

REVIEW

Practical energy densities, cost, and technical challenges for magnesium-sulfur batteries

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Abstract

Amid burgeoning environmental concerns, electrochemical energy storage has rapidly gained momentum. Among the contenders in the “beyond lithium” energy storage arena, the magnesium-sulfur (Mg/S) battery has emerged as particularly promising, owing to its high theoretical energy density. However, the gap between fundamental research and practical application is still hindering the commercialization of Mg/S batteries. Here, through reviewing the recent developments of Mg/S batteries technologies, especially with respect to energy density and cost, we present the primary technical challenges on both materials and device level to surpass the energy density and cost-effectiveness of lithium-ion battery. While the high electrolyte-sulfur ratio and the expensive liquid electrolyte are significantly limiting the practical application of Mg/S batteries, we found that solid-state Mg electrolyte appears to be a feasible solution on the basis of energy density and cost evaluation.

KEYWORDS

cost analysis, magnesium-sulfur battery, practical energy density, solid-state electrolytes

Rameez Razaq and Ping Li should be considered joint first author.

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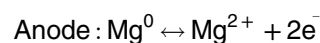
1 | INTRODUCTION

The ever-increasing quest for battery technologies with long life, high energy density, materials sustainability and safety, has led to the development of advanced energy-storage systems. In the field of rechargeable batteries, Lithium-ion batteries (LIBs) have dominated the numerous application fields such as portable electronics, electric vehicles, grid, and residential energy storage.¹ However, after more than three decades of development, the current LIBs technology is impending a fundamental limit in terms of energy density, safety, and cost.^{2,3} For electric vehicle applications, there is still an urgent demand to further upgrade the energy density to improve the driving range to at least 500 km.⁴ Hence, there is tremendous effort to develop battery technologies that could offer high energy density. On the one hand, Li metal-based batteries, such as all-solid-state batteries⁵ are extensively considered to surpass LIBs in terms of specific gravimetric (E_g) (Wh kg^{-1}) and volumetric energy density (E_v) (Wh L^{-1}). On the other hand, the cathode active materials of LIBs are usually based on critical elements, especially cobalt (Co) and nickel (Ni), which increases the cost of LIBs and imposes potential supply-chain risk.⁶ Alternatively, metal-air batteries such as Fe-O₂, Zn-O₂, Mg-O₂, and Li-O₂ have been widely studied due to high theoretical specific energy density (764, 1084, 2859, and 3505 Wh kg^{-1} , respectively) for emerging application such as electric vehicles and grids storage.⁷⁻¹³ However, for these emerging energy storage systems, it remains challenging to attain practical energy density comparable with LIBs. Therefore, other battery systems, such as Na/S batteries,¹⁴ and magnesium-sulfur (Mg/S) batteries,¹⁵ have been increasingly investigated.

In view of the cost of LIBs, the rapid expansion of Li-ion technology in various applications has led to the increasing price of critical elements, such as Li and Co.⁶ Furthermore, the commercialization of Li metal-based all-solid-state batteries could be accompanied with an increase in cost, due to the high cost of Li-metal ingot (50-130 \$ kg^{-1}) and the solid electrolyte.¹⁶ Moreover, the processing and handling of the highly reactive thin film Li metal give rise to additional process cost, while material cost for solid electrolytes would need to compete with relatively low-cost liquid electrolytes for LIBs.¹⁶ Since the raw material cost for S is very low (0.22 \$ kg^{-1}),¹⁷ cost for Li/S batteries in a very optimistic scenario could be around 100 \$ kWh at the cell level¹⁸ making them a low-cost alternative to LIBs in certain markets.^{16,19,20} In Mg/S batteries, the costly Li metal would be replaced by cheaper Mg metal (4.0 \$ kg^{-1}).²¹ A potentially lower material price for Mg/S batteries than that of Li/S batteries can be achieved.

This driving force of cost reduction inspired the application of earth-abundant Mg metal as an anode and S as a cathode material in Mg/S batteries.²² Considering the high density (1.738 g cm^{-3}) and the divalent nature of Mg^{2+} , Mg metal possesses a higher theoretical volumetric capacity of 3832 mAh cm^{-3} than Li (2062 mAh cm^{-3}).²³ In addition, Mg has a reduction potential of -2.4 V vs SHE, and it can be handled in air. As Mg has a much lower tendency to form dendrites and the melting point (650°C) is substantially higher than that for Li (181°C), it is considered a safer and more reliable anode material.²⁴

A typical Mg/S battery is comprised of an S-carbon-based composite cathode, an organic electrolyte, and an Mg metal anode.²² The Mg metal is oxidized to produce Mg^{2+} which migrates to the S cathode through the organic electrolyte and separator, while electrons arrive at the active S material via an external electrical circuit.²⁵⁻²⁸



Assuming 1672 mAh g^{-1} cathode capacity and a mean discharge voltage of 1.77 V, these reactions deliver high theoretical gravimetric and volumetric energy density of 1684 Wh kg^{-1} and 3221 Wh L^{-1} , respectively. The theoretical volumetric energy density of Mg/S batteries exceeds that (2856 Wh L^{-1}) of Li/S batteries. However, the theoretical gravimetric energy density of Mg/S batteries is lower than that (2600 Wh kg^{-1}) of Li/S batteries.²⁶⁻³¹

Regardless of the high energy density, cost-effectiveness, and safety, several key challenges still need to be addressed to realize the commercialization of Mg/S batteries, which we briefly summarize as follows:

1. A suitable electrolyte that should be chemically compatible with the electrophilic S and capable of reversible Mg deposition/dissolution.^{32,33}
2. Polysulfide shuttle due to dissolution of intermediates Mg-PS_x into the electrolyte.^{26,34}
3. The rapid capacity decay caused by the dissolution and migration of Mg-PS_x species during cycling.^{19,28,35}
4. The low utilization of S due to low electrical conductivity of S and resultant MgS .^{35,36}
5. The formation of Mg dendrites at high current densities.^{24,37-41}
6. The sluggish Mg^{2+} transport; The Mg^{2+} migration barrier calculated for MgS is ~ 900 meV, suggesting that MgS can be electrochemically inactive and can significantly limit Mg transport in the composite electrode.^{42,43}

7. The experimentally observed low discharge potential (around 1.1 V or below).^{26,44}
8. Formation of solid electrolyte interphase (SEI) and inactive MgO passivating film on Mg surface when exposed to air that is impermeable to Mg²⁺.^{23,45,46} For an extensive review of these challenges and proposed solutions, we refer the readers to previously published reviews.^{22,23,32,47,48} We further note that many similar challenges also exist in Li/S and Na/S systems, such as low S loading, high electrolyte to S ratio (E/S), insulating nature of S, polysulfides shuttle, and dendritic growth of metal anode.^{19,49}

Considerable efforts have been made to improve the electrochemical performance of Mg/S batteries which have been summarized in a number of reviews.^{22,23,47,48,50} However, a critical analysis on the practical energy densities, cost, and technical challenges for Mg/S batteries is still lacking. In this review, we first summarize the current status of Mg/S batteries in view of materials development and literature review analysis. In the second section, we systematically investigate the relationships between the energy density, cost, and other parameters of Mg/S cells. Finally, conclusions and future perspectives of high energy density Mg/S batteries are provided.

2 | CURRENT STATUS

2.1 | Material development

Conversion-type S-cathode in Mg/S batteries involve the discharge/charge processes by the reduction and oxidation of elemental S.¹⁵ Various forms of carbon as a conductive matrix (Table S1), such as S-carbon composite ink,²⁶ active carbon cloth,⁵¹ mesoporous carbon,²⁸ microporous carbon,⁵² CMK-3,^{28,53} 2-D GO,²⁷ graphdiyne,⁵² S/nitrogen-doped carbon,⁵⁴ and metal-organic frameworks,⁵⁵ have been reported to enhance the utilization of active S. However, the fast capacity decay by these cathode materials was assigned to the shuttle effect caused by soluble polysulfides and severe overcharging in Mg/S system.

Similar to the well-established Li/S and Na/S batteries, carbon is the most frequently used candidate to host S for Mg/S batteries.⁵⁶⁻⁵⁹ Nonetheless, the physical confinement of polar polysulfides on nonpolar carbon is not enough to reduce the shuttle effect. Henceforth, an improved redox kinetics of S cathode could be realized by applying various electrocatalysts⁶⁰⁻⁶⁵ that not only chemically trap the S species but also enhance conversion efficiency.

Electrolyte is one of the most important components of the cell and medium for the transfer of Mg ions between the S cathode and the Mg anode in Mg/S batteries during the battery operation.⁶⁶⁻⁷⁰ Much efforts have been given to design the appropriate electrolytes for Mg/S batteries. It is worth mentioning that the conventional nucleophilic electrolytes are incompatible with electrophilic S causing cell failure.^{26,23,52,32} This innovative research on nucleophilic electrolytes was further elaborated on the preparation of nonnucleophilic electrolytes.^{28,66,71-76} Apart from the single magnesium salt for electrolytes, dual-salt Mg²⁺/Li⁺ electrolyte results in smoother Mg plating than that of Mg electrolyte only.^{77,78}

Research progress on the development of suitable liquid electrolyte systems for Mg/S batteries is still ongoing (Table S1). The development of novel liquid electrolytes compatible with S cathode clearly depends on utilization of noncorrosive magnesium salts, various solvents, and additives.

Solid-state batteries are promising candidates for overcoming the intrinsic problem associated with liquid electrolyte.⁷⁹⁻⁸¹ At present, one of the key challenges in obtaining a suitable solid-state magnesium-based electrolyte lies in the ionic conductivity at room temperature (around 1 mS cm⁻¹).⁷⁹ However, with few exceptions,⁸²⁻⁸⁴ the low room-temperature ionic conductivities are the utmost challenge hampering the application of solid-state electrolytes (SSEs). Henceforth, the development of an appropriate SSE is highly desired for Mg/S batteries.

The energy density of current LIBs can be exceeded when Mg metal anodes are employed.^{23,45,85} Currently, different forms of commercial magnesium (99.9% purity or higher) such as foils,⁸⁶ discs,^{36,87} and plates^{45,88,89} are being used to develop Mg/S batteries (Table S1).⁹⁰⁻⁹²

Apart from different forms of Mg anode, powder-based magnesium anode demonstrated the effectiveness of structure design on the improvement of Mg/S batteries.⁹³ Similarly Mg₃Bi₂ as an alternative anode material exhibits excellent electrochemical performance.⁹⁴ Other than alloys as an anode, polymer electrolytes,⁹⁵ protective layer,⁹⁶⁻⁹⁹ Mg compounds,⁴² and magnesium-aluminum-chloride-based electrolytes^{100,101} might be effective approaches to protect the Mg metal surface in Mg/S batteries.⁹⁷

Besides designing efficient cathode materials and appropriate electrolytes, modifying the separators also signifies a viable route to trap the Mg-PS_x. Recently, CNF-²⁵ and TiS₂-¹⁰² coated glass fiber by a vacuum-filtration process were employed as a modified separator. However, the coated separator with the carbon S composite as cathode will decrease the energy density by increasing the thickness of the cell.

2.2 | Literature review analysis

Despite the development in materials, the practical application of high energy density Mg/S batteries is still challenging. Herein, we investigate the materials and parameters of Mg/S batteries from 42 publications between 2011 and 2020 and discuss how these parameters are related to the energy density. All the relevant publications, the reported cell parameters and cycling performance are tabulated in Table S1, Supporting Information.

1. Starting from the cell type, currently used cell for Mg/S batteries are coin cell, Swagelok cell and pouch cell. Then, 67% of them are coin cells, while only 3% used the pouch cell (Figure 1A) due to ease of fabrication with less active material and electrolyte. However, it should be noted that insights obtained from coin cells may not be directly applicable to large pouch cells used in practical applications.

2. From the literature review analysis, 42% published works use the Mg foil as an anode (Figure 1B). However, the electrochemical performance of anodes based on the pressed powder of Mg/C (14%) showed better coulombic efficiencies than those based on an Mg foil.

3. Currently used separators in Mg/S batteries are mainly based on commercial glass fiber, Celgard, and polymer membranes (Figure 1c). From the literature review analysis, generally glass fiber separators (68%) outperform others in terms of thermal stability, porosity, permeability, and ionic conductivity; but they are more costly and require more electrolyte.^{78,79}

4. The S content reflects the total S in the whole cathode as wt% S (Figure 1D) which allows the estimation of the capacity of the cell. 50% of publications present the S cathodes with ≤ 50 wt% S contents, but only 11% of publications report the S cathodes with high S content of over 70 wt%. In other words, constructing high

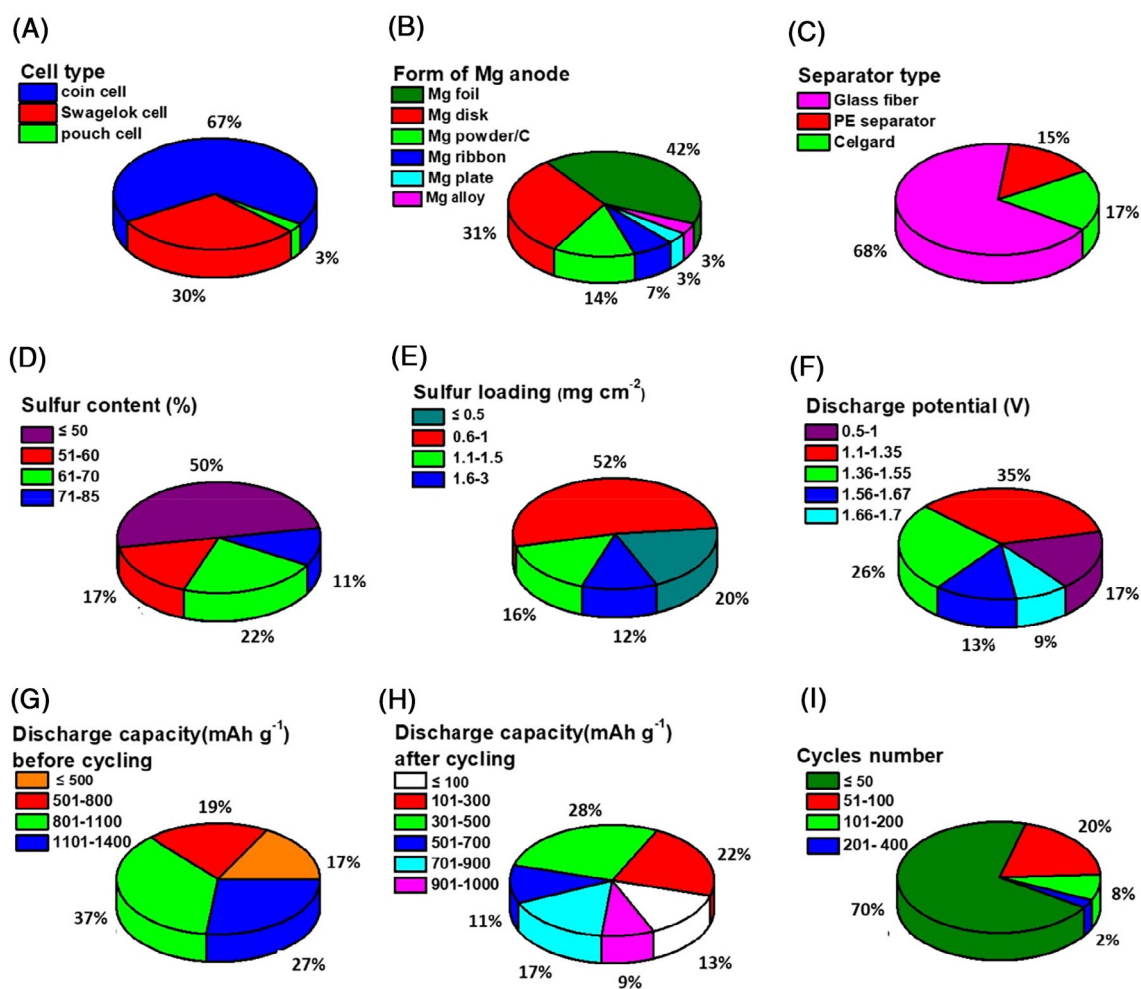


FIGURE 1 Comparative analysis of the materials and parameters of magnesium-sulfur (Mg/S) batteries from 42 publications between 2011 and 2020: A, cell type; B, different forms of Mg anode; C, separator type; D, sulfur contents (wt%); E, sulfur loading (mg cm^{-2}); F, initial discharge potential; G, discharge capacity before cycling; H, discharge capacity after cycling; and I, cycle number

S loading electrodes with S contents higher than 70 wt % is still a challenge due to the extremely low electronic conductivity of S. However, high S content of over 70 wt% in the cathode is necessary to build Mg/S batteries with a high energy density.

- The areal loading of S is a key parameter for the energy density of practical Mg/S batteries. We summarized the literatures from Table S1 with different S loadings. Most of the publications (52%) have developed S loading cathodes with merely 0.6 to 1 mg cm⁻² (Figure 1E). To pave the way to practically viable Mg/S batteries, high areal loading of S is essential.
- Figure 1F shows the literature review analysis of the observed discharge voltages. Nearly 52% of reports present the first discharge voltage potential smaller than 1.35 V; however, only 9% studies showed that discharge potential is close to theoretical potential (1.77 V) meaning that the overpotential in the electrochemical reaction is a significant problem.
- Most of the studies did not provide any information about the electrolyte volume to S mass (E/S) ratio. Only a few papers reported E/S ratios, which were around 80 to 100 μL mg⁻¹ indicating that the E/S ratio has not received enough attention despite its significance.
- Compared with the S content, the situation of discharge capacity and cycling life are even worse. Although 64% of the electrodes could deliver initial discharge capacities >800 mAh g⁻¹ (Figure 1G), the fraction of publications with discharge capacities remaining above 900 mAh g⁻¹ after cycling is only 9%, and 63% of them are ≤500 mAh g⁻¹ indicating the poor cycling stability (Figure 1H). Moreover, only 2% of them achieved over 201 to 400 cycles (Figure 1I), which cannot meet the requirements for electric vehicles and has much lower cycle life than current LIBs.

When taking these results into consideration, the development of high S loading electrodes with high capacity output and discharge voltage close to the theoretical value, and stabilized cycling performance under low E/S ratio will be the main research direction in the future.

3 | EVALUATION AND TARGET OF HIGH ENERGY DENSITY Mg/S BATTERIES

3.1 | Parameterization of Mg/S batteries components based on gravimetric and volumetric energy density

To illustrate the foundation of energy density evaluation, we first analyze the theoretical E_g and E_v only

considering magnesium anode and S cathode and then move on to practical cells. The theoretical E_g and E_v can be calculated by Formulas (1) and (2), respectively, with respect to a full-cell electrochemical reaction of Mg + S → MgS:

$$E_g = \frac{2EF}{\sum M} \quad (1)$$

$$E_v = \frac{2EF}{\sum V} \quad (2)$$

where E is the thermodynamic equilibrium voltage, F is the Faraday constant, $\sum M$ and $\sum V$ are the sum of the molar mass and corresponding sum of volume of reactants, respectively.¹⁰³ When only Mg and S are considered, $\sum M$ and $\sum V$ are the sum of molar mass and molar volume for Mg and S (ie, 56.37 g mol⁻¹ and 27.57 mL mol⁻¹), respectively. The thermodynamic equilibrium voltage at standard state (at the temperature of 298.15 K and the pressure of 1 atm) (E^0) can be calculated by Formulas (3) and (4)

$$\Delta G_r^0 = -2E^0F \quad (3)$$

$$\Delta G_r^0 = \Delta_f G_{MgS}^0 - \Delta_f G_{Mg}^0 - \Delta_f G_S^0 \quad (4)$$

where ΔG_r^0 is the standard molar Gibbs energy of reaction Mg + S → MgS, $\Delta_f G_{MgS}^0$, $\Delta_f G_{Mg}^0$, and $\Delta_f G_S^0$ are the standard molar Gibbs energy of formation of MgS, Mg, and S, respectively. On the basis of tabulated thermodynamic data,¹⁰⁴ the E^0 is calculated to be 1.77 V at standard state. Combining with Formulas (1) and (2), the theoretical E_g and E_v are 1684 Wh kg⁻¹ and 3221 Wh L⁻¹ at standard state, respectively.

Cell-level practical energy density should be considered based on all cell components. Energy density of Mg/S batteries comprising liquid electrolyte is calculated based on a pouch cell. The designed pouch cell is shown in Figure 2A, with a cross-sectional area of 12 × 8 cm². Because the liquid electrolyte is facile to flow and leak, we only considered one layer of cathode and one layer of anode instead of multilayered form. However, we note the energy density generally increases in pouch cell when multiple layers of cathode and anode are used. The magnesium foil acts as both anode and anode current collector (an additional current collector may be required if welding the Ni tab with Mg metal is problematic), the thickness of which is designed based on the negative/positive (N/P) capacity ratio of 1.2 with 20% excess Mg stock. N/P capacity ratio of 1:1 on Li metal batteries with artificial SEI has been recently reported by Wang group.¹⁰⁵

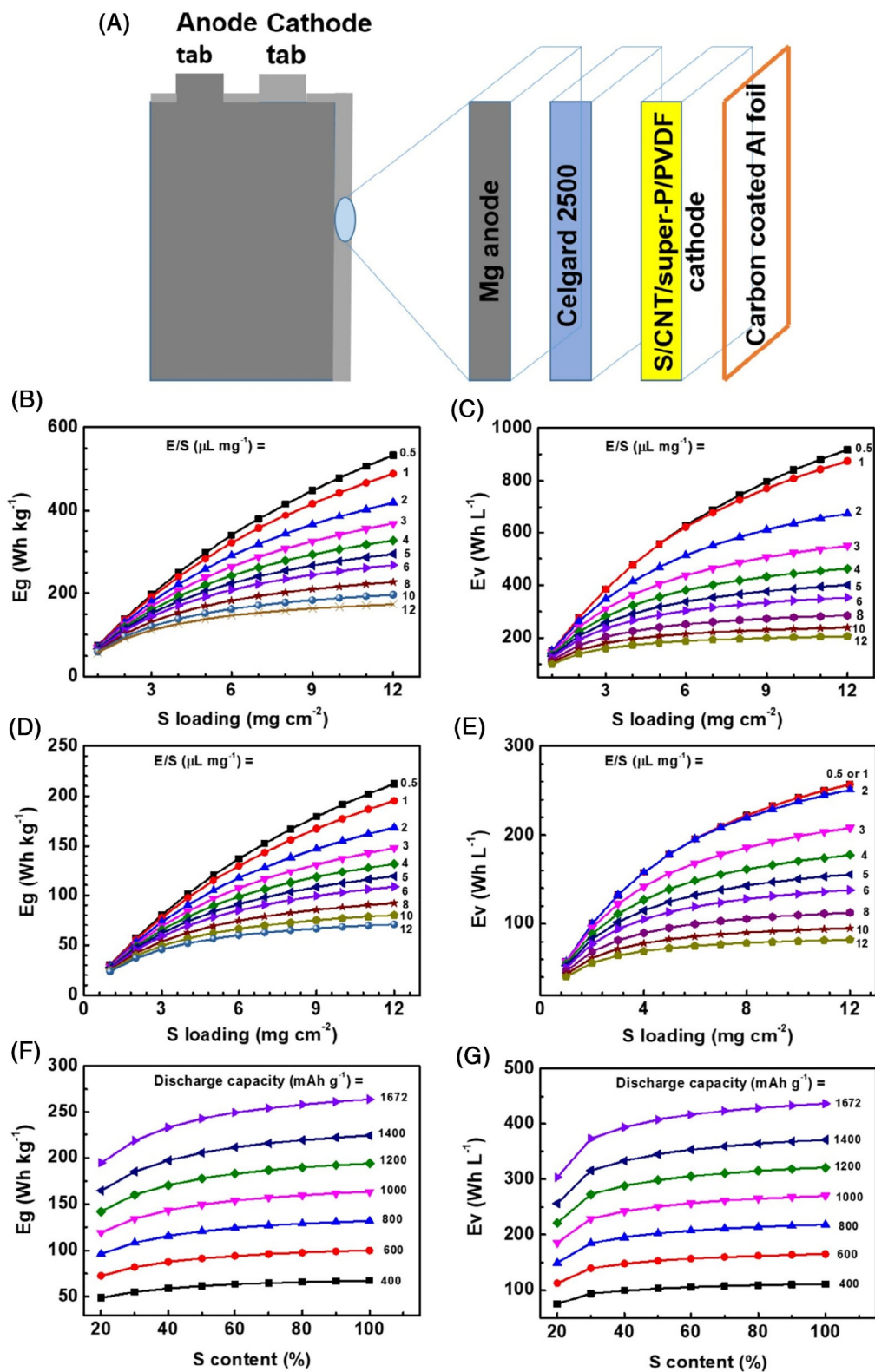


FIGURE 2 Gravimetric and volumetric energy density estimation of magnesium-sulfur (Mg/S) batteries with liquid electrolytes: A, the structure of Mg/S pouch cell with liquid electrolytes; B, the gravimetric; and C, volumetric energy density of ideal cell with 100 wt% sulfur content, 100% sulfur utilization and theoretical discharge voltage of 1.77 V; D, the gravimetric; and E, volumetric energy density of realistic pouch cell with 64 wt% sulfur content, 60.8% sulfur utilization and average discharge voltage of 1.2 V; F, the gravimetric and G, volumetric energy density of pouch cell with fixed sulfur loading of 6 mg cm^{-2} , E/S of $3 \mu\text{L mg}^{-1}$, and average discharge voltage of 1.77 V

Considering that Mg metal is less electrochemically active than Li metal, we believe that an N/P ratio of 1.2 is plausible. In this designed Mg/S cell, the liquid electrolyte is chosen as 0.5 M organic magnesium borated-based electrolyte (OMBB) reported by Du et al.³⁶ The reported liquid electrolytes on Mg/S batteries with more than 50 cycles are summarized in Excel S1 (SI). The energy densities after cycles in Excel S1 are ranked, which is the product of reversible capacity and discharge voltage plateau at the last cycle. It indicates that the OMBB electrolyte is one of the most stable liquid electrolytes in the state-of-the-art Mg/S batteries, which is compatible with S cathode and Mg anode. Cell utilizing OMBB shows a high S utilization of 60.8% (discharge capacity of 1019 mAh g⁻¹) after 100 cycles without obvious capacity fade.³⁶ The electrochemical performance of this electrolyte reported in literature³⁶ is referenced to calculate the energy density in a realistic cell system discussed in the following part. Moreover, the mass ratio of S/carbon nanotubes (CNTs)/super-P/PVDF of 64/16/10/10³⁶ is adopted as the cathode composition, which is reported in the same literature using the OMBB electrolyte. The CNT can disperse super-P to retaining high contact surface area with S and enhance the whole electronic conductivity of cathode composite. We assume that porosity in cathode is 60 vol% to accommodate the volume change of cathode given that cathode porosity should be optimized at 50 to 60 vol% in liquid Li/S cells to achieve a highest energy density.¹⁰⁶ There exists a critical electrolyte volume (ie, critical ratio of E/S has been saved in an Excel S2 [SI]) where liquid electrolyte fills all the pores of cathode and separator exactly. The cathode is coated on a carbon-coated Al foil with a thickness of 18 μm. The reasons why carbon-coated Al foil is used as cathode current collector instead of Cu foil are as follows: (1) Cu current collector could react with S to form copper sulfides,^{36,107,108} while carbon-coated Al foil is compatible with S; (2) electrochemical oxidation stability of 0.5 M OMBB electrolyte is 3 V vs Mg/Mg²⁺ measured by linear sweep voltammograms, which indicates a relatively high oxidation stability of electrolyte on Al foil; (3) carbon-coated on two sides of Al foil can protect the Al foil from corrosion of Cl⁻ in the electrolyte; and (4) the carbon on Al foil can improve adhesion to electrode material, thus achieving a higher S loading. The separator is Celgard 2500 with a thickness of 25 μm. Celgard separator is thinner than glass fiber separator. Therefore, adapting Celgard separator can improve the gravimetric and volumetric energy density of Mg/S batteries. Here, Celgard 2500 is used as a typical Celgard separator in the Mg/S cell (Figure 2A). The porosity of Celgard 2500 is 55 vol%. The cathode and anode tabs are Nickel foils with a fixed mass of 0.16 g per piece. The volume of tab is very small,

thus ignored in our calculation. The practical E_g and E_v can be calculated by Formulas (5) and (6), respectively¹⁰⁹

$$E_g = \frac{Vm_s \cdot C^*A}{\sum W_i} \quad (5)$$

$$E_v = \frac{Vm_s \cdot C^*A}{\sum W_i/\rho_i} \quad (6)$$

where V is the average discharge voltage (V), m_s is the S loading (g cm⁻²) on cathode, C is the specific discharge capacity (mAh g⁻¹), A is the cross-sectional area of S cathode (ie, 8 × 12 cm²), and $\sum W_i$ and $\sum W_i/\rho_i$ are the total mass and volume of components of the pouch cell, respectively. The density of components (ρ_i) of the pouch cell is listed in Table S2.

Many parameters can affect Mg/S batteries energy density, such as S loading, S content, S utilization, average discharge voltage, and E/S. First, an ideal cell of 100 wt% S content cathode with a theoretical discharge capacity of 1672 mAh g⁻¹ and a theoretical discharge voltage of 1.77 V is analyzed. The S loading and E/S ratio are variables to investigate their effect on battery energy density. The ideal cell's parameters are summarized in Table S3. Based on S loading (m_s), E/S ratio, and cell structure, the mass of each component is calculated in Table S4. Combined with the density of each component, the thickness of each component is calculated in Table S5. Consequently, the E_g and E_v of ideal pouch cell vs S loading (0–12 mg cm⁻²) with various E/S ratio (0.5–12 μL mg⁻¹) are plotted in Figure 2B,C, respectively. The energy density generally increases with increasing S loading. For a specified E/S ratio, both the E_g and E_v increase much faster with S loading less than 6 mg cm⁻², and then both tend to increase slowly. For a specified S loading, increasing E/S will decrease energy density rapidly in the range of E/S less than 3 μL mg⁻¹. However, when E/S is further increased, the E_g and E_v drop slowly.

Considering that practical batteries cannot reach the 100 wt% sulfur content, 100% S utilization and theoretical discharge voltage, we calculated the energy density of a realistic pouch cell. The realistic pouch cell has the cathode composed of 64 wt% S, 16 wt% CNT, 10 wt% super-P, and 10 wt% PVDF binder, with 0.5 M OMBB. The parameters of the realistic pouch cell are shown in Table S6. First, the effect of S loading and E/S ratio on energy density is analyzed. With this OMBB electrolyte, the reported 60.8% S utilization (1019 mAh g⁻¹) and average discharge voltage of 1.2 V are treated as constants.³⁶ The mass and thickness of components in a realistic pouch cell are calculated in Tables S7 and S8. The resulting energy density as a function of S loading from 1 to 12 mg cm⁻² and E/S from 0.5 to 12 μL mg⁻¹ is shown in Figure 2D,E. Under

low E/S ratio (smaller than $3 \mu\text{L mg}^{-1}$), increasing S loading will increase E_g and E_v rapidly, while under high E/S ratio (larger than $3 \mu\text{L mg}^{-1}$), the E_g and E_v increase slowly with increased S loading, and tend to be flat earlier with S loading larger than 6 mg cm^{-2} . The gravimetric energy density in Figure 2D is close to 200 Wh kg^{-1} , which is comparable with most of present commercial LIBs, with E/S ratio of $1 \mu\text{L mg}^{-1}$ and S loading of 12 mg cm^{-2} . The E_v of cell with E/S ratio of 0.5 and 1 are the same. This is because the liquid electrolyte has not fully filled the total pore volume of cathode and separator. The maximum volumetric energy density in Figure 2E is 257 Wh L^{-1} with E/S of 0.5 or $1 \mu\text{L mg}^{-1}$ and S loading of 12 mg cm^{-2} , which is much smaller than 600 Wh L^{-1} of present LIB.¹¹⁰ This is attributed to low discharge voltage (1.2 V) and S utilization (60.8%) in cathode.

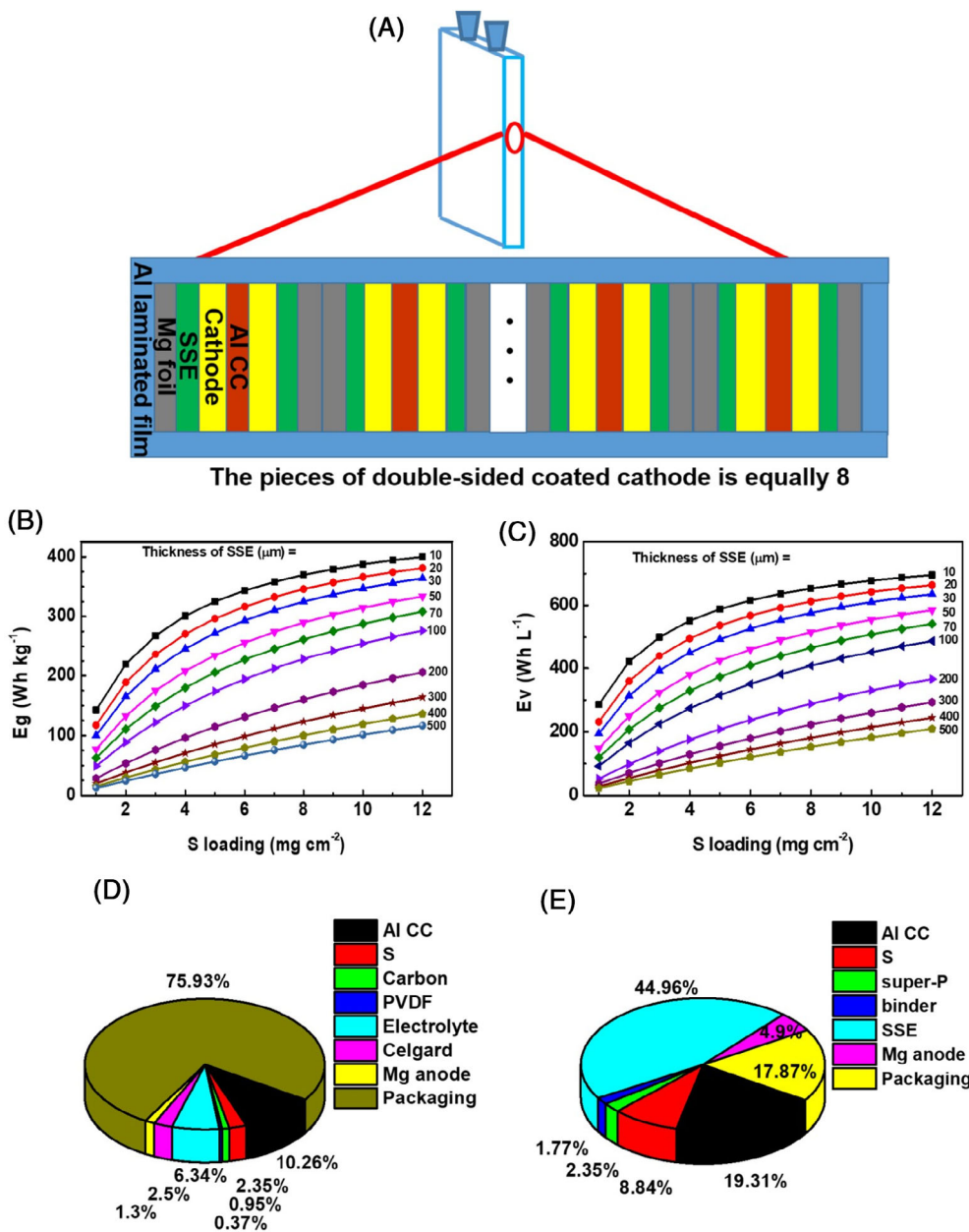
In addition to S loading and E/S, S content and sulfur utilization are also investigated towards the E_g and E_v . According to analyses above, the S loading is fixed at 6 mg cm^{-2} , and the E/S is optimized as $3 \mu\text{L mg}^{-1}$. The average discharge voltage is assumed at theoretical voltage (1.77 V). In this case, S content is varied from 20 to 100 wt%, PVDF binder content is fixed at 10 wt%, and the weight ratio of CNT and super-P is maintained at 16/10 (wt/wt), the same as that in the above realistic pouch cell cathode. S utilization is transferred into discharge capacity (mAh g^{-1}) of S. This cell components' mass and thickness are calculated in Tables S9 and S10. Given the above conditions, E_g and E_v vs S content and discharge capacity are shown in Figure 2F,G. As can be seen, the E_g and E_v increase slowly as S content increases. This indicates that it is not efficient to increase the energy density of Mg/S batteries by increasing S content only. Instead, S utilization and S content should be considered together to optimize energy density. Further, the S utilization is a key electrochemical parameter to impact both E_g and E_v . Increasing discharge capacity can remarkably increase both E_g and E_v . If the discharge capacity is 1400 mAh g^{-1} , the E_g can reach 200 Wh kg^{-1} of the present commercial LIBs with a sulfur content of 50 wt%. Nevertheless, the current maximum discharge capacity reported is 1384 mAh g^{-1} at first discharge with a discharge voltage of 1.37 V when 18 wt% S content is present in cathode.³⁵ Combining this result with Figure 2F,G, the E_g and E_v are estimated to be much smaller than 200 Wh kg^{-1} and 600 Wh L^{-1} , respectively. Therefore, improving S utilization and average discharge voltage is urgent to improve both E_g and E_v of Mg/S batteries.

As described, the present Mg/S pouch cell with liquid electrolyte can hardly achieve the E_g of 200 Wh kg^{-1} and E_v of 600 Wh L^{-1} unless the discharge capacity reaches 1400 mAh g^{-1} and average discharge voltage is close to

the theoretical voltage of 1.77 V with optimized S loading (6 mg cm^{-2}) and E/S ratio ($3 \mu\text{L mg}^{-1}$). However, it may be difficult to achieve these parameters in Mg/S batteries. Moreover, the polysulfide could dissolve in liquid electrolyte and reduce the battery discharge capacity and cycle life. Considering these drawbacks, it is natural to think about Mg/S batteries with SSEs. Inspired by Cao et al.,¹⁰³ the battery is designed as a pouch cell shown in Figure 3A. The pieces of double-sided coated cathode are 8. The SSE and anode have the same number of pieces, that is, 16. The cathode material is coated on carbon-coated Al foil of $18 \mu\text{m}$ thickness. The cathode has weight ratio of S/PVDF/Super-P/SSE of 50/10/13.3/26.7, which is referred from solid-state Li/S batteries.¹¹¹ Besides, the cathode porosity is set at 15 vol% to accommodate the volume change of the cell,¹⁵ which is an optimized value compared with solid-state Li-S batteries in which 15% to 20% porosity of cathode should be retained¹¹¹ and commercial LIBs cathode with a porosity of about 30 vol%.¹¹² The anode is Mg foil with a capacity of 1.2 times of cathode capacity. No anode current collector is used.¹¹³ By reviewing the reported Mg-ion-based SSEs, Mg(Tf)₂-MgAl₂O₄-PVDF-HFP ceramic polymer composite electrolyte is chosen in this battery design, which has a high conductivity of 4 mS cm^{-1} , potential window of 3.3 V, and transference number of 0.66, the state-of-the-art Mg-ion solid-state conductor.¹¹⁴ However, we note that this electrolyte has not yet been tested in Mg/S system. An ideal SSE should possess high ionic conductivity and at the same time be compatible with anode and cathode materials.^{115,116} In this design, S utilization and average discharge voltage are fixed at 60.8% (1019 mAh g^{-1}) and 1.2 V, respectively, to be consistent with the realistic liquid Mg/S batteries. The S loading and thickness of SSEs are treated as variables to estimate the E_g and E_v of this solid-state battery. The above design parameters of this solid-state Mg/S battery are listed in Table S11. The mass and thickness of each component in the solid-state Mg/S pouch cell are calculated in Tables S12 and S13, respectively.

The E_g and E_v of solid-state Mg/S pouch cell have improved as shown in Figure 3B,C. The cell with thickness of SSE less than $100 \mu\text{m}$ and S loading more than 7 mg cm^{-2} can all reach 200 Wh kg^{-1} energy density (present energy density of LIBs). Further reducing the thickness of SSE to $10 \mu\text{m}$ and increase S loading to 12 mg cm^{-2} increase energy density dramatically, reaching 400 Wh kg^{-1} and 700 Wh L^{-1} . Besides, the S loading can affect the E_g and E_v greatly. The E_g and E_v increase rapidly with increasing S loading within 4 mg cm^{-2} , while increase rates of the E_g and E_v become slower when S loading is beyond 4 mg cm^{-2} . However, when the thickness of SSE is larger than $200 \mu\text{m}$, the

FIGURE 3 Gravimetric and volumetric energy density estimation of magnesium-sulfur (Mg/S) batteries with solid-state electrolytes: A, the structure of pouch cell with solid-state electrolytes; B, the gravimetric; and C, volumetric energy density of solid-state Mg/S pouch cells with varied S loading and thickness of solid-state electrolytes, but fixed average discharge voltage of 1.2 V and S utilization of 60.8% (ie, 1019 mAh g⁻¹); D, mass distribution of pouch cell with liquid electrolyte; and E, solid-state electrolyte with same discharge capacity of 1019 mAh g⁻¹ and discharge voltage of 1.2 V. The S loadings in (D) and (E) are same (1 mg cm⁻²). The E/S in (D) is 2.7 μL mg⁻¹ in order to attain 15 vol% porosity in cathode the same as that of cathode in solid-state cell. The thickness of solid-state electrolyte (SSE) separator is 25 μm the same as Celgard 2500



energy density has almost a linear relationship with S loading. The high *E_g* of solid-state Mg/S batteries results from stacked anode and cathode in the solid-state pouch cell, which prominently augments discharge capacity in cell level. Moreover, in the pouch cell with liquid electrolyte, the packaging (containing Al laminated film and tabs) takes up a large percentage of total cell mass (75.93%), while in the solid-state pouch cell the packaging mass percentage (17.87%) decreases and active material mass percentage increases, which contributes to larger gravimetric energy density. This can be proved by cell mass distribution pie figures of the pouch cell with liquid electrolyte (Figure 3D) and SSE (Figure 3E). The average discharge voltage and capacity reported are low (1.2 V and 1019 mAh g⁻¹, respectively), energy density of

solid-state Mg/S cell can be further improved when the voltage is raised from 1.2 V to near 1.77 V and discharge capacity is increased from current 1019 to 1672 mAh g⁻¹.

3.2 | Parameterization of Mg/S batteries components based on cost

The cell material cost is calculated based on each material cost and cell structure parameters. The cell structure is consistent with the ones discussed above with liquid electrolyte or SSE. First, the Mg/S pouch cell with liquid electrolyte is considered, which is composed of Mg foil anode, Celgard 2500, S/CNT/Super-P/PVDF cathode, carbon-coated Al foil current collector, and packaging

materials. The price of each material is collected from online data or recent literatures,¹¹⁷ which is listed in Table S14. The cell material cost is calculated according to Equation (7).¹⁰⁹

$$P_T = \frac{\sum C_i m_i * A + \sum C_j * A}{V \cdot m_s \cdot C * A} \quad (7)$$

where P_T is the total cost per kWh of the pouch cell, C_i and C_j are cost per gram of material “ i ” ($\$ \text{g}^{-1}$) and cost per area of component “ j ” ($\$ \text{cm}^{-2}$), m_i is the mass loading of material “ i ” (g cm^{-2}), V is the discharge voltage of the cell, m_s is the mass loading of sulfur (g cm^{-2}), C is the discharge capacity (mAh g^{-1}), and A is the material corresponding area. Because there is no commercialized Mg/S cell as a reference, the processing cost is not considered.

The S loading and cost of liquid electrolyte are used as variables to investigate their effect on cell material cost with fixed average discharge voltage of 1.2 V, S utilization of 60.8% (1019 mAh g^{-1}), E/S ratio of $3 \mu\text{L mg}^{-1}$. The cell structure is the same as Figure 2A. The cost of 0.5 M OMBB liquid electrolyte used in this cell is calculated to be $23 \text{ \$ g}^{-1}$ according to its composition (in SI below Table S16), which is three orders of magnitude higher than liquid electrolyte cost of LIBs.¹⁰⁹ Therefore, the cost of liquid electrolyte is in the range of 0.1 to $23 \text{ \$ g}^{-1}$. The cost of each component of Mg/S batteries is calculated in Table S15. The S loading is transferred into E_g (Wh kg^{-1}) shown in Figure 4A. The cell material cost of the Mg/S pouch cell with liquid electrolyte is much higher compared with the price of LIBs of $174 \text{ \$ kWh}^{-1}$ in 2018. The S loading in the range of 1 to 12 mg cm^{-2} has a feeble influence on cell material cost ($\text{\$ kWh}^{-1}$), while the cost of liquid electrolyte has a prominent effect on cell material cost. This indicates that decreasing cost of liquid electrolyte can largely reduce the total price of cell.

Second, the effect of S loading and cost of SSE on cell material cost of solid-state Mg/S cell is considered. The cell structure is the same as shown in Figure 3A. If S loading is aimed at 2 mg cm^{-2} (the reported maximum S loading on Mg/S batteries is 2 mg cm^{-2}), only pouch cell with $10 \mu\text{m}$ thickness can achieve 200 Wh kg^{-1} under the condition that the discharge capacity of 1019 mAh g^{-1} and average discharge voltage of 1.2 V. Therefore, the thickness of SSE is set at $10 \mu\text{m}$. The discharge capacity is 1019 mAh g^{-1} , the average discharge voltage is fixed at 1.2 V, and the S loading is varied from 1 to 12 mg cm^{-2} , consistent with above energy density analysis. The cost of the $\text{Mg}(\text{Tf})_2\text{-MgAl}_2\text{O}_4\text{-PVDF-HFP}$ ceramic polymer composite electrolyte is calculated based on its components price (The components price is in Table S14).

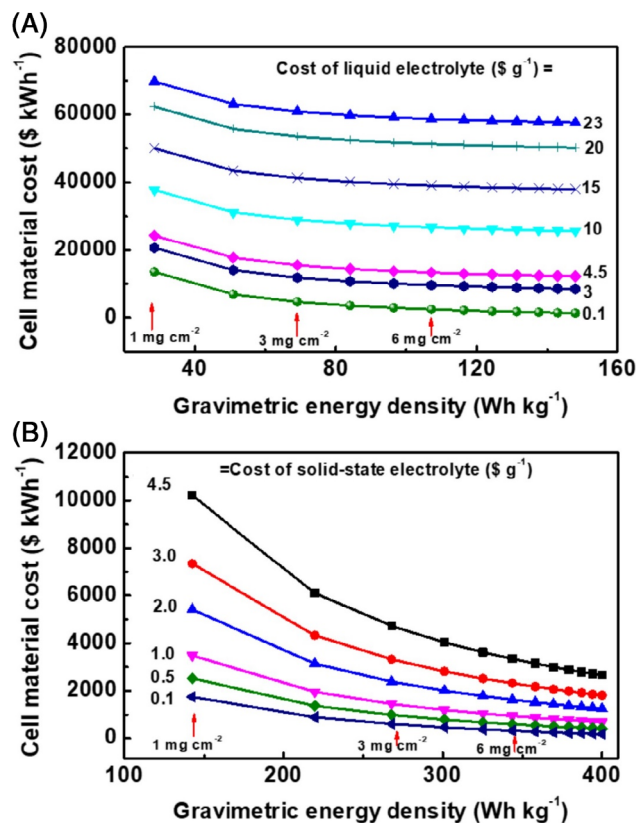


FIGURE 4 The estimated material price for magnesium-sulfur (Mg/S) pouch cells with different liquid electrolyte costs, A, and solid-state electrolyte (SSE) costs, B. The S loading varies from 1 to 12 mg cm^{-2} resulting in different gravimetric energy density and fixed discharge capacity of 1019 mAh g^{-1} , average discharge voltage of 1.2 V in both (A) and (B). In A, the pouch cell has E/S ratio of $3 \mu\text{L mg}^{-1}$. In B, the SSE is $\text{Mg}(\text{Tf})_2\text{-MgAl}_2\text{O}_4\text{-PVDF-HFP}$ ceramic polymer composite electrolyte. The $10 \mu\text{m}$ SSE cost varied from 0.5 to $4.5 \text{ \$ g}^{-1}$

$$C_{\text{SSE}} = \frac{C_{\text{EC}} + C_{\text{PC}} + C_{\text{Mg}(\text{Tf})_2} + C_{\text{PVDF-HFP}} + C_{\text{MgAl}_2\text{O}_4}}{m_{\text{solution}} + m_{\text{PVDF-HFP}} + m_{\text{MgAl}_2\text{O}_4}} = 4.5 \text{ \$ g}^{-1}$$

where C and m present cost and mass of each composition, respectively. Based on this calculation, the cost of SSE is assumed to vary from 0.1 to $4.5 \text{ \$ g}^{-1}$. The material cost of solid-state Mg/S batteries is calculated in Table S16. Contrasted to pouch cell with liquid electrolyte, the cell material cost decreases with increased S loading obviously, as shown in Figure 4B. Besides, the cell material cost difference with different cost of SSE is larger in lower S loading (smaller than 2 mg cm^{-2}) than higher S loading (larger than 3 mg cm^{-2}). This indicates that if the energy density of solid-state Mg/S batteries is high, the small fluctuated price of SSE plays a weak function on cell cost. The much cheaper solid-state cell than the cell with liquid electrolyte results from three reasons. First is that SSE price is much smaller than liquid

electrolyte. Second is larger energy density of solid-state pouch cell. The last is that the cost of batteries does not consider the processing cost. This is in stark contrast to the scenario of Li-ion vs solid-state Li battery, where the cost is expected to rise in solid-state batteries.

4 | CONCLUDING REMARKS AND FUTURE PERSPECTIVES

This review comprehensively and critically discusses the Mg/S batteries technology with respect to material development, literature review analysis, energy density, and cost. In spite of recent progress, critical challenges still exist, including the low discharge potential, passivation layer on the Mg anode surface, sluggish ion transfer, the shuttling effect of polysulfides, the relatively low areal capacity, and so forth. Nevertheless, these challenges should be regarded as the driving force for research in the future, which definitely will promote more discoveries of battery materials, battery configurations, and associated battery chemistries.

We propose the following strategies, which might provide deeper insight and pathway to new technologies.

1. The rational design of S hosts as cathode is highly desired to accomplish better performance in Mg/S batteries. Hence, for long life Mg/S batteries, novel conductive hosts need to be designed, which show robust chemical interactions with Mg-PS_x based on interfacial phenomena rather than spatial confinement to mitigate the shuttle effect and possess high electrical conductivity to improve the S utilization. Furthermore, porous nanostructured materials with abundant interfaces and the tenable exposed surfaces may satisfy the possibility of significant enhancement to anchor Mg-PS_x, leading to a stable cyclic performance in Mg/S batteries.
2. Besides the impact of electrolyte on the battery performance, reducing volume and cost of liquid electrolyte in battery are vital to obtain high energy density and low cost Mg/S batteries. Limited by estimated energy density of liquid Mg/S batteries, it is prospective to explore SSEs for much higher energy density.
3. The high capacity alloy anode materials as well as a suitable protective and conductive artificial interphase on Mg anode might be effective approaches to protect the metal surface.
4. Besides the innovations from a material perspective to build better Mg/S batteries, critical mechanistic understanding of Mg/S systems should also deserve special attention.

5. Reasonable parameter design of cell is important to achieve high energy density of Mg/S batteries. For Mg/S batteries with liquid electrolytes, increasing S loading and decreasing E/S ratio are necessary. However, the current reported maximum S loading is 2 mg cm⁻² and minimum E/S ratio is 64 μL mg⁻¹. Moreover, both reducing cost of liquid electrolyte and improving discharge capacity and voltage are beneficial to obtain the high energy density and low cost for Mg/S batteries. For solid-state Mg/S batteries, it is promising to achieve much higher energy density than liquid Mg/S batteries if a suitable SSE with thickness of several tens of micrometers is prepared.

Mg/S batteries are currently in a nascent stage of progress. With ongoing research progress in lifetime and realistic energy density, a practical and reliable Mg/S cell might be soon realized.

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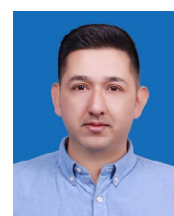
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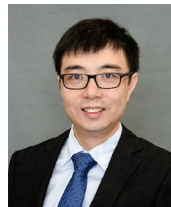


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SUPPORTING INFORMATION

Additional supporting information may be found online in the Supporting Information section at the end of this article.

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