

**THE UNIVERSITY OF MICHIGAN**  
**COLLEGE OF ENGINEERING**  
**DEPARTMENT OF ELECTRICAL ENGINEERING**  
**Radiation Laboratory**

**RADAR CROSS SECTION STUDIES OF A CONE-CYLINDER  
MODEL WITH AND WITHOUT FINS**

August 1962

Final Report  
Purchase Order DY-635706-00

Prepared by: R. E. Hiatt



5246-1-F = RL-2124

**Contract With:** Minneapolis-Honeywell Regulator Company  
2600 Ridgway Road  
Minneapolis 40, Minnesota

**Administered through:**  
**OFFICE OF RESEARCH ADMINISTRATION • ANN ARBOR**

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5246-1-F

Radar Cross Section Studies of a Cone-Cylinder Model with and without Fins

Final Report

August 1962

Prepared by: R. E. Hiatt

The experimental work was performed under the direction of E. F. Knott, assisted by T. E. Hon, R. J. Pelkey, and R. L. Wolford.

The theoretical analysis was made by T. B. A. Senior

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INTRODUCTION

At the request of Minneapolis-Honeywell and in accordance with the requirements of P. O. DY 635706, a limited study has been made of the cross section characteristics of a company-supplied model. The model is a cone-cylinder with detachable fins. It is approximately 12 feet long and the cylindrical portion is 13 inches in diameter. The cone section is  $32\frac{1}{2}$  inches long, making a cone half-angle of about  $11\frac{1}{2}^{\circ}$ . There are four fins, each 18 inches long; spaced  $90^{\circ}$  apart and extending 8.8 inches from the cylinder. The fins are curved in the radial direction, the radius of curvature being approximately equal to that of the cylindrical portion of the model. The fins are attached to a cylindrical sleeve 18 inches long which may be slipped on or off the base of the model. A sketch of the model is shown in Figure 1.

The study included measurements of radar scattering patterns at X- and S-band (9.3 and 2.87 gigacycles respectively). Measurements were made with the model in the horizontal flight condition and usually included the entire  $360^{\circ}$  azimuth coverage. Vertical and horizontal polarizations were used for each frequency and for each of these four frequency-polarization conditions, there were three fin conditions. The model was measured with 1) no fins, 2) fins in the vertical-horizontal condition ( $0^{\circ}$  roll angle), and 3) fins at  $45^{\circ}$  to the vertical ( $45^{\circ}$  roll angle).

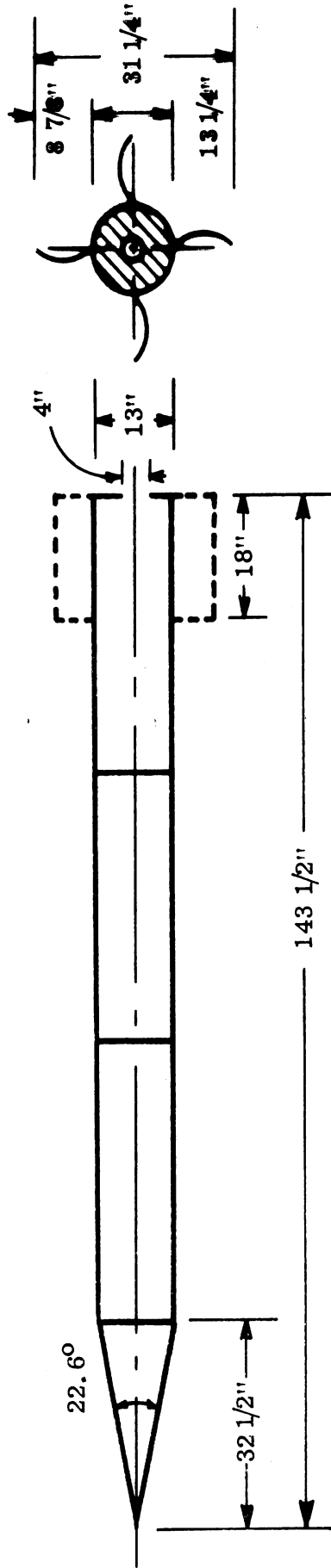


FIGURE 1: M-H CONE-CYLINDER MODEL



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## EXPERIMENTAL FACILITIES AND TECHNIQUES

The equipment used in the measurements is of the conventional cw type. A single antenna is used for both transmitting and receiving. The transmitted and received signals are separated by means of a waveguide hybrid tee acting as a balanced bridge. Since reflections from the load end of the bridge are being balanced against reflections both from the horn and from background scatterers hundreds of wavelengths beyond the horn aperture, one requires an oscillator which is very stable in frequency. At X-band, the required frequency stability is achieved by the use of cavity techniques. At S-band, the frequency stability is derived from a crystal oscillator. A frequency multiplier chain provides the crystal stability at the required microwave frequency.

The target under test is mounted on a styrofoam cylinder which rests on a pedestal placed at the desired range in front of the horn aperture. Prior to placing the model in position the bridge is balanced to minimize the signal to the receiver. When the target is in place, the reflected signal is fed to the super-heterodyne receiver and thence to the recorder. Chart movement in the recorder is synchronized with the rotation of the pedestal. Figure 2 shows a block diagram of the equipment.

The level of the scattered return is obtained by comparing it with the return from a calibrated corner reflector or sphere. The one square meter level thus obtained is indicated on each pattern.

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Measurements on the present model were made with the equipment inside the large open doors of a hangar, with the model and pedestal at a distance of 100 to 200 feet in front of the horn. Absorbing screens between the antenna and model served to minimize field variation at the model.

The measurement procedure was as follows. With no model present the receiver signal was minimized by the waveguide tuner adjustments. The model was then placed on the pedestal and its level checked by means of a theodolite. The 360° azimuth pattern was then run and the model was removed. If the receiver balance was satisfactory, a standard scatter was used to calibrate the level of the return. Before a pattern was selected as satisfactory, the measurement was repeated until three patterns showed a good agreement. For the peak returns, agreement to within a db was usually achieved. For the lower, near nose-on aspects, more attention was paid to the average level. This was usually in agreement to within one or two db.

It should be noted that the above-mentioned ranges are insufficient to meet far field requirements for broadside aspects of a 12 foot model<sup>+</sup>. The ranges used (208 feet for most of the X-band work and 100 feet for S-band) were near the maximum possible compatible with the equipment sensitivity and the model scattering pattern. The ranges are considered adequate for all but near broadside aspects.

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<sup>+</sup>Noted also in U of M Proposal ORA-62-1354-B1, dated 26 June 1962.

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The experimental return for the broadside aspect is expected to be less than the true value since the entire length of the model is not plane wave illuminated.

Another factor which served to decrease the experimental cross section for broadside and other aspects is the poor condition of the model. The model was fabricated from sheet aluminum, rolled into cylindrical or conical sections and welded. The ends of the three sections making up the cylinder were then welded together and this assembly was then welded to the cone. The resulting model differed from a true cone-cylinder quite considerably. Although the welded seams had been ground down, they still extended above the surrounding surface by more than  $1/8$  inch in many places. In other places, the aluminum surface was deformed so that it departed from a true cone or cylinder by as much as  $1/4$  inch. The flat sheet making up the base of the model was convex by about  $1/4$  inch. It is in order to mention these faults in the model since they would obviously produce an asymmetrical scattering pattern. In addition, the specular return from the cylinder, the side of the cone, and the base plate will tend to be lower, and the beamwidth of the scattered pattern broader, as a result of the above-mentioned deformities in the model.

## RESULTS

### 1. X-band

The X-band scattering patterns are shown in Figures 3 through 13 and the S-band patterns in Figures 14 through 21. The insert in the lower center of each pattern indicates the no-fin case or horizontal-vertical fins, or fins at  $45^\circ$ .

Figure 3 is for the no-fin case with X-band vertical polarization. There are prominent lobes at about the  $17 \text{ db} > M^2$  level for the tail and broadside aspects and lobes  $10 \text{ db} > M^2$  are seen at about  $77^\circ$  due to the specular return from the side of the cone. These lobes are characteristic of all the patterns for both frequencies and both polarizations. The broadside return is about 6 db below the theoretical value due to the near field illumination and the model defects. For a perfect model one would expect a single sharp lobe at  $90^\circ$  with a 3 db beamwidth of about  $0.3^\circ$ . In the present case and in several of the patterns that follow, the broadside lobe is composed of 2 or 3 peaks and the 3 db width is approximately  $2^\circ$ . The lobed behaviour is to be expected from a cylinder whose surface is wavy or irregular in the axial direction. These defects and the limited measurement range both tend to increase the beamwidth.

The theoretical value for the tail-on aspect allowing for the 4" diameter hole in the center is about 18.5 db. The experimental values obtained are in good agreement with this allowing for some degradation due to the convex nature

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of the base plate. The theoretical value for the specular return from the side of the cone is about  $10 \text{ db} > M^2$ . The experimental values are generally a little below this due also, it is believed, to the deformations in the side of the cone.

The experimental return for near nose-on aspects for  $0^\circ \pm 70^\circ$  is below the sensitivity of the system for the 200 foot range. Figure 3 shows that the level is at least  $13 \text{ db} < M^2$ . To determine the experimental level, additional X-band patterns were taken at a range of 100 feet for horizontal polarization. The results for the no-fin case (Figure 9) show the average return to be about  $19 \text{ db} < M^2$ . The calculated nose-on cross section, assuming a perfectly smooth cone-cylinder transition is  $21 \text{ db} < M^2$  ( independent of frequency). A projecting rim at the cone-cylinder transition will increase this return in proportion to the area of the projection. A projecting rim  $0.1 \lambda$  wide would, for example, result in a nose-on cross section of  $12 \text{ db} < M^2$ .

Figures 4 and 5 show the patterns for vertical polarization with fins. In Figure 4 the roll angle is  $0^\circ$  and in Figure 5 the roll angle is  $45^\circ$  with the fins inclined at  $45^\circ$  to the vertical. The major effect of the fins is to increase the return for the near nose-on aspects. A rough value for the average return for  $0^\circ \pm 70^\circ$  aspects is about  $10 \text{ db} < M^2$ . Another effect of the fins is to increase the broadside return. In this case the increase is 3 or 4 db. In other

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cases it is less. Additional measurements, some of which are not presented, showed that the  $90^\circ$  return with fins in place was sensitive to small changes in roll angle. The calculated effect of the fins at broadside is to add or subtract 1.5 db to the broadside return of the cone-cylinder. This is believed to account for most of the variation in the broadside return observed in the with-fin patterns.

Figures 6, 7, and 8 are for X-band horizontal polarization in the no-fin, fins at  $0^\circ$ , and fins at  $45^\circ$  cases respectively. As would be expected, there are no major polarization effects. It is probable that most of the observed differences in the two sets of patterns are due to repeatability problems and model asymmetries.

Figures 9, 10, and 11 are repeats of the conditions of 6, 7, and 8 but with the measurement range decreased to 100 feet. This was done to raise the level of the near nose-on aspects so that a more accurate picture could be obtained for the behaviour at these aspects. These figures present nose-on data only, including aspects from  $-72^\circ$  to  $+72^\circ$ . The average return for the no-fin case is about -19 db while for the two cases with fins the average is about -13 db with respect to  $M^2$ .

Figures 12 and 13 show scattering patterns for the fin section only for X-band horizontal polarization. In Figure 12 the axis of the fin section is horizontal and for Figure 13 the axis is vertical. The information contained in both of these patterns is of interest, but it should be noted that the patterns do not show the true return for

the fins as an addition to the large model. The presence of the 18-inch long cylindrical section would be expected to affect the return for all aspects. It will increase the return for the end-on view and for the broadside aspect, its effect will be to increase or decrease the fin return depending on the relative phase of the contributors. The end-on return, Figure 12, is seen to be on the same order of magnitude as the return from the finned model for nose-on aspects. Figure 13 shows the pronounced oscillation that occurs as the roll angle is changed. A maximum return is obtained when the model is viewed normal to a plane containing two fins. This return may be considered to be the return from the sum of the two halves which in this case are in phase. With a  $1^\circ$  or  $2^\circ$  rotation, the phase centers of the two returns move enough to cause the two returns to be out of phase and a null results. As the pattern shows, this phenomena occurs to some extent over the entire  $360^\circ$ .

## 2. S-band

Figures 14 through 21 show the S-band data. The major characteristics of the patterns are similar to those for X-band and has the same relative level of the main scattering peaks as would be expected. As would also be expected, the absolute level of the specular returns for tail, broadside and cone are lower for S-band.



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Figure 14, 15, and 16 are for vertical polarization for the no-fin, fins at  $0^\circ$ , and fins at  $45^\circ$  cases. The corresponding patterns for horizontal polarization are given in Figures 17, 18, and 19. The experimental base return for the two no-fin patterns agrees well with theoretical predictions ( $8.5 \text{ db} > M^2$ ). The experimental broadside return for the no-fin case is again much less (7 or 8 db) than the theoretical estimate. The reasons for this are believed to be the same as those mentioned in the discussion of the X-band results; the near field effects and the imperfect model both tending to reduce the experimental broadside return. The specular return from the side of the cone agrees fairly well with the theoretical value ( $4.5 \text{ db} > M^2$ ).

Compared to the X-band results, the experimental S-band nose-on return ( $12 \text{ db} < M^2$ ) is somewhat higher than expected. It is equivalent to the return which would be obtained from a projecting rim  $\lambda/100$  in depth at the cone-sphere junction.

To provide additional information on the fin contribution, patterns for the fins only are shown in Figures 20 and 21. In Figure 20, the axis of the cylindrical shell is horizontal and the polarization is horizontal. In Figure 21, the axis of the cylinder and the polarization are both vertical, so that in each of the two patterns the polarization is parallel to the axis of the cylinder. As noted in the discussion of the X-band data, we do not obtain the true value of the fin return in these patterns since the cylinder makes a contribution nearly equal to that for the fins for broadside and

probably for most other aspects. The effect of roll angle on the missile will not be as pronounced as that shown in Figure 21, since the fin contribution is small compared to the missile return at broadside aspects.

CONCLUSIONS

The experimental cross sections for the 12 foot cone-cylinder model for two polarizations, two frequencies, and 3 "fin conditions" have been presented in 19 patterns (Figures 3 - 21). Results of selected theoretical calculations are given in the following table in  $db > M^2$ .

Freq.	A S P E C T				
	Tail-on	Broadside	Cone flash	Nose-on no rim	Nose-on $\lambda/100$ rim
9.3Gc	18.5	24	10	-21	-12
2.87Gc	8.5	18.9	4.8	-21	-12

Allowing for the condition of the model, the agreement between theory and experiment is good except for the broadside aspects. This disagreement was expected and is largely due to limited illumination resulting from the short measurement range.

PATTERN No.

DATE

PROJECT

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ENGRS.

805

805

REMARKS

Freq 9.30 gc Vert Polar

Range 208.5' 10" CR

Model Minn-Honey

Roll 00 WITHOUT Fins

(db)

RELATIVE POWER

1MR →

4°  
24°  
144°

5°  
30°  
180°

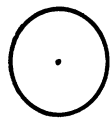
4°  
24°  
144°

108°

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Figure 3  
M-H Cone Cylinder Model w/ out Fine  
Freq. 9.3 Gc. Polarization V  
Model axis Horizontal with Nose at 0°

← 1 M<sup>2</sup>



0

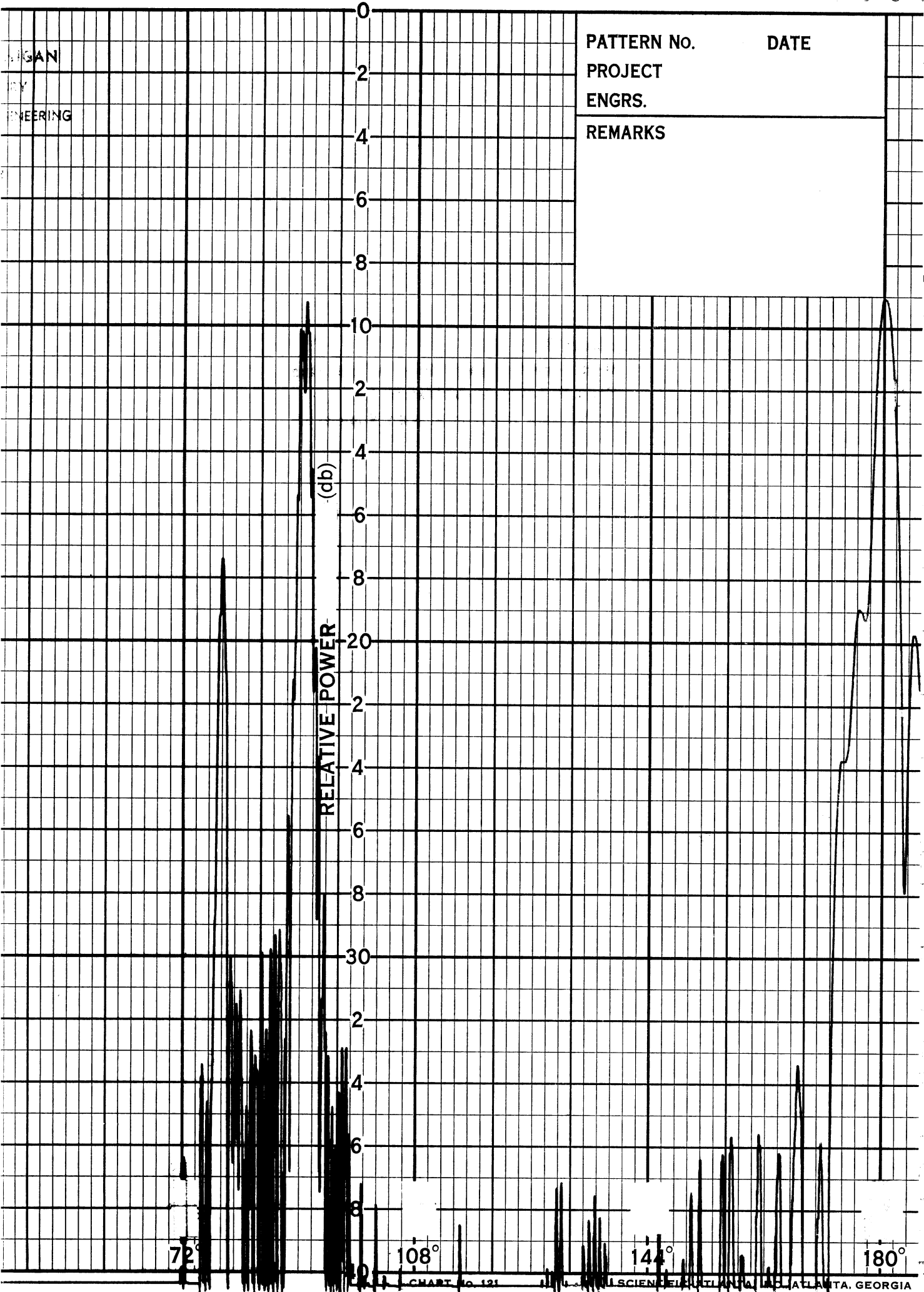
72°

36°

36°

FIGAN  
BY  
ENGINEERING

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PROJECT  
ENGRS.  
REMARKS



PATTERN NO.

DATE

PROJECT

JUL 18 1962

ENGRS.

808

a

REMARKS

Freq 9.30 gc Vert Polar

Range 208.5' 10'' CR

Model Minn-Honey

Roll 0° With Fins

RELATIVE POWER  
-(db)

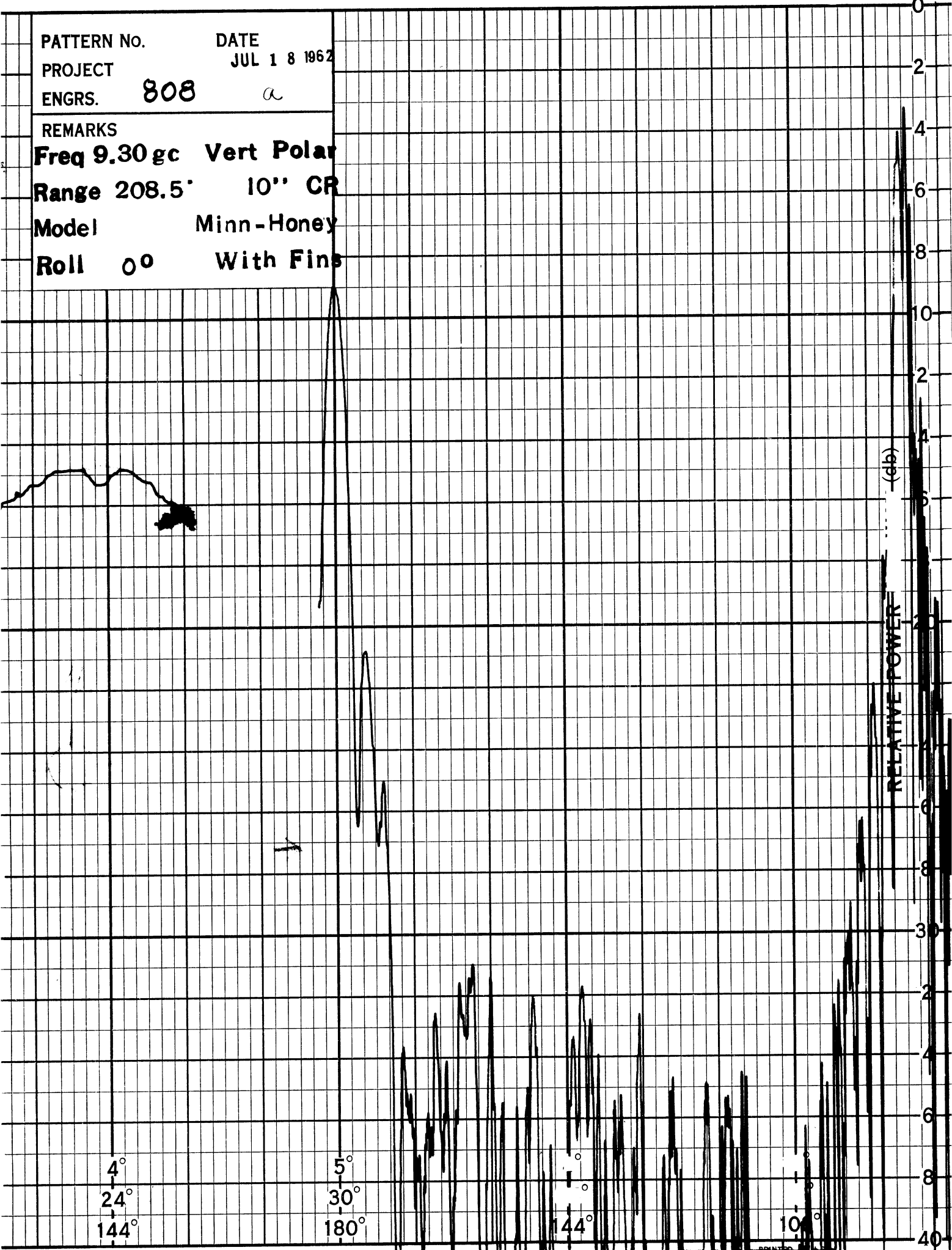
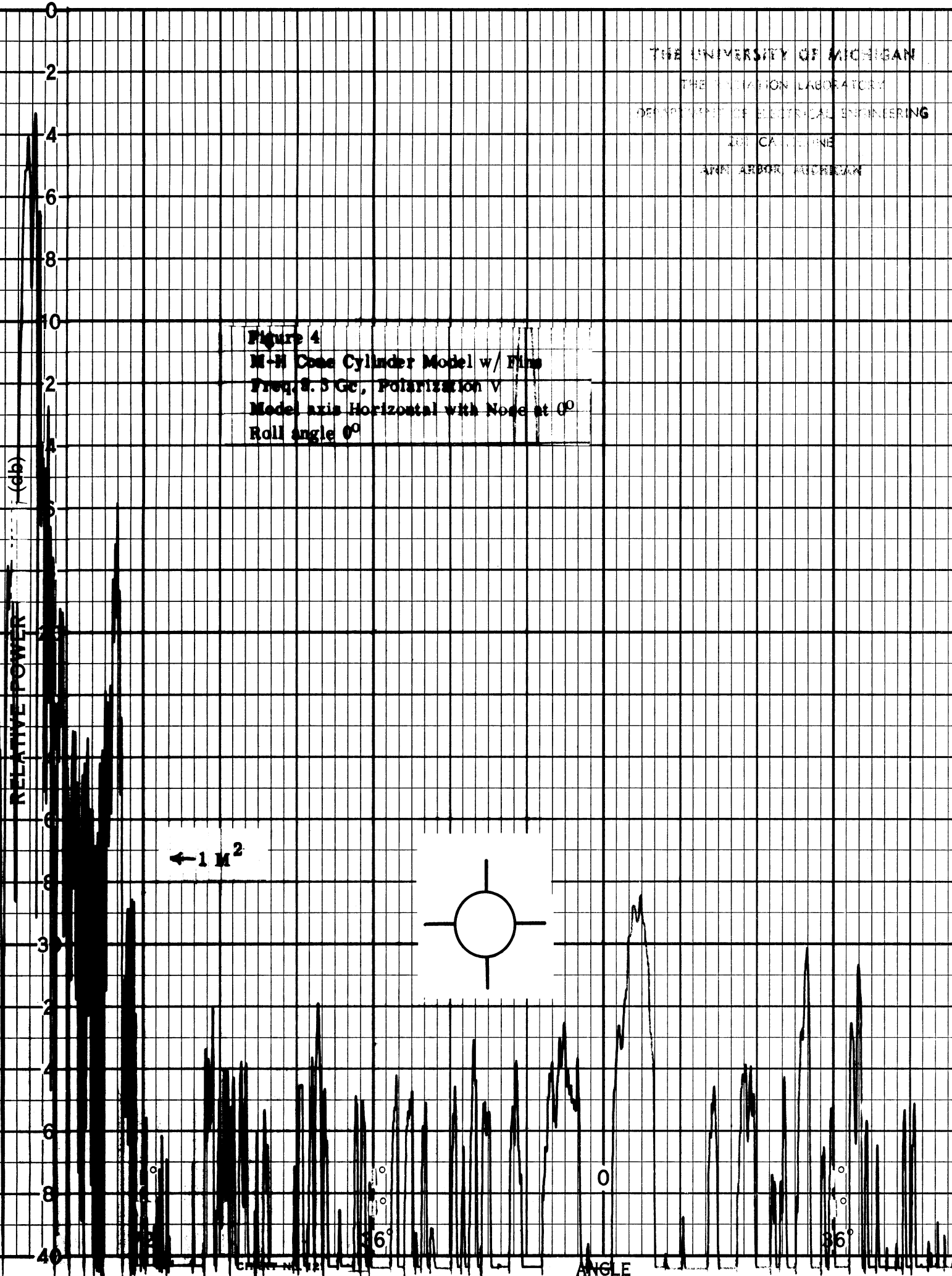
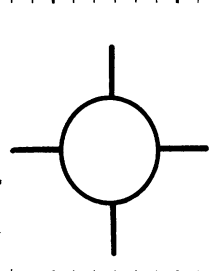


Figure 4  
M-H Cone Cylinder Model w/ Film  
Freq. 8.5 Gc, Polarization V  
Model axis Horizontal with Node at 0°  
Roll angle 0°



← 1 M<sup>2</sup>



36°

0

36°

ANGLE

CHIGAN  
FORM  
ENGINEERING

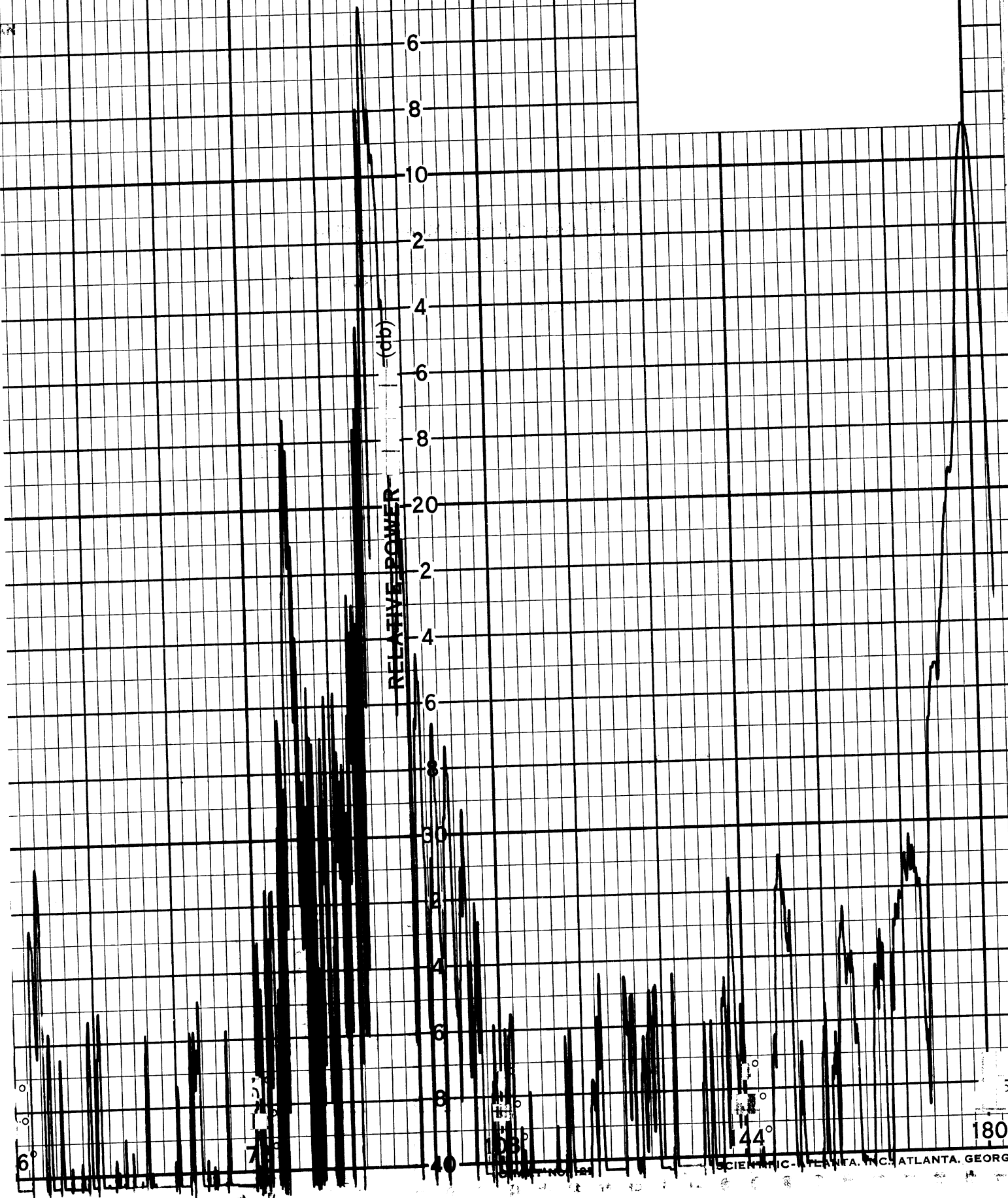
PATTERN No.  
PROJECT  
ENGRS.

DATE

REMARKS

0  
2  
4  
6  
8  
10  
2  
4  
6  
8  
20  
2  
4  
6  
8  
30  
2  
4  
6  
8  
40

RELATIVE POWER  
-(db)



6° 74° 108° 144° 180°

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PATTERN No.

DATE

PROJECT

JUL 18 1962

ENGRS.

815

a

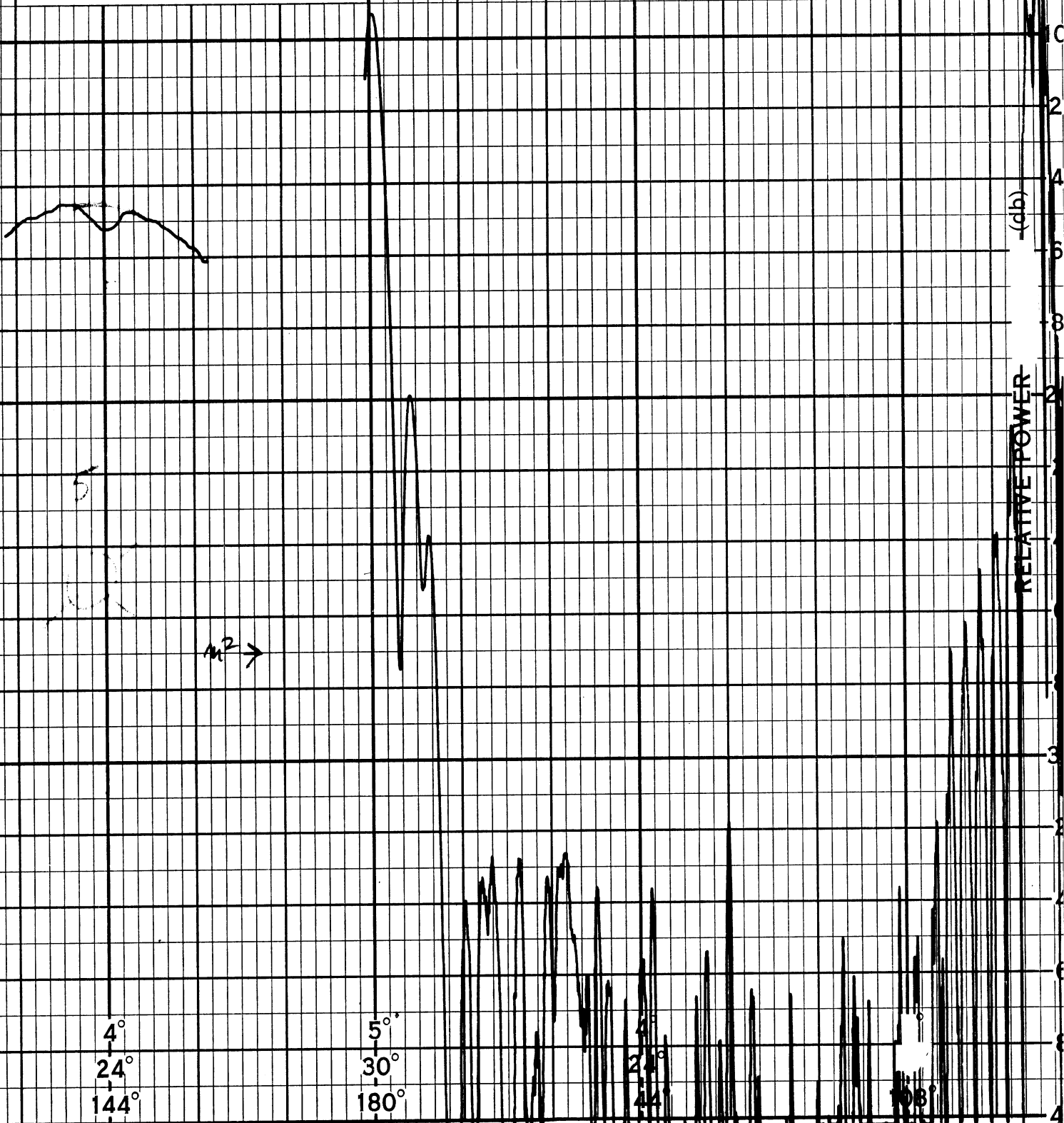
REMARKS

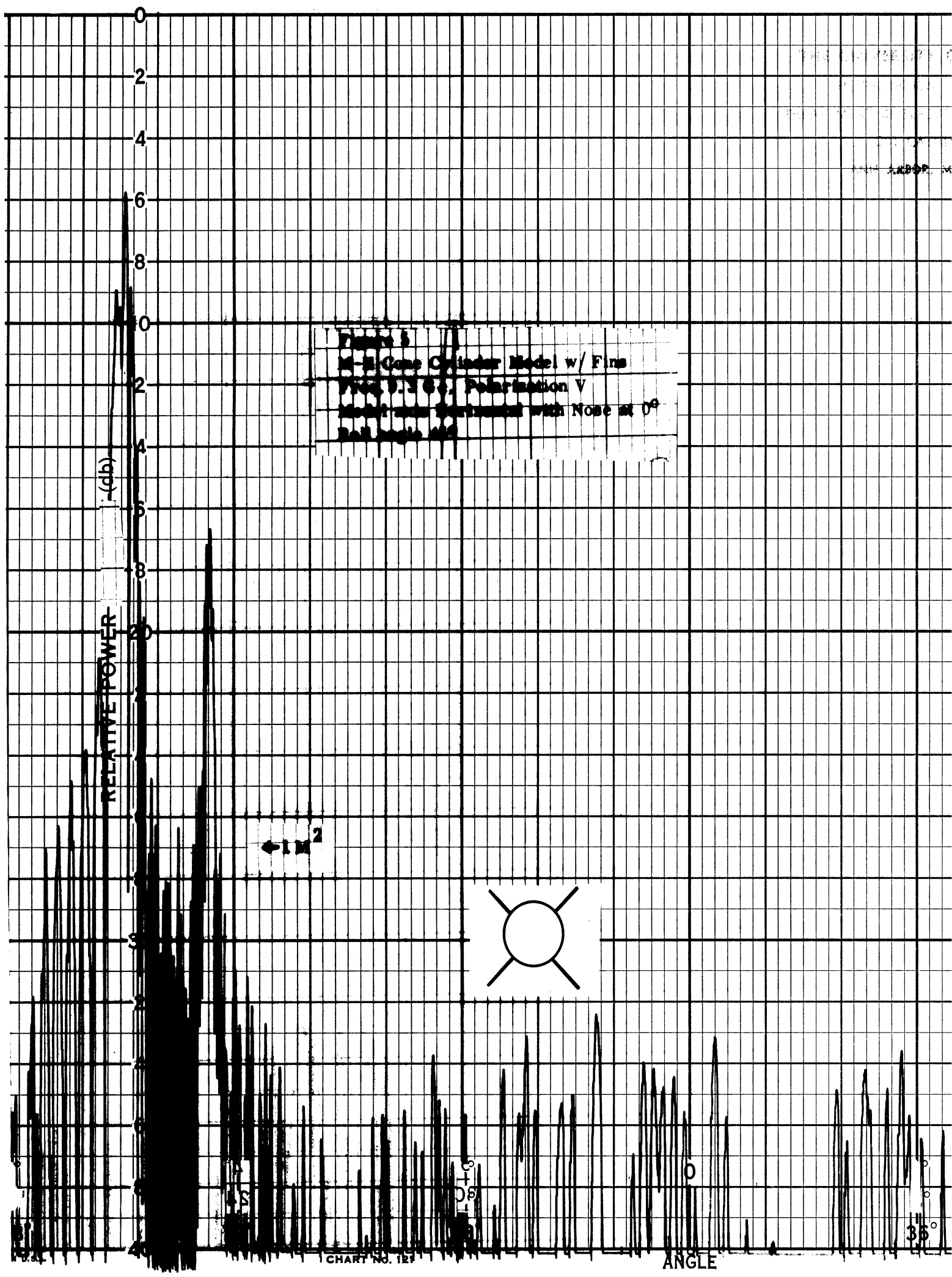
Freq 9.30 gc Vert Polar

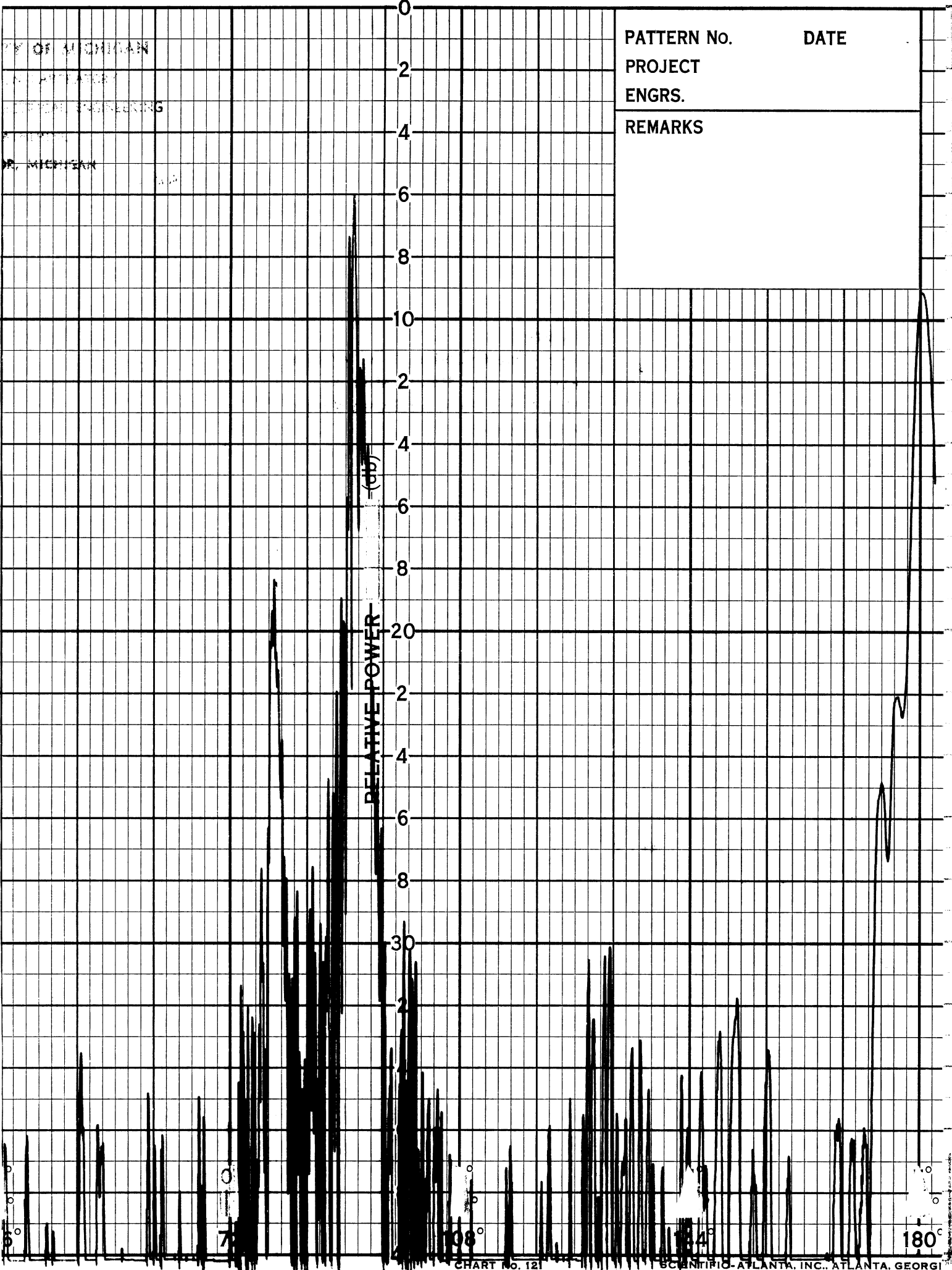
Range 208.5' 10'' CR

Model Minn-Honey

Roll 45° With Fins







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838

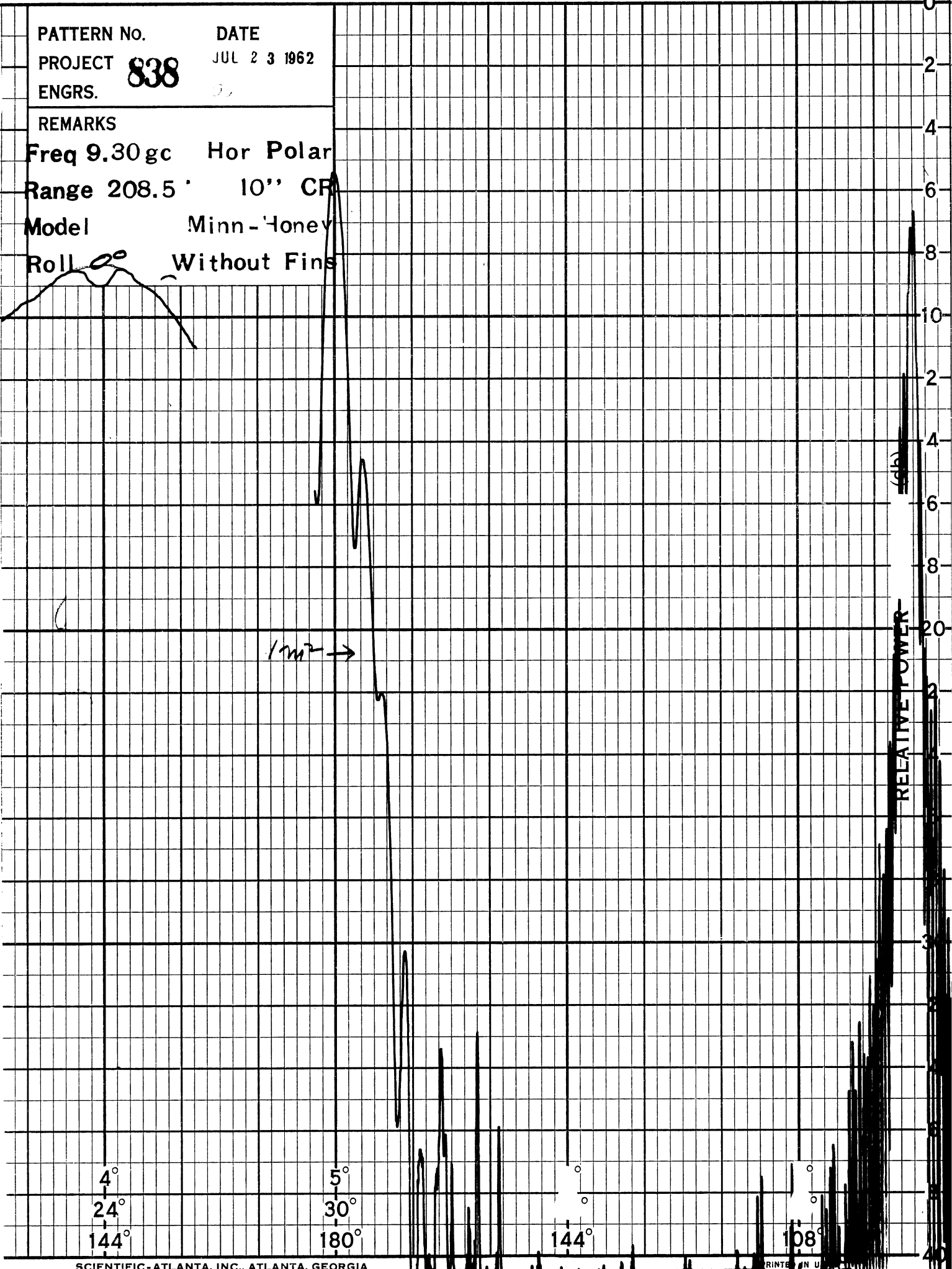
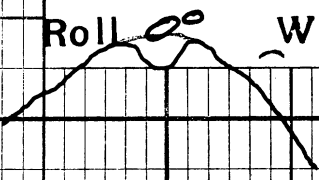
REMARKS

Freq 9.30 gc Hor Polar

Range 208.5' 10" CR

Model Minn-Honey

Roll 0° Without Fins



1 m<sup>2</sup> →

4°  
24°  
144°

5°  
30°  
180°

144°

108°

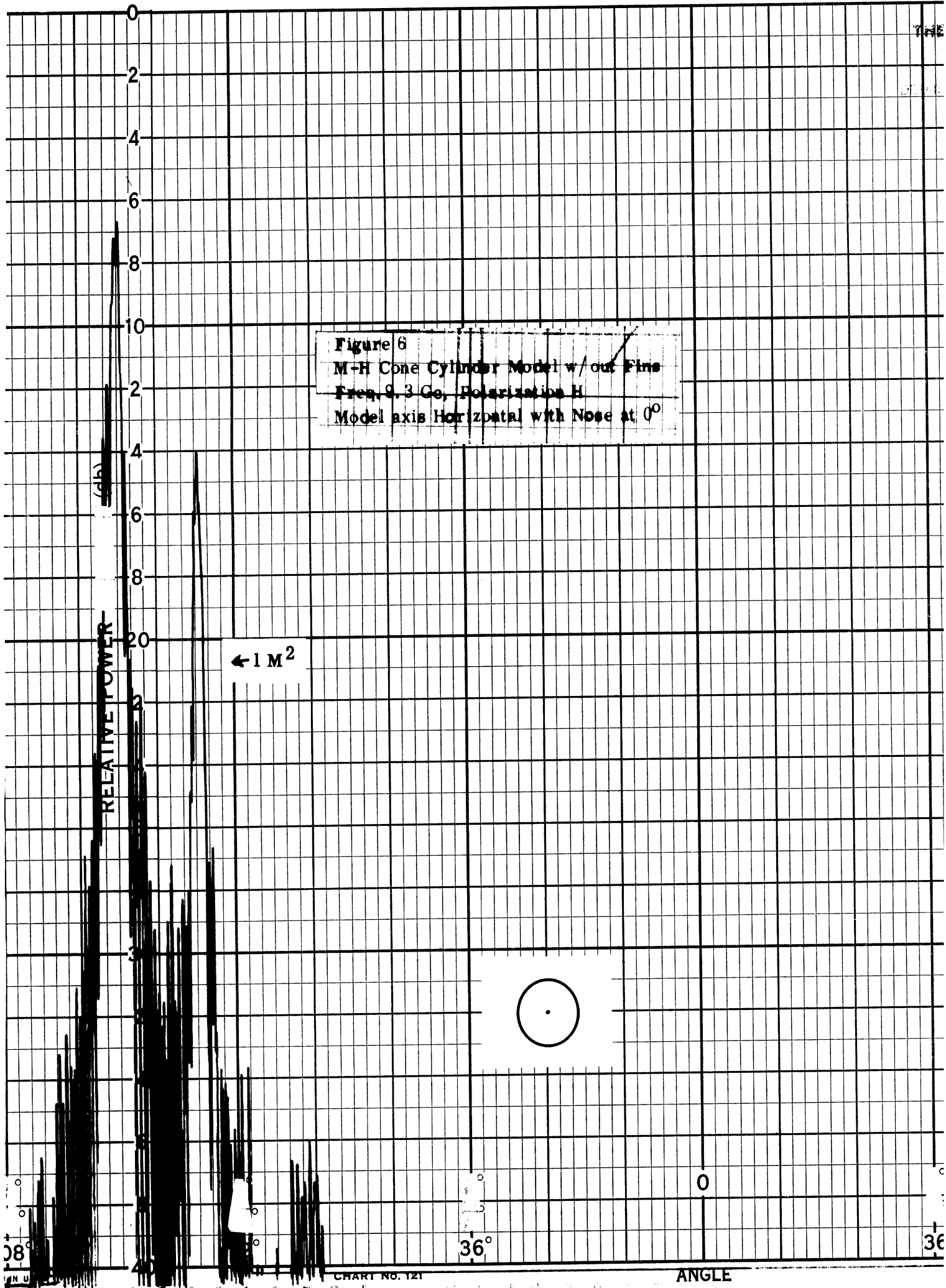
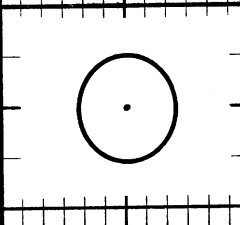


Figure 6  
 M-H Cone Cylinder Model w/out Fins  
 Freq. 9.3 Gc, Polarization H  
 Model axis Horizontal with Nose at 0°

← 1 M<sup>2</sup>



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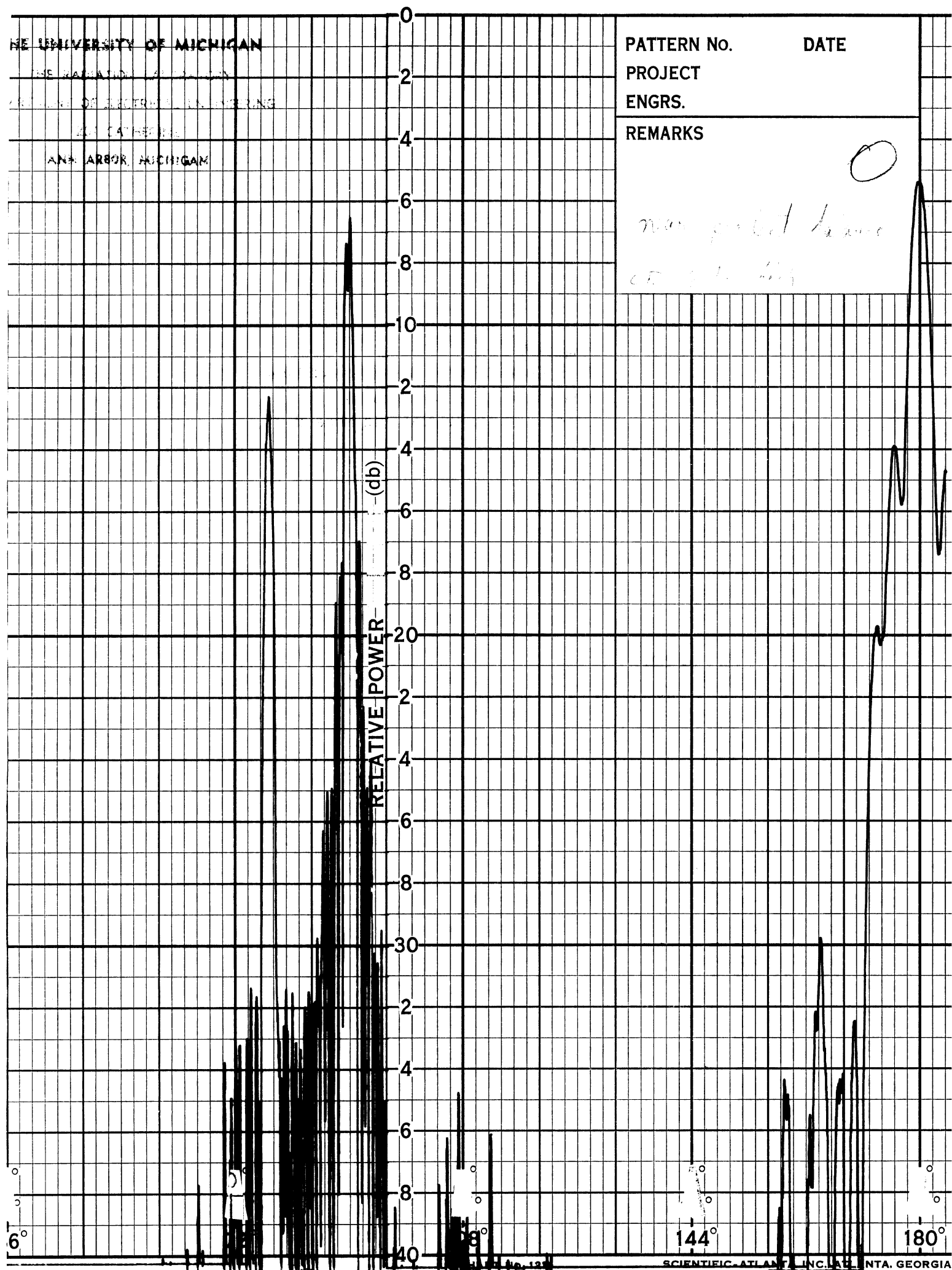
DATE

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REMARKS

*no plot done  
at 144°*



PATTERN NO.

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JUL 23 1962

ENGRS.

834

REMARKS

Freq 9.30 gc Hor Polar

Range 208.5' 10" CB

Model Minn-Honey

Roll 0° With Fins



→ 1M<sup>2</sup>

RELATIVE POWER (db)  
0  
2  
4  
6  
8  
10  
12  
14  
16  
18  
20  
22  
24  
26  
28  
30  
32  
34  
36  
38  
40

4°  
24°  
144°

5°  
30°  
180°

6°  
36°  
144°

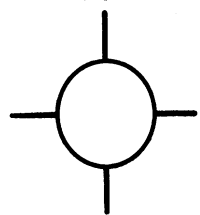
8°  
48°  
144°



Figure 7  
M-H Cone Cylinder Model w/ Fins  
Freq. 9.3 Gc, Polarization H  
Model axis Horizontal with Nose at 0°  
Roll Angle 0°

RELATIVE POWER  
(db)

← 1 M<sup>2</sup>



0°  
36°

ANGLE

36°



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201 CHURCH ST.

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PATTERN No.

DATE

PROJECT

ENGRS.

REMARKS

0

0  
2  
4  
6  
8  
10  
2  
4  
6  
8  
20  
2  
4  
6  
8  
30  
2  
4  
6  
8  
40

RELATIVE POWER  
-(db)

36°

08°

144°

180°

PATTERN No.

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JUL 19 1962

ENGRS. 822

REMARKS

Freq 9.30 gc Hor Polar

Range 208.5' 10" CR

Model Minn-Honey

Roll 45° With Fins



RELATIVE POWER (db)

4°  
24°  
144°

5°  
30°  
180°

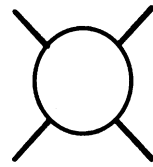
4°  
24°  
144°

5°

RELATIVE POWER  
-(db)

Figure 8  
M-H Cone Cylinder Model w/ Fins  
Freq. 9.3 Gc, Polarization H  
Model axis Horizontal with Nose at 0°  
Roll Angle 45°

← 1 M<sup>2</sup>



0°  
36°

0°

36°

CHART NO. 12

ANGLE

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REMARKS \_\_\_\_\_

0

RELATIVE POWER (db)

36°

72°

108°

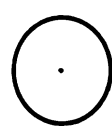
144°

72  
ANN ARBOR, MICHIGAN

Figure 9  
M-H Cone Cylinder Model w/out Fins  
Freq. 9.3 Gc, Polarization H  
Model axis Horizontal with Nose at 0°  
Nose aspects only are shown and  
measurement range is shortened  
to show greater detail.

← 1 M<sup>2</sup>

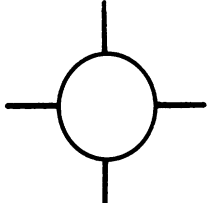
RELATIVE POWER (DB)



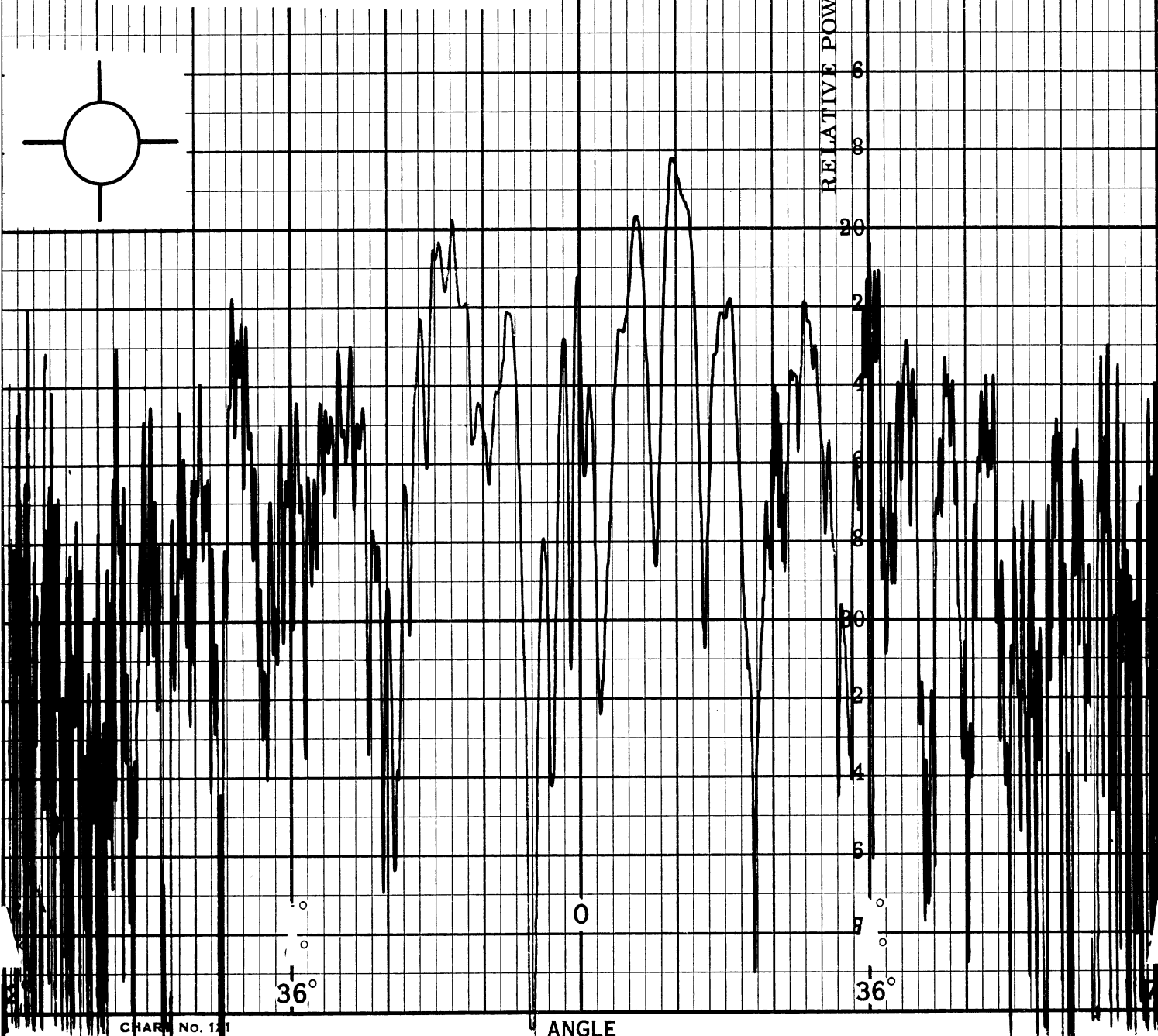
ANGLE

Figure 10  
M-H Cone Cylinder Model w/ Fins  
Freq. 9.3 Gc, Polarization H  
Model axis Horizontal with Nose at 0°  
Roll Angle 0°  
Nose aspects only are shown and  
measurement range is shortened to  
show greater detail.

← 1 M<sup>2</sup>

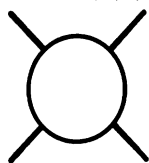


RELATIVE POWER (DB)

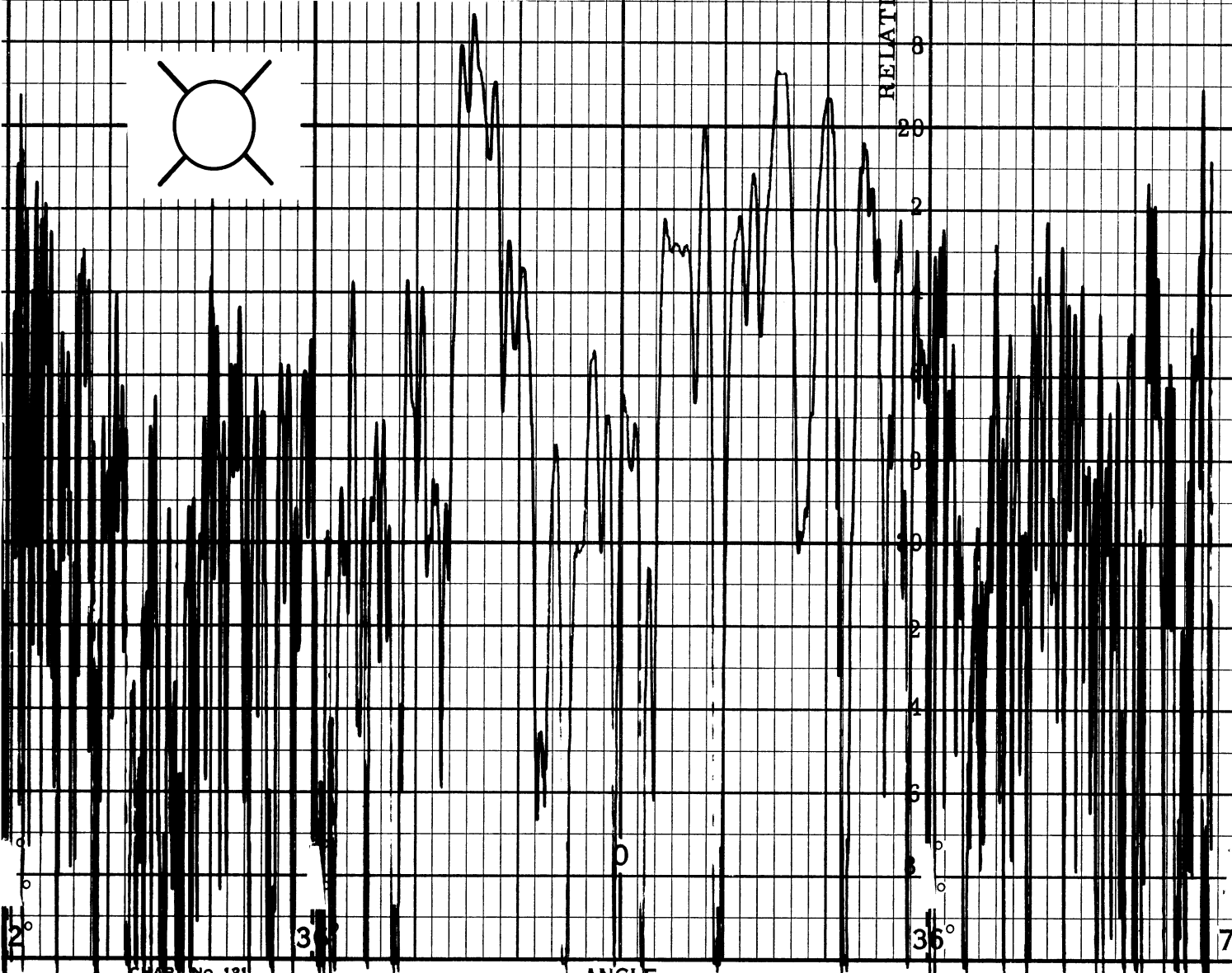


← 1 M<sup>2</sup>

**Figure 11**  
**M-N Cone Cylinder Model w/ Fins**  
**Freq. 9.3 Gc, Polarization H.**  
**Model axis Horizontal with Nose at 0°**  
**Roll Angle 45°**  
Nose aspects only are shown and measurement range is shortened to show greater detail.



RELATIVE POWER (DB)





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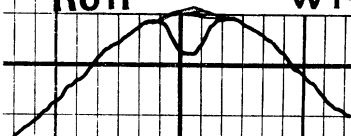
REMARKS

Freq 9.30 gc Hor Polar

Range 100' 10" CR

Model Minn-Honey

Roll Without Fins ONLY



M  
 12  
 C

(dB)

RELATIVE POWER

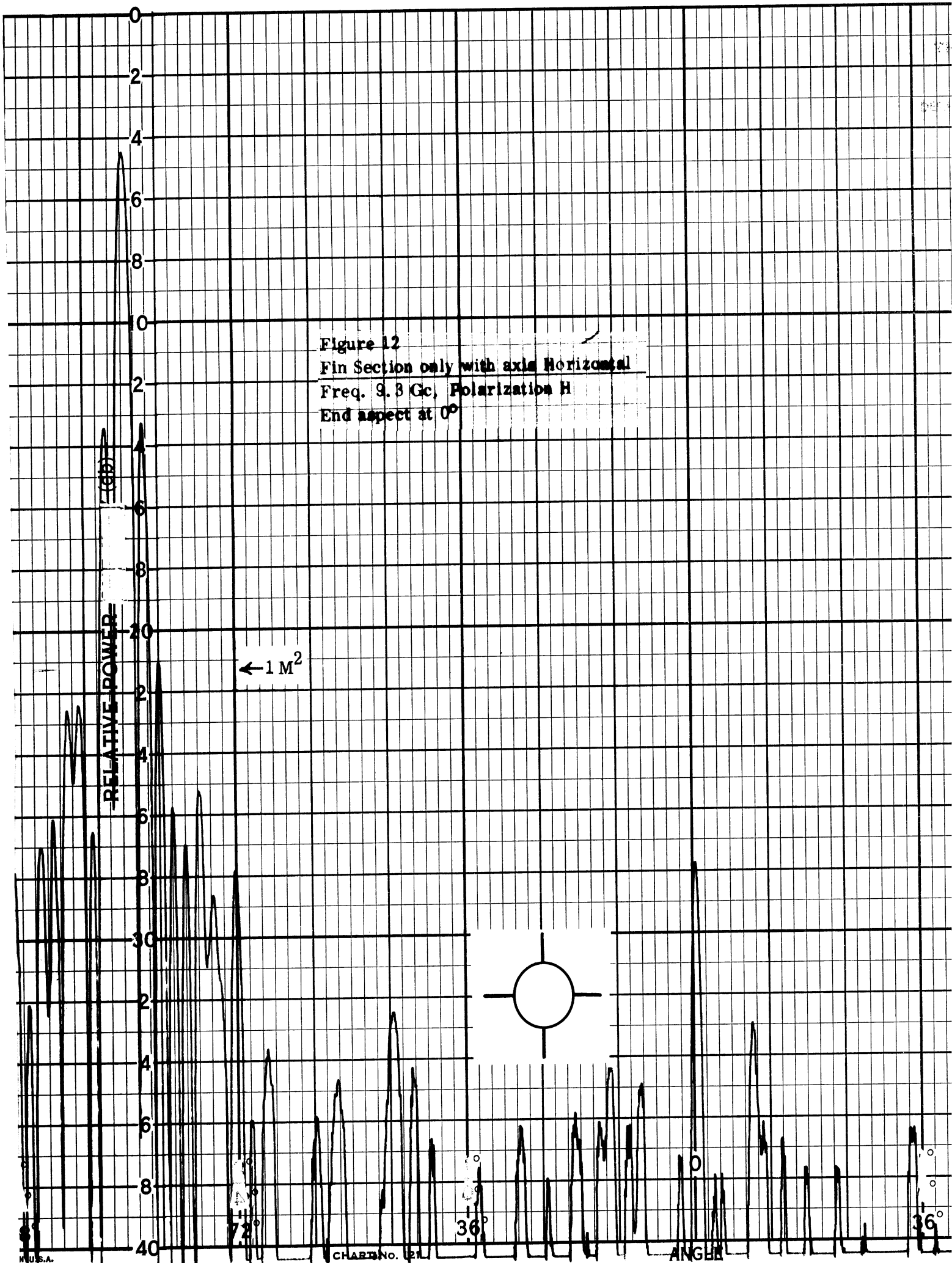
4°  
24°  
144°

5°  
30°  
180°

4°  
24°  
144°

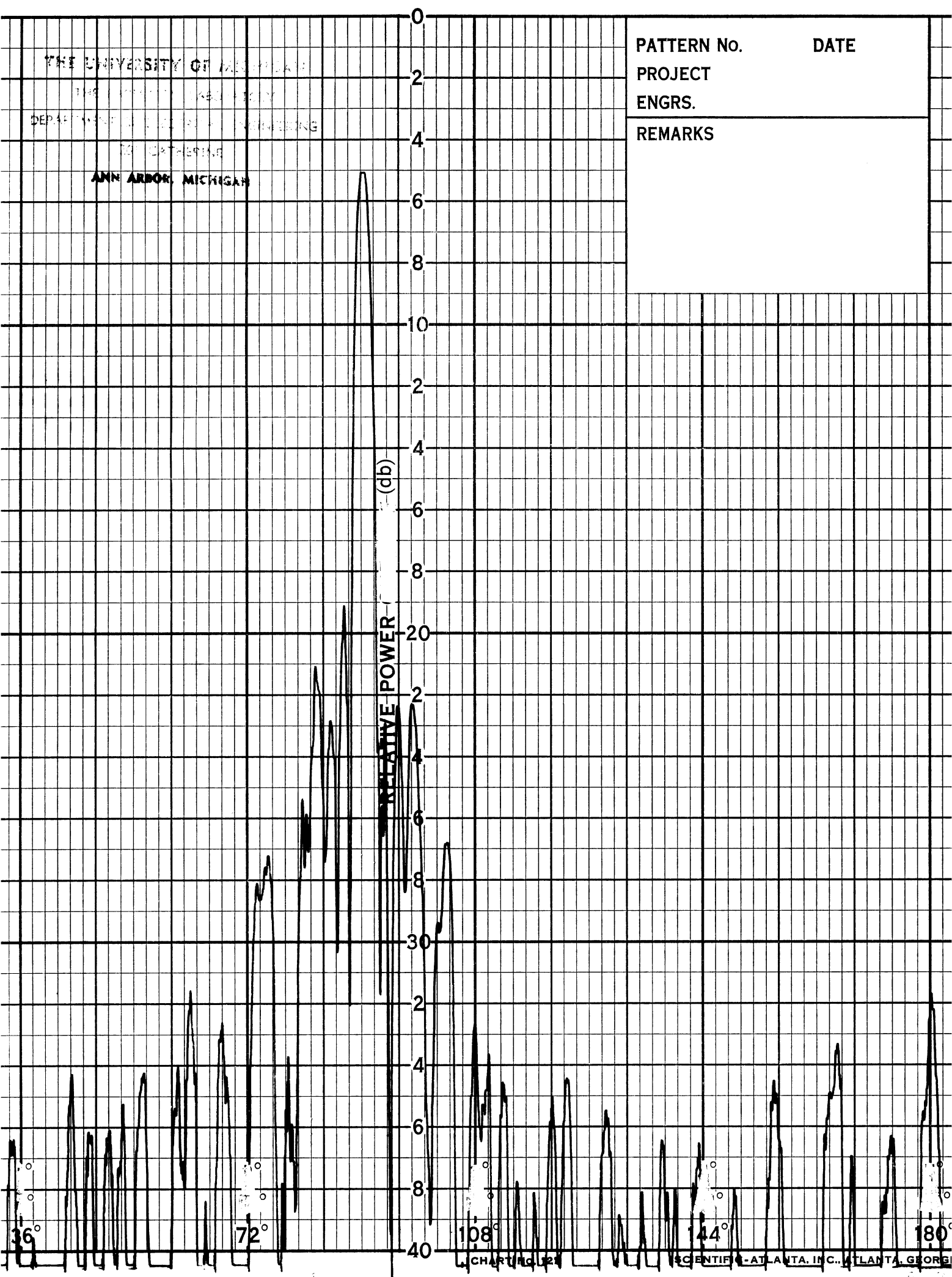
1085





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ANN ARBOR, MICHIGAN

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PROJECT \_\_\_\_\_  
ENGRS. \_\_\_\_\_  
REMARKS \_\_\_\_\_



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541

REMARKS

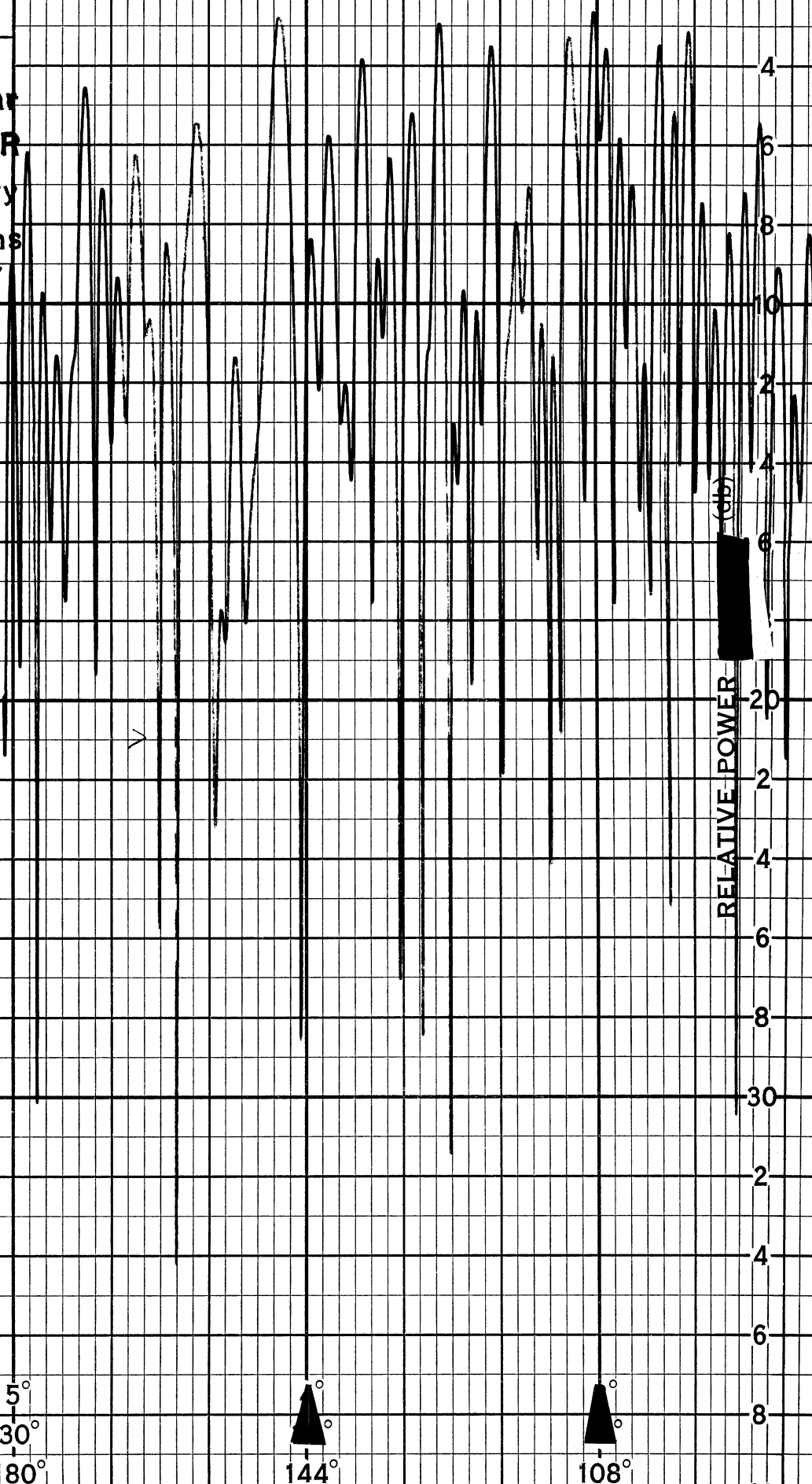
Freq 9.30 gc Hor Polar

Range 100' 10" CR

Model Minn-Honey

Roll Without Fins

ONLY

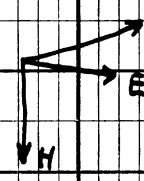


RELATIVE POWER (db)

0  
2  
4  
6  
8  
10  
12  
14  
16  
18  
20  
22  
24  
26  
28  
30  
32  
34  
36  
38  
40

11M

>



4°  
24°  
144°

5°  
30°  
180°

144°

108°

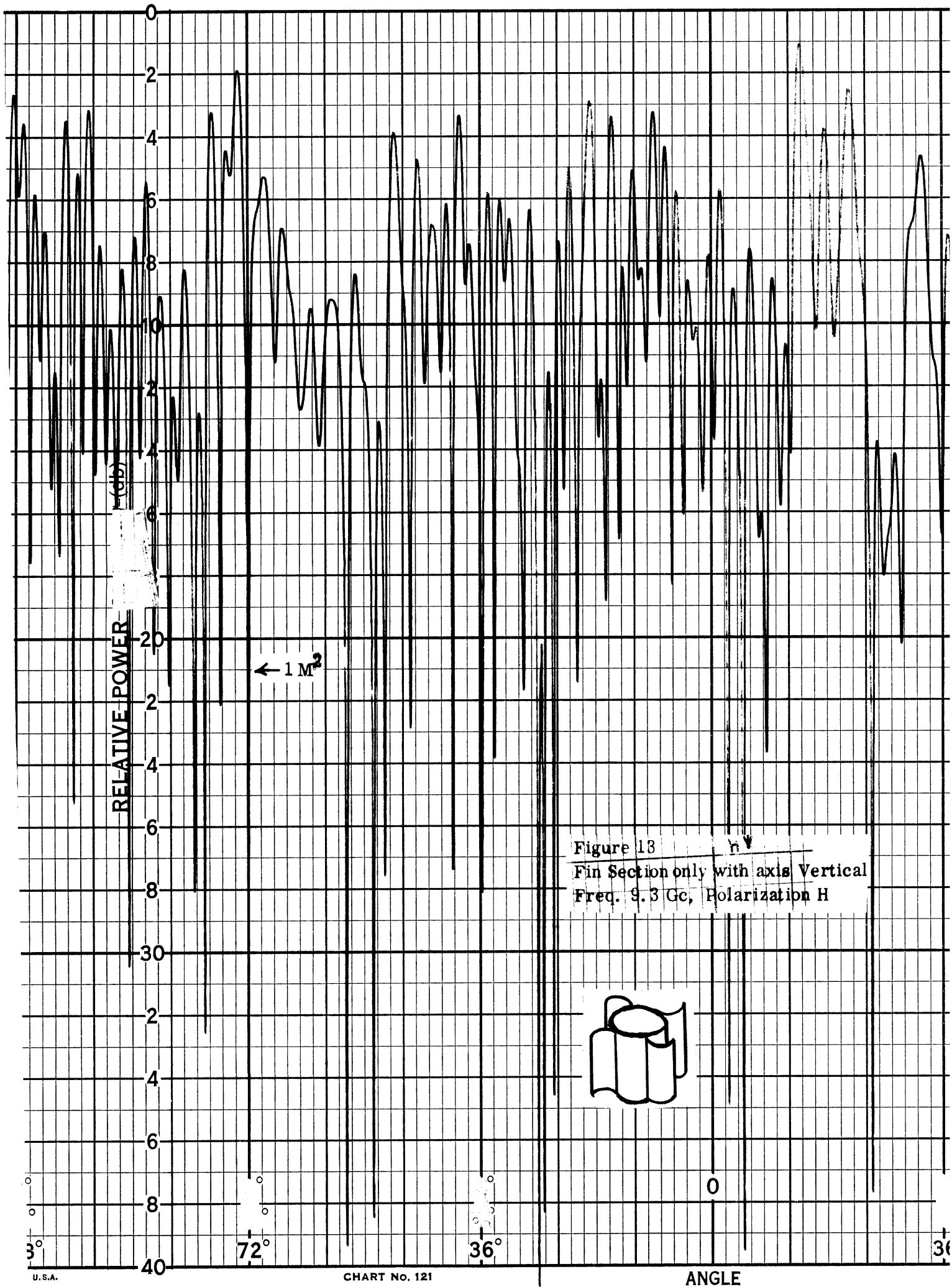
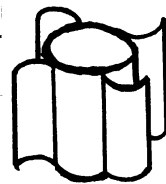


Figure 13  
 Fin Section only with axis Vertical  
 Freq. 9.3 Gc, Polarization H



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PROJECT  
ENGRS.

DATE

REMARKS

RELATIVE POWER (dB)

36°

72°

108°

144°

PATTERN No.

DATE

PROJECT

567

JUL 27 1962

ENGRS.

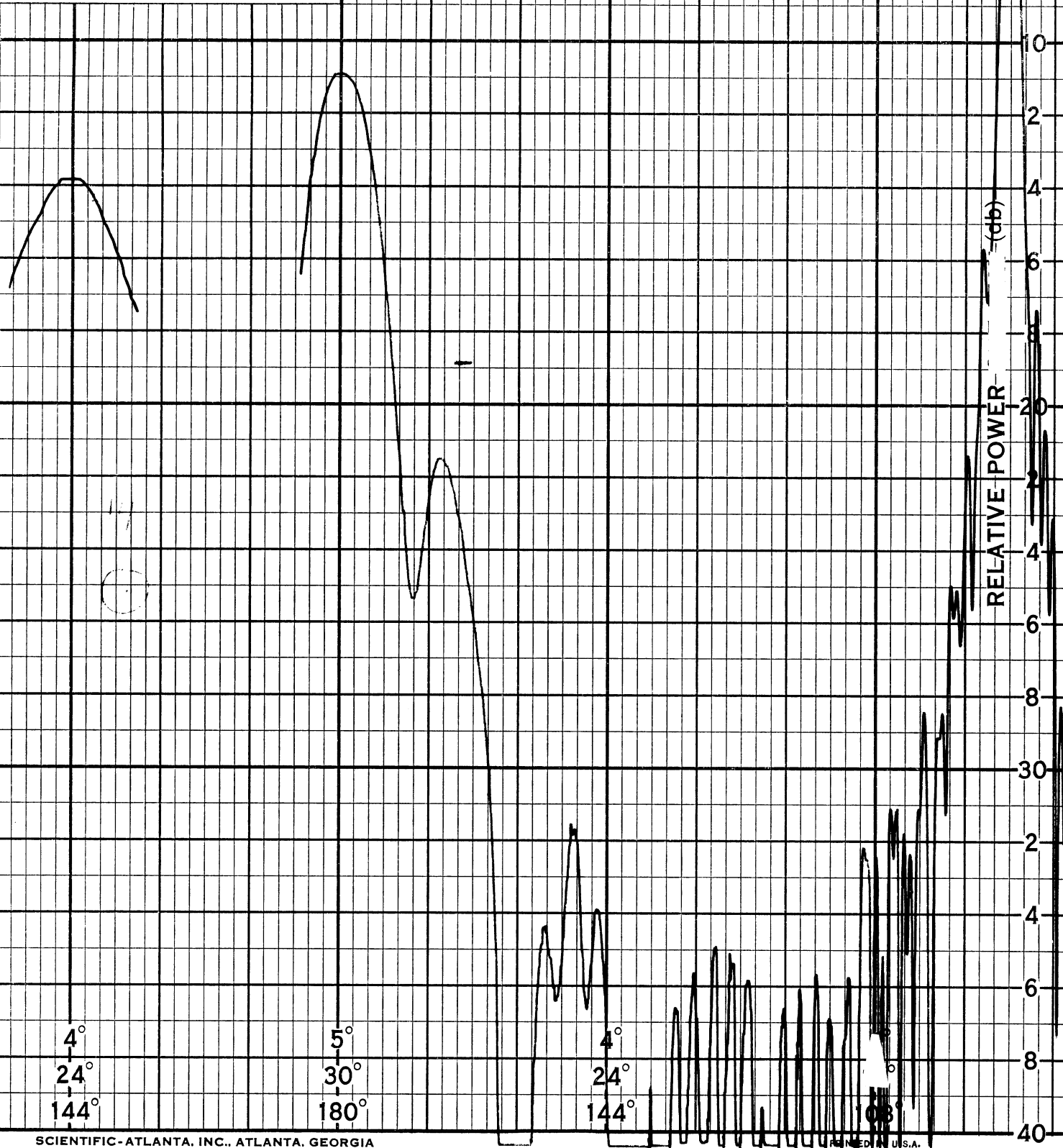
REMARKS

Freq 2.87 gc Vert Polar

Range 100' 10" CR

Model Minn-Honey

Roll 0° Without Fins



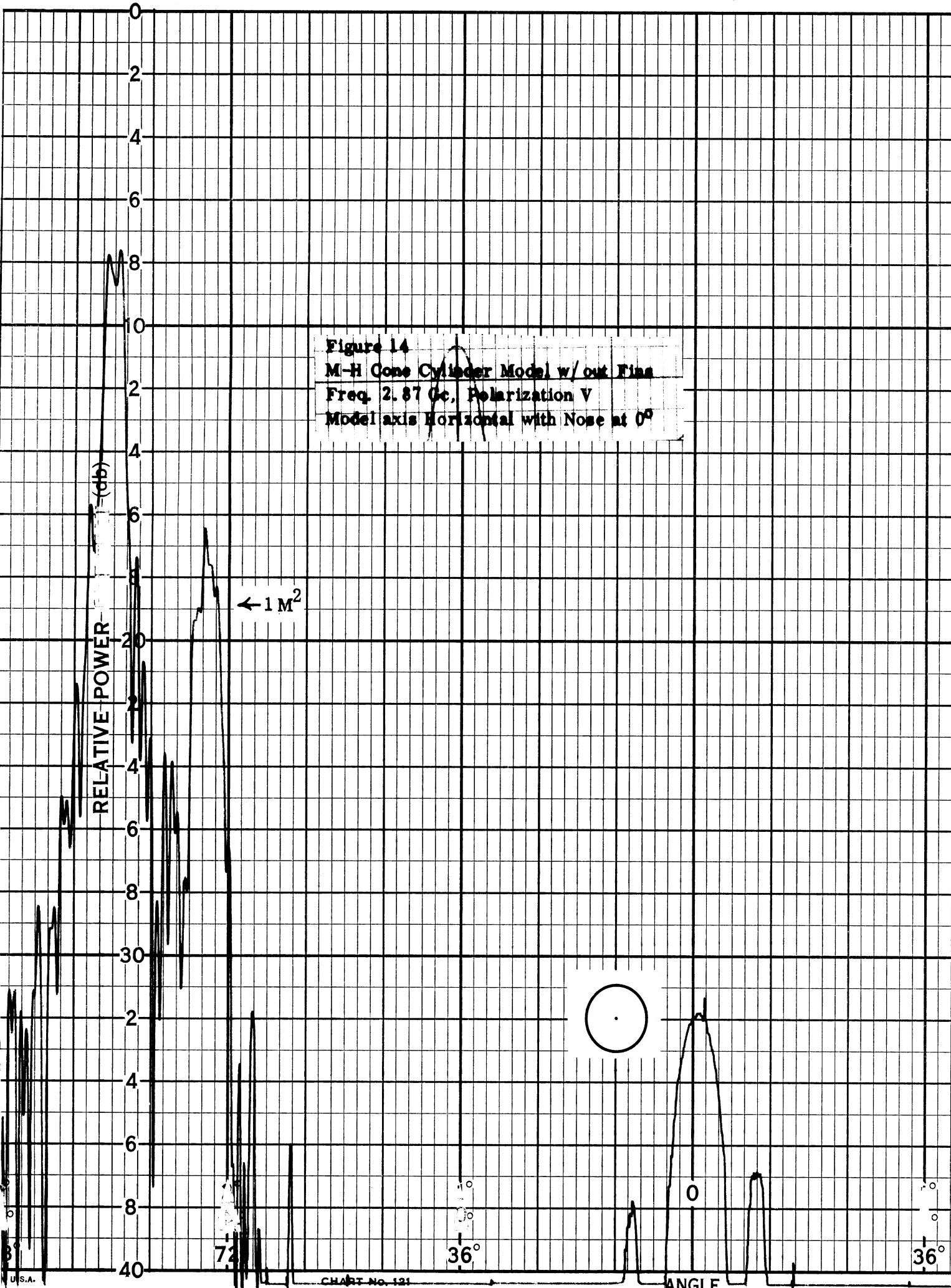
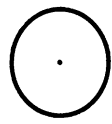


Figure 14  
 M-H Cone Cylinder Model w/ out Fins  
 Freq. 2.87 Gc, Polarization V  
 Model axis Horizontal with Nose at 0°

RELATIVE POWER (db)

← 1 M<sup>2</sup>



ANGLE



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REMARKS

RELATIVE POWER (db)

36°

72°

108°

144°

180°



PATTERN No.

DATE

PROJECT

862

JUL 27 1962

ENGRS.

a

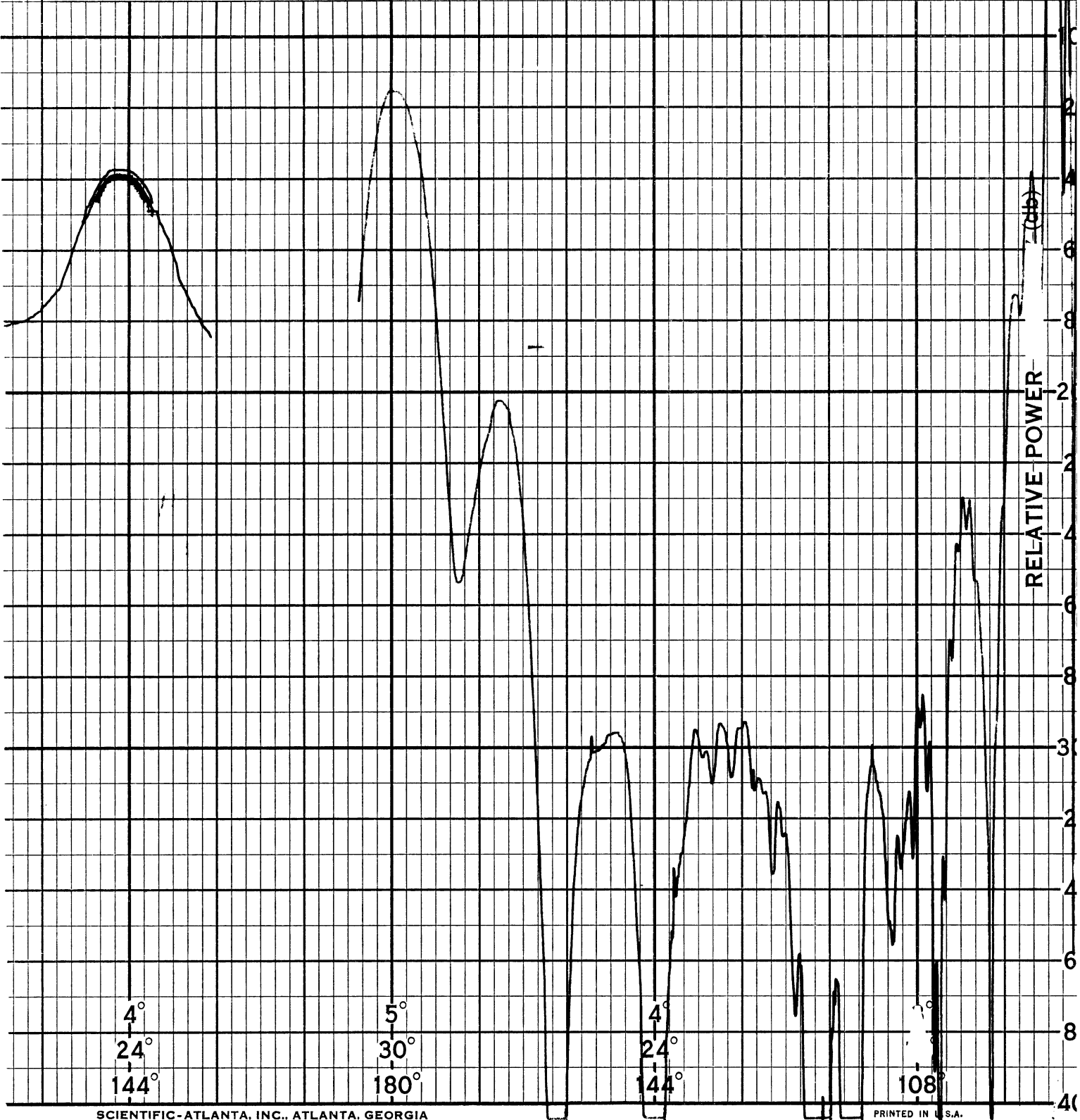
REMARKS

Freq 2.87 gc Vert Polar

Range 100' 10'' CR

Model Minn-Honey

Roll 00 With Fins



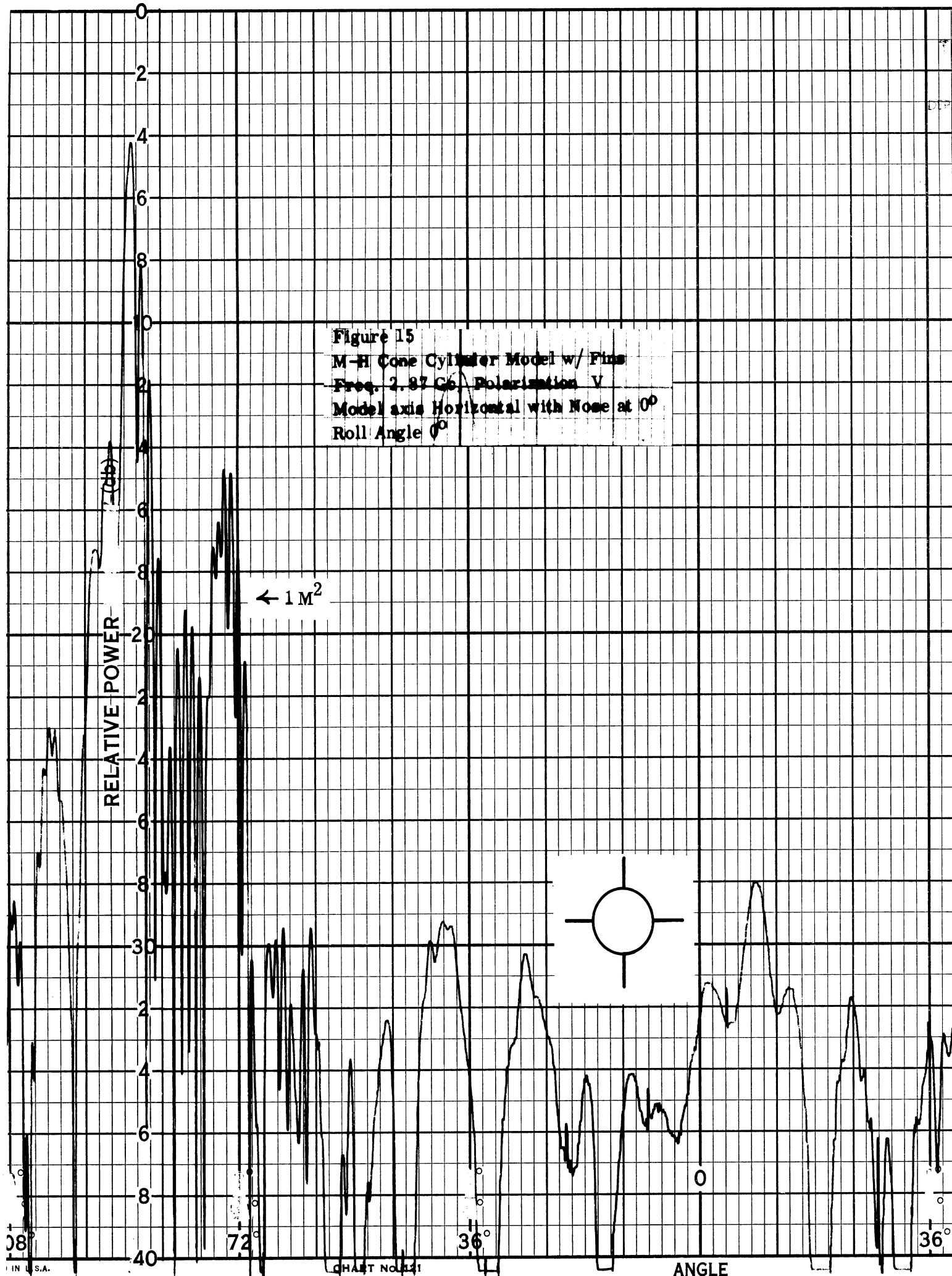
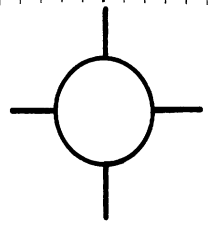


Figure 15  
 M-H Cone Cylinder Model w/ Fins  
 Freq. 2.87 Gc Polarization V  
 Model axis Horizontal with Nose at 0°  
 Roll Angle 0°

RELATIVE POWER (db)

← 1 M<sup>2</sup>



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DATE

PROJECT  
ENGRS.

REMARKS

RELATIVE POWER (db)

36°

72°

108°

144°

180°

PATTERN No.

DATE

PROJECT

858 JUL 27 1962

ENGRS.

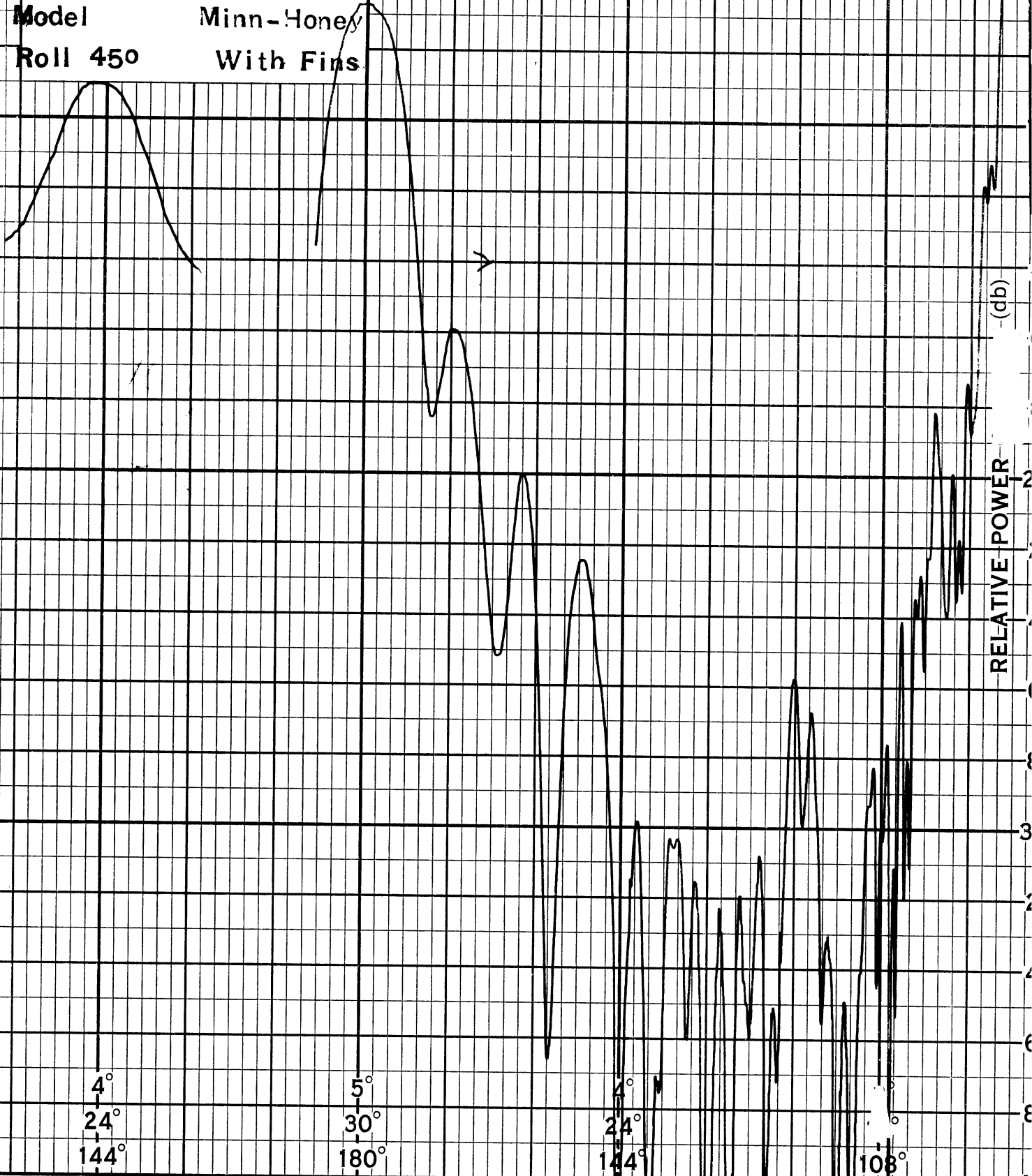
REMARKS

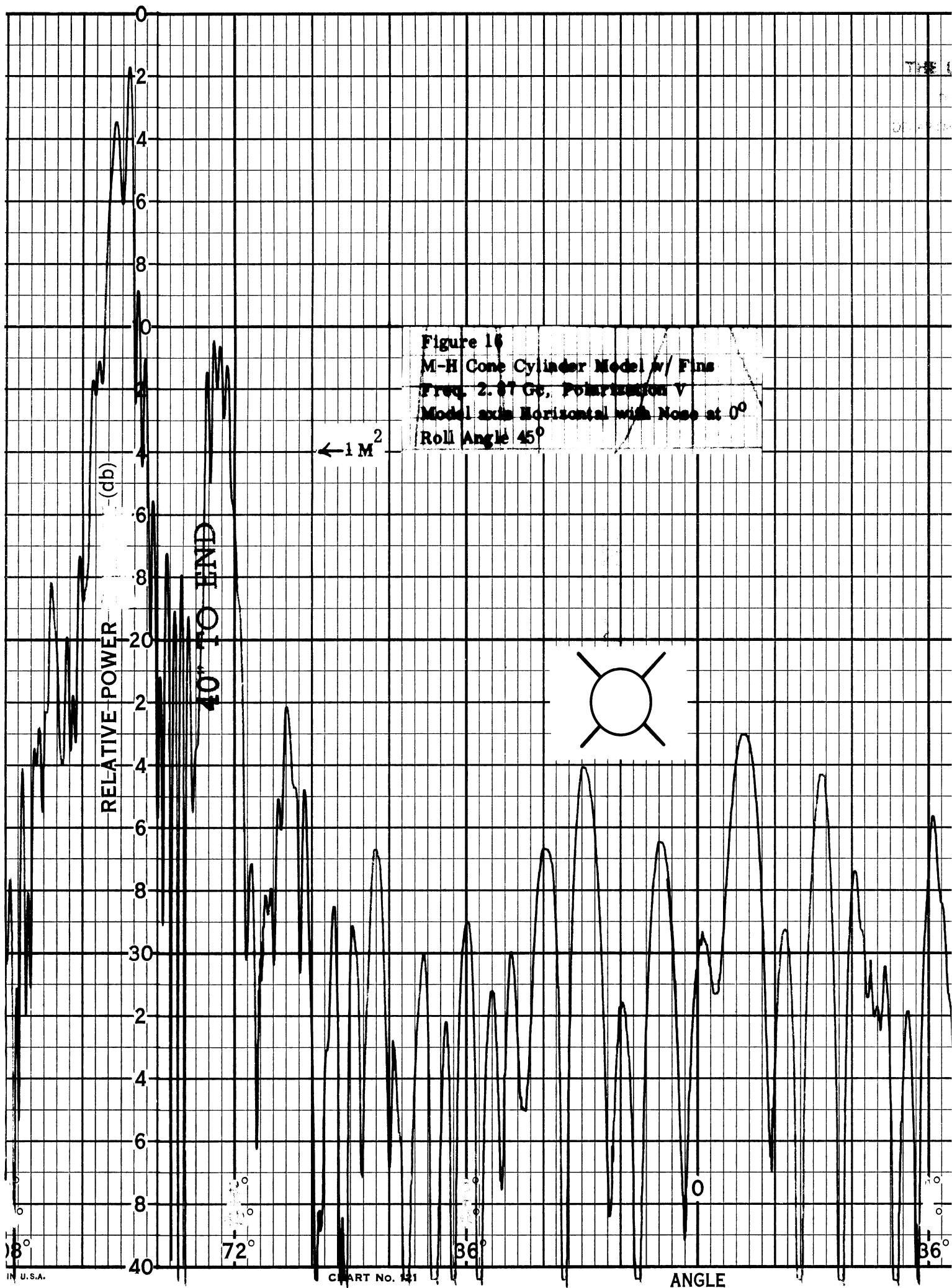
Freq 2.87 gc Vert Polar

Range 100' 10" CR

Model Minn-Honey

Roll 45° With Fins





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ANN ARBOR, MICHIGAN

PATTERN No.

DATE

PROJECT

ENGRS.

REMARKS

0

RELATIVE POWER (db)

36°

72°

108°

144°

180°

PATTERN No.

DATE

PROJECT

875

JUL 29 1962

ENGRS.

a

REMARKS

Freq 2.87 gc Hor Polar

Range 100' 10'' CR

Model Minn-Honey

Roll 0° Without Fins

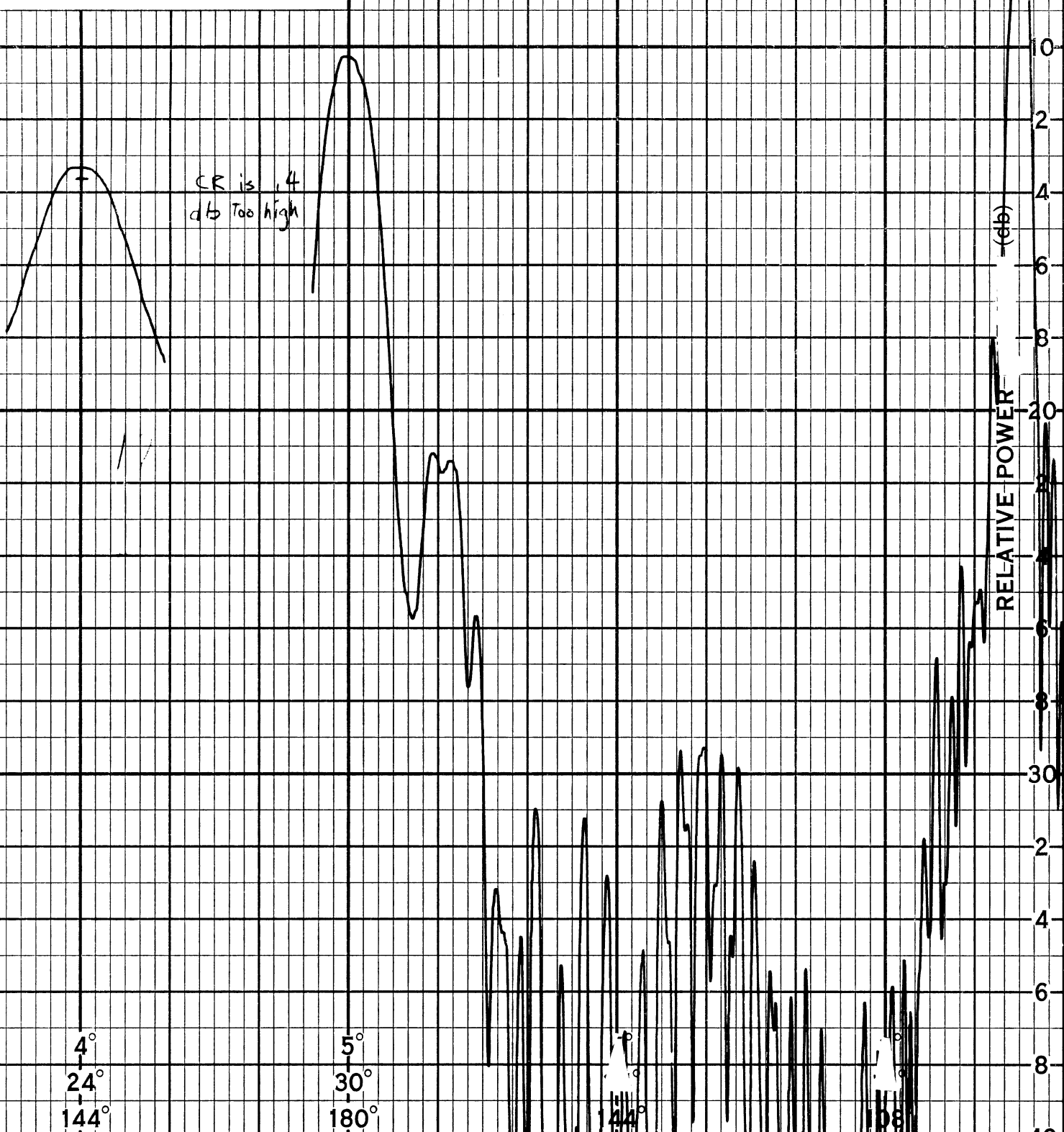
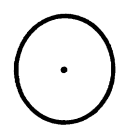




Figure 17  
M-H Cone Cylinder Model w/out Fins  
Freq. 2.87 Gc, Polarization H  
Model axis Horizontal with Nose at 0°

RELATIVE POWER  
(-db)

← 1 M<sup>2</sup>

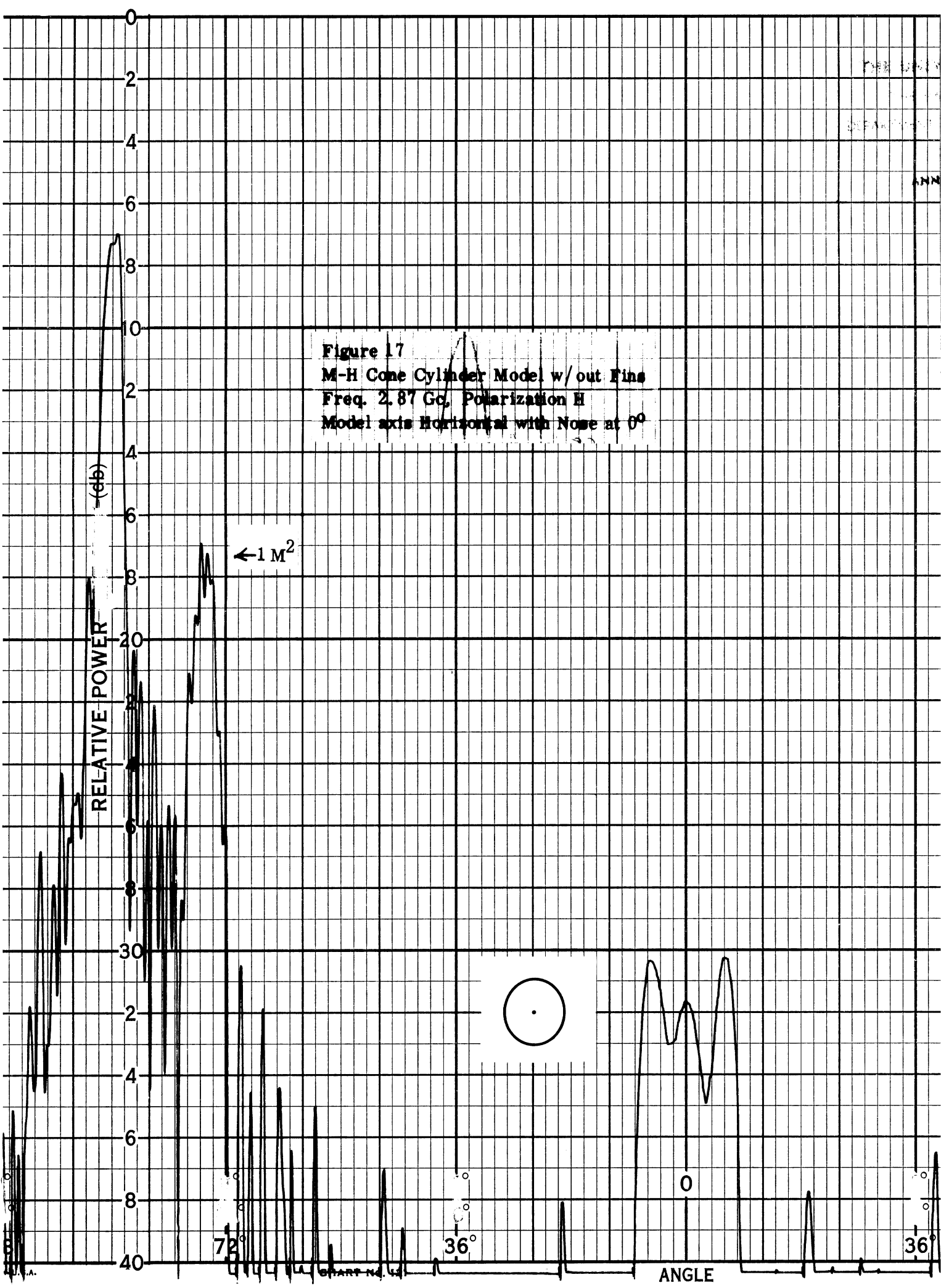


72°

36°

ANGLE

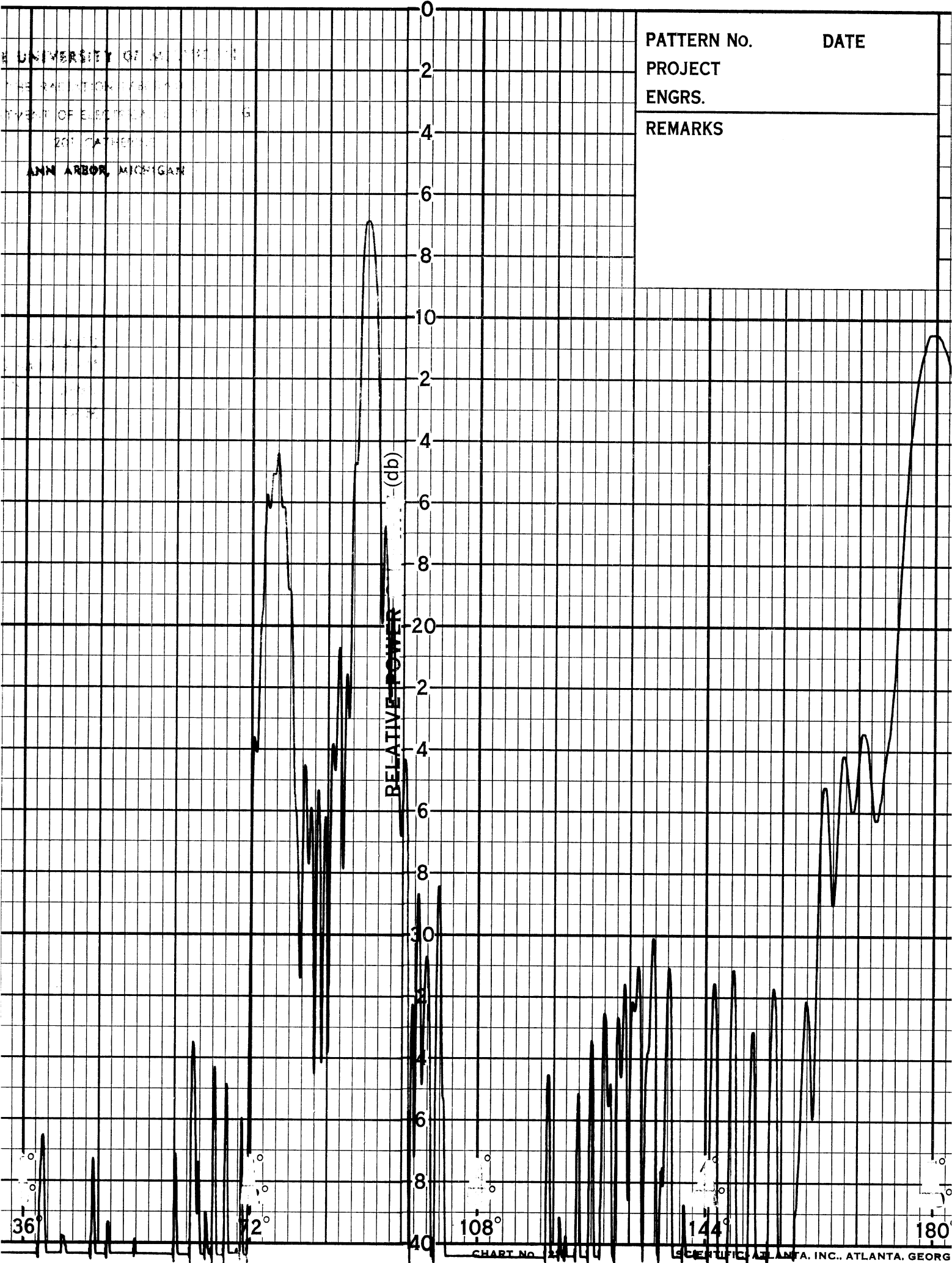
36°





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ANN ARBOR, MICHIGAN

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PROJECT \_\_\_\_\_  
ENGRS. \_\_\_\_\_  
REMARKS \_\_\_\_\_



PATTERN No.

DATE

PROJECT

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ENGRS.

877

a

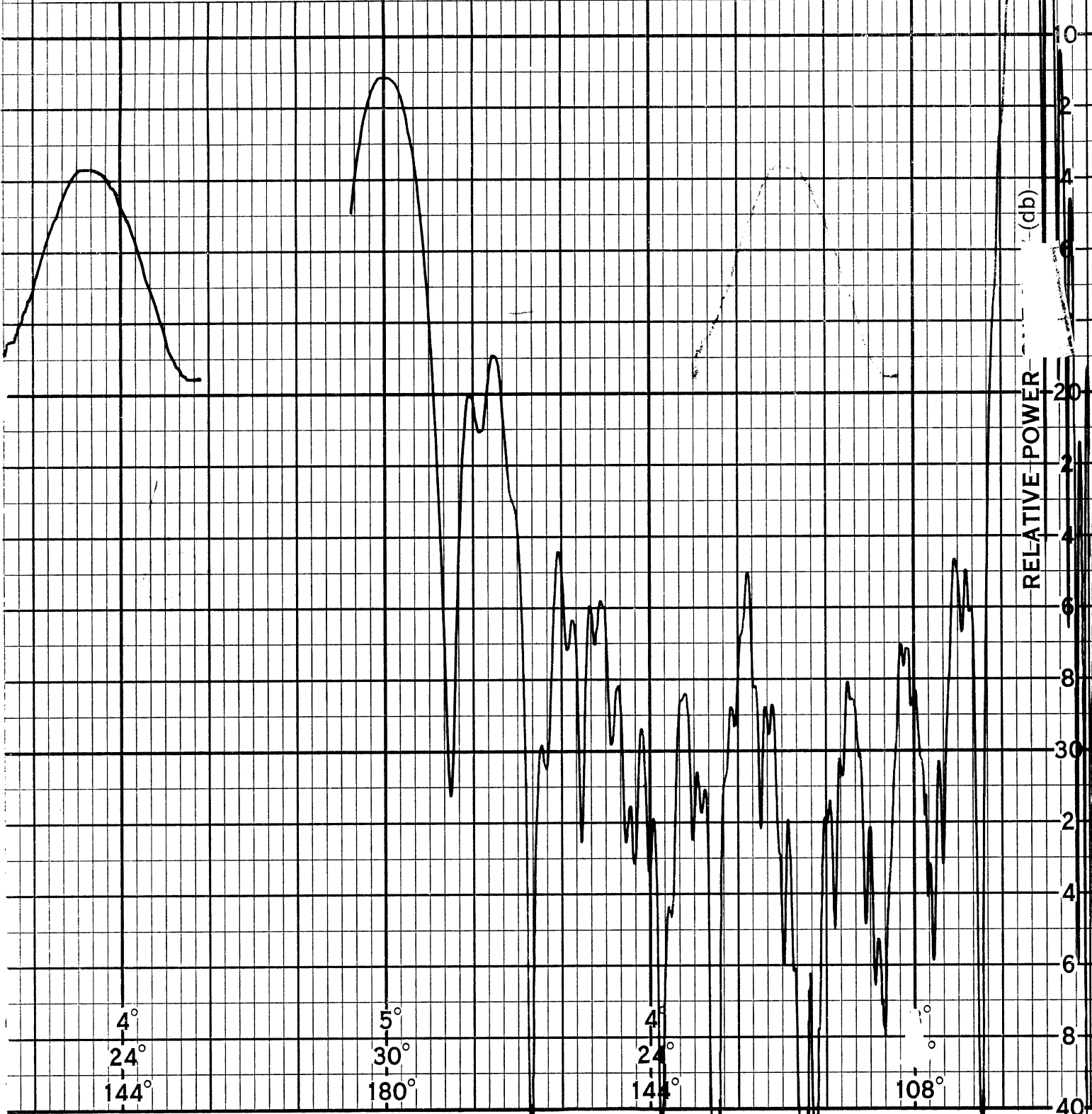
REMARKS

Freq 2.87 gc Hor Polar

Range 100' 10" CR

Model Minn-Honey

Roll 00 With Fins

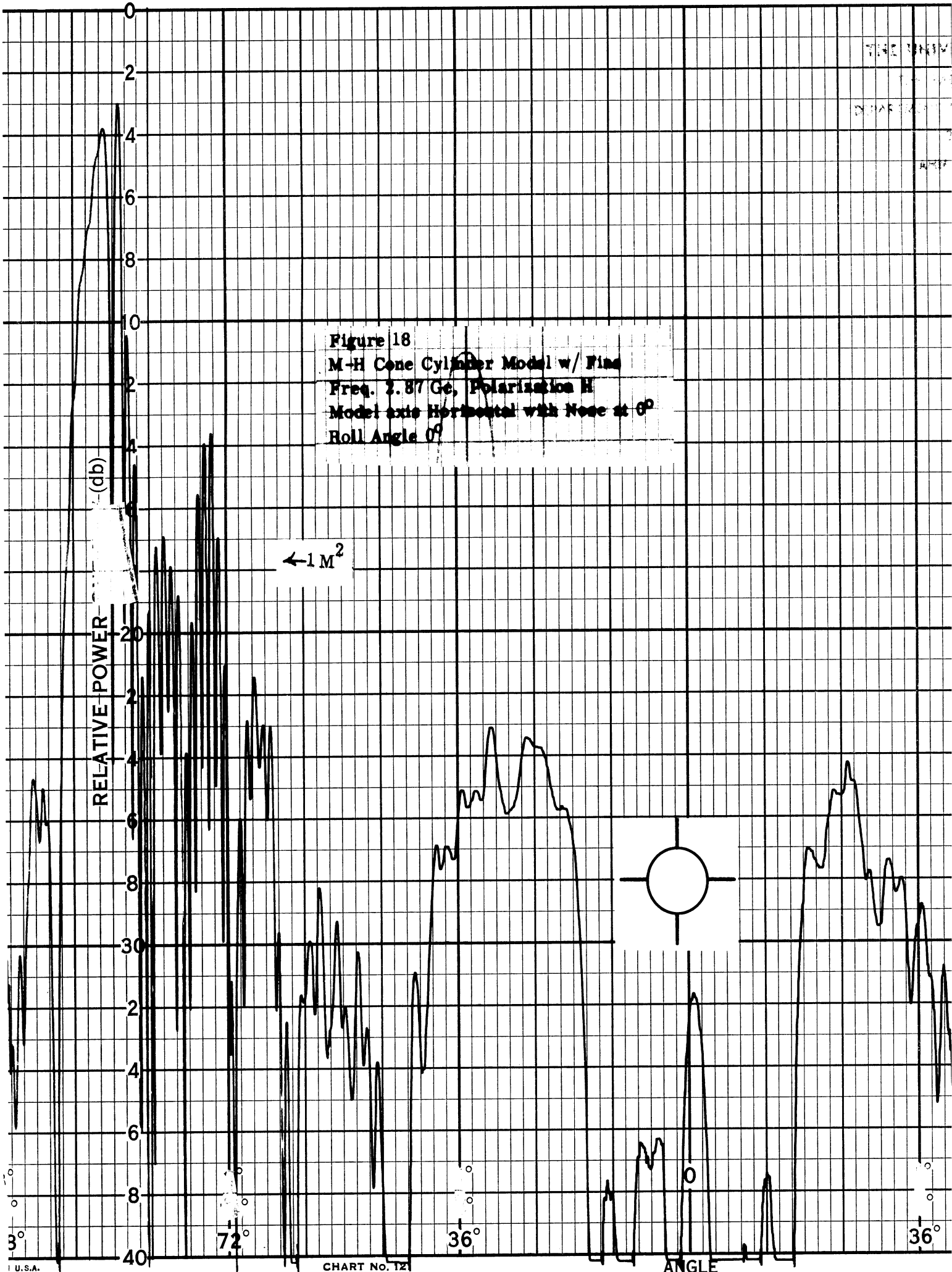
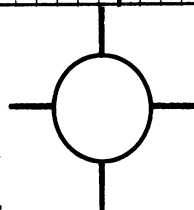


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Figure 18  
M-H Cone Cylinder Model w/ Fin  
Freq. 2.87 Gc, Polarization H  
Model axis Horizontal with Nose at 0°  
Roll Angle 0°

RELATIVE POWER  
(db)

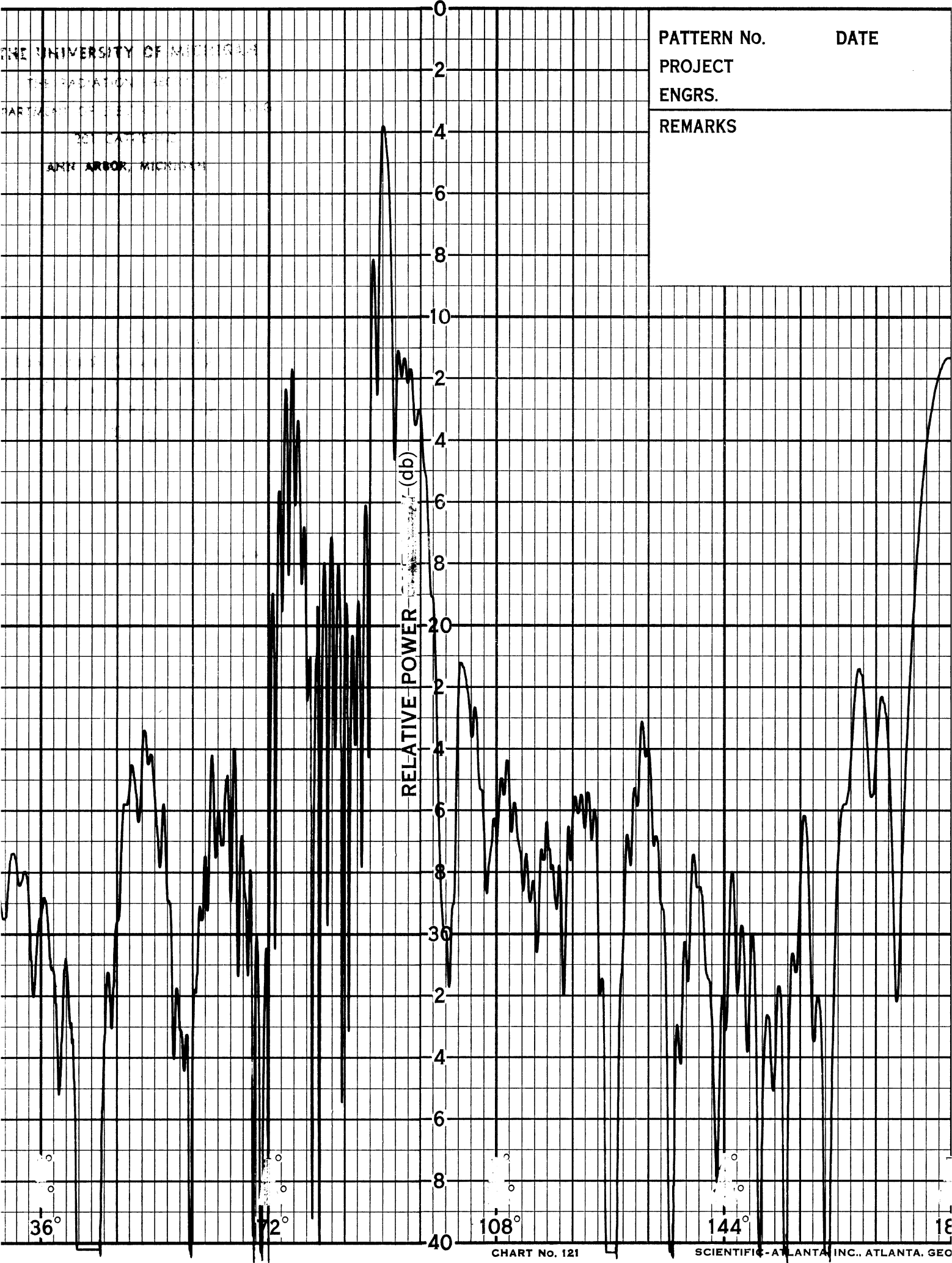
← 1 M<sup>2</sup>



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DEPARTMENT OF ELECTRICAL ENGINEERING  
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ANN ARBOR, MICHIGAN

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ENGRS. \_\_\_\_\_  
REMARKS \_\_\_\_\_

RELATIVE POWER (db)



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ENGRS.

891

REMARKS

Freq 2.87 gc Hor Polar

Range 100' 10'' CR

Model Minn-Honey

Roll 450 With Fins

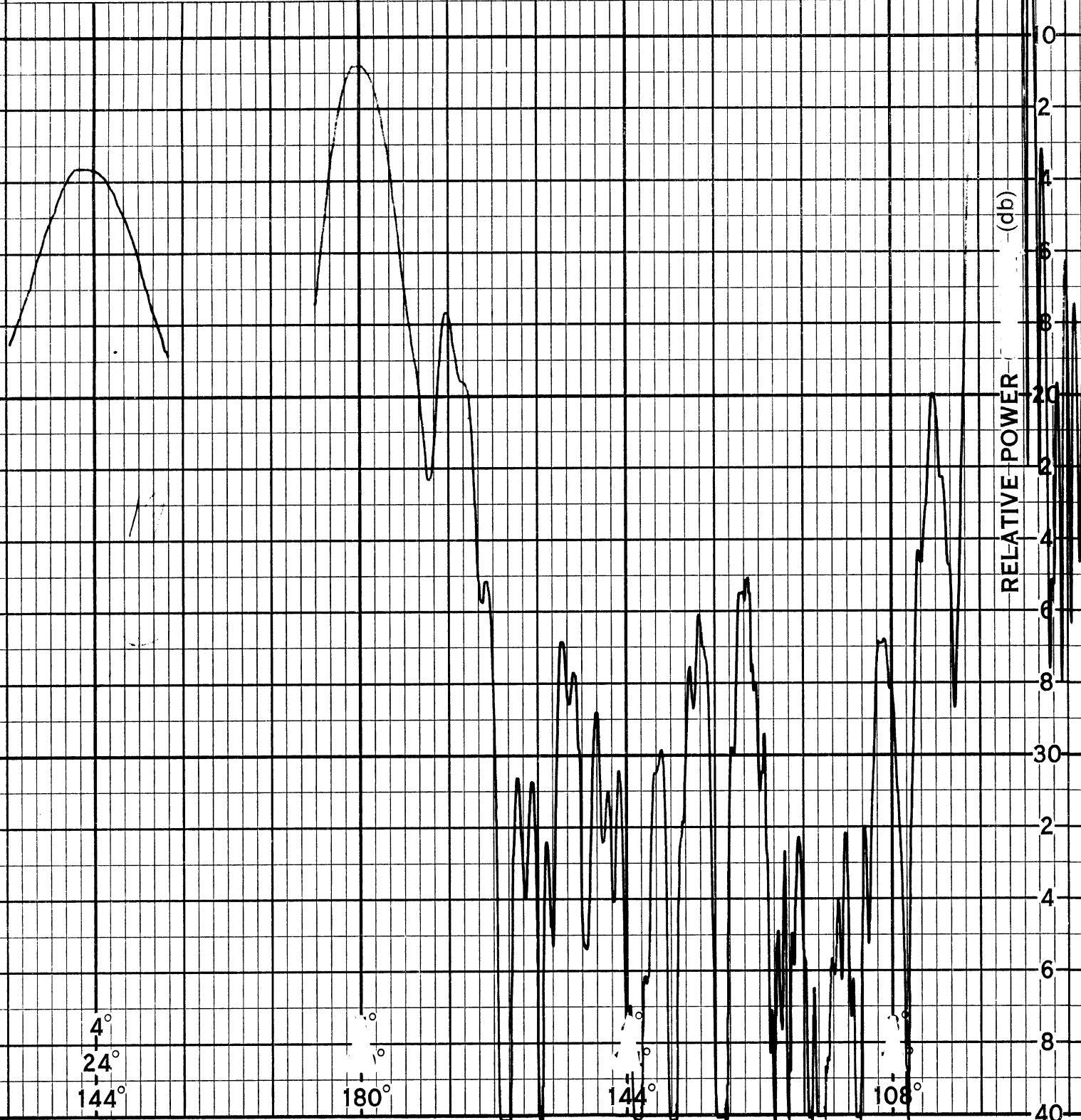
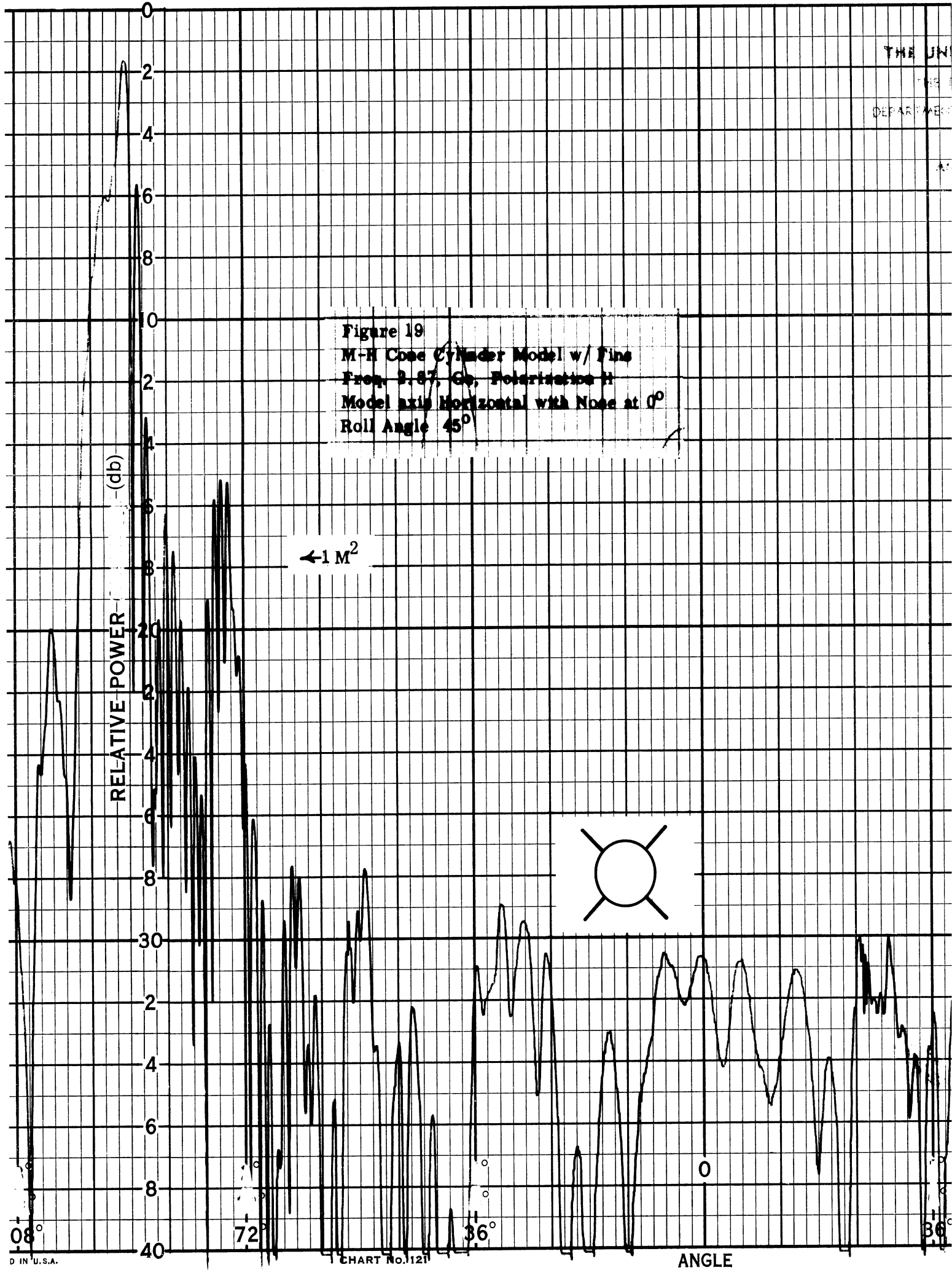
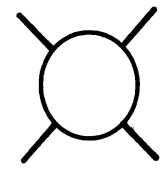


Figure 19  
M-H Cone Cylinder Model w/ Fins  
Freq. 3.87 Gc, Polarization H  
Model axis horizontal with Nose at 0°  
Roll Angle 45°

RELATIVE POWER  
(db)

← 1 M<sup>2</sup>



08°

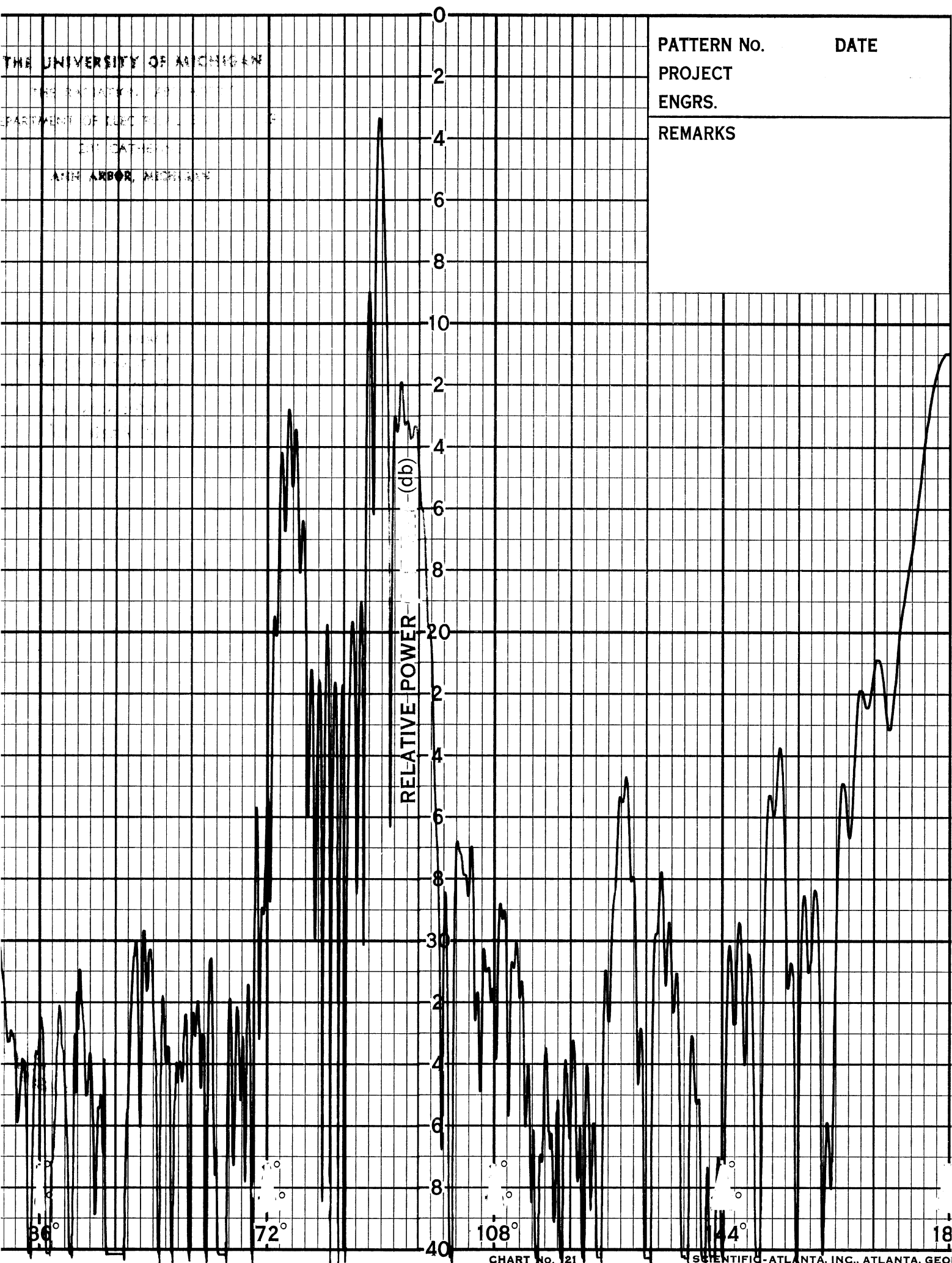
72°

36°

36°

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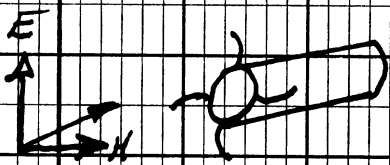
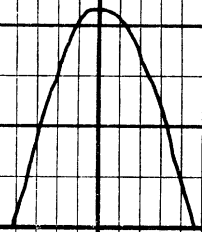
PATTERN No. \_\_\_\_\_ DATE \_\_\_\_\_  
PROJECT \_\_\_\_\_  
ENGRS. \_\_\_\_\_  
REMARKS \_\_\_\_\_





PATTERN No.      DATE  
 PROJECT      886      JUL 29 1962  
 ENGRS.      *U*

REMARKS  
 Freq 2.87 gc    Hor Polar  
 Range 100'      10'' CR  
 Model            Minn-Honey  
 Roll              Fins *ONLY*



RELATIVE POWER (db)

4°      5°      4°      3°  
 24°      30°      24°      0°  
 144°      180°      144°      108°



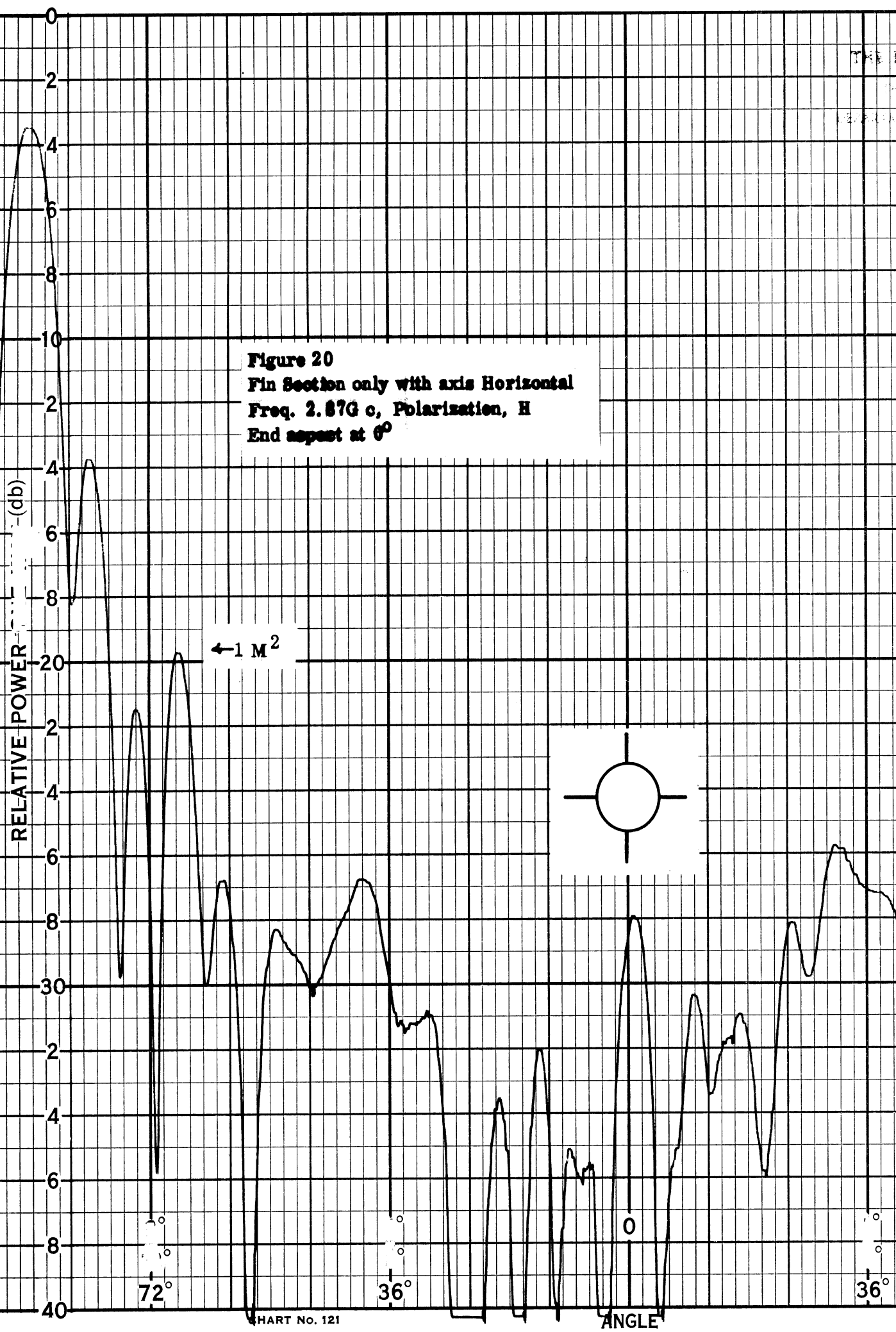
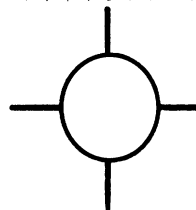


Figure 20  
 Fin Section only with axis Horizontal  
 Freq. 2.87G c, Polarization, H  
 End aspect at 0°

RELATIVE POWER (db)

← 1 M<sup>2</sup>



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1001 CATHERINE

ANN ARBOR, MICHIGAN

PATTERN No.

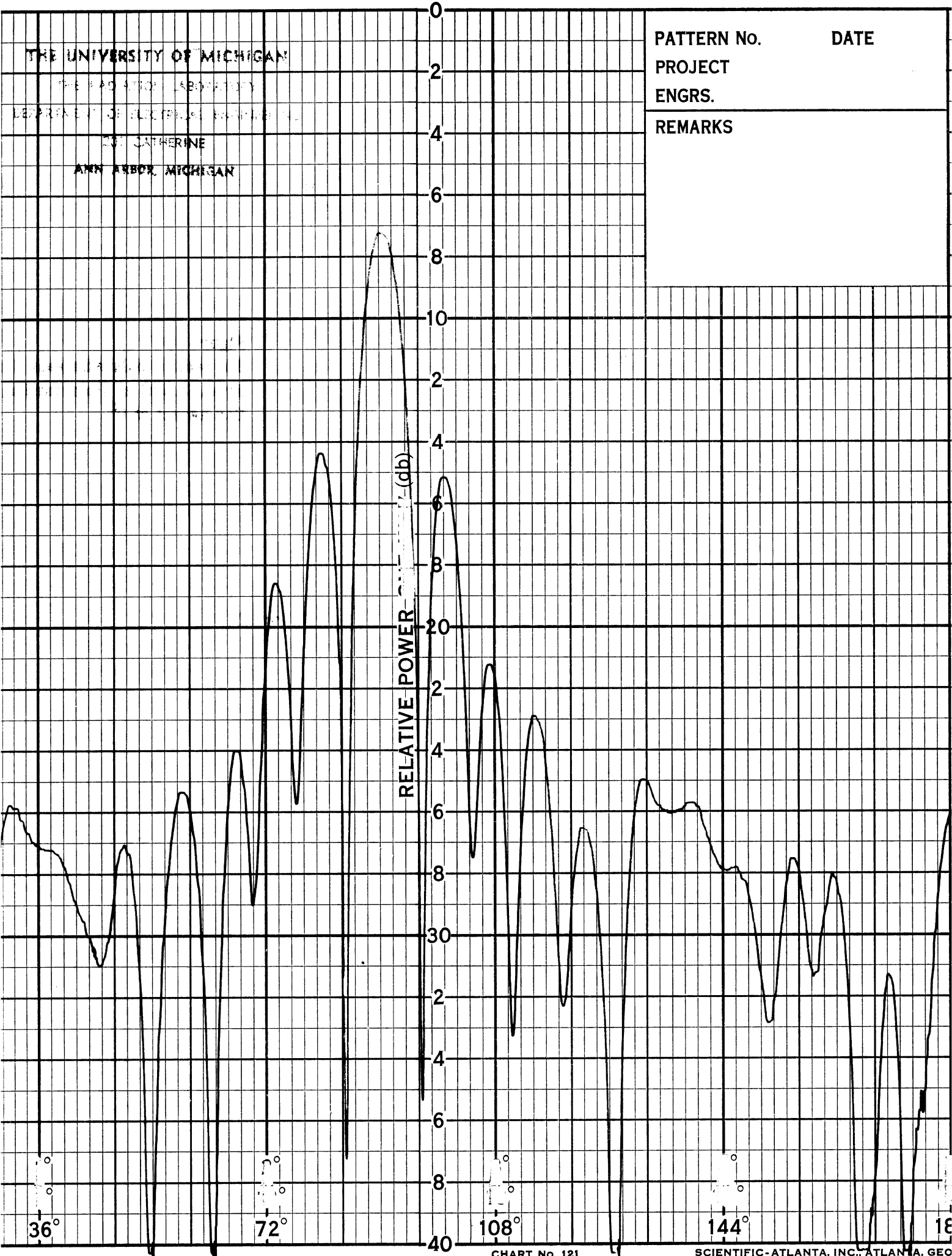
DATE

PROJECT

ENGRS.

REMARKS

RELATIVE POWER (db)



36°

72°

108°

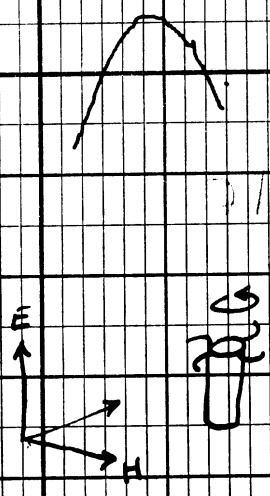
144°

180°

PATTERN No.      DATE (a)  
 PROJECT      870 JUL 29 1962  
 ENGRS.

REMARKS  
 Freq 2.87 gc Vert Polar  
 Range 100'      10" CR  
 Model      Minn-Honey  
 Roll      ~~Without~~ Fins

ONLY



RELATIVE POWER (db) x6

4°      5°      4°      108°  
 24°      30°      24°  
 144°      180°      144°

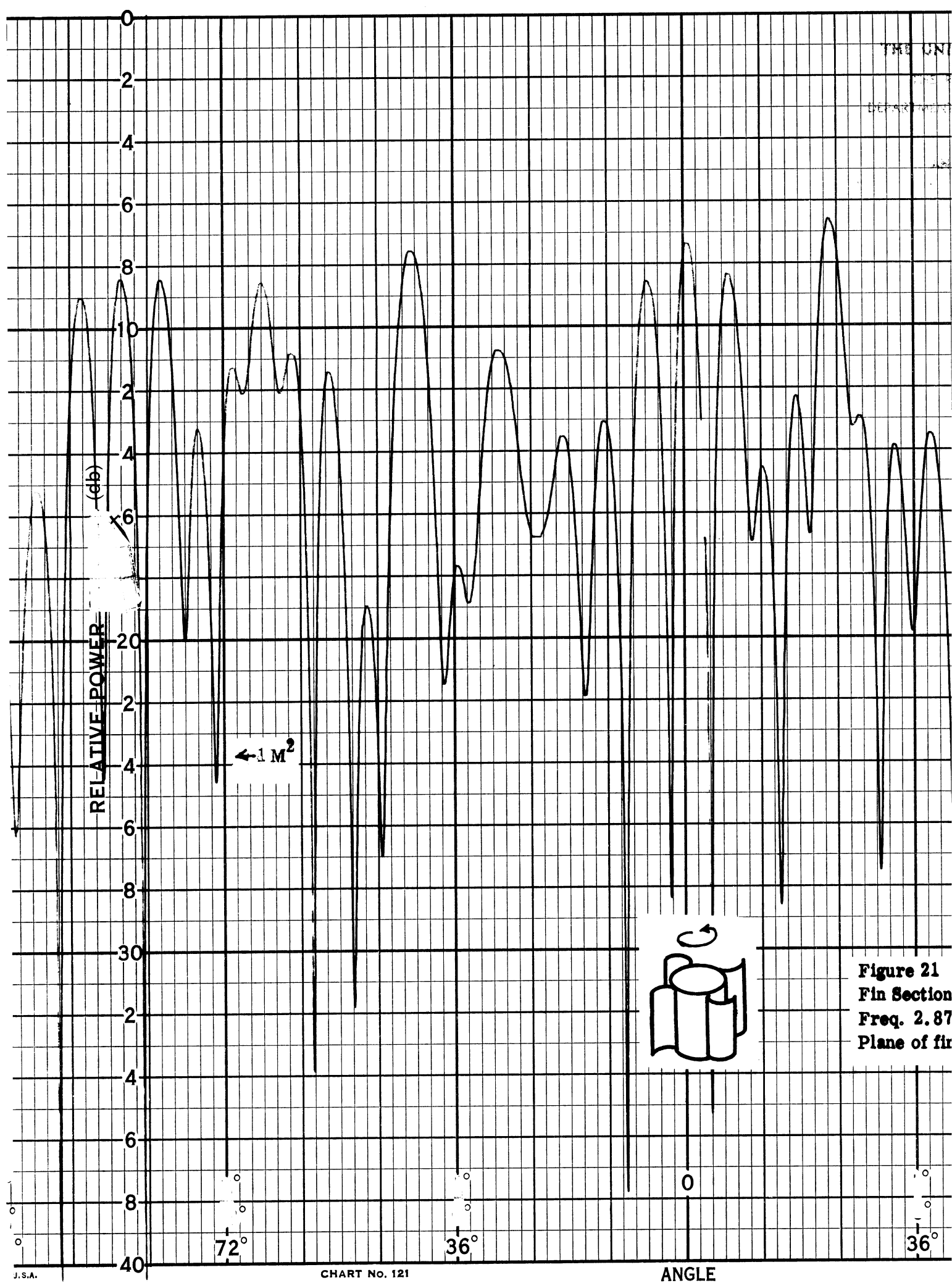


Figure 21  
Fin Section  
Freq. 2.87  
Plane of fir

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REMARKS

RELATIVE POWER  
(db)

Figure 21

Fin Section only with axis Vertical

Freq. 2.87 Gc, Polarization, V

Plane of fins at normal incidence for 0°

36°

72°

108°

144°