

1 **Eruptive Event Generator Based on the Gibson-Low Magnetic**
2 **Configuration**

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Abstract

Coronal Mass Ejections (CMEs), a kind of energetic solar eruptions, are an integral subject of space weather research. Numerical magnetohydrodynamic (MHD) modeling, which requires powerful computational resources, is one of the primary means of studying the phenomenon. With increasing accessibility of such resources, grows the demand for user-friendly tools that would facilitate the process of simulating CMEs for scientific and operational purposes. The Eruptive Event Generator based on Gibson-Low flux rope (EEGGL), a new publicly available computational model presented in this paper, is an effort to meet this demand. EEGGL allows one to compute the parameters of a model flux rope driving a CME via an intuitive graphical user interface (GUI). We provide a brief overview of the physical principles behind EEGGL and its functionality. Ways towards future improvements of the tool are outlined.

Coronal Mass Ejections (CMEs) were first observed in the early 1970s. The phenomenon immediately drew attention of the scientific community and stayed in focus because of the potential hazards that CMEs pose to humanity, its technology and endeavors [Webb, 1995, 2000; Gopalswamy, 2009]. Bodies of works studying either subject constitute two whole branches of physical research [see e.g. Cliver, 2009; Lakhina and Tsurutani, 2016]. The vast range of damage that CMEs may cause highlights how crucial is the ability to mitigate their effects, which may be attained with the forecasting capability in studies of CMEs and their propagation to Earth..

Efforts aimed at developing predictive models include various empirical and statistical models some of which are designed to predict the arrival time of a CME at 1 AU, such as EIEvoHI [Rollett *et al.*, 2016] and a number of others [e.g. Gopalswamy *et al.*, 2001; Riley *et al.*, 2015]. The most significant problem in space weather forecasting at the moment, however, is determining the magnetic field and its southward component, B_z , in particular in an Earth-impacting CME. Among promising recent models that predict B_z are, for example, Savani *et al.* [2015]; Kay *et al.* [2017]. Despite great advancements in empirical techniques, such models are naturally limited in both accuracy and amount of information they are able to provide. Significant complex processes such as CME deflection and rotation caused by interaction with the coronal magnetic field, are inevitably significantly simplified or even omitted in these models. For this reason fully 3-D numerical modeling remains the most promising tool utilized in CME forecasting. These simulations are able to provide predictions for CME arrival time, structure and, most importantly, the magnetic field vector, while taking fully into account complexity of the aforementioned processes.

Over last two decades a very prominent progress has been made in this area. Several so-called kinematic CME models have been developed, e.g. Hakamada-Akasofu-Fry version 2 (HAFv.2) model [Hakamada and Akasofu, 1982; Fry et al., 2001; Dryer et al., 2004] and the cone model [Zhao et al., 2002; Hayashi et al., 2006], which accurately predict the CME arrival time (typically within 8 to 10 hours), although they aren't able to predict CME's plasma parameters. Further, the geometric and kinematic properties of a CME found with the cone model are often used as an input for ENLIL [Odstrčil, 2003], a 3-D MHD heliospheric model. Such combination allows obtaining more detailed results for CME-caused disturbances of plasma parameters, e.g. density and pressure, but lacks accuracy in predicting the magnetic field.

As CME models grew in complexity, due to major advancements in numerical methods and computing capabilities, a new type of challenge has emerged. It became increasingly difficult for an individual researcher to be able to apply these sophisticated computational tools in their work. For this reason, there has been an effort to simplify the access to the models and thus make the modeling of CMEs a more available and frequent practice. An important step towards these goals is the Eruptive Event Generator based on Gibson-Low magnetic configuration (EEGGL).

EEGGL is a supporting numerical tool that provides parameters for an independent CME model, which employs the Gibson and Low [1998] (GL) flux rope configuration. This approach inserts the GL flux rope into a numerical model of the corona. It has been applied in a number of works [Manchester et al., 2004a,b, 2006, 2014b,a; Lugaz et al., 2005, 2007; Kataoka et al., 2009; Jin et al., 2016, 2017a; Shiota and Kataoka, 2016] and has proved to be well-suited for the purposes of simulating CMEs. The GL flux rope serves as a good representation of an erupting magnetic flux rope filled with dense plasma that is representative of a filament. This flux rope expands and evolves into a magnetic cloud as it propagates away from the Sun, which provides the basis for simulating magnetically driven CMEs to 1 AU. We emphasize that by choosing GL configuration we don't claim its superiority over alternatives [e.g. Titov and Démoulin, 1999].

The key idea of constructing a GL flux rope is to convert a spherical magnetic configuration in equilibrium, the spheromak, into a self-similarly expanding flux rope in the presence of gravity. In the MHD equilibrium, the magnetic field \mathbf{B} , current density, \mathbf{j} , and plasma pressure, P , satisfy equation [Landau and Lifshitz, 1960]:

$$\mathbf{j} \times \mathbf{B} - \nabla P = 0, \quad (1)$$

For any equilibrium configuration, $\mathbf{j} \cdot \nabla P = 0$ and $\mathbf{B} \cdot \nabla P = 0$, i.e. a single line of either magnetic field, or electric current is entirely confined within a single *magnetic surface*, which is a surface of constant pressure. For an axisymmetric equilibrium MHD configuration the relation between the magnetic field, current

68 and pressure is further strengthened. The magnetic flux, ψ , and the current, I , bounded by the magnetic
69 surface remain constant at this surface, just as the pressure. Therefore, there is a functional dependence
70 between ψ , I and P : $I=I(\psi)$, $P=P(\psi)$. Under these circumstances, the magnetic field is governed by the
71 Grad-Shafranov equation [Grad and Rubin, 1958; Shafranov, 1966]. In the particular case of constant $\frac{dI}{d\psi}$
72 and $\frac{dP}{d\psi}$, the Grad-Shafranov equation has analytical solutions. One such solution describes the spheromak
73 configuration, bounded by a spherical magnetic surface, $\|\mathbf{R} - \mathbf{R}_s\| = r_0$. Its magnetic field and pressure may
74 be parameterized via three constant parameters B_0 , $\alpha_0 = \mu_0 dI/d\psi$ and $\beta_0 = \frac{\mu_0}{B_0^2} \frac{dP}{d\psi}$ as follows:

$$\mathbf{B}_s(\mathbf{r}) = \left[\frac{j_1(\alpha_0 r)}{\alpha_0 r} - \beta_0 \right] (2\mathbf{B}_0 + \sigma_h \alpha_0 [\mathbf{B}_0 \times \mathbf{r}]) + j_2(\alpha_0 r) \frac{[\mathbf{r} \times [\mathbf{r} \times \mathbf{B}_0]]}{r^2} \quad (2)$$

75

$$P_s(\mathbf{r}) = \left[\frac{j_1(\alpha_0 r)}{\alpha_0 r} - \beta_0 \right] \frac{\beta_0 \alpha_0^2 [\mathbf{r} \times \mathbf{B}_0]^2}{\mu_0} \quad (3)$$

76 $j_1(x) = \frac{\sin x - x \cos x}{x^2}$ and $j_2(x) = \frac{3j_1(x) - \sin x}{x}$ are the spherical Bessel functions of argument $x=\alpha_0 r$, $\sigma_h = \pm 1$
77 is the sign of helicity. Herewith, the vector \mathbf{B}_0 is introduced with the magnitude equal to B_0 directed along
78 the axis of symmetry. In Eqs. 2-3, the coordinate vector, \mathbf{r} , originates at the center of configuration, \mathbf{R}_s ¹.
79 Generally, the coordinate vector, \mathbf{R} , is related to \mathbf{r} as $\mathbf{r} = \mathbf{R} - \mathbf{R}_s$.

80 At the external boundary, $\|\mathbf{R} - \mathbf{R}_s\| = r_0$, the radial and toroidal components of the magnetic field
81 vanish (i.e. $j_1(\alpha_0 r_0) = \beta_0 \alpha_0 r_0$). Thus, for a given β_0 the configuration size, r_0 , is related with the extent
82 of magnetic field twisting, α_0 , needed to close the configuration within this size. The plasma pressure, P ,
83 also turns to zero at the external boundary. In Gibson and Low [1998] and the papers cited therein, the non-
84 trivial choice of *negative* value of β_0 had been proposed (without stating this point explicitly), such that all
85 three components in Eq. 2 vanish at $\|\mathbf{R} - \mathbf{R}_s\| = r_0$. Specifically, the choice of $\beta_0 = j_1(\alpha_0 r_0)/(\alpha_0 r_0) \approx -2.87 \cdot$
86 10^{-2} , where the radius is defined by condition $j_2(\alpha_0 r_0) = 0$, i.e. $\alpha_0 r_0 \approx 5.76$, satisfies this criterion.

87 The negative variation of pressure within the configuration as in Eq. 3 is meaningful only when added to
88 some positive background pressure, P_b , so that the total pressure, $P_s + P_b$, is positive and realistic. To avoid
89 the pressure jump at the boundary, this background pressure should also exist outside the configuration to
90 maintain the force balance, particularly, preventing the configuration's disruption by the internal forces (the
91 so-called hoop force).

¹ In Jin *et al.* [2017b] and papers cited therein R_s is denoted as r_1 . Also, the magnetic field magnitude is expressed in terms of a parameter, α_1 ,
the unit for this parameter being gauss/ R_\odot^2 (note the typo in the note to Table 1 in Jin *et al.* [2017b]). The relationship between the parameters in
the CGS unit system is as follows: $\frac{B_0}{\text{Gs}} \approx 13.17 \frac{\alpha_1}{\text{Gs}/R_\odot^2} \frac{r_0^2}{R_\odot^2}$, where $13.17 \approx \frac{4\pi}{(\alpha_0 r_0)^2 \beta_0}$.

92 A *radial stretching* proposed by *Gibson and Low* [1998] extends the spheromak solution to include the
 93 effect of solar gravity and/or the flux rope acceleration. The magnetic field and pressure distribution of the
 94 new equilibrium configuration in the heliocentric coordinates, \mathbf{R} , are expressed via those of the spheromak
 95 evaluated at the point $\mathbf{R}'(\mathbf{R}) = (1 + \frac{a}{R}) \mathbf{R}$, where $R' = R + a$. An arbitrary constant a is the distance of
 96 stretching. To keep the stretched field divergence-free, one needs to additionally scale it. The final expres-
 97 sion for the field is:

$$\mathbf{B}(\mathbf{R}) = \frac{R'}{R} \left(\mathbb{I} + \frac{a}{R} \mathbf{e}_R \mathbf{e}_R \right) \cdot \mathbf{B}_s(\mathbf{R}' - \mathbf{R}_s) \quad (4)$$

98 where $\mathbf{e}_R = \mathbf{R}/R$ and \mathbb{I} is the identity matrix. The plasma pressure of the stretched magnetic configuration
 99 is defined as:

$$P(\mathbf{R}) = \left(\frac{R'}{R} \right)^2 \left(P_s(\mathbf{R}' - \mathbf{R}_s) - \frac{a}{R} \left(2 + \frac{a}{R} \right) \frac{B_{sR}^2(\mathbf{R}' - \mathbf{R}_s)}{2\mu_0} \right) \quad (5)$$

100 Substituting expressions from Eqs. 4 and 5 into Eq. 1 results in the radial force, F_R , from the added ten-
 101 sion of the stretched magnetic field, $\frac{1}{\mu_0} (\nabla \times \mathbf{B}) \times \mathbf{B} - \nabla P = F_R \mathbf{e}_R$. This excessive force may balance the
 102 gravity acting on the density profile, if:

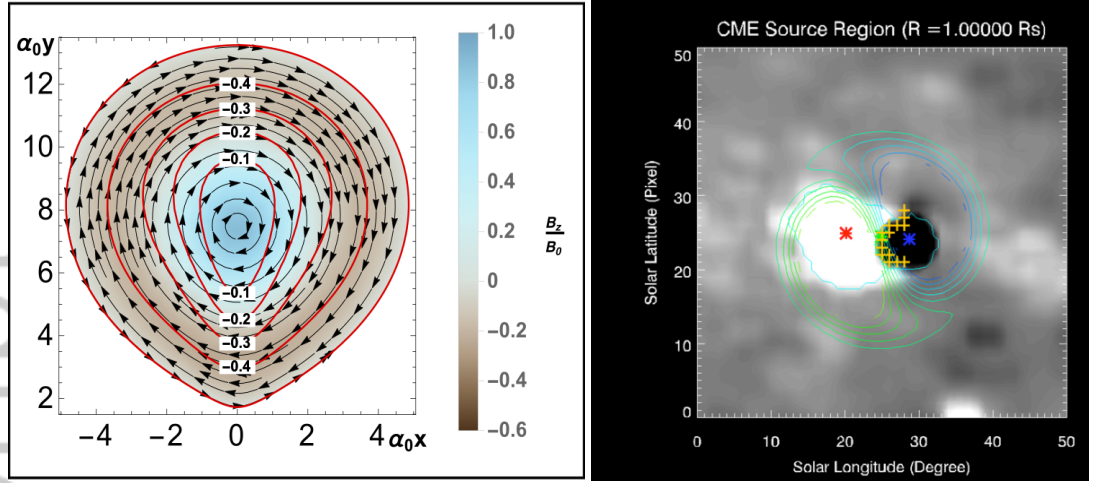
$$\rho = \frac{F_R}{g(R)} \quad (6)$$

103 where $\mathbf{g}(R) = -GM_\odot/R^2 \mathbf{e}_R$, G is the gravitational constant, M_\odot is the solar mass. Eq. 6 results, however, in
 104 negative density. In reality this corresponds to regions with depleted plasma density compared to the back-
 105 ground. In fact, one can superimpose the configuration defined by Eqs. 4, 5 and 6 over any barometric at-
 106 mosphere, $P_{\text{bar}}(\mathbf{R})$ and $\rho_{\text{bar}}(\mathbf{R})$, while retaining the equilibrium condition:

$$\frac{1}{\mu_0} (\nabla \times \mathbf{B}) \times \mathbf{B} - \nabla (P + P_{\text{bar}}) + (\rho + \rho_{\text{bar}}) \mathbf{g} = 0 \quad (7)$$

115 As a result of the transformation, the spherical configuration is stretched towards the heliocenter as shown
 116 in the left panel in Fig. 1. If thus defined flux rope has an initial velocity profile $\mathbf{u} \propto \mathbf{R}$, or if the radial ten-
 117 sion is applied to a reduced density in the configuration, $\rho = \frac{F_R}{g(R)+A(R)}$, to produce an acceleration in the
 118 radial direction, $\mathbf{A} \propto \mathbf{R}$, it would self-similarly travel away from the Sun [*Gibson and Low*, 1998], i.e. mimic
 119 behavior of a CME.

120 When the solution represented by Eq. 4, 5, 6 is superimposed onto the existing corona, the sharper end
 121 of the teardrop shape is submerged below the solar surface. In the wider top part of the configuration ("bal-
 122 loon") the density variation in Eq. 6 is *negative*, which makes the resulting density lower than that of the
 123 ambient barometric background. As the result, the Archimedes (buoyancy) force acting on this part pulls
 124 the whole configuration away from the Sun. Such structure is consistent with the commonly observed three-
 125 part CME configuration consisting of a bright leading loop enclosing a dark low-density cavity contain-



107 **Figure 1.** **Left:** Equatorial plane of the stretched flux rope for $\beta_0 = -2.87 \times 10^{-2}$. The original flux rope is placed by distance
 108 $R_s = 1.6r_0$ along a direction in the equatorial plane and then stretched towards the heliocenter by distance $a = 0.3r_0$. Magnetic field
 109 direction is marked with arrows, off-plane component of the magnetic field is normalized per B_0 and shown by color. Local values
 110 of plasma parameter $\beta(\mathbf{r}) = \mu_0 P(\mathbf{r})/B^2(\mathbf{r})$ are shown with red curves corresponding to levels $\beta = -0.1, -0.2, -0.3, -0.4$. **Right:**
 111 The zoomed-in AR as seen in the GONG magnetogram. By clicking on the white (positive) and black (negative) spots, EEGGL
 112 calculates the GL configuration parameters. The radial magnetic field levels of the recommended GL configuration is shown with
 113 the contour lines. The S-shaped polarity inversion line of the GL configuration, separating the cusped contours, overlaps with that
 114 of the AR (yellow crosses).

126 ing a high-density core [e.g. *Hundhausen, 1993; Howard et al., 1997*]. The core of the structure, the nar-
 127 rower Sun-ward part of the configuration with excessive *positive* density, is typically considered to be fil-
 128 ament material. The prominence material is often visible in the EUV at 304 \AA) where it corresponds with
 129 the the CME core [e.g. *Davis et al., 2009; Liu et al., 2010*] The tip of the configuration with the magnetic
 130 field lines both ingoing and outgoing from the solar surface is anchored to the negative and positive mag-
 131 netic spots of a bipolar active region (see the right panel in Fig. 1), considered as the source of the CME.
 132 Depending on the reconnection rate, the configuration, while it travels toward 1 AU, can either keep being
 133 magnetically connected to the AR, or it may disconnect and close.

134 Self-similarity of the propagation isn't strictly retained in the realistic corona: in order for the config-
 135 uration to remain at force-equilibrium and therefore propagate in a self-similar fashion, a confining shape
 136 needs to have a specific distribution of the external pressure and velocity, which linearly increases with ra-
 137 dial distance. The self-similarity breaks down, when solar wind approaches its terminal velocity, i.e. stops
 138 accelerating. Realistic distribution of pressure in the coronal plasma leads to the pressure imbalance, i.e.

139 the loss of equilibrium, one of the key assumptions of GL approach. Also, coronal magnetic field exerts
140 Ampere's force onto the flux rope's current, thus further contributing to the force imbalance. This effect
141 may be reduced by choosing a more realistic value of β_0 , e.g. $\beta_0=0$, which would allow canceling the back-
142 ground magnetic field, at least partially, within the flux rope. Nevertheless, numerical studies [e.g. *Manch-*
143 *ester et al.*, 2004b,a; *Lugaz et al.*, 2005; *Jin et al.*, 2017a] showed that the evolution of the flux rope is ap-
144 proximately self-similar to a distance of 40-50 R_\odot . which provides a certain predictability of the subsequent
145 CME transport. This, ultimately, defines the suitability of GL flux rope as a tool for initiating CMEs with
146 predefined properties and led to the development of EEGGL.

147 EEGGL ² is a user-friendly tool developed by *Jin et al.* [2017b] and successfully transitioned to the Com-
148 munity Coordinated Modeling Center (CCMC). It integrates solar images of the eruption into an intuitive
149 GUI that allows the user to set the parameters of the GL flux rope, which is designed to model a magnet-
150 ically driven CME and its propagation to 1 AU. EEGGL incorporates magnetograms of the solar magnetic
151 field prior to the eruption, and, if possible, the multi-point coronagraph observations of the CME near the
152 Sun. As seen above, for a fixed $\beta_0 = -2.87 \times 10^{-2}$ a non-accelerating GL flux rope is fully defined by the
153 set of free parameters \mathbf{R}_s , a , r_0 , \mathbf{B}_0 , σ_h . In the current implementation of EEGGL σ_h is chosen according
154 to the hemispheric helicity rule (± 1 for southern/northern hemisphere), while $R_s = 1.8R_\odot$ and $a = 0.6R_\odot$ are
155 fixed. Also, the magnetic field vector, B_0 , has no radial component. Thus, EEGGL needs to determine 5 re-
156 maining free parameters: latitude and longitude of the flux rope's center, orientation of the flux rope's axis,
157 its size, r_0 , and characteristic strength of the magnetic field, B_0 . All parameters are computed based on the
158 pre-eruptive magnetogram and user's input: the choice of an active region (AR), from which the CME origi-
159 nates, and its speed. The latter together with the magnetogram defines B_0 [see *Jin et al.*, 2017b]. The CME
160 speed is obtained with the help of the STEREOcat ³ web-application available at the CCMC, which allows
161 the user to derive both the CME speed and an approximate source location. For detailed instructions we re-
162 fer readers to EEGGL web-site². Using these inputs EEGGL automatically (1) processes the magnetogram;
163 (2) analyzes and calculates the integral parameters of the AR; (3) automatically calculates the parameters
164 of the GL flux rope; and finally (4) visualizes the magnetic field of the AR and of the GL configuration to
165 verify that they match (see the right panel in Fig. 1).

166 EEGGL is not an independent tool and one requires a numerical heliospheric model to perform the ac-
167 tual simulation. The flux rope parameters produced by EEGGL can readily be used to initiate a CME sim-

² Available at <https://ccmc.gsfc.nasa.gov/eeggl/>

³ Available at <https://ccmc.gsfc.nasa.gov/analysis/stereo/>

168 ulation in Space Weather Modeling Framework (SWMF) [Tóth *et al.*, 2012] either at the CCMC’s compu-
169 tational facilities (the link is provided to users together with the results), or manually elsewhere. The pa-
170 rameters may also be used by any numerical heliospheric models, e.g. ENLIL [Odstrčil, 2003], SUSANOO-
171 CME [Shiota and Kataoka, 2016] or EUHFORIA [Poedts and Pomoell, 2017], that supports CME initiation.

172 The primary source of criticism of EEGGL is the overall validity of representing CME by the flux rope
173 of Gibson and Low [1998]. Although all published research to the date succeeds in doing so, the range of
174 applicability of the approach isn’t known. On the other hand, EEGGL presents a suitable tool for explo-
175 ration and finding the conditions, when the technique fails to launch a successful CME.

176 The advantage of EEGGL as a community-wide available tool is simplicity of its interface. The AR is
177 chosen by mouse-click on a magnetogram’s image, the rest of the procedure is fully automated. This allows
178 any user to set simulation parameters in a matter of minutes and focus on studying the physics of the pro-
179 cess rather than the technical details of setting such simulation. At the moment, EEGGL is a unique tool
180 that simplifies the interaction between a user and sophisticated numerical heliospheric models.

181 However, EEGGL hasn’t reached its functionality limits and may be further improved. The further devel-
182 opment will proceed along the following directions. The helicity of the flux rope, instead of being fixed for
183 each hemisphere, will be derived from a vector magnetic field observations [e.g. Space-weather HMI Active
184 Region Patches, SHARPs, Bobra *et al.*, 2014]. More control over the CME propagation will be achieved by
185 applying special variations of the density profile of the flux rope, which results in an accelerated/decelerated
186 self-similar motion [see Gibson and Low, 1998]. Incorporating such a feature would increase the func-
187 tionality and range of the application of EEGGL and is the likely next step of its development. Addition-
188 ally, EEGGL may be complemented with more precise methods of determining CME’s speed in the early
189 phase of eruption, e.g. via estimation of the reconnected flux using post-eruption arcades [Gopalswamy
190 *et al.*, 2017], or through the relationship between the EUV dimming and resulting CME speed [Mason *et al.*,
191 2016]. Implementing new features requires adding new parameters to the model accompanied with exten-
192 sive testing and validation via comparison with observational data.

193 The expected contribution of EEGGL to the community is yet to be measured, but one may expect a
194 significant increase in the number of CME-related works and publications. This would provide opportunities
195 for more detailed numerical studies of the process itself as well as related phenomena.

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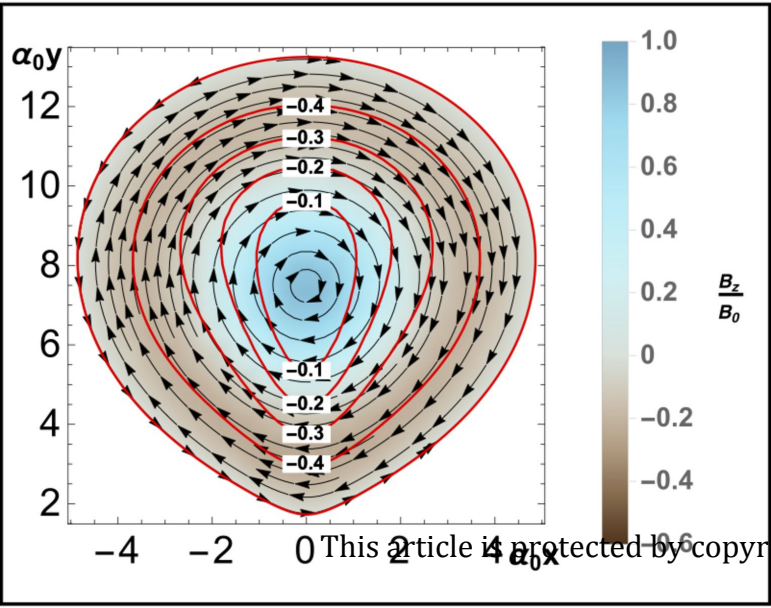
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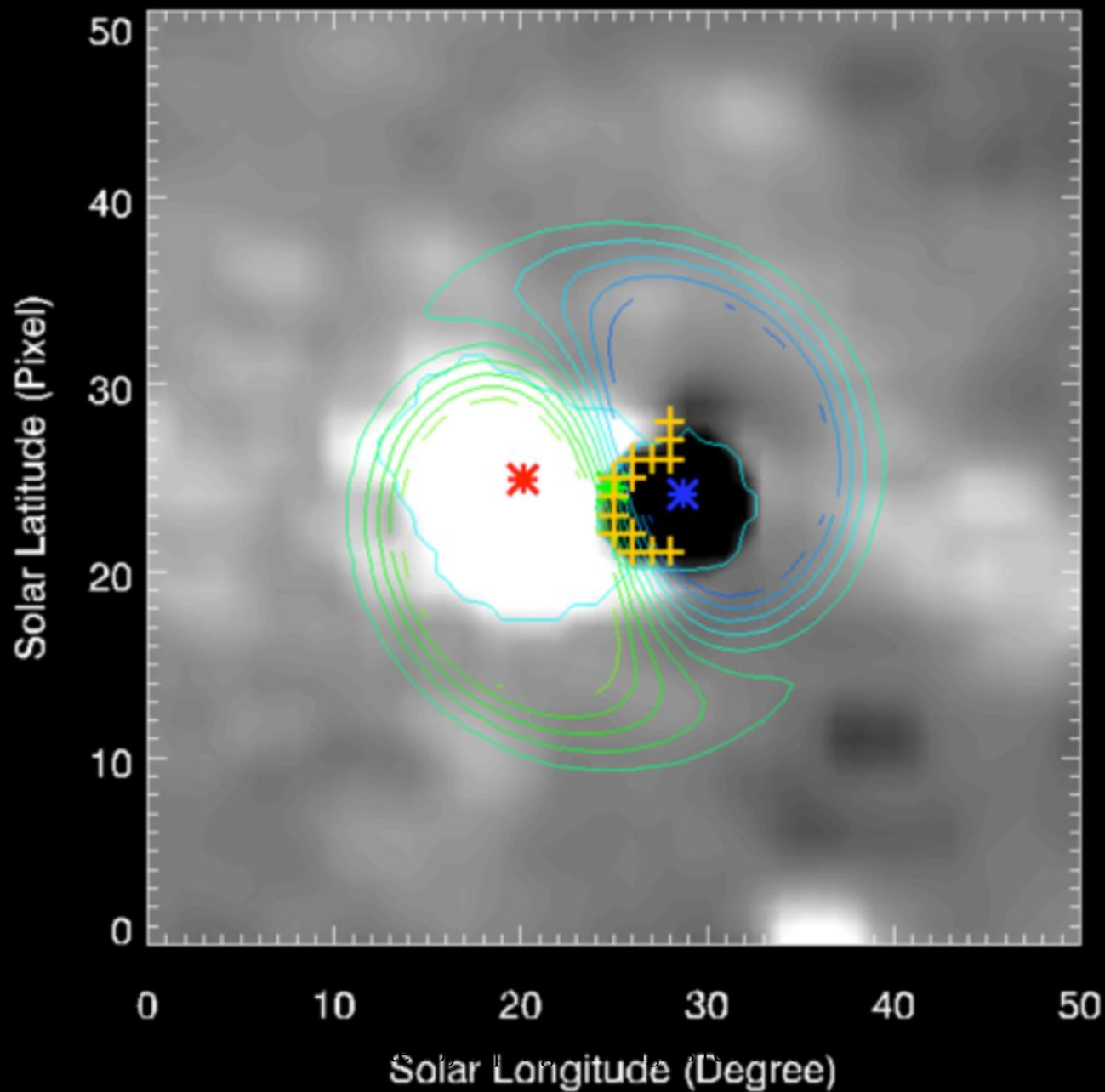
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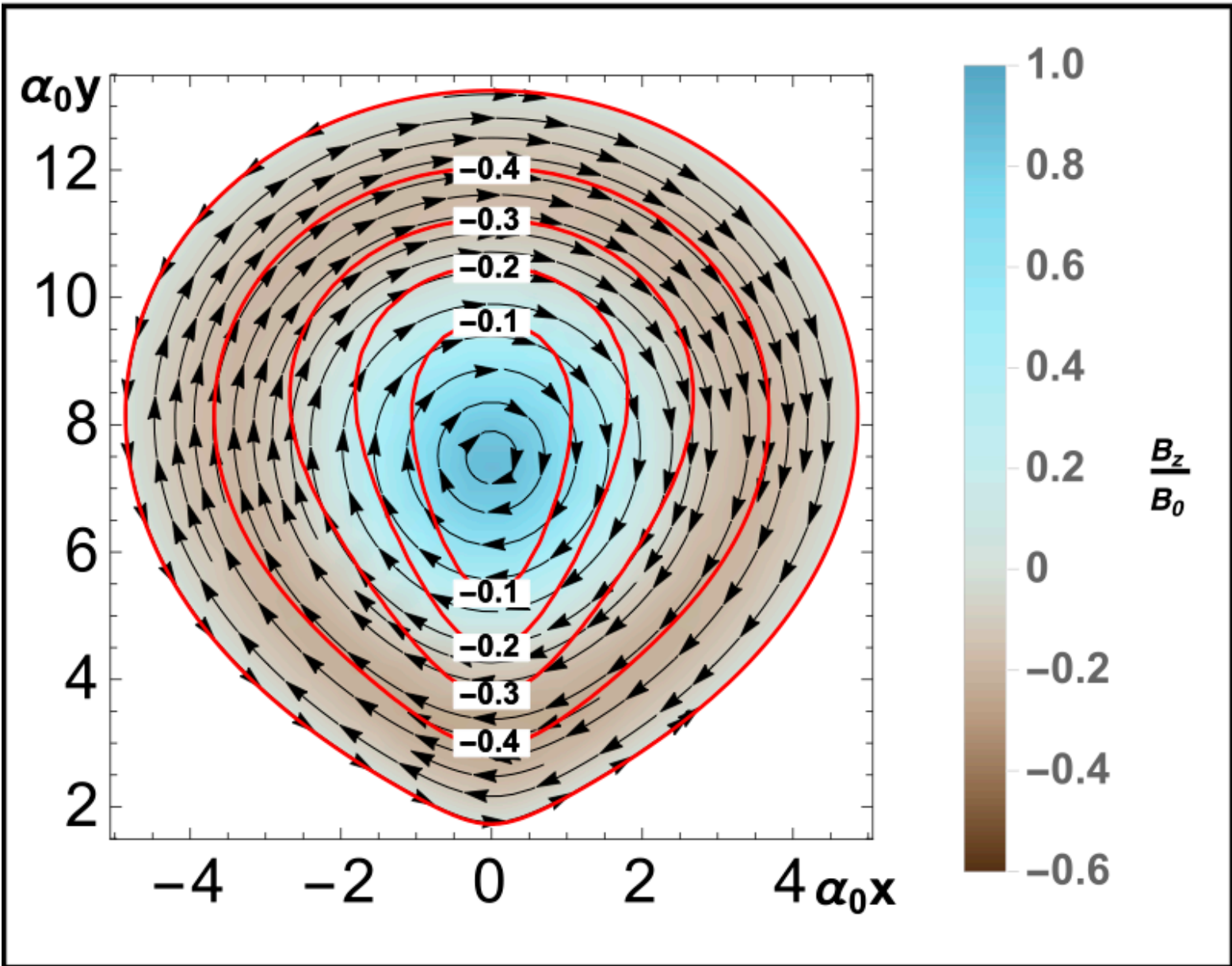
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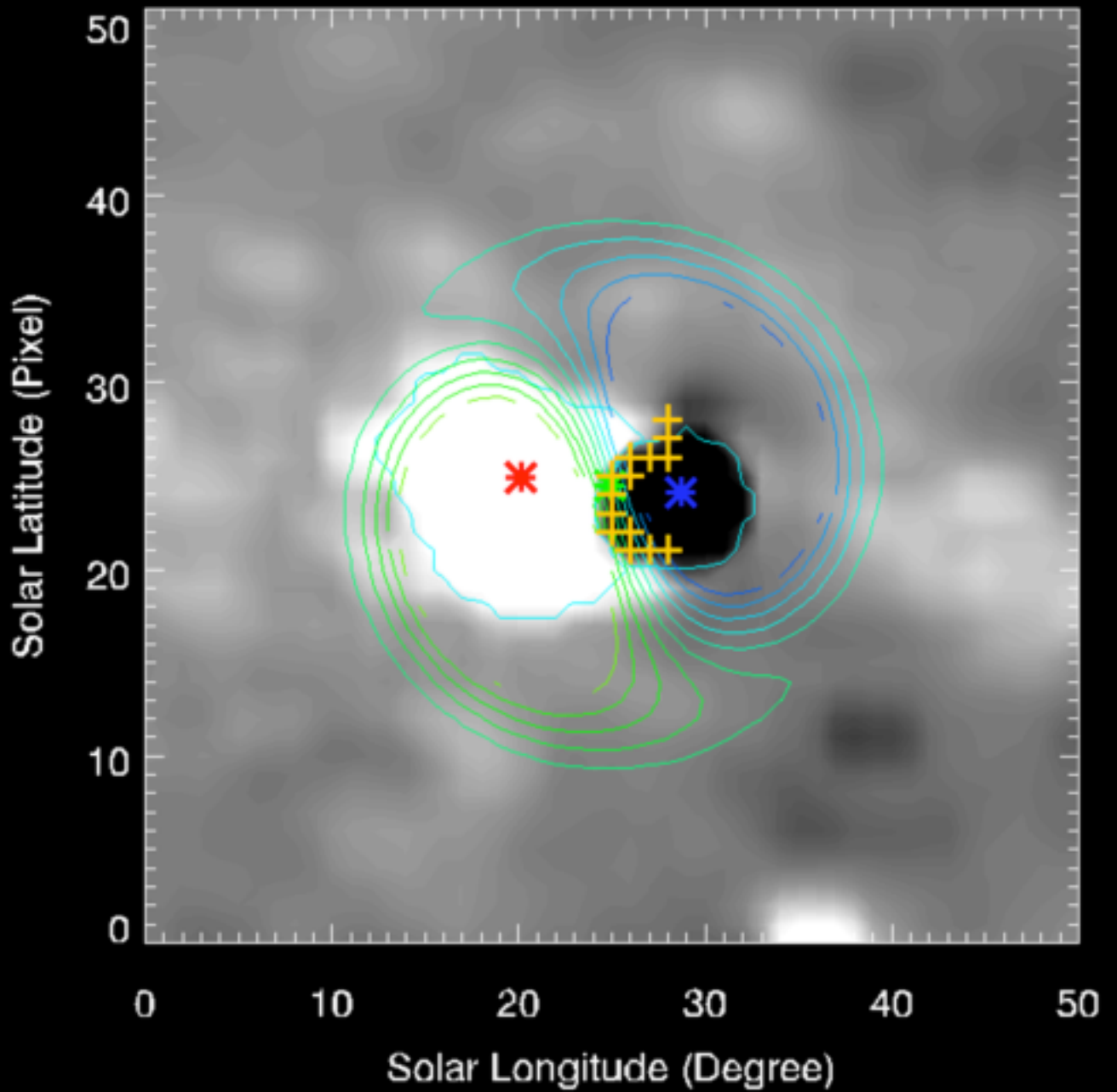
CME Source Region ($R = 1.00000 R_s$)





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