



# Vibrational relaxation and dissociation in $O_2$ -O mixtures

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Thermal relaxation in  $O_2$ -O mixtures is studied using state-specific transition rate coefficients, generated by extensive trajectory simulations. Both  $O_2$ -O and  $O_2$ - $O_2$  collisions are concurrently simulated in the evolving nonequilibrium gas mixture under constant heat bath conditions and in one-dimensional shock flow. Accuracy of the state-resolved and multi-temperature models is assessed by comparing computed temperatures and atomic oxygen number density with experimental data. The effect of rotational nonequilibrium is included to provide a realistic description of the energy balance in strong shock waves. The present study demonstrates the importance of atom-diatom collisions due to the extremely efficient energy randomization in the intermediate  $O_3$  complex. It is shown that the presence of atomic oxygen has a significant impact on vibrational relaxation time at temperatures observed in hypersonic flow. The population of highly-excited  $O_2$  vibrational states is affected by the amount of atomic oxygen when modeling the relaxation under constant heat bath conditions. Recommendations on accuracy of the low fidelity thermochemistry models of oxygen are provided.

## I. Introduction

Hypersonic flight experiments, conducted during the past several decades, have revealed a necessity of coupling the experimental and theoretical approaches in order to improve the existing computational models of nonequilibrium air plasma. One of the important aspects of hypersonic aerothermodynamics is the energy exchange among the translational and internal degrees of freedom (DOF) of species behind a shock wave. Since the characteristic times of excitation of translational and vibrational modes differ by orders of magnitude, the hypersonic flow can be in a state of thermal nonequilibrium. Furthermore, the excitation of internal DOF is coupled to the dissociation process. Thus, it is important to accurately model the energy exchange in order to predict the structure of the shock wave.

Among other phenomena that take place in shock waves, the vibrational excitation and deactivation play an important role in the energy balance. For the past decade, a significant improvement in the fidelity of existing models of air species has been accomplished. Most of the progress has been achieved in modeling of molecular nitrogen [1–3], because of its importance in re-entry flows.

Systems that contain oxygen are studied less often, mainly because oxygen quickly dissociates in a strong shock wave [4–7]. However, a significant amount of molecular oxygen is observed during hypersonic cruise flight in the post-shock region. This flight regime is inherent in hypersonic vehicles which travel at a speed of about 2–3 km/s. The vibrational relaxation in  $O_2$ -O collisions is known to proceed several orders of magnitude faster than in other types of collisions in air and does not follow the conventional dependence on temperature of the gas flow [8]. These factors make a SR kinetic approach a very desirable technique, since it is possible to model thermal nonequilibrium in shock and expanding flows without invoking the thermodynamic definition of temperature.

The state-specific transition rates in  $O_2$ -O collisions were recently computed [9, 10] on the accurate, many-body potential energy surface [11] using the Quasi Classical Trajectory (QCT) method. These rates,

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employed in the master equation simulation [12], revealed an anomalously fast vibrational relaxation time in atom-diatom collisions, compared to other molecular systems containing oxygen. These findings were related to the existence of a large attractive component in the  $O_3$  PES that leads to an extremely efficient energy randomization.

The state-resolved (SR) kinetic models are of significant interest due to their accuracy in describing the nonequilibrium flows over the large range of input parameters. These models are applied to describe kinetics of hypersonic flow in shock waves [13, 14], nozzle flow [15] and in boundary layers [16]. Under nonequilibrium conditions, the population of the vibrational manifold can be appreciably different from the equilibrium distribution. In shock waves, highly energetic vibrational states are underpopulated and dissociative reactions are dominant. The multi-temperature (MT) model is the alternative to the SR models for describing shock flows with the vibrational temperature less than the translational one. However, when the opposite situation takes place, i.e. the flow cools down, the selective recombination pumps energy into high vibrational states, forming the long plateau of the vibrational distribution. The multi-temperature model is not adequate in this regime since the global chemical rates exhibit strong non-Arrhenius behavior. The rates of dissociation in strongly recombining flow are related to either the atomic concentration or to the population of last vibrational state rather than to the vibrational temperature. A comprehensive investigation of  $N_2/N$  cooling flows was performed by Colonna and coworkers [17, 18]. In the present work, some insight on  $O_2/O$  recombinative flow is obtained by implementing the present  $O_2-O$  rates.

In order to bring the present simulation closer to real conditions,  $O_2-O_2$  collisions are included as well. The atom-diatom and diatom-diatom collisions are simultaneously modeled in the present work. Because an accurate trajectory simulation of bimolecular collisions in oxygen gas is yet to be conducted, the Forced Harmonic Oscillator (FHO) model [19] is employed to obtain the  $O_2-O_2$  vibration-translation (VT) and vibration-vibration (VV) transition rates. To model the SR  $O_2-O_2$  dissociation, several techniques are employed in the present paper. First, the SR QCT calculations using the  $O_4$  Varandas PES are conducted. These bound-free (BF) rate coefficients (RC) are compared to the  $O_2(v)-O_2$  BF RCs obtained via the scaling procedure from  $O_2-O$  state-specific QCT data. The third approach employs the concept of preferential dissociation [20] to generate the  $O_2(v)-O_2$  BF RCs. The accuracy of these methods is assessed by comparing computed and experimental values of species number density.

This paper is organized as follows. Section II provides details on  $O_2-O$  collisions, and addresses the main features of the master equations and multi-temperature models. The detailed study of vibrational relaxation and dissociation in oxygen gas is presented in Section III. Vibration-to-translation transition rates and corresponding relaxation times are discussed in Section III.A. Importance of multiquantum transitions in heating and cooling flows is discussed in Section III.B. Dissociation and recombination processes are studied in Section III.C. The comparison of SR and MT thermodynamic models is performed in Section III.D for heat bath conditions. A similar discussion for shock flows is given in Section III.E. Conclusions are provided in Section IV.

## II. Governing equations

### A. Specifics of $O_2-O$ collisions

The  $O_2-O$  vibration-to-translation (VT) transition rates, employed in the present work, are obtained on the accurate potential energy surface by [11] using the Quasi-Classical Trajectory (QCT) method [21]. The Varandas PES generates 47 vibrational levels and a maximum of 236 rotational levels for molecular oxygen in the ground electronic state. The total number of rovibrational levels in the ground electronic state of oxygen is 6,245, however, taking into account the nuclear spin statistics of a homonuclear molecule, the even numbered rotational levels for the  $O_2(X^3\Sigma_g^-)$  state are forbidden. Since, during a bound-bound rovibrational transition, the symmetry of the initial and final states cannot change, transitions of the  $O_2$  molecule in the ground electronic state are only allowed between odd-numbered rotational levels [22]. The energies of rovibrational states are calculated by the WKB approach.

The cross sectional data of bound-bound transitions, generated by the QCT method [23], is modified to take into account the degeneracy of the spin and orbital momentum of reactants. The degeneracy factor of the  $O(^3P)$  and  $O_2(^3X_g^-)$  reactants can be expressed in the form, given by [24]:

$$\frac{1}{g_{BB}} = 3 \left( 5 + 3 \exp \left( -\frac{227.6}{T} \right) + \exp \left( -\frac{325.9}{T} \right) \right) \quad (1)$$

The degeneracy factor of the bound-bound transition is found as a ratio of the PES degeneracy to the degeneracy of the reactants. Taking into account that the present  $O_3$  PES is non-degenerate, the total degeneracy for the reaction of bound-bound transitions is given by Eq. (1). At high temperatures, the degeneracy factor asymptotically approaches a factor of  $1/27$ . This means that the reaction takes place on only one of the 27 possible potential energy surfaces.

The dissociation of molecular oxygen in a shock wave with a temperature above a few thousands of K is unlikely to proceed in the adiabatic manner. One way to account for alternative channels of dissociation from excited electronic states is to assume equilibrium between lower vibrational levels of the excited electronic state and high vibrational levels of the ground state [25]. The contribution of dissociation from the excited electronic level should be added to the dissociation rate from the ground electronic level. It is possible to calculate the degeneracy factor of the dissociation reaction for each rovibrational level of the ground electronic state individually [26]. In this case, the degeneracy is calculated by assuming only electronic levels with a minimum of energy below the energy of the current rovibrational level. The degeneracy of the bound-free transition for the rovibrational level  $(v, j)$  is then computed as follows:

$$g_{BF, \nu, j} = 1 + \frac{\sum g^E}{g^X}, \quad (2)$$

where  $g^X = 3$  is the degeneracy of the ground electronic state, and  $g^E$  is the degeneracy of the electronically excited state. The assumption of equilibrium between the vibrational levels of the ground and excited states is valid if the following condition holds:

$$e_{\nu, j}^X > e_{\nu=0, j=0}^E. \quad (3)$$

Assuming that Eq. (3) holds for every rovibrational level of the ground electronic state, one can obtain the degeneracy factor of the bound-free transition, originally proposed in [25]:  $g_{BF} = 16/3$ .

The vibration-to-translation and vibration-to-vibration (VV) transition rates in  $O_2$ - $O_2$  collisions are obtained by means of the FHO model [19]. In order to generate the state-specific VT and VV transition rates the following parameters of the  $O_2$ - $O_2$  system are used:  $\alpha = 4.2 \text{ \AA}^{-1}$  and  $d = 3.75 \text{ \AA}$ , where  $\alpha$  describes the steepness of a purely repulsive intermolecular potential  $V(r) \sim \exp(-\alpha r)$  and  $d$  is the hard sphere diameter of oxygen. Because the probability of multiquantum jumps in the  $O_2$ - $O_2$  system is much lower than that with  $|\Delta v| = 1$ , only transitions with  $|\Delta v| \leq 5$  are considered in the present work. The database of  $O_2$ - $O$  rates, employed in the present work, includes all possible transitions [23].

## B. Master equations

The preliminary study of vibrational relaxation of oxygen includes only the bound-bound transitions in a system of master equations. Because at moderate temperatures (below 10,000 K) the trans-rotational equilibrium in hypersonic flows occurs much faster than the trans-vibrational one, the former is assumed throughout the present paper. This step significantly reduces the number of equations to be solved. The resulting equation for the number density of vibrational level  $i$  can be written as follows:

$$\begin{aligned} \frac{dn_i}{dt} = & \sum_{i' \neq i} \left( K_{i' \rightarrow i}^{O_2-O} n_{O} n_{i'} - K_{i \rightarrow i'}^{O_2-O} n_{O} n_i \right) + \sum_{i' \neq i} \left( K_{i' \rightarrow i}^{O_2-O_2} n_{O_2} n_{i'} - K_{i \rightarrow i'}^{O_2-O_2} n_{O_2} n_i \right) \\ & \sum_m \sum_{m'} \sum_{i'} \left( Q_{i \rightarrow i'}^{m \rightarrow m'} n_i n_m - Q_{i' \rightarrow i}^{m' \rightarrow m} n_{i'} n_{m'} \right), \quad i = 1 \dots N_v, \end{aligned} \quad (4)$$

where  $K_{i' \rightarrow i}^{O_2-O}$  and  $K_{i \rightarrow i'}^{O_2-O_2}$  are the VT bound-bound transition rates in  $O_2$ - $O$  and  $O_2$ - $O_2$  collisions, respectively,  $Q_{i' \rightarrow i}^{m \rightarrow m'}$  is the VV RC of the reaction  $O_2(m) + O_2(i) \rightarrow O_2(m') + O_2(i')$ , and  $N_v$  is the total number of vibrational states. An implicit method is applied to integrate Eq. (4) with third order accuracy for diagonal and second order accuracy for off-diagonal elements. The initial number density of rovibrational level  $i, j$  is evaluated as follows:

$$n_{i, j}^0 = \frac{Q_{i, j}}{\sum_i Q_{i, j}} n_{O_2}^0, \quad (5)$$

where  $Q_{i, j} = (2j + 1) \exp(-e_{i,0}/kT_v) \times \exp(-(e_{i,j} - e_{i,0})/kT_r)$  is the rovibrational factor of level  $(i, j)$ . The initial number density of vibrational level  $i$  is calculated as a sum of number densities of rotational levels

$j$ , compatible with  $i$ . To reduce influence of statistical error of the QCT method, the principle of detailed balance is invoked to generate rates of exothermic transitions:

$$K_{i,j \rightarrow i',j'} Q_{i,j} = K_{i',j' \rightarrow i,j} Q_{i',j'}. \quad (6)$$

In order to verify the VT and VV rates, the system of master equations is solved assuming only bound-bound transitions in pure molecular oxygen under constant heat bath conditions with temperatures between 1,000 and 30,000 K. The comparison of resulting vibrational relaxation time and the experimental data is provided in section III. In the present work, the vibrational relaxation process is studied for different compositions of O<sub>2</sub> and O mixtures. In order to obtain the vibrational relaxation time in pure molecular oxygen, only terms in the second parentheses and the VV relaxation term in Eq. (4) are considered. The terms in the first parentheses are considered if only the O<sub>2</sub>-O relaxation is of interest. Finally, all terms are taken into account if the relaxation is modeled in the presence of both O<sub>2</sub> and O projectiles.

The master equation in the presence of dissociation and recombination processes has the following appearance:

$$\begin{aligned} \frac{dn_i}{dt} = & \sum_{i' \neq i} \left( K_{i' \rightarrow i}^{O_2-O} n_O n_{i'} - K_{i \rightarrow i'}^{O_2-O} n_O n_i \right) + \sum_{i' \neq i} \left( K_{i' \rightarrow i}^{O_2-O_2} n_{O_2} n_{i'} - K_{i \rightarrow i'}^{O_2-O_2} n_{O_2} n_i \right) + \\ & \sum_m \sum_{m'} \sum_{i'} \left( Q_{i \rightarrow i'}^{m \rightarrow m'} n_m n_i - Q_{i' \rightarrow i}^{m' \rightarrow m} n_{i'} n_{m'} \right) + \\ & R_i^{O_2-O_2} n_{O_2} n_O^2 - D_i^{O_2-O_2} n_{O_2} n_{O_2} + R_i^{O_2-O} n_O^3 - D_i^{O_2-O} n_{O_2} n_O, \quad i = 1 \dots N_\nu \end{aligned} \quad (7)$$

where  $D_i^{O_2-O_2}$ ,  $D_i^{O_2-O}$ ,  $R_i^{O_2-O_2}$  and  $R_i^{O_2-O}$  are the state-specific dissociation and recombination rates in O<sub>2</sub>-O<sub>2</sub> and O<sub>2</sub>-O collisions. The number density of atomic oxygen is given by the following equation:

$$\frac{dn_O}{dt} = \sum_i D_i^{O_2-O_2} n_i n_{O_2} - \sum_i R_i^{O_2-O_2} n_i n_O^2 + \sum_i D_i^{O_2-O} n_i n_O - \sum_i R_i^{O_2-O} n_O^3 \quad (8)$$

The rates of bound-bound and bound-free transitions can be averaged over the range of trans-rotational temperatures, since this type of thermal equilibrium is typically observed in gas flows with temperatures below 10,000 K. The system of master equations that employs rotationally-averaged RCs is termed as the VT model. Otherwise, when a complete set of rovibrationally resolved RCs is utilized, the system of master equations is termed as the RVT model.

### C. State-specific dissociation rates

An important aspect of coupling the dissociation and thermal relaxation processes is the accurate state-specific O<sub>2</sub> dissociation rates in molecule-molecule and molecule-atom collisions. For the latter, accurate data is available for all internal states, obtained via the QCT method [10]. However, a complete database of O<sub>2</sub>-O<sub>2</sub> transition rates is not yet available.

One of possible ways to estimate  $D_i$  in O<sub>2</sub>-O<sub>2</sub> collisions is based on the fact that the dissociation rates in O<sub>2</sub>-O collisions are weakly dependent on the attractive part of the potential energy surface and only affected by its repulsive branch. In [27], two potential energy surfaces were adopted: the first PES was obtained by the summation of the pairwise interactions in the O<sub>2</sub>-O complex, described by the Hulburt-Hirshfelder (HH) potential [28]. The second PES accounted for the three-body interaction [11], in addition to the two-body term, included in the HH PES.

The comparison of these two approaches revealed a very small difference in dissociation rates, which indicates a minor influence of the three-body interaction term. Indeed, the dissociation process occurs at high collisions energies, when colliding particles interact mostly via the repulsive branch of the potential.

Thus, it appears reasonable to scale the accurate SR O<sub>2</sub>-O dissociation RCs in order to obtain the BF transition RCs for the O<sub>2</sub>-O<sub>2</sub> system. In the present work, the scaling factor is calculated as the ratio of the global dissociation RC for atom-diatom and diatom-diatom collisions. The state-specific O<sub>2</sub>-O<sub>2</sub> dissociation RCs are calculated as follows:

$$D_i^{O_2-O_2} = D_i^{O_2-O} \frac{D^{O_2-O_2}}{D^{O_2-O}}, \quad i = 1 \dots N_\nu. \quad (9)$$

Source	$A, cm^3/s$	$B$	$C, K$
Camac, 1961	$5.978 \times 10^{-5}$	-1.00	59415
Johnston, 1968	$4.980 \times 10^{-6}$	-1.00	59500
Bortner, 1969	$1.370 \times 10^{-5}$	-0.83	59400
Park, 1989	$3.320 \times 10^{-3}$	-1.50	59500
Ibraguimova et al., 2003	$1.627 \times 10^1$	-2.50	59380

Table 1: Global dissociation rates in pure oxygen

Several  $O_2$  global dissociation rates were previously reported [29–33]. These data differ by the value of the pre-exponential and temperature dependence factors in the generalized Arrhenius form, shown in Table 1.

Another way to obtain state-specific dissociation rates is based on the Treanor-Marrone model [20]. The state-specific depletion rates are readily obtained by multiplying the global RC of dissociation by a nonequilibrium factor  $Z$ :

$$D_i^{O_2-O_2}(T, e_{v,i}) = Z(T, e_{v,i}) D^{O_2-O_2}(T), \quad (10)$$

where parameter  $Z$  is calculated as follows:

$$Z(T, e_{v,i}) = \frac{Q_v(T)}{Q_v(-U)} \exp\left(\frac{e_{v,i}}{k_B} \left(\frac{1}{T} + \frac{1}{U}\right)\right), \quad (11)$$

where  $Q_v$  is the vibrational partition function, the adjustable parameter  $U$  is referred to as the "characteristic" dissociation temperature and should be chosen according to the best description of available data. A low value of  $U$  corresponds to the situation where quantum effects play an important role in dissociation, while infinite  $U$  means that dissociation is equally probable from any vibrational state. Several empirical values of  $U$ , such as  $D/6k$ ,  $D/3k$  and  $3T$ , have been suggested previously. In the present work a combination of them is chosen by comparing the dissociation rates generated in this way with the available  $O_2$ -O QCT data. Namely, in the present work, the parameter  $U$  is calculated as follows:

$$U = \frac{D_e}{6k} \left(1 - \frac{e_{v,i}}{D_e}\right) + 3T \frac{e_{v,i}}{D_e}, \quad (12)$$

Equation (12) reflects the quantum behavior of the dissociation process for low lying vibrational states at low temperatures and an increase of depletion probability with temperature and for excited states. It was shown previously that the QCT data can be described more accurately using a variable Z-factor [34, 35]. The comparison of  $D_i$  in  $O_2$ -O collisions, obtained from the Treanor-Marrone model with the  $O_2$ -O QCT data is shown in Fig. 1. One can see that the constant value  $U = D/6k$  gives a strong underestimation of rates at high temperatures, where quantum effects are less pronounced. At the same time, the value of  $U = 3T$  gives a strong underestimation of rates at low temperatures, which can be explained by the fact, that the "characteristic" dissociation temperature under these conditions is higher than  $3T$ . The hybrid value of these two values of  $U$ , given by Eq. (12), provides the best description of the  $O_2$ -O QCT data and is used in the present work to obtain the  $O_2$ - $O_2$  state-specific dissociation rates.

The  $O_2$ - $O_2$  state-specific dissociation rates, calculated by means of the Treanor-Marrone model for selected vibrational states from the global rates by Johnston, Park and Ibraguimova, are shown in Fig. 2. While the low-lying states have the conventional behavior of the dissociation RC, the result of the Treanor-Marrone model for highly excited states has a non-physical behavior, suggesting the decrease of dissociation RC at high temperatures. This decrease is larger for the larger absolute value of parameter  $B$  in Table 1. It is interesting to note, that in the work by [34] similar behavior was observed for  $N_2$ -N dissociation rates for  $\nu \geq 60$ , when compared to the results of the QCT method. Apparently, the choice of temperature dependence factor,  $B$ , plays an important role here. Those works, who report the larger absolute value of  $B$ , demonstrate the more significant decrease of  $D_i$  with temperature; this drop can be as large as two orders of magnitude in the temperature range between 1,000 and 10,000 K. In light of this finding, the present work adopts the  $O_2$ - $O_2$  global dissociation RC by [29], which has the smallest absolute value of  $B$  and was originally obtained with an emphasis on hypersonic temperatures. The comparison of scaled rates and those obtained by the Treanor-Marrone model for the  $O_2$ - $O_2$  system is shown in Fig. 3. The Treanor-Marrone

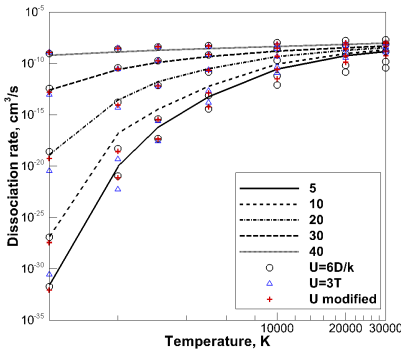


Fig. 1:  $O_2$ -O state-specific dissociation rates, QCT data and Eq. (12)

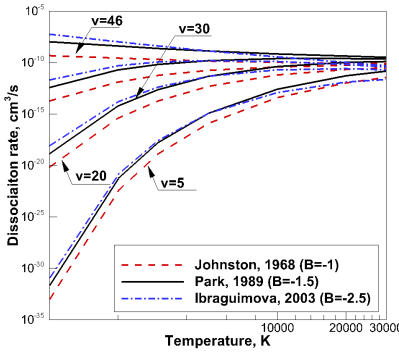


Fig. 2:  $O_2$ - $O_2$  state-specific dissociation rates, Eq. (12)

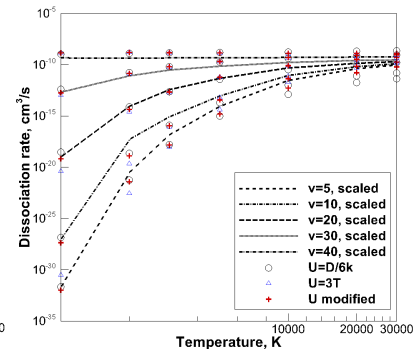


Fig. 3:  $O_2$ - $O_2$  state-specific dissociation rates, Eqs. (12) and (9)

rates, calculated using Eq. (12), again demonstrate the best agreement with the rates obtained by means of the scaling procedure, using Eq. (9).

Finally, it is possible to derive state-specific dissociation RCs from the QCT simulations using the six-dimensional  $O_4$  PES obtained by the double many-body expansion method [36]. Although the complete calculation of RCs for all rovibrational states is expensive, the estimation of rotationally-averaged bound-free RCs appears to be tractable for several selected trans-rotational temperatures. Results of the QCT simulation using the Varandas  $O_4$  PES for trans-rotational temperatures of 6000 and 10,000 K are given in Tables 2 and 3. Calculations are performed for selected low-lying as well for all highly excited vibrational states, since the latter are mainly responsible for dissociation during the QSS phase. The QCT data is compared to the  $O_2(v)$ - $O_2$  BF RCs obtained by means of scaling procedure, Eq. (9) and by means of the Z factor approach, Eq. (11), that adopts the Camac global dissociation RC.

The QCT data for highly excited vibrational states is in good agreement with scaled state-specific RCs, underestimating the scaled RCs by a maximum of 20 %. On the other hand, the RCs obtained by means of the Z factor approach, are somewhat higher than the scaled state-specific RCs. Overall, the QCT and Z-factor RCs are different by a factor of two for vibrational states with  $v > 40$ . The situation for low-lying vibrational states is drastically different. These states are initially responsible for the generation of atomic oxygen immediately behind the shock wave, and their contribution is important under strongly nonequilibrium conditions, as will be shown later. For low vibrational states, the QCT, scaling and Z-factor approaches produce different results. The QCT method gives the highest BF RCs. The scaled RCs are lower than the QCT data by a factor of 2 to 3. The Z-factor approach generates state-specific RCs that are lower by more than an order of magnitude than the scaled RCs. In the present work, both scaled and Z-factor RCs are implemented in calculations, and the corresponding species number density is compared to the experimental data in Section III.E.

Vib. state	QCT, $O_4$ PES	Eq. (9), Camac	Eq. (11), $Z = D_e/6$ , Camac
$v=0$	$6.77 \times 10^{-14}$	$1.49 \times 10^{-14}$	$2.51 \times 10^{-16}$
$v=10$	$1.71 \times 10^{-12}$	$7.48 \times 10^{-13}$	$6.95 \times 10^{-14}$
$v=20$	$3.13 \times 10^{-11}$	$1.65 \times 10^{-11}$	$7.32 \times 10^{-12}$
$v=30$	$2.34 \times 10^{-10}$	$1.74 \times 10^{-10}$	$2.30 \times 10^{-10}$
$v=35$	$4.66 \times 10^{-10}$	$4.18 \times 10^{-10}$	$7.42 \times 10^{-10}$
$v=40$	$7.43 \times 10^{-10}$	$8.04 \times 10^{-10}$	$1.54 \times 10^{-9}$
$v=41$	$7.53 \times 10^{-10}$	$8.87 \times 10^{-10}$	$1.68 \times 10^{-9}$
$v=42$	$1.04 \times 10^{-9}$	$1.19 \times 10^{-9}$	$1.80 \times 10^{-9}$
$v=43$	$1.16 \times 10^{-9}$	$1.36 \times 10^{-9}$	$1.88 \times 10^{-9}$
$v=44$	$1.33 \times 10^{-9}$	$1.64 \times 10^{-9}$	$1.93 \times 10^{-9}$

Table 2: State-specific  $O_2(v)$ - $O_2$  dissociation RCs,  $cm^3/s$ ,  $T = T_r = 6000$  K



Vib. state	QCT, O <sub>4</sub> PES	Eq. (9), Camac	Eq. (11), $Z = D_e/6$ , Camac
v=0	$3.97 \times 10^{-12}$	$1.03 \times 10^{-12}$	$1.27 \times 10^{-14}$
v=10	$2.66 \times 10^{-11}$	$1.13 \times 10^{-11}$	$8.70 \times 10^{-13}$
v=20	$8.47 \times 10^{-11}$	$7.05 \times 10^{-11}$	$2.87 \times 10^{-11}$
v=30	$4.13 \times 10^{-10}$	$2.82 \times 10^{-10}$	$3.81 \times 10^{-10}$
v=35	$6.57 \times 10^{-10}$	$5.14 \times 10^{-10}$	$9.21 \times 10^{-10}$
v=40	$9.05 \times 10^{-10}$	$8.45 \times 10^{-10}$	$1.59 \times 10^{-9}$
v=41	$9.34 \times 10^{-10}$	$9.14 \times 10^{-10}$	$1.70 \times 10^{-9}$
v=42	$1.18 \times 10^{-9}$	$1.18 \times 10^{-9}$	$1.79 \times 10^{-9}$
v=43	$1.25 \times 10^{-9}$	$1.33 \times 10^{-9}$	$1.85 \times 10^{-9}$
v=44	$1.51 \times 10^{-9}$	$1.59 \times 10^{-9}$	$1.89 \times 10^{-9}$

Table 3: State-specific O<sub>2</sub>(*v*)-O<sub>2</sub> dissociation RCs, cm<sup>3</sup>/s,  $T = T_r = 10,000$  K

The thermal equilibrium O<sub>2</sub>-O<sub>2</sub> dissociation RC obtained by the QCT method is shown in Fig. 4 for a temperature range of 5000–10,000 K. This data is obtained by averaging state-specific RCs assuming  $T_v = T_r = T$ . The averaging of RCs over vibrational quantum number leads to the vanishing of differences observed in Table 2. The overall good agreement of the QCT global RC with the experimental data suggests that dissociation proceeds in a similar manner under thermal equilibrium conditions, however this fact has little application to the present study of nonequilibrium processes in shock flows.

#### D. Multi-temperature models

The SR approach becomes prohibitively expensive with increasing number of diatomic species and dimensionality of the problem. Although reduced order models that retain the main features of SR approach have been proposed recently [37], the MT models remain popular due to their simplicity. The solution of master equations provides new insight on parameters that are used in MT models. The present paper addresses the question of efficient utilization of the master equation results. The RVT MT model when formulated for a simple heat bath conditions consist of the following equations

$$\begin{cases} \frac{d}{dt}(\rho e_v) &= \rho_{O_2} \frac{e_v^* - e_v}{\tau_v} + \dot{\omega}_{O_2} C_{DV} D_e, \\ \frac{d}{dt}(\rho e_r) &= \rho_{O_2} \frac{e_r^* - e_r}{\tau_r} + \dot{\omega}_{O_2} C_{DR} D_e, \\ \dot{\omega}_{O_2} &= R(T_a) n_O^2 n_x - D(T_a) n_{O_2} n_x. \end{cases} \quad (13)$$

In Eq. 13,  $e_v$  and  $e_v^*$  are the O<sub>2</sub> vibrational energy evaluated at  $T_v$  and  $T$ , respectively,  $e_r$  and  $e_r^*$  are the O<sub>2</sub> rotational energy evaluated at  $T_r$  and  $T$ , respectively,  $\rho$  and  $\rho_{O_2}$  are the density of the O<sub>2</sub>-O mixture and partial density of O<sub>2</sub>,  $D_e$  is the classical dissociation energy,  $\tau_v$  is the vibrational relaxation time,  $n_x$  is the projectile number density, in this particular case it is atomic oxygen. The global recombination RC,  $R$ , is estimated from  $D$  via the principle of detailed balance. Vibrational energy coupling coefficient,  $C_{DV}$  and  $C_{DR}$  coefficients correspond to the loss of vibrational and rotational energies normalized by the classical dissociation energy.

Vibrational and rotational relaxation times in O<sub>2</sub>-O collisions were recently obtained on the accurate O<sub>3</sub> Varandas PES [10]. One should note that the vibrational relaxation time in the presence of rotational equilibrium is different than that when trans-rotational nonequilibrium is assumed. The latter  $\tau_v$  is lower than the  $\tau_v$  at  $T = T_r$ . This fact is taken into account in the present MT model.

The vibrational relaxation time in O<sub>2</sub>-O<sub>2</sub> collisions was measured experimentally in multiple works [31, 38–41]. In the present work, recommendations on  $\tau_v$  given in [30] are implemented. Because accurate state-specific transition RCs for the O<sub>2</sub>-O<sub>2</sub> system are currently not available, vibrational relaxation times for VT and RVT MT models are assumed to be the same. For the same reason, the O<sub>2</sub>-O<sub>2</sub> rotational relaxation time is derived from the approximation based on the experimental measurements at temperatures between 150 and 1300 K. The experimental data and the present approximation of rotational collisional number is shown in Fig. 5. The compilation of available experimental data is taken from [42].

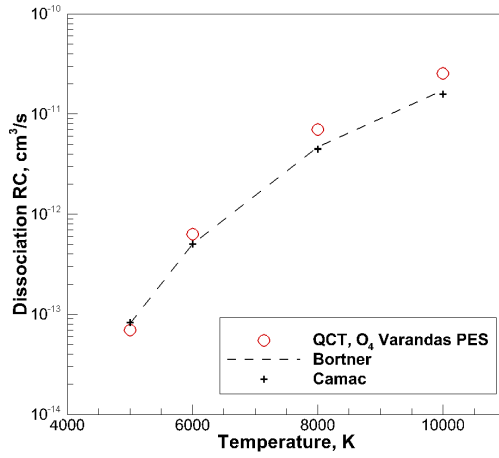


Fig. 4: Thermal equilibrium  $O_2-O_2$  dissociation RC

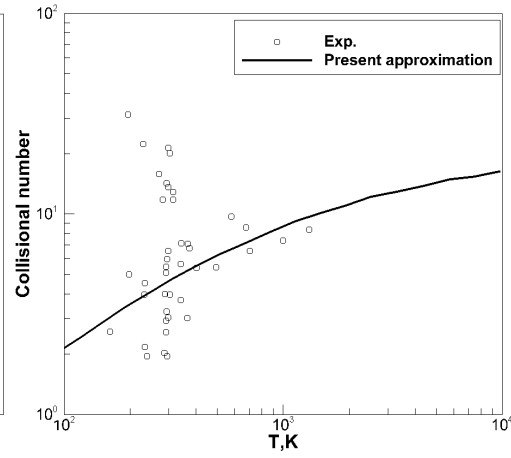


Fig. 5:  $O_2-O_2$  rotational collisional number

One should discuss how the adjustable parameters, namely  $\tau_v$ ,  $\tau_r$ ,  $D$ ,  $C_{DV}$  and  $C_{DR}$ , can be obtained from the system of master equations. The thermal relaxation times, when the complete set of state-specific RCs is available, are obtained by the e-folding method [43]. The dissociation RC, measured in shock tube experiments, should be referred to as the quasi-stationary dissociation RC. Vibrational thermalization at the moment of onset of dissociation is incomplete, and the QSS dissociation RC is lower than the RC estimated at thermal equilibrium conditions. Hence, it is necessary to re-evaluate the QSS dissociation RC as if the vibrational ladder is populated at  $T_v = T$ . According to Ref. [44],  $D^{QSS}$  and  $D^{eq}$  are related through the following empirical relation:

$$D^{QSS} = D^{eq} \frac{T}{T_v} \exp\left(\frac{\tilde{D}}{RT} \left(\frac{1}{T} - \frac{1}{T_v}\right)\right), \quad (14)$$

where parameter  $\tilde{D} = D_e - \beta RT$  describes the average loss of vibrational energy due to dissociation. The recommended range of  $\beta$  is between 1 and 2, in the present work  $\beta$  is set to 3/2.

The average loss of internal energy,  $C_{DV}$  and  $C_{DR}$ , is estimated as a product of the state-specific dissociation and recombination RCs and the instantaneous population of either the vibrational or rotational state [3]. The master equation approach generates time-dependent profiles of  $C_{DV}$  and  $C_{DR}$  that can be used to improve the accuracy of the conventional MT approach in which a constant value of these coefficients is assumed throughout the relaxation process.

For the description of shock tube experimental data, the conservation equations of mass, momentum and total energy must be added to Eq. (13). In the present work, these equations are formulated in the following manner:

$$\begin{cases} \frac{d}{dx}(\rho u) & = 0, \\ \frac{d}{dx}(p + \rho u^2) & = 0, \\ \frac{d}{dx}(h + \rho u^2/2) & = 0, \end{cases} \quad (15)$$

where  $u$  is the mean velocity of the flow,  $p$  is the total pressure,  $h = \sum_s h_{0,s}^f r_s + 2.5RT \sum_s r_s + (e_r + e_v)r_{O_2}$  is the internal enthalpy of the flow,  $s$  is the species index,  $h_{0,s}^f$  and  $r_s$  are the standard formation enthalpy and the molar concentration of species  $s$ . The conversion between time and spatial derivatives in Eqs. (13) and (15) is the following:  $dx = u dt$ . Since the original experimental data in [38] was reported for the laboratory system of coordinates, one needs to convert the time in this system of coordinates into the distance behind the shock wave:  $x = \int V_{sh} dt_L$ , where  $V_{sh}$  is the shock speed,  $t_L$  is the time in the laboratory coordinates system.



### III. Results

#### A. Vibrational relaxation in O<sub>2</sub>-O and O<sub>2</sub>-O<sub>2</sub> collisions

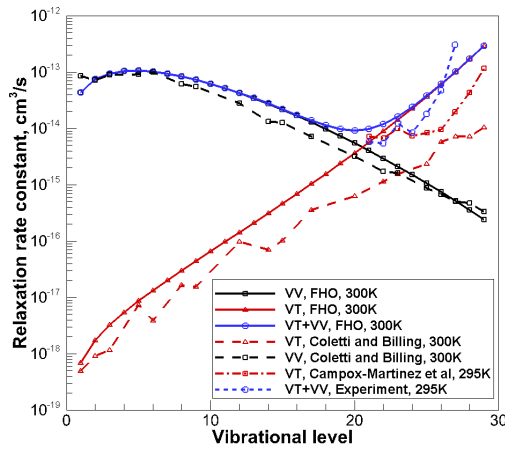
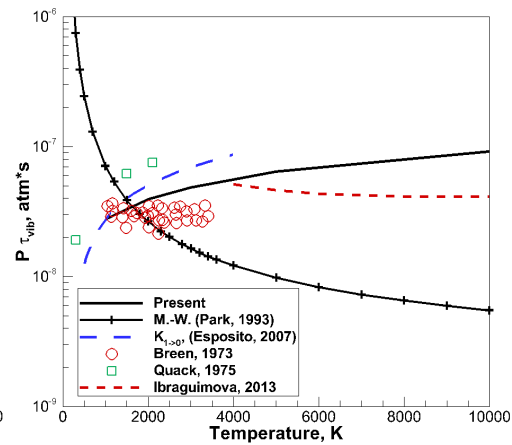
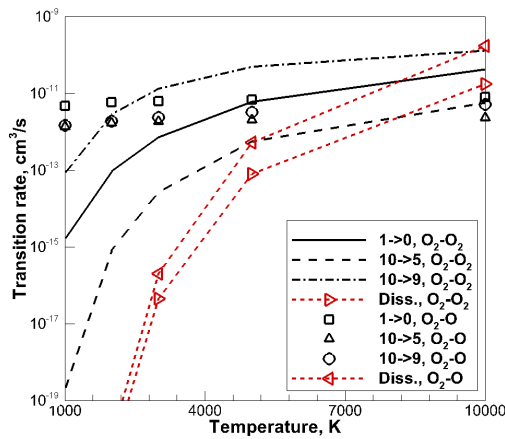
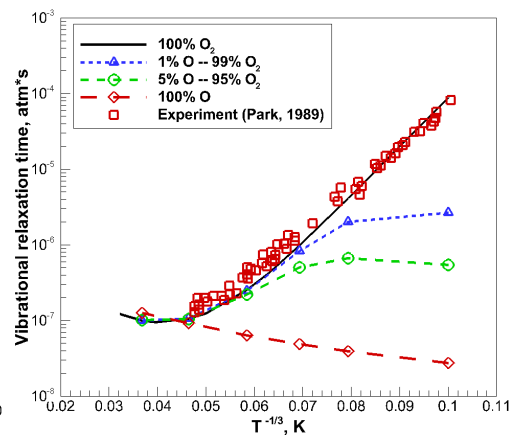
The O<sub>2</sub>-O vibrational relaxation time, previously obtained in [23] from the solution of master equations, is compared to the vibrational relaxation time derived from the monoquantum deactivation RC, reported by [9] and [45] in Fig. 7. The solid line describes the vibrational relaxation time by the VT model. The relaxation time, given by the short dashed line, is taken from experimental work [45]. The long dashed line represents the relaxation time derived from the monoquantum deactivation RC by [46]. The symbolized line represents Park's curve fit to the Millikan-White (MW) equation [39] using the data by [4]. Theoretical calculations by [8] are shown by squares.

The vibrational relaxation time, obtained from the VT thermodynamic model, is in good agreement with the existing experimental data in the range from 1,000 K to 3600 K. The largest difference with Breen et al. data is observed in the high temperature region and is not higher than 15 %. Taking into account the overall uncertainty of shock tube facilities, the agreement with the experimental data is very satisfactory. To the authors' knowledge, other simulations that adopt a master equation, do not exist. The direct extrapolation of experimental data, performed by [30], suggests that the vibrational relaxation of oxygen by the parent atom becomes more efficient with temperature [30]. The present data supports the directly opposite temperature dependence: the vibrational relaxation time becomes smaller at low temperatures. This observation is in agreement with the results by [8]. The relaxation times, reported in [45], provide a good description of vibrational temperature behind shock waves in the range of temperatures from 4000 K to 10800 K. The agreement between results in [45] and those generated by the present VT model is very satisfactory and both results are substantially different from the MW relation. As pointed out in [23], the increase of O<sub>2</sub>-O vibrational relaxation time with temperature is due to the barrierless O<sub>3</sub> PES. The energy randomization in the O<sub>3</sub> complex is especially efficient at low collision energies, while at high temperatures particles interact mostly via the repulsive part of potential.

The large attractive component in the O<sub>3</sub> potential energy surface has significant influence on the rates of mono- and multiquantum transitions as well. The rates of  $v = 1 \rightarrow v' = 0$ ,  $v = 10 \rightarrow v' = 9$  and  $v = 10 \rightarrow v' = 5$  transitions for O<sub>2</sub>-O and O<sub>2</sub>-O<sub>2</sub> are shown in Fig. 8. For reference, the global dissociation RCs are also shown by dashed symbolized lines. While the rates of O<sub>2</sub>-O<sub>2</sub> bound-bound transitions demonstrate a strong temperature dependence, the O<sub>2</sub>-O rates are nearly constant in the considered temperature range. Moreover, the O<sub>2</sub>-O rates of multiquantum transitions are only slightly lower than that of a monoquantum jump. Also, the dissociation RC in collisions with oxygen radical is substantially higher than in O<sub>2</sub>-O<sub>2</sub> and comparable to that of bound-bound transitions, which can be important in high temperature flow with an abundance of oxygen atoms. This subject is investigated in greater detail below.

The accuracy of O<sub>2</sub>-O<sub>2</sub> VT and VV FHO RCs is an important subject in the present work. Unfortunately, rates obtained by trajectory simulation on an accurate PES are not available for temperatures relevant to hypersonic flows. However, the O<sub>4</sub> system was extensively studied at conditions corresponding to atmospheric chemistry [47-49]. The present FHO rates are compared with the available experimental and theoretical data in Fig. 6. Reactions of VT energy transfer (O<sub>2</sub>( $v$ ) + O<sub>2</sub> → O<sub>2</sub>( $v - 1$ ) + O<sub>2</sub>) and VV energy transfer (O<sub>2</sub>( $v$ ) + O<sub>2</sub>(0) → O<sub>2</sub>( $v - 1$ ) + O<sub>2</sub>(1)) are considered. Solid lines describe the present FHO data, long dashed lines correspond to rates by Coletti and Billing [48] and dashed-dotted line presents results by Campo-Martínez et al. [49] Short dashed line gives the total (VT+VV) RC of energy removal based on the experimental measurements by Rogaski et al. [50] The difference in theoretical calculations by Coletti and Billing and Campo-Martínez et al. is first of all due to the O<sub>4</sub> PES adopted for the calculations. The former work used a modified potential surface based on molecular beam experiments [47], where particles behave like rigid rotors. The work by Campo-Martínez et al. used the PES by Varandas, obtained via the DMBE method. Unlike the former PES, the O<sub>4</sub> DBME PES introduces the open reaction channel for ozone formation. This particular fact leads to the appreciable difference in the VV RCs for high  $v$  [48]. The present VV+VT FHO RC has good agreement with the experimental data at  $v > 20$ . For low  $v$ , the agreement of the VT and VV FHO rates with those by Coletti and Billing is satisfactory.

The e-folding O<sub>2</sub>-O<sub>2</sub> vibrational relaxation time is shown in Fig. 9 by the solid black line. The summary of experimental measurements, reflected in [30], is shown by square symbols. The present FHO rates satisfactorily describe the vibrational relaxation time in O<sub>2</sub>-O<sub>2</sub> collisions in the considered temperature range as well as the deviation of relaxation time from the linear dependence at high temperatures due to the breakdown of the Landau-Teller theory.

Fig. 6: VT and VV RCs at  $T = 300$  KFig. 7:  $O_2$ - $O$  vibrational relaxation timeFig. 8:  $O_2$ - $O$  and  $O_2$ -Ar RCs of bound-bound and bound-free transitionsFig. 9: E-folding vibrational relaxation time in various mixtures of  $O_2$  and  $O$  species

The influence of a small concentration of atomic oxygen, admixed with the pure  $O_2$ , on vibrational relaxation time is shown in Fig. 9 with the short-dashed and long-dashed lines that correspond to 1 % and 5% molar fractions of atomic particles. The long-dashed line with diamond symbols corresponds to the vibrational relaxation time in  $O_2$ - $O$  collisions. The presence of even a small concentration of atoms greatly reduces the relaxation time at moderate hypersonic temperatures. This is the direct consequence of the anomalously fast vibrational energy randomization in ozone [8]. As temperature increases, the  $O_2$ - $O$  relaxation becomes less efficient and the average relaxation time in the  $O_2$ - $O$  mixture converges to the conventional MW dependence.

## B. Multiquantum transitions

Existing kinetic theories, such as the FHO model, that are currently used to evaluate the probabilities of mono- and multiquantum transitions, predict the latter to be much smaller compared to that with  $|\Delta v|=1$  at low and moderate temperatures, relevant to hypersonic flow. This result rests on the assumption of a strong repulsion between colliding particles that governs the trans-vibrational energy exchange. The probability of multiquantum transitions increases with temperature, nevertheless, for most practical applications the inclusion of transitions with  $|\Delta v| \leq 5$  is usually enough to perform accurate SR simulations of shock flows [51]. However, because of the large attractive component in the  $O_3$  potential energy surface, the probability of multi- and single quantum jumps in  $O_2$ - $O$  collisions has the same order of magnitude, as can be seen in Fig. 8.

This section investigates the influence of transitions with  $|\Delta v| > 1$  on the process of thermal relaxation.

The variation of the population of the vibrational ladder with time is shown in Figs. 10 and 11 for the cases of heating and cooling flows. The translational temperature is set to a constant value of 3,000 K. The initial vibrational temperature is set to 100 K and 10,000 K, respectively. The simulations are performed using the complete set of SR RCs as well as including transitions with  $|\Delta v| \leq 5, 2$  and 1. The initial concentrations of atoms and molecules is set to  $0.9 \times 10^{18}$  and  $0.1 \times 10^{18} \text{ cm}^{-3}$ . In both cases of heating and cooling flows, the multi-quantum jumps play a significant role in the vibrational relaxation process. For the former, the influence of multi-quantum jumps is more pronounced for the excited vibrational states due to the larger number of open relaxation channels. Specifically, for the lower vibrational states the multi-quantum transitions result in the overpopulation and faster relaxation to equilibrium ( $v=5$  and 10). For highly excited states, the multi-quantum jumps have the opposite effect of faster depopulation ( $v=20$  and 30). The influence of multi-quantum transitions on the relaxation in the expanding flow is large for the entire vibrational ladder. In this case, failure to account for multi-quantum jumps will lead to the underestimation of the population of ground and low-lying states and to the overestimation of the population of highly excited states.

The evolution of vibrational temperature to thermal equilibrium for the considered heat bath conditions is shown in Figs. 12 and 13 for translational temperatures of 3,000 and 10,000 K, respectively. The upper and lower parts of the plot correspond to the cooling and heating flows. Due to the fast vibrational relaxation and relatively slow dissociation at 3,000 K, the QSS state is reached only at the equilibrium temperature. In the case of  $T = 3,000 \text{ K}$  the influence of multi-quantum vibrational jumps is less pronounced in the heating flow due to the low population of excited states. However, for the expanding flow calculations with transitions  $|\Delta v| \leq 5$  lead to a difference compared to those using the complete database. For both types of flows, the difference in the relaxation time and the duration of the QSS state between the full SR approach and the one with  $|\Delta v| = 1$  is approximately one order of magnitude.

The variation of vibrational temperature with time in the case of  $T=10,000 \text{ K}$  has a different pattern. Because in this case dissociation is faster, the nonequilibrium QSS state can be clearly observed in both types of flows. The QSS vibrational temperature and the duration of the QSS phase are similar for heating and shock flows. Since the initial concentration of atomic oxygen, set to  $0.9 \times 10^{18} \text{ cm}^{-3}$ , is less than that in equilibrium, the QSS state is accompanied by strong dissociation, which leads to a drop of vibrational temperature below the translational one for the cooling flow, as can be seen in Fig. 13. Accounting for multi-quantum jumps leads to a higher vibrational temperature and a shorter duration of the QSS phase.

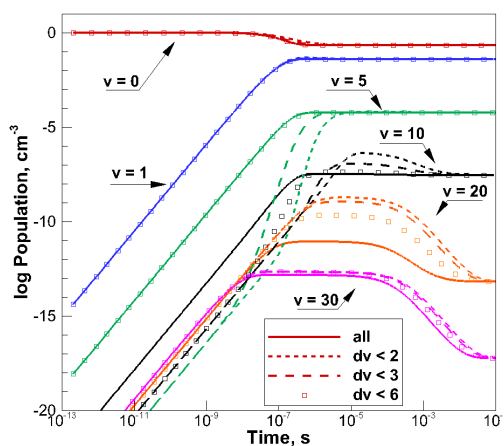


Fig. 10: Variation of the population of the vibrational ladder with time at  $T=3,000 \text{ K}$ , heating flow

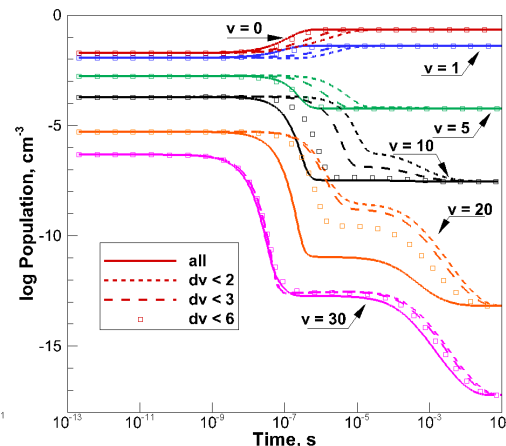


Fig. 11: Variation of the population of the vibrational ladder with time at  $T=3,000 \text{ K}$ , cooling flow

### C. Dissociation

Experimental measurements of dissociation rates in nitrogen [52] and oxygen [53] indicate that the depletion of gas proceeds more efficiently in the parent atom-diatom rather than in the diatom-diatom collisions. As pointed out in [54], one of the reasons for this is a "scrambling" effect of pre-collisional vibrational states

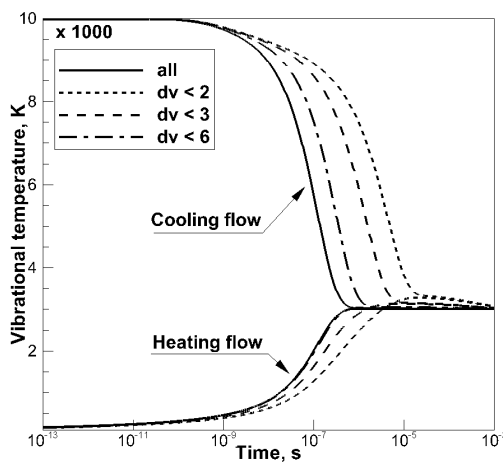


Fig. 12: Evolution of vibrational temperature with time under heating and cooling conditions,  $T=3,000$  K,  $T_v^0=100$  and  $10,000$  K

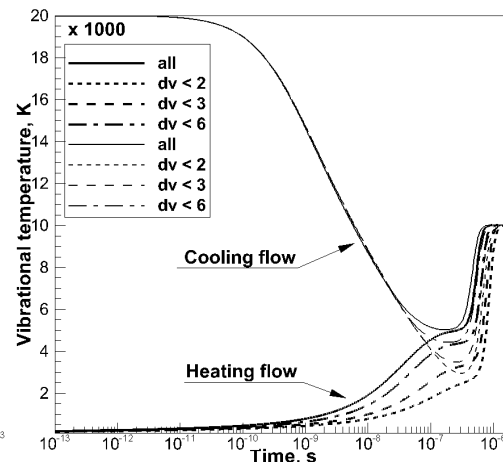


Fig. 13: Evolution of vibrational temperature with time under heating and cooling conditions,  $T=10,000$  K,  $T_v^0=100$  and  $20,000$  K

that takes place during the exchange reaction in  $N_2-N$  collisions. Because the insertion mechanism in the  $N_2-N$  system is more efficient than that in  $N_2-N_2$ , the former implicitly affects the populations of higher vibrational states that ultimately lead to dissociation.

It was recently shown [23] that the exchange reaction has a large impact on the energy randomization in the  $O_3$  complex at collisions energies below 1 eV. Furthermore, the exchange mechanism is responsible for the large multiquantum jumps during the vibrationally inelastic collisions. Taking these facts into account, one can expect a large influence of oxygen radicals on not only the vibrational relaxation but also on the duration of the QSS phase. Presently adopted  $O_2-O$  and  $O_2-O_2$  dissociation rates support the conclusions, made in [54]: the ratio of  $D^{O_2-O}$  and  $D^{O_2-O_2}$  is equal to 3.90 at  $T=2,000$  K, increasing up to 9.43 at  $T=10,000$  K. Thus, it is important to accurately model the amount of oxygen atoms in the flow and the population of the vibrational ladder prior to the QSS regime.

The evolution of vibrational temperature and species concentration with time is shown in Figs. 14 and 15 when only  $O_2-O$  and  $O_2-O_2$  collisions are considered, respectively. In both cases the initial  $T_v$  is set to 100 K, and translational temperature is set to a constant in the range of 2,000 to 30,000 K. In the case of only atom-diatom collisions, the vibrational relaxation occurs mostly prior to the QSS phase at temperatures below 5,000 K, and the dissociation takes place from the vibrational ladder, populated at a nearly equilibrium temperature. As temperature increases further, the dissociation becomes faster, and the vibrational temperature during the QSS phase starts to deviate from the equilibrium value. Now, because the  $O_2-O$  vibrational relaxation time increases with temperature, unlike in  $O_2-O_2$  collisions, and the dissociation rates follow the conventional Arrhenius form, the further increase of translational temperature does not lead to an increase of vibrational temperature during the QSS phase. The plateau, that is typically observed at low temperatures, is shorter and smeared. In other words, the increase of vibrational relaxation time with temperature in  $O_2-O$  collisions has a limiting effect on vibrational temperature during the QSS phase. One should use this observation with caution, because electronic excitation, that appears to be an additional channel of  $O_2-O$  collisions at high temperatures, is not included in the derivation of the present vibrational relaxation time.

Solutions of the master equations when only diatom-diatom collisions are considered are shown in Fig. 15. In contrast to the case with  $O_2-O$  relaxation, the vibrational temperature during the QSS phase increases monotonically in the considered interval of translational temperatures. The dissociation at temperatures not exceeding 5000 K occurs only after the vibrational relaxation is complete. This is true for both  $O_2$  and  $O$  heat bath conditions. At higher temperatures, the depletion of molecules may occur prior to thermalization of the vibrational mode. At  $T=10,000$  K nearly 20 % of  $O_2$  is depleted in the case of a molecular heat bath. Under the same conditions of an atomic heat bath, the increase of  $n_O$  is comparable with that of the equilibrium composition. This is due to the faster dissociation in  $O_2-O$  collisions compared to the pure  $O_2$

case. The separation of the QSS and relaxation phases is justified for the  $O_2-O$  system only at temperatures lower than 10,000 K.

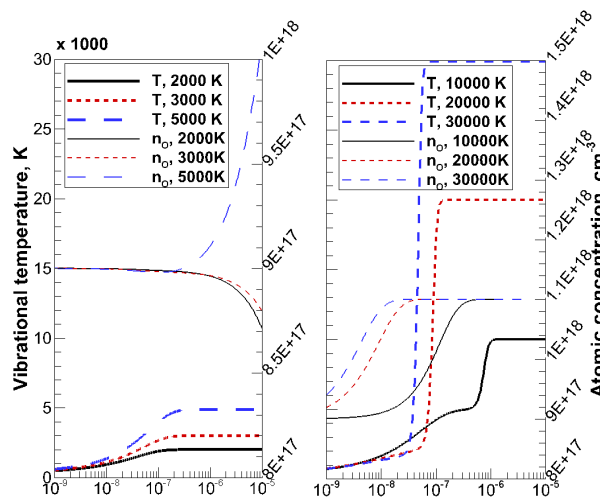


Fig. 14: Evolution of  $T_v$  and  $n_O$  with time, heat bath of oxygen atoms

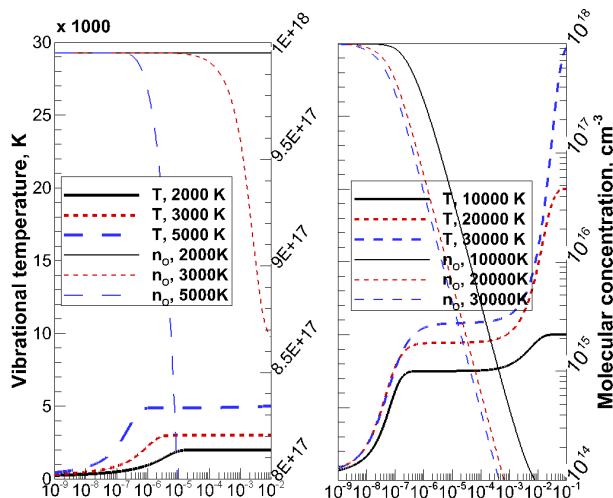


Fig. 15: Evolution of  $T_v$  and  $n_{O_2}$  with time, heat bath of oxygen molecules

The recombination process can be important in the nozzle flow with  $T_v > T$  when the atomic concentration substantially exceeds the equilibrium composition. Because the population of the vibrational ladder exhibits a strongly non-Boltzmann dependence, the global rates of chemical reactions have a non-Arrhenius behavior. The multi-temperature model [30], popular due to its simplicity, is inadequate for describing the chemical composition in rapidly expanding flows for this reason. The system of master equations, coupled to the accurate rates of energy exchange in  $O_2-O_2$  and  $O_2-O$  collisions, is an accurate tool for studying nonequilibrium kinetics in a strongly recombinative flow.

In the present paper, the nozzle flow kinetics is simulated at two initial vibrational temperatures of 3000 and 5000 K and at a fixed translational temperature of 1000 K. The initial molar fraction of atomic oxygen is set to 0.9. The evolution of vibrational population with time is shown in Fig. 16. In the case of lower  $T_v^0$ , the initial phase of thermal relaxation can be characterized by the formation of a long plateau above the initial distribution. This mechanism is attributed to a selective recombination to higher vibrational states. Because the excited states are strongly overpopulated, it is preferable to describe the rates of chemical transformation in terms of the population of the last vibrational state [18]. The lower vibrational states initially maintain a nearly constant population, while the extensive energy exchange takes place. For this reason, the dissociation RC, described by the vibrational temperature, would give misleading results in these simulations. The depopulation of lower states occurs only at the late stage of relaxation when the vibrational temperature of the system converges to the equilibrium value. It is worth to note that at stronger nonequilibrium conditions,  $T_v^0 = 5000$  K, the up pumping of excited states does not occur, since those states are already densely populated. The formation of a plateau can be achieved by increasing the initial concentration of oxygen atoms.

#### D. Simulation of heat bath conditions

Due to the high cost of the SR approach there is a potential interest to use the information about nonequilibrium populations and state-specific rates in order to improve the accuracy of the simple and efficient MT approach. In the present work, the solution from the SR and MT models are compared side-by-side for ideal heat bath of oxygen at translational temperatures of 5000, 8000, 10,000 and 14,000 K. There are three primary parameters that can be adjusted in order to fit the solution of the MT approach to that of the SR method. Namely, these are the vibrational relaxation time, dissociation RC and the average loss of internal energy due to dissociation. It was shown recently [10] that the  $O_2-O$  e-folding relaxation time accurately describes the evolution of vibrational energy when incorporated in the Landau-Teller (LT) equation. Therefore, it is decided to keep the LT term and vibrational relaxation time unadjusted.

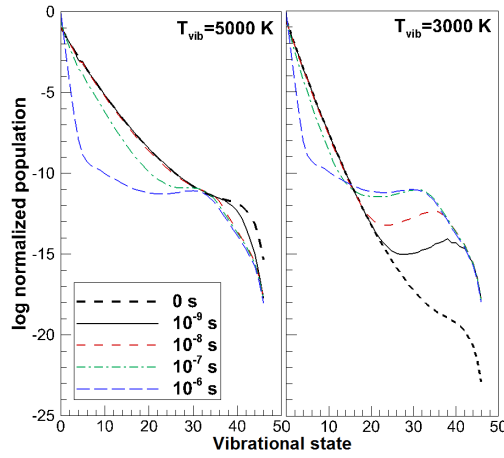


Fig. 16: Population of vibrational ladder in recombinative flow

The appropriate adjustment of dissociation RC and vibration-dissociation coupling parameter should be based on the temporal evolution of these parameters during thermalization. The dissociation RC and the vibration-dissociation coupling parameter are shown for considered heat bath conditions in Figs. 17 and 18. In Fig. 17, the symboled lines correspond to the instantaneous RC computed as the ratio of difference in the O<sub>2</sub> number density and the time step, dashed lines correspond to  $D^{QSS}$ . At low temperatures, the maximum of the instantaneous RC corresponds to the plateau at the QSS level. At higher temperatures, the QSS assumption breaks down and the QSS RC is bounded by some minimal and maximal values of instantaneous RC, shifting toward the lower bound with increasing temperature. In fact, the differences between minimum and maximum of instantaneous RC becomes smaller at higher temperatures. One should note that little to no dissociation occurs at low temperatures, hence it will be appropriate to assume the effective dissociation RC equal to QSS RC at these conditions. At higher temperatures, the dissociation occurs simultaneously with thermal relaxation, hence again, it will be accurate to assume the QSS RC as the replacement for the actual dissociation RC. The most pronounced inaccuracy in the modified MT model will be observed for intermediate temperatures.

Figure 18 illustrates that it is incorrect to assume a constant  $C_{DV}$  throughout the entire relaxation process. In fact, this coupling parameter has initially a very small value reaching a nearly constant level during the QSS phase and *thereafter*. For the sake of simplicity, a linear dependence of  $C_{DV}$  on  $T_v$  can be proposed:

$$C_{DV} = C_{DV}^{QSS} \times \min\left(\frac{T_v}{T_v^{QSS}}, 1\right), \quad (16)$$

where  $C_{DV}^{QSS}$  and  $T_v^{QSS}$  are the vibration-dissociation coupling parameter and vibrational temperature during the QSS phase [10, 38]. The comparison of SR and modified MT approaches is shown in Fig. 19 for translational temperatures of 5000, 8000, 10,000 and 14,000 K. The adjusted MT approach performs very adequately, compared to the unadjusted MT model, presented in Ref. [10]. As expected, the least successful agreement is observed for moderate temperatures.

## E. 1D shock flow simulation

Measurements of vibrational temperature of shock-heated oxygen was recently reported in the work by Ibraguimova et al. [38]. In these experiments, the absorption of laser radiation in O<sub>2</sub> Schumann-Runge bands was reported. The attenuation of radiation was analyzed using Beer's law and the tabulated absorption coefficients. The latter depends on vibrational and translational temperatures of the gas media and can be utilized specifically for the analysis of thermal nonequilibrium flows. By judging the amount of absorbed radiation, the O<sub>2</sub> vibrational temperature was derived in the range of translational temperatures between 4000 and 10800 K. The present work attempts to describe the results by Ibraguimova by utilizing the two- and three-temperature as well as the SR models of nonequilibrium shock flows.



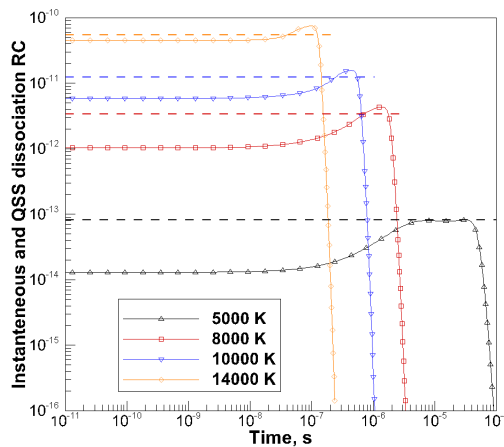


Fig. 17: O<sub>2</sub>-O instantaneous and QSS dissociation RCs

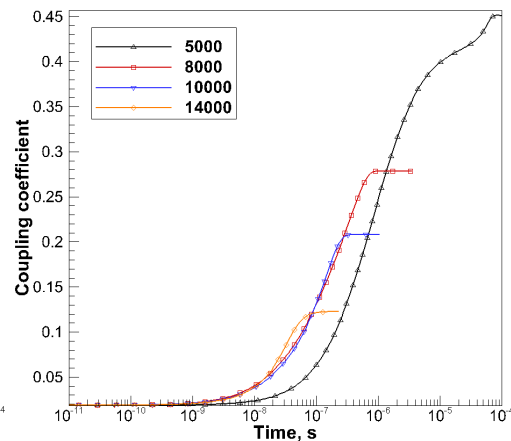


Fig. 18: O<sub>2</sub>-O vibration-dissociation coupling parameter

A summary of the available experimental data is shown in Table 5. In the present work, six cases with different ambient pressure and shock velocity are studied. The pressure before the shock wave varies between 2 torr for mild nonequilibrium conditions and 0.8 torr for the strongest nonequilibrium experimental run. The velocity in the test runs varies from 3.07 to 4.44 km/s. Both measurements of translational and vibrational temperatures are available except the first, C1, case. For two cases with the strongest shock wave, the mass fraction of atomic oxygen is also reported.

The present work describes the experimental data by comparing the SR and multi-temperature models side-by-side for each case. Three variations of MT models are studied. The simplest one assumes the presence of trans-rotational equilibrium and adopts the Park vibrational relaxation times and dissociation RCs for O<sub>2</sub>-O and O<sub>2</sub>-O<sub>2</sub> collisions in the manner proposed in [30]. The Park model of governing temperature  $T_a = \sqrt{TT_v}$  is used to simulate the effect of vibrational nonequilibrium on the dissociation RC. The Park correction of  $\tau_v$  is used to modify the O<sub>2</sub>-O<sub>2</sub> relaxation time, while O<sub>2</sub>-O  $\tau_v$  remains unchanged.

The modified VT MT model employs the QSS dissociation RC estimated at the translational temperature of the flow. The justification of such an approach to model nonequilibrium dissociation is given in the previous section. Additionally, the QCT O<sub>2</sub>-O  $\tau_v$  is adopted by the VT MT QSS model. This MT model assumes the presence of trans-rotational equilibrium as well.

The highest fidelity MT RVT QSS model, allows for rotational nonequilibrium and employs the RVT QSS O<sub>2</sub>-O dissociation RC for describing the depletion in O<sub>2</sub>-O collisions. A summary of the MT models is given in Table 4. To model rotational nonequilibrium,  $\tau_r$  in O<sub>2</sub>-O collisions is taken from the QCT calculations presented in [10]. The O<sub>2</sub>-O<sub>2</sub> rotational relaxation time is calculated from the approximation of experimental data on rotational collisional number, shown in Fig. 5.

Model	O <sub>2</sub> -O $\tau_v$	O <sub>2</sub> -O <sub>2</sub> $\tau_v$	O <sub>2</sub> -O $\tau_r$	O <sub>2</sub> -O <sub>2</sub> $\tau_r$	O <sub>2</sub> -O Diss.	O <sub>2</sub> -O <sub>2</sub> Diss.	Noneq. coupling
MT VT Park	MW, [30]	MW, [30]	N/A	N/A	[30]	[30]	$T_a = \sqrt{TT_v}$ , [30]
MT VT QSS	VT QCT	MW, [30]	N/A	N/A	VT QSS RC	[30]	VT QSS RC
MT RVT QSS	RVT QCT	MW, [30]	RVT QCT	Fig. 5	RVT QSS RC	[30]	RVT QSS RC

Table 4: Parameters of MT models

The SR models apply the FHO O<sub>2</sub>-O<sub>2</sub> vibration-to-translation RCs, described in Section II. The O<sub>2</sub>-O<sub>2</sub> dissociation RCs are obtained by means of the scaling procedure as well as applying the nonequilibrium factor  $Z$  given by Eq. 11. The comparison of vibrational and translational temperatures with the experimental data is performed using only O<sub>2</sub>-O<sub>2</sub> dissociation RCs derived from the Z-factor approach. The species number density in C5 and C6 cases are computed using both scaled and Z-factor O<sub>2</sub>-O<sub>2</sub> dissociation RCs.

The comparison with the experimental data starts from the case with the mildest shock. The distribution of translational, vibrational and rotational temperatures is shown in Figs. 20a-20b for case C1. The SR approach accurately captures the vibrational temperature prior to the dissociation as well as the point where

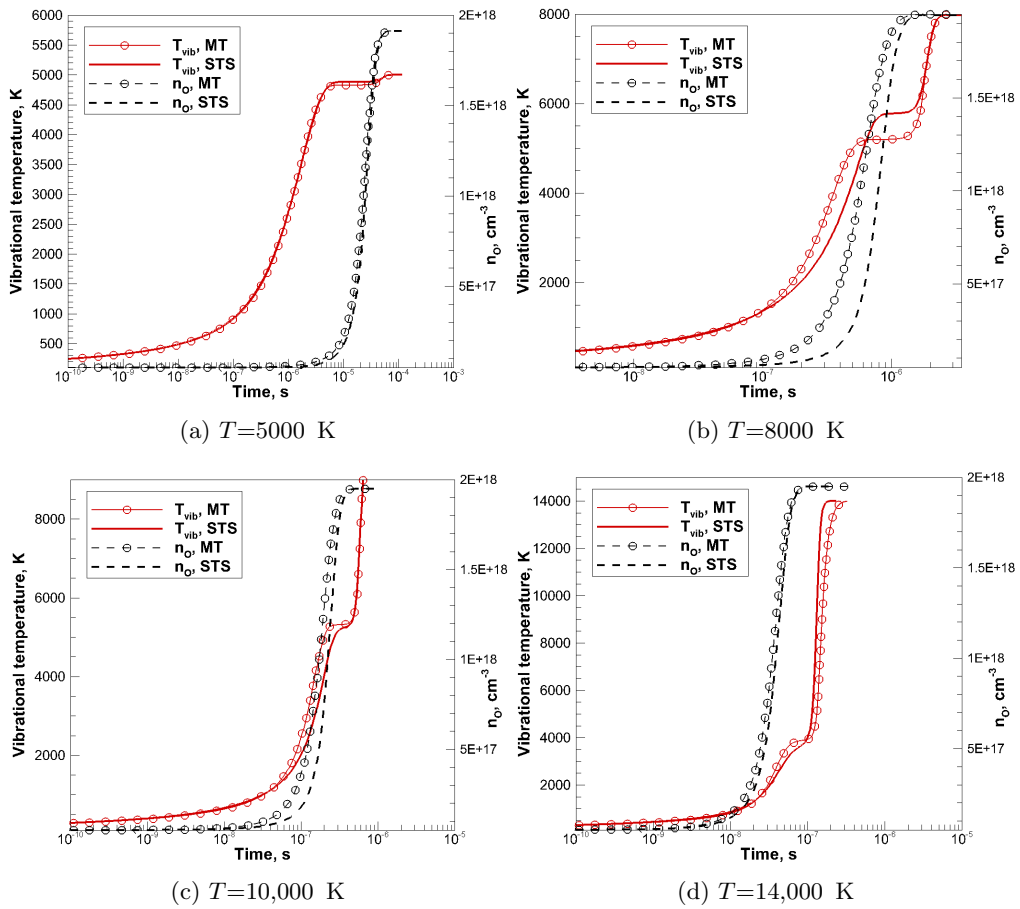


Fig. 19: Comparison of SR and modified MT approaches

Case	Pressure, torr	Velocity, km/s	Available $T$ ?	Available $T_v$ ?	Available $Y_O$ ?
C1	2.0	3.07	–	Yes	–
C2	1.0	3.40	Yes	Yes	–
C3	1.0	3.95	Yes	Yes	–
C4	1.0	4.132	Yes	Yes	–
C5	1.0	4.35	Yes	Yes	Yes
C6	0.8	4.44	Yes	Yes	Yes

Table 5: Summary of shock tube experiments [38]

$T$  becomes equal to  $T_v$ . There is a subtle overestimation of the slope of  $T_v$  during the onset of dissociation by the SR model. This can be related to the uncertainty in  $O_2$ – $O_2$  state-specific dissociation RCs. The MT VT and RVT QSS models satisfactorily describe the vibrational relaxation phase, however the maximum of vibrational temperature is predicted less accurately than in the SR model. This is explained by the fact that the actual dissociation RC is smaller than the QSS RC prior to the phase of active dissociation, as follows from Fig. 17. The effect of rotational nonequilibrium is minimal at these translational temperatures.

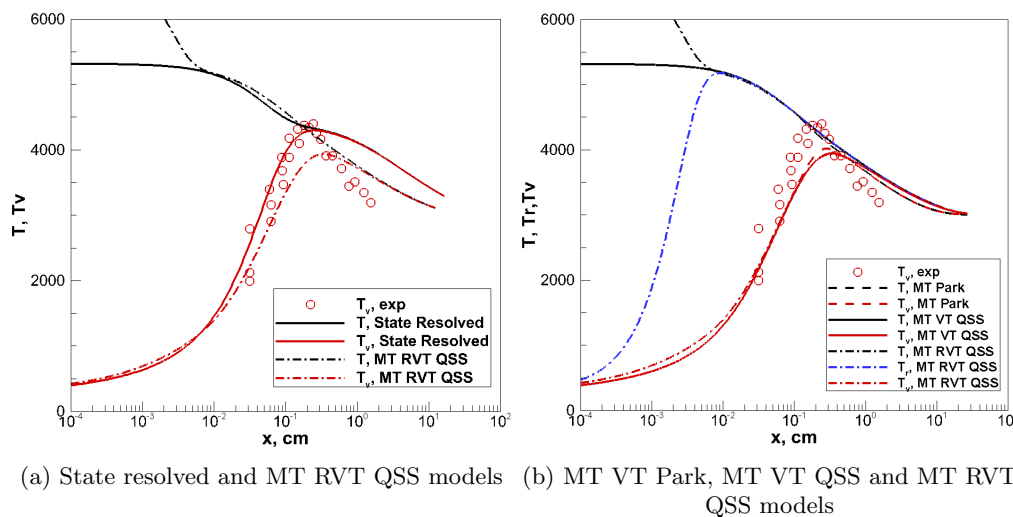


Fig. 20: Translational, vibrational and rotational temperatures, C1

The results for the C2 - C4 cases, shown in Figs. 21a–23b, indicate that the SR approach is more accurate in describing the vibrational and translational temperatures than any of the MT models. This includes the description of vibrational and translational temperatures prior to the active dissociation, the peak of vibrational temperature and the width of vibrational nonequilibrium zone. The application of the QSS dissociation RC as the model of vibrational-dissociation coupling improves the agreement of vibrational temperature in MT QSS models compared to the MT VT Park model. The latter model appreciably underestimates the actual vibrational temperature during coupled vibration and dissociation thermalization.

Finally, for the strongly nonequilibrium C5–C6 cases, shown in Figs. 24a–25b, the SR approach demonstrates significantly more accurate prediction of post-shock vibrational and translational temperatures, compared to the Park MT model. These two cases can be characterized by a certain degree of rotational nonequilibrium. The rotational mode reaches equilibrium only two times faster than the vibrational mode. The trans-rotational nonequilibrium results in an increase of vibrational temperature in the zone of rotational nonequilibrium. This is explained by a lower QSS RC used in the RVT QSS model compared to that in the VT QSS model.

The accuracy of the considered models can also be assessed by comparing the mass fraction of atomic oxygen with the experimental data, as shown in Figs. 26a and 26b for the C5 and C6 cases, respectively. The black solid and dashed lines correspond to the SR model with  $O_2$ – $O_2$  dissociation RCs using nonequilibrium

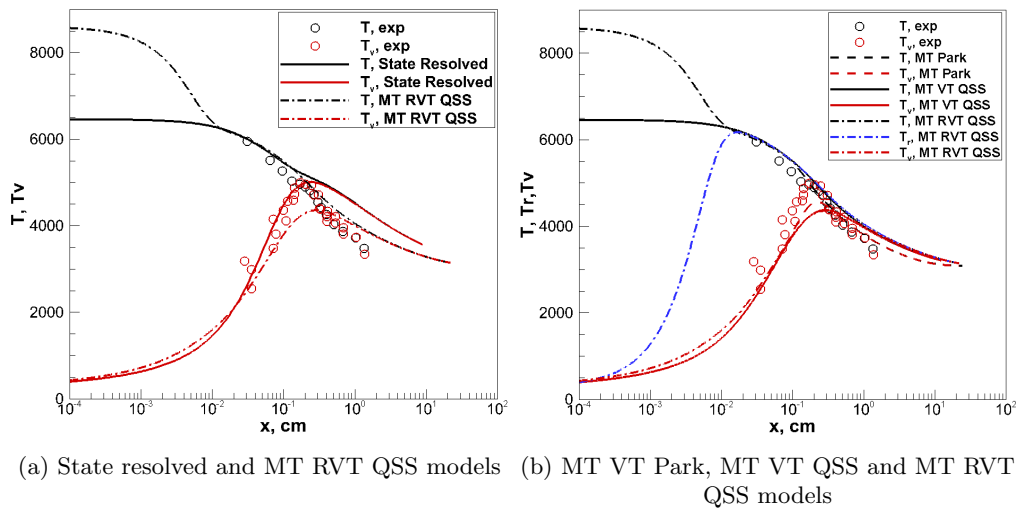


Fig. 21: Translational, vibrational and rotational temperatures, C2

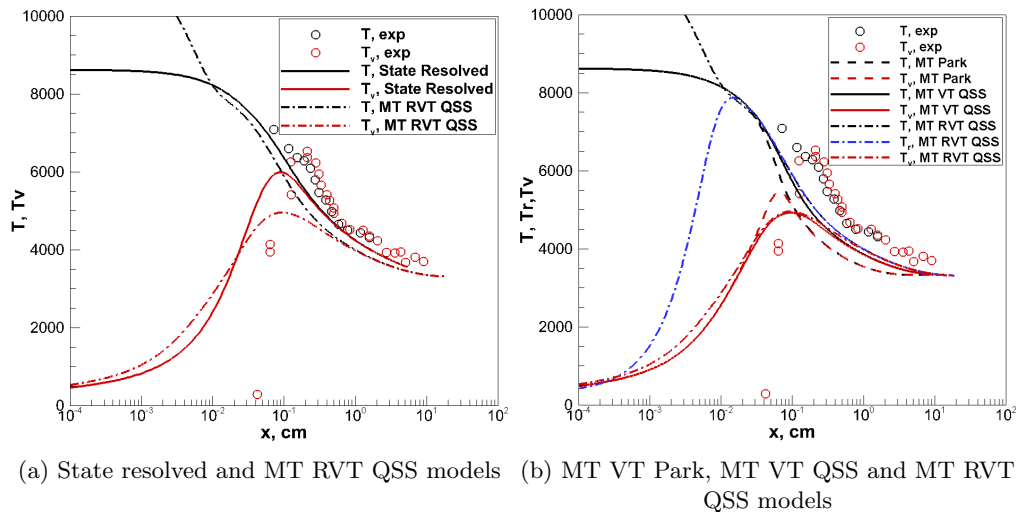


Fig. 22: Translational, vibrational and rotational temperatures, C3

factor  $Z$  and scaling methods, respectively. It can be clearly seen that the approach based on the variable nonequilibrium factor produces a much slower accumulation of atomic oxygen compared to the approach with a constant scaling factor. This confirms the observation that immediately behind the shock wave the low lying vibrational states are responsible for initial generation of atomic oxygen. Because the  $Z$ -factor approach results in much lower  $O_2$ - $O_2$  bound-free RCs for  $v < 10$  compared to other methods, this set of BF RCs gives the best agreement with the experimental data for the C5 and C6 cases. It is interesting to note that the implementation of the QSS VT and QSS RVT dissociation RCs provides a fairly good agreement between the MT model and the experimental data as well.

The vibrational temperature observed prior to the onset of dissociation (i.e. the maximum of  $T_v$ ) is shown in Fig. 27. The horizontal scale corresponds to the maximum of translational temperature, measured immediately after the shock wave arrives at the optical station. In the entire range of nonequilibrium conditions, the present SR model accurately predicts the maximum of vibrational temperature. The leveling-off of  $T_v$  at strongly nonequilibrium conditions is captured as well. Unlike the SR model, the MT model underestimates the maximum of vibrational temperature. This observation is related to the fact that the governing temperature  $T_a$ , implemented in the MT VT Park model does not describe the population of

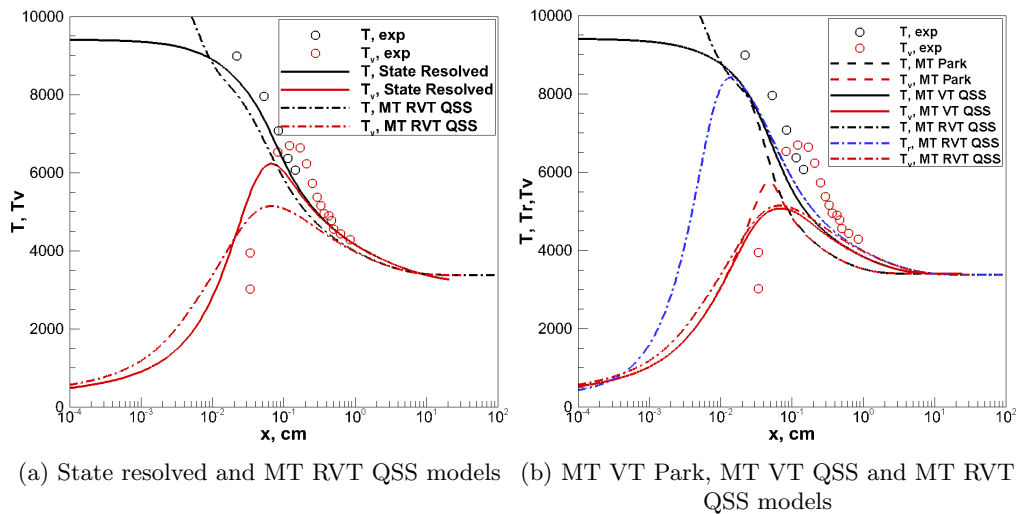


Fig. 23: Translational, vibrational and rotational temperatures, C4

excited vibrational states, which is typically lower than the distribution of the vibrational ladder at thermal equilibrium conditions. Despite the good accuracy of the SR approach, it is highly desired in the future to repeat the present calculations with a complete set of  $O_2(v)-O_2$  RCs generated on an accurate  $O_4$  PES.

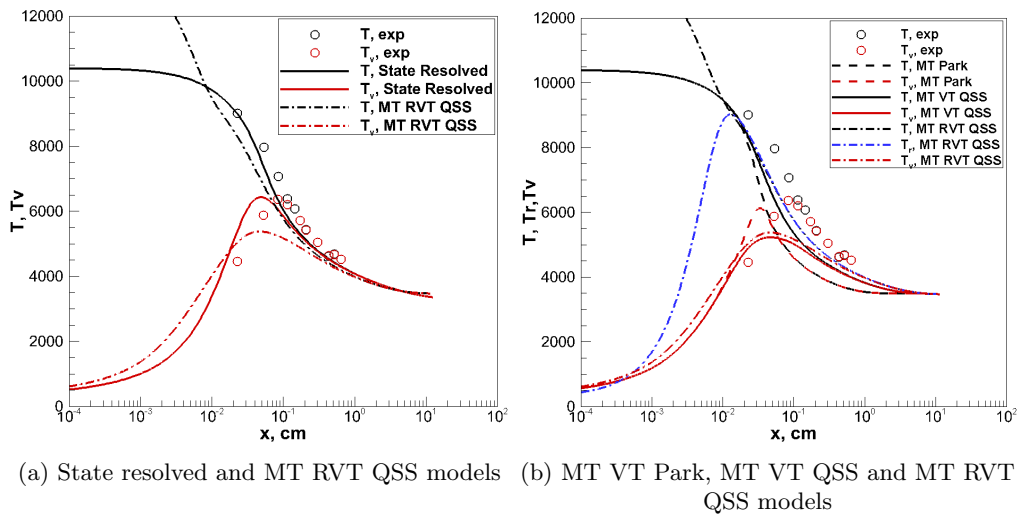


Fig. 24: Translational, vibrational and rotational temperatures, C5

## IV. Conclusion

Thermal relaxation and dissociation of molecular oxygen is studied by means of master equations and 1D shock flow in the presence of atom-molecule and bimolecular collisions. Accurate bound-bound and bound-free transition rates, generated by the QCT method, are adopted to model the  $O_2-O$  interaction. The FHO model is used to generate the VT and VV bimolecular relaxation rates. Both QCT and empirical approaches are used to obtain state-specific  $O_2(v)-O_2$  dissociation RCs.

A strong dependence of vibrational relaxation time in the  $O_2-O$  mixture on the amount of atomic oxygen in the gas mixture is observed. The average relaxation time in the presence of a small (1-5% molar fraction) amount of oxygen atoms is several orders of magnitude lower than in pure oxygen at temperatures below 3,000 K. As temperature increases, this difference becomes smaller.

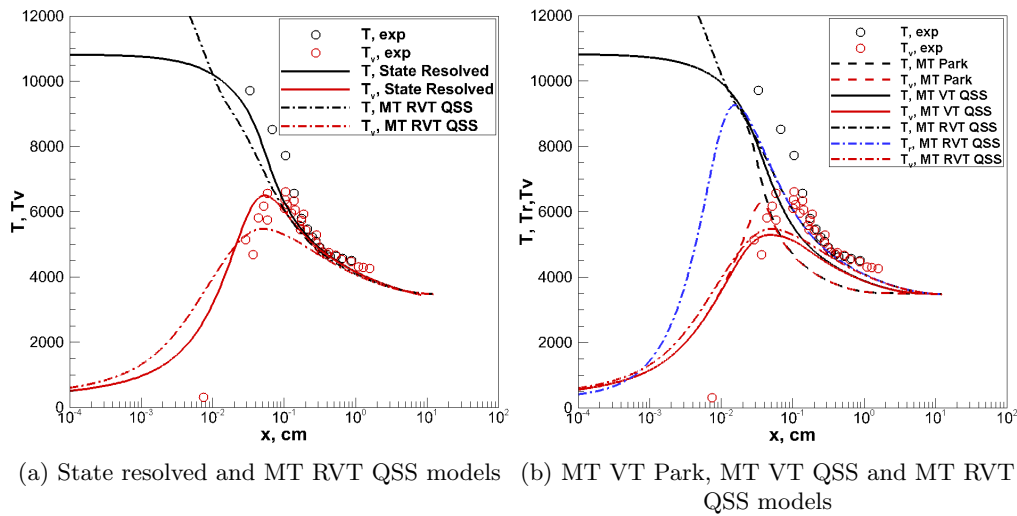


Fig. 25: Translational, vibrational and rotational temperatures, C6

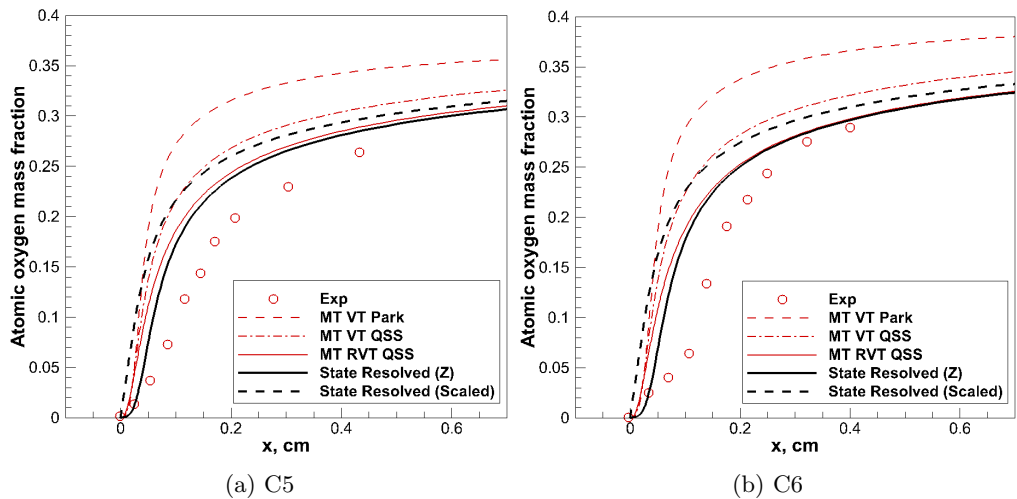


Fig. 26: Mass fraction of atomic oxygen

The efficient energy randomization in  $O_2-O$  collisions causes a strong over- and underpopulation of highly-excited vibrational states in heating and cooling flows, respectively. Moreover, the state-resolved populations are strongly defined by the multiquantum transitions. In the case of cooling flow, the multiquantum jumps noticeably affect even the population of the ground state. Failure to account for all possible transitions that take place during  $O_2-O$  collisions may lead to a strong overestimation of relaxation time in the gas mixture.

The present paper focuses on the accuracy of the multi-temperature models by implementing the newly generated QCT and master equation parameters in the low fidelity thermochemistry models. The study of heat bath conditions indicates that the  $O_2-O$  QSS dissociation RCs improves the accuracy of the MT model when implemented as the governing RCs without the traditional coupling of the translational and vibrational modes. At lower temperatures this approach is augmented by the fact that there is no to little dissociation prior to the QSS phase. At high temperatures, although there is a noticeable depletion at the early stage of relaxation, the instantaneous dissociation RCs change insignificantly and the constant QSS RC is well suited for describing the dissociation process.

Finally, a three temperature model is introduced for describing shock flows at translational temperatures between 4000 and 11000 K and compared to the state-resolved model and to the experimental data. Similarly to the simulations of heat bath conditions, the implementation of the QSS dissociation RCs leads to an



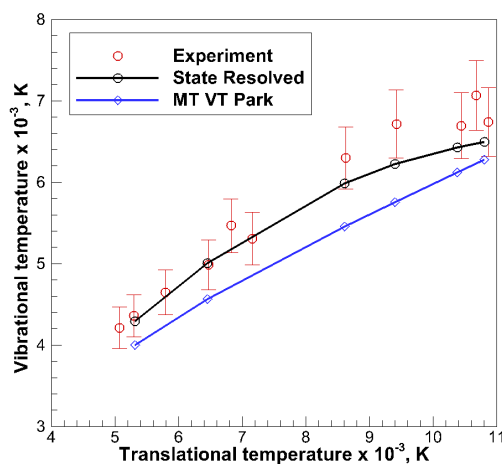


Fig. 27: Maximum of vibrational temperature behind the shock wave

improvement in the accuracy of the MT model, judging by the agreement of temperatures and species concentrations with the experimental data. However, due to unavailability of accurate  $O_2$ – $O_2$  RCs, the state-resolved models still appears to be more accurate. The state-specific  $O_2(v)$ – $O_2$  dissociation RCs are important in describing the atomic oxygen number density under strongly nonequilibrium conditions. The empirical estimation of these coefficients using the nonequilibrium factor  $Z$  appears to be more accurate than the scaling procedure that is based on the  $O_2$ – $O$  QCT data.

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