## Supporting information for "Long-term Earth-Moon evolution with high-level orbit and ocean tide models"

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## Alternative solution for lunar equatorial tilt

In the Daher et al. paper that this supporting information accompanies, the lunar equatorial tilt I is solved for using equation (43) of that paper, which is taken from Ward (1975). Here we present an alternative solution for I, taken from equation (52c) of Williams et al. (2001):

$$\sin I = \frac{G_t}{G_b},\tag{1}$$

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$$G_t = -3n^2 \sin i \cos(\sigma - \tau)(0.9865\beta + 0.0041\alpha + E),$$
(2)

$$G_b = 2.0002 \frac{d\Omega}{dt} \omega_z + 3n^2 (0.9754\beta + 0.0048\alpha + E) - 1.9982 (\frac{d\Omega}{dt})^2 - 2\frac{dF}{dt} \frac{K_{Moon}}{C_{Moon}} \frac{\xi}{1+\xi^2}, \quad (3)$$

 $\sigma$  is a physical libration angle, and  $\tau$  is the physical libration in longitude. Here

$$\alpha = \frac{C_{Moon} - B_{Moon}}{A_{Moon}} = \frac{\beta - \gamma}{1 - \beta\gamma},\tag{4}$$

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$$E = \frac{k_{2Moon}\zeta}{3}, \qquad \qquad \zeta = \frac{M_M R_M^2}{C_{Moon}} \frac{M_E}{M_M} (\frac{R_M}{a})^3, \qquad (5)$$

$$\frac{dF}{dt} = n - \frac{d\Omega}{dt},\tag{6}$$

and  $\omega_z$ , the body-referenced z-component of the Moon's angular velocity vector, is given by

$$\omega_z = \frac{d\Omega}{dt}\cos(I) + \frac{dF}{dt}.$$
(7)

We evaluate  $\cos(\sigma - \tau)$  via Williams et al. (2001, equation 51):

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$$\sin(\sigma - \tau) = -\frac{K_{Moon}}{C_{Moon}(1 + \xi^2)} \frac{2\frac{dF}{dt} \sin I \cos I}{3n^2 \sin i(0.9840\beta + 0.0059\alpha)}.$$
(8)

47 The non-integer coefficients depend on the average  $U_{ij}$  functions in Williams et al. (2001).

Because  $K_{Moon}/C_{Moon}$ ,  $\kappa$  (see equation 52 in main text),  $\xi$ , and I are inter-related, 48 they are obtained with an iterative solver. For some parameter values, small imaginary 49 values crop up, and are omitted. Near and within the Cassini state transition, the solver 50 is unable to find solutions for some values of a, in which case it assigns "NaN" (Not a 51 Number) values to the parameters  $K_{Moon}/C_{Moon}$ ,  $\xi$ , and I. For a small number of a val-52 ues near or within the transition, parameter values can contain large imaginary values, 53 or absolute values of I that exceed 90 degrees. In cases where the imaginary part of the 54 solution of  $K_{Moon}/C_{Moon}$ ,  $\xi$ , or I is 1% or more of the real part of the solution, or where 55 |I| exceeds 90 degrees, we assign values of all three parameters  $(K_{Moon}/C_{Moon}, \xi, \text{ and})$ 56 I) to "NaN". 57

We first compare the values of lunar equatorial tilt I using the Ward (1975) equa-58 tion (equation 43, Daher et al.) versus the Williams et al. (2001) equation (1) in the case 59 where the lunar inclination i is assumed to be fixed. We choose values of  $i=5.145^{\circ}$ , the 60 present-day value, and  $i=15.18^{\circ}$ , the 4.5 Ga mean value of i from the Monte Carlo sim-61 ulations (Table 8, Daher et al.), and plot I as a function of a (supporting information 62 Figure 1). For both of these fixed i values, the values of I taken from the two solutions 63 lie close together over the part of parameter space where |I| is small. Both the Ward and 64 Williams solutions display a Cassini state transition, near which the I values diverge from 65 each other. In the Ward solutions, the transition takes place at about a=33.7R for the 66 present-day i value of  $5.145^{\circ}$  and at about a=31.5R for the 4.5 Ga mean i value of  $15.18^{\circ}$ . 67 In the Williams solutions for  $i=5.145^{\circ}$ , there is a gap, between about 35.5 and 37.7 R, 68 where only a small number of solutions for I that meet the criteria above (small imag-69 inary values, assigned to non-NaN values, etc.) exists. Similarly, when  $i=15.18^{\circ}$ , there 70 is a gap between about 33.0 and 39.7 R with only a small number of solutions. A back-71 wards integration of the orbital dynamics solutions in Daher et al. using (1) has the po-72 tential to fail, if a becomes small enough that the solutions for I fall into this gap, as may 73 happen in some of our future simulations. For this reason, the solutions displayed in Da-74 her et al. (Figures 5 to 11), employ the Ward (1975) (equation 43, Daher et al.). 75

In the Daher et al. orbital dynamics solutions that employ ocean tide model results, *a* never becomes small enough for a Cassini state transition to take place. Therefore, we are able to successfully employ the Williams et al. (2001) equation (1) in backwards 4.5 Ga integrations. We employed equation (1) in simulations that use the four



Figure 1. Lunar equatorial tilt I, plotted vs. semi-major axis a, computed from Williams et al. (2001) equation (1) and from Ward (1975) (equation 43 in Daher et al.), using (a) presentday i value of  $5.145^{\circ}$  and (b) the 4.5 Ga mean i value of  $15.18^{\circ}$  (Table 8 in Daher et al.). The curves are based upon 9001 values of semi-major axis a. The Williams et al. (2001) solutions are plotted as light-colored dots, which appear to be continuous over much of parameter space; small numbers of isolated solutions appear within the gap that covers the Cassini state transition.

- <sup>80</sup> fixed ocean basin geometries. Throughout the simulations employing the four basin ge-
- ometries, the differences between solutions that employ the Williams et al. (2001) equa-
- tion (1) vs. the Ward equation (43, in Daher et al.) are qualitatively similar. For brevity,
- we only display the solutions employing the PD geometry here. We plot Earth rotation
- period  $\frac{2\pi}{\omega_E}$ , obliquity  $\epsilon$ , semi-major axis a, eccentricity e, lunar orbit inclination i, and
- $_{25}$  lunar equatorial tilt I in supporting information Figure 2, for results that use the Williams
- et al. (2001) equation (1) vs. results obtained from the Ward (1975) solution (equation
- 43 in Daher et al.). The solutions for  $\frac{2\pi}{\omega_E}$  and  $\epsilon$  lie close together. The solutions for a and e display a small amount of divergence near the 4.5 Ga endpoint, and the solutions for
- e display a small amount of divergence near the 4.5 Ga endpoint, and the solutions for *i* and particularly *I* show the greatest amount of divergence. This summarizes our al-
- *i* and particularly *I* show the greatest amount of divergence. This summarizes our alternative method for computing the lunar equatorial tilt *I*, and the effects that the al-
- ternative method have on the orbital dynamics solutions.

## 92 **References**

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Figure 2. Orbital dynamics solutions employing the ocean tide results from fixed PD ocean basin geometry and the Williams et al. (2001) equation (1) vs. the Ward (1975) solution (equation 43 in Daher et al.) for lunar equatorial tilt *I*. Displayed are (a) Earth rotation period  $\frac{2\pi}{\omega_E}$ , (b) obliquity  $\varepsilon$ , (c) semi-major axis *a*, (d) eccentricity *e*, (e) lunar orbit inclination *i*, and (f) lunar equatorial tilt *I*.