HYBRID FINITE ELEMENT AND MOMENT METHOD SOFTWARE FOR THE SERAT ARRAY

1st Quarterly Report

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PROJECT INFORMATION

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PROJECT CHRONOLOGY

April 1996 Proposal Submission

July 1996 Answers to Proposal Questions

August 1996 Contract Negotiations

Sept. 20 1996 Kickoff meeting at Ann Arbor

(attended by Sanders, UM and UH)

October 1996 Contract Signed between U-M

and Sanders in Mid October

October 1996 Subcontract to the Univ of Houston

(formalized in early November)

Nov. 15 1996 SERAT Review meeting (at Nashua)

1 INTRODUCTION

The goal of the SERAT project at the University of Michigan (with subcontract to Univ. Of Houston) is to develop a suite of software for the analysis of strip and slot dipoles on multilayered substrates backed by a frequency selective surface. The dipoles are equipped with photonic switches permitting variable electrical dipole lengths for broadband performance and the FSS is suitably designed to simulate a variable substrate thickness for optimal operation. A general view of the geometry is given in Figure 1.

The UM/UH team proposed to construct a code which combines various computational modules interfaced with appropriate pre-processors and post-processors. The computational modules include: Stand-alone moment method simulation of the FSS with up to 10 layers with commensurate and non-commensurate periodicities. Simple moment method simulation of the antenna elements on the FSS panels Hybrid FEM simulation modules for small arrays, planar periodic arrays and curved arrays on FSS panels. Various options for modeling the FSS and for mesh truncation were proposed to provide a compromise between speed and accuracy. These are outlined in the proposal and summarized in the attached milestone chart (repeated from the proposal) .

2 MEETINGS

As noted above, the UM/UH SERAT activity began earnestly in October 1996 when the UM and Sanders contract was formally signed. Therefore, this is our first quarterly report covering the period from 1 October to 31 December 1996. The UH subcontract was initiated immediately afterwards and was formally in place by early November.

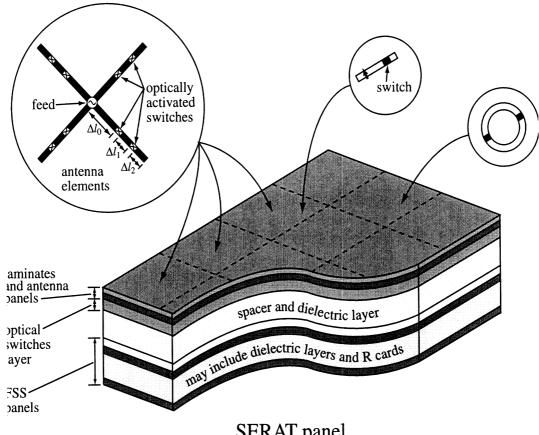
The kickoff meeting took place on September 20, 1996 and was attended by Roland Gilbert (Sanders), Henry Karwacki (Sanders), J. Volakis (UM), J. Gong (UM), S. Bindiganavale (UM), D. Wilton (UH) and D. Jackson (UH). At the meeting, Dr. Gilbert presented an overview of the SERAT program and UM/UH presented the code development plan and related R&D effort at some detail. Follow-up discussions between the Sanders and UM/UH centered on the various parts of the codes, their feasibility and the capabilities of the Green's function for non-commensurate periodicities.

UM gave a follow-up review of the SERAT analysis software at the Nov 15, 1996 review meeting of the SERAT program held at Nashua.

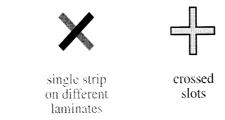
3 HIGHLIGHTS OF THE 1ST QUARTERLY ACTIV-ITY

3.1 Code Development and Integration Plan

Before beginning with the implementation of the tasks outlined in the proposal (attached in section 4 of this report) and summarized in the milestone chart, it was necessary to designate a careful code development plan. This was done by Dr. Gong who is in charge of the overall code development plan. An overview of the proposed code integration plan is depicted in



SERAT panel



FSS elements

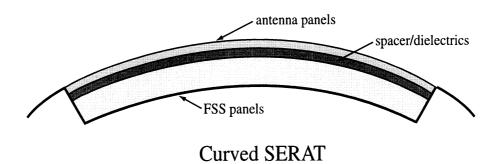


Figure 1: An Example of SERAT Configuration

Figure 2. Basically, the analysis engine (FEM, hybrid and moment method modules) will require a single geometrical interface, and the pre-processors will be used to translate and/or reformat data as needed for the various computational modules. The post-processors will include the necessary data interfaces for graphical display and parameter extraction. We investigated a number of Unix platform plotting and visualization packages in October and we selected two freeware packages. One of the them is the xmgr plotting package with ease to use graphical interface allowing for plotting and data display with X windows. This package reads in spreadsheet output datafile which can be also ported on personal computer (PC and Macs) for plotting and display. A second package was also investigated for less interactive capability but easy to integrate with our developed code and to be called directly from inside the code. The output will be high quality postscript format which can be displayed and printed on any platform.

In addition to the above, a rather major effort during this quarter was devoted to the investigation of fast solver for sparse FEM system. Specifically, we investigated the convergence of new BCG, QMR and GMRES algorithms and concluded that BCG is still the most attractive of all these algorithms. However, a new fast solver was recently introduced for inverting sparse systems. This solver, referred to as CVSS, was developed by NASA funding and is available to U.S. companies, agencies and institutions. CVSS is an LU type solver specialized to sparse systems but because of its efficient memory use, speed and limited need for interface with user, it was shown to be competitive with the iterative methods. At this stage, we will continue the investigation of these solvers and we will report on them after their use in a specific SERAT analysis module.

In accordance with the schedule shown in the milestone chart, two major activities were carried out in parallel:

3.2 FSS and Simple Moment Method Code Development

This subproject is carried out at the Univ of Houston(UH) by Profs. Wilton and Jackson. As stated in the proposal, these moment method codes will serve for the evaluation of the multilayered FSS and simple antenna(strip and slots) element analysis in the presence of the FSS. A first version of the code(s) will be completed by the end of the 2nd quarter for commensurate periods with the more general code versions for non-commensurate periods to be available at the end of the first year. UH is on schedule for the delivery of these codes.

At the start of the contract, UH had two codes available for target scattering and antenna radiation in the presence of multilayered media (See Figure 3). One of them was capable of modeling periodic FSS-type structures but was not equipped with the ease to use I/O interfaces. Moreover, the employed periodic Green's function was not optimized for fast convergence. The second code (referred to as EIGER) is equipped with a much improved I/O interface and its implementation is based on the more attractive and rigorous mixed potential integral equation(MPIE) formulation. However, the code is not specialized to periodic structures. The latter implies a necessary replacement of the Green's function and since neither code employed a fast convergent Green's function, UH decided to employ the EIGER code as the basis for the development of the new moment method SERAT code.

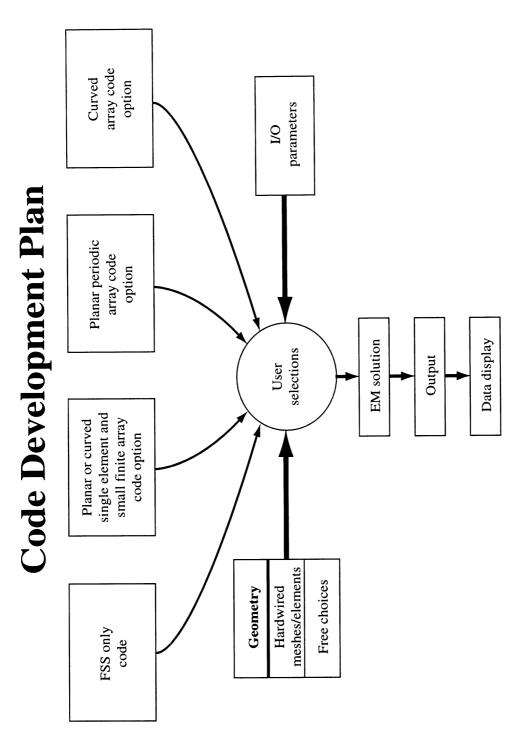


Figure 2: Code Development/Integration Plan

Milestone Chart for EM Model Development (Tasks 1 and 2) Quarterly Progress

Task	1st Q.	2nd Q.	3rd Q.	4th Q.	5th Q.	6th Q.	7th Q.
FSS Green's function and Code (U of Houston)		-					
Mesh Generator for Antenna Elements		├ ->					
Mesh generator for FSS elements				\longrightarrow			
Single Element and Small Array							
Planar and Curved-IBC	-	>					
Planar-FEM/Moment Method							
Curved-FEM for antenna and FSS					-		
Planar Periodic Array							
FEM with IBCs		-	•				
Simple Moment Method code				-	•		
FEM and Moment Method for FSS					-		
FEM for antenna and FSS					\rightarrow		
Curved Array							
Cylindrical						•	
Approximate Doubly Curved							
Doubly Curved with fast integral algorithms for mesh truncations							•
Software Integration and I/O Displays						-	
Validation							
Software Support							

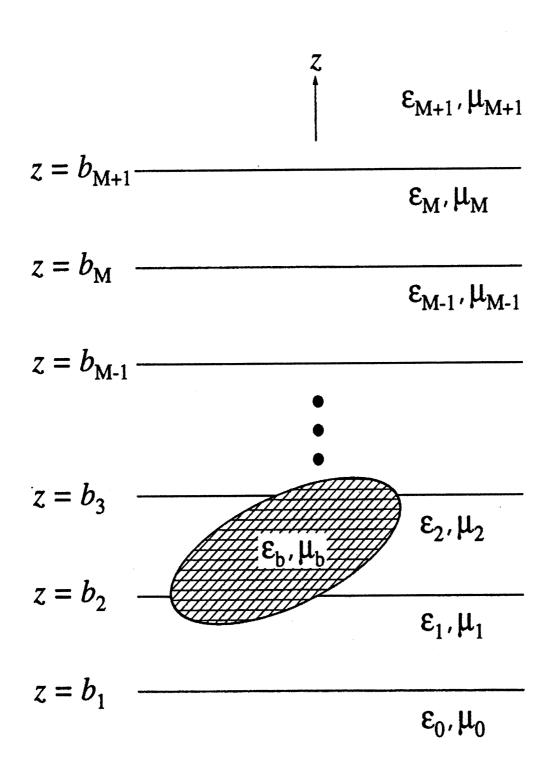


Figure 3: Obstacle or antenna radiator in the presence of multilayered medium

In addition to upgrading EIGER, during the past three months, UH emphasized the development and implementation of acceleration techniques for a fast implementation of the periodic multilayered Green's function. This is the crux of the moment method code implementation and its efficiency is therefore essential in delivering a useful stand-alone and hybrid FEM code. Instead of using the Singh et.al. approach, UH employed an acceleration technique introduce by Ewald. This technique replaces the periodic (Floquet expansion) Green's function (a sum of spectral integrals) by sums of sampled values of the spectra on a reciprocal lattice. Basically, the summations of the Floquet expansion are replaced by a fast converging semi-definite integrals which can be cast in terms of complimentary error functions. Using these replacements, the resulting Floquet sums are rapidly converging. Initial results based on the free standing periodic structure show that speed-ups on the order of 50 to 100 can be achieved using the Ewald approach. Actual series convergence curves are given in Figures 4 and 5 for the two sums (spectral and spatial) of the Floquet representation. It is seen that the new series converges using 2 to 3 terms, whereas the older approach (based on Singh's method) requires 50 to 200 terms to achieve convergence using the same error criterion.

A short description of UH's acceleration technique and MPIE formulation is given in the attached section to this quarterly report. More details on the technical aspects of the implementation will be given after code completion.

In the next quarter, UH plans to implement the new acceleration technique for the multilayered periodic media and to complete the moment method code for commensurate periods. The code will then be delivered to UM for incorporation into the FEM hybrid code and for stand-alone analysis.

3.3 Small Array hybrid FEM code

UM began the development of this module in early November 1996. According to our schedule, the plan is to complete a first version of the small array and planar periodic codes by the end of 4th quarter. Over the past two months, we developed the formulation of the FEM code using second order prismatic elements. Instead of proceeding to modify one of our existing FEM codes, we opted to develop a totally new code to accommodate the planned mesh truncation options, IBC simulations of the FSS and specialization to the FSS configurations. Developing a new code from scratch is certainly a more time consuming task but will result in a better overall code. Moreover, this approach will avoid potential difficulties typically associated with older codes written for different applications.

A key feature of the code under development is the use of higher order prismatic elements which will permit a straightforward application of the code to doubly curved arrays and FSS panels. We anticipate that the testing of the code will begin toward the end of January. At that time we will also test the use of higher order IBCs for modeling FSS panels.

Attached to this quarterly report in the Appendices are the Code Development Flow Chart, the feature descriptions of the chosen FEM elements, and the post processing package.

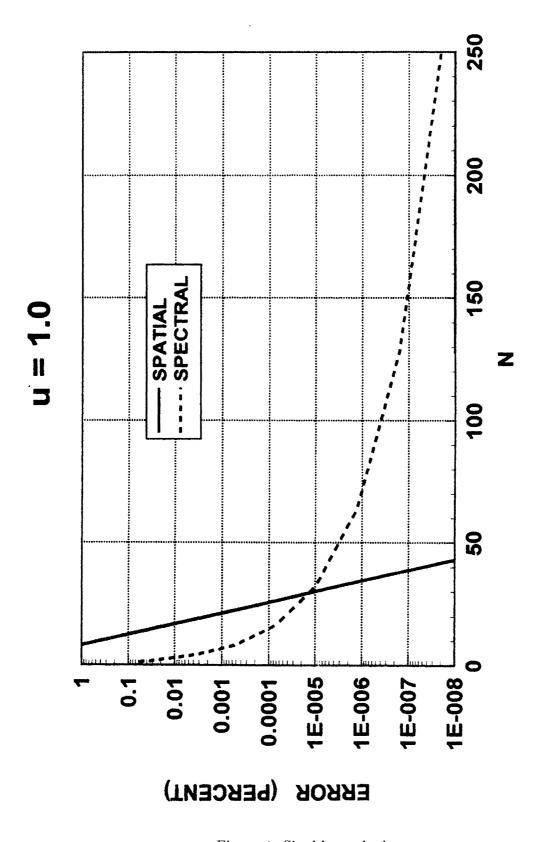
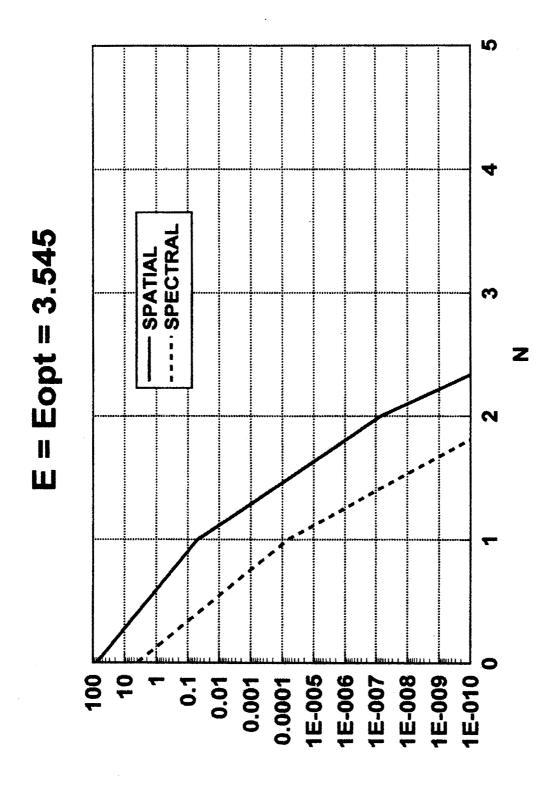


Figure 4: Singh's method



ЕВВОВ (РЕВСЕЙТ)

Figure 5: Ewald's method

A ANTICIPATED TASKS AND SCHEDULE

The following anticipated 'ready-for-delivery' time is referred with respect to the project starting time from October 1996.

Single Element or Small Array Code:

- Scheduled Ready-for-Delivery Time: sixth months
- Purpose: to model elementary parts of the SERAT panel and acts as an FEM kernel
- Features:
 - Modular (FE-BI, FE-PML, FE-IBC, etc.);
 - Capable for fast solutions;
 - Capable of modeling antenna/FSS elementary coupling;
 - Simplified feed models;
 - Rendering reconfigurable design of SERAT platform (thickness)
- Challenging Efforts:
 - Development of a high-order p-type element FEM code
 - Fast solution scheme (robust iterative/direct solvers)
 - Mesh automation/semi-automation (triangularization)
 - Speed-up PML convergence; improve BI efficiency (whenever used)
 - User-friendly environment design

Periodic Array Code:

- Scheduled Ready-for-Delivery Time: one year
- Purpose: to model the periodic infinite SERAT panel
- Features:
 - Able to model infinitely large SERAT panel (in contrast to MoM)
 - Capable of incorporating inhomogeneity, feedlines, etc.
 - Fast and efficient
 - Appropriate for reconfigurable design
- Challenging Efforts:
 - Period FEM development (periodic BC's)
 - Periodic BI development
 - Periodic IBC development
 - Combination with BI/IBC

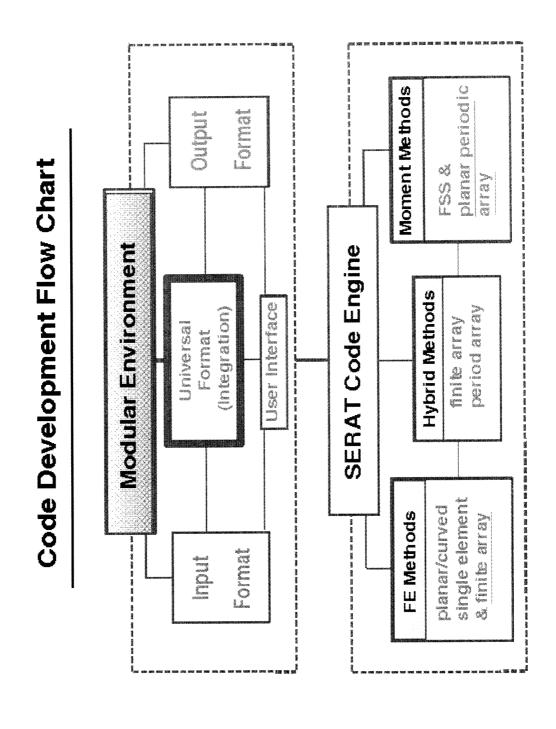
- Feed model incorporation
- Fast solver testing
- User interface design
- Reconfigurable design ability

Full Hybrid FEM Code

- Scheduled Ready-for-Delivery Time: 16-18th months
- Purpose: to accurately model the entire non-commensurate SERAT
- Features:
 - Considers the entire couplings of FSS-FSS, antenna-antenna, FSS-antenna, feed-line, etc.
 - Considers the finite sized platform (edge effects, etc.)
 - Considers the curved platform
- Challenging Efforts:
 - Mesh generation
 - User-friendly interface design
 - Curved platform incorporation
 - Speed-up solution time as much as possible!!!

Package Integration and Validation

- Universal file format design/modification
- Modular environment design and integration
- Software validation
- Software documentation



B ATTRIBUTES OF PRISMATIC ELEMENTS

- Suited for multi-layered structures
- With minimum number of unknowns for large thicknessslot-ratio
- Good system condition
- More accurate with higher order version of basis functions
- Meshing needed only on a surface
- Extendable to doubly-curved structures

C POST PROCESSING PACKAGES

A FEW ATTRIBUTES OF XMGR PLOTTING PACKAGE

- User defined scaling, tick marks, labels, symbols, line styles, colors.
- Batch mode for unattended plotting.
- Read and write parameters used during a session.
- Polynomial regression, splines, running averages, DFT/FFT, cross/auto-correlation.
- Hardcopy support for PostScript, HP-GL, and FrameMaker .mif format.

Figure 6 is the sample layout by the XMGR package.

ABOUT PGPLOT PLOTTING PACKAGE

PGPLOT is a Fortran subroutine package for drawing scientific graphs on various graphics display devices. It is intended for the Fortran programmer who wishes to write a program generating graphical output. For most applications, the program can be device-independent, and the output can be directed to the appropriate device at run time.

Figure 7 shows the graphic sample plots using the PGPLOT package.

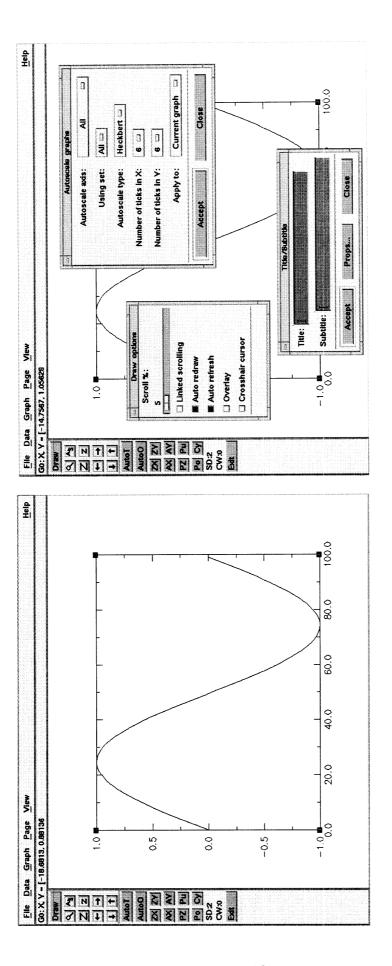


Figure 6: Sample Layout of the XMGR Plotting Package

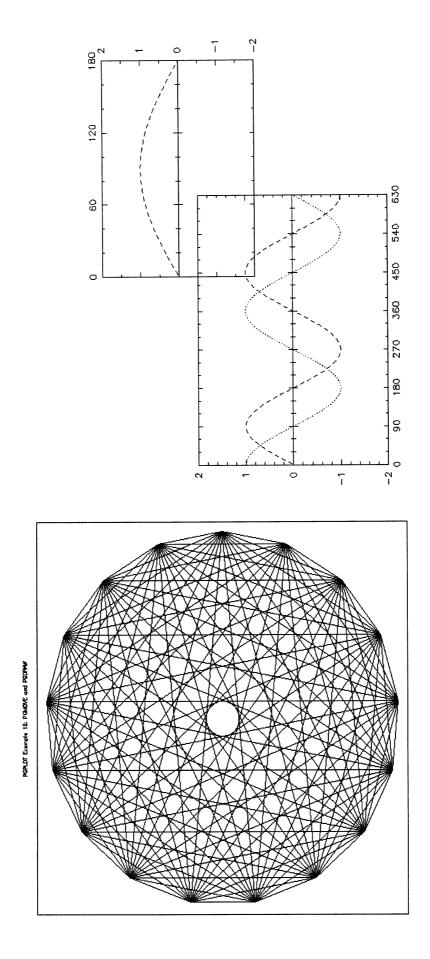


Figure 7: Sample Graphic Plots Using PGPLOT Package

D Field Representations for Multi-Layered Periodic Media

The electric field due to equivalent electric and magnetic currents is written in the mixed potential integral equation (MPIE) representation as

$$\boldsymbol{E}^{s}(\boldsymbol{r}) = -j\omega\boldsymbol{A} - \boldsymbol{\nabla}\Phi - \frac{1}{\epsilon}\boldsymbol{\nabla}\times\boldsymbol{F}, \tag{1}$$

with the corresponding magnetic field expressed as

$$\mathbf{H}^{s}(\mathbf{r}) = -j\omega\mathbf{F} - \nabla\Psi + \frac{1}{\mu}\nabla \times \mathbf{A}.$$
 (2)

The magnetic vector potential is defined as

$$\mathbf{A}(\mathbf{r}) = \int_{S} \mathcal{G}^{A}(\mathbf{r}, \mathbf{r}') \cdot \mathbf{J}(\mathbf{r}') dS'$$
(3)

while the electric vector potential is

$$F(r) = \int_{S} \mathcal{G}^{F}(r, r') \cdot M(r') dS'. \tag{4}$$

The electric scalar potential is

$$\Phi(\mathbf{r}) = \frac{j\omega}{k^2} \nabla \cdot \mathbf{A}(\mathbf{r})$$

$$= \frac{j\omega}{k^2} \int_{S} \nabla \cdot \mathbf{\mathcal{G}}^A(\mathbf{r}, \mathbf{r}') \cdot \mathbf{J}(\mathbf{r}') dS'$$

$$= \int_{S} \nabla'_{S} \cdot \mathbf{J}(\mathbf{r}') K^{\Phi}(\mathbf{r}, \mathbf{r}') dS' + \int_{S} \hat{\mathbf{z}} \cdot \mathbf{J}(\mathbf{r}') P_{z}(\mathbf{r}, \mathbf{r}') dS', \qquad (5)$$

wher the last equality follows from using the relation

$$\frac{j\omega}{k^2} \nabla \cdot \mathcal{G}^A(\boldsymbol{r}, \boldsymbol{r}') = -\nabla' K^{\Phi}(\boldsymbol{r}, \boldsymbol{r}') + \hat{\boldsymbol{z}} P_z(\boldsymbol{r}, \boldsymbol{r}'), \tag{6}$$

followed by an integration by parts. Michalski shows that such a splitting of the scalar potential is always possible and permits the order of the singularity in the scalar potential kernel to be reduced by transferring a derivative from the kernel onto the current.

The corresponding magnetic scalar potential is

$$\Psi(\mathbf{r}) = \frac{j\omega}{k^2} \nabla \cdot \mathbf{F}(\mathbf{r})$$

$$= \frac{j\omega}{k^2} \int_{S} \nabla \cdot \mathcal{G}^F(\mathbf{r}, \mathbf{r}') \cdot \mathbf{M}(\mathbf{r}') dS'$$

$$= \int_{S} \nabla'_{S} \cdot \mathbf{M}(\mathbf{r}') K^{\Psi}(\mathbf{r}, \mathbf{r}') dS' + \int_{S} \hat{\mathbf{z}} \cdot \mathbf{M}(\mathbf{r}') Q_{z}(\mathbf{r}, \mathbf{r}') dS', \tag{7}$$

which can be written as

$$\frac{j\omega}{k^2} \nabla \cdot \mathcal{G}^F(\boldsymbol{r}, \boldsymbol{r}') = -\nabla' K^{\Psi}(\boldsymbol{r}, \boldsymbol{r}') + \hat{\boldsymbol{z}} Q_z(\boldsymbol{r}, \boldsymbol{r}'). \tag{8}$$

The vector potential dyadic Green's function \mathcal{G}^A is not unique, but the most convenient form for numerical work has the form

$$\mathcal{G}^{A}(\boldsymbol{r},\boldsymbol{r}') = \begin{bmatrix}
G_{xx}^{A}(\boldsymbol{r},\boldsymbol{r}') & 0 & 0 \\
0 & G_{yy}^{A}(\boldsymbol{r},\boldsymbol{r}') & 0 \\
G_{zx}^{A}(\boldsymbol{r},\boldsymbol{r}') & G_{zy}^{A}(\boldsymbol{r},\boldsymbol{r}') & G_{zz}^{A}(\boldsymbol{r},\boldsymbol{r}')
\end{bmatrix}$$

$$= \frac{1}{A} \sum_{p=-\infty}^{\infty} \sum_{q=-\infty}^{\infty} \tilde{\mathcal{G}}_{pq}^{A}(z,z') e^{-j\boldsymbol{k}_{pq}\cdot(\boldsymbol{\rho}-\boldsymbol{\rho}')}, \qquad (9)$$

where $\tilde{\mathcal{G}}_{pq}^A$ constitutes a set of sampled values of the spectral representation of the magnetic vector potential for a point source in a layered medium. The sampled values are on the reciprocal lattice of the wavenumber domain and correspond to the grating lobe wavenumbers of the periodic structure. The series may be said to be a Floquet modal or grating lobe series representation for the magnetic vector potential. The elements of the dyad, in turn, may be

written as

$$\tilde{\mathcal{G}}_{pq}^{A}(z,z') = \begin{bmatrix}
\frac{1}{j\omega}V_{i}^{h}(z,z') & 0 & 0 \\
0 & \frac{1}{j\omega}V_{i}^{h}(z,z') & 0 \\
\frac{\mu k_{xpq}}{jk_{\rho pq}^{2}} \left[I_{i}^{h}(z,z') - I_{i}^{e}(z,z')\right] & \frac{\mu k_{ypq}}{jk_{\rho pq}^{2}} \left[I_{i}^{h}(z,z') - I_{i}^{e}(z,z')\right] & \frac{\mu}{j\omega\epsilon'}I_{v}^{e}(z,z'),
\end{bmatrix},$$
(10)

where, for example, $V_i^h(z, z')$ is the voltage at z due to a unit current source at z' on the cascaded transmission lines representing the layered media for TE_z (h-) polarized fields with transverse wavenumbers \mathbf{k}_{tpq} . Similarly, $I_v^e(z, z')$ is the current at z due to a unit voltage source at z' for the corresponding TM_z (e-) polarized fields, and so on. The corresponding scalar potential grating lobe series representations are

$$K^{\Phi}(\boldsymbol{r}, \boldsymbol{r}') = \frac{1}{A} \sum_{p=-\infty}^{\infty} \sum_{q=-\infty}^{\infty} \tilde{K}^{\Phi}_{pq}(z, z') e^{-j\boldsymbol{k}_{pq}\cdot(\boldsymbol{\rho}-\boldsymbol{\rho}')}, \qquad (11)$$

where

$$\tilde{K}_{pq}^{\Phi}(z,z') = \frac{V_i^h(z,z') - V_i^e(z,z')}{k_{gpg}^2}, \tag{12}$$

and

$$P_z(\boldsymbol{r}, \boldsymbol{r}') = \frac{1}{A} \sum_{p=-\infty}^{\infty} \sum_{q=-\infty}^{\infty} \tilde{P}_{zpq}(z, z') e^{-j\boldsymbol{k}_{pq}\cdot(\boldsymbol{\rho}-\boldsymbol{\rho}')}, \qquad (13)$$

where

$$\tilde{P}_{zpq}(z,z') = \frac{j\omega\mu'}{k_{ppq}^2} \left[V_v^h(z,z') - V_v^e(z,z') \right]. \tag{14}$$

The electric vector potential is completely dual to the magnetic vector potential above and is given by

$$\mathcal{G}^{F}(\boldsymbol{r}, \boldsymbol{r}') = \begin{bmatrix}
G_{xx}^{F}(\boldsymbol{r}, \boldsymbol{r}') & 0 & 0 \\
0 & G_{yy}^{F}(\boldsymbol{r}, \boldsymbol{r}') & 0 \\
G_{zx}^{F}(\boldsymbol{r}, \boldsymbol{r}') & G_{zy}^{F}(\boldsymbol{r}, \boldsymbol{r}') & G_{zz}^{F}(\boldsymbol{r}, \boldsymbol{r}')
\end{bmatrix}$$

$$= \frac{1}{A} \sum_{p=-\infty}^{\infty} \sum_{q=-\infty}^{\infty} \tilde{\mathcal{G}}_{pq}^{F}(z, z') e^{-j\boldsymbol{k}_{pq} \cdot (\boldsymbol{\rho} - \boldsymbol{\rho}')}, \qquad (15)$$

where

$$\tilde{\mathcal{G}}_{pq}^{F}(z,z') \ = \ \begin{bmatrix} \frac{1}{j\omega}I_{v}^{e}(z,z') & 0 & 0\\ 0 & \frac{1}{j\omega}I_{v}^{e}(z,z') & 0\\ \frac{\epsilon k_{xpq}}{jk_{\rho pq}^{2}}\left[V_{v}^{e}(z,z') - V_{v}^{h}(z,z')\right] & \frac{\epsilon k_{ypq}}{jk_{\rho pq}^{2}}\left[V_{v}^{e}(z,z') - V_{v}^{h}(z,z')\right] & \frac{\epsilon}{j\omega\mu'}V_{i}^{h}(z,z') \end{bmatrix}.$$

(16)

Similarly, the corresponding scalar potentials dual to those above are given as follows:

$$K^{\Psi}(\boldsymbol{r}, \boldsymbol{r}') = \frac{1}{A} \sum_{p=-\infty}^{\infty} \sum_{q=-\infty}^{\infty} \tilde{K}_{pq}^{\Psi}(z, z') e^{-j\boldsymbol{k}_{pq}\cdot(\boldsymbol{\rho}-\boldsymbol{\rho}')}, \qquad (17)$$

where

$$\tilde{K}_{pq}^{\Psi}(z,z') = \frac{I_v^e(z,z') - I_v^h(z,z')}{k_{\rho pq}^2}$$
(18)

and

$$Q_z(\boldsymbol{r}, \boldsymbol{r}') = \frac{1}{A} \sum_{p=-\infty}^{\infty} \sum_{q=-\infty}^{\infty} \tilde{Q}_{zpq}(z, z') e^{-j\boldsymbol{k}_{pq}\cdot(\boldsymbol{\rho}-\boldsymbol{\rho}')}, \qquad (19)$$

where

$$\tilde{Q}_{zpq}(z,z') = \frac{j\omega\epsilon'}{k_{ppq}^2} \left[I_i^e(z,z') - I_i^h(z,z') \right]. \tag{20}$$

Various derivatives of the potentials are needed to complete the field descriptions. In particular, the curl of the magnetic vector potential is

$$\nabla \times \boldsymbol{A}(\boldsymbol{r}) = \int_{S} \nabla \times \boldsymbol{\mathcal{G}}^{A}(\boldsymbol{r}, \boldsymbol{r}') \cdot \boldsymbol{J}(\boldsymbol{r}') dS'$$
 (21)

$$\nabla \times \mathcal{G}^{A}(\mathbf{r}, \mathbf{r}') = \begin{bmatrix} \frac{\partial G_{zx}^{A}}{\partial y} & \left(\frac{\partial G_{zy}^{A}}{\partial y} - \frac{\partial G_{yy}^{A}}{\partial z}\right) & \frac{\partial G_{zz}^{A}}{\partial y} \\ \left(\frac{\partial G_{xx}^{A}}{\partial z} - \frac{\partial G_{zx}^{A}}{\partial x}\right) & -\frac{\partial G_{zy}^{A}}{\partial x} & -\frac{\partial G_{zz}^{A}}{\partial x} \\ -\frac{\partial G_{xx}^{A}}{\partial y} & \frac{\partial G_{yy}^{A}}{\partial x} & 0 \end{bmatrix}$$
(22)

$$= \frac{1}{A} \sum_{p=-\infty}^{\infty} \sum_{q=-\infty}^{\infty} \tilde{\boldsymbol{\nabla}}_{pq} \times \tilde{\boldsymbol{\mathcal{G}}}_{pq}^{A}(z,z') e^{-j\boldsymbol{k}_{pq} \cdot (\boldsymbol{\rho} - \boldsymbol{\rho}')},$$

where the spectral form of the nabla operator is defined as

$$\tilde{\mathbf{\nabla}}_{pq} = -j\mathbf{k}_{tpq} + \hat{\mathbf{z}}\frac{\partial}{\partial z} = -jk_{xpq}\hat{\mathbf{x}} - jk_{ypq}\hat{\mathbf{y}} + \hat{\mathbf{z}}\frac{\partial}{\partial z}.$$

Thus, we have

$$\tilde{\boldsymbol{\nabla}}_{pq} \times \tilde{\boldsymbol{\mathcal{G}}}_{pq}^{A}(z,z') = \begin{bmatrix} -\frac{\mu k_{xpq} k_{ypq}}{k_{\rho pq}^{2}} [I_{i}^{h} - I_{i}^{e}] & -\frac{\mu k_{ypq}^{2}}{k_{\rho pq}^{2}} [I_{i}^{h} - I_{i}^{e}] + \mu I_{i}^{h} & -\frac{\mu k_{ypq}}{\omega \epsilon'} I_{v}^{e} \\ \frac{\mu k_{xpq}^{2}}{k_{\rho pq}^{2}} [I_{i}^{h} - I_{i}^{e}] - \mu I_{i}^{h} & \frac{\mu k_{xpq} k_{ypq}}{k_{\rho pq}^{2}} [I_{i}^{h} - I_{i}^{e}] & \frac{\mu k_{xpq}}{\omega \epsilon'} I_{v}^{e} \\ \frac{k_{ypq}}{\omega} V_{i}^{h} & -\frac{k_{xpq}}{\omega} V_{i}^{h} & 0 \end{bmatrix},$$
(23)

where the transmission line equations are used to replace any z-derivatives with voltage or current quantities again.

Similarly, the gradients of the electric scalar potential functions are defined as

$$\nabla K^{\Phi}(\boldsymbol{r}, \boldsymbol{r}') = \frac{1}{A} \sum_{p=-\infty}^{\infty} \sum_{q=-\infty}^{\infty} \tilde{\nabla}_{pq} \tilde{K}_{pq}^{\Phi}(z, z') e^{-j\boldsymbol{k}_{pq} \cdot (\boldsymbol{\rho} - \boldsymbol{\rho}')}, \qquad (24)$$

where

$$\tilde{\boldsymbol{\nabla}}_{pq}\tilde{K}_{pq}^{\Phi}(z,z') = \left[-j\boldsymbol{k}_{tpq} \left(\frac{V_i^h - V_i^e}{k_{\rho pq}^2} \right) + \hat{\boldsymbol{z}} \frac{jk_{zpq}}{k_{\rho pq}^2} \left(\frac{k_{zpq}}{\omega \epsilon} I_i^e - \frac{\omega \mu}{k_{zpq}} I_i^h \right) \right], \tag{25}$$

and

$$\nabla P_z(\boldsymbol{r}, \boldsymbol{r}') = \frac{1}{A} \sum_{p=-\infty}^{\infty} \sum_{q=-\infty}^{\infty} \tilde{\nabla}_{pq} \tilde{P}_{zpq}(z, z') e^{-j\boldsymbol{k}_{pq} \cdot (\boldsymbol{\rho} - \boldsymbol{\rho}')}, \qquad (26)$$

where

$$\tilde{\boldsymbol{\nabla}}_{pq}\tilde{P}_{zpq}(z,z') = \left[\boldsymbol{k}_{tpq}\frac{\omega\mu'}{k_{\rho pq}^2}(V_v^h - V_v^e) + \hat{\boldsymbol{z}}\frac{\omega\mu'k_{zpq}}{k_{\rho pq}^2}\left(\frac{\omega\mu}{k_{zpq}}I_v^h - \frac{k_{zpq}}{\omega\epsilon}I_v^e\right)\right]$$
(27)

By duality, we obtain the curl of the electric vector potential,

$$\nabla \times F(r) = \int_{S} \nabla \times \mathcal{G}^{F}(r, r') \cdot M(r') dS,$$
 (28)

where

$$\nabla \times \mathcal{G}^{F}(\mathbf{r}, \mathbf{r}') = \begin{bmatrix} \frac{\partial G_{zx}^{F}}{\partial y} & \left(\frac{\partial G_{zy}^{F}}{\partial y} - \frac{\partial G_{yy}^{F}}{\partial z}\right) & \frac{\partial G_{zz}^{F}}{\partial y} \\ \left(\frac{\partial G_{xx}^{F}}{\partial z} - \frac{\partial G_{zx}^{F}}{\partial x}\right) & -\frac{\partial G_{zy}^{F}}{\partial x} & -\frac{\partial G_{zz}^{F}}{\partial x} \\ -\frac{\partial G_{xx}^{F}}{\partial y} & \frac{\partial G_{yy}^{F}}{\partial x} & 0 \end{bmatrix}$$
(29)

$$= \frac{1}{A} \sum_{p=-\infty}^{\infty} \sum_{q=-\infty}^{\infty} \tilde{\boldsymbol{\nabla}}_{pq} \times \tilde{\boldsymbol{\mathcal{G}}}_{pq}^{F}(z,z') e^{-j\boldsymbol{k}_{pq} \cdot (\boldsymbol{\rho} - \boldsymbol{\rho}')},$$

and where

$$\tilde{\boldsymbol{\nabla}}_{pq} \times \tilde{\boldsymbol{\mathcal{G}}}_{pq}^{F}(z,z') = \begin{bmatrix} -\frac{\epsilon k_{xpq}k_{ypq}}{k_{\rho pq}^{2}}[V_{v}^{e} - V_{v}^{h}] & -\frac{\epsilon k_{ypq}^{2}}{k_{\rho pq}^{2}}[V_{v}^{e} - V_{v}^{h}] + \epsilon V_{v}^{e} & -\frac{\epsilon k_{ypq}}{\omega \mu'}V_{i}^{h} \\ \frac{\epsilon k_{xpq}^{2}}{k_{\rho pq}^{2}}[V_{v}^{e} - V_{v}^{h}] - \epsilon V_{v}^{e} & \frac{\epsilon k_{xpq}k_{ypq}}{k_{\rho pq}^{2}}[V_{v}^{e} - V_{v}^{h}] & \frac{\epsilon k_{xpq}}{\omega \mu'}V_{i}^{h} \\ \frac{k_{ypq}}{\omega}I_{v}^{e} & -\frac{k_{xpq}}{\omega}I_{v}^{e} & 0 \end{bmatrix}.$$

$$(30)$$

Similarly, the gradients of the scalar potentials are given by

$$\nabla K^{\Psi}(\boldsymbol{r}, \boldsymbol{r}') = \frac{1}{A} \sum_{p=-\infty}^{\infty} \sum_{q=-\infty}^{\infty} \tilde{\nabla}_{pq} \tilde{K}_{pq}^{\Psi}(z, z') e^{-j\boldsymbol{k}_{pq} \cdot (\boldsymbol{\rho} - \boldsymbol{\rho}')}, \tag{31}$$

where

$$\tilde{\boldsymbol{\nabla}}_{pq}\tilde{K}_{pq}^{\Psi}(z,z') = \frac{1}{A} \sum_{p=-\infty}^{\infty} \sum_{q=-\infty}^{\infty} \left[-j\boldsymbol{k}_{tpq} \left(\frac{I_v^e - I_v^h}{k_{\rho pq}^2} \right) + \hat{\boldsymbol{z}} \frac{jk_{zpq}}{k_{\rho pq}^2} \left(\frac{k_{zpq}}{\omega \mu} V_v^h - \frac{\omega \epsilon}{k_{zpq}} V_v^e \right) \right]$$
(32)

and

$$\nabla Q_z(\boldsymbol{r}, \boldsymbol{r}') = \frac{1}{A} \sum_{p=-\infty}^{\infty} \sum_{q=-\infty}^{\infty} \tilde{\nabla}_{pq} \tilde{Q}_{zpq}(z, z') e^{-j\boldsymbol{k}_{pq} \cdot (\boldsymbol{\rho} - \boldsymbol{\rho}')}, \tag{33}$$

where

$$\tilde{\boldsymbol{\nabla}}_{pq}\tilde{Q}_{zpq}(z,z') = \left[\boldsymbol{k}_{tpq}\frac{\omega\epsilon'}{k_{\rho pq}^2}(I_i^e - I_i^h) + \hat{\boldsymbol{z}}\frac{\omega\epsilon'k_{zpq}}{k_{\rho pq}^2}\left(\frac{\omega\epsilon}{k_{zpq}}V_i^e - \frac{k_{zpq}}{\omega\mu}V_i^h\right)\right]. \tag{34}$$

E Extraction of Asymptotic Forms of Series

When z and z' are well-separated, the convergence of the grating lobe series is, in principal, exponential. When z or z' are in the same or in adjacent layers, however, we attempt to enhance the convergence of the grating lobe series representations. The procedure for doing this may be summarized as follows:

- The asymptotic forms of the transmission line quantities are determined for large spectral values. These forms contain terms of the form $\frac{e^{-jk_z|z-z'|}}{2jk_z}$ and $\frac{e^{-jk_z|(z-d)-(d-z')|}}{2jk_z}$ which may be identified as so-called direct and quasi-static image terms, respectively. They appear to arise as a direct or homogeneous medium contribution from the actual source located at z=z' or from its image at z=2d-z'. The direct contribution is exact; the image contribution is only asymptotically correct, but becomes exact as $\omega \to 0$. Hence it is often said to be a the quasi-static image.
- Terms from the asymptotic series series are removed from the grating lobe series (Kummer's transformation) to enhance its convergence.
- The contributions from terms removed from the series must be replaced. It may be shown, however, that they constitute contributions from an array of phased point sources (spatial representation), and may be obtained by using Poisson's transformation on the removed series. We thus obtain a hybrid spectral representation in which most of the layered media effects are in the spectral (grating lobe) series, while effects of the direct and first-bounce images of the source in adjacent layers are primarily contained in the form of spatial series.
- The spatial series summations may be accelerated using Singh's method, Ewald's method, or other acceleration methods (discussed later).

By standard transmission line theory, the asymptotic forms of the transmission line voltages and currents are obtained as follows:

$$V_{i}^{s}(z,z') = \begin{cases} \frac{Z'^{s}}{2} \left(e^{-jk_{z}|z-z'|} + \overrightarrow{\Gamma}_{\infty}^{\prime s} e^{-jk_{z}|z+z'-2b_{m'+1}|} + \overleftarrow{\Gamma}_{\infty}^{\prime s} e^{-jk_{z}|z+z'-2b_{m'}|} \right), & m = m', \\ \frac{Z'^{s}}{2} \left(1 + \overrightarrow{\Gamma}_{\infty}^{\prime s} \right) e^{-jk_{z}|z-z'|}, & m = m' + 1 \\ \frac{Z'^{s}}{2} \left(1 + \overleftarrow{\Gamma}_{\infty}^{\prime s} \right) e^{-jk_{z}|z-z'|}, & m = m' - 1 \end{cases}$$

$$= \frac{Z'^{s}}{2} \left[\left(\delta_{m,m'} + \delta_{m,m'+1} (1 + \overrightarrow{\Gamma}_{\infty}^{\prime s}) + \delta_{m,m'-1} (1 + \overleftarrow{\Gamma}_{\infty}^{\prime s}) \right) e^{-jk_{z}|z-z'|} + \delta_{m,m'} \left(\overrightarrow{\Gamma}_{\infty}^{\prime s} e^{-jk_{z}|z+z'-2b_{m'+1}|} + \overleftarrow{\Gamma}_{\infty}^{\prime s} e^{-jk_{z}|z+z'-2b_{m'}|} \right) \right]$$

$$I_{i}^{s}(z,z') = \begin{cases} \frac{1}{2} \left(\operatorname{sgn}(z-z')e^{-jk_{z}|z-z'|} + \overrightarrow{\Gamma}_{\infty}^{\prime s} \operatorname{sgn}(z+z'-2b_{m'+1}) e^{-jk_{z}|z+z'-2b_{m'+1}|} \right. \\ + \overrightarrow{\Gamma}_{\infty}^{\prime s} \operatorname{sgn}(z+z'-2b_{m'}) e^{-jk_{z}|z+z'-2b_{m'}|} \right), \qquad m = m', \\ \frac{1}{2} \left(1 - \overrightarrow{\Gamma}_{\infty}^{\prime s} \right) \operatorname{sgn}(z-z')e^{-jk_{z}|z-z'|}, \qquad m = m' + \\ \frac{1}{2} \left(1 - \overrightarrow{\Gamma}_{\infty}^{\prime s} \right) \operatorname{sgn}(z-z')e^{-jk_{z}|z-z'|}, \qquad m = m' - \end{cases}$$

$$= \frac{1}{2} \left[\left(\delta_{m,m'} + \delta_{m,m'+1} (1 - \overrightarrow{\Gamma}_{\infty}^{\prime s}) + \delta_{m,m'-1} (1 - \overleftarrow{\Gamma}_{\infty}^{\prime s}) \right) \operatorname{sgn}(z-z')e^{-jk_{z}|z-z'|} \right]$$

(36)

(35)

 $+ \delta_{m,m'} \left(\overrightarrow{\Gamma}_{\infty}^{\prime s} \operatorname{sgn}(z + z' - 2b_{m'+1}) e^{-jk_z|z + z' - 2b_{m'+1}|} \right)$

+ $\stackrel{\leftarrow}{\Gamma_{\infty}}$ sgn $(z+z'-2b_{m'})e^{-jk_z|z+z'-2b_{m'}|}$

$$I_{v}^{s}(z,z') = \begin{cases} \frac{1}{2Z'^{s}} \left(e^{-jk_{z}|z-z'|} - \overrightarrow{\Gamma}_{\infty}^{'s} e^{-jk_{z}|z+z'-2b_{m'+1}|} - \overleftarrow{\Gamma}_{\infty}^{'s} e^{-jk_{z}|z+z'-2b_{m'}|} \right), & m = m', \\ \frac{1}{2Z'^{s}} \left(1 - \overrightarrow{\Gamma}_{\infty}^{'s} \right) e^{-jk_{z}|z-z'|}, & m = m' + 1, \\ \frac{1}{2Z'^{s}} \left(1 - \overleftarrow{\Gamma}_{\infty}^{'s} \right) e^{-jk_{z}|z-z'|}, & m = m' - 1, \end{cases}$$

$$= \frac{1}{2Z'^{s}} \left[\left(\delta_{m,m'} + \delta_{m,m'+1} (1 - \overrightarrow{\Gamma}_{\infty}^{'s}) + \delta_{m,m'-1} (1 - \overleftarrow{\Gamma}_{\infty}^{'s}) \right) e^{-jk_{z}|z-z'|} - \delta_{m,m'} \left(\overrightarrow{\Gamma}_{\infty}^{'s} e^{-jk_{z}|z+z'-2b_{m'+1}|} + \overleftarrow{\Gamma}_{\infty}^{'s} e^{-jk_{z}|z+z'-2b_{m'}|} \right) \right]$$

(37)

$$V_{v}^{s}(z,z') = \begin{cases} \frac{1}{2} \left(\operatorname{sgn}(z-z')e^{-jk_{z}|z-z'|} - \overrightarrow{\Gamma}_{\infty}'^{s} \operatorname{sgn}(z+z'-2b_{m'+1}) e^{-jk_{z}|z+z'-2b_{m'+1}|} \right) \\ - \overrightarrow{\Gamma}_{\infty}'^{s} \operatorname{sgn}(z+z'-2b_{m'})e^{-jk_{z}|z+z'-2b_{m'}|} \right), & m = m', \\ \frac{1}{2} \left(1 + \overrightarrow{\Gamma}_{\infty}'^{s} \right) \operatorname{sgn}(z-z')e^{-jk_{z}|z-z'|}, & m = m' + \frac{1}{2} \left[\left(\delta_{m,m'} + \delta_{m,m'+1}(1 + \overrightarrow{\Gamma}_{\infty}'^{s}) + \delta_{m,m'-1}(1 + \overrightarrow{\Gamma}_{\infty}'^{s}) \right) \operatorname{sgn}(z-z')e^{-jk_{z}|z-z'|} \right] \\ - \delta_{m,m'} \left(\overrightarrow{\Gamma}_{\infty}'^{s} \operatorname{sgn}(z+z'-2b_{m'+1})e^{-jk_{z}|z+z'-2b_{m'+1}|} \right) \end{cases}$$

(38)

where $\delta_{mm'}$ is defined as

$$\delta_{mm'} = \begin{cases} 1, & m = m', \\ 0, & m \neq m', \end{cases}$$

 $+ \stackrel{\leftarrow}{\Gamma_{\infty}^{\prime s}} \operatorname{sgn}(z + z^{\prime} - 2b_{m^{\prime}}) e^{-jk_z|z + z^{\prime} - 2b_{m^{\prime}}|} \Big) \Big]$

and z is in layer m, z' is in layer m'. The spectrally asymptotic values of the layer interface reflection coefficients are given by

$$\vec{\Gamma}_{\infty}^{\prime e} = \frac{\epsilon_{m'} - \epsilon_{m'\pm 1}}{\epsilon_{m'} + \epsilon_{m'\pm 1}}$$

and

$$\Gamma_{\infty}^{'h} = \frac{\mu_{m'\pm 1} - \mu_{m'}}{\mu_{m'+1} + \mu_{m'}}.$$

Using these asymptotic expressions, one determines the following asymptotic forms for the potential quantities:

$$\tilde{\mathcal{G}}_{pq}^{A}(z,z') \sim \tilde{\mathcal{G}}_{pq}^{A0}(z,z') = \begin{bmatrix} \tilde{\mathcal{G}}_{xxpq}^{A0} & 0 & 0 \\ 0 & \tilde{\mathcal{G}}_{yypq}^{A0} & 0 \\ \tilde{\mathcal{G}}_{zxpq}^{A0} & \tilde{\mathcal{G}}_{zypq}^{A0} & \tilde{\mathcal{G}}_{zzpq}^{A0} \end{bmatrix}$$
(39)

where

$$\tilde{\mathcal{G}}_{xxpq}^{A0} = \tilde{\mathcal{G}}_{yypq}^{A0} = \frac{\mu'}{2jk_{zpq}} \left[\left(\delta_{m,m'} + \delta_{m,m'+1} (1 + \overset{\rightarrow}{\Gamma}_{\infty}^{'h}) + \delta_{m,m'-1} (1 + \overset{\leftarrow}{\Gamma}_{\infty}^{'h}) \right) e^{-jk_{zpq}|z-z'|} + \delta_{m,m'} \left(\overset{\rightarrow}{\Gamma}_{\infty}^{'h} e^{-jk_{zpq}|z+z'-2b_{m'+1}|} + \overset{\leftarrow}{\Gamma}_{\infty}^{'h} e^{-jk_{zpq}|z+z'-2b_{m'}|} \right) \right]$$
(40)

$$\tilde{\mathcal{G}}_{zxpq}^{A0} = \frac{\mu k_{xpq}}{jk_{\rho pq}^{2}} \left[\left(\delta_{m,m'+1} (\overrightarrow{\Gamma}_{\infty}^{\prime e} - \overrightarrow{\Gamma}_{\infty}^{\prime h}) + \delta_{m,m'-1} (\overrightarrow{\Gamma}_{\infty}^{\prime e} - \overrightarrow{\Gamma}_{\infty}^{\prime h}) \right) \operatorname{sgn}(z - z') e^{-jk_{zpq}|z - z'|} \\
- \delta_{m,m'} \left((\overrightarrow{\Gamma}_{\infty}^{\prime e} - \overrightarrow{\Gamma}_{\infty}^{\prime h}) \operatorname{sgn}(z + z' - 2b_{m'+1}) e^{-jk_{zpq}|z + z' - 2b_{m'+1}|} \\
+ (\overrightarrow{\Gamma}_{\infty}^{\prime e} - \overrightarrow{\Gamma}_{\infty}^{\prime h}) \operatorname{sgn}(z + z' - 2b_{m}) e^{-jk_{zpq}|z + z' - 2b_{m'}|} \right) \right]$$

(41)

$$\tilde{\mathcal{G}}_{zypq}^{A0} = \frac{\mu k_{ypq}}{jk_{\rho pq}^{2}} \left[\left(\delta_{m,m'+1} (\overrightarrow{\Gamma}_{\infty}^{\prime e} - \overrightarrow{\Gamma}_{\infty}^{\prime h}) + \delta_{m,m'-1} (\overrightarrow{\Gamma}_{\infty}^{\prime e} - \overrightarrow{\Gamma}_{\infty}^{\prime h}) \right) \operatorname{sgn}(z-z') e^{-jk_{zpq}|z-z'|} \right. \\
\left. - \delta_{m,m'} \left((\overrightarrow{\Gamma}_{\infty}^{\prime e} - \overrightarrow{\Gamma}_{\infty}^{\prime h}) \operatorname{sgn}(z+z'-2b_{m'+1}) e^{-jk_{zpq}|z+z'-2b_{m'+1}|} \right. \\
\left. + (\overrightarrow{\Gamma}_{\infty}^{\prime e} - \overrightarrow{\Gamma}_{\infty}^{\prime h}) \operatorname{sgn}(z+z'-2b_{m}) e^{-jk_{zpq}|z+z'-2b_{m'}|} \right) \right]$$

 $\tilde{\mathcal{G}}_{zzpq}^{A0} = \frac{\mu}{2jk_{zpq}} \left[\left(\delta_{m,m'} + \delta_{m,m'+1} (1 - \overrightarrow{\Gamma}_{\infty}^{\prime e}) + \delta_{m,m'-1} (1 - \overrightarrow{\Gamma}_{\infty}^{\prime e}) \right) e^{-jk_{zpq}|z-z'|} - \delta_{m,m'} \left(\overrightarrow{\Gamma}_{\infty}^{\prime e} e^{-jk_{zpq}|z+z'-2b_{m'+1}|} + \overrightarrow{\Gamma}_{\infty}^{\prime e} e^{-jk_{zpq}|z+z'-2b_{m'}|} \right) \right]$

(43)

(42)

$$\begin{split} \tilde{K}_{pq}^{\Phi}(z,z') &\sim & \tilde{K}_{pq}^{\Phi0}(z,z') \\ &= & \frac{1}{2\omega\epsilon'k_{zpq}} \left[\left(\delta_{mm'} + \delta_{m,m'+1} (1 + \stackrel{\rightarrow}{\Gamma}_{\infty}^{\prime e}) + \delta_{m,m'-1} (1 + \stackrel{\leftarrow}{\Gamma}_{\infty}^{\prime e}) \right) \, e^{-jk_{zpq}|z-z'|} \right. \\ &\left. + \delta_{mm'} \left(\stackrel{\rightarrow}{\Gamma}_{\infty}^{\prime e} \, e^{-jk_{zpq}|z+z'-2b_{m'+1}|} + \stackrel{\leftarrow}{\Gamma}_{\infty}^{\prime e} \, e^{-jk_{zpq}|z+z'-2b_{m'}|} \right) \right] \end{split}$$

(44)

$$\tilde{\boldsymbol{\mathcal{G}}}_{pq}^{F}(z,z') \sim \tilde{\boldsymbol{\mathcal{G}}}_{pq}^{F0}(z,z') = \begin{bmatrix} \tilde{\mathcal{G}}_{xxpq}^{F0} & 0 & 0\\ 0 & \tilde{\mathcal{G}}_{yypq}^{F0} & 0\\ \tilde{\mathcal{G}}_{zxpq}^{F0} & \tilde{\mathcal{G}}_{zypq}^{F0} & \tilde{\mathcal{G}}_{zzpq}^{F0} \end{bmatrix}$$

$$(45)$$

where

$$\tilde{\mathcal{G}}_{xxpq}^{F0} = \tilde{\mathcal{G}}_{yypq}^{F0} = \frac{\epsilon'}{2jk_{zpq}} \left[\left(\delta_{m,m'} + \delta_{m,m'+1} (1 - \overset{\rightarrow}{\Gamma}_{\infty}^{'h}) + \delta_{m,m'-1} (1 - \overset{\leftarrow}{\Gamma}_{\infty}^{'h}) \right) e^{-jk_{zpq}|z-z'|} - \delta_{m,m'} \left(\overset{\rightarrow}{\Gamma}_{\infty}^{'h} e^{-jk_{zpq}|z+z'-2b_{m'+1}|} + \overset{\leftarrow}{\Gamma}_{\infty}^{'h} e^{-jk_{zpq}|z+z'-2b_{m'}|} \right) \right]$$
(46)

$$\tilde{\mathcal{G}}_{zxpq}^{F0} = \frac{\epsilon k_{xpq}}{jk_{\rho pq}^{2}} \left[\left(\delta_{m,m'+1} (\overset{\rightarrow}{\Gamma}_{\infty}^{\prime e} - \overset{\rightarrow}{\Gamma}_{\infty}^{\prime h}) + \delta_{m,m'-1} (\overset{\leftarrow}{\Gamma}_{\infty}^{\prime e} - \overset{\leftarrow}{\Gamma}_{\infty}^{\prime h}) \right) \operatorname{sgn}(z-z') e^{-jk_{zpq}|z-z'|} \right. \\
\left. - \delta_{m,m'} \left((\overset{\rightarrow}{\Gamma}_{\infty}^{\prime e} - \overset{\rightarrow}{\Gamma}_{\infty}^{\prime h}) \operatorname{sgn}(z+z'-2b_{m'+1}) e^{-jk_{zpq}|z+z'-2b_{m'+1}|} \right. \\
\left. + (\overset{\leftarrow}{\Gamma}_{\infty}^{\prime e} - \overset{\leftarrow}{\Gamma}_{\infty}^{\prime h}) \operatorname{sgn}(z+z'-2b_{m}) e^{-jk_{zpq}|z+z'-2b_{m'}|} \right) \right] \tag{47}$$

$$\tilde{\mathcal{G}}_{zypq}^{F0} = \frac{\epsilon k_{ypq}}{jk_{\rho pq}^{2}} \left[\left(\delta_{m,m'+1} (\overrightarrow{\Gamma}_{\infty}^{\prime e} - \overrightarrow{\Gamma}_{\infty}^{\prime h}) + \delta_{m,m'-1} (\overrightarrow{\Gamma}_{\infty}^{\prime e} - \overrightarrow{\Gamma}_{\infty}^{\prime h}) \right) \operatorname{sgn}(z - z') e^{-jk_{zpq}|z - z'|} \\
- \delta_{m,m'} \left((\overrightarrow{\Gamma}_{\infty}^{\prime e} - \overrightarrow{\Gamma}_{\infty}^{\prime h}) \operatorname{sgn}(z + z' - 2b_{m'+1}) e^{-jk_{zpq}|z + z' - 2b_{m'+1}|} \\
+ (\overrightarrow{\Gamma}_{\infty}^{\prime e} - \overrightarrow{\Gamma}_{\infty}^{\prime h}) \operatorname{sgn}(z + z' - 2b_{m}) e^{-jk_{zpq}|z + z' - 2b_{m'}|} \right) \right]$$

(48)

$$\tilde{\mathcal{G}}_{zzpq}^{F0} = \frac{\epsilon}{2jk_{zpq}} \left[\left(\delta_{m,m'} + \delta_{m,m'+1} (1 + \overrightarrow{\Gamma}_{\infty}^{\prime e}) + \delta_{m,m'-1} (1 + \overrightarrow{\Gamma}_{\infty}^{\prime e}) \right) e^{-jk_{zpq}|z-z'|} + \delta_{m,m'} \left(\overrightarrow{\Gamma}_{\infty}^{\prime e} e^{-jk_{zpq}|z+z'-2b_{m'+1}|} + \overrightarrow{\Gamma}_{\infty}^{\prime e} e^{-jk_{zpq}|z+z'-2b_{m'}|} \right) \right]$$
(49)

$$\begin{split} \tilde{K}_{pq}^{\Psi}(z,z') &\sim & \tilde{K}_{pq}^{\Psi 0}(z,z') \\ &= & \frac{1}{2\omega\mu'k_{zpq}} \left[\left(\delta_{mm'} + \delta_{m,m'+1} (1 - \overset{\rightharpoonup}{\Gamma}_{\infty}^{\prime e}) + \delta_{m,m'-1} (1 - \overset{\rightharpoonup}{\Gamma}_{\infty}^{\prime e}) \right) \, e^{-jk_{zpq}|z-z'|} \\ &- \delta_{mm'} \left(\overset{\rightharpoonup}{\Gamma}_{\infty}^{\prime e} \, e^{-jk_{zpq}|z+z'-2b_{m'+1}|} + \overset{\rightharpoonup}{\Gamma}_{\infty}^{\prime e} \, e^{-jk_{zpq}|z+z'-2b_{m'}|} \right) \right] \end{split}$$

(50)

Similar asymptotic forms exist and may be obtained for the potentials P_z and Q_z as well as for all the derivatives of the potentials, but this task has not yet been completed. Instead, focus has been on the acceleration of the spatial domain representations which arise from applying the Poisson transformation to these terms. A summary of two-dimensional Fourier transform definitions and properties, as well as a brief derivation of the Poisson transformation for periodic structures on skewed lattices is contained in the appendix J to this report.

F Code Validation

The preceding formulas have been validated by the following tests:

- A Fortan 90 code has been developed which handles the multilayered medium problem, but which does not yet handle periodicity. This code is being modified to handle the periodic problem using the acceleration procedures outlined. Its principal differences are 1) the grating lobe sums are actually integrals over the spectral variables, and 2) the direct and image contributions are not an array of contributions, but single point source contributions. Using this code, the following items have been validated:
 - Electric fields and associated potential representations, all associated transmission line calculations, and incident field expressions for multi-layered media by solving for currents on conductors in multi-layered media using the electric field integral equation (EFIE).
 - Correctness of direct and quasi-static image extraction terms from boundaries both above and below the source point.
 - Correctness of magnetic field and associated potential representations by obtaining electric currents on conductors by duality.
- A separate FORTRAN 77 code exists which implements the formulation presented here for conductors in multi-layered material only. This code does not have the more advanced acceleration procedures begin developed here, nor the ability to handle magnetic currents or fields. Furthermore the associated code is less flexible and maintainable than the Fortran 90 code. Nevertheless, it serves as a benchmark for validating many of the new code's capabilities.

G Acceleration of the Free-space Periodic Green's Function by the Method of Singh

The free-space periodic Green's function has the spatial representation

$$G(\mathbf{r}, \mathbf{r}') = \sum_{m=-\infty}^{\infty} \sum_{n=-\infty}^{\infty} e^{-jmk_{x_0}a} e^{-jnk_{y_0}b} \frac{e^{-jkR_{mn}}}{4\pi R_{mn}},$$
(51)

where

$$R_{mn} = \sqrt{(x - x' - ma)^2 + (y - y' - nb)^2 + (z - z')^2}.$$

The wavenumbers k_{x0} and k_{y0} are given by $k_{x0} = k \cos \phi_0 \sin \theta_0$ and $k_{y0} = k \sin \phi_0 \sin \theta_0$, where (θ_0, ϕ_0) either specify the angles to which the array is scanned or the direction of propagation of a plane wave exciting the array.

An alternative, spectral-domain representation of the periodic free-space Green's function is

$$G(\boldsymbol{r}, \boldsymbol{r}') = \frac{1}{ab} \sum_{m=-\infty}^{\infty} \sum_{n=-\infty}^{\infty} \frac{1}{2jk_{z_{mn}}} e^{-j\boldsymbol{k}_{t_{mn}} \cdot (\boldsymbol{\rho} - \boldsymbol{\rho}')} e^{-jk_{z_{mn}}|z-z'|},$$
(52)

where

$$\boldsymbol{\rho} = x\hat{\boldsymbol{x}} + y\hat{\boldsymbol{y}}, \quad \boldsymbol{\rho}' = x'\hat{\boldsymbol{x}} + y'\hat{\boldsymbol{y}},$$

$$\boldsymbol{k}_{t_{mn}} = \left(k_{x_0} + \frac{2m\pi}{a}\right)\hat{\boldsymbol{x}} + \left(k_{y_0} + \frac{2n\pi}{b}\right)\hat{\boldsymbol{y}} = k_{x_m}\hat{\boldsymbol{x}} + k_{y_n}\hat{\boldsymbol{y}},$$

and the wavenumbers $k_{z_{mn}}$ are given by

$$k_{z_{mn}} = \sqrt{k^2 - k_{x_m}^2 - k_{y_n}^2},$$

where $\operatorname{Re}(k_{z_{mn}}) \geq 0$, $\operatorname{Im}(k_{z_{mn}}) \leq 0$.

In the method of Singh, acceleration of the spectral form is achieved by adding and subtracting the periodic Green's function for a medium with an imaginary wavenumber k = -ju (which will be called the "modified Green's function"). The spectral form of the modified Green's function is subtracted from the spectral form of the free-space Green's function, and then the spatial form of the modified Green's function is added back on. This results in a hybrid spectral/spatial form of the free-space Green's function, given as

$$G(\boldsymbol{r}, \boldsymbol{r}') = \frac{1}{ab} \sum_{m=-\infty}^{\infty} \sum_{n=-\infty}^{\infty} e^{-j\boldsymbol{k}_{t_{mn}} \cdot (\boldsymbol{\rho} - \boldsymbol{\rho}')} \left[\frac{e^{-jk_{z_{mn}}|z-z'|}}{2jk_{z_{mn}}} - \frac{e^{-j\kappa_{mn}|z-z'|}}{2j\kappa_{mn}} \right] + \sum_{m=-\infty}^{\infty} \sum_{n=-\infty}^{\infty} e^{-jmk_{x_0}a} e^{-jnk_{y_0}b} \frac{e^{-uR_{mn}}}{4\pi R_{mn}}$$

$$(53)$$

where $k_{z_{mn}}$ in the medium with the imaginary wavenumber has been denoted as κ_{mn} , given by

$$\kappa_{mn} = \sqrt{-u^2 - k_{x_m}^2 - k_{y_n}^2},\tag{54}$$

where $\text{Re}(\kappa_{mn}) \geq 0$, $\text{Im}(\kappa_{mn}) \leq 0$. The free-space periodic Green's function is now given as the sum of two series, one denoted as a "spectral" series (the first one) and one denoted as a "spatial" series (the second one). (Of course, these series are different than the spectral and spatial series defined previously, which are alternative representations of the total Green's function.) The variable u is called a "smoothing" or "acceleration" parameter. As u is increased the spatial series converges faster, while the spectral series converges slower. Ideally, u should be chosen to obtain an optimum balance for the convergence rates of the two series, to obtain an accurate calculation with the fewest total terms. The optimum value of u will depend on the error criterion specified for convergence - the smaller the error criterion, the smaller the value of u becomes. This is because the spatial series converges exponentially, while the spectral series converges algebraically.

An alternative acceleration method, which is also a hybrid method, is the Ewald method. This method results in two series that each have exponential (gaussian) type of convergence. This method is discussed next.

H Acceleration of the Free-Space Periodic Green's Function by the Ewald Method

We begin with the spatial domain form of the Green's function,

$$G(\boldsymbol{r}, \boldsymbol{r}') = \sum_{m=-\infty}^{\infty} \sum_{n=-\infty}^{\infty} e^{-j\boldsymbol{k}_{t_{00}} \cdot \boldsymbol{\rho}_{mn}} \frac{e^{-jkR_{mn}}}{4\pi R_{mn}}$$
(55)

and make use of the identity

$$\frac{e^{-jkR_{mn}}}{R_{mn}} = \frac{2}{\sqrt{\pi}} \int_0^\infty e^{-R_{mn}^2 s^2 + \frac{k^2}{4s^2}} ds, \tag{56}$$

where s is a complex variable and the path is chosen such that the integrand remains bounded as $s \to 0$,

$$\arg(s) \in \left[\arg(k) + \frac{\pi}{4}, \arg(k) + \frac{3\pi}{4}\right],\tag{57}$$

and decays as $s \to \infty$,

$$\arg(s) \in \left[-\frac{\pi}{4}, \frac{\pi}{4} \right]. \tag{59}$$

Observing that $-\frac{\pi}{4} \leq \arg(k) \leq 0$, it is convenient to restrict s to the intersection of these two regions, i.e. the angular sector

$$\arg(s) \in \left[\arg(k) + \frac{\pi}{4}, \frac{\pi}{4}\right]. \tag{61}$$

Next (56) is substituted into (55), and the parameter E is introduced to split the integral into two terms, as

$$G(\mathbf{r}, \mathbf{r}') = G_1(\mathbf{r}, \mathbf{r}') + G_2(\mathbf{r}, \mathbf{r}')$$
(63)

(64)

where

$$G_1(\mathbf{r}, \mathbf{r}') = \sum_{m=-\infty}^{\infty} \sum_{n=-\infty}^{\infty} e^{-j\mathbf{k}_{t_{00}}} \cdot \mathbf{\rho}_{mn} \frac{2}{\sqrt{\pi}} \int_0^E e^{-R_{mn}^2 s^2 + \frac{k^2}{4s^2}} ds,$$
 (65)

$$G_2(\mathbf{r}, \mathbf{r}') = \sum_{m=-\infty}^{\infty} \sum_{n=-\infty}^{\infty} e^{-j\mathbf{k}_{t_{00}}} \cdot \mathbf{\rho}_{mn} \frac{2}{\sqrt{\pi}} \int_E^{\infty} e^{-R_{mn}^2 s^2 + \frac{k^2}{4s^2}} ds,$$
 (66)

Using the identity

$$\frac{2}{\sqrt{\pi}} \int_{E}^{\infty} e^{-R_{mn}^{2}s^{2} + \frac{k^{2}}{4s^{2}}} ds, = \frac{1}{2R_{mn}} \left[e^{-jkR_{mn}} \operatorname{erfc}\left(R_{mn}E - \frac{jk}{2E}\right) + e^{jkR_{mn}} \operatorname{erfc}\left(R_{mn}E + \frac{jk}{2E}\right) \right],$$
(67)

 $G_2(\mathbf{r},\mathbf{r}')$ can be written as

$$G_{2}(\boldsymbol{r},\boldsymbol{r}') = \sum_{m=-\infty}^{\infty} \sum_{n=-\infty}^{\infty} \frac{e^{-j\boldsymbol{k}_{t_{00}} \cdot \boldsymbol{\rho}_{mn}}}{8\pi R_{mn}} \left[e^{-jkR_{mn}} \operatorname{erfc}\left(R_{mn}E - \frac{jk}{2E}\right) + e^{jkR_{mn}} \operatorname{erfc}\left(R_{mn}E + \frac{jk}{2E}\right) \right],$$

$$(68)$$

Poisson transformation of (55) (c.f. Appendix) now yields

$$G_{1}(\boldsymbol{r},\boldsymbol{r}') = \frac{1}{A} \sum_{m=-\infty}^{\infty} \sum_{n=-\infty}^{\infty} \frac{1}{4jk_{zmn}} e^{-j\boldsymbol{k}_{tmn}\cdot(\boldsymbol{\rho}-\boldsymbol{\rho}')} \times \left[e^{-jk_{zmn}|z-z'|} \operatorname{erfc}\left(\frac{jk_{zmn}}{2E} - |z-z'|E\right) + e^{jk_{zmn}|z-z'|} \operatorname{erfc}\left(\frac{jk_{zmn}}{2E} + |z-z'|E\right) \right].$$

$$(69)$$

Each of the new series $G_1(\mathbf{r}, \mathbf{r}')$ and $G_2(\mathbf{r}, \mathbf{r}')$ generally converge at a much faster rate than the original series $G(\mathbf{r}, \mathbf{r}')$. The series $G_2(\mathbf{r}, \mathbf{r}')$ is a modified spatial series, and is therefore denoted as the "spatial" part of the Ewald representation, while $G_1(\mathbf{r}, \mathbf{r}')$ is denoted as the "spectral" part.

H.1 Choice of the optimum E parameter

The two series G_1 and G_2 both converge exponentially. The parameter E controls the convergence rate. As E becomes larger the the "spatial" series G_2 will converge faster, while the "spectral" series G_1 will converge slower. The optimum parameter is that which makes the two series converge at the same rate, so that equal number of terms are required in the calculation of both series (this assumes that the calculation time for each term in the two series is the same). To prove this assertion, assume that the Ewald parameter has first been chosen so that both series converge at the same rate ($E = E_{opt}$), so that each of the series are summed from -N to +N. The total computation time due to the summation of both series is

$$T_{opt} = CN^2 + CN^2 = 2CN^2 (70)$$

where C is some constant. Now assume that a different Ewald parameter has been chosen, and denote $r = E/E_{opt}$. In order to obtain the same accuracy in each summation, the summation limits must be changed. The limit for the spatial sum is inversely proportional to E, while the limit for the spectral sum is proportional to E. Hence the new computation time is

$$T = CN^2 \left(r^2 + \frac{1}{r^2}\right). \tag{71}$$

The ratio of computation time to that with the optimum Ewald parameter, in order to obtain the same accuracy in the summations, is is

$$T/T_{opt} = r^2 + \frac{1}{r^2}. (72)$$

The minimum value of the above function occurs at r=1. Hence, the selection of the optimum Ewald parameter will yield the least number of total terms in the two series, for a given accuracy criterion.

To derive a simple formula for the optimum Ewald parameter E_{opt} , we enforce the condition that the asymptotic rate of convergence is the same for the series G_1 and G_2 . For simplicity, the optimum Ewald parameter is derived here only for the case z = z'. However, the value of z - z' does not affect the asymptotic rate of convergence of the series.

The two series are written in the form

$$G_1 = \sum_{m = -\infty}^{\infty} A_{mn}^{(1)},\tag{73}$$

$$G_2 = \sum_{m=-\infty}^{\infty} A_{mn}^{(2)}. (74)$$

We then enforce the condition that

$$A_{mn}^{(1)} \sim A_{nm}^{(2)} \tag{75}$$

as $m, n \to \infty$. Note that the m and n indices are switched in the subscripts of the two series in the above equations. This is because the indices m and n are multiplied by the lengths a and b to construct R_{mn} in the spatial sum G_2 , whereas they are divided by these lengths to construct the wavenumber term k_{zmn} in the spectral sum G_1 . The asymptotic form of the summands is calculated by using the asymptotic form of the complimentary error function,

$$\operatorname{erfc}(z) \sim \frac{e^{-z^2}}{\sqrt{\pi}z}.$$
 (76)

Equation (75) then yields

$$\frac{e^{-\left(\frac{\alpha_{mn}}{2E}\right)^2}}{4ab\sqrt{\pi}\left(\frac{\alpha_{mn}}{2E}\right)\alpha_{mn}} = \frac{e^{-R_{nm}^2E^2}}{8\pi\sqrt{\pi}\left(R_{nm}E\right)R_{nm}},\tag{77}$$

where

$$\alpha_{mn} = \sqrt{\left(\frac{2\pi m}{a}\right)^2 + \left(\frac{2\pi n}{b}\right)^2}. (78)$$

The exponentials in this equation will converge at the same rate provided

$$\frac{\alpha_{mn}}{2E} = R_{nm}E. \tag{79}$$

Hence,

$$E = \sqrt{\frac{\alpha_{mn}}{2R_{nm}}}. (80)$$

This yields

$$E = \left[\frac{\left(\frac{m\pi}{a}\right)^2 + \left(\frac{n\pi}{b}\right)^2}{(n\pi)^2 + (mb)^2} \right]^{1/4}.$$
 (81)

Multiplying and dividing by \sqrt{ab} yields the result

$$E = \sqrt{\frac{\pi}{ab}}. ag{82}$$

The above choice of E makes the exponential terms in the two series converge at the same rate. It is not completely clear yet if two series will converge at exactly the same rate however, due to the presence of the other terms in Eq. (77). Using Eq. (80), the ratio R of the LHS to the RHS terms in this equation is

$$R = \frac{\pi E^2 R_{nm}^2}{\alpha_{mn}^2 ab}.$$
(83)

In view of Eqs. (80) and (82), it follows that R=1. Hence, the optimum Ewald parameter is

$$E_{opt} = \sqrt{\frac{\pi}{ab}}. ag{84}$$

I Results Comparing Acceleration Methods

During the first quarter of this contract, the Ewald method has been extensively tested and compared with a previous acceleration scheme, the method of Singh et al. The Ewald method has been tested for a wide variety of lattice parameters, including lattice spacing, interelement phase shift, and location of the observation point. Only a few sample results will be presented here. The conclusion is that the Ewald method is a very robust method, requiring only a few terms in each series to obtain very accurate results. The convergence rate is almost always significantly better than that of the Singh method, at least for the case z = z', which is of most interest since this is when the original series converge the slowest. The results presented here are for a typical case with $a = b = 0.5\lambda_0$, $x = y = 0.25\lambda_0$, and $k_{x0} = k_{y0} = 0$.

Figure 8 shows the convergence rate of the Singh method, using the Singh acceleration parameter u=1.0 (which is a typical value). The spatial and spectral curves denote the alternative spatial and spectral forms of the periodic Green's function, with no acceleration. The hybrid curve is the combined spatial/spectral representation used in the Singh method. The integer N is the summation limit in the double sums. As can be seen, the Singh method provides significantly better convergence than using no acceleration at all. However, Fig. 9, which shows the same result on a different scale, shows that N must typically be 10 or more before a small error is obtained.

Figure 10 shows the percent error in the spatial and spectral parts of the Singh (hybrid) method as a function of N (In the Singh method, the final result is the sum of these two parts - the designation "spatial" and "spectral" therefore has a different meaning in this figure than in the previous figures). In order to obtain very small errors, on the order of 10^{-5} , N needs to be on the order of 30.

Figure 11 shows the same type of error plot as Fig. 10, but with the Ewald method, using the optimum acceleration parameter E_{opt} . The curves labeled "spatial" and "spectral" now denote the series G_2 and G_1 (which are in essence spatial and spectral series modified by the complimentary error function terms). It is quite remarkable that fairly accurate results (less than 0.1% error) are obtained with only N=1. And extremely accurate results (percent error less than 10^{-7}) are obtained using N=2.

Many results similar to Fig. 11 have been generated to examine the convergence rate of the Ewald method as the various parameters of the lattice are changed. In all of the cases where the lattice is square (a = b), the conclusion has been the same as for the sample case shown in Fig. 11. With an oblong lattice $(a \neq b)$, the convergence may be slower. This aspect is still under investigation. Also, when $z \neq z'$, faster convergence may be obtained by using an Ewald parameter that is slightly greater than that given by the E_{opt} formula. This is also under investigation at the present time.

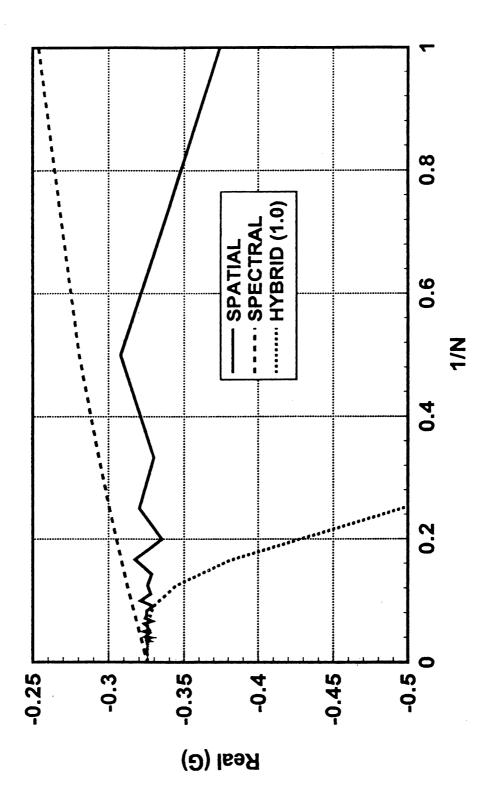


Figure 8: Comparison of convergence rates for the spatial form of the periodic Green's function, the spectral form, and the hybrid form (Singh's method). The convergence is shown for the real part of the Green's function. $a=b=0.5\lambda_0, x=y=0.25\lambda_0, z=z',$ $k_{x0}=k_{y0}=0.$

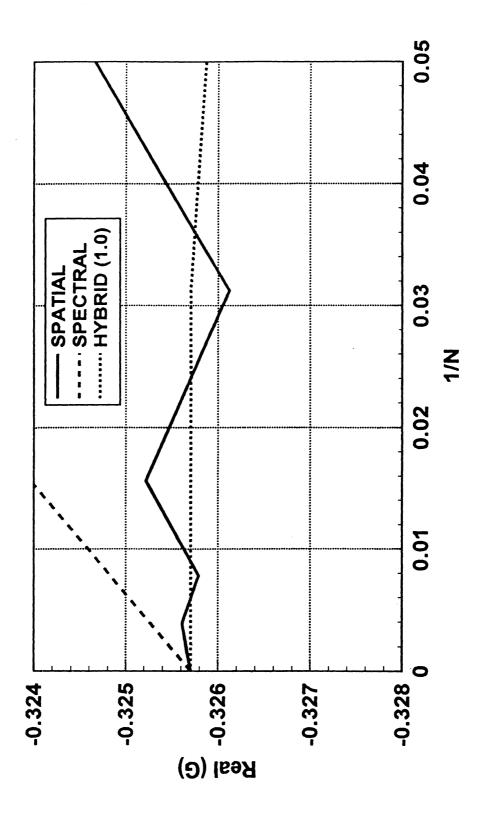


Figure 9: The same comparison of convergence rates shown in Fig. 8, plotted on a different scale.

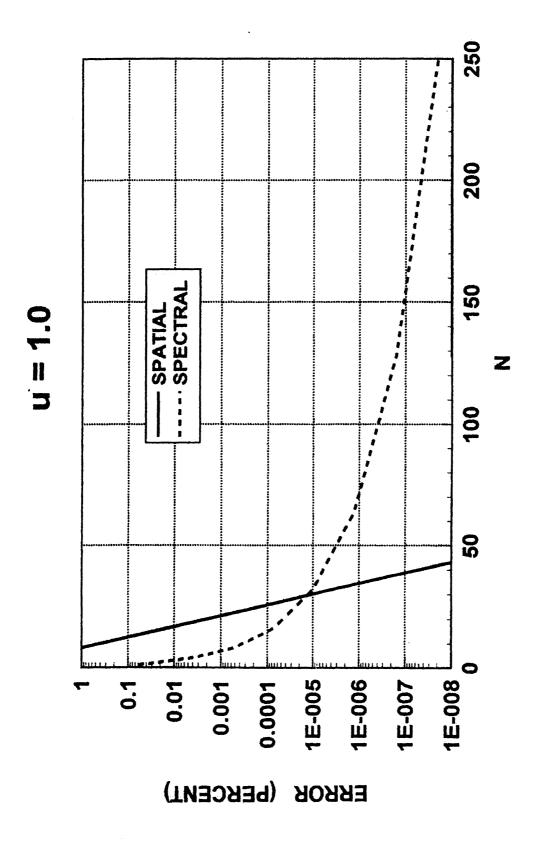
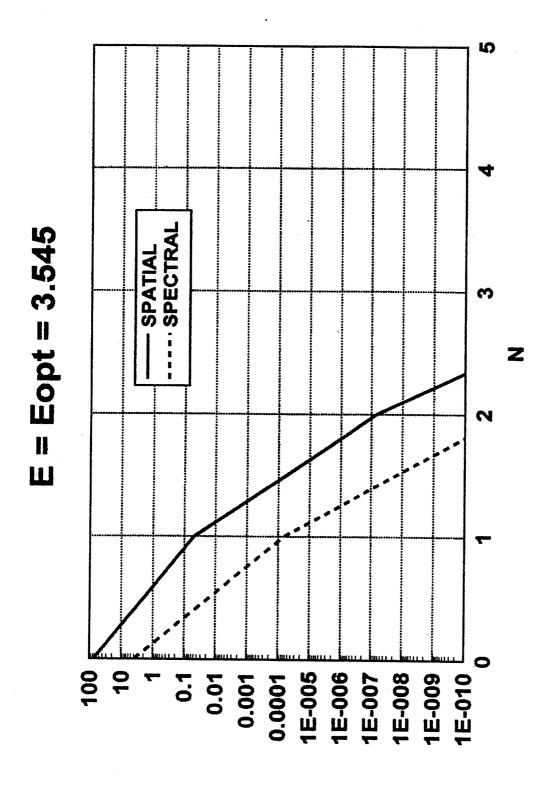


Figure 10: Percent error in the spatial and spectral series that form the hybrid method of Singh, plotted versus the summation limit in the series. The geometry is the same as in Fig. 8. The acceleration parameter u has been chosen as 1.0, which is a typical value.



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Figure 11: Percent error in the spatial and spectral series that form the Ewald method, plotted versus the summation limit in the series. The geometry is the same as in Fig. 8. The Ewald parameter E has been chosen to be the optimum value E_{opt} .

J Two-Dimensional Fourier Transform Properties for Periodic Structure Applications

This appendix collects a number of two-dimensional Fourier transform relations useful in periodic structure analysis. Though most of these relations are well known, they are somewhat scattered throughout the literature and often notationally inconsistent. Furthermore, they are often specialized to rectangular lattices, or have other limitations. For reference, therefore, we collect here the most basic definitions and provide simple proofs for the most useful of these formulas. Use of vector notation throughout not only results in more compact expressions, but also emphasizes the coordinate-free nature of the results.

J.1 The Two-Dimensional Fourier Transform

The two-dimensional Fourier transform of a function $f(\rho) = f(x, y)$ is defined as

$$\tilde{F}(\mathbf{k}) = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} f(\boldsymbol{\rho}) e^{j\mathbf{k}\cdot\boldsymbol{\rho}} dx dy$$
(85)

and the inverse transform as

$$f(\boldsymbol{\rho}) = \frac{1}{(2\pi)^2} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \tilde{F}(\boldsymbol{k}) e^{-j\boldsymbol{k}\cdot\boldsymbol{\rho}} dk_x dk_y.$$
 (86)

We use the notation

$$f(\boldsymbol{\rho}) \iff \tilde{F}(\boldsymbol{k})$$
 (87)

to denote the correspondence between $f(\rho)$ and its transform $\tilde{F}(\mathbf{k})$.

The exponential factor $\mathbf{k} \cdot \boldsymbol{\rho}$ is often written as

$$\mathbf{k} \cdot \boldsymbol{\rho} = k_x x + k_y y \tag{88}$$

and this form is more convenient when one-dimensional transforms, whose familiarity is assumed, are applied in succession to obtain properties of two-dimensional transforms. However, not only is this form less compact, but it is usually less convenient for analyzing skewed

lattices, where lattice points in the spectral and spatial domains (k and ρ domains, respectively) do not necessarily fall on lines of constant coordinates.

Using the Fourier transform definition (85), it is easily proved that

$$\int_{-\infty}^{\infty} \int_{-\infty}^{\infty} f(-\boldsymbol{\rho}) e^{j\boldsymbol{k}\cdot\boldsymbol{\rho}} dx dy = \tilde{F}(-\boldsymbol{k})$$
(89)

and

$$\int_{-\infty}^{\infty} \int_{-\infty}^{\infty} f^*(\boldsymbol{\rho}) \, e^{j\boldsymbol{k}\cdot\boldsymbol{\rho}} \, dx \, dy = \tilde{F}^*(-\boldsymbol{k}), \tag{90}$$

where the asterisk denotes complex conjugate. These results are summarized as

$$f(-\boldsymbol{\rho}) \iff \tilde{F}(-\boldsymbol{k})$$
 (91)

$$f^*(\boldsymbol{\rho}) \iff \tilde{F}^*(-\boldsymbol{k}).$$
 (92)

J.2 Transform of the Two-Dimensional Delta-Function

The two-dimensional delta function may be defined as

$$\delta(\boldsymbol{\rho} - \boldsymbol{\rho}') = \delta(x - x')\delta(y - y'), \tag{93}$$

and hence its Fourier transform is given by

$$\int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \delta(\boldsymbol{\rho} - \boldsymbol{\rho}') e^{j\boldsymbol{k}\cdot\boldsymbol{\rho}} dx dy = e^{j\boldsymbol{k}\cdot\boldsymbol{\rho}'}.$$
 (94)

Fourier inverse transforming yields the useful identity

$$\frac{1}{(2\pi)^2} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} e^{j\mathbf{k}\cdot(\boldsymbol{\rho}'-\boldsymbol{\rho})} dk_x dk_y = \delta(\boldsymbol{\rho}-\boldsymbol{\rho}'). \tag{95}$$

Thus,

$$\delta(\boldsymbol{\rho} - \boldsymbol{\rho}') \iff e^{j\boldsymbol{k}\cdot\boldsymbol{\rho}'}. \tag{96}$$

J.3 The Two-Dimensional Shift and Multiplication Theorems

Consider the Fourier transform of the "shifted" function $f(\rho - \rho')$:

$$\int_{-\infty}^{\infty} \int_{-\infty}^{\infty} f(\boldsymbol{\rho} - \boldsymbol{\rho}') e^{j\boldsymbol{k}\cdot\boldsymbol{\rho}} dx dy = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} f(\boldsymbol{\rho}'') e^{j\boldsymbol{k}\cdot\boldsymbol{\rho}''} e^{j\boldsymbol{k}\cdot\boldsymbol{\rho}'} dx'' dy''$$
$$= e^{j\boldsymbol{k}\cdot\boldsymbol{\rho}'} \tilde{F}(\boldsymbol{k}), \tag{97}$$

where the substitution $\rho'' = \rho - \rho'$ is used.

Thus, the *shift theorem* states that shifting in the spatial domain is equivalent to multiplying by a linearly varying exponential in the spectral domain. When the shift is in the spectral domain, the exponential multiplier appears in the spatial domain, a result which is often called the *multiplication theorem*:

$$\frac{1}{(2\pi)^2} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \tilde{F}(\boldsymbol{k} - \boldsymbol{k}') e^{-j\boldsymbol{k}\cdot\boldsymbol{\rho}} dk_x dk_y = e^{-j\boldsymbol{k}'\cdot\boldsymbol{\rho}} f(\boldsymbol{\rho}).$$
 (98)

These results are summarized as

$$f(\boldsymbol{\rho} - \boldsymbol{\rho}') \iff e^{j\boldsymbol{k}\cdot\boldsymbol{\rho}'}\,\tilde{F}(\boldsymbol{k})$$
 (99)

$$e^{-j\boldsymbol{k}'\cdot\boldsymbol{\rho}}f(\boldsymbol{\rho}) \iff \tilde{F}(\boldsymbol{k}-\boldsymbol{k}').$$
 (100)

J.4 The Two-Dimensional Derivative Theorems

Define

$$\nabla = \hat{\boldsymbol{x}} \frac{\partial}{\partial x} + \hat{\boldsymbol{y}} \frac{\partial}{\partial y}$$
 (101)

and

$$\tilde{\mathbf{\nabla}} = \hat{\mathbf{x}} \frac{\partial}{\partial k_x} + \hat{\mathbf{y}} \frac{\partial}{\partial k_y}. \tag{102}$$

Then

$$\nabla f(\boldsymbol{\rho}) = \frac{1}{(2\pi)^2} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} (-j\boldsymbol{k}) \, \tilde{F}(\boldsymbol{k}) \, e^{-j\boldsymbol{k}\cdot\boldsymbol{\rho}} \, dk_x \, dk_y, \tag{103}$$

so that

$$\nabla f(\rho) \iff (-j\mathbf{k})\,\tilde{F}(\mathbf{k}).$$
 (104)

The rate of change of a function $f(\rho)$ along the direction of the unit vector $\hat{\boldsymbol{\ell}}$, $\frac{df(\boldsymbol{\rho})}{d\ell}$, is given by

$$\frac{df(\boldsymbol{\rho})}{d\ell} = \hat{\boldsymbol{\ell}} \cdot \boldsymbol{\nabla} f(\boldsymbol{\rho}) \tag{105}$$

and hence

$$\frac{df(\boldsymbol{\rho})}{d\ell} = \hat{\boldsymbol{\ell}} \cdot \boldsymbol{\nabla} f(\boldsymbol{\rho}) \iff \left(-j\boldsymbol{k} \cdot \hat{\boldsymbol{\ell}}\right) \tilde{F}(\boldsymbol{k}). \tag{106}$$

Similarly,

$$\rho f(\rho) \iff -j\tilde{\nabla}\tilde{F}(k)$$
 (107)

and

$$\left(\boldsymbol{\rho}\cdot\hat{\boldsymbol{\ell}}\right)f(\boldsymbol{\rho})\iff -j\frac{d\tilde{F}(\boldsymbol{k})}{d\ell}=-j\hat{\boldsymbol{\ell}}\cdot\tilde{\boldsymbol{\nabla}}\tilde{F}(\boldsymbol{k}).$$
 (108)

J.5 Two-Dimensional Convolution Theorems

The two-dimensional convolution between two functions $f(\boldsymbol{\rho})$ and $g(\boldsymbol{\rho})$ is defined as

$$\int_{-\infty}^{\infty} \int_{-\infty}^{\infty} f(\boldsymbol{\rho}') g(\boldsymbol{\rho} - \boldsymbol{\rho}') dx' dy'. \tag{109}$$

With the substitution $\rho'' = \rho - \rho'$ and subsequent replacement of the dummy coordinate ρ'' by ρ' , one finds that

$$\int_{-\infty}^{\infty} \int_{-\infty}^{\infty} f(\boldsymbol{\rho}') g(\boldsymbol{\rho} - \boldsymbol{\rho}') dx' dy' = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} g(\boldsymbol{\rho}') f(\boldsymbol{\rho} - \boldsymbol{\rho}') dx' dy', \qquad (110)$$

or using the symbol '*' to denote convolution.

$$f(\boldsymbol{\rho}) * g(\boldsymbol{\rho}) = g(\boldsymbol{\rho}) * f(\boldsymbol{\rho}). \tag{111}$$

The Fourier transform of the convolution integral is

$$\int_{-\infty}^{\infty} \int_{-\infty}^{\infty} f(\boldsymbol{\rho}) * g(\boldsymbol{\rho}) e^{j\boldsymbol{k}\cdot\boldsymbol{\rho}} dx dy \qquad (112)$$

$$= \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} f(\boldsymbol{\rho}') \left[g(\boldsymbol{\rho} - \boldsymbol{\rho}') e^{j\boldsymbol{k}\cdot\boldsymbol{\rho}} dx dy \right] dx' dy'$$

$$= \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} f(\boldsymbol{\rho}') \tilde{G}(\boldsymbol{k}) e^{j\boldsymbol{k}\cdot\boldsymbol{\rho}'} dx' dy'$$

$$= \tilde{F}(\boldsymbol{k}) \tilde{G}(\boldsymbol{k}), \qquad (113)$$

evaluated with the aid of the shift theorem. Thus we have

$$f(\boldsymbol{\rho}) * g(\boldsymbol{\rho}) \iff \tilde{F}(\boldsymbol{k}) \, \tilde{G}(\boldsymbol{k}).$$
 (114)

In a similar manner, it is shown that

$$\frac{1}{(2\pi)^2} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \tilde{F}(\boldsymbol{k}) * \tilde{G}(\boldsymbol{k}) e^{-j\boldsymbol{k}\cdot\boldsymbol{\rho}} dk_x dk_y = (2\pi)^2 f(\boldsymbol{\rho}) g(\boldsymbol{\rho})$$
 (115)

or, equivalently,

$$f(\boldsymbol{\rho}) g(\boldsymbol{\rho}) \iff \frac{1}{(2\pi)^2} \tilde{F}(\boldsymbol{k}) * \tilde{G}(\boldsymbol{k}).$$
 (116)

A number of alternative forms of the convolution theorem may be obtained by combining (115) or (116) with (89) and (90).

J.6 The Power Theorems

The power density at a point ρ is often proportional to the quantity $f(\rho)g^*(\rho)$, and hence the total power crossing the transform plane is given by

$$\int_{-\infty}^{\infty} \int_{-\infty}^{\infty} f(\boldsymbol{\rho}) g^{*}(\boldsymbol{\rho}) dx dy$$

$$= \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} f(\boldsymbol{\rho}) g^{*}(\boldsymbol{\rho}) e^{j\boldsymbol{k}'\cdot\boldsymbol{\rho}} dx dy \Big|_{\boldsymbol{k}'=0}$$

$$= \frac{1}{(2\pi)^{2}} \tilde{F}(\boldsymbol{k}') * \tilde{G}^{*}(-\boldsymbol{k}') \Big|_{\boldsymbol{k}'=0}$$

$$= \frac{1}{(2\pi)^{2}} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \tilde{F}(\boldsymbol{k}) \tilde{G}^{*}(\boldsymbol{k}) dk_{x} dk_{y},$$

where (115) has been used.

This result,

$$\int_{-\infty}^{\infty} \int_{-\infty}^{\infty} f(\boldsymbol{\rho}) g^*(\boldsymbol{\rho}) dx dy = \frac{1}{(2\pi)^2} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \tilde{F}(\boldsymbol{k}) \tilde{G}^*(\boldsymbol{k}) dk_x dk_y, \qquad (117)$$

is known as the *power theorem*. If both $f(\rho)$ and $g(\rho)$ are real, the conjugation symbol on the left hand side may be removed, resulting in a form often called *Parseval's theorem*:

$$\int_{-\infty}^{\infty} \int_{-\infty}^{\infty} f(\boldsymbol{\rho}) g(\boldsymbol{\rho}) \, dx \, dy = \frac{1}{(2\pi)^2} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \tilde{F}(\boldsymbol{k}) \tilde{G}^*(\boldsymbol{k}) \, dk_x \, dk_y, \quad (f, g \text{ real}).$$
(118)

Combining this with (89) and (90), we have alternatively

$$\int_{-\infty}^{\infty} \int_{-\infty}^{\infty} f(\boldsymbol{\rho}) g(-\boldsymbol{\rho}) \, dx \, dy = \frac{1}{(2\pi)^2} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \tilde{F}(\boldsymbol{k}) \tilde{G}(\boldsymbol{k}) \, dk_x \, dk_y, \quad (f, g \text{ real}).$$
(119)

When $f(\rho) = g(\rho)$, the power theorem becomes Rayleigh's theorem:

$$\int_{-\infty}^{\infty} \int_{-\infty}^{\infty} |f(\boldsymbol{\rho})|^2 \, dx \, dy = \frac{1}{(2\pi)^2} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} |\tilde{F}(\boldsymbol{k})|^2 \, dk_x \, dk_y.$$
 (120)

J.7 The Two-Dimensional Sampling Function

The one-dimensional sampling or replicating function comb(x) is a periodic train of delta functions defined as

$$comb(x) = \sum_{n=-\infty}^{\infty} \delta(x-n)$$
 (121)

and which has the Fourier transform

$$\int_{-\infty}^{\infty} \cosh(x) e^{jkx} dx = \sum_{n=-\infty}^{\infty} e^{jkn} = \lim_{N \to \infty} \sum_{n=-N}^{N} e^{jkn}$$

$$= \lim_{N \to \infty} (2N+1) \frac{\sin(2N+1)\frac{k}{2}}{(2N+1)\sin\frac{k}{2}} = \begin{cases} 0, & k \neq 2m\pi \\ \infty, & k = 2m\pi. \end{cases}$$
(122)

These properties suggest that the transform is also a periodic train of delta functions located at $k = 2m\pi$ for m an integer. To determine the magnitude of each delta function, we calculate the area under each as follows:

$$\int_{(2m-1)\pi}^{(2m+1)\pi} \left(\lim_{N \to \infty} \sum_{n=-N}^{N} e^{jkn} \right) dk = 2\pi,$$
 (123)

where the orthogonal properties of the exponential functions are invoked. Thus, we assert

$$\int_{-\infty}^{\infty} \cosh(x) e^{jkx} dx = 2\pi \sum_{m=-\infty}^{\infty} \delta(k - 2m\pi) = \sum_{m=-\infty}^{\infty} \delta(\frac{k}{2\pi} - m)$$
$$= \operatorname{comb}(\frac{k}{2\pi})$$
(124)

so that the comb function is found to be its own Fourier transform. Comparing (122) and (124), we also establish the important identity

$$comb\left(\frac{k}{2\pi}\right) = \sum_{n=-\infty}^{\infty} e^{jkn}.$$
 (125)

Now consider the two-dimensional version of the sampling or function

$$\sum_{m=-\infty}^{\infty} \sum_{n=-\infty}^{\infty} \delta(\boldsymbol{\rho} - \boldsymbol{\rho}_{mn}), \tag{126}$$

where $\rho_{mn} = m\mathbf{s}_1 + n\mathbf{s}_2$ and $\mathbf{s}_1, \mathbf{s}_2$ are the lattice vectors of a skewed cell of a periodic structure. Eq. (126) represents, for example, an array of point sources corresponding to the scalar Green's function of a periodic structure. The Fourier transform of (126) is

$$\int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \left(\sum_{m=-\infty}^{\infty} \sum_{n=-\infty}^{\infty} \delta(\boldsymbol{\rho} - \boldsymbol{\rho}_{mn}) \right) e^{j\boldsymbol{k}\cdot\boldsymbol{\rho}} dx dy$$

$$= \sum_{m=-\infty}^{\infty} \sum_{n=-\infty}^{\infty} e^{j\boldsymbol{k}\cdot\boldsymbol{\rho}_{mn}}$$

$$= \sum_{m=-\infty}^{\infty} \sum_{n=-\infty}^{\infty} e^{j\boldsymbol{k}\cdot(m\boldsymbol{s}_{1}+n\boldsymbol{s}_{2})}$$

$$= \sum_{m=-\infty}^{\infty} \sum_{n=-\infty}^{\infty} e^{jm\boldsymbol{k}\cdot\boldsymbol{s}_{1}} e^{jn\boldsymbol{k}\cdot\boldsymbol{s}_{2}}$$

$$= \operatorname{comb}\left(\frac{\boldsymbol{k}\cdot\boldsymbol{s}_{1}}{2\pi}\right) \operatorname{comb}\left(\frac{\boldsymbol{k}\cdot\boldsymbol{s}_{1}}{2\pi}\right), \tag{127}$$

where (125) is used. The product of the two comb functions on the left hand side of (127) forms another sampling or replicating function on the so-called reciprocal lattice in the transform domain. The principal planes of the reciprocal lattice are perpendicular to s_1 and s_2 and spaced a distance of $\frac{2\pi}{|s_1|}$ and $\frac{2\pi}{|s_2|}$, respectively. Hence if the spatial domain lattice is skewed, so is the reciprocal lattice. The reciprocal lattice vectors are easily found to be

$$\mathbf{k}_{1} = \frac{2\pi(\mathbf{s}_{2} \times \hat{\mathbf{z}})}{A}$$

$$\mathbf{k}_{2} = \frac{2\pi(\hat{\mathbf{z}} \times \mathbf{s}_{1})}{A},$$
(128)

where $A = |\mathbf{s}_1 \times \mathbf{s}_2|$ is the area of a unit cell in the spatial lattice, and the lattice vectors satisfy the biorthogonality conditions

$$\boldsymbol{k}_i \cdot \boldsymbol{s}_j = 2\pi \delta_{ij}, \tag{129}$$

where δ_{ij} is the Kronecker delta.

Eq. (127) implies that the transform of the two-dimensional sampling function is also a sampling function with two-dimensional delta functions located at the lattice plane intersections where neither comb function in (127) vanishes. However, the amplitude of each of these delta functions depends on the lattice skewness, and it may be determined by integrating over a unit cell in the reciprocal lattice plane. For this purpose, we introduce the normalized unit cell coordinates

$$\xi_1 = \frac{k \cdot \mathbf{s}_1}{2\pi},$$

$$\xi_2 = \frac{k \cdot \mathbf{s}_2}{2\pi}.$$
(130)

Since this transformation of coordinates from (k_x, k_y) to (ξ_1, ξ_2) is linear, the Jacobian of the transformation is constant and is easily found to be $\frac{(2\pi)^2}{A}$ merely by equating areas of the reciprocal lattice unit cell computed both in lattice and normalized coordinates:

$$\int_{\text{unit cell}} dk_x dk_y = (\mathbf{k}_1 \times \mathbf{k}_2) \cdot \hat{\mathbf{z}} = \frac{2\pi(\mathbf{s}_2 \times \hat{\mathbf{z}})}{A} \times \frac{2\pi(\hat{\mathbf{z}} \times \mathbf{s}_1)}{A}$$

$$= \frac{(2\pi)^2}{A^2} (\mathbf{s}_1 \times \mathbf{s}_2) \cdot \hat{\mathbf{z}} = \frac{(2\pi)^2}{A}$$

$$= \frac{(2\pi)^2}{A} \int_0^1 \int_0^1 d\xi_1 d\xi_2. \tag{131}$$

Thus since

$$\int_{\text{cell}} \text{comb}\left(\frac{\boldsymbol{k} \cdot \boldsymbol{s}_1}{2\pi}\right) \text{comb}\left(\frac{\boldsymbol{k} \cdot \boldsymbol{s}_1}{2\pi}\right) dk_x dk_y \tag{132}$$

$$= \frac{(2\pi)^2}{A} \int_0^1 \int_0^1 \text{comb}(\xi_1) \text{comb}(\xi_2) d\xi_1 d\xi_2 = \frac{(2\pi)^2}{A}, \tag{133}$$

each two-dimensional delta function of (127) has amplitude $\frac{(2\pi)^2}{A}$ and therefore the sampling function and its transform are related as

$$\sum_{m=-\infty}^{\infty} \sum_{n=-\infty}^{\infty} \delta(\boldsymbol{\rho} - \boldsymbol{\rho}_{mn}) \iff \frac{(2\pi)^2}{A} \sum_{p=-\infty}^{\infty} \sum_{q=-\infty}^{\infty} \delta(\boldsymbol{k} - \boldsymbol{k}_{pq}), \tag{134}$$

where $\mathbf{k}_{pq} = p\mathbf{k}_1 + q\mathbf{k}_2$.

A similar relationship useful in periodic structure analysis is obtained using (134) with the shift theorem:

$$\sum_{m=-\infty}^{\infty} \sum_{n=-\infty}^{\infty} \delta(\boldsymbol{\rho} - \boldsymbol{\rho}_{mn}) e^{-j\boldsymbol{k}_{00} \cdot \boldsymbol{\rho}_{mn}} \iff \frac{(2\pi)^2}{A} \sum_{p=-\infty}^{\infty} \sum_{q=-\infty}^{\infty} \delta(\boldsymbol{k} - \boldsymbol{k}_{pq}), \tag{135}$$

where now $\mathbf{k}_{pq} = \mathbf{k}_{00} + p\mathbf{k}_1 + q\mathbf{k}_2$.

J.8 The Poisson Transformation

Choosing $g(\rho)$ to be the two-dimensional sampling function with linear progressive phase shift, (135), in the power theorem yields the so-called *Poisson transformation*:

$$\int_{-\infty}^{\infty} f(\boldsymbol{\rho}) \left(\sum_{m=-\infty}^{\infty} \sum_{n=-\infty}^{\infty} \delta(\boldsymbol{\rho} - \boldsymbol{\rho}_{mn}) e^{-j\boldsymbol{k}_{00} \cdot \boldsymbol{\rho}_{mn}} \right)^{*} dx dy$$

$$= \sum_{m=-\infty}^{\infty} \sum_{n=-\infty}^{\infty} f(\boldsymbol{\rho}_{mn}) e^{j\boldsymbol{k}_{00} \cdot \boldsymbol{\rho}_{mn}}$$

$$= \frac{1}{(2\pi)^{2}} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \tilde{F}(\boldsymbol{k}) \left(\frac{(2\pi)^{2}}{A} \sum_{p=-\infty}^{\infty} \sum_{q=-\infty}^{\infty} \delta(\boldsymbol{k} - \boldsymbol{k}_{pq}) \right) dk_{x} dk_{y}$$

$$= \frac{1}{A} \sum_{m=-\infty}^{\infty} \sum_{q=-\infty}^{\infty} \tilde{F}(\boldsymbol{k}_{pq}).$$
(136)

The resulting transformation,

$$\sum_{m=-\infty}^{\infty} \sum_{n=-\infty}^{\infty} f(\boldsymbol{\rho}_{mn}) e^{j\boldsymbol{k}_{00} \cdot \boldsymbol{\rho}_{mn}} = \frac{1}{A} \sum_{p=-\infty}^{\infty} \sum_{q=-\infty}^{\infty} \tilde{F}(\boldsymbol{k}_{pq}).$$
 (138)

converts a spatial summation into a spectral sum, often with improved convergence properties.