- 1 Supplementary Materials
- 2

### 3 Site descriptions

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5 Site maps, photographs and more detailed site descriptions can be found in Von
6 Voigtlander (2016).

7

8 Road Cut sites are along Highway 270. The east site Road Cut (east and west) 9 was located directly above the section interpreted by Goodfellow et al., (2013), and the 10 Road Cut west site is located across Highway 270 from the east site. Both locations 11 host sparse vegetation including small trees and grasses and have a MAP of 500 m/yr (Giambelluca et al., 2013). Two P-wave lines were run with 3 and 1 meter spacing on 12 13 top of a 4.2 m tall road cut at an elevation of 78 m above sea level. One P-wave line 14 with 3 meter spacing was run on the Road Cut West site on top of a 3 m high at the 15 road cut. One S-wave line was run with 1 meter spacing on the east site. The S-wave 16 lines, and the P-wave lines, share a centerline. The S-wave line was translated by one 17 sensor spacing (1 m) in the array direction six times for developing the 2D S-wave 18 profile. This resulted in a total survey line length of 21. A source offset distance of 3 m 19 was used.

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Sapphire Cove The Sapphire Cove lies 3.2 km north of the Road Cut
location at an elevation of 8 m, 30 m from the shoreline and receives 500 mm/yr MAP
(Giambelluca et al., 2013). Two P-wave surveys were performed here with 1 m (line 1)

and 2.5 m (line 2). The survey line 2 was run parallel to the ocean and perpendicular to
line 1. Like the Road Cut site, core stones were visible at the ground surface and were
interspersed with soil that hosts sparse grasses and a few trees.

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*Kapa'a Beach Kapa'a Beach*Kapa'a Beach is located 4.5 km north of Sapphire Cove and
30 m from the shoreline at an elevation of 2 m above sea level. Vegetation consists of
Koa trees and grass; the MAP is 604 mm/yr (Giambelluca et al., 2013). One P-wave line
with 1.5 meter spacing was run perpendicular to the shoreline.

32

33 Airport The Airport site is located west of the Upolu Airport, at the northern tip of 34 the Kohala peninsula about 7.8 km north of Kapa'a Beach and at 8 m above sea level. 35 This site is in the transition from relatively dry to wet sites, with an MAP of 1000 mm/yr 36 (Giambelluca et al., 2013). The vegetation consists of grasses and no trees are present 37 near the survey lines. Three parallel and overlapping P-wave lines were run on a grassy 38 hill about 30 meters back from a sea cliff. Lines 1 and 2 had geophone spacing of 3 m 39 with six overlapping geophones totaling a length of 72 m. Line 3 had geophone spacing 40 of 1 m, a total length of 15 m and was run parallel along the centerline of lines 1 and 2 41 (3 m spacing). One S-wave line was run with 1 m spacing. The survey line was 42 positioned with the same centerline as P-wave lines 1 and 2, and 3. S-wave line was 43 translated by one sensor spacing twelve times for line 2 for developing the 2D S-wave 44 profile. This resulted in total survey line length of 27 m. A source offset distance of 3 m 45 was used.

46

47 Lighthouse The lighthouse site is located at the Kauhola Point lighthouse. about 10 km to the southeast of the Airport site (MAP 1510 mm/yr, Giambelluca et al., 48 49 2013). Three parallel and overlapping P wave arrays were run and positioned 10 m 50 back from the edge of the sea cliff, which is approximately 7 m above sea level. Surveys 51 were run on a grassy area adjacent to a grove of trees. Surveys 1 and 2 were recorded 52 with six overlapping geophones spaced 2 m apart with a total array length of 52 m. Line 53 3 had 3 m spacing with an array length of 45. The active erosion of the sea cliff provides 54 fresh exposure of the subsurface profile along the vertical cliff faces. One S-wave 55 survey line was run at this site with a spacing of 2 m. The centerline of the survey line 56 was positioned equidistant between the centerlines of P-wave lines 1 and 2. The S-57 wave line was translated by one sensor spacing twelve times for a total survey line 58 length of 54 m. A source offset of 5 m was used for S-wave line shots.

59

60 Awini Landslide The Awini site is located along the re-established Awini trail, which 61 traverses the amphitheater canyons on the wet side of the island. This trail was 62 demolished during landsliding caused by the 2006  $M_w$  6.7 Kiholo Bay earthquake (Harp 63 et al., 2012). The re-established trail crosses a large landslide just below the base of its 64 headscarp along a steep (~ 40 degree) slope. This site receives 2070 mm/yr MAP 65 (Giambelluca et al., 2013). The vegetation at this site had been mostly stripped away by 66 rock fall during and since the earthquake except for the presence of grasses. One P-67 wave line was collected along a narrow footpath parallel to the slope using geophones 68 spaced 1 m apart.

69

Waipio Canyon The Waipio Canyon site (1169 m asl) is located on the wet side of the Kohala peninsula at the head of one of the deeply incised "amphitheater canyons" (e.g. Lamb et al., 2007). This site is 23 km south of the Lighthouse site and has the highest MAP of all our study sites (3060 mm/yr) (Giambelluca et al., 2013). One P-wave survey was collected with 3 m geophone spacing. The array was run on a dirt road with slightly compacted soil surrounded by dense vegetation.

76 Shot locations at the west end of the array (position 45 m) produced audible 77 vibrations and sensible ground shaking when the plate was struck, but the east end of 78 the array did not produce these same observations. We speculate that a large void was 79 present at depth on the west end of the line; however, we are not able to resolve a low-80 velocity layer using the applied methods. We note that the RMSE of the inferred models 81 are much higher at this site compared to our other surveys. The presence of a void 82 beneath the west end of the array may explain the thicker layer lower velocities on that 83 end of the profile.

84

85 P-wave data and modeling P-wave models were derived by a refraction 86 method using the first-arrivals of seismic energy, collected by a reciprocal survey (shots 87 are conducted at either end and within the profile). Details of modeling parameters 88 tested for each site are further elaborated in Von Voigtlander (2016). Using the 89 Seisimager software module "Pickwin" (OYO Corporation, 2006; Hayashi and 90 Takahashi (2011)), the waveform data from each line was displayed and first-break 91 picks (FPB) were first automatically assigned then manually adjusted. Following 92 waveform interpretation, FBPs were imported into the Seisimager analysis platform,

93 "Plotrefa" (OYO Corporation, 2006), and displayed as travel-time curves. Plotrefa was 94 used to analyze variations in the travel-time curves and invert for the velocity structure 95 of the shallow subsurface. Prior to interpretation, the travel-time curves were checked 96 for reciprocity in order to ensure data quality. The Principle of Reciprocity states that 97 velocity is independent of direction of travel, meaning that the rate of wave propagation 98 from the source to the receiver should be equal to the rate if the direction was reversed 99 and traveled from the receiver to the source, regardless of subsurface anomalies (e.g. Hayashi and Takahashi, 2011). FBPs were corrected if the error was larger than 5%. 100 101 resulting in a velocity model with smaller residuals. The travel-time curves were then 102 inverted using Plotrefa to produce a 2D velocity model using a linearized tomographic 103 inversion. Examples from a dry and wet sites are shown in Supplementary Figures 1 104 and 2. For dry sites, the uneven soil coverage and patchy exposure of core stones 105 resulted in a more complicated near surface travel time curve compared to wet sites 106 that had a well developed soil profile in the upper few meters.

107 A linearized tomographic inversion is suitable for sites with complicated velocity 108 structures and lateral velocity variations, and can be applied to areas of both less 109 distinct velocity contrasts as well as a layered subsurface with sharp velocity contrasts. 110 Prior to inversion, an initial model must be constructed using a velocity range and assigning the number of layers in the model. A sensitivity analysis was performed to 111 112 guantify dependence of the final velocity cross-sections on the initial model using line 1 113 taken from the Airport site (Supplementary Figure 3). Fifty independent linear initial 114 velocity models were constructed; minimum velocities fell between 50-250 mm/s 115 whereas maximum velocities ranged from 3000-5000 m/s at 20 km depth. We invert

data from the Lighthouse site for each of these initial velocity profiles and calculate the average velocity and standard deviation of velocity across the profile. The average standard deviation of velocities within the profile was 40 m/s, and the maximum standard deviation is 0.13 km/s within the upper 2 m of the survey. From these results, we suggest that the choice of the initial model does not influence the final velocity model at the resolution of our interpretation, in which we evaluate different weathering layers with hundreds of m/s velocity difference.

For our final inversions, we computed the linearized tomographic inversion by iteratively tracing rays through nodes bounded by velocity cells, and therefore constructing the fastest theoretical travel times for an individual ray path. The difference between the observed and theoretical travel times for the ray paths was given by the RMSE and allows assessment of the validity of the inferred velocity models. We assigned velocity layers to the linearized tomographic inversion to aid in visual interpretation of the data.

Three 1-D Vp profiles were collected at a site of a historic flow (1859 AD) near
Kiholo Bay (south of Kohala) in order to evaluate the velocity of fresh, chemically
unaltered pahohoe basalt in this environment. The results of these profiles suggest near
surface velocities of ~ 300 – 1000 m/s, which are substantially lower than "typical"
basalt velocities (> 5000 m/s; Barton, 2007) and likely reflect initial fracturing and
porosity in fresh lava flows.

136

137MASW data and modelingAll modeling was performed in the SeisImager138SW/2D software suite (OYO Corporation, 2006). Two-dimensional and one-dimensional

S-wave profiles were modeled using different methods. For one-dimensional S-wave 139 140 profiling, the Park et al. (1998) method was used to develop the frequency-velocity 141 spectrum. Dispersion curve points were selected by manually picking spectral peaks in 142 the frequency-velocity domain. For two-dimensional S-wave profiling, the Hayashi and 143 Suzuki (2004) common-midpoint cross-correlation (CMPCC) method was used to 144 develop the frequency-velocity spectra. The dispersion curves were similarly picked by 145 selecting spectral peaks in each respective spectrum of the 2D array. The surface wave 146 dispersion curves were compared to the dispersion curves of initially assumed S-wave 147 profiles with consideration for higher mode Rayleigh waves (Xia et al., 2003). The S-148 wave profiles were manually adjusted and the dispersion curves recalculated until the 149 best fit with surface wave dispersion curves was achieved. This is often routinely done 150 by determining a nonlinear-least-squares solution. Manual adjustments are made to the 151 S-wave model to ensure the dispersion curves match closely across all frequencies. 152 Lower frequency Rayleigh waves induce particle motion at greater depths in the 153 subsurface (Stokoe and Santamarina, 2000). Therefore it is important to have close 154 matching across all frequencies in order to have a reliable S-wave model. S-wave 155 modeling and dispersion curve matching was performed in the WaveEQ module of the 156 Seisimager SW/2D software suite. When the closest dispersion curve match is 157 achieved, the S-wave profile for the modeled dispersion curve is taken as the 1D final 158 profile. For a 2D MASW survey, this is done for each CMPCC dispersion curve. The 159 individual 1D profiles are then compiled into a 2D cross-section profile. The 160 incorporation of individual S-wave profile sections into a complete 2D profile was 161 performed in the GeoPlot module of the SeisImager SW/2D software suite. Example

- 162 plots of 2D survey design, frequency-phase velocity diagrams, and dispersion curves
- are shown for each site (Supplementary Materials Figures 5-7).
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Supplementary Figure 1. Example data from dry sites (Road Cut Site Line 2). A) Wave form data with first break pick assignments (red). Pink line represents the travel time curve. B) Observed versus theoretical travel time curves. C) Linearized model after 60 iterations with ray path coverage shown. Geophone array noted by arrows.



Supplementary Figure 2. Example data from wet sites (Lighthouse line 2). A) Wave form data with first break pick assignments (red). Pink line represents the travel time curve. B) Observed (blue) versus calculated (black) travel time curves from the linearized model. C) Linearized model with ray path coverage shown.





Supplementary Figure 3. Sensitivity analysis for Lighthouse site. A) Initial velocity profiles used in the sensitivity analysis. B) Calculated standard deviation of velocity for resulting models (ms) using the range of initial velocity models in A.



Supplementary Figure 4. 1D Vp profiles from historic flow (1859 A.D.) near Kiholo Bay, Hawaii. A) Example waveform data and first-break picks (red). Pink line denotes travel-time curve. B) Travel time curve for three repeat trials. Near surface velocity is equal to the inverse slope of linear time-distance segments and ranges from ~ 300 - 1000 m/s. C) Photograph of fresh lava surface at survey site.



Supplementary Figure 5. MASW survey and data from the Upolo airport site (wet). A) Schematic of 2D MASW testing setup showing location of geophones. Shot and geophone location were shifted by one sensor spacing (1 m) in the direction of the array. Each shifted geometry is shown adjacent to the previous geometry for illustrative purposes. B) Frequency-Phase velocity diagram (blue showing preferred phase velocity for each Rayleigh wave frequency, red points show selected dispersion points plotted in part C. C) Measured dispersion points from B and modeled dispersion curve.



Supplementary Figure 6. MASW survey and data from the Lighthouse airport site (wet). A) Schematic of 2D MASW testing setup showing location of geophones. Shot and geophone location were shifted by one sensor spacing (2 m) in the direction of the array. Each shifted geometry is shown adjacent to the previous geometry for illustrative purposes. B) Frequency-Phase velocity diagram (blue showing preferred phase velocity for each Rayleigh wave frequency, red points show selected dispersion points plotted in part C. C) Measured dispersion points from B and modeled dispersion curve.





Supplementary Figure 7. MASW survey and data from the Highway 270 road cut east site (dry). A) Schematic of 2D MASW testing setup showing location of geophones. Shot and geophone location were shifted by one sensor spacing (1 m) in the direction of the array. Each shifted geometry is shown adjacent to the previous geometry for illustrative purposes. B) Frequency-Phase velocity diagram (blue showing preferred phase velocity for each Rayleigh wave frequency, red points show selected dispersion points plotted in part C. C) Measured dispersion points from B and modeled dispersion curve.

# Supplementary Table 1: Seismic survey sites

Site Name	Latitude	Longitude	Elevation (m)	Mean Annual	
	(degrees)	(degrees)		Precipitation (mm)	
Highway 270 Roadcut East	20.1361 N	155.88607 W	78 m	500 mm	
Highway 270 Roadcut West	20.13669 N	155.88645 W	78 m	500 mm	
Sapphire Cove	20.16220 N	155.89844 W	8 m	500 mm	
Kapa'a Beach	20.202116 N	155.902483 W	2 m	604 mm	
Upolo Airport	20.26493 N	155.86737 W	8 m	1000 mm	
Lighthouse	20.24602 N	155.77101 W	7m	1510 mm	
Awini Landslide	20.19369 N	155.72258 W	111 m	2070 mm	
Waipio Canyon	20.06458 N	155.66764 W	1169 m	3060 mm	

#### Supplementary Table 2: P wave seismic survey and model parameters

Site Name	Line Number	Geophone	Off-end Shot	Length of	Shot Density	Maximum	Depth	Geophone	Geophone	Hammer	Model RMSE (ms)
		Spacing (m)	Distance (m)	Survey (m)		Resolution (m)	Surveyed (m)	Frequency (Hz)	Base	Weight(s) (lb)§	
Ui-h	1	3 m	5 m	55 m	13	1x1.5m	18 m	4.5 Hz	Tripod	16	1.4
Roadcut East	2	1 m	3 m	21 m	19	0.25x0.5	3 m	4.5 Hz	Tripod	4, 8 <sup>§</sup>	0.7
Highway 270	1 (start)**	3 m	10 m	65 m	19	0.5x1.0	21 m	40 Hz	Spike	16	1.5
Roadcut West	2 (shift)**	3 m	10 m	65 m	19	0.5x1.0	21 m	40 Hz	Spike	16	1.4
Sannhira	1*	1 m	3 m	21 m	18	0.25x0.5	3 m	4.5 Hz	Spike	16	1.2
Cove	2*	2.5 m	5 m	47.5 m	13	1x1	12 m	4.5 Hz	Spike	8	1.2
	1	1.5 m	3 m	28.5 m	17	0.3x1	5.5 m	4.5 Hz	Spike	8	0.8
Kapa'a Beach											
	1 (start)**	3 m	5 m	55 m	13	0.5x1.5	18 m	4.5 Hz	Spike	8	0.9
Upolo Airport	2 (shift)**	3 m	5 m	55 m	13	0.5x1.5	18 m	4.5 Hz	Spike	8	1
	3	1 m	3 m	21 m	20	0.25x0.5	7 m	4.5 Hz	Spike	4, 8 <sup>§</sup>	0.5
	1 (start)**	2 m	5 m	40 m	17	0.5x1.0	12 m	40 Hz	Spike	16	0.9
Lighthouse	2 (shift)**	2 m	5 m	40 m	18	0.5x1.0	13 m	40 Hz	Spike	16	0.8
	3	3 m	5 m	55 m	14	1x1.5	18 m	4.5 Hz	Spike	16	1.6
Awini Landslide	1	1 m	2.5 m	20 m	8	0.2x1	4 m	4.5 Hz	Spike	16	0.5
Waipio Canyon	1	3 m	1.5 m	47.5 m	11	1.0x1.5	15 m	4.5 Hz	Tripod	16	4.1

\* Lines perpendicular to each other with no overlap

\*\*(start) lines were (shift)ed, first six geophones replaced last six geophones of previous array. 37.5% overlap

<sup>§</sup>When multiple hammer weights are used, the larger hammer is used for off-end shots only

## Supplementary Table 3: S wave seismic survey parameters

Site Name	Geophone	Off-end Shot	Length of	Max model	Number of	Geophone	Hammer	Number	Recording
	Spacing (m)	Distance (m)	Survey (m)	depth	Array Shifts	Base	Weight (lb)	of Stacks	length (s)
Highway 270 Roadcut East	1 m	3 m	21 m	13 m	6	Tripod	8	8	0.5
Upolu Airport	1 m	3 m	27 m	13 m	12	Spike	8	8	0.25
Lighthouse	2 m	5 m	54 m	24 m	12	Spike	16	10	1