1502,1830)	CIGS(7863,8445)
CVSB(2564,2877)	CIGS(9161,9474)
CVSB(2918,4698)	CIGS(9544,11350)

TABLE C.4

COMPLETELY NEW OR EXTENSIVELY CHANGED CODE

1.	Subroutine DRCQUA	(new code)
2.	Subroutine OUTREC	(new code)
3.	Subroutine PLOTR1, PLOTR2, PLOTRA	(new code)
4.	Subroutine QUAT	(new code)
5.	Subroutine STASH	(new code)
6.	Main program for CUTS replaces old subroutine POSTPR	(new code)
7.	Old subroutine POSTPR (CVSB) replaced by CUTS Main	
8.	Subroutine FETCH	(new code)
9.	New dummied subroutine HICCSI	
10.	Old subroutine HICCSI	
11.	Subroutine INREAD	(new code)
12.	Subroutines PICKUP and PRTLIN	(new code)
13.	New dummied subroutine SLPLOT	
14.	Old subroutine SLPLOT	
15.	Subroutines VECADD and VECSUB	(new code)

Line	Block Data	Line	Block Data
1		1	
30	F,NSSF,NBGSF COMMON/RSERVE/ XSG(3,20,3).DPMI(3,3,100),LPMI(1 OO),NSG(7) *MSG(20,7) COMMON/CDINT/ UU(4),GH(3,4), E(3,800),FF(5,800),GG(5,800),Y(5,800),U(5,800), H,HPRINT,TSAVE,TPRINT,TSTART,IC NT,IDBL,IFLAG, * DMMY(200,25),DMMY2(5000,25) COMMON/DAMPER/ APSDM(3,20),APSDN(3,20),ASD(5,2 O),MSDM(20),MSDN(20) * ISTEP,NSTEPS,NDINT,NEQ,IRSN,IR	28 equal lines	PRJNT(7,100),NPANEL(5),NPSF,NBS F,NSSF,NBGSF COMMON/RSERVE/ DPMI(3,3,100),LPMI(100) * COMMON/CDINT/ UU(4),GH(3,4), E(3,800),FF(5,800),GG(5,800),Y(5,800),U(5,800), H,HPRINT,TSAVE,TPRINT,TSTART,IC * COMMON/DAMPER/ APSDM(3,20),APSDN(3,20),ASD(5,2 O),MSDM(20),MSDN(20) * ISTEP,NSTEPS,NDINT,NEQ,IRSN,IR
31		31	
32		32	
33		33	
34		34	
35		35	
36		35	
37		35	
98	SOUT	96	SOUT
99	LOGICAL NPRT1,NPRT2,NPRT3	97	LOGICAL NPRT1,NPRT2,NPRT3 ,NPRT18
100	CALL ELTIME(1,1)	98	CALL ELTIME(1,1)
109	1*****	107	1*****
110	111 FORMAT(3(22X,'*****',70X,'*****',/),22X,'*** **',9X, 2'GGGGGG',6X,'MM MM',6X,'CCCCCCC',6X,'VV V V',6X,'SSSSSS',5X, 2'*****',/22X,'*****',9X, 3'GG G',6X,'MM MM',6X,'CCCCCCC',6X,'VV V V',6X,'SSSSSS',5X, 3'*****',/22X,'*****',9X, 4'GG',6X,'MMM MMM',6X,'CC ,6X,'SS ,5X, 4'*****',/22X,'*****',9X, 9'GG GGG',6X,'MMM MMM',6X,'CC ,6X,'SSSSSS',5X, 9'*****',/22X,'*****',9X, 5'GG GG',6X,'MM M MM',6X,'CC ,6X,'SS',5X, 5'*****',/22X,'*****',9X, 6'GG GG',6X,'MM M MM',6X,'CCCCCCC',6X,' VVV ,6X,'SSSSSS',5X, 6'*****',/22X,'*****',9X, 7'GGGGG G',6X,'MM MM',6X,'CCCCCCC',6X,' V ,6X,'SSSSSS',5X, 7'*****',/22X,'*****',9X, 112 FORMAT(3(22X,'*****',73X,'*****',/),22X,'*** ***',17X, 8' X, *****',73X,'*****',/ 17 FORMAT('O NPRT ARRAY'/3X,36I3/3X,36I3) NPRT4 = NPRT(4) IF (NPRT(4).LT.O) GO TO 50		
111		109	
112		110	
113		111	
114		112	
115		113	
116		114	
117		115	
118		116	
119		117	
120		118	
121		119	
122		120	
123		121	
124		122	
125		123	
126		124	
127		125	
158		156	
159		156	
160		156	
161		157	
183		179	
184		180	

Table C.5. Comparison of GUCVS with GMCVS (Page 1 of 41)


```

= 185 AL ****') RETURN
= 186 CALL RSTART(1,IRSIN)
= 187 CALL RSTART(4,5)
= 188 NPRT4 = NPRT(4)

= 189 19 IF (IRSOUT.NE.O) CALL RSTART(2,IRSOUT)
=====
= 201 21 CALL RSTART(4,5)
= 202 IF (NPRT(4).LT.O) GO TO 50
= 203 23 CALL DINT
=====
= 225 C
= 226 C 5. SUBROUTINE ELTIME ON PRIMARY OUTPUT UNIT CO
NTROLLED BY NPRT(2).
=====
= 227 C
=====
= 228 NPRT18 = (NPRT(18).EQ. 1)
= 229 IF (NPRT(18).GT. 1) NPRT18 = (MOD(ISTEP,NPRT(
= 230 18)).EQ. O)
= 231 IF (NPRT(18).NE. O .AND. ISTEP .EQ. O) CALL P
LOTR1
= 232 IF (NPRT18) CALL PLOTR2
= 233 C
= 234 C 6. SUBROUTINE ELTIME ON PRIMARY OUTPUT UNIT CO
NTROLLED BY NPRT(2).
=====
= 235 C
=====
= 236 IF (ISTEP.LE.NSTEPS) GO TO 20
= 237 C 6. SUBROUTINE POSTPR ON PRIMARY OUTPUT UNIT CO
NTROLLED BY NPRT(4).
=====
= 238 C
= 239 50 IF (NPRT4.GT.O) END FILE 8
= 240 IF (NPRT(4).EQ.O .OR. NPRT(4).EQ.4) GO TO 60
= 241 PRDT = 1000.O*DT
= 242 CALL POSTPR (PRDT)
= 243 IF (NPRT2) CALL ELTIME (2,1)
= 244 C
=====
= 246 C
= 247 60 IF (.NOT.NPRT2) CALL ELTIME (2,1)
= 248 STOP 1
= 249 END

=====
= 181 AL ****') RETURN
= 182 C *****
= 183 C REGULAR RESTART CODE IS COMMENTED OUT BELOW.
= 184 C
= 185 C CALL RSTART(1,IRSIN)
= 186 C CALL RSTART(4,5)
= 187 19 IF (IRSOUT.NE.O) CALL RSTART(2,IRSOUT)
=====
= 199 21 CALL RSTART(4,5)
=====
= 200 23 CALL DINT
=====
= 222 C
= 223 C 5. PROGRAM PLOTCS PLOT DATA ON UNIT 9 CONTROL
LED BY NPRT(18).
=====
= 224 C
= 225 NPRT18 = (NPRT(18).EQ. 1)
= 226 IF (NPRT(18).GT. 1) NPRT18 = (MOD(ISTEP,NPRT(
18)).EQ. O)
= 227 IF (NPRT(18).NE. O .AND. ISTEP .EQ. O) CALL P
LOTR1
= 228 IF (NPRT18) CALL PLOTR2
= 229 C
= 230 C 6. SUBROUTINE ELTIME ON PRIMARY OUTPUT UNIT CO
NTROLLED BY NPRT(2).
=====
= 231 C
=====
= 239 IF (ISTEP.LE.NSTEPS) GO TO 20
= 240 50 IF (NPRT2) CALL ELTIME (2,1)
=====
= 241 C
= 242 C
= 243 IF (.NOT.NPRT2) CALL ELTIME (2,1)
= 244 STOP 1
= 245 END
= 246

```

Table C.5. Comparison of GUCVS with GMCVS (Page 2 of 41)

Unit 0: CVSA(250,856)

Unit 1: SUSP:CIGS(247,856)

=	250	SUBROUTINE ADJUST (M,D1)		247	SUBROUTINE ADJUST (M,D1)	=
-----			5 equal lines	-----		-----
=	256	* E(3,800), F(5,800),GG(5,800),Y(5		253	* E(3,800), F(5,800),GG(5,800),Y(5	=
=		,800),U(5,800),			,800),U(5,800),	=
=	257	* H,HPRINT,HS,TPRINT,TSTART,ICNT,I		254	* H,HPRINT,HS,TPRINT,TSTART,ICNT,I	=
		DBL,IFLAG,			DBL,IFLAG	
=	258	* DMMY(200,25)				=
=	259	COMMON/COMAIN/ VAR(800),DER(800),DT,HO,HMAX,HM		255	COMMON/COMAIN/ VAR(800),DER(800),DT,HO,HMAX,HM	=
		IN,RSTIME,			IN,RSTIME,	
-----			362 equal lines	-----		-----
=	622	C		618	C	=
	623	L = NSEG + NBAG + 2		619	L = NGRND + NBAG	
	624	K = NSEG + 2		620	K = NGRND	
=	625	W(L) = W(K)		621	W(L) = W(K)	=
-----			16 equal lines	-----		-----
=	642	19 SGTEST(I,4,L) = SGTEST(I,4,K)		638	19 SGTEST(I,4,L) = SGTEST(I,4,K)	=
	643	NGRND = NSEG + NBAG + 2		639	NGRND = NGRND + NBAG	
=	644	DO 40 J=1,NBAG		640	DO 40 J=1,NBAG	=
-----			211 equal lines	-----		-----
=	856	49 PYMOUT(J) = CYMOUT(J)		852	49 PYMOUT(J) = CYMOUT(J)	=
				853	50 CONTINUE	
				854	99 CALL ELTIME(2,29)	
				855	RETURN	
				856	END	

```

=====
= 861 SUBROUTINE BELTG (ZA,ZB,ZC,BD) 857 SUBROUTINE BELTG (ZA,ZB,ZC,BD)
= 1042 SUBROUTINE BELTRT(I,II,MM,M,NT) 1038
= 1043 C SUBROUTINE BELTRT(I,II,MM,M,NT)
=====
= 1044 REV 20 05/23/80
= C THE ROUTINE CALLS SUBROUTINE BELTG TO COMPUTE 1039
= THE TANGENT POINTS 180 equal lines
= 1051 * NS,NQ,NSD,NFLX,NHRNSS,NWINDF,NJ 6 equal lines
= NTF,NPRT(36) 1046
= COMMON/SGMNTS/ D(3,3,100),WMEG(3,100),WMEGD(3, 1047
= U1(3,100), 100),U1(3,100),
= * U2(3,100),SEGLP(3,100),SEGLV(3,100),SEGLA(3, 1048
= (3,100),NSYM(100)
= COMMON/CNTRSFR/ PL(17,100),BELT(20,8),TPTS(6,8) 1049
= ,BD(24,110)
= COMMON/TABLES/MXNTI,MXNTB,MXTB1,MXTB2,NTI(300) 1050
= ,NTAB(3000),
= *TAB(9600)
= COMMON/FORCES/ PSF(7,100),BSF(4,20),SSF(10,20) 1051
= ,BAGSF(3,20), 1052
= * PRJNT(7,100),NPANEL(5),NPSF,NBS 1053
= F,NSSF,NBGSF
=====
= 1068 C 9 equal lines
= 1069 MA = MM 1063
= 1070 MB = MM 1064
=====
= 1071 CALL DOT31 (D(1,1,MA),BELT(1,M),TA) 1066
= 1159 CALL DOT31(D(1,1,I),UVB,TTT) 87 equal lines
= 1160 DO 30 K=1,3 1155
= TTT(K) = TTT(K)+TT(K) 1156
= 30 U1(K,I) = U1(K,I)+TTT(K) 1157
= 1158 1157
= 1159 1158
= 1160 1159
= 1163 C 1 equal line
= 1165 C 1 equal line
=====
= 1166 CALL CROSS(APA,UVA,TT)
= 1168 DO 40 K=1,3 1 equal line
=====
= 1169 40 U2(K,I) = U2(K,I)+(TT(K)+TTT(K))
= 1367 * UNITL,UNITM,UNITT,GRAVITY(3) 197 equal lines
= 1368 COMMON/RSAVE/XSG(3,20,3),DPMI(3,3,100),LPMI(10 1370
= O),NSG(7),MSG(20,7)
= 1369 COMMON/TEMPVS/ YPR1(3,100),YPR2(3,100),YPR3(3, 1372
= 100),YPRPMI(3,100),
= * UNITL,UNITM,UNITT,GRAVITY(3) 66 equal lines
= 1436 1 UNITL,UNITM,UNITT,GRAVITY(3) 1439
= 1437 COMMON/RSAVE/XSG(3,20,3),DPMI(3,3,100),LPMI(10 1440
= O),NSG(7),MSG(20,7)
=====

```

```

= 1438      COMMON/TEMPVS/ YPR1(3,100),YPR2(3,100),YPR3(3,
=          100),YPRPMI(3,100),
=          COMMON/TEMPVS/ YPR1(3,100),YPR2(3,100),YPR3(3,
=          100),YPRPMI(3,100),
= 1778      END
=          END
=          339 equal lines
=          1781
=          END

```

Unit 0: CVSA(1779,3506)

Unit 1: SUSP:CIGS(1782,3508)

```

= 1779      SUBROUTINE CFACTT(A,B,D)                                1782      SUBROUTINE CFACTT(A,B,D)                                =
----- 196 equal lines -----
= 1976      *      E(3,800), F(5,800),GG(5,800),Y(5,800),          1979      *      E(3,800), F(5,800),GG(5,800),Y(5,800),          =
=          O),U(5,800),                                           O),U(5,800),                                           =
= 1977      *      H,HPRINT,HS,TPRINT,TSTART,ICNT,IDBL           1980      *      H,HPRINT,HS,TPRINT,TSTART,ICNT,IDBL           =
=          ,IFLAG,                                               ,IFLAG,                                               =
= 1978      *      DMMY(200,25)                                    1981      *      DMMY(200,25)                                    =
= 1979      COMMON/COMAIN/ VAR(800),DER(800),DT,HO,HMAX,HM        1981      COMMON/COMAIN/ VAR(800),DER(800),DT,HO,HMAX,HM        =
=          IN,RSTIME,                                           IN,RSTIME,                                           =
----- 4 equal lines -----
= 1984      CALL DZP (NEQ,VAR,GG,E,FT,M)                          1986      CALL DZP (NEQ,VAR,GG,E,FT,M)                          =
= 1985      IF (NPRT(26).EQ.2) CALL OUTPUT(0)                    1987      IF (NPRT(4).EQ.2) CALL OUTPUT(0)                    =
= 1986      CALL PDAUX (VAR,DER,NEQ,K)                          1988      CALL PDAUX (VAR,DER,NEQ,K)                          =
= 1987      IF (NPRT(26).EQ.2) CALL OUTPUT(1)                    1989      IF (NPRT(4).EQ.2) CALL OUTPUT(1)                    =
= 1988      RETURN                                              1990      RETURN                                              =
----- 230 equal lines -----
= 2219      J2      IF (NJ2.GT.200) WRITE (6,11) NS,NFLX,NQ,NJNT,N 2221      J2      IF (NJ2.GT.200) WRITE (6,11) NS,NFLX,NQ,NJNT,N =
=          11 FORMAT('ONS=',I6,',NFLX=',I6,',NQ=',I6,',NJNT=    2222      11 FORMAT('ONS=',I6,',NFLX=',I6,',NQ=',I6,',NJNT=
=          ',I6,' AND NJ2=',I6/                                ',I6,' AND NJ2=',I6/
= 2221      *' THE VALUE OF NJ2 EXCEEDS THE ARRAY SIZES FOR     2223      *' THE VALUE OF NJ2 EXCEEDS THE ARRAY SIZES FOR =
=          RHS AND IJK IN SUBR                                RHS AND IJK IN SUBR
----- 1284 equal lines -----
= 3506      END                                                  3508      END

```

Unit 0: CVSA(3507,3781)

Unit 1: SUSP:CIGS(3509,3782)

= 3507	SUBROUTINE DHHPIN(DD,BN,L,M,N)	43 equal lines	3509	SUBROUTINE DHHPIN(DD,BN,L,M,N)	=
= 3551	* E(3,800), F(5,800),GG(5,800),Y(5,800),U(5,800),		3553	* E(3,800), F(5,800),GG(5,800),Y(5,800),U(5,800),	=
= 3552	* H,HPRINT,HS,TPRINT,TSTART,ICNT,IDBL		3554	* H,HPRINT,HS,TPRINT,TSTART,ICNT,IDBL	=
3553	,IFLAG,			,IFLAG	
= 3554	* DMMY(200,25)		3555	* DMMY(200,25)	=
=	COMMON/COMAIN/ VAR(800),DER(800),DT,HO,HMAX,HM			COMMON/COMAIN/ VAR(800),DER(800),DT,HO,HMAX,HM	=
=	IN,RSTIME,			IN,RSTIME,	=
= 3588	ICNT = -2	33 equal lines	3589	ICNT = -2	=
3589	IF (ISTEP.EQ.O .OR. NPRT(26).EQ.2) CALL OUT		3590	IF (ISTEP.EQ.O .OR. NPRT(4).EQ.2) CALL OUTP	=
= 3590	PUT(O) CALL PDAUX (VAR,DER,NEQ,K)		3591	UT(O) CALL PDAUX (VAR,DER,NEQ,K)	=
3591	IF (ISTEP.NE.O .AND. NPRT(26).EQ.2) CALL OUT		3592	IF (ISTEP.NE.O .AND. NPRT(4).EQ.2) CALL OUTP	=
= 3592	PUT(1) DO 14 I=1,NEQ		3593	UT(1) DO 14 I=1,NEQ	=
= 3630	IF (L.EQ.1) M = 0	37 equal lines	3631	IF (L.EQ.1) M = 0	=
3631	IF (NPRT(26).NE.2) CALL OUTPUT(O)		3632	IF (NPRT(4).NE.2) CALL OUTPUT(O)	=
= 3632	CALL CMPUTE (K,M, H)		3633	CALL CMPUTE (K,M, H)	=
= 3679	58 IF (H.LE.HMIN+EPS(8)) GO TO 61	46 equal lines	3680	58 IF (H.LE.HMIN+EPS(8)) GO TO 61	=
3680	IF (NPRT(26).EQ.2) CALL OUTPUT(1)		3681	IF (NPRT(4).EQ.2) CALL OUTPUT(1)	=
= 3681	59 TIME = TSTART		3682	59 TIME = TSTART	=
= 3781	END	99 equal lines	3782	END	=

T8

Unit 0: CVSA(5235,60,45)

Unit 1: SUSP:CIGS(5257,6304)

```

= 5235      SUBROUTINE FINPUT
=====
= 5265      *
=          NFWNT(5)
=
= 5266      COMMON/TEMPVS/JTITLE(5,301),NF(5),MS(3),KTITLE
=          (31)
=
= 5344      41 FORMAT('O',I7,'-',I3,I11,'-',I3,I8,4I21)
5345      IF (NJ.NE.J) WRITE (6,42)
=====
=          SUBROUTINE FINPUT
=====
=          *
=          NFWNT(5)
=          COMMON /PLOTRES/ ELYPR(3,100), PLPTS(3,3,100),
=          NELSEG(100), LDNPCS
=          1 . IELPS, IELPB, IELP, NNELP, NPLSEG(100)
=          REAL*4 PLPTS
=          COMMON/TEMPVS/JTITLE(5,301),NF(5),MS(3),KTITLE
=          (31)
=          41 FORMAT('O',I7,'-',I3,I11,'-',I3,I8,4I21)
=          IF (NJ.NE.J) GO TO 426
=          IF (NJ .GT. 100) GO TO 426
=          IF (I .NE. 1) GO TO 422
=          NN = IABS(MS(1))
=          IF (NN .GT. 100) GO TO 426
=          IF (NJ .GT. NPL) GO TO 426
=          IF (NPLSEG(NJ) .EQ. O) NPLSEG(NJ) = NN
=          IF (NPLSEG(NJ) .NE. NN) GO TO 426
=          422 IF (I .GT. 3) GO TO 429
=          IF (I .NE. 3) GO TO 424
=          NN = IABS(MS(1))
=          IF (NN .GT. 100) GO TO 426
=          IF (NN .GT. NSEG .AND. NN .LT. NGRND) GO TO 42
=          6
=          IF (ELSEG(NN) .EQ. O) NELSEG(NN) = NJ
=          IF (ELSEG(NN) .NE. NJ) GO TO 426
=          424 MM = IABS(MS(3))
=          IF (MM .GT. 100) GO TO 426
=          M = IABS(MS(2))
=          IF (MM .GT. NSEG .AND. MM .LT. NGRND) GO TO 42
=          6
=          IF (ELSEG(MM) .EQ. O) NELSEG(MM) = M
=          IF (ELSEG(MM) .EQ. M) GO TO 429
=          426 WRITE (6,42)
=          42 FORMAT(' CONTACT INPUT ERROR. PROGRAM TERMINAT
=          ED.')
=          STOP 14
=          5347 IF (NJ.NE.J) STOP 14
=          5348 NLT = 1
=          5349 DO 43 JJ = 1,31
=====
=          908 equal lines
=          6304 END
=====

```

Table C.5. Comparison of GUCVS with GMCVS (Page 8 of 41)

Line	Code	Subroutine	Heding	Lines	LPP	Line	Code	Subroutine	Heding	Lines	LPP
6420	C	REV 20 05/18/80	IMPLICIT REAL*8 (A-H,O-Z)			835	C	SUBROUTINE HEDING	(KTG, LIN, LPAG)		
6421	=					836		REV 20 05/18/80			
6422						837		COMMON/HOLDIT/	BAGTTL(5.6), BDYTTL(5), BLTTTL		
6423						838		(5.8), COMMENT(40),			
6424						839		1DATE(3), DT, JOINT(100), INCSML, INCBIG, PLTTL			
6425						840		(5.100),			
6426						841		2SEG(100), VPSTTL(20), LLFRST, KASTOP, NRNTIM,			
6427						842		3TIMLAS, MULTPL, NPL, NPLT, NRNVAR, LFENKT,			
6428						843		4NBAG, NBLT, LBBAG, LBBELT, LBJNT, LBPL,			
6429						844		5LBSEG, KKNTRL(241), NSD, NSEG, ISPSWT,			
6430						845		6NSTEPS, NVEH, NGRND, NHRNSS, NJNT			
6431						846		COMMON/PRESET/	ISYMB(49), KASLIN(3,16), LDNR		
6432						847		Y(3), LPP, NW60			
6433						848		1, MAXKAP			
6434						849		COMMON/FETCH/	D(3,3,12), DPMI(3,3,100), G, L		
6435						850		PMI(100), PI,			
6436						851		1SEGLA(3,12), SEGLP(3,12), WMEG(3,			
6437						852		12),			
6438						853		2WMEGD(3,12), UNITL, UNITT, RADIAN, TIMM			
6439						854		AX,			
6440						855		3IKASE(12), NKASE, KASKOL, KASPAG, KASFUL			
6441						856		COMMON/HLDCON/	NRNBAS(246), LFIRST(241), KASN		
6442						857		UM, KATKOL(12),			
6443						858		1KPRLM(3), KATKAS(3,12), KASKTL(5.241), MAXPTS			
6444						859		2NRN, LSTEP, LASREC(3)			
6445						860		COMMON/IOCNTL/	LDNRWK, KWDPLN, IOTALK		
6446						861		COMMON/FETCHU/	PQUANT(16), KONTLP(6,3), JDTP		
6447						862		S(18), IPIN(3),			
6448						863		1KKAS, MSECPT, MTIMPT			
6449						864		COMMON/ZTTHNG/	TIME(6000), ZTTH(6000,11), LIN		
6450						865		EQT(6000)			
								DIMENSION CONTLP(6,3), HHEAD(6), HEAD(2,3)			
								EQUIVALENCE (CONTLP(1.1),KONTLP(1.1)), (HHEAD(
								1), HEAD(1,1))			
								-DIMENSION PHED(5),HEDJ(8,2),HEADJJ(8,2) . WRTO			
								PT(2,2), WRT(2,3)			
								DATA HEDJ/'IPIN', 4H FL, 4HEXUR, 4HE A, 4HZI			
								MU, 4HTH			
								14HTORS, 4HION, 4HIEUL, 4HER, 'PREC', 4H. N,			
								24HUTAT, 4HION, 4H SP, 4HIN /			
								DATA BLANK/' /', PAGEB/O./			
								DATA PHED/'SPRF', 'PNL1', 'PNL2', 'PNL3', 'PNL4' /			
								DATA WRTOPT/4H"W.R, 4H.T.", 4H(W.R, 4H.T.) /			


```

6451 DATA BLANK/4H /
6452 DATA PHED/4HSPRF, 4HPNL1, 4HPNL2, 4HPNL3, 4HPNL4/
6453 NPRT4 = NPRT(4) + 4
6454 IF (NPRT4.LE.O .OR. NPRT4.GT.8) STOP 40
6455 GO TO (11,11,82,12,12,11,11,12) , NPRT4
6456 11 LOLD = .FALSE.
6457 LNEW = .TRUE.
6458 GO TO 13
6459 12 LOLD = .TRUE.
6460 LNEW = .FALSE.
6461 13 MT = 20
6462 NLINES = MOD(LINES-1,LPP)+1
6463 XPAGE = 0.01*FLOAT((LINES + LPP-1)/LPP)
6464
6465 C NOTE: MT WILL BE THE PAGE OR OUTPUT UNIT COUNT
6466 ER
6467 C NT WILL BE THE ACTUAL OUTPUT UNIT NUMBER
6468 C IT WILL BE THE INDEX TO THE DATA ARRAY
6469 C NLINES WILL BE THE NUMBER OF LINES TO BE
6470 C PRINTED
6471 C EVERY LPP LINES PRINT HEADINGS FOR 7 TYPES OF
6472 C OUTPUT ABOVE.
6473 DO 20 K=1,7
6474 IF (NSG(K).LE.O) GO TO 20
6475 KSG = NSG(K)
6476 J3 = 2
6477 IF (K.EQ.7) J3 = 2
6478 DO 19 J1=1,KSG,J3
6479 MT = MT + 1
6480 NT = MT
6481 IF (LNEW) NT = 6
6482 IT = MT - 20
6483 PAGE = FLOAT(MT) + XPAGE
6484 WRITE (NT,21) DATE,PAGE,COMENT,VPSTTL,BDYTTL
6485 IF (K.EQ.1) WRITE (NT,22)
6486 IF (K.EQ.2) WRITE (NT,23) UNITL,UNITT
6487 IF (K.EQ.3) WRITE (NT,24) UNITL
6488 IF (K.EQ.4) WRITE (NT,25) UNITT
6489 IF (K.EQ.5) WRITE (NT,26) UNITT
6490 IF (K.EQ.6) WRITE (NT,27)
6491 IF (K.EQ.7) WRITE (NT,28)
6492 J2 = MINO(J1+J3-1,KSG)
6493 DO 14 J=J1,J2
6494 KK = MSG(J,K)
6495 HEAD(J) = SEG(KK)
6496 IF (K.LT.7) GO TO 14
6497 KK = IABS(KK)
6498 HEAD(J) = JOINT(KK)
6499 JJ2 = J-J1+1
6500 K2 = 1
6501
6502 C CURRENT CATEGORY NUMBER
6503 KAT = KTG
6504 IF (KAT.LE.O) GO TO 550
6505 IF (KAT.GT.14) GO TO 550
6506 INITIILIZE TIME POINT ON PAGE LINE COUNT
6507 LPAG = 0
6508 C FIRST TIME POINT FOR NEW PAGE
6509 LINES = LIN
6510 NPAG = MAXO((LINES + LPP - 2) / (LPP - 1), 1)
6511 IF (LINES.EQ.1) PAGEB = PAGEB + 1
6512 PAGE = PAGEB + FLOAT(NPAG) / 100.
6513 NT = 6
6514 IF (KAT.GT.7) GO TO 210
6515 K = KAT
6516 WRITE (NT,10) DATE,PAGE,COMENT,VPSTTL,BDYTTL
6517
6518 10 FORMAT('1',18X,'DATE:',3X,3A4,68X,'PAGE:',F6.2
6519 18X,'RUN DESCRIPTION:',3X,20A4/27X,20A4/
6520 23X,'VEHICLE DECELERATION:',3X,20A4/
6521 311X,'CRASH VICTIM:',3X,5A4 )
6522 IF (K.EQ.1) WRITE (NT,20)
6523 20 FORMAT('O', 27X,
6524 1'SEGMENT LINEAR ACCELERATIONS (G'S)')
6525 IF (K.EQ.2) WRITE (NT,30) UNITL,UNITT
6526 30 FORMAT('O', 27X,
6527 1'SEGMENT LINEAR VELOCITIES ('.A4,/'A4,')')
6528 IF (K.EQ.3) WRITE (NT,40) UNITL
6529 40 FORMAT('O', 27X,
6530 1'SEGMENT LINEAR DISPLACEMENTS ('.A4,')')
6531 IF (K.EQ.4) WRITE (NT,50) UNITT
6532 50 FORMAT('O'/'O', 27X,
6533 1'SEGMENT ANGULAR ACCELERATIONS (REV/'A4,')**2)
6534 )
6535 IF (K.EQ.5) WRITE (NT,60) UNITT
6536 60 FORMAT('O'/'O', 27X,
6537 1'SEGMENT ANGULAR VELOCITIES (REV/'A4,')')
6538 IF (K.EQ.6) WRITE (NT,70)
6539 70 FORMAT('O'/'O', 27X,
6540 1'SEGMENT ANGULAR DISPLACEMENTS (DEG)')
6541 IF (K.EQ.7) WRITE (NT,80)
6542 80 FORMAT('O', 27X,'JOINT PARAMETERS')
6543 DO 110 L = 1, KKAS
6544 KK = IABS(KONTLP(4, L))
6545 HEAD(1,L) = SEG(KK)
6546 JJ = KONTLP(5, L)
6547 HEAD(2,L) = SEG(JJ)
6548 IF (K.GT.3) GO TO 90
6549 LL = 1
6550 IF (KONTLP(4,L).LT.O) LL = 2
6551 WRT(1,L) = WRTOPT(1,LL)
6552 WRT(2,L) = WRTOPT(2,LL)
6553 GO TO 110
6554 90 IF (K.LT.7) GO TO 110
6555 KK = IABS(KK)
6556 HEAD(1,L) = JOINT(KK)
6557
6558 K2 = 1

```

```

6501 IF (MSG(J,K).LT.O) K2 = 2
6502 DO 35 K1=1,4
6503 35 HEADJJ(K1,JJ2) = HEDJ(K1,K2)
6504 14 CONTINUE
6505 IF (K.LE.3) WRITE (NT,29) (BLANK,(XSG(I,J,K),I
=1,3),J=J1,J2)
6506 IF (K.LE.6) WRITE (NT,30) (BLANK,MSG(J,K),HEAD
(J),J=J1,J2)
6507 IF (K.LE.5) WRITE (NT,31) (BLANK,J=J1,J2)
6508 IF (K.EQ.6) WRITE (NT,32) (BLANK,J=J1,J2)
6509 IF (K.LT.7) GO TO 15
6510 WRITE (NT,33) (BLANK,MSG(J,K),HEAD(J),J=J1,J2)
6511 WRITE (NT,36) (BLANK,UNITL,UNITM,J=J1,J2)
6512 WRITE (NT,37) (BLANK,(HEADJJ(K1,J),K1=1,4),J=1
,JJ2)
6513 15 WRITE (NT,38)
6514 IF (.NOT.LNEW) GO TO 19
6515 IF (K.EQ.7) GO TO 17
6516 JJ = 4*(J2-J1+1)
6517 DO 16 I=1,NLINES
6518 16 WRITE (NT,39) USEC(I),(ZTTH(J,I,IT),J=1,JJ)
6519 GO TO 19
6520 17 JJ = 7*(J2-J1+1)
6521 DO 18 I=1,NLINES
6522 18 WRITE (NT,40) USEC(I),(ZTTH(J,I,IT),J=1,JJ)
6523 19 CONTINUE
6524 20 CONTINUE
6525 21 FORMAT('1',18X,'DATE:',3X,3A4,68X,'PAGE:',F6.2
/
* 8X,'RUN DESCRIPTION:',3X,20A4/27X,20A4/
* 3X,'VEHICLE DECELERATION:',3X,20A4/
* 11X,'CRASH VICTIM:',3X,5A4)
6526 22 FORMAT(' '//27X,
* 'SEGMENT LINEAR ACCELERATIONS (G'S) IN LOCAL
REFERENCE'//)
6527 23 FORMAT(' '//27X,
* 'SEGMENT LINEAR VELOCITIES (' ,A4,'/',A4,' ') IN
VEHICLE REFERENCE'//)
6528 24 FORMAT(' '//27X,
* 'SEGMENT LINEAR DISPLACEMENTS (' ,A4,' ') IN VEHI
CLE REFERENCE'//)
6529 25 FORMAT(' '//27X,
* 'SEGMENT ANGULAR ACCELERATIONS (REV//',A4,'**2)
IN LOCAL REFERENCE'
*//)
6530 26 FORMAT(' '//27X,
* 'SEGMENT ANGULAR VELOCITIES (REV//',A4,' ') IN VE
HICLE REFERENCE'//)
6531 27 FORMAT(' '//27X,

```

```

920 IF (IABS(IPIN(L)) .EQ. 4) K2 = 2
921 DO 100 K1=1,8
922 100 HEADJJ(K1,L) = HEDJ(K1,K2)
923 110 CONTINUE
924 IF (K.LE.3) WRITE (NT,120) (BLANK,(CONTRP(I,J)
,I=1,3)
1,J=1,KKAS)
925 120 FORMAT(9X,3(A4,3X,'POINT (' ,F6.2,' ,',F6.2,' ,',
F6.2,' ) ON ' ) )
926 IF (K.LE.6) WRITE (NT,130) (BLANK, KONTLP(4,J)
, HEAD(1,J)
1 (WRT(K,J),K= 1, 2), KONTLP(5,J), HEAD(2,J),
J =1, KKAS)
927 130 FORMAT('O TIME ',3(A2,'SEGMENT NO.',I3,'(' ,
A4,' ,', 2A4,
1 I3, '( , A4, ' ) ' ) )
928 IF (K.LE.5) WRITE (NT,140) (BLANK,J=1,KKAS)
929 140 FORMAT('O (MSEC)',3(A4,5X,'X',8X,'Y',8X,'Z',
7X,'RES',1X) )
930 IF (K.EQ.6) WRITE (NT,150) (BLANK,J=1,KKAS)
931 150 FORMAT('O (MSEC)',3(A4,4X,'YAW',5X,'PITCH',5
X,'ROLL',5X,'RES '))
932 IF (K.LT.7) GO TO 190
933 WRITE (NT,160) (BLANK,KONTLP(4,J),HEAD(1,J),J=
1,KKAS)
934 160 FORMAT(9X,2(A1,21X,'JOINT NO.',I3,' - ',A4,20X
) )
935 WRITE (NT,170) (BLANK,UNITL,UNITM,J=1,KKAS)
936 170 FORMAT('O TIME ',2(A1,'STATE',5X,'JOINT ANG
LES (DEG)',8X,
1'TOTAL TORQUE (' ,2A4,' ') )
937 WRITE (NT,180) (BLANK,(HEADJJ(K1,J),K1=1,8),J=
1,L)
938 180 FORMAT('O (MSEC)',2(A1,8A4,4X,'SPRING VISCO
US RES. ' ) )
939 190 WRITE (NT,200)
940 200 FORMAT(1X)
941 GO TO 550

```

```

6541 * 'SEGMENT ANGULAR DISPLACEMENTS (DEG) IN VEHIC
LE REFERENCE'//)
6542 28 FORMAT(' ',/27X,'JOINT PARAMETERS'//)
6543 29 FORMAT(9X,3(A4,3X,'POINT (' ,F6.2,' ,F6.2,' ,',
F6.2,' ) ON ' ) )
6544 30 FORMAT(' ', TIME ',3(A4,9X,'SEGMENT NO.',I3,'
',A4,5X) )
6545 31 FORMAT(' ', (MSEC)',3(A4,5X,'X',8X,'Y',8X,'Z',7
X,'RES',.1X) )
6546 32 FORMAT(' ', (MSEC)',3(A4,4X,'YAW',5X,'PITCH',5X
,'ROLL',5X,'RES ' ) )
6547 33 FORMAT(9X,2(A1,21X,'JOINT NO.',I3,' - ',A4,20X
) )
6548 36 FORMAT(' ', TIME ',2(A1,'STATE',5X,'JOINT ANGL
ES (DEG)',8X,
*
6549 'TOTAL TORQUE (' ,2A4.' ) )
6550 37 FORMAT(' ', (MSEC)',2(A1,4A8,4X,'SPRING VISCOU
S RES. ' ) )
6551 38 FORMAT(1X)
6552 39 FORMAT(F9.3,3(3X,4F9.3) )
6553 40 FORMAT(F9.3,2(F5.0,3F9.3,2X,3F9.3))
6554
===== 1 equal 1 line
C
=====
6556 C
6557 C
6558 C
6559 C
6560 C
6561 C
6562 C
6563 C
6564 C
6565 C
6566 C
6567 C
6568 C
6569 C
6570 C
6571 C
6572 C
6573 C
6574 C
6575 C
6576 C
6577 C
6578 C
6579 C
6580 C
6581 C
6582 C
6583 C
6584 C
=====
MPSF = O
IF (NPL.EQ.O) GO TO 52
DO 42 J=1,NPL
IF (MNPL(J).EQ.O) GO TO 42
KPL = MNPL(J)
DO 41 I=1,KPL
MPSF = MPSF+1
NOPL(MPSF) = J
41 MOPL(MPSF) = MPL(2,I,J)
42 CONTINUE
IF (MPSF.EQ.O) GO TO 52
DO 44 J1=1,MPSF,2
J2 = MINO(J1+1,MPSF)
MT = MT + 1
NT = MT
IF (LNEW) NT = 6
IT = MT - 20
PAGE = FLOAT(MT) + XPAGE
WRITE (NT,21) DATE,PAGE,COMENT,VPSTTL,BDYTTL
WRITE (NT,45)
N1 = NOPL(J1)
N2 = NOPL(J2)
M1 = MOPL(J1)
M2 = MOPL(J2)
IF (J1.EQ.J2) WRITE (NT,46)
*
EG(M1) BLANK,N1,( PLTTL(I,N1),I=1,5),M1,S
IF (J1.NE.J2) WRITE (NT,46)
*
EG(M1) BLANK,N1,( PLTTL(I,N1),I=1,5),M1,S
=====
946 C
947 C
948 C
949 C
950 C
951 C
952 C
953 C
954 C
955 C
956 C
957 C
958 C
959 C
960 C
961 C
962 C
963 C
964 C
965 C
966 C
967 C
968 C
969 C
970 C
971 C
972 C
973 C
974 C
975 C
976 C
=====
210 NGO = KAT - 7
IF (NGO .LT. 1 .OR. NGO .GT. 7) GO TO 550
GO TO (220, 430, 280, 340, 380, 450, 470), NGO
220 N1 = KONTLP(2,1)
N2 = KONTLP(2,2)
M1 = KONTLP(3,1)
M2 = KONTLP(3,2)
M1A = KONTLP(4,1)
M2A = KONTLP(4,2)
WRITE (NT,10) DATE,PAGE,COMENT,VPSTTL,BDYTTL
WRITE (NT,230)
230 FORMAT(27X,'CONTACT FORCES - VEHICLE PANELS VS
ELLIPSOIDS')
IF (KKAS .EQ. 1) WRITE (NT,240)
1BLANK,N1,( PLTTL(I,N1),I=1,5),M1A,SEG(M1)
240 FORMAT('O',8X,2(A4,' PANEL',I3,' (' ,5A4,' ) V
S. ELLIPSOID',I3,
1' (' ,A4,' ) ) )
IF (KKAS .EQ. 2) WRITE (NT,240)
1BLANK,N1,( PLTTL(I,N1),I=1,5),M1A,SEG(M1)
2BLANK,N2,( PLTTL(I,N2),I=1,5),M2A,SEG(M2)
WRITE (NT,250) (BLANK,UNITL,J=1,KKAS)
250 FORMAT(' ',8X,A4,'DEFL- NORMAL FRICTION RESU
LTANT CONTACT LOCAT
1ION (' ,A4,' ),A2,'DEFL- NORMAL FRICTION RESU
LTANT CONTACT LOCAT
2ION (' ,A4,' ) )
WRITE (NT,260) (BLANK,J=1,KKAS)
260 FORMAT(' ', TIME ',2(A4,'ECTION FORCE FORC
E FORCE (VEHI
1CLE REFERENCE' ) )
WRITE (NT,270) (BLANK,UNITL,UNITM,UNITN,UNITO,
J=1,KKAS)
270 FORMAT(' ', (MSEC)',2(A3,' (' ,A4,' )',2X,' (' ,A4,'
) ',4X,' (' ,A4,' )',3X,

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Table C.5. Comparison of GUCVS with GMCVS (Page 12 of 41)

6585	* EG(M2)	BLANK,N2,(PLTTL(I,N2),I=1,5),M2,S	977	1(' ,A4,') X Y Z '))
6586		WRITE (NT,47) (BLANK,UNITL,J=J1,J2)	978	WRITE (NT,200)
6587		WRITE (NT,48) (BLANK,J=J1,J2)	979	GO TO 550
6588		WRITE (NT,49) (BLANK,UNITL,UNITM,UNITM,J =J1,J2)		
6589		WRITE (NT,38)		
6590		IF (.NOT.LNEW) GO TO 44		
6591		JJ = 7*(J2-J1+1)		
6592		DO 43 I=1,NLINES		
6593		43 WRITE (NT,50) USEC(I),(ZTTH(J,I,IT),J=1,JJ)		
6594		44 CONTINUE		
6595		45 FORMAT(27X,'CONTACT FORCES - VEHICLE PANELS VS . SEGMENTS')		
6596		46 FORMAT(' /8X,2(A4,' PANEL',I3,' (' ,5A4,') VS . SEGMENT',I3, * (' ,A4,') '))		
6597				
6598		47 FORMAT(' ',8X,A4,'DEFL- NORMAL FRICTION RESU LTANT CONTACT LOCAT		
6599		*ION (' ,A4,')',A2,'DEFL- NORMAL FRICTION RESU LTANT CONTACT LOCAT		
6600		*ION (' ,A4,')')		
6601	E	48 FORMAT(' TIME',2(A4,'ECTION FORCE FORC FORCE (VEHI *CLE REFERENCE') '))		
6602				
6603		49 FORMAT(' (MSEC)',2(A3,' (' ,A4,')',2X,' (' ,A4,)',4X,' (' ,A4,')',3X, * (' ,A4,') X Y Z '))		
6604				
6605		50 FORMAT(F9.3,2(F9.3,3F9.2,3F8.3))		
6606		51 FORMAT(3X,'(MSEC)',4(A1,9X,'X',8X,'Y',8X,'Z',1 X))		
= 6607	C	=====	980	C
= 6609	C	===== 1 equal line =====	982	C
6610		52 MBSF = 0	983	280 N1 = KONTLP(2,1)
6611		IF (NBLT.EQ.0) GO TO 83	984	N2 = KONTLP(2,2)
6612		DO J=1,NBLT	985	M1 = KONTLP(3,1)
6613		IF (IT(J).EQ.0) GO TO 54	986	M2 = KONTLP(3,2)
6614		MBSF = MBSF+1	987	WRITE (NT,10) DATE,PAGE,COMENT,VPSTTL,BDYTTL
6615		NOPL(MBSF) = J	988	WRITE (NT,290)
6616		MOPL(MBSF) = MBLT(2,1,J)	989	290 FORMAT('O',26X,'CONTACT FORCES - BELTS VS. SEG MENTS')
6617		54 CONTINUE	990	IF (KKAS.EQ.1) WRITE (NT,300)
6618		IF (MBSF.EQ.0) GO TO 83	991	1BLANK,N1,(BLTTTL(I,N1),I=1,5),M1,SEG(M1)
6619		DO 56 J1=1,MBSF,2	992	300 FORMAT(' ',7X,2(A4,' BELT',I3,' (' ,5A4,') VS . SEGMENT',I3, 1' (' ,A4,') '))
6620		J2 = MINO(J1+1,MBSF)	993	
6621		MT = MT + 1	994	IF (KKAS.EQ.2) WRITE (NT,300)
6622		NT = MT	995	1BLANK,N1,(BLTTTL(I,N1),I=1,5),M1,SEG(M1),
6623		IF (LNEW) NT = 6	996	2BLANK,N2,(BLTTTL(I,N2),I=1,5),M2,SEG(M2)
6624		IT = MT - 20	997	WRITE (NT,310) (BLANK,J=1,KKAS)
6625		PAGE = FLOAT(MT) + XPAGE	998	310 FORMAT(' ',2X,2(A4,11X,'ANCHOR POINT A',14X, 'ANCHOR POINT B'))
6626		WRITE (NT,21) DATE,PAGE,COMENT,VPSTTL,BDYTTL	999	WRITE (NT,320) (BLANK,J=1,KKAS)
6627		WRITE (NT,57)	1000	320 FORMAT(4X,'TIME',2(A4,5X,'STRAIN',7X,'FORCE',1 2X, 1'STRAIN',7X,'FORCE',3X))
6628		N1 = NOPL(J1)	1001	WRITE (NT,330) (BLANK,UNITL,UNITL,UNITM,UNITL, UNITL,UNITM,J=1, 1KKAS)
6629		N2 = NOPL(J2)	1002	
6630		M1 = MOPL(J1)	1003	

Table C.5. Comparison of GUCVS with GMCVS (Page 13 of 41)

```

6631 M2 = MOPL(J2)
6632 IF (J1.EQ.J2) WRITE (NT,58)
6633 * BLANK,N1,(BLTTTL(I,N1),I=1,5),M1,S
EG(M1)
6634 IF (J1.NE.J2) WRITE (NT,58)
6635 * BLANK,N1,(BLTTTL(I,N1),I=1,5),M1,S
EG(M1),
6636 * BLANK,N2,(BLTTTL(I,N2),I=1,5),M2,S
EG(M2)
6637 WRITE (NT,59) (BLANK,J=J1,J2)
6638 WRITE (NT,60) (BLANK,J=J1,J2)
6639 WRITE (NT,61) (BLANK,UNITL,UNITM,UNITL,U
NITL,UNITM,J=J1,J2)
6640 WRITE (NT,38)
6641 IF (.NOT.LNEW) GO TO 56
6642 JJ = 4*(J2-J1+1)
6643 DO 55 I=1,NLINES
6644 55 WRITE (NT,62) USEC(I),(ZTTH(J,I,IT),J=1,JJ)
6645 56 CONTINUE
6646 57 FORMAT('O',26X,'CONTACT FORCES - BELTS VS. SEG
MENTS')
6647 58 FORMAT(' ',7X,2(A4,' BELT',I3,' ('',5A4,'') VS
SEGMENT',I3,
* ('',A4,'')')
6648 59 FORMAT(' ',2X,2(A4,11X,'ANCHOR POINT A',14X,
'ANCHOR POINT B')
6649 60 FORMAT(4X,'TIME',2(A4,5X,'STRAIN',7X,'FORCE',1
2X,
* 'STRAIN',7X,'FORCE',3X)
)
6650 61 FORMAT(3X,'(MSEC)',2(A4,2X,'(',A4,'/',A4,''),4
X,'(',A4,''),9X,
* ('',A4,'/',A4,''),4X,
('',A4,''),3X)
6651 62 FORMAT(F9.3,4(F15.6,F12.2,3X) )
=====
C
=====
6657 C
6658 83 IF (NHRNSS.LE.O) GO TO 91
6659 MBSF = O
6660 J1 = 1
K1 = 1
D0 85 I=1,NHRNSS
IF (NBLTPH(I).LE.O) GO TO 85
J2 = J1 + NBLTPH(I) - 1
D0 84 J=J1,J2
MBSF = MBSF + 1
IF (NPTSPB(J).LE.O) GO TO 84
K2 = K1 + NPTSPB(J) - 1
NOPL(2*MBSF-1) = J
NOPL(2*MBSF) = I
MOPL(2*MBSF-1) = K1
MOPL(2*MBSF) = K2
=====
C
=====
1008 C
1009 340 WRITE (NT,10) DATE,PAGE,COMENT,VPSTTL,BDYTTL,
WRITE (NT,350)
1010 350 FORMAT('O',26X,'HARNES SYSTEM BELT ENDPOINT F
ORCES')
1011 WRITE (NT,360) (BLANK,(KONTLP(I,J),I=1,2),J=1,
KKAS)
1012 360 FORMAT(9X,2(A4,11X,'BELT NO.',I4,' OF HARNES
NO.',I3,15X))
1013 WRITE (NT,370) (BLANK,(KONTLP(I,J),I=3,4),J=1,
KKAS)
1014 370 FORMAT(9X,2(A4,6X,'POINT NO.',I5,16X,'POINT NO
',I5,6X))
1015 WRITE (NT,320) (BLANK,J=1,KKAS)
1016 WRITE (NT,330) (BLANK,UNITL,UNITM,UNITL,UNITM,UNITL,
UNITL,UNITM,J=1,
1KKAS)
1017 WRITE (NT,200)
1018 GO TO 550
1019
1020
1021
1022

```

Table C.5. Comparison of GUCVCS with GMCVCS (Page 14 of 41)

```

6673 K1 = K2 + 1
6674 84 CONTINUE
6675 J1 = J2 + 1
6676 85 CONTINUE
6677 DO 87 J1=1,MBSF,2
6678 J2 = MINO(J1+1,MBSF)
6679 MT = MT + 1
6680 NT = MT
6681 IF (LNEW) NT = 6
6682 IT = MT - 20
6683 PAGE = FLOAT(MT) + XPAGE
6684 WRITE (NT,21) DATE,PAGE,COMENT,VPSTTL,BDYTTL
6685 WRITE (NT,88)
6686 WRITE (NT,89) (BLANK,NOPL(2*J-1),NOPL(2*J),J=J
1,J2)
6687 WRITE (NT,90) (BLANK,MOPL(2*J-1),MOPL(2*J),J=J
1,J2)
6688 WRITE (NT,60) (BLANK,J=J1,J2)
6689 WRITE (NT,61) (BLANK,UNITL,UNITL,UNITM,UNITL,U
NITL,UNITM,J=J1,J2)
6690 WRITE (NT,38)
6691 IF (.NOT.LNEW) GO TO 87
6692 JJ = 4*(J2-J1+1)
6693 DO 86 I=1,NLINES
6694 86 WRITE (NT,62) USEC(I),(ZTTH(J,I,IT),J=1,JJ)
6695 87 CONTINUE
6696 88 FORMAT('O',26X,'HARNES SYSTEM BELT ENDPOINT F
ORCES')
6697 89 FORMAT(9X,2(A4,11X,'BELT NO.',I4,' OF HARNES
NO.',I3,15X))
6698 90 FORMAT(9X,2(A4,6X,'POINT NO.',I5,16X,'POINT NO
',I5,6X))
6699 C
6700 C
6701 IF (NSD.LE.O) GO TO 63
6702 DO 94 J1=1,NSD,4
6703 J2 = MINO(J1+3,NSD)
6704 MT = MT + 1
6705 NT = MT
6706 IF (LNEW) NT = 6
6707 IT = MT - 20
6708 PAGE = FLOAT(MT) + XPAGE
6709 WRITE (NT,21) DATE,PAGE,COMENT,VPSTTL,BDYTTL
6710 WRITE (NT,95) (BLANK,J=J1,J2)
6711 DO 92 J=J1,J2
6712 M1 = MSDM(J)
6713 N1 = MSDM(J)
6714 POSSIBLE OVERFLOW INTO NOPL ARRAY IS INTENTION
AL.
6715 C
6716 HEAD(2*J-1) = SEG(M1)
6717 92 HEAD(2*J) = SEG(N1)
6718 WRITE (NT,96)(BLANK,MSDM(J),HEAD(2*J-1),MSDN(J
),HEAD(2*J),J=J1,J2)
6719 WRITE (NT,97) (BLANK,J=J1,J2)
6720 WRITE (NT,98) (BLANK,UNITL,UNITM,J=J1,J2)
6721 WRITE (NT,38)
6722 IF (.NOT.LNEW) GO TO 94
6723 JJ = 2*(J2-J1+1)

```

```

=====
C
1023 line
1025 C
1026 380 M1 = KONTLP(1,1)
1027 N1 = KONTLP(2,1)
1028 M2 = KONTLP(3,1)
1029 N2 = KONTLP(4,1)
1030 M3 = KONTLP(1,2)
1031 N3 = KONTLP(2,2)
1032 M4 = KONTLP(3,2)
1033 N4 = KONTLP(4,2)
1034 JKAS = 1
1035 IF (M2.NE.O) JKAS = 2
1036 IF (M3.NE.O) JKAS = 3
1037 IF (M4.NE.O) JKAS = 4
1038 WRITE (NT,10) DATE,PAGE,COMENT,VPSTTL,BDYTTL
1039 WRITE (NT,390) (BLANK,J,J=1,JKAS)
1040 C
1041 390 FORMAT('O',26X,'SPRING DAMPER FORCES'/
19X,4(A3,3X,'SPRING DAMPER NO.',I3,4X))
1042 GO TO (400,404,406,408),JKAS
1043 C
1044 400 WRITE(NT,401) BLANK,M1,SEG(M1),N1,SEG(N1)
1045 401 FORMAT(9X,4(A3,'SEG',I3,'(',A4,',') - SEG',I3,'(
',A4,',')')
1046 GO TO 409
1047 404 WRITE(NT,401) BLANK,M1,SEG(M1),N1,SEG(N1),
1BLANK,M2,SEG(M2),N2,SEG(N2)

```

```

6724 DO 93 I=1,NLINES
6725 93 WRITE (NT,99) USEC(I),(ZTTH(J,I,IT),J=1,JJ)
6726 94 CONTINUE
6727 95 FORMAT('O',26X,'SPRING DAMPER FORCES'//
6728 9X,4(A3,3X,'SPRING DAMPER NO.',I3,4X))
6729 96 FORMAT(9X,4(A3,SEG,I3,'(','A4,') - SEG',I3,'(
',A4,')'))
6730 97 FORMAT(4X,'TIME',1X,4(A3,5X,'LENGTH',7X,'FORCE
',4X))
6731 98 FORMAT(3X,'(MSEC)',4(A3,5X,'(','A4,')',6X,'(','A
4,')',4X))
6732 99 FORMAT (F9.3,4(F14.3,F12.2,4X))

= 6733 C
===== 1 equal =====
= 6735 C
6736 63 MSSF = O
6737 DO 65 J=1,NSEG
6738 IF (MNSEG(J).EQ.O) GO TO 65
6739 LSEG = MNSEG(J)
6740 DO 64 I=1,LSEG
6741 MSSF = MSSF+1

6742 NOPL(MSSF) = J
6743 MOPL(MSSF) = MSEG(2,I,J)

6744 65 CONTINUE

6745 IF (MSSF.EQ.O) GO TO 70
6746 DO 67 J=1,MSSF
6747 MT = MT + 1
6748 NT = MT
6749 IF (LNEW) NT = 6
6750 IT = MT - 20
6751 PAGE = FLOAT(MT) + XPAGE
6752 WRITE (NT,21) DATE,PAGE,COMENT,VPSTTL,BDYTTL
6753 N1 = NOPL(J)
6754 M1 = MOPL(J)
6755 WRITE (NT,68) N1,SEG(N1),M1,SEG(M1),UNITL,N1,M

1
6756 ,UNITL,UNITM,UNITM,UNITM
6757 IF (.NOT.LNEW) GO TO 67

6758 DO 66 I=1,NLINES
6759 66 WRITE (NT, 69) USEC(I),(ZTTH(J,I,IT),JJ=1,10
)
6760 67 CONTINUE

```

```

GO TO 409
WRITE (NT,401) BLANK,M1,SEG(M1),N1,SEG(N1),
1BLANK,M2,SEG(M2),N2,SEG(N2),
2BLANK,M3,SEG(M3),N3,SEG(N3)
GO TO 409
WRITE (NT,401) BLANK,M1,SEG(M1),N1,SEG(N1),
1BLANK,M2,SEG(M2),N2,SEG(N2),
2BLANK,M3,SEG(M3),N3,SEG(N3),
3BLANK,M4,SEG(M4),N4,SEG(N4)
409 WRITE (NT,410) (BLANK,J=1,JKAS)
410 FORMAT(4X,'TIME',1X,4(A3,5X,'LENGTH',7X,'FORCE
',4X))
WRITE (NT,420) (BLANK,UNITL,UNITM,J=1,JKAS)
420 FORMAT(3X,'(MSEC)',4(A3,5X,'(','A4,')',6X,'(','A
4,')',4X))
WRITE (NT,200)
GO TO 550

C
=====
C
430 N1A = KONTLP(2,1)
N1 = KONTLP(1,1)
M1A = KONTLP(4,1)
M1 = KONTLP(3,1)
WRITE (NT,10) DATE,PAGE,COMENT,VPSTTL,BDYTTL
WRITE (NT,440) N1A,SEG(N1),M1A,SEG(M1),UNITL,N
1,M1
1,UNITL,UNITM,UNITM,UNITM
440 FORMAT('O',26X,'CONTACT FORCES - ELLIPSOID NO.
',I3,'(','A4,
1') VS. ELLIPSOID NO.',I3,'(','A4,')'//
13X,'DEFL- NORMAL
2 FRICTION RESULTANT',
14X,'CONTACT LOCATI
3ON ('',A4,')//
4X,'TIME ECTION',
4,3(3X,'FORCE',1X),
2(' SEG',I3,' LOC
5AL REFERENCE ')/
3X,'(MSEC)',3X,'(
6A4,')',3(3X,'(','A4,')'),
2(5X,'X',7X,'Y',7X,
7'Z',4X)/1X)
GO TO 550

C
C AIRBAG QUANTITIES HEADINGS
C
450 WRITE (NT,10) DATE,PAGE,COMENT,VPSTTL,BDYTTL
WRITE (NT,460) J,(BAGTTL(I,J),I=1,5)
460 FORMAT('O',26X,'PARAMETERS FOR AIRBAG NO.',I2,
4X,5A4//
116X,'SUPPLY CYLINDER STATIC'/
24X,'TIME',8X,'PRES.',4X,'TEMP.',4X,'PRES.',12X
,'AIRBAG',3X,
3'CENTER',14X,'AIRBAG SEMIAXES',12X,'ORIENTATI
ON (DEG.)'/
3X,

```

```

6761 68 FORMAT('O',26X,'CONTACT FORCES - SEGMENT NO.',1091
13,'(',A4,')',26X,'CONTACT FORCES - SEGMENT NO.',13,
*      ' '), VS. SEGMENT NO.',13,
*      '(',A4,')')//
*      13X,'DEFL- NORMAL FRICTION RESULTANT',1093
*      14X,'CONTACT LOCATION(',A4,')//
*      4X,'TIME ECTION',3(3X,'FORCE',1X),
*      2(' SEG.',13,' LOCAL REFERENCE ')/
*      3X,'(MSEC)',3X,'(',A4,')',3(3X,'(',A4,')')
),
*      2(5X,'X',7X,'Y',7X,'Z',4X)/1X)
69 FORMAT(2F9.3,3F9.2,3F8.3,2X,3F8.3)
=====
C      1 equal line
=====
6772 C      470 DO 520 K = 1, KKAS
6773          N1 = KONTLP(1,K)
6774          N2 = KONTLP(2,K)
6775          IF (N1.GT. O) GO TO 480
6776          HEAD(1,K) = PHED(-N1)
6777          GO TO 490
6778          480 HEAD(1,K) = SEG(N1)
6779          490 J2 = 3
6780          IF (N2) 500, 520, 510
6781          500 HEAD(2,K) = PHED(-N2)
6782          J2 = 4
6783          GO TO 520
6784          510 HEAD(2,K) = SEG(N2)
6785          )
6786          J2 = 4
6787          520 CONTINUE
6788          J = KONTLP(1, KKAS)
6789          WRITE (NT,10) DATE,PAGE,COMENT,VPSTTL,BDYTTL
6790          WRITE (NT,530)UNITM,J,(BAGTTL(I,J),I=1,5).(BLA
NK,J,(HEAD(I,K),
6791          1I = 1, 2), K = 1, J2)
6792          530 FORMAT('O',26X,'CONTACT FORCES (' ,A4,') ON AIR
BAG NO.',12.4X,5A4//
6793          1/4X,'TIME',4(A1,11X,'AIRBAG',I2,' VS. ',A4,1X)
)
6794          WRITE (NT,540) (BLANK,K=1,J2)
6795          540 FORMAT(3X,'(MSEC)',4(A1,9X,'X',8X,'Y',8X,'Z',1
X))
6796          WRITE (NT,200)
6797          550 RETURN
6798          )
6799          )
6800          )
6801          )
6802          )
6803          )
6804          )
6805          )
6806          )
6807          )
6808          )
6809          )
6810          )
6811          )

```



```

6812      77 CONTINUE
6813      78 FORMAT('O',26X,'PARAMETERS FOR AIRBAG NO.',I2,
4X,5A4//
6814      *      16X,'SUPPLY CYLINDER  STATIC'/
6815      *      4X,'TIME',8X,'PRES.',4X,'TEMP.',4X,'PRES.
',12X,'AIRBAG',
6816      *      3X,'CENTER',14X,'AIRBAG SEMIAXES',12X,'ORIE
NTATION (DEG.)'/
6817      *      3X,'(MSEC)',7X,'(PSIG) (DEG.R) (PSIG)',8X
,'X',8X,'Y',8X,'Z',
6818      *      11X,'A',8X,'B',8X,'C',10X,'YAW',4X,'PITCH',5
X,'ROLL' / )
6819      79 FORMAT (F9.3,3X,3F9.2,2(3X,3F9.3),3X,3F9.2)
6820      80 FORMAT('O',26X,'CONTACT FORCES ('A4,') ON AIR
BAG NO.',I2,4X,5A4//
6821      *      /4X,'TIME',4(A1,11X,'AIRBAG',I2,' VS. ',A4,
1X))
6822      81 FORMAT (F9.3,4(3X,3F9.2))
6823      82 RETURN
6824      END

```

1122

END

Unit 0: CVSB(166,1501)

Unit 1: SUSP:CIGS(6527,7862)

```

=====
166 SUBROUTINE HINPUT
=====
286 * U2(3,100), SEGLP(3,100), SEGLV(3,100), SEGVA(3,
100), NSYM(100)
=====
287 COMMON/RSAVE/XSG(3,20,3), DPMI(3,3,100), LPMI(10
O), NSG(7), MSG(20,7)
=====
288 COMMON/HRNESS/ BAR(15,100), BB(100), BBDOT(100),
PLOSS(2,100),
=====
315 * POINT POINT SEGMENT LENGTH ENER
=====
316 * REFERENCE POINT ('A4,')', 13X, 'BELT FORC
GY LOSS', 5X,
ES ('A4,')',
=====
317 * 9X, 'ENERGY LOSS'/
=====
1144 * /' SEGMENT', 11X, 'LINEAR POSITION ('A4,')'
=====
1145 * 14X, 'LINEAR VELOCITY ('A4,')'/'
1146 * NO. SEG', 2(9X, 'X', 11X, 'Y', 11X, 'Z', 5X)
)
=====
1151 44 FORMAT('O INITIAL ANGULAR ROTATION AND VELOCIT
Y', 71X, 'CARDS G.3'//
1152 * SEGMENT', 11X, 'ANGULAR ROTATION (DEG)'
=====
1153 * 14X, 'ANGULAR VELOCITY (DEG/'A4,')'/'
=====
1501 END
=====

```

1502	C	SUBROUTINE OUTPUT(IJK)	7863		SUBROUTINE OUTPUT(IJK)
1503		REV 20 05/18/80	7864		IMPLICIT REAL*8(A - H, O - Z)
1504	C	CONTROLS TABULATED OUTPUT ON FORTRAN UNITS (ST	7865		COMMON /CONTRL/ TIME, NSEG, NJNT, NPL, NBLT, N
1505	C	ARTING WITH NO. 21)	7866		BAG, NVEH, NGRND,
1506	R	OF SELECTED OPTIONAL SEGMENT LINEAR AND ANGULA	7867		1 NS, NQ, NSD, NFLX, NHRNSS, NWINDF, NJNT
1507	C	R ACCELERATIONS,	7868		F, NPRT(36)
1508	C	VELOCITIES AND DISPLACEMENTS, JOINT PARAMETERS	7869		COMMON /SGMNTS/ D(3.3,100), WMEG(3,100), WMEGD
	C	AND SELECTED DATA	7870		(3,100), U1(3,100),
	C	FROM ALL ALLOWED CONTACT FORCE COMPUTATIONS BE	7871		1 U2(3,100), SEGLP(3,100), SEGLV(3,100),
	C	TWEEN BODY SEGMENTS	7872		2 NSYM(100)
	C	AND VEHICLE COMPONENTS.	7873		COMMON /DESCRP/ PHI(3,100), W(100), RW(100), S
			7874		R(3,200), HA(3,200),
			7875		HB(3,200), RPHI(3,100), HT(3.3,200), SP
			7876		RING(5.300),
			7877		1 VISC(7.300), JNT(100), IPIN(100), ISING
			7878		(100), IGLOB(100),
			7879		2 JOINTF(100)
			7880		3 COMMON /JBARTZ/ MNPL(100), MNBLT(8), MNSEG(100
			7881), MNBAG(6),
			7882		1 MPL(3.5,100), MBLT(3.5,8), MSEG(3.5,100
			7883), MBAG(3.10,6),
			7884		2 NTPL(5,100), NTBLT(5,8), NTSEG(5,100)
			7885		COMMON /TITLES/ DATE(3), COMENT(40), VPSTTL(20
			7886), BDYTTL(5),
			7887		1 BLTTTL(5.8), PLTTL(5.100), BAGTTL(5,6),
			7888		SEG(100),
			7889		2 JOINT(100), CGS(100), JS(100)
			7890		REAL DATE, COMENT, VPSTTL, BDYTTL, BLTTTL, PLT
			7891		TL, BAGTTL, SEG,
			7892		1 JOINT
			7893		LOGICAL*1 CGS, JS
			7894		COMMON /FORCES/ PSF(7,100), BSF(4,20), SSF(10,
			7895		20), BAGSF(3,20),
			7896		1 PRJNT(7,100), NPANEL(5), NPSF, NBSF, NS
			7897		SF, NBGSF
					COMMON /CNSNTS/ PI, RADIANT, G, THIRD, EPS(24),
					UNITL, UNITM,
					1 UNITT, GRAVITY(3)
					COMMON /RSAVE/DPMI(3,3,100), LPMI(100)
					COMMON /COMAIN/ VAR(800), DER(800), DT, HO, HM
					AX, HMIN, RSTIME,
					1 ISTEP, NSTEPS, NDINT, NEQ, IRSIN, IRSOU
					T
					COMMON /DAMPER/ APSDM(3,20), APSDN(3,20), ASD(
					5,20), MSDM(20),
					1 MSDN(20)
					COMMON /IOCNL/ LDNRWK, KWDPLN, IOTALK
					COMMON /HRNESS/ BAR(15,100), BB(100), BBDOT(10
					O), PLOSS(2,100),
					1 XLONG(20), HTIME(2), IBAR(5,100), NL(2,
					100), NPTSPB(20),
					2 NPTPLY(20), NTHRNS(20), NBLTPH(5)
					COMMON /HLDCON/ LDNARY(3), NRBAS(246), LFIRST
					(241), KASNUM,
					1 KATKOL(12), KPRELM(3), KATKAS(3,12), KA
					SKTL(5,241), MAXPTS,

```

7898      2      LINES, KASE, KATG, NRN, LSTEP, LASREC(3
)
7899      COMMON /TEMPVS/ RSTF(27), FDPMI(900)
7900      DIMENSION KSTF(27)
7901      REAL*4 FFIRST(241), FRNBAS(246), FENKAT(51), F
DPMI, FLPMI(100).
7902      1      RSTF, FKASKL(1205)
7903      EQUIVALENCE (KSTF(1),RSTF(1)). (FFIRST(1),LFIR
ST(1)),
7904      1      (FRNBAS(1),NRNBAS(1)). (FENKAT(1),
KATKOL(1)),
7905      2      (FKASKL(1),KASKTL(1,1)), (FLPMI(1)
,LPMI(1))
7906      REAL*4 VS, BLANK, HARN1, HARN2, SPDAM1, SPDAM2
, SPDAM3.
7907      1      SPDAM4, PARM, PNTS
7908      DATA INZ, VS, BLANK, HARN1, HARN2, SPDAM1, SPD
AM2, SPDAM3, SPDAM4.
7909      1      PARM, PNTS /O, ' VS ', ' ', 'HARN', 'E
SS', 'SPRI', 'NG D',
7910      2      'AMPE', 'R', 'PARM', 'PNTS'/
7911      C
7912      IF (INZ .NE. O) GO TO 10
7913      INZ = 1
7914      LINES = O
7915      KOPY = 1
7916      TPRINT = O.DO
7917      10 IF (IJK .NE. O) GO TO 30

C      IMPLICIT REAL*8 (A-H,O-Z)
COMMON/CONTRL/ TIME,NSEG,NJNT,NPL,NBLT,NBAG,NV
EH,NGRND.
*      NS,NQ,NSD,NFLX,NHRNSS,NWINDF,NJNT
F,NPRT(36)
COMMON/SGMNTS/ D(3,3,100),WMEGD(3,100),U1(3,100),
* U2(3,100), SEGLP(3,100),SEGLV(3,100),SEGLA(3,
100),NSYM(100)
COMMON/DESCRP/ PHI(3,100),W(100),RW(100),SR(3,
200),HA(3,200),
*HB(3,200),RPHI(3,100),HT(3,3,200),SPRING(5,300
),VISC(7,300),
* JNT(100),IPIN(100),ISING(100),IGLOB
(100),JOINTF(100)
COMMON/JBARTZ/ MNPL( 100),MNBTL( 8),MNSEG( 100
),MNBAG( 6),
* MPL(3,5,100),MBLT(3,5,8),MSEG(3,5
,100),MBAG(3,10,6),
* NTPL( 5,100),NTBLT( 5,8),NTSEG( 5
,100)
COMMON/TITLES/ DATE(3),COMENT(40),VPSTTL(20),B
DYTTL(5),
* BLTTTL(5,8),PLTTL(5,100),BAGTTL(5
,6),SEGE(100),
* JOINT(100),CGS(100),JS(100)
REAL DATE,COMENT,VPSTTL,BDYTTL,BLTTTL,PLTTL,BA
GTTL,SEG,JOINT
LOGICAL*1 CGS,JS
COMMON/FORCES/ PSF(7,100),BSF(4,20),SSF(10,20)
,BAGSF(3,20),
* PRJNT(7,100),NPANEL(5),NPSF,NBSF,
NSSF,NBGSF
COMMON/CNSNTS/ PI,RADIAN,G,THIRD,EPS(24),
* UNITL,UNITM,UNITT,GRAVITY(3)
COMMON/RSAVE/XSG(3,20,3),DPMI(3,3,100),LPMI(10
0),NSG(7),MSG(20,7)
COMMON/COMAIN/VAR(800),DER(800),DT,HO,HMAX,HMI

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Table C.5. Comparison of GUCVS with GMCVS (Page 21 of 41)

1532	N,RSTIME, *	ISTEP,NSTEPS,NDINT,NEQ,IRSIN,IRSOU			
1533	T	COMMON/DAMPER/ APSDM(3,20),APSDN(3,20),ASD(5,2			
1534		0),MSDM(20),MSDN(20)			
1535		COMMON/HRNESS/ BAR(15,100),BB(100),BBDOT(100),			
1536		PLOSS(2,100),			
1537	*	XLONG(20),HTIME(2),IBAR(5,100),NL			
1538		(2,100),			
1539	*	NPTSPB(20),NPTPLY(20),NTHRNS(20),			
1540		NBLTPH(5)			
1541		COMMON/TEMPVS/TDATA(14,300),ACC(7,20),T1(3),T2			
1542		(3),T3(3),T4(9)			
1543		LOGICAL LTAPE8 , LTHIST			
1544	C	DATA LINES/O/,LPP/45/			
1545		IF (IJK.NE.O) GO TO 13			
1546	C		7918	C	=
1547	C		7919	C	=
1548	C		7920	C	=
1549	C	DO 11 I=1,1740	7921		
1550		11 PSF(I,1) = 0.0	7922		
1551		GO TO 66	7923		
1552			7924	C	
1553			7925	C	
1554			7926	R	
1555			7927	C	
1556			7928		
1557			7929		
1558			7930		
1559			7931		
1560			7932	C	
1561			7933	C	
1562			7934	C	
1563			7935		
1564			7936		
1565			7937		
1566			7938		
1567			7939		
1568			7940		
1569			7941		
1570			7942		
1571			7943		
1572			7944		
1573			7945		
1574			7946		
1575			7947		
1576			7948		
1577			7949		
1578			7950		
1579			7951		
1580			7952		
1581			7953		
1582			7954		
1583			7955		
1584			7956	C	

Table C.5. Comparison of GUCVS with GMCVS (Page 22 of 41)

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1570 C 1ST TIME IN ROUTINE, READ CARD INPUT FOR OUTPU 7957 C LAYOUT RECORDING CATEGORIES AND CASES
1571 T CONTROL. 7958 C
1572 C 1. NO. OF SEGMENT LINEAR ACCELERATIONS, SEGME 7959 C CATEGORY 1---TIME VALUES
1573 C NT NOS. AND LOCATION 7960 KATKOL(1) = 3
1574 C 2. NO. OF SEGMENT LINEAR VELOCITIES , SEGME 7961 KATKAS(1,1) = 1
1575 C NT NOS. AND LOCATION 7962 C CATEGORY 2---SEGMENT LINEAR KINEMATICS
1576 C 3. NO. OF SEGMENT LINEAR DISPLACEMENTS, SEGME 7963 KATKOL(2) = 9
1577 C NT NOS. AND LOCATION 7964 KATKAS(1,2) = NGRND
1578 C 4. NO. OF SEGMENT ANGULAR ACCELERATIONS AND S 7965 C CATEGORY 3---SEGMENT ANGULAR VELOCITIES, ETC.
EGMENT NOS. 7966 KATKOL(3) = 9
7967 KATKAS(1,3) = NGRND
7968 C CATEGORY 4---SEGMENT DIRECTION COSINE MATRICE
S
7969 KATKOL(4) = 9
7970 KATKAS(1,4) = NGRND
7971 CATEGORY 5---JOINT FORCES
7972 KATKOL(5) = 8
7973 KATKAS(1,5) = NUJNT
7974 C CATEGORY 6---PLANE-SEGMENT CONTACT FORCES
7975 KATG = 6
7976 KASE = 0
7977 KASNUM = 0
7978 IF (NPL .LE. 0) GO TO 70
7979 DO 60 I = 1, NPL
7980 KPL = IABS(MNPL(I))
7981 IF (KPL .EQ. 0) GO TO 60
7982 DO 50 J = 1, KPL
7983 KASE = KASE + 1
7984 KASKTL(1,KASE) = KATG + 2
7985 KASKTL(2,KASE) = MPL(1,J,I)
7986 KASKTL(3,KASE) = I
7987 KASKTL(4,KASE) = MPL(2,J,I)
7988 KASKTL(5,KASE) = MPL(3,J,I)
7989 CONTINUE
7990 50 CONTINUE
7991 60 CONTINUE
7992 KATKOL(KATG) = 7
7993 KATKAS(1,KATG) = KASE
7994 GO TO 80
7995 70 KATKOL(KATG) = 0
7996 KATKAS(1,KATG) = 0
7997 KASNUM = KASNUM + KASE
7998 C CATEGORY 7---SEGMENT : SEGMENT CONTACT FORCES
7999 KATG = 7
8000 KASE = 0
8001 IF (NSEG .LE. 0) GO TO 110
8002 DO 100 I = 1, NSEG
8003 KSG = IABS(MNSEG(I))
8004 IF (KSG .EQ. 0) GO TO 100
8005 DO 90 J = 1, KSG
8006 KASE = KASE + 1
8007 KASTRU = KASNUM + KASE
8008 KASKTL(1,KASTRU) = KATG + 2
KASKTL(2,KASTRU) = MSEG(1,J,I)

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8009          KASKTL(3,KASTRU) = I
8010          KASKTL(4,KASTRU) = MSEG(2,J,I)
8011          KASKTL(5,KASTRU) = MSEG(3,J,I)
8012          90  CONTINUE
8013          100 CONTINUE
8014          IF (KASE .EQ. 0) GO TO 110
8015          KATKOL(KATG) = 10
8016          KATKAS(1,KATG) = KASE
8017          GO TO 120
8018          110 KATKOL(KATG) = 0
8019          KATKAS(1,KATG) = 0
8020          120 KASNUM = KASNUM + KASE
8021          C   CATEGORY 8---BELT FORCES
8022          KATG = 8
8023          KASE = 0
8024          IF (NBLT .LE. 0) GO TO 150
8025          DO 140 I = 1, NBLT
8026             KBL = IABS(MNBLT(I))
8027             IF (KBL .EQ. 0) GO TO 140
8028             DO 130 J = 1, KBL
8029                KASE = KASE + 1
8030             KASTRU = KASNUM + KASE
8031             KASKTL(1,KASTRU) = KATG + 2
8032             KASKTL(2,KASTRU) = MBLT(1,J,I)
8033             KASKTL(3,KASTRU) = I
8034             KASKTL(4,KASTRU) = MBLT(2,J,I)
8035             KASKTL(5,KASTRU) = MBLT(3,J,I)
8036          130  CONTINUE
8037          140 CONTINUE
8038          KATKOL(KATG) = 4
8039          KATKAS(1,KATG) = KASE
8040          GO TO 160
8041          150 KATKOL(KATG) = 0
8042          KATKAS(1,KATG) = 0
8043          160 KASNUM = KASNUM + KASE
8044          C   CATEGORY 9---HARNESS BELT FORCES
8045          KATG = 9
8046          KASE = 0
8047          IF (NHRNSS .LE. 0) GO TO 190
8048          J1 = 1
8049          K1 = 1
8050          DO 180 I = 1, NHRNSS
8051             KBL = NBLTPH(I)
8052             IF (KBL .LE. 0) GO TO 180
8053             J2 = J1 + KBL - 1
8054             DO 170 J = J1, J2
8055                KASE = KASE + 1
8056                KASTRU = KASNUM + KASE
8057                KN = NPTSPB(J)
8058                IF (KN .LE. 0) GO TO 170
8059                K2 = K1 + KN - 1
8060                KASKTL(1,KASTRU) = KATG + 2
8061          C   HARNESS BELT NUMBER
8062          KASKTL(2,KASTRU) = J
8063          C   HARNESS NUMBER
8064          KASKTL(3,KASTRU) = I
8065          C   FIRST AND LAST POINT NUMBERS
8066          KASKTL(4,KASTRU) = K1
8067          KASKTL(5,KASTRU) = K2
8068          K1 = K2 + 1

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8069 170 CONTINUE
8070     J1 = J2 + 1
8071 180 CONTINUE
8072     KATKOL(KATG) = 4
8073     KATKAS(1,KATG) = KASE
8074     GO TO 200
8075 190 KATKOL(KATG) = 0
8076     KATKAS(1,KATG) = 0
8077     KASNUM = KASNUM + KASE
8078     CATEGORY 10---SPRING DAMPER FORCES
8079     KATG = 10
8080     KASE = 0
8081     IF (NSD .LE. 0) GO TO 220
8082     DO 210 I = 1, NSD, 2
8083     KASE = KASE + 1
8084     KASTRU = KASNUM + KASE
8085     KASKTL(1,KASTRU) = KATG + 2
8086     KASKTL(2,KASTRU) = MSDM(I)
8087     KASKTL(3,KASTRU) = MSDN(I)
8087.1   KASKTL(4,KASTRU) = 0
8087.2   KASKTL(5,KASTRU) = 0
8088     IF (I .EQ. NSD) GO TO 210
8089     KASKTL(4,KASTRU) = MSDM(I + 1)
8090     KASKTL(5,KASTRU) = MSDN(I + 1)
8091 210 CONTINUE
8092     KATKOL(KATG) = 4
8093     KATKAS(1,KATG) = KASE
8094     GO TO 230
8095 220 KATKOL(KATG) = 0
8096     KATKAS(1,KATG) = 0
8097     KASNUM = KASNUM + KASE
8098     CATEGORY 11---AIRBAG PARAMETERS
8099     KATG = 11
8100     KASE = 0
8101     IF (NBAG .LE. 0) GO TO 250
8102     NUM = NBAG + NBAG
8103     DO 240 I = 1, NUM
8104     KASE = KASE + 1
8105     KASTRU = KASNUM + KASE
8106     KB = (NUM + 1) / 2
8107     KC = 2 - MOD(NUM,2)
8108     KASKTL(1,KASTRU) = KATG + 2
8109     NUMBER OF AIRBAG
8110     KASKTL(2,KASTRU) = KB
8111     NUMBER OF PARAMETER GROUP
8112     KASKTL(3,KASTRU) = KC
8113 240 CONTINUE
8114     KATKOL(KATG) = 6
8115     KATKAS(1,KATG) = KASE
8116     GO TO 260
8117 250 KATKOL(KATG) = 0
8118     KATKAS(1,KATG) = 0
8119     KASNUM = KASNUM + KASE
8120     CATEGORY 12---AIRBAG CONTACT FORCES
8121     KATG = 12
8122     KASE = 0
8123     IF (NBAG .LE. 0) GO TO 290
8124     DG 280 I = 1, NBAG
8125     KPA = NPANEL(I) + 1
8126     KPT = KPA + MNBAG(I)

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8127 IF (KPT .LE. O) GO TO 280
8128 DO 270 J = 1, KPT, 2
8129 J1 = J
8130 J2 = MINO(J+1, KPT)
8131 J5 = J2 - J1 + 1
8132 IF (J2 .GT. KPA) GO TO 262
8133 J5 = -J5
8134 J3 = -J1
8135 J4 = -J2
8136 GO TO 266
8137 262 IF (J1 .GT. KPA) GO TO 264
8138 J5 = O
8139 J3 = -J1
8140 J4 = MBAG(2, J2-KPA, I)
8141 GO TO 266
8142 264 J3 = MBAG(2, J1-KPA, I)
8143 J4 = MBAG(2, J2-KPA, I)
8144 KASE = KASE + 1
8145 KASTRU = KASNUM + KASE
8146 KASKTL(1,KASTRU) = KATG + 2
8147 KASKTL(2,KASTRU) = I
8148 KASKTL(3,KASTRU) = J3
8149 KASKTL(4,KASTRU) = J4
8150 KASKTL(5,KASTRU) = J5
8151 266 CONTINUE
8152 270 CONTINUE
8153 280 CONTINUE
8154 KATKOL(KATG) = 6
8155 KATKAS(1,KATG) = KASE
8156 GO TO 300
8157 290 KATKOL(KATG) = O
8158 KATKAS(1,KATG) = O
8159 KASNUM = KASNUM + KASE
8160 DO 320 I = 1, 5
8161 IF (KATKAS(1,I) .GT. O) GO TO 310
8162 KATKAS(2,I) = O
8163 KATKAS(3,I) = O
8164 GO TO 320
8165 KATKAS(2,I) = 1
8166 KATKAS(3,I) = KATKAS(1,I)
8167 310 CONTINUE
8168 LAST = O
8169 DO 340 I = 6, 12
8170 IF (KATKAS(1,I) .GT. O) GO TO 330
8171 KATKAS(2,I) = O
8172 KATKAS(3,I) = O
8173 GO TO 340
8174 KATKAS(2,I) = LAST + 1
8175 LAST = LAST + KATKAS(1,I)
8176 KATKAS(3,I) = LAST
8177 330 CONTINUE
8178 WRITE (6,350) KASNUM
8179 ES//20X,
1 'NUMBER OF CASES = ', I4/5X, 'CASE', 5X
2 'CATEGORY', 5X,
'N', 8X, 'NN', 10X, 'M', 8X, 'MM'
DO 510 J = 1, KASNUM
KAT = KASKTL(1,J)
N = KASKTL(2,J)
NN = KASKTL(3,J)
8180
8181
8182
8183
8184

```

		8185	M = KASKTL(4,J)	
		8186	MM = KASKTL(5,J)	
		8187	JJ = KAT - 7	
		8188	IF (JJ .LT. 1) GO TO 510	
		8189	IF (JJ .GT. 7) GO TO 510	
		8190	DO 360 I = 1, 7	
		8191	RSTF(I) = BLANK	
		8192	360 CONTINUE	
		8193	GO TO (370, 390, 400, 420, 430, 440, 460), J	
			J	
		8194	370 DO 380 I = 1, 5	
		8195	RSTF(I) = PLTTL(I,NN)	
		8196	380 CONTINUE	
		8197	GO TO 480	
		8198	390 RSTF(4) = SEG(N)	
		8199	GO TO 480	
		8200	400 DO 410 I = 1, 5	
		8201	RSTF(I) = BLTTTL(I,NN)	
		8202	410 CONTINUE	
		8203	GO TO 480	
		8204	420 RSTF(3) = HARN1	
		8205	RSTF(4) = HARN2	
		8206	GO TO 490	
		8207	430 RSTF(2) = SPDAM1	
		8208	RSTF(3) = SPDAM2	
		8209	RSTF(4) = SPDAM3	
		8210	RSTF(5) = SPDAM4	
		8211	GO TO 490	
		8212	440 DO 450 I = 1, 5	
		8213	RSTF(I) = BAGTTL(I,N)	
		8214	450 CONTINUE	
		8215	RSTF(7) = PARM	
		8216	GO TO 490	
		8217	460 DO 470 I = 1, 5	
		8218	RSTF(I) = BAGTTL(I,N)	
		8219	470 CONTINUE	
		8220	RSTF(7) = PNTS	
		8221	GO TO 490	
		8222	480 RSTF(6) = VS	
		8223	RSTF(7) = SEG(M)	
		8224	490 WRITE (6,500) J, KAT, N, NN, M, MM, (RSTF(I)	
			.I=1,7)	
		8225	500 FORMAT (5X, I3, 5X, I7, 3X, I6, 2X, I6, 7X,	
			I6, 2X, I6, 5X, 6A4,	
		8226	1 2X, A4)	
		8227	510 CONTINUE	
		8228	WRITE (6,520) (K,(KATKAS(I,K),I=1,3),KATKOL(K)	
			,K=1,12)	
		8229	520 FORMAT ('O', 40X, ' CASES BY CATEGORY'/5X, 'CA	
			TEGORY', 5X,	
		8230	1 'NUMBER OF CASES', 5X, 'STARTING CASE',	
			5X, 'ENDING CASE',	
		8231	2 5X, 'RECORDED COLUMNS'/(5X,I6,10X,I6,15	
			X,I6,10X,I6,14X,I6))	
		8232	IF (IOTALK .NE. 0) WRITE (6,660)	
=	1579	C		
	1580		DO 20 K=1,7	=
=	1581	C		
	1582	C	INPUT CARDS H.(K).(J) FOR K=1,3	=
			8233	C
			8234	C RECORD TIME INVARIANT INFORMATION ON HOLD FIL
				E WITH 1ST TIME
			8235	C
			8236	NRNVAR = 3

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1583 C          IF (K.LE.3) READ (5,18) KSG,(MSG(J,K),(XSG(I,J
1584 ,K),I=1,3),J=1,KSG)
1585 C          IF (K.LE.3) WRITE(6,88) KSG,(MSG(J,K),(XSG(I,J
1586 ,K),I=1,3),J=1,KSG)
1587 C          18 FORMAT(2I6,3F12.6/(I12,3F12.6))
1588 C          88 FORMAT(1X,'CARDS H.(K).(J)',/,1X,2I6,3F12.6/(1
1589 X,I12,3F12.6))
=
1588 C          INPUT CARDS H.(K)          FOR K=4,7
1589 C
8237 LAST = NRVAR
8238 CALL STASH(VPSTTL, 20, LAST)
8239 CALL STASH(COMENT, 40, LAST)
8240 IF (NBLT .LE. O) GO TO 530
8241 LBBELT = LAST
8242 CALL STASH(BLTTL, 5*NBLT, LAST)
8243 IF (NBAG .LE. O) GO TO 540
8244 LBBAG = LAST
8245 CALL STASH(BAGTTL, 5*NBAG, LAST)
8246 IF (NJNT .LE. O) GO TO 550
8247 LBJNT = LAST
8248 CALL STASH(JOINT, NJNT, LAST)
8249 IF (NSEG .LE. O) GO TO 590
8250 LBSEG = LAST
8251 CALL STASH(SEG, NGRND, LAST)
8252 CALL STASH(FLPMI, NSEG, LAST)
8253 LK = O
8254 DO 580 K = 1, NSEG
8255 DO 570 J = 1, 3
8256 DO 560 I = 1, 3
8257 LK = LK + 1
8258 FDPMI(LK) = DPMI(I,J,K)
8259 CONTINUE
8260 CONTINUE
8261 CONTINUE
8262 CALL STASH(FDPMI, LK, LAST)
8263 IF (NPL .LE. O) GO TO 600
8264 LBPL = LAST
8265 CALL STASH(PLTTL, 5*NPL, LAST)
8266 LLFRST = LAST
8267
8268 C          COMPUTE LAYOUT SPACING AND BASE INDICES
8269 C          FOR INDIVIDUAL CASES
=
8270 C
8271 C          STPMIN = DMIN1(HMAX,IMIN)*1000.DO
8272 IF (NPRT(4) .EQ. O) STPMIN = DT*1000.DO
8273 RSTF(1) = STPMIN
8274 TIMMAX = NSTEPS * DT * 1000.DO
8275 MAXPTS = -1
8276 IF (STPMIN .GT. O.) MAXPTS = TIMMAX / STPMIN +
1.5
8277 C          LIMIT MAXPTS TO MAXIMUM TIME POINT CAPACITY
OF CVSOUT
8278 MAXPTS = MINO(MAXPTS,6000)
8279 LSTEP = (MAXPTS + 2) / 3 + 1
8280 NRBAS(1) = O
8281 LFIRST(1) = -1
8282 DO 610 I = 2, 6
8283 ILAS = I - 1
8284 NRBAS(I) = NRBAS(ILAS) + KATKAS(1,ILAS) *
LSTEP
8285 LFIRST(I) = -1
8286 IF (KATKAS(I,ILAS) .LE. O) NRBAS(ILAS) = O
8287 CONTINUE
8288 KASTOP = KASNUM + 5

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8289 DO 620 I = 7, KASTOP
8290   NRNBAS(I) = NRNBAS(I - 1) + LSTEP
8291   IF (I .GT. KASNUM) GO TO 620
8292     LFIRST(I) = -1
8293   620 CONTINUE
8294     WRITE (6,630) KASTOP
8295   630 FORMAT ('1', 40X, 'TIME VARIANT QUANTITIES RECO
8296     RDED (NUMBER =', I5,
8297     ')/5X, 'QUANTITY NO.', 4X, 'QUANTITY H
8298     EADER REC',
8299     'ORD NO.', 4X, 'RECORDING CATEGORY', 5X
8300     , 'NUMBER OF CASES',
8301     5X, 'CASE NO.')
8302   DO 650 I = 1, KASTOP
8303     IF (I .GT. 5) GO TO 633
8304     KATG = I
8305     NUM = KATKAS(1,KATG)
8306     KAS = 0
8307     GO TO 636
8308   633   NUM = 1
8309     KAS = I - 5
8310     KATG = KASKTL(1,KAS)
8311   636   WRITE (6,640) I, NRNBAS(I), KATG, NUM, KAS
8312   640   FORMAT (8X, I6, 19X, I6, 19X, I6, 15X, I5, 1
8313     OX, I6)
8314   650 CONTINUE
8315     WRITE (6,660)
8316   660   FORMAT ('1')
8317     CALL STASH(FFIRST(1), KASNUM, LAST)
8318     CALL STASH(FRNBAS, KASTOP, LAST)
8319     CALL STASH(FKASKL, 5*KASNUM, LAST)
8320     LFENKT = 51
8321     KPREL(1) = LAST + (KWDPLN + LFENKT - 1) / KWD
8322     PLN + 1
8323     KPREL(2) = 1
8324     KPREL(3) = 1
8325     CALL STASH(FENKAT, LFENKT, LAST)
8326     IZERO = 0
8327     RSTF(2) = PI
8328     RSTF(3) = G
8329     RSTF(4) = RADIAN
8330     RSTF(5) = UNITL
8331     RSTF(6) = UNITR
8332     RSTF(7) = UNITM
8333     RSTF(8) = DT * 1000.DO
8334     RSTF(9) = TIMMAX
8335     WRITE (LDNWRK'1) IZERO, IZERO, IZERO, IZERO, I
8336     ZERO, IZERO,
8337     1 IZERO, IZERO
8338     WRITE (LDNWRK'2) NVEH, NGRND, NSEG, NPL, NJUNT,
8339     NSD, NBAG, NBLT,
8340     1 NHRNSS, MAXPTS, LSTEP, NSTEPS, KASNUM, N
8341     RNVAR, LBBELT,
8342     2 LBBAG, LBJNT, LBSEG, LBPL, LLFRST
8343     WRITE (LDNWRK'3) DATE, BDYTTL, KASTOP, LFENKT,
8344     (RSTF(I), I=1,9),
8345     1 NPRT(4)
8346     IF (IOTALK .EQ. 0) GO TO 680
8347     WRITE (6,670) NVEH, NGRND, NSEG, NPL, NJUNT, NS
8348     D, NBAG, NBLT,

```


1NHRNSS, MAXPTS, LSTEP, NSTEPS, KASNUM, NNRVAR,
 LBBELT, LBBAG,
 2LBJNT, LBSEG, LBPL, LLFRST, DATE, BDYTTL, KAST
 OP, LFENKT,
 3(RSTF(I), I=1,9), NPRT(4)
 670 FORMAT ('O RN=2 ', 20I6/' RN=3 ', 3A4, 5X, 5A
 4. 2I6, 3G20.10/7X,
 1 G20.10, 8X, A4, 16X, A4, 16X, A4, 8X, 2
 G20.10, I3)
 C
 C RECORD TIME VARIANT INFORMATION ON HOLD FILE
 FOR CURRENT TIME

8339
 8340
 8341
 8342
 8343
 8344
 8345

```

1590 C
1591 IF (K.GT.3) READ (5,19) KSG,(MSG(J,K),J=1,KSG)
1592 IF (K.GT.3) WRITE(6,89) KSG,(MSG(J,K),J=1,KSG)
1593 19 FORMAT(12I6/(I12,10I6))
1594 89 FORMAT(1X,'CARDS H.(K)FOR K =4,7',/,1X,2I6,3F1
1595 2.6/(1X,I12,3F12.6))
1596 IF (K.NE.7 .OR. KSG.EQ.0) GO TO 20
1597 DO 12 J=1,KSG
1598 L = MSG(J,K)
1599 IF (IABS(IPIN(L)).EQ.4) MSG(J,K) = -L
1600 12 CONTINUE
1601 20 NSG(K) = KSG
1602 10 IF (.NOT.LTAPE8) GO TO 21
1603 WRITE (8) NSEG,NJNT,NPL,NBLT,NBAG,NVEH
1604 .NGRND,NPANEL,
1605 *
1606 T,MSEG,MBAG
1607 WRITE (8)
1608 TTTL,PLTTL,BAGTTL,
1609 *
1610 G,MSG,XSG,
1611 *
1612 MSDN
1613 21 LINES = LINES + 1
1614 IF (MOD(LINES,LPP).EQ.1 .AND. LTHIST) CALL H
1615 EDING (LINES,LPP)
1616 NT = 20
1617 USEC = 1000.0*TIME
1618 C COMPUTE AND PRINT DATA FOR 7 TYPES OF OUTPUT A
1619 BOVE
1620 C
1621 DO 44 K=1,7
1622 IF (NSG(K).LE.0) GO TO 44
1623 KSG = NSG(K)
1624 J3 = 3
1625 IF (K.EQ.7) J3 = 2
1626 DO 43 J1=1,KSG,J3
1627 J2 = MINO(J1+J3-1,KSG)
1628 NT = NT+1
1629 DO 38 J=J1,J2
1630 L = IABS(MSG(J,K))
1631 GO TO (22,24,26,29,31,34,35),K
1632 C 1. SEGMENT LINEAR ACCELERATIONS IN LOCAL REFER
1633 ENCE
1634 C
1635 22 CALL CROSS (WMEG(1,L),XSG(1,J,K),T1)
1636
1637
1638
1639
1640
1641
1642
1643
1644
1645
1646
1647
1648

```

```

1629 CALL CROSS (WMEG(1,L),T1,T2)
1630 CALL CROSS (WMEGD(1,L),XSG(1,J,K),T3)
1631 CALL MAT31(D(1,1,L),SEGLA(1,L),T4)
1632 DO 23 I=1,3
1633 ACC(I,J) = (T4(I)+T3(I)+T2(I))/G
1634 T1(I) = ACC(I,J)
1635 IF (LPMI(L).NE.O) CALL DOT31 (DPMI(1,1,L),T1
    .ACC(1,J))
    GO TO 33
1636 C
1637 C
1638 C 2. SEGMENT LINEAR VELOCITIES IN VEHICLE REFERENCE
    NCE
1639 C
1640 CALL CROSS (WMEG(1,L),XSG(1,J,K),T1)
1641 CALL DOT31(D(1,1,L),T1,T2)
1642 DO 25 I=1,3
1643 T3(I) = T2(I) + SEGLV(I,L) - SEGLV(I,NVEH)
1644 GO TO 28
1645 C
1646 C 3. SEGMENT LINEAR DISPLACEMENTS IN VEHICLE REFERENCE
1647 C
1648 IF (LPMI(L).EQ.O) GO TO 76
1649 CALL DOT33 (DPMI(1,1,L),D(1,1,L),T4)
1650 CALL DOT31 (T4,XSG(1,J,K),T1)
1651 GO TO 77
1652 CALL DOT31 (D(1,1,L),XSG(1,J,K),T1)
1653 DO 27 I=1,3
1654 T3(I) = T1(I) + SEGLP(I,L) - SEGLP(I,NVEH)
1655 CALL MAT31 (D(1,1,NVEH),T3,ACC(1,J))
1656 GO TO 33
1657 C
1658 C 4. SEGMENT ANGULAR ACCELERATIONS IN LOCAL REFERENCE
1659 C
1660 DO 30 I=1,3
1661 ACC(I,J) = WMEGD(I,L)/(2.0*PI)
1662 T1(I) = ACC(I,J)
1663 IF (LPMI(L).NE.O) CALL DOT31 (DPMI(1,1,L),T1
    .ACC(1,J))
    GO TO 33
1664 C
1665 C
1666 C 5. SEGMENT ANGULAR VELOCITIES IN VEHICLE REFERENCE
1667 C
1668 CALL DOT31 (D(1,1,L),WMEG(1,L),T1)
1669 CALL MAT31 (D(1,1,NVEH),T1,T2)
1670 DO 32 I=1,3
1671 ACC(I,J) = (T2(I)-WMEG(I,NVEH))/(2.0*PI)
1672 ACC(4,J) = DSQRT(ACC(1,J)**2+ACC(2,J)**2+ACC(3
    ,J)**2)
    GO TO 38
1673 C
1674 C
1675 C 6. SEGMENT ANGULAR DISPLACEMENTS IN VEHICLE REFERENCE
1676 C
1677 IF (LPMI(L).EQ.O) GO TO 36
1678 CALL DOT33(DPMI(1,1,L),D(1,1,L),T4)
    CALL DOT33(T4,D(1,1,NVEH),T1)
1679

```

```

8356 KSTF(3) = MULTPL
8357 KATG = 1
8358 KASE = 1
8359 CALL OUTREC(RSTF(1))
8360 IF (LINES.EQ.1) GO TO 690
8361 KOPY = 0
8362 IF (USEC.LE.TIMLAS) GO TO 690
8363 KOPY = 1
8364 INCCUR = (USEC - TIMLAS) / STPMIN + .5
8365 INCSML = MINO(INCSML,INCCUR)
8366 INCBIG = MAXO(INCBIG,INCCUR)
8367 IF (NGRND.LE.O) GO TO 720
8368 DO 710 I = 1, NGRND
8369 DO 700 J = 1, 3
8370 RSTF(J) = SEGLP(J,I)
8371 RSTF(J + 3) = SEGLV(J,I)
8372 RSTF(J + 6) = SEGLA(J,I)
8373 RSTF(J + 9) = WMEG(J,I)
8374 RSTF(J + 12) = WMEGD(J,I)
8375 RSTF(J + 15) = U1(J,I)
8376 RSTF(J + 18) = D(J,1,I)
8377 RSTF(J + 21) = D(J,2,I)
8378 RSTF(J + 24) = D(J,3,I)
8379 CONTINUE
8380 KATG = 2
8381 KASE = I
8382 CALL OUTREC(RSTF(1))
8383 KATG = 3
8384 KASE = I
8385 CALL OUTREC(RSTF(10))
8386 KATG = 4
8387 KASE = I
8388 CALL OUTREC(RSTF(19))
8389 CONTINUE
8390 IF (NJNT.LE.O) GO TO 750
8391 KATG = 5
8392 DO 740 I = 1, NJNT
8393 DO 730 J = 1, 7
8394 RSTF(J) = PRJNT(J,I)
8395 CONTINUE
8396 KSTF(8) = IPIN(I)
8397 KASE = I
8398 CALL OUTREC(RSTF(1))
8399 CONTINUE
8400 IF (KASNUM.LE.O) GO TO 890
8401 DO 880 II = 1, KASNUM
8402 KASE = ABSOLUTE CASE NUMBER AMONG ALL TIME D
    EPENDANT RECS
8403 KASE = II
8404 KATG = KASKTL(1,II) - 2
8405 KAS = RELATIVE CASE NUMBER WITHIN RECORDING
    CATEGORY
8406 KAS = KASE - KATKAS(2,KATG) + 1

```

```

1680 GO TO 37
1681 36 CALL DOTT33 (D(1,1,L),D(1,1,NVEH),T1)
1682 37 CALL YPRDEG(T1,ACC(1,J))
1683 TRACE = 0.5*(T1(1)+T2(2)+T3(3))-1.0)
1684 IF (TRACE.GT. 1.0) TRACE = 1.0
1685 IF (TRACE.LT.-1.0) TRACE = -1.0
1686 ACC(4,J) = DARCOS(TRACE)/RADIAN
1687 GO TO 38
1688
1689 C
1690 C
1691 C
1692 C
1693 C
1694 C
1695 C
1696 C
1697 C
1698 C
1699 IF (.NOT.LTAPE8) GO TO 40
1700 KK = 0
1701 I2 = 4
1702 IF (K.EQ.7) I2 = 7
1703 DO 39 J=J1,J2
1704 DO 39 I=1,I2
1705 KK = KK+1
1706 39 TDATA(KK,NT-20) = ACC(I,J)
1707 40 IF (.NOT.LTHIST) GO TO 43
1708 IF (K.LE.6) WRITE (NT,41) USEC,((ACC(I,J),I=1,
4),J=J1,J2)
1709 41 FORMAT(F9.3,3(X,4F9.3) )
1710 IF (K.EQ.7) WRITE (NT,42) USEC,((ACC(I,J),I=1,
7),J=J1,J2)
1711 42 FORMAT(F9.3,2(F5.0,3F9.3,2X,3F9.3))
1712 43 CONTINUE
1713
1714 44 CONTINUE
1715 C
1716 C
1717 C
1718 C
1719 C
1720 C
1721 45 MPST = MPST + MNPL(J)
1722 IF (MPSF.EQ.0) GO TO 49
1723 DO 47 J1=1,MPSF,2
1724 J2 = MINO(J1+1,MPSF)
1725 NT = NT+1
1726 IF (.NOT.LTAPE8) GO TO 47
1727 KK = 0
1728 DO 46 J=J1,J2
1729 DO 46 I=1,7
1730 KK = KK+1
1731 46 TDATA(KK,NT-20) = PSF(I,J)
1732 47 IF (LTHIST) WRITE (NT,48) USEC,((PSF(I,J),I=
1,7),J=J1,J2)
1733 48 FORMAT(F9.3,2(F9.3,3F9.2,3F8.3) )
C

```

```

8407 KOL = KATKOL(KATG)
8408 K = KATG - 5
8409 GO TO (760, 780, 820, 800, 810, 850, 840), K
8410 DO 770 I = 1, KOL
8411 RSTF(I) = PSF(I,KAS)
8412 CONTINUE
8413 GO TO 870
8414 DO 790 I = 1, KOL
8415 RSTF(I) = SSF(I,KAS)
8416 CONTINUE
8417 GO TO 870
8418 IF (KATKAS(2,8) .LE. 0) GO TO 820
8419 KAS = KAS + KATKAS(2,9) - KATKAS(2,8)
8420 GO TO 820
8421 IF (KATKAS(2,8) .LE. 0) GO TO 815
8422 KAS = KAS + KATKAS(2,10) - KATKAS(2,8)
8423 GO TO 820
8424 IF (KATKAS(2,9) .LE. 0) GO TO 820
8425 KAS = KAS + KATKAS(2,10) - KATKAS(2,9)
8426 DO 830 I = 1, KOL
8427 RSTF(I) = BSF(I,KAS)
8428 CONTINUE
8429 GO TO 870
8430 KAS = KAS + KATKAS(2,12) - KATKAS(2,11)
8431 K = KAS + KAS - 1
8432 DO 860 I = 1, KOL
8433 RSTF(I) = BAGSF(I,K)
8434 CONTINUE
8435 CALL OUTREC(RSTF(1))
8436
8437 880 CONTINUE
8438 890 RSTF(1) = USEC
8439
8440 L, INCBIG, INCSML
8441 IF (IOTALK .NE. 0) WRITE (6,900) RSTF(1), LINE
8442 S, LASREC, MULTPL,
8443 1 INCBIG, INCSML
8444 900 FORMAT ('O RN=1 ', G20.10, 7I12)
8445 LAST = LLFRST
8446 CALL STASH(FFIRST(1), KASNUM, LAST)
8447 IF (KOPY .NE. 0) TIMLAS = USEC
8448 CALL ELTIME(2, 8)
8449 910 RETURN
8450 920 WRITE (6,930)
8451 930 FORMAT ('OFATAL ERROR---MORE TIME POINTS THAN
MIMUM STEP. ')
8452 STOP 1111

```



```

1734 C PRINT BELT FORCES
1735 C
1736 49 MBSF = 0
1737 IF (NBLT.EQ.O) GO TO 67
1738 DO 50 J=1,NBLT
1739 50 MBSF = MBSF + MBLT(J)
1740 IF (MBSF.EQ.O) GO TO 67
1741 DO 52 J1=1,MBSF.2
1742 J2 = MINO(J1+1,MBSF)
1743 NT = NT+1
1744 IF (.NOT.LTAPE8) GO TO 52
1745 KK = 0
1746 DO 51 J=J1,J2
1747 DO 51 I=1,4
1748 KK = KK+1
1749 51 TDATA(KK,NT-20) = BSF(I,J)
1750 52 IF (LTHIST) WRITE (NT,53) USEC,((BSF(I,J),I=
1,4),J=J1,J2)
1751 53 FORMAT(F9.3,4(F15.6,F12.2,3X) )
1752 C
1753 C PRINT HARNESS-BELT ENDPOINT FORCES (STORED IN
BSF ARRAY).
1754 C
1755 67 IF (NHRNSS.LE.O) GO TO 71
1756 MBSF1 = MBSF + 1
1757 DO 68 I=1,NHRNSS
1758 68 MBSF = MBSF + NBLTPH(I)
1759 DO 70 J1=MBSF1,MBSF.2
1760 J2 = MINO(J1+1,MBSF)
1761 NT = NT+1
1762 IF (.NOT.LTAPE8) GO TO 70
1763 KK = 0
1764 DO 69 J=J1,J2
1765 DO 69 I=1,4
1766 KK = KK+1
1767 69 TDATA(KK,NT-20) = BSF(I,J)
1768 70 IF (LTHIST) WRITE (NT,53) USEC,((BSF(I,J),I=
1,4),J=J1,J2)
1769 C
1770 C PRINT SPRING DAMPER FORCES (STORED IN BSF ARRA
Y).
1771 C
1772 71 IF (NSD.LE.O) GO TO 54
1773 MBSF1 = MBSF + 1
1774 MBSF = MBSF + (NSD+1)/2
1775 DO 73 J1=MBSF1,MBSF.2
1776 J2 = MINO(J1+1,MBSF)
1777 NT = NT+1
1778 IF (.NOT.LTAPE8) GO TO 73
1779 KK = 0
1780 DO 72 J=J1,J2
1781 DO 72 I=1,4
1782 KK = KK+1
1783 72 TDATA(KK,NT-20) = BSF(I,J)
1784 73 IF (LTHIST) WRITE (NT,74) USEC,((BSF(I,J),I=
1,4),J=J1,J2)
1785 74 FORMAT (F9.3,4(F14.3,F12.2,4X))
1786 C
1787 C PRINT SEGMENT CONTACT FORCES
1788 C

```

```

1789 54 MSSF = 0
1790 DO 55 J=1,NSEG
1791 55 MSSF = MSSF + MNSEG(J)
1792 IF (MSSF.EQ.O) GO TO 59
1793 DO 57 J=1,MSSF
1794 NT = NT+1
1795 IF (.NOT.LTAPE8) GO TO 57
1796 DO 56 I=1,10
1797 56 TDATA(I,NT-20) = SSF(I,J)
1798 57 IF (LTHIST) WRITE (NT,58) USEC.((SSF(I,J),I=1
. 10)
1799 58 FORMAT(2F9.3,3F9.2,3F8.3,2X,3F8.3)
1800 C
1801 C PRINT AIRBAG FORCES
1802 C
1803 C
1804 C
1805 59 IF (NBAG.EQ.O) GO TO 65
1806 K1 = 1
1807 DO 64 J=1,NBAG
1808 IF (MNBAG(J).EQ.O) GO TO 64
1809 KBAG = MNBAG(J)+NPANEL(J)+5
1810 DO 63 J1=1,KBAG,4
1811 J2 = MINO(J1+3,KBAG)
1812 K2 = K1+J2-J1
1813 NT = NT+1
1814 IF (.NOT.LTAPE8) GO TO 61
1815 KK = 0
1816 DO 60 K=K1,K2
1817 DO 60 I=1,3
1818 KK = KK+1
1819 60 TDATA(KK,NT-20) = BAGSF(I,K)
1820 61 IF (.NOT.LTHIST) GO TO 63
1821 IF (J1.EQ.1) WRITE (NT,75) USEC.((BAGSF(I,K)
.I=1,3),K=K1,K2)
1822 IF (J1.NE.1) WRITE (NT,62) USEC.((BAGSF(I,K)
.I=1,3),K=K1,K2)
1823 75 FORMAT (F9.3,3X,3F9.2,2(3X,3F9.3),3X,3F9.2)
1824 62 FORMAT(F9.3,4(3X,3F9.2))
1825 63 K1 = K2+1
1826 64 CONTINUE
1827 65 NT = NT-20
1828 IF (LTAPE8) WRITE (8) NT,USEC.((TDATA(I,J),I
=1,14),J=1,NT)
1829 PREVT = TIME
1830 CALL ELTIME(2,8)
66 RETURN
END
8445 END

```

Unit 0: CVSB(2564,2879)

Unit 1: SUSP:CIGS(9161,9474)

```
= 2564 SUBROUTINE PRINT(SUB)
=====
= 2594 * UNITL,UNITM,UNITT,GRAVITY(3)
2595 COMMON/RSAVE/XSG(3,20,3),DPMI(3,3,100),LPMI(10
O),NSG(7),MSG(20,7)
= 2596 COMMON/TEMPVS/ YPR(3),T1(3),T2(3),HH(3),T3(3,3
)
=====
= 2873 DO 20 J=1,3
2874 F(3,J,I)=E1*F(3,J,I)+T1(J)+EB*X(J,I)
2875 F(4,J,I)=E1*F(4,J,I)+T2(J)+EC*X(J,I)
2876 Y(3,J,I)=E1*Y(1,J,I)+T3(J)-E2*X(J,I)
2877 20 Y(4,J,I)=E1*Y(2,J,I)+T4(J)-E2D*X(J,I)
2878 RETURN
2879 END
=====
= 9161 SUBROUTINE PRINT(SUB)
=====
= 9191 * UNITL,UNITM,UNITT,GRAVITY(3)
9192 COMMON/RSAVE/DPMI(3,3,100),LPMI(100)
= 9193 COMMON/TEMPVS/ YPR(3),T1(3),T2(3),HH(3),T3(3,3
)
=====
= DO 20 J=1,3
9470 F(3,J,I)=E1*F(3,J,I)-T1(J)+EB*X(J,I)
9471 F(4,J,I)=E1*F(4,J,I)+EC*X(J,I)
9472 Y(3,J,I)=E1*Y(1,J,I)-T3(J)-E2*X(J,I)
9473 20 Y(4,J,I)=E1*Y(2,J,I)-T4(J)-E2D*X(J,I)
9474 RETURN
END
```

Unit O: CVSB(2918,4698)

Unit 1: SUSP:CIGS(9544,11950)

```

=====
= 2918 SUBROUTINE ROTATE 9544
=====
= 2926 * NS,NQ,NSD,NFLX,NHRNSS,NWINDF,NJNT 7 equal 1 lines
= F,NPRT(36) * NS,NQ,NSD,NFLX,NHRNSS,NWINDF,NJNT
= COMMON/RSAVE/XSG(3,20,3),DPMI(3,3,100),LPMI(10
= O),NSG(7),MSG(20,7) COMMON/RSRVE/DPMI(3,3,100),LPMI(100)
= 200),HA(3,200), PHI(3,100),W(100),RW(100),SR(3,
= * E(3,800),FF(5,800),GG(5,800),Y(5,8 SR(3,
= OO),U(5,800); E(3,800),FF(5,800),GG(5,800),Y(5,8
= * H,HPRINT,HS,TPRINT,TSTART,ICNT,IDB
= L,IFLAG. H,HPRINT,HS,TPRINT,TSTART,ICNT,IDB
= 3305 DMMY(200,25)
= 3306 C NOTE: FF REPLACES F FROM SUBROUTINE DINT.
= 3329 C 21 22 equal 1 lines
= 3330 O),NSG(7),MSG(20,7) COMMON/RSAVE/XSG(3,20,3),DPMI(3,3,100),LPMI(10
= 3331 DIMENSION RC21(450),IC21(177)
= 3332 EQUIVALENCE (RC21(1),XSG(1,1,1)), (IC21(1),LP
= MI(1))
=====
= 3333 C 22 593 equal 1 lines
= 3927 C
= 3928 SG DATA C21/ 8HXSG ,8HDPMI ,8HLPMI ,8HN ,8H*
= ,8HMSG /
= 3929 DATA NC21/3,20,3 , 3,3,30 , 30,0,0 , 7,0
= ,0 , 20,7,0 /
=====
= 4492 * UNITL,UNITM,UNITT,GRAVITY(3) 562 equal 1 lines
= COMMON /PLOTTRS/ ELYPR(3,100), PLPTS(3,3,100),
= NELSEG(100), LDNPSCS
= 1 IELPS, IELPB, IELP, NNELP, NPLSEG(100)
= REAL*4 PLPTS
= COMMON/TEMPVS/ P1(3),P2(3),P3(3),DE(3,3)
=====
= 4493 DATA IDYPR/3,2,1/ 1 equal 1 lines
= DO 6 I=1,100
= NPLSEG(I) = 0
= DO 4 J=1,3
= ELYPR(J,I) = 0.00
= DO 2 K=1,3
= PLPTS(J,K,I) = 0.
= 2 CONTINUE
= 4 CONTINUE
= 6 CONTINUE
= C
= DO 26 I =1,3
= PLPTS(1,I,J) = P1(I)
= PLPTS(2,I,J) = P2(I)
= PLPTS(3,I,J) = P3(I)
= P2(I) = P2(I)-P1(I)
=====

```

```

= 4595      35 IF (NBAG.NE.O) CALL AIRBG1
=
= 4596      IF (NELP.LE.O) GO TO 51
=
= 4618      BD(I+3,M) = P2(I)
=
= 4619      DO 45 J=1,3
=
= 4627      45 BD(K+9,M) = SUM2
=
= 4628      50 CONTINUE
=
= 4629      C
=
= 4671      * 5X,'SEGMENT',9X,'SEGMENT M',16X,'SEGMENT N',1
=
= 4672      * 'SPRING FORCE FUNCTION',12X,'DAMPING FORCE FUN
=
= 4673      * , NO. M N',2(6X,'X',7X,'Y',7X,'Z',2X),7X,'
=
= 4698      DO',9X,'A1',11X,
=
=          END
=
11237      35 IF (NBAG.NE.O) CALL AIRBG1
11238      NNELP = NSEG
11239      IELP = O
11240      IELPB = O
11241      IELPS = 101
11242      IF (NELP.LE.O) GO TO 51
11264      BD(I+3,M) = P2(I)
11265      ELYPR(I,M) = P3(I)
11266      DO 45 J=1,3
11274      45 BD(K+9,M) = SUM2
11275      IF (M.LE.NSEG) GO TO 50
11276      IELPS = MINO(IELPS, M)
11277      IELPB = MAXO(IELPB, M)
11278      IELP = IELP + 1
11279      50 CONTINUE
11280      NNELP = NSEG + IELP
11281      C
11323      * 5X,'SEGMENT',9X,'SEGMENT M',16X,'SEGMENT N',1
11324      * 'SPRING FORCE FUNCTION',12X,'DAMPING FORCE FU
11325      * , NO. M N',2(6X,'X',7X,'Y',7X,'Z',2X),7X,'
11350      DO',9X,'A1',11X,
11350      END

```

5058	=====	SUBROUTINE TRIGFS	11649	=====	SUBROUTINE TRIGFS
5062	*	E(3.800), F(5.800), GG(5.800), Y(5.8	lines	=====	E(3.800), F(5.800), GG(5.800), Y(5.8
5063	*	H, HPRINT, HS, TPRINT, TSTART, ICNT, IDB	11654	=====	H, HPRINT, HS, TPRINT, TSTART, ICNT, IDB
5064	*	DMMY(200, 25)		=====	
5065	BETA = 0.0		11655	=====	BETA = 0.0
5115	*	NTPL(5, 100), NTBLT(5, 8), NTSEG(5	lines	=====	NTPL(5, 100), NTBLT(5, 8), NTSEG(5
5116	, 100)		11706	=====	, 100)
5117	O), NSG(7), MSG(20, 7)			=====	COMMON/RSAVE/DPMI(3, 3, 100), LPMI(100)
	COMMON/TEMPVS/ XD(3, 3, 100), XSEGLP(3, 100), XPL(1		11707	=====	COMMON/TEMPVS/ XD(3, 3, 100), XSEGLP(3, 100), XPL(1
	7, 100), XBD(24, 110),			=====	7, 100), XBD(24, 110),
5745	=====	SUBROUTINE VINPVT	lines	=====	SUBROUTINE VINPVT
5746	C		12335	=====	
5747	REV 20 05/07/80		12336	=====	
	C PERFORMS CARD INPUT AND COMPUTES DATA AND TABL			=====	C PERFORMS CARD INPUT AND COMPUTES DATA AND TABL
	ES REQUIRED BY			=====	ES REQUIRED BY
5758	COMMON/SGMNTS/ D(3, 3, 100), WMEG(3, 100), WMEGD(3,		lines	=====	COMMON/SGMNTS/ D(3, 3, 100), WMEG(3, 100), WMEGD(3,
5759	100), U1(3, 100),		12347	=====	100), U1(3, 100),
	* U2(3, 100), SEGLP(3, 100), SEGLV(3, 100), SEGLA(3,		12348	=====	* U2(3, 100), SEGLP(3, 100), SEGLV(3, 100), SEGLA(3,
	100), NSYM(100)			=====	100), NSYM(100)
5760	COMMON/DESCRP/ PHI(3, 100), W(100), RW(100), SR(3,		12349	=====	COMMON/DESCRP/ PHI(3, 100), W(100), RW(100), SR(3,
	200), HA(3, 200)			=====	200), HA(3, 200)
5761	* HB(3, 200), RPHI(3, 100), HT(3, 3, 200), SPRING(5, 300		12350	=====	* HB(3, 200), RPHI(3, 100), HT(3, 3, 200), SPRING(5, 300
), VISC(7, 300),			=====), VISC(7, 300),
5762	* JNT(100), IPIN(100), ISING(100), IGLOB		12351	=====	* JNT(100), IPIN(100), ISING(100), IGLOB
	(100), JOINTF(100)			=====	(100), JOINTF(100)
5763	COMMON/VPOSTN/ ZPLT(3), SPLT(3), AXV(3, 6), VATAB(12352	=====	COMMON/VPOSTN/ ZPLT(3), SPLT(3), AXV(3, 6), VATAB(
	6, 101, 6),			=====	6, 101, 6),
5764	* VTO(6), VDT(6), TIMEV(6), OMEGV(6), N		12353	=====	* VTO(6), VDT(6), TIMEV(6), OMEGV(6), N
	VTAB(6), INDXV(6)			=====	VTAB(6), INDXV(6)
5765	COMMON/TEMPVS/ XO(3), XDOTO(3), XCOMP(3), XVCOMP(12354	=====	COMMON/TEMPVS/ XO(3), XDOTO(3), XCOMP(3), XVCOMP(
	3), ANGLE(3),			=====	3), ANGLE(3),
5766	* ATAB(15, 100), DVEH(3, 3), VMEG(3), VM		12355	=====	* ATAB(15, 100), DVEH(3, 3), VMEG(3), VM
	EGD(3),			=====	EGD(3),
5767	* XACOMP(3), THET(3), AX(3), F(5, 100), X		12356	=====	* XACOMP(3), THET(3), AX(3), F(5, 100), X
	YZ(102, 6), TT(102),			=====	YZ(102, 6), TT(102),
5768	* VIPS, VMPPH, ATO, ADT, VTIME, OMEG, NATA		12357	=====	* VIPS, VMPPH, ATO, ADT, VTIME, OMEG, NATA
	B			=====	B
5769	COMMON/INTEST/ SGTEST(3, 4, 100), XTEST(3, 400), SE		12359	=====	COMMON/INTEST/ SGTEST(3, 4, 100), XTEST(3, 400), SE
	GT(400), REGT(400)			=====	GT(400), REGT(400)
5771	COMMON/CNSNTS/ PI, RADIAN, G, THIRD, EPS(24),		line	=====	COMMON/CNSNTS/ PI, RADIAN, G, THIRD, EPS(24),
5772	* UNITL, UNITM, UNITT, GRAVITY(3)		12361	=====	* UNITL, UNITM, UNITT, GRAVITY(3)
5773	COMMON/TITLES/ DATE(3), COMENT(40), VPSTTL(20), B		12362	=====	COMMON/TITLES/ DATE(3), COMENT(40), VPSTTL(20), B
	DYTTL(5),		12363	=====	DYTTL(5),
5774	* BLTTTL(5, 8), PLTTL(5, 100), BAGTTL(5		12364	=====	* BLTTTL(5, 8), PLTTL(5, 100), BAGTTL(5
	, 6), SEG(100),			=====	, 6), SEG(100),
5775	* JOINT(100), CGS(100), JS(100)		12365	=====	* JOINT(100), CGS(100), JS(100)
5776	REAL DATE, COMENT, VPSTTL, BDYTTL, BLTTTL, PLTTL, BA		12366	=====	REAL DATE, COMENT, VPSTTL, BDYTTL, BLTTTL, PLTTL, BA
	GTTL, SEG, JOINT			=====	GTTL, SEG, JOINT

```

===== 16 equal
5793 WRITE (6,15) VPSTTL,ANGLE,VIPS,VTIME,XO,NATAB,
=
5794 ATO,ADT,MSEG
12383
5795 RDS,C'//3X,20A4//
12384
5796 VTIME',7X,'YAW',9X,'PITCH',7X,'ROLL',8X,'VIPS',8X,
12385
5797 'ADT',4X,'MSEG',
12386
5798 * 8F12.3,15,2X,2F12.6,15)
12387
5799 DA1 = ANGLE(1)*RADIAN
12388
5816 17 FORMAT('O PASSENGER COMPARTMENT DISPLACEMENT H
=
12406
5817 IISTORY'//
12407
5818 * ' ANALYTICAL HALF-SINE WAVE DECELERATION
=
12408
5819 ES =',3F7.2,
12409
5820 GO TO 28
12410
5855 ATAB(J,I) = ATAB(J,I-1) + DA2*(5.0*F1+8.0*F2
=
12445
5856 21 ATAB(J,I+1) = ATAB(J,I-1) + DA1*( F1+4.0*F2+
=
12446
5857 22 UNITS = 1.0
12447
5862 23 FORMAT('O UNIDIRECTIONAL VEHICLE POSITION TABL
=
12452
5863 ES'//
12453
5864 POSITION',,)/
12454
5865 X,('A4,')',4X)/
12455
5890 C READ LINEAR DECELERATION AND ANGULAR ACCELERAT
=
12480
5891 ION TABLES
12481
5892 C FROM CARDS C.4.
12482
5904 WRITE (6,36) LTYPE,LFIT,NPTS,
12494
5905 (TT(I),(XYZ(I,J),J=1,6),I=1,LPTS)
12495
5906 36 FORMAT ('O SPLINE FIT TABULAR INPUT'//
12496
5907 3X,'LTYPE =',I6,' LFIT =',I6,' NPTS =',
12497
5908 ,I6//
12498
5909 (F15.6,3X,3F12.3,3X,3F12.3))
12499
5910 DO 37 I=1,3
5911 XO(I) = XYZ(1,I)
5912 IF (LTYPE.EQ.1) GO TO 37
5913 XDOTO(I) = XYZ(2,I)
5914 VMERG(I) = XYZ(2,I+3)
5915 37 ANGLE(I4) = XYZ(1,I+3)
5916 DO 45 II=1,6
=
5917 CALL SPLINE (TT(LTYPE),XYZ(LTYPE,II),F,NPTS,LF
=
IT)
IT)

```

Table C.5. Comparison of GUCVS with GMCVS (Page 39 of 41)


```

12566 CALL CROSS(QC(2),W1(2),A1)
12567 DO 86 K = 1,3
12568 VMEG(K) = CCC*(W1(1)*QC(K+1) - QC(1)*W1(K+1)
+ A1(K))
12569 CALL DRCQUA(DVEH,W1)
12570 CALL YPRDEG(DVEH,ANGLE)
12571 CALL CROSS(QD(2),W1(2),QC(2))
12572 DO 89 K = 2,4
12573 ATAB(K+8,J) = CCC*(W1(1)*QD(K)-QD(1)*W1(K) +
QC(K))
12574 90 CONTINUE
12575 46 DO 55 J=1,MATAB
lines -----
12582 48 FORMAT(I1,' VEHICLE LINEAR TIME HISTORY',3X,2
OA4,3X,
)
12583 * 'PAGE NO.',I3//
12584 * 4X,'TIME',12X,'LINEAR DECELERATIONS (G'S
)',
12585 * 11X,'LINEAR VELOCITIES ('.A4,/'
',A4,')',
12586 * 11X,'LINEAR DISPLACEMENTS ('.A4
.',) /
12587 * 3X,'(MSEC)',3(11X,'X',11X,'Y',11X,'Z',3X
) /
12588 ISKIP = 1
lines -----
12594 ATAB(I+6,J) = XO(I)
12595 ATAB(I+12,J) = VMEG(I)
50 THET(I) = ANGLE(I)*RADIAN
CALL DRCYPR (DVEH,ANGLE,IDYPR)
12596 53 ATAB(I+6,J) = ATAB(I+6,J-1)
12606 * +ADT*(ATAB(I+3,J-1)-G*ADT/6.O*(2.O*ATAB(I,J-
1)+ATAB(I,J)))
12607 54 T1 = (ATO + DFLOAT(J-1)*ADT)*1000.O
lines -----
12618 57 FORMAT('1 VEHICLE ANGULAR TIME HISTORY',3X,2OA
4,3X,'PAGE NO.',I3//
G/,'.A4, '**2)',
7X,'ANGULAR VELOCITIES (DEG/'
'.A4,')',
11X,'ANGULAR DISPLACEMENTS (DE
G)' /
12622 * 3X,'(MSEC)',2(11X,'X',11X,'Y',11X,'Z',3X
),
12623 * 10X,'YAW',8X,'PITCH',8X,'ROLL' /)
12624 58 IF(J.EQ.1) GO TO 60
lines -----
12695 NGRND = NVEH+1
12696 IF (NGRND.GT.100 .OR. NVH.GT.6) STOP 7
12697 SEG(NGRND) = GRND
lines -----
13072 END

```

```

3783 SUBROUTINE DRCQUA(DC,Q)
3784 COMPUTES DIRECTION COSINE MATRIX FROM QUATERNIONS
3785 IMPLICIT REAL*8(A-H,O-Z)
3786 DIMENSION DC(3,3),Q(4)
3787 C = Q(1)**2 + Q(2)**2 + Q(3)**2 + Q(4)**2
3788 E = (Q(1) + Q(1)) / C
3789 F = Q(1) * E - 1.DO
3790 DO 12 I = 1,3
3791 DO 10 J = 1,3
3792 10 DC(I,J) = 2.0*Q(I+1)*Q(J+1) / C
3793 12 DC(I,I) = DC(I,I) + F
3794 DO 14 I = 1,3
3795 J = 1 + MOD(I,3)
3796 K = 1 + MOD(I+1,3)
3797 D = E*Q(I+1)
3798 DC(K,J) = DC(K,J) - D
3799 14 DC(J,K) = DC(J,K) + D
3800 DO 18 I = 1,3
3801 DO 18 J = 1,3
3802 18 IF(DABS(DC(I,J)).GT.1.0DO)DC(I,J) = DSIGN(1.0DO,DC(I,J))
3802.5 RETURN
3803 END

```

```

8446 SUBROUTINE OUTREC(ARRAY)
8447 DIMENSION ARRAY(2)
8448 COMMON /HLDCON/ LDINARY(3), NRNBAS(246), LFIRST(241), KASNUM,
8449 KATKOL(12), KPRLM(3), KATKAS(3,12), KASKTL(5,241), MAXPTS,
8450 LINES, KASE, KATG, NRN, LSTEP, LASREC(3)
8451
8452 C
8453 C 1. FOR KATG = 1 TO 5:
8454 KASE = 1 TO KATKAS(1,KATG)
8455 ONLY NRNBAS(KATG) APPLIES
8456 C
8457 C *2. FOR KATG = 6 TO 12:
8458 KASE = KATKAS(2,KATG) TO KATKAS(3,KATG)
8459 NRNBAS(KASE+5) AND LFIRST(KASE) APPLY
8460 C
8461 C 3. KASADJ = NRNBAS INDEX FOR ALL CATEGORIES AND CASES
8462 C
8463 LEN = KATKOL(KATG)
8464 IF (KATG .GT. 5) GO TO 10
8465 LINOFF = 0
8466 KASADJ = KATG
8467 LADJST = KASE * LSTEP - LSTEP
8468 KATABL = KATG
8469 GO TO 20
8470 10 LINOFF = LFIRST(KASE)
8471 KASADJ = KASE + 5
8472 LADJST = 0
8473 KATABL = KATG + 2
8474 20 IF (LINOFF .GE. 0) GO TO 40
8475 DO 30 I = 1, LEN
8476 IF (ARRAY(I) .EQ. 0.) GO TO 30
8477 RECORD STARTING LINES OFFSET
8478 LINOFF = LINES - 1
8479 LFIRST(KASE) = LINOFF
8480 GO TO 40
8481 30 CONTINUE
8482 GO TO 60
8483 40 LINREL = LINES - LINOFF
8484 LMOD = MOD(LINREL,3)
8485 IF (LMOD .EQ. 0) LMOD = 3
8486 LDN = LDINARY(LMOD)
8487 LBASE = NRNBAS(KASADJ) + KPRLM(LMOD) + LADJST
8488 LINREC = (LINREL + 2) / 3
8489 IF (LINREC .EQ. 1) WRITE (LDN/LBASE) KATABL, KASE, LINES, LINOFF
8490 50 NRN = LBASE + LINREC
8491 WRITE (LDN/NRN) (ARRAY(I),I=1,LEN)
8492 LASREC(LMOD) = MAXO(LASREC(LMOD), NRN)
8493 60 RETURN
8494 END
8495 SUBROUTINE PANEL (DRR,ZR,JB)

```

```

8853      SUBROUTINE PLOTR1
8854      IMPLICIT REAL*8(A-H, O-Z)
8855      COMMON/CONTRL/ TIME,NSEG,NJNT,NPL,NBLT,NBAG,NVEH,NGRND,
8856      *          NS,NQ,NSD,NFLX,NHRNSS,NWINDF,NJNTF,NPRT(36)
8857      COMMON/CNTRSRF/ PL(17,100),BELT(20,8),TPTS(6,8),BD(24,110)
8858      COMMON/TITLES/ DATE(3),COMENT(40),VPSTTL(20),BDYTTL(5),
8859      *          BLTTTL(5,8),PLTTL(5,100),BAGTTL(5,6),SEG(100),
8860      *          JOINT(100),CGS(100),JS(100)
8861      REAL DATE,COMENT,VPSTTL,BDYTTL,BLTTTL,PLTTL,BAGTTL,SEG,JOINT
8862      LOGICAL*1 CGS,JS
8863      COMMON /PLOTRES/ ELYPR(3,100), PLPTS(3,3,100), NELSEG(100), LDNPCS
8864      1 , IELPS, IELPB, IELP, NNELP, NPLSEG(100)
8865      REAL*4 PLPTS
8866      REAL*4 SOFT(3,100), BOFT(3,6), BBELT(20,8), BBDD(3,100),
8867      1      ELD(9,100), BL
8868      COMMON /TEMPVS/ DE(9), SOFT, BOFT, BBELT, BBDD, ELD
8869      DIMENSION IDYPR(3)
8870      DATA IDYPR/3,2,1/
8871      C
8872      C-----
8873      C
8874      DATA BL/4H      /
8875      LDNPCS = 9
8876      C
8877      C BELT DATA
8878      C
8879      DO 40 I=1, 8
8880      DO 39 J=1, 6
8881      BBELT(J, I) = BELT(J, I)
8882      39 CONTINUE
8883      40 CONTINUE
8884      C
8885      C AND SIMILARLY FOR SEMI-MAJOR AXES, TO YIELD THE
8886      C PLOTCS ARRAY "BD"
8887      C
8888      IF(NSEG.EQ.O) GOTO 55
8889      DO 52 I=1, NSEG
8890      DO 49 J = 1,3
8891      BBDD(J,I) = BD(J,I)
8892      SOFT(J,I) = BD(J+3,I)
8893      IF (NELSEG(I) .EQ. O) NELSEG(I) = I
8894      49 CONTINUE
8895      CALL DRCYPR(DE,ELYPR(1,I),IDYPR)
8896      DO 50 J=1,9
8897      ELD(J,I) = DE(J)
8898      50 CONTINUE
8899      52 CONTINUE
8900      IF (IELP .LE. O) GO TO 55
8901      II = NSEG
8902      DO 56 I = IELPS, IELPB
8903      IF (BD(1,I) .EQ. O.) GO TO 56
8904      IF (NELSEG(I) .EQ. O) GO TO 56
8905      II = II + 1
8906      NELSEG(II) = NELSEG(I)
8907      DO 53 J = 1,3
8908      BBDD(J,II) = BD(J,I)
8909      SOFT(J,II) = BD(J+3,I)
8910      53 CONTINUE

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```

8911 CALL DRCYPR(DE,ELYPYR(1,I),IDYPR)
8912 DO 54 J=1,9
8913 ELD(J,II) = DE(J)
8914 CONTINUE
8915 54 CONTINUE
8916 56 CONTINUE
8917 C
8918 C FINALLY, BOFT -- THE BAG OFFSETS
8919 C
8920 55 DO 90 I=1, NBAG
8921 II = NVEH + I
8922 DO 89 J=4, 6
8923 BOFT(J-3, I) = BD(J, II)
8924 CONTINUE
8925 89 CONTINUE
8926 90 CONTINUE
8927 C
8928 C RECORD TIME INVARIANT PLOTCS VALUES
8929 C
8930 WRITE (LDNPCS) NSEG,NJNT,NBLT,NBAG,NPL,NNELP,NGRND,
8931 1 DATE, COMENT, VPSTTL, BDYTTL,
8932 2 (SEG(N),N=1,NGRND), (CGS(J),J=1,NSEG)
8933 IF (NNELP .LE. 0) GO TO 9110
8934 WRITE (LDNPCS) ((BBDD(I,J),S0FT(I,J),ELD(I,J),
8935 1 ELD(I+3,J),ELD(I+6,J),I=1,3),NELSEG(J),J=1,NNELP)
8936 9110 IF (NJNT .LE. 0) GO TO 9120
8937 WRITE (LDNPCS) (JOINT(I),I=1,NJNT), (JS(J),J=1,NJNT)
8938 9120 IF (NBLT .LE. 0) GO TO 9130
8939 WRITE (LDNPCS) ((BLTTL(I,J),I=1,3), (BBELT(K,J),
8940 1 K=1,6),J=1,NBLT)
8941 9130 IF (NBAG .LE. 0) GO TO 9140
8942 WRITE (LDNPCS) ((BAGTTL(I,J),I=1,5), (BOFT(K,J),
8943 1 K=1,3),J=1,NBAG)
8944 9140 IF (NPL .LE. 0) GO TO 9150
8945 WRITE (LDNPCS) ((PLTTL(I,J),I=1,5),J=1,NPL)
8946 C
8947 9150 RETURN
8948 END
8949 SUBROUTINE PLOTR2
8950 IMPLICIT REAL*8(A-H, O-Z)
8951 COMMON/CONTRL/ TIME, NSEG, NJNT, NPL, NBLT, NBAG, NVEH, NGRND,
8952 * NS, NQ, NSD, NFLX, NHRNSS, NWINDF, NJNTF, NPRT(36)
8953 COMMON/SGMNTS/ D(3,3,100), WMEGD(3,100), WMEGD(3,100), U1(3,100),
8954 * U2(3,100), SSEGLP(3,100), SEGLV(3,100), SEGLA(3,100), NSYM(100)
8955 COMMON/VPOSTN/ ZPLT(3), SPLT(3), AXV(3,6), VATAB(6,101,6),
8956 * VTO(6), VDT(6), TIMEV(6), OMEGV(6), NVTAB(6), INDXY(6)
8957 COMMON/CNTRS/ PL(17,100), BELT(20,8), TPTS(6,8), BD(24,110)
8958 COMMON/PLOTCS/ ELYPR(3,100), PLPTS(3,3,100), NELSEG(100), LDNPCS
8959 1, IELPS, IELPB, IELP, NNELP, NPLSEG(100)
8960 REAL*4 PLPTS, TYME
8961 REAL*4 TTPTS(6,8), DD(3,3,100), SSEGLP(3,100), BBDD(3,8)
8962 REAL*4 PPLTS(4,3,100)
8963 COMMON /TEMPVS/ TTPTS, DD, SSEGLP, BBDD, PPLTS
8964 C
8965 C-----
8966 TYME = TIME
8967 IF (NBLT .LE. 0) GO TO 25
8968 DO 20 I=1, NBLT
8969 DO 19 J=1, 6

```

```

8969 TPTS(J, I) = TPTS(J, I)
8970 19 CONTINUE
8971 20 CONTINUE
8972 C
8973 DO 30 I=1, NGRND
8974 DO 29 J=1, 3
8975 DO 28 K=1, 3
8976 DD(K, J, I) = D(K, J, I)
8977 28 CONTINUE
8978 SSEGLP(J, I) = SSEGLP(J, I)
8979 29 CONTINUE
8980 30 CONTINUE
8981 C
8982 IF (NBAG .LE. O) GO TO 50
8983 II = O
8984 IBAGA = NVEH + 1
8985 IBAGB = NVEH + NBAG
8986 DO 40 I= IBAGA, IBAGB
8987 DO 39 J=1, 3
8988 II = II + 1
8989 BBDD(J, II) = BD(J+3, I)
8990 39 CONTINUE
8991 40 CONTINUE
8992 C
8993 50 IF (NPL .LE. O) GO TO 85
8994 DO 80 I=1, NPL
8995 DO 70 J=1, 3
8996 PPLTS(4, J, I) = PLPTS(1,J,I)
8997 PPLTS(1, J, I) = PLPTS(3,J,I)
8998 PPLTS(3, J, I) = PLPTS(2,J,I)
8999 PPLTS(2, J, I) = PLPTS(2,J,I) + PLPTS(3,J,I) - PLPTS(1,J,I)
9000 70 CONTINUE
9001 NN = NPLSEG(I)
9002 IF (NN .LE. O) NN = NVEH
9003 IF (NN .GE. NGRND) GO TO 80
9004 DO 75 IJ = 1, 4
9005 CALL PLOTTRA(IJ,PPLTS(1,1,I),NN)
9006 75 CONTINUE
9007 80 CONTINUE
9008 C
9009 C RECORD TIME VARIANT PLOTCS VALUES FOR CURRENT TIME
9010 C
9011 85 WRITE (LDNPCS) TYME,
9012 2 ((SSEGLP(I, J), I=1, 3), J=1, NGRND),
9013 4 (((DD(K, I, J), K=1, 3), I=1, 3), J=1, NGRND)
9014 IF (NPL .LE. O) GO TO 90
9015 WRITE (LDNPCS)((PPLTS(I,J,K), I=1, 4), J=1, 3), K=1, NPL)
9016 IF (NBLT .LE. O) GO TO 100
9017 WRITE (LDNPCS)((TPTS(I, J), I=1, 6), J=1, NBLT)
9018 IF (NBAG .LE. O) GO TO 110
9019 WRITE (LDNPCS)((BBDD(I, J), I=1, 3), J= 1, II)
9020 C
9021 110 RETURN
9022 END
9023 SUBROUTINE PLOTTRA(I, XYZ, N)
9024 IMPLICIT REAL*8(A-H, O-Z)
9025 REAL*4 XYZ
9026 COMMON/SGMNTS/ D(3,3,100),WMEG(3,100),WMEGD(3,100),U1(3,100),

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```

9027      * U2(3,100) . SEGLP(3,100) . SEGLV(3,100) . SEGLA(3,100) . NSYM(100)
9028      DIMENSION XYZ(4,3), X(3), T1(3)
9029      II = I
9030      NN = N
9031      X(1) = XYZ(II,1)
9032      X(2) = XYZ(II,2)
9033      X(3) = XYZ(II,3)
9034      CALL DOT31(D(1,1,NN), X(1), T1(1))
9035      DO 10 J=1, 3
9036          XYZ(II,J) = T1(J) + SEGLP(J,NN)
9037      CONTINUE
9038      RETURN
9039      END
10

```

```

9477      SUBROUTINE QUAT(ANG,Q)
9478      COMPUTES QUATERNIONS FROM YAW, PITCH, ROLL ANGLES IN DEGREES
9479      IMPLICIT REAL *8(A-H,O-Z)
9480      DIMENSION ANG(3),Q(4),R(4),T(3)
9481      COMMON/CNSNTS/PI,RADIAN
9482      A = 0.5*ANG(1)*RADIAN
9483      Q(1) = DCOS(A)
9484      Q(2) = 0.0
9485      Q(3) = 0.0
9486      Q(4) = DSIN(A)
9487      K = 3
9488      DO 10 I = 2,3
9489      A = 0.5*ANG(I)*RADIAN
9490      R(1) = DCOS(A)
9491      R(2) = 0.0
9492      R(3) = 0.0
9493      R(4) = 0.0
9494      R(K) = DSIN(A)
9495      DOT = Q(2)*R(2) + Q(3)*R(3) + Q(4)*R(4)
9496      CALL CROSS(Q(2),R(2),T)
9497      DO 5 J = 2,4
9498      5 Q(J) = Q(1)*R(J) + R(1)*Q(J) + T(J-1)
9499      Q(1) = Q(1)*R(1) - DOT
9500      10 K = 2
9501      SUM = DSQRT(Q(1)**2 + Q(2)**2 + Q(3)**2 + Q(4)**2)
9502      DO 12 I = 1,4
9503      12 Q(I) = Q(I)/SUM
9504      RETURN
9505      END

```



```

11620 SUBROUTINE STASH (ARRAY,NUMWRD,LASNRN)
11621 COMMON /IOCNTL/ LDNRK, KWDPLN, IOTALK
11622 DIMENSION ARRAY(2)
11623 NLIN = (NUMWRD + KWDPLN - 1) / KWDPLN - 1
11624 NLAS = NUMWRD - NLIN * KWDPLN
11625 IF (IOTALK.NE. 0) WRITE(6,9998) NUMWRD, NLIN, NLAS,
11626 1 LASNRN, KWDPLN
11627 9998 FORMAT (BHOSTASH :. 5I10)
11628 IPTB = 0
11629 NRN = LASNRN
11630 IF (NLIN.LE. 0) GO TO 20
11631 DO 10 I = 1, NLIN
11632 IPTA = IPTB + 1
11633 IPTB = IPTB + KWDPLN
11634 NRN = NRN + 1
11635 WRITE(LDNRK'NRN) (ARRAY(J), J=IPTA,IPTB)
11636 IF (IOTALK.GT. 1) WRITE(6,9999) NRN, IPTA, IPTB, (ARRAY(J),
11637 1 J=IPTA,IPTB)
11638 10 CONTINUE
11639 20 IPTA = IPTB + 1
11640 IPTB = IPTB + NLAS
11641 NRN = NRN + 1
11642 WRITE(LDNRK'NRN) (ARRAY(L), L=IPTA,IPTB)
11643 IF (IOTALK.GT. 1) WRITE(6,9999) NRN, IPTA, IPTB, (ARRAY(J),
11644 1 J=IPTA,IPTB)
11645 9999 FORMAT (1H0,3I5/ (5X,6Z20))
11646 LASNRN = NRN
11647 RETURN
11648 END

```

```

1 COMMON /PLOTIT/ NYP(20), MX(3,20), MY(3,10,20), NX(20), XO(20),
2 XN(20), XS(20), YN(20), YO(20), YL(20), YL(20), XL(20),
3 YS(20), YLAB(15,20), NXLAB(20), NYLAB(20), YLAB(15,20),
4 NYPLT, NPLB1(20), PLB1(15,20), NPLSMB(10,20)
5 COMMON /HOLDIT/ BAGTTL(5,6), BDYTTL(5), BLTTL(5,8), COMENT(40),
6 DATE(3), DT, JOINT(100), INCSML, INCBIG, PLTTL(5,100),
7 SEG(100), VPSSTL(20), LLFRST, KASTOP, NRNTIM,
8 TIMLAS, MULTPL, NPL, NPLT, NRNVAR, LFENKT,
9 NBAG, NBLT, LBBAG, LBBELT, LBUNT, LBPL,
10 LBSEG, KKNTRL(241), NSD, NSEG, ISPSWT,
11 NSTEPS, NVEH, NGRND, NHRNSS, NJNT
12 COMMON /PRESET/ ISYMB(49), KASLIN(3,16), LDINARY(3), LPP, NW60
13 . MAXKAP
14 COMMON /FETCH/ D(3,3,12), DPMI(3,3,100), G, LPMI(100), PI,
15 SEG(3,12), SEGLP(3,12), SEGLV(3,12), WMEG(3,12),
16 WMEGD(3,12), UNITL, UNITT, UNITM, RADIAN, TIMMAX,
17 IKASE(12), NKASE, KASKOL, KASPAG, KASFUL
18 COMMON /FETCHU/ POUANT(16), KONTLP(6,3), JDTPTS(18), IPIN(3),
19 KKAS, MSECT, MTIMPT
20 COMMON /HLDCON/ NRNBAS(246), LFIRST(241), KASNUM, KATKOL(12),
21 KPRLM(3), KATKAS(3,12), KASKTL(5,241), MAXPTS,
22 NRN, LSTEP, LASREC(3)
23 COMMON /ZITHNG/ TIME(6000), ZTTH(6000,11), LINEQT(6000)
24 COMMON /IOCNTL/ LDNRWK, KWDPLN, IOTALK
25 COMMON /AVDCON/ RSTF(27), FDPMI(900), XSG(3,50,3), NSG(7),
26 MSG(50,7), MMSG(50,6)
27 DIMENSION IORDER(16), NEEDK(16), NTS(16), KIK(2,7),
28 CONTLP(6,3), KSTF(27), FKASKL(1205),
29 FFIRST(241), FRNBAS(246), FENKAT(51), FLPMI(100)
30 EQUIVALENCE (KSTF(1),RSTF(1)), (FFIRST(1),LFIRST(1)),
31 (FRNBAS(1),NRNBAS(1)), (FENKAT(1),KATKOL(1)),
32 (FKASKL(1),KASKTL(1,1)), (FLPMI(1),LPMI(1)),
33 (CONTLP(1,1),KONTLP(1,1))
34 REAL*4 JOINT
35
36
37 C
38 C
39 C
40 C
41 C
42 C
43 C
44 C
45 C
46 C
47 C
48 C
49 C
50 C
51 C
52 C
53 C
54 C
55 C
56 C
57 C
58 C

```

INITIALIZATION FOR OUT PROCESSOR

DO 10 I = 1, 16
 IORDER(I) = 0
 NEEDK(I) = 0
 NTS(I) = 0
 10 CONTINUE
 DO 12 I = 1, 7
 KIK(1,I) = 0
 KIK(2,I) = 0
 12 CONTINUE
 MSECT = 0
 MTIMPT = 0
 LBBELT = 0
 LBBAG = 0
 LBUNT = 0
 LBSEG = 0
 LBPL = 0
 LLFRST = 0
 IOTALK = 0
 LDNRWK = LDINARY(1)

```

59      C
60      READ (5,15) BEGT, FINT, TINC, IOTALK
61      15 FORMAT (3E8.0, I5)
62      C
63      C      READ TIME INVARIANT INFORMATION FROM HOLD FILE
64      C
65      READ (LDNWRK'1) TIMLAS, LINES, LASREC, MULTPL, INCBIG, INCSML
66      READ (LDNWRK'2) NVEH, NGRND, NSEG, NPL, NJNT, NSD, NBAG, NBLT,
67      1      NHRNSS, MAXPTS, LSTEP, NSTEPS, KASNUM, NRNVAR, LBBELT, LBBAG,
68      2      LBJNT, LBSEG, LBPL, LLFRST
69      READ (LDNWRK'3) DATE, BDYTTL, KASTOP, LFENKT, STPMIN, PI, G,
70      1      RADIAN, UNITL, UNITT, UNITM, DT, TIMMAX, ISPSWT
71      LAST = NRNVAR
72      CALL PICKUP(VPSTTL, 20, LAST)
73      CALL PICKUP(COMENT, 40, LAST)
74      IF (NBLT .LE. 0) GO TO 20
75      LAST = LBBELT
76      CALL PICKUP(BLTITL, 5*NBLT, LAST)
77      20 IF (NBAG .LE. 0) GO TO 30
78      LAST = LBBAG
79      CALL PICKUP(BAGTTL, 5*NBAG, LAST)
80      30 IF (NJNT .LE. 0) GO TO 40
81      LAST = LBJNT
82      CALL PICKUP(JOINT, NJNT, LAST)
83      40 IF (NSEG .LE. 0) GO TO 50
84      LAST = LBSEG
85      CALL PICKUP(SEG, NGRND, LAST)
86      CALL PICKUP(FLPMI, NSEG, LAST)
87      LK = 9 * NSEG
88      CALL PICKUP(DPMI, LK, LAST)
89      C      COMPLETE SEGMENT REPORTING AXIS ORIENTATIONS
90      50 DO 58 I = 1, NGRND
91      IF (I .GT. NSEG) GO TO 52
92      IF (LPMI(I) .NE. 0) GO TO 58
93      52 DO 56 J = 1, 3
94      DO 54 K = 1, 3
95      DPMI(K, J, I) = 0.
96      54 CONTINUE
97      56 CONTINUE
98      DPMI(1, 1, I) = 1.
99      DPMI(2, 2, I) = 1.
100     DPMI(3, 3, I) = 1.
101     LPMI(I) = 0
102     58 CONTINUE
103     IF (NPL .LE. 0) GO TO 60
104     LAST = LBPL
105     CALL PICKUP(PLTTL, 5*NPL, LAST)
106     60 LAST = LLFRST
107     CALL PICKUP(FFIRST, KASNUM, LAST)
108     CALL PICKUP(FRNBAS, KASTOP, LAST)
109     CALL PICKUP(FKASKL, 5*KASNUM, LAST)
110     CALL PICKUP(FENKAT, LFENKT, LAST)
111     C
112     C      READ USER CONTROL DATA FOR THIS RUN OF THE OUT PROCESSOR
113     C
114     KBEG = BEGT / STPMIN + .5
115     KINC = TINC / STPMIN + .5
116     KFIN = FINT / STPMIN + .5

```

125

Listing of SUSP:CUTS(1,584) at 10:06:02 on AUG 29, 1985 for CCID=SS53

```

117 KSTP = DT / STPMIN + .5
118 KSADJ = MAXO(KSTP - 1,0)
119 GET ALL POINTS IF TINC < DT
120 IF (KINC .LT. KSTP) KINC = 0
121 MAKE TINC MULTIPLE OF DT
122 KINC = KSTP * ((KINC + KSADJ)/KSTP)
123 BEGT MUST BE POSITIVE
124 IF (KBEG .LT. 0) KBEG = 0
125 KBEG = KSTP * ((KBEG + KSADJ)/KSTP)
126 IF FINI TOO SMALL, SET FOR END OF ALL POINTS
127 IF (KFIN .LE. 0) KFIN = MULTPL
128 KMINSP = MAXO(KINC,KSTP)
129 IF (KFIN .LE. KBEG) KFIN = KBEG + KMINSP
130 IF (KFIN .GT. MULTPL) KFIN = MULTPL
131 C NOW REDEFINE KFIN TO BE A MULTIPLE OF KMINSP
132 KFIN = KBEG + ((KFIN-KBEG+MAXO(KMINSP-1,0)) / KMINSP) * KMINSP
133 READ (5,90) IORDER
134 90 FORMAT (16I4)
135 KATDO = 0
136 DO 100 I = 1, 16
137 N = IORDER(I)
138 IF (N .EQ. 0) GO TO 102
139 IF (N .LT. 0) GO TO 100
140 IF (N .GT. 16) GO TO 100
141 KATDO = KATDO + 1
142 NEEDK(N) = I
143 100 CONTINUE
144 102 IF (KATDO .GT. 0) GO TO 110
145 DO 104 I = 1, 16
146 IORDER(I) = I
147 NEEDK(I) = I
148 104 CONTINUE
149 KATDO = 16
150 C
151 C READ CASE CONTROLS FOR PRINT CATEGORIES 8 TO 14
152 C THESE ARE ALL CONTACT FORCE RELATED
153 C
154 110 READ (5,120) NTS
155 120 FORMAT (16I4)
156 NKNTL = 0
157 DO 130 I = 1, 16
158 N = NTS(I)
159 IF (N .LE. 0) GO TO 135
160 IF (N .GT. KASNUM) GO TO 130
161 KATG = KASKTL(1,N)
162 IF (NEEDK(KATG) .EQ. 0) GO TO 130
163 IF (NKNTL .GE. 241) GO TO 135
164 NKNTL = NKNTL + 1
165 KKNTL(NKNTL) = N
166 IF (NEEDK(KATG) .GT. 0) NEEDK(KATG) = -NEEDK(KATG)
167 IF (NKNTL .EQ. 241) GO TO 135
168 130 CONTINUE
169 GO TO 110
170 C
171 C WRITE PROLOGUE ON PRIMARY OUTPUT UNIT.
172 C
173 135 WRITE (6,140)
174 WRITE (6,150)

```

Table C.6. Listings of Code Changes to GUCVS (Page 11 to 38)

Listing of SUSP:CUTS(1,584) at 10:06:02 on AUG 29, 1985 for CCid=SS53

```

175 140 FORMAT ('1', 21X, '*****', /, 22X,
176 1* , '*****', /, 22X,
177 2 '*****', /, 22X,
178 3 '*****', /, 22X,
179 150 FORMAT (3(22X, '*****', /), 22X, '*****', 9X,
180 'GGGGGG', 6X, 'UU UU', 6X, 'CCCCCC', 6X, 'VV VV',
181 6X, 'SSSSSS', 5X, '*****', /, 22X, '*****', 9X,
182 'GG G', 6X, 'UU UU', 6X, 'CCCCCC', 6X, 'VV VV',
183 6X, 'SSSSSS', 5X, '*****', /, 22X, '*****', 9X,
184 'GG G', 6X, 'UU UU', 6X, 'CC', 6X, 'VV VV',
185 6X, 'SS', 5X, '*****', /, 22X, '*****', 9X,
186 'GG GGG', 6X, 'UU UU', 6X, 'CC', 6X, 'VV VV',
187 6X, 'SSSSSS', 5X, '*****', /, 22X, '*****', 9X,
188 'GG G', 6X, 'UU UU', 6X, 'CC', 6X, 'VVV',
189 6X, 'SS', 5X, '*****', /, 22X, '*****', 9X,
190 'GG GG', 6X, 'UUUUUU', 6X, 'CCCCCC', 6X, 'VVV',
191 6X, 'SSSSSS', 5X, '*****', /, 22X, '*****', 9X,
192 'GGGG G', 6X, 'UUUUUU', 6X, 'CCCCCC', 6X, 'V',
193 6X, 'SSSSSS', 5X, '*****')
194 WRITE (6,160) DATE, COMENT
195 FORMAT (3(22X, '*****', /), 22X, '*****', 17X,
196 'GMR/UMTRI OUT PROCESSOR', 2X, 3A4, 17X, '*****', /,
197 22X, '*****', 73X, '*****', /, 2(22X,
198 3 '*****', /), //, 1X, 20A4, /, 1X, 20A4)
199 *****
200 BEGT = KBEG * STPMIN
201 TINC = KINC * STPMIN
202 FINT = KFIN * STPMIN
203 IF (TINC .EQ. 0.) GO TO 190
204 WRITE (6,180) BEGT, FINT, TINC
205 FORMAT ('O', 10X, 'PRINT QUANTITIES BEGINNING AT TIME=', F10.3,
206 ' THROUGH TIME =', F10.3, ' AT EVERY INCREMENT OF ',
207 F10.3)
208 GO TO 210
209 WRITE (6,200) BEGT, FINT
210 FORMAT ('O', 10X, 'PRINT QUANTITIES FOR ALL RECORDED TIMES',
211 ' BEGINNING AT TIME=', F10.3, ' THROUGH TIME=', F10.3)
212 WRITE (6,220) (I,I=1,16), (IORDER(J),J=1,16), (NEED(K),K=1,16)
213 FORMAT ('O', 10X, 'CATEGORIES IN ORDER AND ORDER FOR CATEGORIES',
214 ' TO BE PRINTED'/11X, 'POSITION/CATEGORY', 7X,
215 16I5/11X, 'CATEGORY FOR POSITION', 3X, 16I5/11X,
216 ' POSITION FOR CATEGORY', 3X, 16I5)
217 IF (NKNTRL .LE. 0) GO TO 340
218 WRITE (6,230)
219 FORMAT (35X, '(POSITIVE INDICATES ALL CASES FOR CATEGORY',
220 ' PRINTED IN ASSIGNED ORDER;/35X,'NEGATIVE THAT CASES',
221 ' AND ORDER HAVE BEEN SPECIFIED FOR CATEGORY.)/'
222 '1', 42X, 'INDIVIDUALLY SPECIFIED CONTACT CASES'/
223 10X, 'NUMBER', 10X, 'CASE NO.', 10X, 'CATEGORY NO.',
224 10X, 'CASE OF CATG', 7X, 'N', 9X, 'NN', 10X, 'M',
225 9X, 'MM')
226
227 C
228 C SORT SPECIFIED CASES IN PRINT ORDER BY CATEGORIES
229 C KEEPING PRESCRIBED ORDER WITHIN CATEGORIES
230 C
231 NSAM = 0
232 IPNT = 1

```

```

233 JPNT = IPNT + 1
234 IKAS = KKNTRL(IPNT)
235 IKAT = KASKTL(1,IKAS)
236 IORD = IABS(NEEDK(IKAT))
237 JKAS = KKNTRL(JPNT)
238 JKAT = KASKTL(1,JKAS)
239 JORD = IABS(NEEDK(JKAT))
240 IF (IORD - JORD) 300, 270, 260
241 NSAM = 0
242 GO TO 280
243 NSAM = NSAM + 1
244 KOPA = IPNT + NSAM
245 KOPB = JPNT - 1
246 KTOP = KOPA + KOPB
247 IF (KOPA .GT. KOPB) GO TO 300
248 DO 290 JJ = KOPA, KOPB
249 J = KTOP - JJ
250 KKNTRL(J + 1) = KKNTRL(J)
251 CONTINUE
252 KKNTRL(KOPA) = JKAS
253 IF (IORD .EQ. JORD) GO TO 300
254 IKAS = JKAS
255 IKAT = JKAT
256 IORD = JORD
257 NSAM = 0
258 JPNT = JPNT + 1
259 IF (JPNT .LE. NKNTRL) GO TO 250
260 IPNT = IPNT + NSAM + 1
261 NSAM = 0
262 IF (IPNT .LT. NKNTRL) GO TO 240
263
264 C
265 C
266 C
267 KNUM = 0
268 KLAS = 0
269 DO 330 I = 1, NKNTRL
270 II = I
271 IKAS = KKNTRL(I)
272 IKAT = KASKTL(1,IKAS)
273 IORD = IABS(NEEDK(IKAT))
274 IF (IKAT .EQ. KLAS) GO TO 310
275 LKIK = IKAT - 7
276 IF (LKIK .GT. 0 .AND. LKIK .LT. 8) GO TO 306
277 WRITE(6,303) LKIK, II, IKAT, IKAS, IORD
278 FORMAT ('OWARNING---ILLEGAL LKIK=', 5I6)
279 GO TO 330
280 KIK(1, LKIK) = II
281 KLAS = IKAT
282 KNUM = 0
283 KIK(2, LKIK) = II
284 WRITE(6,320) II, IKAS, IKAT, KNUM, (KASKTL(J,IKAS), J=2,5)
285 FORMAT (8X, I6, 11X, I6, 13X, I6, 17X, I6, 7X, I6, 5X, I6,
286 1 5X, I6, 5X, I6)
287 CONTINUE
288 WRITE(6,335)
289 FORMAT(1H0)
290 C

```

Table C.6. Listings of Code Changes to GUCVS (Page 13 to 38)

```

291 C READ PRINTED OUTPUT CONTROLS (H CARDS)
292 C
293 340 DO 370 K = 1, 3
294 IF (NEEDK(K) .EQ. 0) GO TO 370
295 READ (5,350,ERR=430,END=450) KSG, MMSG(1,K), MSG(1,K),
296 1 (XSG(I,1,K),I=1,3)
297 350 FORMAT (I6, 2I3, 3F12.6)
298 WRITE(6,353) K, KSG
299 353 FORMAT('OCATEGORY', I3, ' CONTROLS:', I5, ' CASES')
300 IF (KSG .GT. 50) GO TO 410
301 NSG(K) = KSG
302 IF (KSG-1) 352, 363, 355
303 352 NEEDK(K) = 0
304 GO TO 370
305 355 READ (5,360,ERR=430,END=450) (MMSG(J,K),MSG(J,K),(XSG(I,J,K),
306 1 I=1,3),J=2,KSG)
307 360 FORMAT (6X, 2I3, 3F12.6)
308 363 WRITE(6,365) (J,MMSG(J,K),MSG(J,K),(XSG(I,J,K),I=1,3),J=1,KSG)
309 365 FORMAT (26X, 3I5, 3G20.10)
310 370 CONTINUE
311 DO 400 K = 4, 6
312 IF (NEEDK(K) .EQ. 0) GO TO 400
313 READ (5,380,ERR=430,END=450) KSG, (MMSG(J,K),MSG(J,K),J=1,11)
314 380 FORMAT (I6, 22I3)
315 WRITE(6,353) K, KSG
316 IF (KSG .GT. 50) GO TO 410
317 NSG(K) = KSG
318 IF (KSG .GT. 0) GO TO 385
319 NEEDK(K) = 0
320 GO TO 400
321 385 IF (KSG .LT. 12) GO TO 393
322 READ (5,390,ERR=430,END=450) (MMSG(J,K),MSG(J,K),J=12,KSG)
323 390 FORMAT (6X, 22I3)
324 393 WRITE(6,395) (J, MMSG(J,K), MSG(J,K), J = 1, KSG)
325 395 FORMAT (26X, 3I5)
326 400 CONTINUE
327 IF (NEEDK(7) .EQ. 0) GO TO 480
328 READ (5,402,ERR=430,END=450) KSG, (MSG(J,7), J=1, 11)
329 402 FORMAT (12I6)
330 K = 7
331 WRITE (6,353) K, KSG
332 IF (KSG .GT. 50) GO TO 410
333 NSG(7) = KSG
334 IF (KSG .GT. 0) GO TO 404
335 NEEDK(7) = 0
336 GO TO 480
337 404 IF (KSG .LT. 12) GO TO 408
338 READ (5,406,ERR=430,END=450) (MSG(J,7),J=12, KSG)
339 406 FORMAT (6X, 11I6)
340 408 WRITE (6,409) (J, MSG(J,7), J=1, KSG)
341 409 FORMAT (26X, I5, 5X, I5)
342 GO TO 480
343 410 WRITE (6,420)
344 420 FORMAT ('OFATAL ERROR---MORE THAN 50 PRINT REQUESTS SPECIFIED.')
345 GO TO 470
346 430 WRITE (6,440) K, J
347 440 FORMAT ('OFATAL ERROR---READ ERROR FOR K, J=', 2I6)
348 GO TO 470

```

```

349      450  WRITE (6,460) K, J
350      460  FORMAT ('OFATAL ERROR---EOF FOR K, J=', 2I6)
351      470  CALL ERROR
352      C
353      C      READ INPUT CARD H.8.A TO CONTROL COMPUTATION OF HIC, HSI & CSI.
354      C
355      480  IF (NEEDK(15) .EQ. 0) GO TO 510
356      READ (5,520) JDTPPTS
357      WRITE (6,490) JDTPPTS
358      490  FORMAT ('OCATEGORY 15 CONTROLS:', 9(2I4, 2X))
359      NDPT = 0
360      DO 500 KDT = 1, 18
361      500  IF (JDTPPTS(KDT) .NE. 0) NDPT = NDPT + 1
362      IF (NDPT .EQ. 0) NEEDK(15) = 0
363      C
364      C      READ INDICES OF VARIABLES TO BE PLOTTED AND
365      C      ARGUMENTS TO SUBROUTINE SLPLOT ON CARDS I.
366      C
367      C      INPUT CARD I.1
368      C
369      510  IF (NEEDK(16) .EQ. 0) GO TO 560
370      READ (5,520) NPLT, (NYP(K),K=1,NPLT)
371      520  FORMAT (18I4)
372      WRITE (6,523) NPLT
373      523  FORMAT ('OCATEGORY 16 CONTROLS:', I5, ' CASES')
374      IF (NPLT .GT. 0) GO TO 525
375      NEEDK(16) = 0
376      GO TO 560
377      525  DO 550 K = 1, NPLT
378      NYPLT = NYP(K)
379      WRITE(6,528) K, NYPLT
380      528  FORMAT(10X, 'FOR PLOT NO.', I3, ', NO. OF CURVES = ', I3)
381      C
382      C      INPUT CARD I.2.K
383      C
384      READ (5,529) MX(1,K), MX(2,K), MX(3,K), (MY(1,J,K),MY(2,J,K),
385      1  MY(3,J,K), NPLSMB(J,K), J = 1, NYPLT)
386      529  FORMAT (19I3/ (9X, 16I3))
387      WRITE (6,529) MX(1,K), MX(2,K), MX(3,K), (MY(1,J,K),MY(2,J,K),
388      1  MY(3,J,K), NPLSMB(J,K), J = 1, NYPLT)
389      C
390      C      INPUT CARD I.3.K
391      C
392      READ (5,530) NX(K), XO(K), XN(K), XL(K), XS(K)
393      530  FORMAT (I4, 4X, 4F8.0)
394      C
395      C      INPUT CARD I.4.K
396      C
397      READ (5,530) NY(K), YO(K), YN(K), YL(K), YS(K)
398      C
399      C      INPUT CARD I.5.K
400      C
401      READ (5,540) NXLAB(K), (XLAB(I,K),I=1,NW60)
402      540  FORMAT (I4, 4X, 15A4)
403      C
404      C      NOTE - ABOVE FORMAT ASSUMES 4 ALPHANUMERIC CHARACTERS FOR SINGLE
405      C      PRECISION WORDS ON IBM 360 AND 370 COMPUTERS. THE 15A4 TERM IN THE
406      C      FORMAT WILL HAVE TO BE CHANGED ON NON-IBM COMPUTERS TO PRODUCE A

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407 C CONTINUOUS STRING OF 60 CHARACTERS IN CORE MEMORY.
408 C
409 C INPUT CARD I.6.K
410 C
411 C READ (5,540) NYLAB(K), (YLAB(I,K),I=1,NW60)
412 C
413 C INPUT CARD I.7.K
414 C
415 C READ (5,540) NPLB1(K), (PLB1(I,K),I=1,NW60)
416 550 CONTINUE
417 560 IF (LINES .LE. 0) GO TO 740
418 C
419 C READ IN SELECTED TIMES FOR COMMON REFERENCE
420 C
421 C KATG = 1
422 C KASE = 1
423 C KPT = 0
424 C KWANT = KBEG
425 C LASTM = -1
426 C DO 590 I = 1, LINES
427 C CALL INREAD(KATG, KASE, I, RSTF(1))
428 C KMUL = KSTF(3)
429 C IF (KINC .LE. 0) GO TO 580
430 C IF (KMUL - LASTM) 590, 585, 565
431 565 IF (KWANT .GT. KMUL) GO TO 590
432 C IF (KWANT .NE. KMUL) WRITE (6,570) KWANT, KMUL
433 570 FORMAT ('OWARNING---EXPECTED NEXT TIME MISSING=', I6,
434 1 ' REPLACED BY ', I6)
435 580 KPT = KPT + 1
436 C TIME(KPT) = RSTF(1)
437 585 LINEQT(KPT) = KSTF(2)
438 C IF (KWANT .EQ. KFIN) GO TO 600
439 C LASTM = KMUL
440 C KWANT = MINO(KWANT + KINC,KFIN)
441 590 CONTINUE
442 C
443 C PRINT DESIRED CATEGORIES
444 C
445 600 IF (KATDO .LE. 0) GO TO 800
446 C
447 C LOOP OVER DESIRED CATEGORIES
448 C
449 C DO 780 IA = 1, KATDO
450 C GET GENERAL CATEGORY CONTROLS
451 C NKAT = IORDER(IA)
452 C IF (NEEDK(NKAT) .EQ. 0) GO TO 780
453 C ZERO PRINTING CONTROLS FOR THIS CATEGORY TO INITIALIZE.
454 C DO 604 L = 1, 3
455 C DO 602 M = 1, 6
456 C KONTLP(M,L) = 0
457 602 CONTINUE
458 604 CONTINUE
459 C KASKOL = KASLIN(1,NKAT)
460 C KASPAG = KASLIN(2,NKAT)
461 C KASFUL = KASLIN(3,NKAT)
462 C GET RANGE OF CASE DRIVER INDICES FOR CURRENT CATEGORY
463 C IF (NKAT .GT. 7) GO TO 610
464 C KASTAR = 1

```

Listing of SUSP:CUTS(1,584) at 10:06:02 on AUG 29, 1985 for CCID=SS53

```

465 KASTOP = NSG(NKAT)
466 GO TO 660
467 IF (NKAT - 15) 620, 640, 650
468 IF (NEEDK(NKAT) .LT. 0) GO TO 630
469 ITS = NKAT - 2
470 IF (KATKAS(1,ITS) .LE. 0) GO TO 780
471 KASTAR = KATKAS(2,ITS)
472 KASTOP = KATKAS(3,ITS)
473 GO TO 660
474 ITS = NKAT - 7
475 KASTAR = KIK(1, ITS)
476 KASTOP = KIK(2, ITS)
477 GO TO 660
478 KASTAR = 1
479 KASTOP = NDPT
480 GO TO 660
481 KASTAR = 1
482 KASTOP = NPLT
483 IF (KASTAR .GT. KASTOP) GO TO 780
484
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KASTOP = NSG(NKAT)
GO TO 660
IF (NKAT - 15) 620, 640, 650
IF (NEEDK(NKAT) .LT. 0) GO TO 630
ITS = NKAT - 2
IF (KATKAS(1,ITS) .LE. 0) GO TO 780
KASTAR = KATKAS(2,ITS)
KASTOP = KATKAS(3,ITS)
GO TO 660
ITS = NKAT - 7
KASTAR = KIK(1, ITS)
KASTOP = KIK(2, ITS)
GO TO 660
KASTAR = 1
KASTOP = NDPT
GO TO 660
KASTAR = 1
KASTOP = NPLT
IF (KASTAR .GT. KASTOP) GO TO 780

LOOP OVER DESIRED CASES WITHIN CURRENT CATEGORY:
ONE PAGE AT A TIME

SET UP FETCH CONTROLS FOR CURRENT PAGE

DO 770 IB = KASTAR, KASTOP, KASPAG
KETCHA = IB
KETCHB = MINO(IB + KASPAG - 1, KASTOP)
KKAS = 0
DO 730 KKI = KETCHA, KETCHB
KK = KKI
KKAS = KKAS + 1
KONTLP(6, KKAS) = KKI
IF (NKAT .GT. 7) GO TO 680
MG = 0
IF (NKAT .EQ. 7) GO TO 668
MG = MMSG(KK, NKAT)
IF (MG) 662, 666, 668
662 IF (MG .EQ. -2) GO TO 664
MG = NGRND
GO TO 668
664 MG = NVEH
GO TO 668
666 MG = NVEH
IF (NKAT .EQ. 1 .OR. NKAT .EQ. 4) MG = IABS(MSG(KK, NKAT))
668 KONTLP(5, KKAS) = MG
KONTLP(4, KKAS) = MSG(KK, NKAT)
IF (NKAT .GT. 3) GO TO 670
KONTLP(1, KKAS) = XSG(1, KK, NKAT)
KONTLP(2, KKAS) = XSG(2, KK, NKAT)
KONTLP(3, KKAS) = XSG(3, KK, NKAT)
GO TO 725
670 KONTLP(1, KKAS) = 0
KONTLP(2, KKAS) = 0
KONTLP(3, KKAS) = 0
GO TO 725
680 IF (NKAT - 15) 690, 710, 720
690 IF (NEEDK(NKAT) .GT. 0) GO TO 700

```

Table C.6. Listings of Code Changes to GUCVS (Page 17 of 38)

```

523 KK = KKNTRL(KKI)
524 KONTLP(6, KKAS) = KK
525 KONTLP(1, KKAS) = KASKTL(2, KK)
526 KONTLP(2, KKAS) = KASKTL(3, KK)
527 KONTLP(3, KKAS) = KASKTL(4, KK)
528 KONTLP(4, KKAS) = KASKTL(5, KK)
529 KONTLP(5, KKAS) = O
530 GO TO 725
531 CALL HICCSI(KK, KPT)
532 GO TO 725
533 CALL SLPLOT(KK, KPT)
534 IF (IOTALK .EQ. O) GO TO 730
535 WRITE (6,728) NKAT, KETCHA, KK, KKAS, (KONTLP(I, KKAS), I=1,6),
536 1 (CONTLP(J, KKAS), J=1,6)
537 FORMAT ('OKONTLP:', 10I10/ 8X, 6G20.10)
538 CONTINUE
539 IF (KKAS .LE. O) GO TO 770
540 IF (NKAT .GT. 14) GO TO 770
541
542 C SET UP TIME LOOP FOR CURRENT PAGE
543 C
544 C
545 NTIM = O
546 LINPPG = O
547 NTITL = 1
548 NTIM = NTIM + 1
549 DO 745 I = 1, 12
550 IKASE(I) = O
551 CONTINUE
552 NKASE = O
553 KOLBEG = 1 - KASKOL
554 DO 750 II = 1, KKAS
555 KOLBEG = KOLBEG + KASKOL
556 CALL FETCH(NKAT, II, NTIM, KOLBEG)
557 CONTINUE
558 IF (NTITL .NE. O) CALL HEDING(NKAT, NTIM, LINPPG)
559 NTITL = O
560 LINPPG = LINPPG + 1
561 CALL PRTLIN(NKAT)
562 IF (NTIM .GE. KPT) GO TO 770
563 IF (LINPPG .LT. LPP) GO TO 740
564 NTITL = 1
565 GO TO 760
566 CONTINUE
567 CONTINUE
568 C
569 C
570 C INSERT ANY PLOT TERMINATION CODE REQUIRED BY YOUR SYSTEM HERE.
571 C
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Table C.6. Listings of Code Changes to GUCVS (Page 18 of 38)

Listing of SUSP:CUTS(1,584) at 10:06:02 on AUG 29, 1985 for CCid=SS53

Page 11

```
581      1  7,2,14,10,1,10,4,2,8,4,2,8,4,2,8,6,2,12,6,2,12,0,1,0,0,1,0/  
582 DATA LPP, NW60, MAXKAP, KWDPLN / 41, 15, 6000, 20/  
583 DATA LDNARY / 8, 10, 11/  
584 END
```

```

2313 SUBROUTINE POSTPR(PRDT)
2314
2315 C CONTROLS GENERATION OF PRINTED TABULAR TIME HISTORIES
2316 C AND PLOTS BY THE VALUE OF NPRT(4) AS FOLLOWS:
2317
2318 C VALUE OF TIME HISTORIES PLOTS
2319 C NPRT(4)
2320 C
2321 C +4 ** NO
2322 C +3 YES YES
2323 C +2 YES NO
2324 C +1 ** YES
2325 C 0 ** NO
2326 C -1 NO YES
2327 C -2 YES NO
2328 C -3 YES YES
2329 C
2330 C
2331 C
2332 C
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2334 C
2335 C
2336 C
2337 C
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2369 C
2370 C

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REV 20 05/18/80

COMMON/CDINT/JDTPTS(18) , Z(6000,25)
NOTE: THIS OVERWRITES COMMON /CDINT/.

COMMON/CONTRL/ TIME,NSEG,NJNT,NPL,NBLT,NBAG,NVEH,NGRND,
NS,NQ,NSD,NFLX,NHRNSS,NWINDF,NUNTF,NPRT(36)

REAL*8 TIME
COMMON/FORCES/ PSF(7,100),BSF(4,20),SSF(10,20),BAGSF(3,20),
PRJNT(7,100),NPANEL(5),NPSF,NBSF,NSSF,NBGSF

REAL*8 PSF,BSF,SSF,BAGSF,PRJNT

COMMON/TITLES/ DATE(3),COMMENT(40),VPSTTL(20),BDYFTTL(5),
BLTTTL(5,8),PLTTL(5,100),BAGTTL(5,6),SEG(100),
JOINT(100),CGS(100),JS(100)

REAL DATE,COMMENT,VPSTTL,BDYFTTL,BLTTTL,PLTTL,BAGTTL,SEG,JOINT
LOGICAL*1 CGS,JS

COMMON/CNSNTS/ PI,RADIAN,G,THIRD,EPS(24),
UNITL,UNITM,UNITT,GRAVITY(3)

REAL*8 PI,RADIAN,G,THIRD,EPS,UNITL,UNITM,UNITT,GRAVITY

COMMON/JBARTZ/ MNPL(100),MNBTL(8),MNSEG(100),MNBAG(6),
MPL(3,5,100),MBLT(3,5,8),MSEG(3,5,100),MBAG(3,10,6),
NTPL(5,100),NTBLT(5,8),NTSEG(5,100)

COMMON/DAMPER/ APSDM(3,20),APSDN(3,20),ASD(5,20),MSDM(20),MSDN(20)
REAL*8 APSDM,APSDN,ASD

COMMON/HRNESS/ BAR(15,100),BB(100),BBDOT(100),PLOSS(2,100),
XLONG(20),HTIME(2),IBAR(5,100),NL(2,100),
NPTSPB(20),NPTPLY(20),NTHRNS(20),NBLTPH(5)

REAL*8 BAR,BB,BBDOT,PLOSS,XLONG,HTIME

COMMON/RSAVE/XSG(3,20,3),DPMI(3,3,100),LPMI(100),NSG(7),MSG(20,7)
REAL*8 XSG,DPMI,TDATA,UMSEC,PRDT,TEST

NOTE: SUBROUTINES POSTPR & HEDING SHARE THIS COMMON/TEMPS/.

THE FIRST DIMENSION OF XLAB,YLAB,PLB1 AND PLB2 SHOULD BE THE SAME
AS THE VALUE ASSIGNED TO NW60 WHICH IS THE NUMBER OF WORDS THAT
IS NECESSARY TO CONTAIN 60 CONSECUTIVE CHARACTERS DEPENDING ON THE
COMPUTER SYSTEM THIS PROGRAM IS OPERATING ON. THE VALUE OF NW60
SHOULD BE 15 ON IBM 360 AND 370, 10 ON UNIVAC 1108, 6 ON CDC 6600.
THE LAST TERM IN FORMAT 13 BELOW SHOULD BE 15A4(IBM), 10A6(UNIVAC)
OR 6A10(CDC). ALSO, THE FIRST DIMENSION OF PLDATA IN SUBROUTINE
HEDING SHOULD BE 97(IBM), 77(UNIVAC) OR 53(CDC).

COMMON/TEMPS/TDATA(14,300),HEDATA(220),
XO(20),XN(20),XL(20),XS(20),XLAB(15,20),PLB1(15,20),

Table C.6. Listings of Code Changes to GUCVS (Page 20 of 38)

Listing of CVSB(2313,2563) at 10:09:05 on AUG 29, 1985 for CCID=SS53

```

2371 *      YO(20),YN(20),YL(20),YS(20),YLAB(15,20),PLB2(15,20),
2372 *      NYP(20),MX(2,20),MY(2,10,20),NX(20),NY(20),
2373 *      NXLAB(20),NYLAB(20),NPLB1(20),NPLB2(20),
2374 *      USEC(45),ZTTH(14,45,2),
2375 *      COMMON /IPLSMB/NPLSMB(100)
2376 LOGICAL LTABH,LPLT
2377 DATA LPP/45/, NZD1/5000/
2378 DATA NW60/15/
2379 LTABH = .FALSE.
2380 LPLT = .FALSE.
2381 NPRT4 = IABS(NPRT(4))
2382 IF (NPRT4.EQ.1) LPLT = .TRUE.
2383 IF (NPRT4.EQ.3) LPLT = .TRUE.
2384 IF (NPRT4.EQ.2) LTABH = .TRUE.
2385 IF (NPRT4.EQ.3) LTABH = .TRUE.
2386 DO 2 KKK =1,100
2387   NPLSMB(KKK)=0
2388 C
2389 C
2390 C
2391 C
2392 C
2393 C
2394 C
2395 C
2396 C
2397 C
2398 C
2399 C
2400 C
2401 C
2402 C
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2419 C
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2428 C

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      READ INPUT CARD H.8.A TO CONTROL COMPUTATION OF HIC, HSI & CSI.
      READ (5,11) JDTPTS
      WRITE (6,91) JDTPTS
      FORMAT(1X,18I4)
      NDPT = 0
      DO 4 KDT =1,18
      IF (JDTPTS(KDT).NE.O) NDPT = NDPT + 1
      IF (.NOT.LPLOT .AND. .NOT.LTABH .AND. NDPT.EQ.O) GO TO 99
      CALL ELTIME (1,36)
      IF (.NOT.LPLOT) GO TO 20
      INPUT CARD I.1
      READ (5,11) NPLT, (NYP(K),K=1,NPLT)
      WRITE (6,91) NPLT,(NYP(K),K=1,NPLT)
      FORMAT (18I4)
      IF (NPLT.LE.O) LPLT = .FALSE.
      IF (.NOT.LPLOT) GO TO 20
      DO 15 K=1,NPLT
      NYPLT = NYP(K)
      INPUT CARD I.2.K
      READ (5,11) MX(1,K), MX(2,K), (MY(1,J,K), MY(2,J,K),NPLSMB(J),
      1,J=1,NYPLT)
      WRITE (6,11) MX(1,K),MX(2,K), (MY(1,J,K),MY(2,J,K), NPLSMB(J),
      1,J=1,NYPLT)
      INPUT CARD I.3.K
      READ (5,12) NX(K), XO(K), XN(K), XL(K), XS(K)
      FORMAT (14, 4X, 4F8.0)
      INPUT CARD I.4.K
      READ (5,12) NY(K), YO(K), YN(K), YL(K), YS(K)

```

Table C.6. Listings of Code Changes to GUCVS (Page 21 of 38)

Listing of CVSB(2313,2563) at 10:09:05 on AUG 29, 1985 for CCID=SS53

```

2429 C INPUT CARD I.5.K
2430 C
2431 C
2432 C READ (5,13) NXLAB(K), (XLAB(I,K),I=1,NW60)
2433 C FORMAT (14, 4X, 15A4)
2434 C
2435 C NOTE - ABOVE FORMAT ASSUMES 4 ALPHANUMERIC CHARACTERS FOR SINGLE
2436 C PRECISION WORDS ON IBM 360 AND 370 COMPUTERS. THE 15A4 TERM IN THE
2437 C FORMAT WILL HAVE TO BE CHANGED ON NON-IBM COMPUTERS TO PRODUCE A
2438 C CONTINUOUS STRING OF 60 CHARACTERS IN CORE MEMORY.
2439 C
2440 C INPUT CARD I.6.K
2441 C
2442 C READ (5,13) NYLAB(K), (YLAB(I,K),I=1,NW60)
2443 C
2444 C INPUT CARD I.7.K
2445 C
2446 C 15 READ (5,13) NPLB1(K), (PLB1(I,K),I=1,NW60)
2447 C
2448 C READ TIME HISTORY DATA FROM TAPE 8.
2449 C
2450 C 20 NPTS = 0
2451 C LINES = 0
2452 C IF (NPR(4).GT.O) REWIND 8
2453 C READ (8,END=29) NSEG,NJNT,NPL,NBLT,NBAG,NVEH,NGRND,NPANEL,
2454 C * MNPL,MNBLT,MNSEG,MNBAG,MPL,MBLT,MSEG,MBAG
2455 C READ (8,END=29) DATE,COMENT,VPSTTL,BDYTTL,BLTTL,PLTTL,BAGTTL,
2456 C * SEG,JOINT,UNITL,UNITM,UNITT,NSG,MSG,XSG.
2457 C * NHRNSS,NBLTPH,NPTSPB,NSD,MSDM,MSDN
2458 C 21 READ (8,END=29) NT,UMSEC, ((TDATA(I,J),I=1,14),J=1,NT)
2459 C NPTS = NPTS + 1
2460 C Z(NPTS,1) = UMSEC
2461 C IF (NDPT.EQ.O) GO TO 22
2462 C
2463 C STORE DATA FOR HIC, HSI AND CSI.
2464 C
2465 C
2466 C JJ = 1
2467 C DO 61 I=1,18
2468 C IF (JDTPTS(I).EQ.O) GO TO 61
2469 C JJ = JJ + 1
2470 C JD = JDTPTS(I) - 1
2471 C JE = 4*MOD(JD,3) + 4
2472 C JP = JD/3 + 1
2473 C Z(NPTS,JJ) = TDATA(JE,JP)
2474 C 61 CONTINUE
2475 C JHIC= JJ
2476 C 22 IF (.NOT.LPLOT) GO TO 25
2477 C
2478 C STORE DATA FOR PLOTTING
2479 C
2480 C JY = NDPT + 1
2481 C DO 24 K=1,NPLT
2482 C JE = IABS(MX(2,K))
2483 C IF (JE.EQ.O) GO TO 23
2484 C JY = JY + 1
2485 C JP = MX(1,K) - 20
2486 C Z(NPTS,JY) = TDATA(JE,JP)

```

Table C.6. Listings of Code Changes to GUCVS (Page 22 of 38)

```

2487      23  NYPLT = NYP(K)
2488      DO 24 J=1,NYPLT
2489      JY = JY + 1
2490      JP = MY(1,J,K) - 20
2491      JE = IABS(MY(2,J,K))
2492      Z(NPTS,JY) = UMSEC
2493      24  IF (JE.NE.O) Z(NPTS,JY) = TDATA(JE,JP)
2494      25  IF (.NOT.LTABH) GO TO 21
2495      C
2496      C   STORE DATA TO PRINT TABULAR TIME HISTORIES
2497      C
2498      TEST = DMOD(UMSEC,PRDT)
2499      TEST = DMIN1(TEST,DABS(PRDT-TEST))
2500      IF (NPRT(26).EQ.O .AND. TEST.GT.EPS(4)) GO TO 21
2501      LINES = LINES + 1
2502      NTHH = MOD(LINES-1,LPP) + 1
2503      USEC(NTHH) = UMSEC
2504      DO 26 J=1,NT
2505      DO 26 I=1,14
2506      26  ZTHH(I,NTHH,J) = TDATA(I,J)
2507      IF (NTHH.EQ.LPP) CALL HEDING (LINES,LPP)
2508      GO TO 21
2509      29  IF (.NOT.LTABH .OR. LINES.EQ.O) GO TO 30
2510      IF (NTHH.NE.LPP) CALL HEDING (LINES,LPP)
2511      30  IF (NDPT.NE.O) CALL HICCSI(NPTS,JHIC)
2512      IF (.NOT.LPLOT) GO TO 98
2513      C
2514      C   PLOT DATA VIA SUBROUTINE SLPLOT.
2515      C
2516      C
2517      CALL COMPRS
2518      JZ = NDPT+1
2519      DO 50 K=1,NPLT
2520      JX = 1
2521      IF (MX(2,K).EQ.O) GO TO 42
2522      JZ = JZ + 1
2523      JX = JZ
2524      IF (Z(1,JX).EQ.O.O .OR. MX(2,K).GE.O) GO TO 42
2525      DO 41 I=2,NPTS
2526      41  Z(I,JX) = Z(I,JX) - Z(1,JX)
2527      Z(1,JX) = O.O
2528      42  NYPLT = NYP(K)
2529      DO 44 J=1,NYPLT
2530      JY = JZ + J
2531      IF (Z(1,JY).EQ.O.O .OR. MY(2,J,K).GE.O) GO TO 44
2532      DO 43 I=2,NPTS
2533      43  Z(I,JY) = Z(I,JY) - Z(1,JY)
2534      Z(1,JY) = O.O
2535      44  CONTINUE
2536      NXK = NX(K)
2537      NYK = NY(K)
2538      XOK = XO(K)
2539      YOK = YO(K)
2540      XNK = XN(K)
2541      YNK = YN(K)
2542      XLK = XL(K)
2543      YLK = YL(K)
2544      XSK = XS(K)

```


Listing of CVSB(2319,2563) at 10:09:05 on AUG 29, 1985 for CCid=SS53

```

2545 YSK = YS(K)
2546 NXLABK = NXLAB(K)
2547 NYLABK = NYLAB(K)
2548 NPLB1K = NPLB1(K)
2549 NPLB2K = NPLB2(K)
2550 CALL SLPLOT(Z(1,JX ), NXK, XOK, XNK, XLK, XSK, XLAB(1,K), NXLABK,
2551 Z(1,JZ+1), NYK, YOK, YNK, YLK, YSK, YLAB(1,K), NYLABK,
2552 * NPTS,NYPLT,NZD1,PLB1(1,K),NPLB1K,PLB2(1,K),NPLB2K,K)
2553 *
C INSERT ANY CODE REQUIRED BY YOUR SYSTEM TO ADVANCE PLOT PAGES HERE
2554 C
2555 C
2556 50 JZ = JZ + NYPLT
2557 CALL DONEPL
2558 C
2559 C INSERT ANY PLOT TERMINATION CODE REQUIRED BY YOUR SYSTEM HERE.
2560 C
2561 98 CALL ELTIME (2.36)
2562 99 RETURN
2563 END

```

```

631      SUBROUTINE FETCH(KATG, KASPT, NLIN, KOLB)
632      COMMON /HOLDIT/ BAGTTL(5,6), BDYTTL(5), BLTTTL(5,8), COMENT(40),
633      1      DATE(3), DT, JOINT(100), INCSML, INCBIG, PLTTL(5,100),
634      2      SEG(100), VPSTTL(20), LLFRST, KASTOP, NRNTIM,
635      3      TIMLAS, MULTPL, NPL, NPLT, NRNVAR, LFENKT,
636      4      NBAG, NBLT, LBBAG, LBBELT, LBJNT, LBPL,
637      5      LBSEG, KKNTRL(241), NSD, NSEG, ISPSWT,
638      6      NSTEPS, NVEH, NGRND, NHRNSS, NJNT
639      COMMON /PRESET/ ISYMB(49), KASLIN(3,16), LDNARY(3), LPP, NW60
640      1      , MAXKAP
641      COMMON /FETCH/ D(3,3,12), DPMI(3,3,100), G, LPMI(100), PI,
642      1      SEGLA(3,12), SEGLP(3,12), SEGLV(3,12), WMEG(3,12),
643      2      WMEGD(3,12), UNITL, UNITT, UNITM, RADIAN, TIMMAX,
644      3      IKASE(12), NKASE, KASKOL, KASPAG, KASFUL
645      COMMON /IOCNTL/ LDNWRK, KWDPLN, IOTALK
646      COMMON /FETCHU/ PQUANT(16), KONTLP(6,3), JDTPPTS(18), IPIN(3),
647      1      KKAS, MSECPT, MTIMPT
648      COMMON /HLDCON/ NRNBAS(246), LFIRST(241), KASNUM, KATKOL(12),
649      1      KPRELM(3), KATKAS(3,12), KASKTL(5,241), MAXPTS,
650      2      NRN, LSTEP, LASREC(3)
651      COMMON /ZTTHNG/ TIME(6000), ZTTH(6000,11), LINEQT(6000)
652      DIMENSION CONTLP(6,3), V(3,12), FM(3,3,3), ISWT(2), LSWT(2)
653      1      , KQUANT(14)
654      EQUIVALENCE (CONTLP(1,1), KONTLP(1,1)), (KQUANT(1),PQUANT(1))
655      DATA TWOPI/6.283185/
656      LIN = LINEQT(NLIN)
657      KPT = KASPT
658      KAT = KATG
659      KOL = KOLB
660      MSECPT = NLIN
661      MTIMPT = LIN
662      KAS = KONTLP(6, KPT)
663      IF (KAT .LE. 0) GO TO 900
664      IF (KAT - 7) 5, 700, 800
665      5      ITO = KONTLP(5, KPT)
666      ISWT(2) = ITO
667      IFRM = IABS(KONTLP(4, KPT))
668      ISWT(1) = IFRM
669      DO 90 J = 1, 2
670      II = J
671      LSWT(II) = 0
672      DO 10 I = 1, 12
673      IF (IKASE(I) .LE. 0) GO TO 20
674      IF (IKASE(I) .NE. ISWT(II)) GO TO 10
675      LSWT(II) = I
676      GO TO 90
677      10      CONTINUE
678      20      JJ = NKASE + 1
679      IF (NKASE .LT. 12) GO TO 40
680      DO 30 I = 1, 12
681      IF (IKASE(I) .EQ. NVEH) GO TO 30
682      IF (IKASE(I) .EQ. NGRND) GO TO 30
683      JJ = I
684      GO TO 40
685      30      CONTINUE
686      WRITE(6,9999) IKASE, NKASE, ISWT, LSWT, LIN, KPT, KAT, KOL
687      9999  FORMAT('OFATAL ERROR---FETCH CURRENT CASE SPACE ',
688      1      ' FILLED WITH VECH/GRND.'/ (5X, 12I10))

```

```

689      STOP 99
690      40  IF (NKASE .LT. 12) NKASE = JJ
691          IKASE(JJ) = ISWT(II)
692          LSWT(II) = JJ
693      C  RECORDING CATEGORY 2
694          CALL INREAD(2, ISWT(J), LIN, ZTTH(1,1))
695          DO 60 M = 1, 3
696              SEGLP(M, JJ) = ZTTH(M,1)
697              SEGLV(M, JJ) = ZTTH(M+3,1)
698              SEGLA(M, JJ) = ZTTH(M+6,1)
699      60  CONTINUE
700      C  RECORDING CATEGORY 3
701          CALL INREAD(3, ISWT(J), LIN, ZTTH(1,1))
702          DO 70 M = 1, 3
703              WMEG(M, JJ) = ZTTH(M,1)
704              WMEGD(M, JJ) = ZTTH(M+3,1)
705      70  CONTINUE
706      C  RECORDING CATEGORY 4
707          CALL INREAD(4, ISWT(J), LIN, D(1,1,JJ))
708      90  CONTINUE
709          JFRM = LSWT(1)
710          JTO  = LSWT(2)
711          IF (IOTALK .EQ. 0) GO TO 95
712          WRITE(6,93) KAT, KPT, LIN, NLIN, KOL, ISWT, LSWT
713      93  FORMAT ('OFETCH:', 11I10)
714      95  IF (KAT .LT. 4) CALL MAT31(DPMI(1,1,IFRM), CONTLP(1,KPT), V(1,12))
715          GO TO (100, 200, 300, 400, 500, 600), KAT
716      C
717      C  LINEAR ACCELERATION OF POINTS ATTACHED TO SEGMENTS
718      C
719      100 CALL CROSS(WMEG(1,JFRM), V(1,12), V(1,1))
720          CALL CROSS(WMEG(1,JFRM), V(1,1), V(1,2))
721          CALL CROSS(WMEGD(1,JFRM), V(1,12), V(1,3))
722          CALL VECADD(V(1,2), V(1,3), V(1,4))
723          CALL DOT31(D(1,1,JFRM), V(1,4), V(1,5))
724          CALL VECADD(V(1,5), SEGLA(1,JFRM), V(1,6))
725          IF (KONTLP(4,KPT) .GT. 0) GO TO 110
726          CALL DOT31(D(1,1,JFRM), V(1,12), V(1,11))
727          CALL VECADD(SEGLP(1,JFRM), V(1,11), V(1,10))
728          CALL VECSUB(V(1,10), SEGLP(1,JTO), V(1,9))
729          CALL MAT31(D(1,1,JTO), V(1,9), V(1,2))
730          CALL DOT31(D(1,1,JFRM), V(1,1), V(1,3))
731          CALL VECADD(V(1,3), SEGLV(1,JFRM), V(1,4))
732          CALL VECSUB(V(1,4), SEGLV(1,JTO), V(1,5))
733          CALL CROSS(WMEG(1,JTO), V(1,2), V(1,3))
734          CALL VECSUB(V(1,5), V(1,3), V(1,1))
735          CALL VECSUB(V(1,6), SEGLA(1,JTO), V(1,7))
736          CALL MAT31(D(1,1,JTO), V(1,7), V(1,8))
737          CALL CROSS(WMEG(1,JTO), V(1,1), V(1,3))
738          CALL SCALED(V(1,3), .5, V(1,1))
739          CALL VECSUB(V(1,8), V(1,1), V(1,6))
740          CALL CROSS(WMEG(1,JTO), V(1,2), V(1,3))
741          CALL CROSS(WMEG(1,JTO), V(1,3), V(1,4))
742          CALL CROSS(WMEGD(1,JTO), V(1,2), V(1,1))
743          CALL VECADD(V(1,1), V(1,4), V(1,5))
744          CALL VECSUB(V(1,6), V(1,5), V(1,7))
745          GO TO 120
746      110 CALL MAT31(D(1,1,JTO), V(1,6), V(1,7))

```

```

747 120 CALL DOT31(DPMI(1,1,ITO), V(1,7), V(1,8))
748 CALL SCALED(V(1,8), G, PQUANT(KOL))
749 GO TO 550
750
751 C
752 C
753 C
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804 C

      LINEAR VELOCITIES OF POINTS ATTACHED TO SEGMENTS
CALL CROSS(WMEG(1,JFRM), V(1,12), V(1,11))
CALL DOT31(D(1,1,JFRM), V(1,1), V(1,2))
CALL VECADD(V(1,2), SEGLV(1,JFRM), V(1,3))
CALL VECSUB(V(1,3), SEGLV(1,JTO), V(1,4))
CALL MAT31(D(1,1,JTO), V(1,4), V(1,5))
LL = 5
IF (KONTLP(4,KPT) .GT. 0) GO TO 210
CALL DOT31(D(1,1,JFRM), V(1,12), V(1,11))
CALL VECADD(V(1,11), SEGLP(1,JFRM), V(1,10))
CALL VECSUB(V(1,10), SEGLP(1,JTO), V(1,9))
CALL MAT31(D(1,1,JTO), V(1,9), V(1,8))
CALL CROSS(WMEG(1,JTO), V(1,8), V(1,7))
CALL VECSUB(V(1,7), V(1,6))
LL = 6
CALL DOT31(DPMI(1,1,ITO), V(1,LL), PQUANT(KOL))
GO TO 550

      LINEAR DISPLACEMENTS OF POINTS ATTACHED TO SEGMENTS
CALL DOT31(D(1,1,JFRM), V(1,12), V(1,11))
CALL VECADD(V(1,1), SEGLP(1,JFRM), V(1,2))
CALL VECSUB(V(1,2), SEGLP(1,JTO), V(1,3))
IF (KONTLP(4,KPT) .GT. 0) GO TO 310
CALL MAT31(D(1,1,JFRM), V(1,3), V(1,4))
CALL SCALED(V(1,4), -1., PQUANT(KOL))
GO TO 550
CALL MAT31(D(1,1,JTO), V(1,3), PQUANT(KOL))
GO TO 550

      ANGULAR ACCELERATIONS OF SEGMENTS
CALL DOT31(D(1,1,JFRM), WMEGD(1,JFRM), V(1,2))
CALL MAT31(D(1,1,JTO), V(1,2), V(1,3))
CALL VECSUB(V(1,3), WMEGD(1,JTO), V(1,4))
CALL DOT31(DPMI(1,1,ITO), V(1,4), V(1,5))
CALL SCALED(V(1,5), TWOPI, PQUANT(KOL))
GO TO 550

      ANGULAR VELOCITIES OF SEGMENTS
CALL DOT31(D(1,1,JFRM), WMEG(1,JFRM), V(1,1))
CALL MAT31(D(1,1,JTO), V(1,1), V(1,2))
CALL VECSUB(V(1,2), WMEG(1,JTO), V(1,3))
CALL SCALED(V(1,3), TWOPI, V(1,4))
CALL DOT31(DPMI(1,1,ITO), V(1,4), PQUANT(KOL))
PQUANT(KOL+3) = SQRT(PQUANT(KOL)**2 + PQUANT(KOL+1)**2 +
1 PQUANT(KOL+2)**2)
GO TO 900

      EULER ANGLE ORIENTATION OF SEGMENTS
CALL DOT33(DPMI(1,1,IFRM), D(1,1,JFRM), FM(1,1,1))

```

Listing of SUSP:CUTS(631,834) at 10:06:51 on AUG 29, 1985 for CCId=SS53

```

805 CALL DOTT33(FM(1,1,1),D(1,1,JTO),FM(1,1,2))
806 CALL MAT33(FM(1,1,2),DPMI(1,1,ITO),FM(1,1,3))
807 CALL YPRDEG(FM(1,1,3), PQUNT(KOL))
808 TRACE = .5*(FM(1,1,3) + FM(2,2,3) + FM(3,3,3) - 1.0)
809 IF (TRACE .GT. 1.0) TRACE = 1.0
810 IF (TRACE .LT. -1.0) TRACE = -1.0
811 PQUNT(KOL+3) = ARCOS(TRACE) / RADIAN
812 GO TO 900
813
814 C      JOINT PARAMETERS
815 C
816 C      700
817 CALL INREAD(5, KAS, LIN, PQUNT(KOL))
818 PQUNT(KOL+1) = PQUNT(KOL+1) / RADIAN
819 PQUNT(KOL+2) = PQUNT(KOL+2) / RADIAN
820 PQUNT(KOL+3) = PQUNT(KOL+3) / RADIAN
821 PQUNT(KOL+4) = SQRT(PQUNT(KOL+4))
822 PQUNT(KOL+5) = SQRT(PQUNT(KOL+5))
823 PQUNT(KOL+6) = SQRT(PQUNT(KOL+6))
824 IPIN(JJ) = KQUANT(KOL+7)
825 GO TO 900
826
827 C      ALL OTHER FORCE PRODUCERS
828 C
829 C      800 CALL INREAD(KAT,KAS,LIN,PQUNT(KOL))
830 C      900 IF (IOTALK .EQ. 0) GO TO 1000
831 KOLZ = KOL + KASKOL - 1
832 WRITE(6,910) (PQUNT(I), I=1, KOLZ)
833 FORMAT(7X, 6G20.10)
834 1000 RETURN
      END

```

Table C.6. Listings of Code Changes to GUCVS (Page 28 of 38)

```
1123      SUBROUTINE HICCSI(KASE, NUMTIM)
1124      DATA NUM /0/
1125      C          DUMMY HICCSI SUBPROGRAM
1126      C*****
1127      C          ORIGINAL ROUTINE FOUND IN FILE "CVSHICCSI".
1128      C          THIS ROUTINE NEEDS MODIFICATION BEFORE IT CAN BE USED.
1129      C*****
1130      NUM = NUM + 1
1131      WRITE (6,9999) NUM, KASE, NUMTIM
1132      9999 FORMAT ('OHICCSI CALL NO. ', I5, '; ARGS=', 2I10)
1133      RETURN
1134      END
```

```

62      SUBROUTINE HICCSI(NPTS,JJ)
63
64      C
65      C
66      C
67      C
68      C
69      C
70      C
71      C
72      C
73      C
74      C
75      C
76      COMMON/CDINT/ JDTPTS(18),Z(6000.25)
77      DIMENSION AREA(6000)
78      IF (NPTS.LT.25) GO TO 25
79      WRITE (6,14)
80      FORMAT (1H1, ' HIC, HSI AND CSI RESULTS')
81      JCCC= 0
82      JSET= JJ/2
83      DO 30 IND = 1,JJ,2
84      JH= IND+1
85      JC= IND+2
86      JH1= JH-1
87      JC1= JC-1
88      JCCC=JCCC+1
89      IF (JDTPTS(JH1).EQ.O) JC = JC-1
90      CSI = O.O
91      HSI = O.O
92      HIC = O.O
93      CMX = Z(1,JC)
94      HMX = Z(1,JH)
95      IF (JDTPTS(JC1).EQ.O) GO TO 16
96      C
97      C
98      C
99      H1 = SQRT(Z(1,JC)) * Z(1,JC)**2
100     DO 15 I=2,NPTS
101     H2 = SQRT(Z(I,JC)) * Z(I,JC)**2
102     DT = Z(I,1) - Z(I-1,1)
103     CSI = CSI + O.5*DT*(H1+H2)
104     IF (CMX.GT.Z(I,JC)) GO TO 15
105     CMX = Z(I,JC)
106     CMT = Z(I,1)
107     H1 = H2
108     CSI = O.OO1*CSI
109     GO TO 23
110     IF (JDTPTS(JH1).EQ.O) GO TO 23
111     C
112     C
113     C
114     C
115     C
116     C
117     C
118     C
119     C
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120 IF (HMX.GT.Z(I,JH)) GO TO 17
121 HMX = Z(I,JH)
122 HMT = Z(I,1)
123 H1 = H2
124 HSI = O.OO1*HSI
125
126 C
127 C
128 C
129 C
130 C
131 C
132 C
133 C
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      COMPUTE HIC - HEAD INJURY CRITERION - AND TIME DURATION HT1,HT2

DO 19 K=2,NPTS
DO 18 L=K,NPTS
DT = Z(L,1) - Z(K-1,1)
DH = AREA(L) - AREA(K-1)
HT = DH/DT
HM = DT*SQRT(HT)*HT**2
IF (HM.LE.HIC) GO TO 18
HIC = HM
HT1 = Z(K-1,1)
HT2 = Z(L,1)
HA2 = Z(L,JH)
HA1 = Z(K-1,JH)
AVE = HT
18 CONTINUE
19 CONTINUE
HIC = O.OO1*HIC
WRITE (6,31) JDOCC
31 FORMAT(1H0,'***** OCCUPANT NO. ',I4,'/1X,
1 /,'
2 *****')
WRITE (6,21) HIC,HT1,HT2,HA1,HA2,AVE
21 FORMAT (1H0,' HEAD INJURY CRITERION'//
* HIC = ', F8.2,
* 9X,' TIME DURATION = ', F9.3, ' TO ', F9.3, ' MSEC'//
* 20X,' WITH HEAD RESULTANTS = ', F9.3, ' AND ', F9.3, ' G'S'//
* 14X,' AVERAGE HEAD RESULTANT FOR TIME DURATION = ', F9.3, ' G'S'//
WRITE (6,22) HSI,HMX,HMT
22 FORMAT (1H0,' HEAD SEVERITY INDEX'//
* HSI = ', F8.2//
* ' MAX HEAD RESULTANT = ', F9.3, ' G'S AT ', F9.3, ' MSEC')
23 IF (JDTPTS(JC1).EQ.O) GO TO 30
WRITE (6,24) CSI,CMX,CMT
24 FORMAT (1H0,' CHEST SEVERITY INDEX'//
* CSI = ', F8.2//
* ' MAX CHEST RESULTANT = ', F9.3, ' G'S AT ', F9.3, ' MSEC')
30 CONTINUE
25 RETURN
END

```


Listing of SUSP:CUTS(1135,1189) at 10:07:36 on AUG 29, 1985 for CC1d=SS53

```

1135 SUBROUTINE INREAD(KAT, KAS, LIN, ARRAY)
1136 DIMENSION ARRAY(2)
1137 COMMON /PRESET/ ISYMB(49), KASLIN(3,16), LDNARY(3), LPP, NW60
1138 1 MAXKAP
1139 COMMON /HLDCON/ NRNBAS(246), LFIRST(241), KASNUM, KATKOL(12),
1140 1 KPRLM(3), KATKAS(3,12), KASKTL(5,241), MAXPTS,
1141 2 NRN, LSTEP, LASREC(3)
1142
1143 C
1144 C
1145 C
1146 C
1147 C
1148 C
1149 C
1150 C
1151 C
1152 C
1153 C
1154 C
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NOTE: THERE EXISTS A DUAL ROLE FOR CATEGORIES IN INREAD.
CATEGORIES 1-5 ARE RECORDING CATEGORIES,
CATEGORIES 8-14 ARE PRINTING CATEGORIES, AND
ALL OTHER CATEGORY NUMBERS ARE SKIPPED.

```

1. FOR KATG = 1 TO 5:
   KASE = 1 TO KATKAS(1,KATG)
   ONLY NRNBAS(KATG) APPLIES
2. FOR KATG = 8 TO 14:
   KASE = KATKAS(2,KATG-2) TO KATKAS(3,KATG-2)
   NRNBAS(KASE+5) AND LFIRST(KASE) APPLY
3. KASADJ = NRNBAS INDEX FOR ALL CATEGORIES AND CASES

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KATG = KAT
IF (KATG .LT. 1) GO TO 60
IF (KATG .GT. 14) GO TO 60
KASE = KAS
LINES = LIN
IF (KATG .GT. 7) GO TO 10
IF (KATG .GT. 5) GO TO 60
LINOFF = 0
KASADJ = KATG
LADJUST = KASE * LSTEP - LSTEP
KATABL = KATG
GO TO 20
10 LINOFF = LFIRST(KASE)
KASADJ = KASE + 5
LADJUST = 0
KATABL = KATG - 2
LEN = KATKOL(KATABL)
IF (LINOFF .LT. 0) GO TO 30
IF (LINOFF .LT. LINES) GO TO 50
DO 40 I=1, LEN
  ARRAY(I) = 0.
40 CONTINUE
GO TO 60
50 LINREL = LINES - LINOFF
LMOD = MOD(LINREL,3)
IF (LMOD .EQ. 0) LMOD = 3
LDN = LDNARY(LMOD)
LBASE = NRNBAS(KASADJ) + KPRLM(LMOD) + LADJUST
LINREC = (LINREL + 2) / 3
NRN = LBASE + LINREC
READ (LDN'NRN) (ARRAY(I),I=1,LEN)
LASREC(LMOD) = MAXO(LASREC(LMOD), NRN)
60 RETURN
END

```

```

1212 SUBROUTINE PICKUP(ARRAY,NUMWRD,LASNRN)
1213 COMMON /IOCNTL/ LDNRWK, KWDPLN, IOTALK
1214 DIMENSION ARRAY(2)
1215 NLIN = (NUMWRD + KWDPLN - 1) / KWDPLN - 1
1216 NLAS = NUMWRD - NLIN * KWDPLN
1217 IF (IOTALK.NE.0) WRITE(6,9998) NUMWRD, NLIN, NLAS.
1218 1 LASNRN, KWDPLN
1219 9998 FORMAT (8HOPICKUP:, 5I10)
1220 IPTB = 0
1221 NRN = LASNRN
1222 IF (NLIN.LE.0) GO TO 20
1223 DO 10 I = 1, NLIN
1224 IPTA = IPTB + 1
1225 IPTB = IPTB + KWDPLN
1226 NRN = NRN + 1
1227 READ(LDNRWK,NRN) (ARRAY(J), J=IPTA,IPTB)
1228 IF (IOTALK.GT.1) WRITE(6,9999) NRN, IPTA, IPTB, (ARRAY(J),
1229 1 J=IPTA,IPTB)
1230 10 CONTINUE
1231 20 IPTA = IPTB + 1
1232 IPTB = IPTB + NLAS
1233 NRN = NRN + 1
1234 READ(LDNRWK,NRN) (ARRAY(L), L=IPTA,IPTB)
1235 IF (IOTALK.GT.1) WRITE(6,9999) NRN, IPTA, IPTB, (ARRAY(J),
1236 1 J=IPTA,IPTB)
1237 9999 FORMAT (1H0,3I5/ (5X,6Z20))
1238 LASNRN = NRN
1239 RETURN
1240 END
1241 SUBROUTINE PRTLIN(NKAT)
1242 COMMON /HOLDIT/ BAGTTL(5,6), BDYTTL(5), BLTTTL(5,8), COMENT(40),
1243 1 DATE(3), DT, JOINT(100), INCSML, INCBIG, PLTTL(5,100),
1244 2 SEG(100), VPSTTL(20), LLFRST, KASTOP, NRNTIM,
1245 3 TIMLAS, MULTPL, NPL, NPLI, NRNVAR, LFENKT,
1246 4 NBAG, NBLT, LBBAG, LBBELT, LBJNT, LBPL,
1247 5 LBSEG, KKNTL(241), NSD, NSEG, ISPSWT,
1248 6 NSTEPS, NVEH, NGRND, NHRNSS, NJNT
1249 COMMON /PRESET/ ISYMB(49), KASLIN(3,16), LDNARY(3), LPP, NW60
1250 1 COMMON , MAXKAP
1251 COMMON /FETCH/ D(3,3,12), DPMI(3,3,100), G, LPMI(100), PI,
1252 1 SEGLA(3,12), SEGLP(3,12), SEGLV(3,12), WMEG(3,12),
1253 2 WMEGD(3,12), UNITL, UNITI, UNITM, RADIAN, TIMMAX,
1254 3 IKASE(12), NKASE, KASKOL, KASPAG, KASFUL
1255 COMMON /HLDCON/ NRNBAS(246), LFIRST(241), KASNUM, KATKOL(12),
1256 1 KPREL(3), KATKAS(3,12), KASKTL(5,241), MAXPTS,
1257 2 NRN, LSTEP, LASREC(3)
1258 COMMON /FETCHU/ PQUANT(16), KONTLP(6,3), JDTPTS(18), IPIN(3),
1259 1 KKAS, MSECPT, MTIMPT
1260 COMMON /ZTTHNG/ TIME(6000), ZTTH(6000,11), LINEQT(6000)
1261 KAT = NKAT
1262 JJ = KKAS * KASKOL
1263 NT = 6
1264 IF (KAT.GT.7) GO TO 50
1265 IF (KAT.EQ.7) GO TO 30
1266 WRITE (NT,20) TIME(MSECPT), (PQUANT(J),J=1,JJ)
1267 20 FORMAT (F9.3, 3(3X,4F9.3))
1268 GO TO 190
1269 30 WRITE (NT,40) TIME(MSECPT), (PQUANT(J),J=1,JJ)

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1270      40 FORMAT (F9.3, 2(F5.0,3F9.3,2X,3F9.3))
1271      GO TO 190
1272      50 NGO = KAT - 7
1273      IF (NGO .LT. 1 .OR. NGO .GT. 7) GO TO 190
1274      GO TO (60, 130, 80, 100, 110, 150, 170), NGO
1275      60 WRITE (NT,70) TIME(MSECPT), (PQUANT(J),J=1,JJ)
1276      70 FORMAT (F9.3, 2(F9.3,3F9.2,3F8.3))
1277      GO TO 190
1278      80 WRITE (NT,90) TIME(MSECPT), (PQUANT(J),J=1,JJ)
1279      90 FORMAT (F9.3, 4(F15.6,F12.2,3X))
1280      GO TO 190
1281      100 WRITE (NT,90) TIME(MSECPT), (PQUANT(J),J=1,JJ)
1282      GO TO 190
1283      110 JJ = 2
1284      IF (KONTLP(3,1) .NE. 0) JJ = 4
1285      IF (KONTLP(1,2) .NE. 0) JJ = 6
1286      IF (KONTLP(3,2) .NE. 0) JJ = 8
1287      WRITE (NT,120) TIME(MSECPT), (PQUANT(J),J=1,JJ)
1288      120 FORMAT (F9.3, 4(F14.3,F12.2,4X))
1289      GO TO 190
1290      130 WRITE (NT,140) TIME(MSECPT), (PQUANT(J),J=1,10)
1291      140 FORMAT (2F9.3, 3F9.2, 3F8.3, 2X, 3F8.3)
1292      GO TO 190
1293      150 WRITE (NT,160) TIME(MSECPT), (PQUANT(J),J=1,12)
1294      160 FORMAT (F9.3, 3X, 3F9.2, 2(3X,3F9.3), 3X, 3F9.2)
1295      GO TO 190
1296      170 WRITE (NT,180) TIME(MSECPT), (PQUANT(J),J=1,JJ)
1297      180 FORMAT (F9.3, 4(3X,3F9.2))
1298      190 RETURN
1299      END
1300      SUBROUTINE SCALED(VA,D,VB)
1301      DIMENSION VA(3),VB(3)
1302      DO 10 I = 1, 3
1303      VB(I) = VA(I) / D
1304      10 CONTINUE
1305      RETURN
1306      END

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149

```
1307 SUBROUTINE SLPLOT(KASE, NUMTIM)
1308 DATA NUM /O/
1309 C DUMMY SLPLOT SUBPROGRAM
1310 C*****
1311 C ORIGINAL ROUTINE FOUND IN FILE "CVSSLPLOT".
1312 C THIS ROUTINE NEEDS MODIFICATION BEFORE IT CAN BE USED.
1313 C*****
1314 NUM = NUM + 1
1315 WRITE (6,9999) NUM, KASE, NUMTIM
1316 9999 FORMAT ('OSLPLOT CALL NO. ', I5, ' ; ARGS=', 2I10)
1317 RETURN
1318 END
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4699      SUBROUTINE SLPLOT(X, NX, XO, XN, XL, XSIZE, XLAB, NXLB,
4700      *          Y, NY, YO, YN, YL, YSIZE, YLAB, NYLB,
4701      *          NPTS, NYY, NDY, PLAB1, NPLB1, PLAB2, NPLB2,KPLT)
4702      C                                          06/02/83
4703      C
4704      C ARGUMENTS:
4705      C X(NPTS) - ARRAY OF NPTS ABSCISSAS TO BE PLOTTED.
4706      C Y(NDY,NYY) - ARRAY OF NPTS*NY Y ORDINATES TO BE PLOTTED.
4707      C NX,NY - O OR POSITIVE - LINEAR PLOTS ON POSITIVE AXIS
4708      C          NEGATIVE - LOGARITHMIC PLOT ON NEGATIVE AXIS.
4709      C          NX,NY ARE GRID DIVISIONS ALONG X- AND Y-AXES.
4710      C XO,YO - MINM VALUES OF X AND Y.
4711      C XN,YN - MAXM VALUES OF X AND Y.
4712      C XL,YL - LENGTH (INCHES) OF X,Y AXES.
4713      C XSIZE,YSIZE - PAPER SIZE (INCHES) IN X,Y DIRECTIONS.
4714      C XLAB,YLAB - X,Y AXES LABELS (ALPHANUMERIC ARRAYS).
4715      C NXLB,NYLB - NO. OF CHARACTERS IN X,Y LABELS.
4716      C NPTS - NO. OF POINTS IN X ARRAY AND EACH Y ARRAY.
4717      C NYY - NO. OF Y ARRAYS TO BE PLOTTED VS. X ARRAY.
4718      C NDY - FIRST DIMENSION OF Y ARRAY IN CALLING ROUTINE.
4719      C          (NDY MUST BE .GE. NPTS)
4720      C PLAB1,PLAB2 - 1ST & 2ND LINES OF PLOT ID LABELS (ALPHANUMERIC).
4721      C NPLB1,NPLB2 - NO. OF CHARACTERS IN PLOT ID LABELS.
4722      C KPLT - PLOT NUMBER
4723      C NPLSMB - SYMBOL NO. TO BE USED FOR EACH CURVE
4724      C
4725      C NOTE: PLOTS WILL BE TRUNCATED AS FOLLOWS:
4726      C NX,NY POSITIVE - XO,YO .LE. X,Y .LE. XN,YN
4727      C NX,NY NEGATIVE - XO,YO .LE. X,Y .LE. XN,YN
4728      C
4729      C COMMON/IPLSMB/NPLSMB(100)
4730      C DIMENSION X(NPTS),Y(NDY,NYY),XLAB(1),YLAB(1),PLAB1(1),PLAB2(1)
4731      C DIMENSION XPL(5000),YPL(5000)
4732      C
4733      C
4734      C WRITE (6,4) NDY,NYY,NPTS,Y
4735      C 4 FORMAT(1X,' NDY ',I6,5X,' NYY ',I6,5X,' NPTS ',I6,/,.(1X,6E15.5))
4736      C CALL BGNPL(KPLT)
4737      C CALL PAGE(XSIZE,YSIZE)
4738      C CALL NOBRDR
4739      C CALL NOCHEK
4740      C
4741      C CHECK TYPE OF PLOT AXIS
4742      C
4743      C CALL HEIGHT(0.18)
4744      C CALL INTAXS
4745      C CALL TITLE(PLAB1,NPLB1,XLAB,NXLB,YLAB,NYLB,XL,YL)
4746      C CALL FRAME
4747      C YMESS=YL+0.25
4748      C XMESS=XL-2.5
4749      C CALL HEIGHT(0.16)
4750      C IF (NX.LT.O) XCYCL=ALOG10(XN/XO)
4751      C IF (NY.LT.O) YCYCL=ALOG10(YN/YO)
4752      C IF (NX.GT.O) XSTEP=(XN-XO)/XL
4753      C IF (NY.GT.O) YSTEP=(YN-YO)/YL
4754      C IF (NY.GE.O .AND. NX.GE.O) CALL GRAF(XO,'SCALE',XN,YO,'SCALE',YN)
4755      C IF (NX.LT.O .AND. NY.LT.O) CALL LOGLOG(XO,XCYCL,YO,YCYCL)
4756      C IF (NX.GE.O .AND. NY.LT.O) CALL YLOG(XO,XSTEP,YO,YCYCL)

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4757         IF (NX.LT.O .AND. NY.GE.O) CALL XLOG(XO,XYCL,YO,YSTEP)
4758         IF (NX.GT.O) IGRX=NX
4759         IF (NX.LT.O) IGRX=-NX
4760         IF (NY.GT.O) IGRY=NY
4761         IF (NY.LT.O) IGRY=-NY
4762         IF (NX.EQ.O) IGRX=1
4763         IF (NY.EQ.O) IGRY=1
4764         CALL GRID(IGRX,IGRY)
4765         DO 40 J=1,NYY
4766         JJP=NPLSMB(J)
4767   C       WRITE (6,52) XO,YO,XN,YN,XL,YL,JJP,XSTEP,YSTEP,J,NYY
4768         52 FORMAT(1X,' XO, YO ',2F15.5,5X,' XN, YN ',2F15.5,/,1X,' XL, YL ',
4769         12F15.5,5X,' NPLSMB ',I5,/,1X,' XSTEP, YSTEP ',2F15.5,
4770         25X,' J ',I4,5X,' NYY ',I4)
4771         DO 39 I=1,NPTS
4772         XPL(I)=X(I)
4773         YPL(I)=Y(I,J)
4774   39      CONTINUE
4775         IF (JJP.LT.O) CALL DASH
4776         IF (JJP.LT.O) JJP1=JJP+1
4777         IF (JJP.GE.O) JJP1=JJP
4778         CALL CURVE(XPL,YPL,NPTS,JJP1)
4779         IF (JJP.LT.O) CALL RESET('DASH')
4780   40      CONTINUE
4781         CALL HEIGHT(0.15)
4782         CALL MESSAG('ODIAC1 / GMR',12,XMESS,YMESS)
4783         YMS1=YMESS-0.15
4784         XMS1=XMESS-0.05
4785         CALL MESSAG('.....$',100,XMS1,YMS1)
4786         CALL ENDPL(KPLT)
4787         RETURN
4788         END

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1319      SUBROUTINE VECADD(VA,VB,VC)
1320      DIMENSION VA(3), VB(3), VC(3)
1321      DO 10 I = 1, 3
1322      VC(I) = VA(I) + VB(I)
1323 10 CONTINUE
1324      RETURN
1325      END
1326      SUBROUTINE VECSUB(VA, VB, VC)
1327      DIMENSION VA(3), VB(3), VC(3)
1328      DO 10 I = 1, 3
1329      VC(I) = VA(I) - VB(I)
1330 10 CONTINUE
1331      RETURN
1332      END
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