## ENGINEERING RESEARCH INSTITUTE UNIVERSITY OF MICHIGAN ANN ARBOR

# MODEL STUDY FOR HARBOR OF REFUGE FOR LIGHT DRAFT VESSELS AT PORT SANILAC, MICHIGAN

Technical Report No. I Lake Hydraulics Laboratory Department of Civil Engineering

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Project M 804 - Contract W-20-064-eng-1774 Detroit District, Corps of Engineers, United States Army

### ENGINEERING RESEARCH INSTITUTE UNIVERSITY OF MICHIGAN ANN ARBOR

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FOR

LIGHT DRAFT VESSELS AT PORT SANILAC, MICHIGAN

BY

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Project M804

CORPS OF ENGINEERS DETROIT, MICHIGAN

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### MODEL STUDIES FOR HARBOR OF REFUGE

FOR

### LIGHT DRAFT VESSELS AT PORT SANILAC, MICHIGAN

### INTRODUCTION

Port Sanilac, Michigan is located approximately 30 miles from the southern end of Lake Huron as shown by the map in Drawing 1. It is proposed to construct breakwaters and to dredge areas within the breakwaters in order to create a harbor of refuge for light draft vessels at this location. The primary purpose of the model study was to determine the breakwater arrangement which would afford the maximum protection from wave action in the harbor area. As an additional basis for comparison, currents were measured within the harbor and near the harbor entrance for each of the plans. The effect of the size of the harbor opening was investigated by constructing one of the plans with a larger opening than those of the others. The effect of the shape of the breakwaters was studied by reconstructing one of the plans with verticalwalled breakwaters. Rubble mound breakwaters were simulated in all other plans.

The study was made as a result of a contract dated November 8, 1948, between the University of Michigan Engineering Research Institute and the Detroit District, Corps of Engineers, U. S. Army. The initiation of the work was expedited by the interest and financial support of the Michigan State Waterways Commission.

Throughout the model study frequent consultations were held with the following personnel of the Detroit District: Colonel Louis J. Rumaggi, District Engineer, Tom C. Trelfa, Harley F. Lawhead and Charles E. Lee. Colonel E. W. Nelson and W. H. Booth, Jr. of the Great Lakes Division Office, Corps of Engineers, visited the laboratory in connection with the work. Mr. R. Y. Hudson of the Waterways Experiment Station, Vicksburg, Mississippi, visited the laboratory at various stages of the work, as did Colonel H. D. Vogel, District Engineer of the Buffalo District.

Members of the Michigan State Waterways Commission visited the laboratory at various times. E. W. Kiefer, Chairman, and Leonard H. Thomson, Secretary, were in close touch with the work throughout the tests.

The University of Michigan Lake Hydraulics Laboratory where the tests were made is a facility of the Engineering Research Institute and the Department of Civil Engineering of the College of Engineering. Professor A. E. White is Director and Professor C. W. Good is Assistant Director of the Engineering Research Institute. Professor Earnest Boyce is Chairman of the Department of Civil Engineering and Ivan C. Crawford is Dean of the College of Engineering. The laboratory is under the general direction of C. O. Wisler, Professor of Hydraulic Engineering, and the model tests were conducted under the supervision of E. F. Brater, Associate Professor of Civil Engineering. The following men took an active part in conducting the tests: John H. Boeckerman, Jerome Pepper, Leslie D. Stair and Dah C. Woo.

### THE MODEL

The model was built to an undistorted linear scale of 1 to 75. Templates were cut from 3/8-inch waterproof plywood according to sounding data supplied by the Corps of Engineers. The templates were spaced at 1.5-foot intervals in and near the harbor area and at 3-foot intervals in the more remote regions. A plan of the model and wave tank is shown in Drawing 2. The space between the templates was packed with sand to within an inch of their upper edges. The model was then surfaced with cement mortar which was screeded to conform with the edges of the templates. The accuracy of the model was checked by means of an engineer's level and again by checking contours of the lake bottom against locations of the shore line for various water surface elevations. Plate 1 shows the templates in place before the concrete was poured.

### METHOD OF CONDUCTING TESTS

The waves were generated by means of a plunger-type wave machine 30 feet long. The wave machine is shown in Plate 1. The amplitude and period of the plunger may be varied to produce waves of any required height, length and period. The wave machine is portable, so that any desired wind direction can be simulated.

Wave heights were measured with electric resistance gages arranged so that variations in water level were recorded by means of oscillographs. The calibrations of the resistance gages were checked systematically during the tests. The wave height at any point was determined by computing the average of the highest one-third of 180 successive waves. The instruments described above are shown in Plate 2.

Surface currents were measured by timing the movements of small floats with reference to coordinate lines on the model.

The elevation of the water surface in the tank was checked by means of a hook gage mounted on one of the tank walls. It was necessary to add small amounts of water occasionally to compensate for evaporation and leakage.

### THE TESTING PROGRAM

Five breakwater arrangements designated as Plans 1, 2, 3, 4 and 5 were tested. Each of these was constructed to simulate the shape of a rubble mound breakwater as shown in Drawing 1. In each of these the outer 200 feet of the north breakwater had the shape designated in Drawing 1 as Type A, whereas the remainder was of Type B. Plan 6 consisted of vertical-walled breakwaters placed in the same position as those of Plan 3. Typical sections through these breakwaters are also shown in Drawing 1.

For all plans, except Plan 4, the width of the dredged entrance channel was 150 feet and the distance from toe to toe of rubble mound breakwaters was 185 feet. Plan 4 was constructed with a dredged entrance channel 200 feet wide and a distance from toe to toe of rubble mound breakwaters of 235 feet. The clear distance between the vertical faces of breakwaters of Plan 6 was 210 feet at the harbor entrance.

The harbor arrangement designated as Plan 1 may be seen in Drawings 3-9 and 11-13 and Plate 2. Plan 1a, shown in Drawing 10, consisted of the same breakwater arrangement as Plan 1 with the elevation of the north breakwater raised to prevent overtopping by waves from the NNE.

Plan 2 differed from Plan 1 only in having the outer 100 feet of the south breakwater rotated toward the lake as shown in Drawings 14-22 and Plates 3 and 4.

For Plan 3, the south breakwater was in the same position as for Plan 1. The entire north breakwater was rotated in a clockwise direction to the position shown in Drawings 23-31 and Plates 4, 5 and 6.

Plan 4 was similar to Plan 3 except that the south breakwater was moved southward a distance sufficient to increase the size of the opening by 50 feet. Plan 4 is illustrated in Drawings 32-40 and Plates 7 and 8.

Plan 5 consisted of curved breakwaters placed in the same general location as for Plan 3. Plan 5 is shown in Drawings 41-49 and Plates 9 and 10.

The breakwater arrangement for Plan 6 was exactly the same as for Plan 3, the only difference being in the nature of the cross section of the breakwaters as previously described. The drawings for Plan 6 are numbered 50-56 and 58-60, and photographs are shown in Plates 10, 11 and 12.

Plan 6a consisted of the breakwaters of Plan 6 with spurs added to the inner face of the north breakwater as shown in Drawing 57.

### TEST CONDITIONS

The basic wave data were prepared by H. F. Lawhead and C. E. Lee of the Detroit District Office. Deep water wave heights were computed from the records of wind velocity and duration for the following four wind directions: N,NNE, E and SSE. Refraction diagrams were then prepared for each wind direction. It was found from these diagrams that the wave action at Port Sanilac resulting from a north wind was similar to but less severe than that produced by a wind from the NNE. Consequently no tests were run for the north direction. The refraction diagrams for the three wind directions used in the tests are reproduced in Appendix C at the end of this report.

For Plan 6 one additional wind direction was tested. This direction was approximately SE. It was determined in the wave tank by trial so that the resulting wave would be projected directly into the harbor entrance; i.e., the waves moved in a direction parallel to the north breakwater as they approached the harbor. This same wind direction was used in the test on Plan 6a.

For each wind direction a "large" wave and a "small" wave was projected against the harbor. The large wave was one that would be produced by a severe storm. The small wave would be produced by less severe storms of more frequent occurrence. A summary of the characteristics of the waves used in the tests is given in Table I. The frequencies shown in the table were determined from curves given in Appendix C.

### TABLE I

### SUMMARY OF WAVE DATA

	SI	nall Wa	ve	Large Wave			
Wave Characteristic	SSE	È	NNE	SSE	Е	NNE	
Deep Water Wave Height (Ft.)	4.5	4.5	4.5	8.7	7.0	13.0	
Deep Water Wave Length (Ft.)	81.9	81.9	81.9	90.3	81.9	190.5	
Wave Period (Sec.)	4.0	4.0	4.0	4.2	4.0	6.1	
Frequency *	75	45	272	1	5	4	

\* Number of times wave height will be equaled or exceeded in ten years.

It is believed that the larger waves would give an indication of the disturbance inside the harbor when severe Lake Huron storms have reached their full intensity and are producing near maximum waves at the harbor site. The smaller waves would occur more frequently and might be thought to represent the conditions that would commonly exist when small boats are entering

the harbor to seek refuge from a major storm before it has reached its full intensity. Finally, the smaller waves permit a comparison of the various harbor arrangements under conditions of virtually no overtopping of the breakwaters by storm waves, whereas in the case of the larger waves the conditions inside the harbor are affected by overtopping to some extent for the SSE and E winds and to a greater degree for the NNE wind.

Low-water datum for Lake Huron is at elevation 578.5. The crests of the breakwaters were set 8 feet above low-water datum. Throughout the tests the lake elevation was kept 3 feet above low-water. Thus, the crests of the breakwaters were 5 feet above the still water level of the lake. Such a high water condition is primarily the result of a prolonged westerly wind which tends to cause some Lake Michigan water to enter Lake Huron through the Straits of Mackinac. A change in wind direction will then produce the conditions simulated in the tests. The lake stage used in the tests was determined from a consideration of the records of the U. S. Lake Survey's water level precorder at Harbor Beach, Michigan, covering a number of storm periods.

### PRESENTATION OF RESULTS

All of the data obtained from the tests are presented in Drawings 3-60. The successive plans are presented in numerical order. For each plan the drawings showing measured values of harbor wave heights are presented first. These are followed by drawings giving the results of current measurements. Photographs showing harbor conditions during large wave tests are presented in Plates 1-12.

### Wave Heights

Wave heights were measured at from 25 to 30 locations for each test. The measured values are recorded on the drawings at the gage locations. With these values as a basis, lines of equal wave height were drawn. The regions where the wave heights were less than 1.5 feet and where they were greater than 5.0 feet were hatched. The direction in which the predominant wave was moving is indicated at each gage location by means of an arrow. The wave height drawings for Plans 1, 3, 4 and 6 were also reproduced on single sheets for each wind direction. These are shown on Pages 81 through 91 following Drawing 61.

Some numerical averages were found to be useful in analyzing the test data. In Table II are shown three groups of averages for each wind direction and for both the large and small waves. The first group consists of the measurements made near the harbor entrance. The second group comprises those inside the harbor. The dividing line between the two groups is shown as a dotted line in Drawing 61. A third group designated in Table II as the "mooring area" consisted of eleven measuring stations located in the quietest portion of the harbor. This region is outlined by the dashed line in Drawing 61.

### Currents

The magnitude and direction of velocities in and around the harbor are shown on the drawings by means of arrows. The lengths of the arrows were made proportional to the velocities according to a scale shown on the drawings. Paths followed by the floats are shown by means of dotted lines. In some locations the velocities varied with time, so that occasionally different paths may be seen to emanate from the same point. A summary of the maximum

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### TABLE II

### AVERAGE WAVE HEIGHTS

		Er	trance	)	1	Harbor		Mooring Area		
	Plan	SSE	E	NNE	SSE	E	NNE	SSE	E	NNE
	l	4.6	2.0	0.9	0.9	0.5	0.1	0.6	0.6	0.1
Small Wave	2	4.5	1.2	1.4	1.8	0.4	0.4	1.4	0.5	0.5
	3	4.0	2.1	1.6	1.2	0.2	0.3	0.6	0.3	0.2
	4	3.9	2.6	0.9	1.4	0.6	0.2	0.6	0.7	0.2
	5	4.8	2.2	1.3	1.2	0.6	0.2	0.6	0.8	0.2
	6	4.9	4.3	0.9	1.2	1.1	0.1	0.6	0.7	0.1
	l	5.6	5.2	5.1	1.4	1.6	1.7	1.0	1.3	1.8
Ø	2	7.0	3.8	4.2	2.1	1.4	1.6	1.6	1.1	1.4
Wav	3	5.5	4.6	3.6	1.4	0.6	1.2	0.9	0.6	1.1
arge	4	6.1	4.2	2.8	1.6	0.8	1.6	0.8	0.8	1.5
ы	5	6.0	4.1	3.9	1.5	0.9	1.6	0.8	0.7	1.6
	6	6.7	5.2	2.2	2.0	1.6	0.6	1.2	1.0	0.6

velocities found in various locations is given in Table III.

### TABLE III

### MAXIMUM CURRENTS FOUND IN VARIOUS HARBOR LOCATIONS

Values are in mi. per hr.

Between Shore

Plan	En	Entrance			Harbor			Mooring Area			and Inner End of Breakwater			
	SSE	E	NNE	SSE	E	NNE	S	SE	E	NNE	SSE	E	NNE	
1	3.1	2.8	2.5	3.3	1.8	2.4	C	.9	0.9	2.4	3.3		2.0	
2	1.2	2.0	3.2	1.0	3.5	2.2	1	.1	3.5	2.2	1.0	1.0	2.5	
3	0.8	2.3	3.0	0.6	1.0	2.6	C	.4	0.7	2.6	0.8			
4	1.7	2.6	2.4	3.1	1.8	1.5	C	8.0	1.8	1.5	1.7		0.5	
5	2.4	1.1	3.2	3.1	1.6	1.6	1	3	1.4	1.6	1.9	1.2	1.1	
6	2.1	1.5	3.6	2.5	0.9	1.6	l	1	0.9	1.5	2.0	1.6	2.0	

### CONCLUSIONS

The model tests provided data which permit the evaluation of the effectiveness of the various plans in regard to wave heights inside the harbor, wave heights in the vicinity of the entrance and currents. The final selection of a plan will require the consideration of other factors, such as the costs of the various plans, the availability of construction materials, desirable entrance size and suitability for mooring and docking purposes.

On the basis of an inspection and comparison of the wave height drawings, Table IV was prepared, showing the best plans for various conditions. Where two or more plans have been tabulated, it was for the reason that several seemed to be so nearly equal that it would have been misleading to select only one. It will be noted that Plan 3 appears 10 times in Table IV, whereas the

			·		
	re	11			
the others appear o	only 4 or 5 times				
	т	ABLE IV			
PLANS GIVING	THE MOST FAVORA	BLE RESULTS FOR	VARIOUS CONDI	TIONS	
Wind	Small	Wave	Large	Wave	
Direction	Entrance	Harbor	Entrance	Harbor	
SSE	3,4	1,3,4,5,6	3	3	
E	1,2,3	2,3,5	3,4	3	
NNE	1,2,3,4,5,6	1,2,3,4,5,6	5,6	6	

In Table V is given a set of values obtained by numbering the average wave heights of Table II from 1 to 6 in order of ascending size. Thus. the best plan for any region and wind direction is given the value 1, the next best 2, and so on. The sum of the values for each wave size is given for all of the plans. Plan 3 is again indicated as being better than the others. Α more detailed method of summarizing the values in Table V is shown in Table VI. Here the values for a particular plan are added for each wind direction and wave size. This tabulation indicates that Plan 3 is as good or better than the others for waves from the SSE and E, but for the NNE direction Plan 6 is very good for both the large and small waves. For the large wave this is due in part to the fact that harbor waves resulting from the NNE wind were affected to a considerable degree by the overtopping of the north breakwater. The rectangular shape of the breakwaters of Plan 6 broke up the overtopping waves much more than the sloping shape of the other breakwaters. In this connection it should be noted that harbor waves resulting from overtopping cannot be determined as confidently from model tests as those entering through openings in the breakwaters. It can be assumed that harbor waves will be worse

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in the model than for comparable conditions in the prototype because the surface of the model breakwater is relatively smoother than the prototype surfaces. It is also probable that the wind action may tend to break up some of the overtopping waves in the prototype.

### TABLE V

Ρ	lan	Ent SSE	rance E	NNE	H SSE	arbor E	NNE	Moor SSE	ing Ar E	ea. NNE	Summation
	l	ե	2	2	1	3	1.5	3	3	1.5	21
. Wave	2	3	1	5	6	2	6	6	2	6	37
	3	2	4	6	3	1	5	3	l	4	29
[Lam;	4	l	3	2	5	4.5	3.5	3	4.5	4	30.5
202	5	5	5	4	3	4.5	3.5	3	6	4	38
	6	6	6	2	3	6	1.5	3	4.5	1.5	33.5
	l	2	5.5	6	1.5	5.5	6	4	6	6	42.5
ve	2	6	1	5	6	4	4	6	5	3	40
e War	3	1	4	3	1.5	1	2	3	1	2	18.5
Larg	4	4	3	2	4	2	4	1.5	3	4	27.5
	5	3	2	4	3	3	4	1.5	2	5	27.5
	6	5	5.5	l	5	5.5	1	5	4	1	33

NUMERICAL EVALUATION OF THE VARIOUS PLANS

The results shown in Tables V and VI fail to take into account the magnitude of the differences between various plans. This is also true to some extent of the evaluations shown in Table IV. Consequently, these summaries can only be considered as a guide and constant reference must be made to the

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original wave height drawings and the wave height averages of Table II in evaluating the various plans.

### TABLE VI

SUMMARY OF THE NUMERICAL EVALUATION OF THE VARIOUS PLANS

	Sma	ll Wave		Large Wave				
Plan	SSE	Έ	NNE	SSE	Έ	NNE		
1	8	8	5	7.5	17	18		
2	15	5	17	18	10	12		
3	8	6	15	5.5	6	7		
4	9	12	9.5	9.5	8	10		
5	11	15.5	11.5	7.5	7	13		
6	12	16.5	5	15	15	3		

The following evaluations of the various plans are based entirely on wave heights. However, the results of the current measurements shown in the drawings and summarized in Table III are generally in accord with the conclusions reached.

### Plan 1

This breakwater arrangement gave good results for the small waves. However, the large wave tests indicated that Plan 3 has definite advantages over Plan 1. Therefore, barring other considerations, Plan 3 should be chosen in preference to Plan 1.

### Plan la

Overtopping of the north breakwater was prevented in the model by placing bricks on the breakwater. Tests were run only for the large NNE wave. The results of the tests, given in Drawing 10, may be compared with those obtained under the same conditions with the normal breakwater elevation, as shown in Drawing 7, to obtain an indication of the effect of overtopping on the harbor conditions. With overtopping prevented, the waves in the harbor were less than one-third of the height of those during overtopping. However, the results are not entirely comparable with those that would occur if the sloping faces of the breakwater were carried high enough to prevent overtopping. This is because the sloping face would absorb some of the energy which was reflected by the vertical face of the bricks.

### Plan 2

This plan gave the least satisfactory results of any of the plans tested. It can be eliminated from further discussion.

### Plan 3

This plan gave very good results. Its relative advantages and disadvantages will be discussed in more detail as a basis for comparison with Plans 4 and 6.

### Plan 4

In general, the average wave heights inside the harbor were found to be from 0.2 feet to 0.4 feet higher for Plan 4 than for Plan 3. The choice between Plans 3 and 4 depends upon whether the advantages of the larger entrance of Plan 4 outweigh the more comfortable mooring conditions provided by Plan 3.

### Plan 5

The tests showed that the curved breakwaters of this plan provided no advantages over several of the other plans.

### Plan 6

Plan 6 is better than Plan 3 during NNE wind storms, but Plan 3 provides much better protection during storms from the SSE and E. The frequencies given in Table I indicate that for every 4 occurrences of the large wave from the NNE, the combined number of occurrences from the SSE and E will be 6. However, in the case of the small waves, there will be more than twice as many occurrences from the NNE as the combined number from the SSE and E. Consequently, from a statistical point of view the large wave tests would lead to the conclusion that Plan 3 is the better one, whereas the reverse would be indicated by the small wave tests. However, the statistical importance of the small wave from the NNE is nearly nullified by the fact that actual wave heights in the harbor and at the entrance are only a small amount greater for Plan 3 than for Plan 6. This may be seen by comparing Drawings 28 and 55. In contrast, the small waves from the east result in much greater differences between the two plans, as shown by Drawings 26 and 53. Moreover, the verticalwalled breakwaters of Plan 6 produce regions of large wave height near the entrance and in the northeastern portion of the harbor during both the large and the small waves from the SSE. Therefore, unless other considerations favor the use of the rectangular-shaped breakwater, the tests indicate that Plan 3 should be selected.

### Plan 6: IntermediateWind Direction

The conditions for this test would be produced by a wind from approximately the SE direction. The deep water wave height used in the test was 8.0 feet, as compared with values of 8.7 feet for the SSE and 7.0 feet for the E. The results of the test shown in Drawing 56 may be compared with those of the SSE (Drawing 50) and E(Drawing 52). It will be seen that the harbor and harbor 16

entrance wave heights were somewhat higher than those from the E and lower than those from the SSE. The test provided assurance that an intermediate wind direction would not cause unusually bad harbor conditions.

### Plan 6a

A limited number of measurements were taken with spurs on the inner face of the north breakwater. The wind direction was SE and the deep water wave height was 8.0 as in the test described in the previous paragraph. The results are shown in Drawing 57. The spurs were found to have little effect at the entrance and in the northerly portion of the harbor. However, they caused reflections which more than doubled the wave height in the mooring area. APPENDIX A

DRAWINGS























29






















































Drawing 37









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Drawing 48

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Drawing 52





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Drawing 55



















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APPENDIX B

PHOTOGRAPHS



TEMPLATES



## WAVE MACHINE

PORT SANILAC, MICHIGAN HARBOR MODEL PLATE 1.



## PLAN 1 - E WIND



#### PLAN 1 - NNE WIND

PORT SANILAC, MICHIGAN HARBOR MODEL PLATE 2.



PLAN 2 - SSE WIND



#### PLAN 2 - SSE WIND

PORT SANILAC, MICHIGAN HARBOR MODEL PLATE 3.



PLAN 2 - NNE WIND



PLAN 3 - SSE WIND

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PORT SANILAC, MICHIGAN HARBOR MODEL PLATE 4.



PLAN 3 - SSE WIND



PLAN 3 - E WIND

PORT SANILAC, MICHIGAN HARBOR MODEL PLATE 5.

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100



PLAN 3 - E WIND



### PLAN 3 - NNE WIND

#### PORT SANILAC, MICHIGAN HARBOR MODEL PLATE 6.



#### PLAN 4 - SSE WIND





PLAN 4 - E WIND



# PLAN 4 - NNE WIND

PORT SANILAC, MICHIGAN HARBOR MODEL PLATE 8.


PLAN 5 - SSE WIND



### PLAN 5 - E WIND

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PORT SANILAC, MICHIGAN HARBOR MODEL PLATE 9.

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PLAN 5 - NNE WIND



## PLAN 6 - SSE WIND

PORT SANILAC, MICHIGAN HARBOR MODEL PLATE 10.

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![](_page_110_Picture_0.jpeg)

![](_page_110_Picture_1.jpeg)

PLAN 6 - SSE WIND

![](_page_110_Picture_3.jpeg)

# PLAN 6 - E WIND

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PORT SANILAC, MICHIGAN HARBOR MODEL PLATE 11.

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![](_page_111_Picture_1.jpeg)

PLAN 6 - NNE WIND

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![](_page_111_Picture_3.jpeg)

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## PLAN 6 - SE WIND

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PORT SANILAC, MICHIGAN HARBOR MODEL PLATE 12.

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APPENDIX C

DRAWINGS SUPPLIED

BY

THE DETROIT DISTRICT,

CORPS OF ENGINEERS, U. S. ARMY

![](_page_114_Figure_0.jpeg)

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![](_page_120_Picture_0.jpeg)

![](_page_121_Picture_0.jpeg)

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RIT ALPHANUMERIC RESOLUTION TEST OBJECT, RT-1-71