

**DESIGN AND IMPLEMENTATION OF A C-BAND
SINGLE ANTENNA POLARIMETRIC ACTIVE
RADAR CALIBRATOR**

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ABSTRACT

This report serves as a documentation of the design parameters and performance characteristics of a C-band single antenna polarimetric active radar calibrator (SAPARC) developed for JPL and NASA at the University of Michigan's Radiation Laboratory. The device is one of four which are currently being constructed for future JPL/NASA Synthetic Aperture Radar (SAR) missions. The report includes details of the SAPARC's RF and digital / analog electronics design, as well as test results from a number of anechoic chamber measurements. Application notes and suggestions are also included throughout.

CHAPTER I

INTRODUCTION

Active and passive radar calibrators are often used in conjunction with airborne and space borne polarimetric imaging SAR platforms. When strategically placed, these devices serve as ground-based calibration targets with specified radar cross sections (RCS). Trihedrals / corner reflectors are by far the most common type of calibration device used; however, their physical size and weight make them undesirable for field deployment. The drawbacks associated with trihedrals are two-fold. First, an actual deployment of the device can be physically awkward and inconvenient. Trihedrals can be as large as 12 ft by 12 ft by 12 ft, and they can weigh up to 300 pounds. In addition to their cumbersome size and weight, trihedrals tend to act like large rain and snow collectors, thus complicating the chances of performing an accurate calibration.

The second drawback is a bit more subtle, but just as significant. The accuracy of an external calibration of a radar system directly relies on the knowledge of the scattering matrix of the calibration target. Although it is possible to estimate the elements of the scattering matrix of a calibration target analytically, manufacturing tolerances may leave a fair amount of uncertainty in the estimated values. Therefore, it is necessary to measure the calibration targets against a precise calibration target, such as a metallic sphere. This reveals the second drawback of passive calibrators with large physical dimensions, namely that the far field condition and uniform illumination criteria are difficult to meet in the laboratory. Hence, it becomes difficult to accurately define the performance characteristics of passive calibrators of this size and type.

Polarimetric active radar calibrators (PARCs), on the other hand, tend to be much smaller and easier to handle than their passive counterparts. A PARC also yields better calibration measurements since its SAR image can be translated over a dark background, thus providing a higher signal to background ratio. As a result of these advantages,

PARCs are rapidly becoming the calibration device of choice for future space borne missions.

As a final point, PARCs traditionally are designed with two antennas which can cause severe degradation in their performance, as will be explained later. Here a new design for the C-band PARC is used which requires a single antenna.

The purpose of this report is to outline of the theory, design, and implementation of the C-band single antenna PARCs developed for NASA and JPL at the University of Michigan. The content of this project reflects the modifications and improvements made to previous PARC and SAPARC units (specifically, an L-band SAPARC prototype built by Sarabandi and Oh for the University of Michigan's Radiation Laboratory [1]). Currently, the C-Band SAPARCs are tentatively planned for field deployment in October 1993, where they will be used as calibration devices for NASA's SIR-C (Shuttle Imaging Radar -C) mission.

CHAPTER II

PARC THEORY / DESIGN CRITERIA

In its simplest form, a PARC consists of a receive antenna, an amplifier, and a transmit antenna (see Figure 2.1). With this configuration, the PARC merely acts like a repeater, whereby an incoming radar signal is received, amplified, and re-transmitted back to the SAR platform. Variations on this simple design do, however, lead to a variety of merits.

Figure 2.2 depicts the modifications which are employed in this project's SAPARC units. The most notable difference is the addition of a delay line along with an orthogonal mode transducer (OMT) / single antenna implementation. The device now serves as a specialized type of repeater, where the signal is captured with respect to one polarization and re-transmitted via its opposite polarization. The pre-amplifier and power amplifier ensure the proper amplification of the signal, while the delay line electrically delays the signal for reasons which will be given later. As a final note, the switches provide the attenuation needed for applicability to SIR-C as well as JPL AIRSAR missions.

2.1 PARC Radar Cross Section

The fundamental equation defining the radar cross section (RCS) of a PARC is given by

$$\sigma = G_{Loop} \frac{G_T G_R \lambda^2}{4\pi} \quad [2]$$

where G_T and G_R are the transmit and receive antenna gains, and G_{Loop} is the net loop gain associated with the gains and losses from the system's amplifiers, switches, and delay line. Generally speaking, a larger RCS is more desirable. Hence, the driving

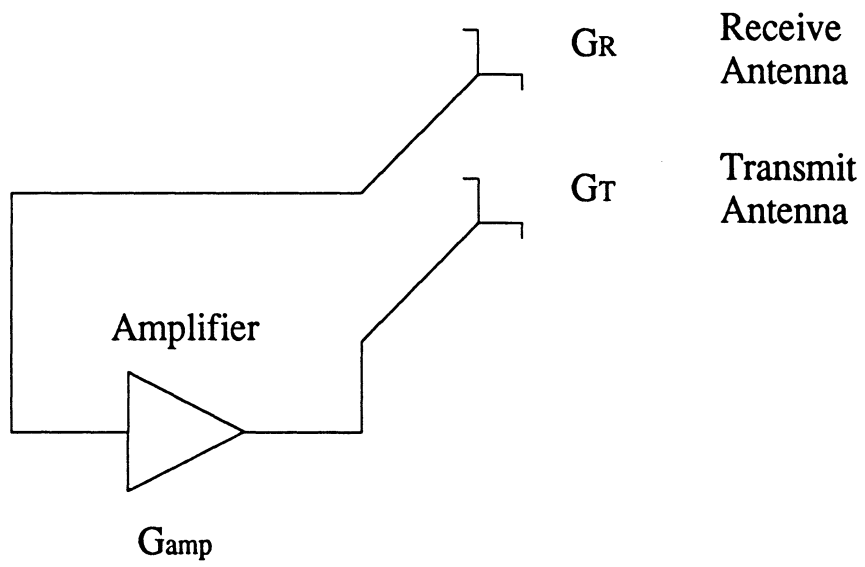


Figure 2.1: Basic PARC Configuration

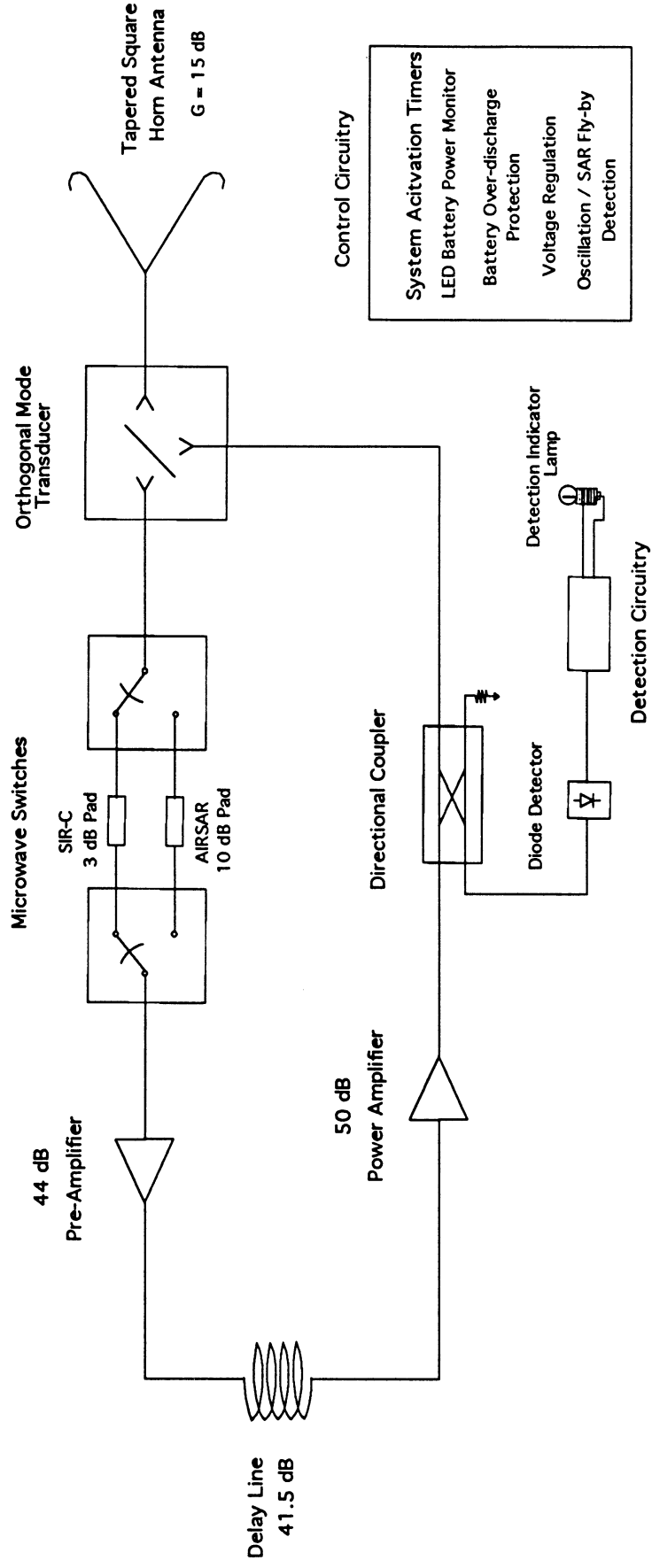


Figure 2.2: C-Band SAPARC Block Diagram

impetus behind most PARC designs is the maximization of G_{Loop} , G_T , and G_R . These parameters, in turn, are limited by beamwidth requirements, transducer isolation performance, and physical size and weight considerations. The following sections address each of these parameters in more detail.

2.2 Antenna Design

In the design of early PARC systems, two antennas, one for transmit and one for receive, were employed to achieve the necessary isolation between the receiver and transmitter modes of the PARC. The transmit and receive antennas were placed in close proximity to one another to meet the compactness requirement of the PARC design. However, since the antennas are in the near field of each other, the RCS pattern of the PARC becomes asymmetric and causes ripples in the phase and amplitude responses which tend to mar the PARC's performance [1] (see Figure 2.3). In order to counter these setbacks and yet to meet the compactness requirement, a single antenna PARC was considered. In this design, the PARC employs a dual polarized horn antenna with a very good polarization isolation and low return loss for both polarization channels. Wide bandwidth and beamwidth with high cross polarization isolation can be achieved through the implementation of an OMT (Orthogonal Mode Transducer) in conjunction with a piecewise tapered square horn.

The geometry of a piecewise tapered horn is shown in Figures 2.4a, 2.4b, and 2.4c. The waveguide discontinuity at a flared intersection excites higher order waveguide modes which are proportional to the flare angle. Since the waveguide is square, the higher order modes can couple energy into the orthogonal channel (TE_{10} to TE_{01} , for example). It was noticed that when the flare angle is less than 5° , the energy transfer from between the orthogonal channels is minimized. However, in order to get the desired aperture over a reasonable length, the square horn can be flared (with angles less than 5°) at many points along its length, thereby simulating an exponential taper. Note that the length of each section should be longer than the wavelength.

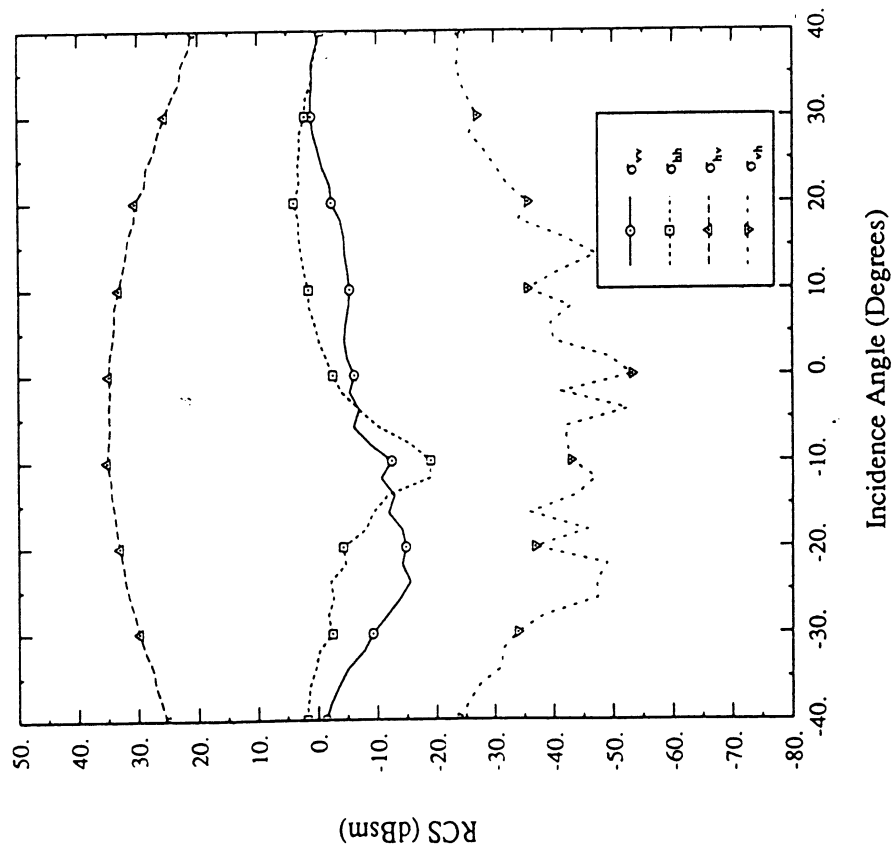
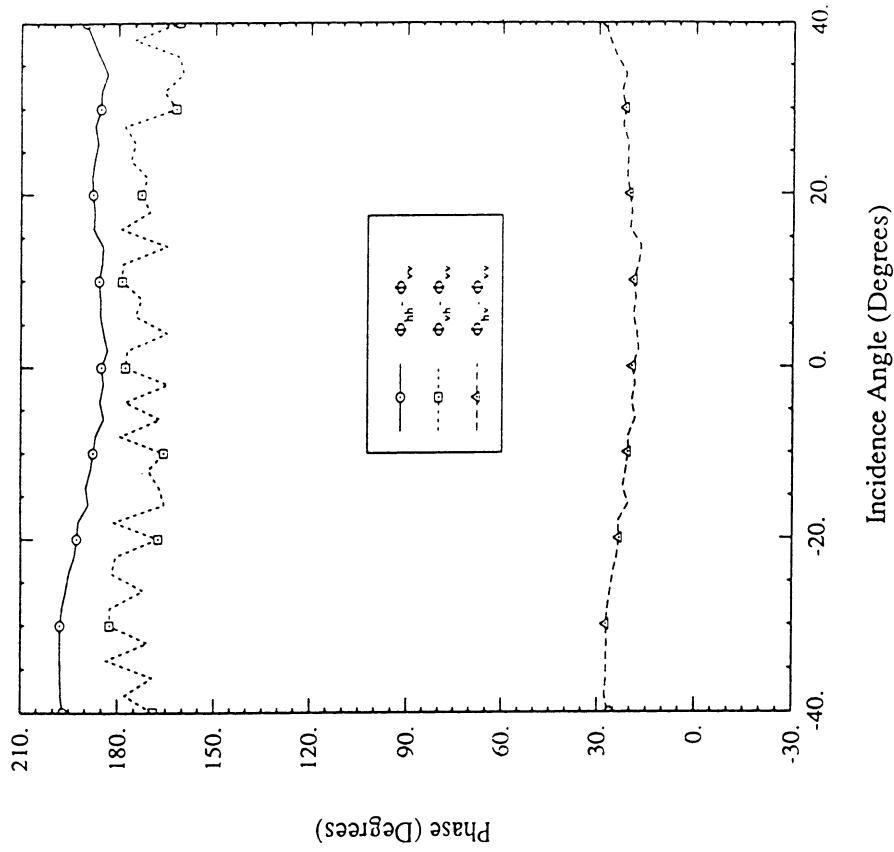
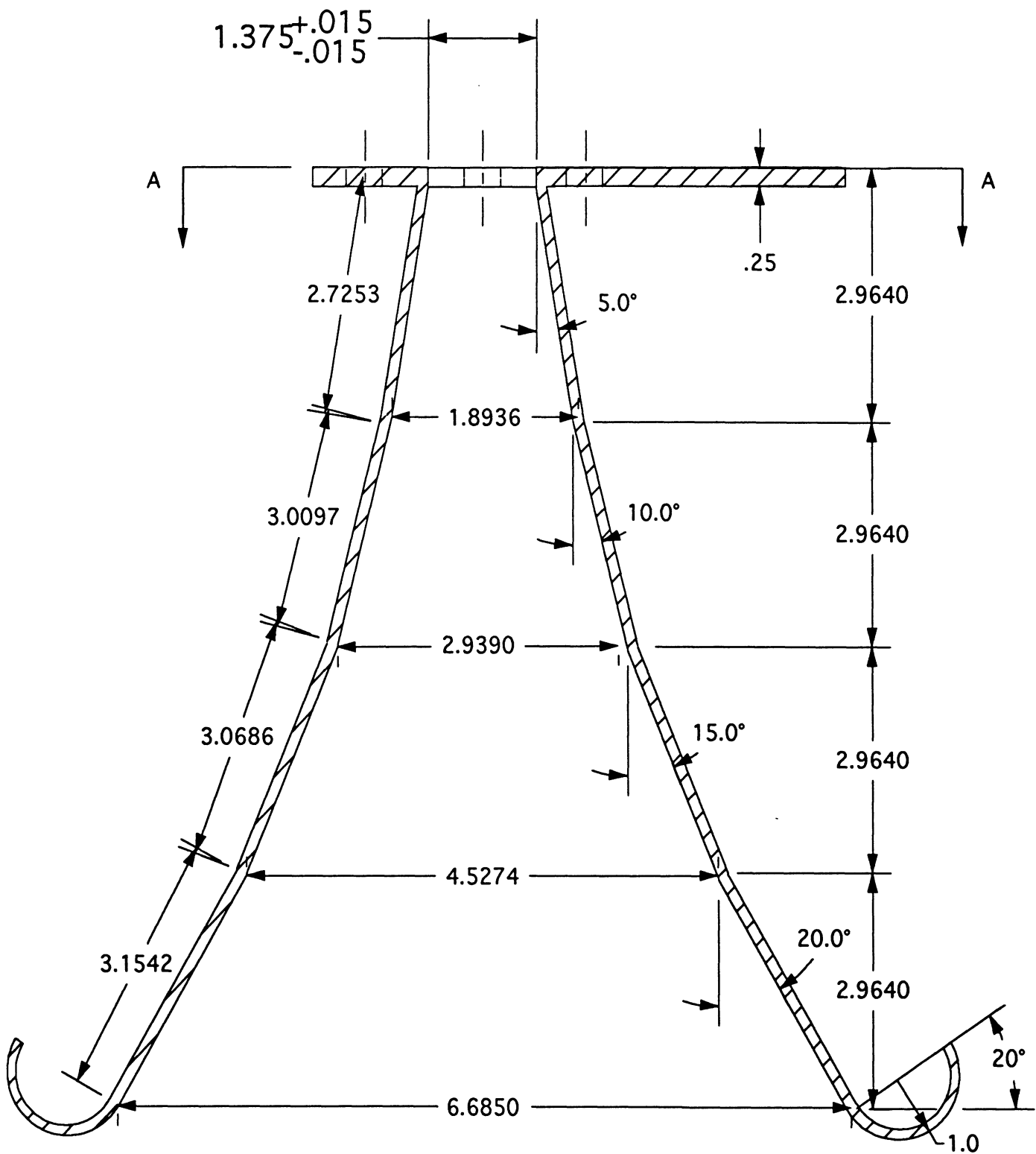


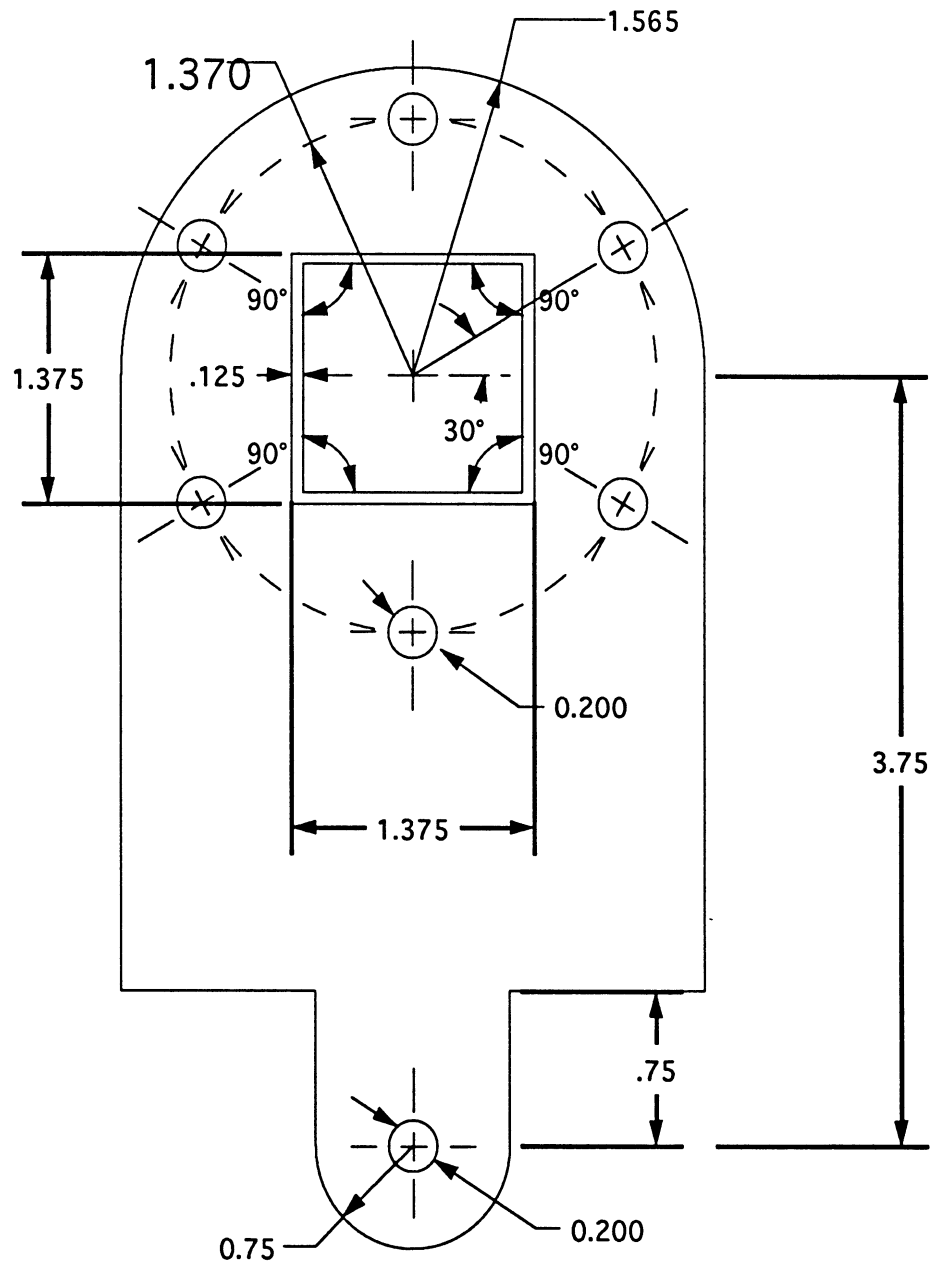
Figure 2.3: Magnitude and Phase Patterns for a Two Antenna PARC System



- All tolerances ± 0.03 inches (unless noted otherwise)
- All angle tolerances ± 1.0 degrees
- All dimensions are in inches and all values pertain to inner dimensions as shown

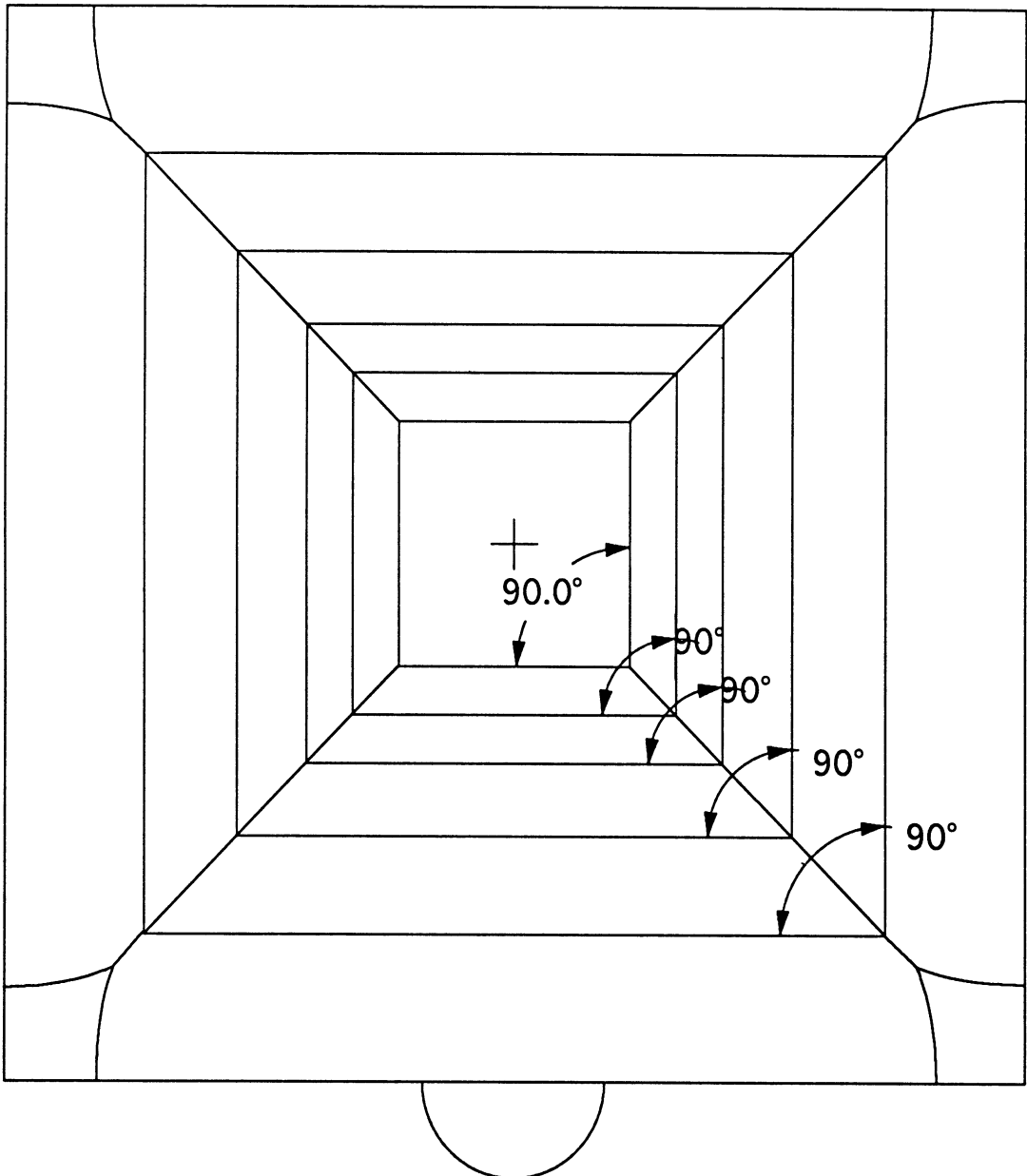
Figure 2.4a: Side View of the C-Band Tapered Square Horn Antenna

View A-A



- All dimensions are in inches
- All tolerances ± 0.03 inches
- All angle tolerances ± 0.5 degrees

Figure 2.4b: Adapter Flange for the C-Band Tapered Square Horn Antenna



- All angle dimensions ± 0.5 degrees
- All pertinent dimensions given for side view

Figure 2.4c: Frontal View of the C-Band Tapered Square Horn Antenna

2.2.1 C-Band Antenna Specifications

The goal of the SAPARC's antenna design is to reduce the RF mismatch and cross-talk (i.e. cross polarization generation) while at the same time providing adequate gain, beamwidth, and bandwidth. For the C-band SAPARC, the primary concern of the design was the trade-off between the reciprocal parameters of antenna gain and beamwidth. Physical size and weight were not major factors due to the relatively small wavelength of the C-band system.

From a practical point of view, the scattering matrix of the SAPARC must be rather insensitive to orientation angles, i.e. a SAPARC should be immune to possible pointing errors). Thus, one of the design goals is to achieve a two-way antenna beamwidth of around 20° . Note that the relatively large beamwidth ensures a successful calibration even if the SAPARC is not directly within the line of sight of the SAR platform. Figure 2.5 demonstrates pictorially the importance of having a wide antenna beamwidth.

A secondary goal was to reduce the sidelobes radiating from the aperture, thereby minimizing the effect of multipath reflections to and from the SAPARC's ground-based position. Multipath contributions yield inaccurate RCS responses since unwanted electromagnetic energy is effectively being collected by the SAPARC antenna system (see Figure 2.6). The nominal RCS response, however, is measured within an anechoic chamber where multipath contributions are negligible. Hence, measurements taken within anechoic chamber and field environments may differ considerably. Using an antenna with small sidelobes is advantageous in that multipath contributions will be reduced; thus, measurements taken during actual field deployment conditions will more closely resemble measurements taken within the chamber environment.

One of the project's early prototypes incorporated the use of a corrugated horn with a square aperture. Note that corrugated horns generally offer improved performance since they reduce the sidelobes in the antenna pattern. Unfortunately, this prototype yielded a high degree of co-polarized mismatch and extremely poor cross polarization isolation. The concept of employing a dielectric lense was also tried; however, the costs of

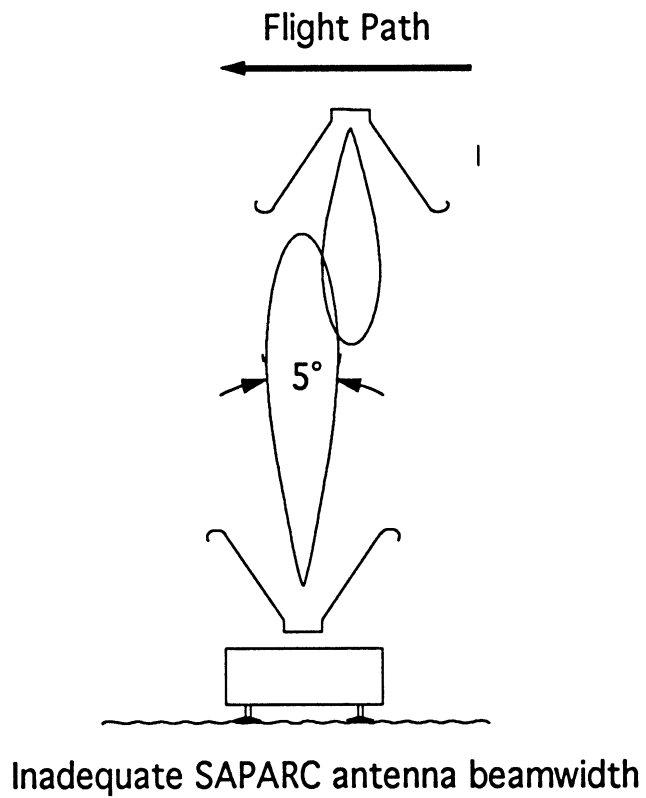
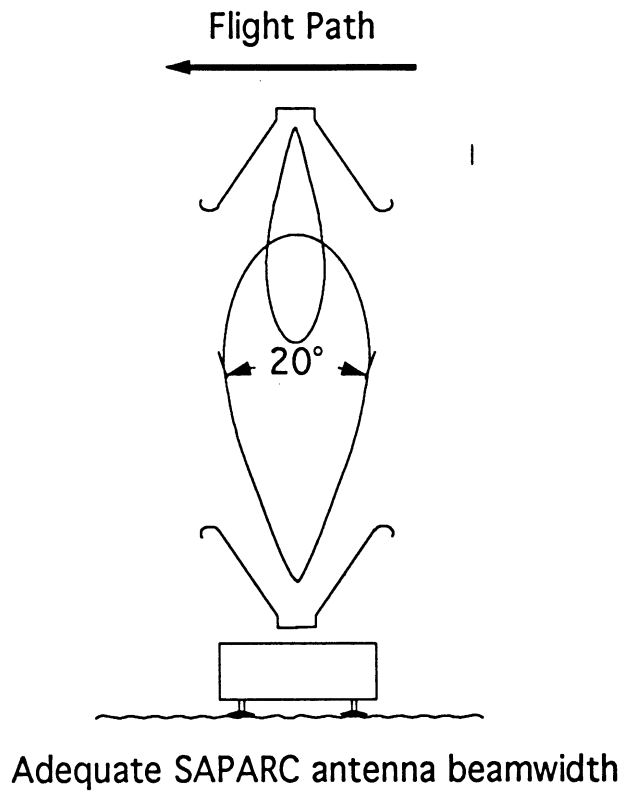


Figure 2.5: Depiction of Adequate and Inadequate Beamwidths for the Tapered Square Horn

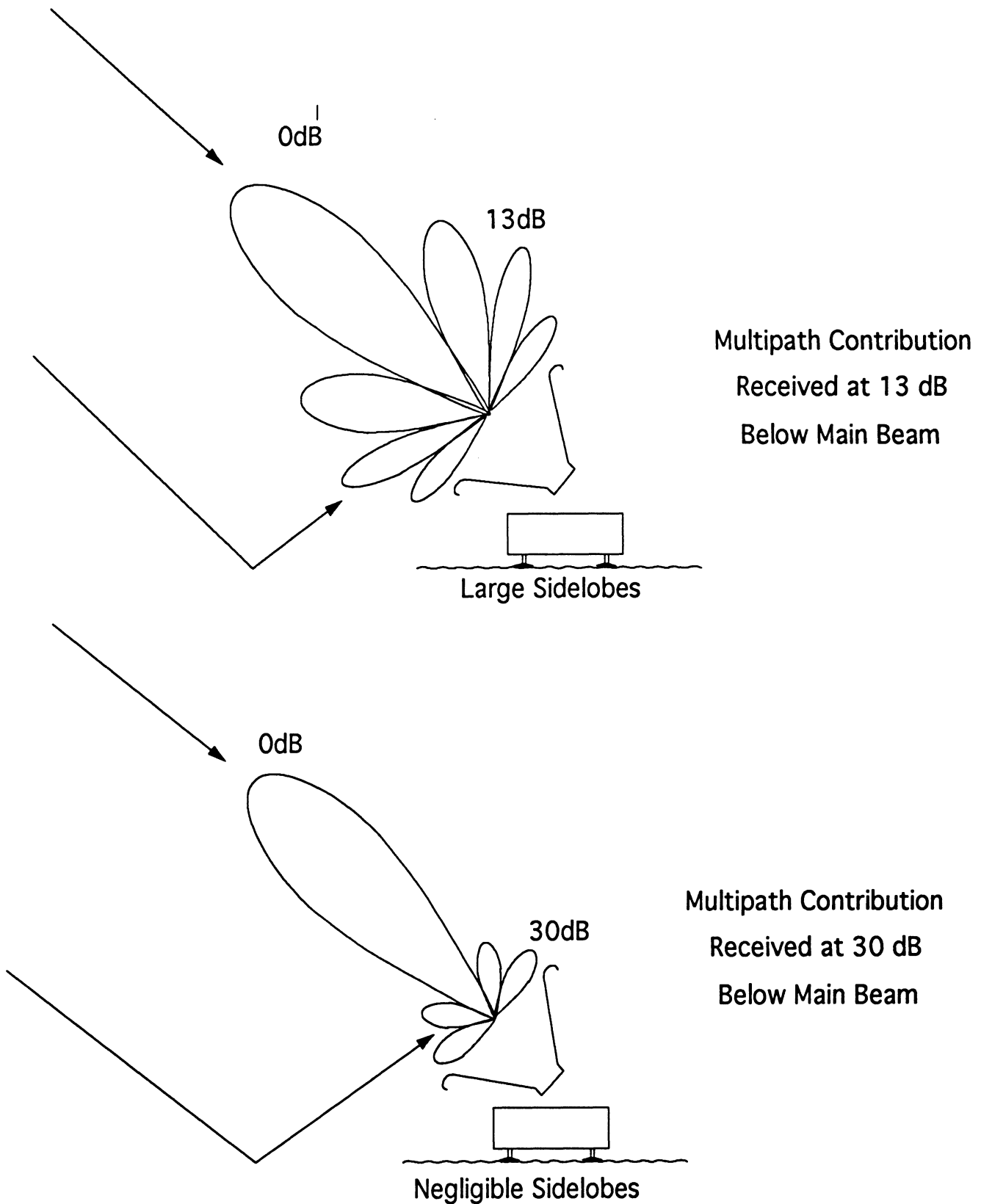


Figure 2.6: Multipath Contribution Scenarios for Horn Antennas With and Without Significant Sidelobes

constructing adequate lenses or custom made corrugated horns became much too prohibitive. Therefore, it was decided that the most economically feasible design would forego the multipath considerations.

Due to the high costs involved, first a prototype horn (made from copper plated printed circuit board material) was constructed and found to yield a one way 3 dB antenna pattern beamwidth of 26° . The physical dimensions of the prototype horn was chosen to be 28 cm in length with a square aperture of 17.6 cm by 17.6 cm (3.11λ by 3.11λ). Based on these promising results, a final design was implemented using four equi-length sections flared in 5° steps. As shown in Figure 2.4, the overall length of the horn is 30.11 cm with an aperture of 16.98 cm by 16.98 cm (3λ by 3λ). This final design also incorporated rounded aperture edges which, in theory, reduce the diffraction effects inherent with the abrupt edges of a typical horn [3]. For the center frequency of 5.3 GHz, the radius of curvature for the rounded edge was chosen to be 2.83 cm, which corresponds to a $\lambda / 2$ radius of curvature.

As a final point, the C-band SAPARC's design employs an OMT purchased from Atlantic Microwave (model # OM1370). This device provides cross polarization isolation of better than 50 dB with a VSWR smaller than 1.5 over the frequency range of 5.2 - 5.9 GHz. A VSWR of 1.07 to 1.08 is the typical value for this OMT. See Appendix A for the detailed OMT test specifications. Figure 2.7 depicts the completed horn and OMT combination.

2.2.2 C-Band Antenna Performance

The results from the final design varied from fair to excellent. The largest disappointment came in the form of the narrow 3 dB beamwidths demonstrated in Figures 3.24 and 3.26 (0° and 45° Orientations). As shown in these pattern measurements, the antenna provides two way beamwidths of 15° for both orientations. Although these beamwidths are relatively narrow, the overall capabilities of the SAPARC will not be degraded.

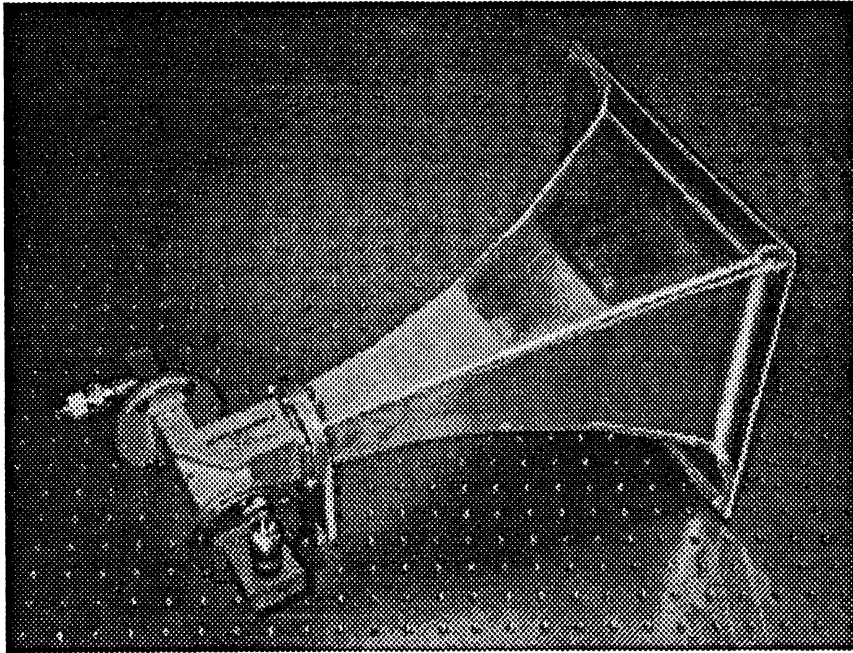


Figure 2.7: C-Band SAPARC Antenna System

The horn design does, however, provide exceptional cross polarization isolation between the receive and transmit ports. Appendix D outlines the steps taken in measuring the horn's cross polarization performance. These measurements were conducted within the UM Radiation Laboratory's anechoic chamber, as shown in Figure D.1. Figures D.2 a - h reflect the time and frequency domain responses taken with a Hewlett Packard 8510 network analyzer. Note that the frequency domain plots incorporated time gating and background subtraction over a frequency range of 5.0 - 5.6 GHz.

From the plots given in Figure D.2, we can deduce that the antenna system (horn and OMT combination) yields a cross polarization isolation exceeding 42 dB. This quality of the horn is instrumental in providing the SAPARC's 38 dB of overall cross polarization isolation (Figure 3.24) and relatively high G_{Loop} gain. Note the 4 dB discrepancy between the system's RCS cross polarization isolation and the isolation resulting from the antenna system alone (measured independently). One possible explanation is that the system's RCS cross polarization isolation was measured in conjunction with another horn and OMT combination (i.e. the radar's antenna system) which similarly possesses a finite isolation capability. The antenna system isolation measurements, on the other hand, used a metal sphere which theoretically acts like a perfectly pure reflective polarizer, i.e. the sphere cannot de-polarize incident electromagnetic waves (as can an imperfect horn antenna). Therefore, it is reasonable to expect that the 4 dB discrepancy is due, at least in part, to the imperfections of the radar's antenna system. Other sources of calibration error may contribute to the discrepancy as well.

Finally, it should be noted that the maximization of G_{Loop} is dependent upon the level of isolation between the receive and transmit ports on the antenna. Refer to Figure 2.1. From this simple diagram, one can see how a feedback scenario results whenever a small fraction of energy is coupled from the transmit antenna to the receive antenna. The coupled electromagnetic wave is then repeatedly amplified as the energy continues along the feedback loop. Eventually, the coupled energy will increase to a magnitude which saturates the amplifiers. For obvious reasons, this situation cannot be tolerated for a PARC design. Therefore, the antenna system's cross polarization isolation must be large enough to prevent the occurrence of a feedback loop.

2.2.3 Summary of Horn Performance

<u>Physical Characteristics</u>	<u>Electrical Characteristics</u>
Aperture Size: 16.98cm X 16.98cm	Gain: 15.93 dB
Length: 30.11 cm	2-Way 3 dB
Weight: 3.5 lbs.	Beamwidth: 15°
Material: Aluminum	Cross Polarization
Manufacturer: Midwest Enterprises	Isolation: 42 dB

Table 2.1: C-Band Antenna System Characteristics

2.3 G_{Loop} Design

2.3.1 Delay Line

At the heart of any PARC system is the G_{Loop} component of the RCS. As mentioned above, a PARC can enhance a calibration measurement by translating its SAR response over a dark background (i.e. a background with a specular surface, such as an airport runway or a large body of water -- See Figure 2.8). This technique is easily implemented by adding a low loss delay line between the receiver and transmitter, as shown in Figure 2.2.

When calculating the length of the delay line, a number of system parameters had to be incorporated in order to insure an adequate SAR delay. The slant range resolution, r_y , is given as 6.67 m for JPL's AIRSAR. As shown in Figure 2.8, the SAPARC should "appear" as if it is situated directly over a body of water. The quantity Δp corresponds to the distance between the physical location of the PARC and its desired SAR image position. An acceptable Δp is approximately 10 pixels (i.e. 10 range bins); therefore,

$$\Delta p = 10r_y = 66.7m$$

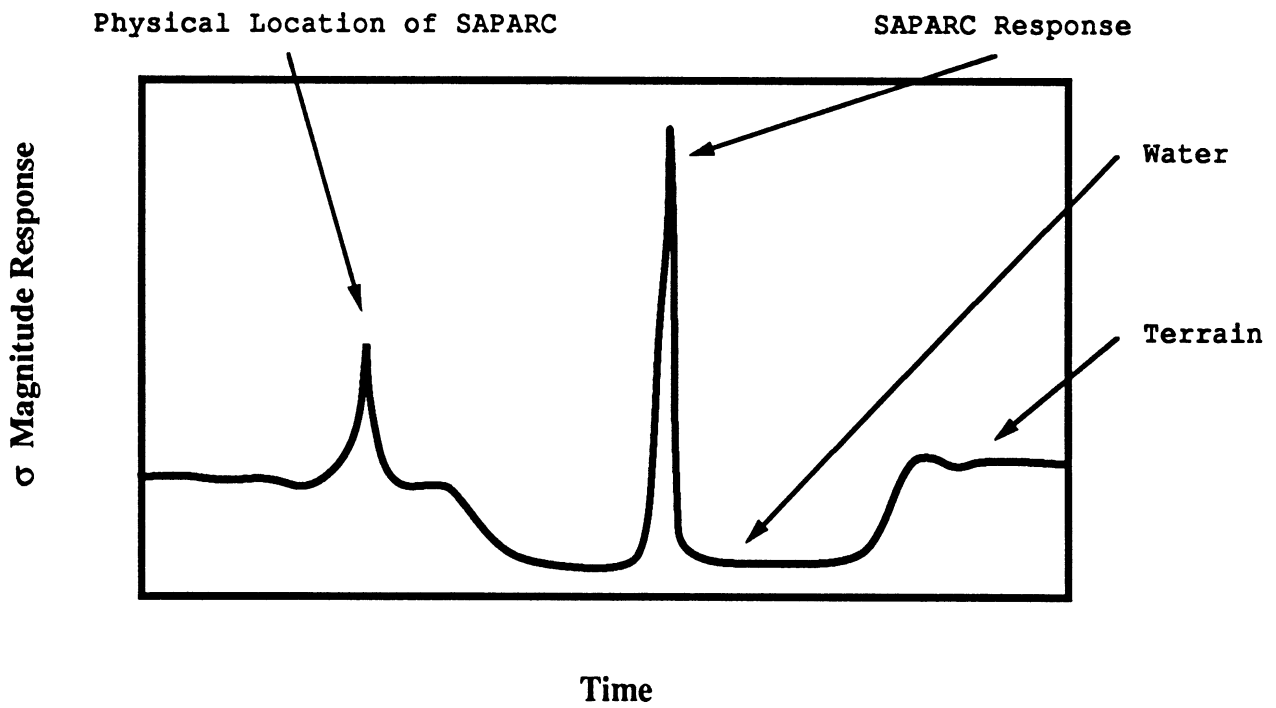
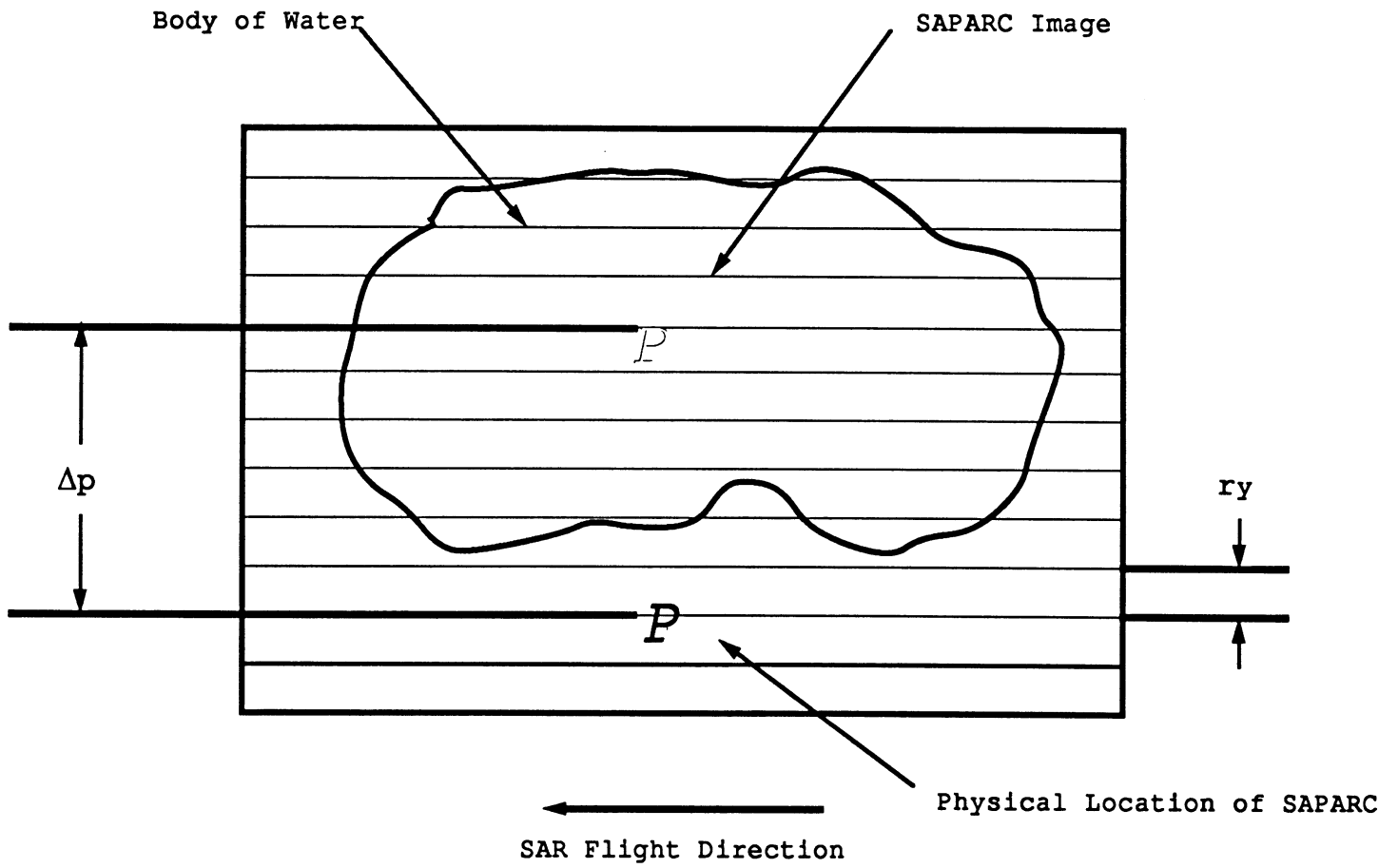


Figure 2.8: The Effects of Placing a Delay Line Within the PARC System

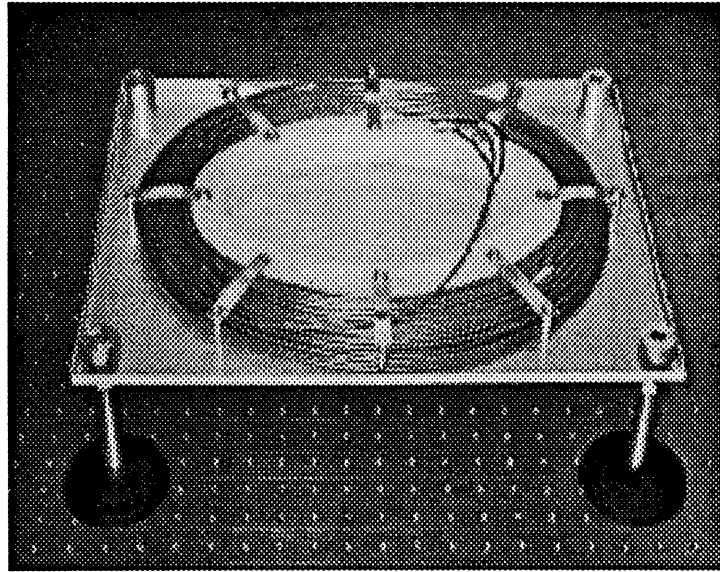


Figure 2.9: C-Band 0.141 Inch Semi-rigid
Microporous Coaxial Delay Line

Figure 2.10: S_{11} Time Domain Response of the C-Band Delay Line

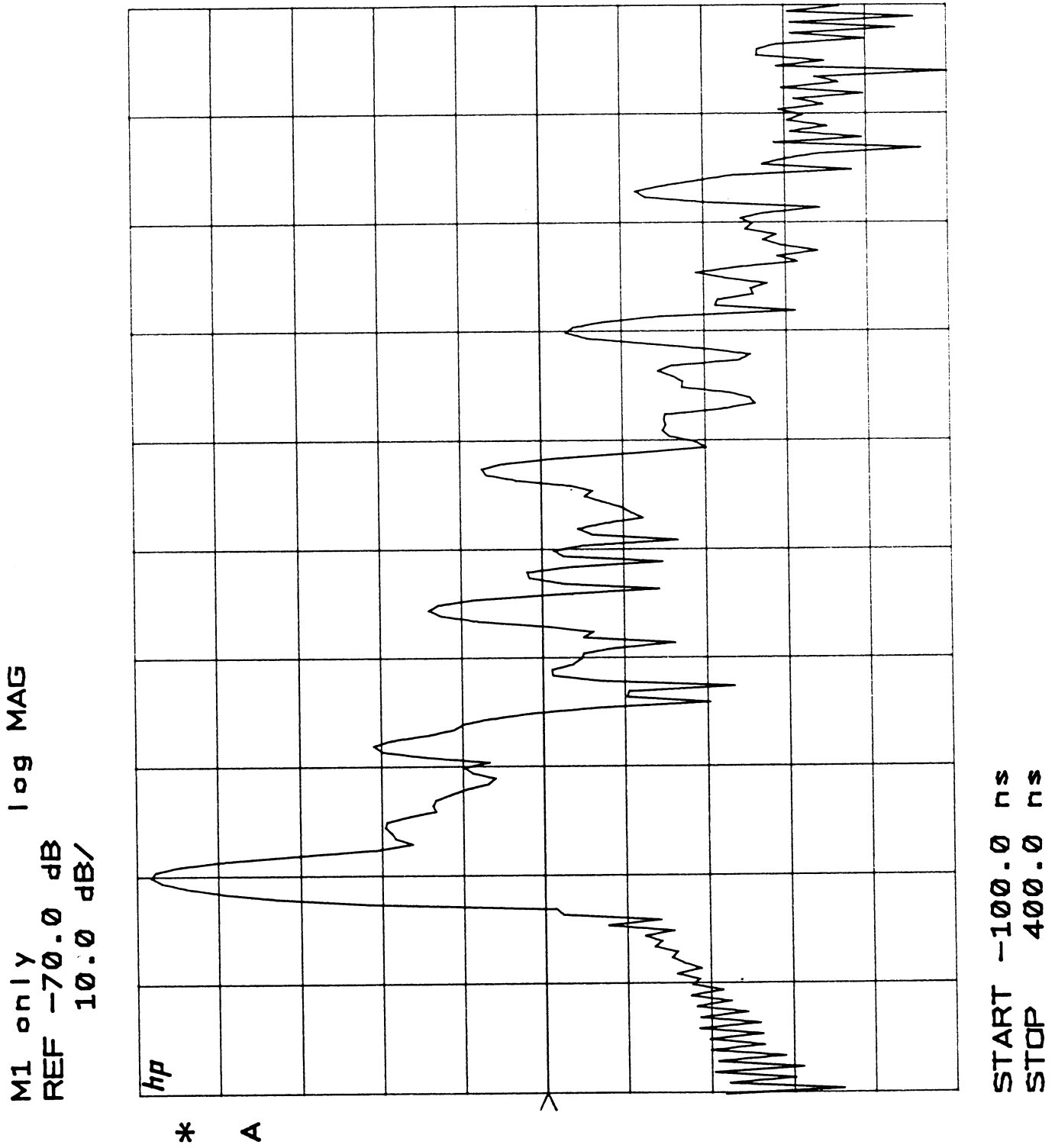
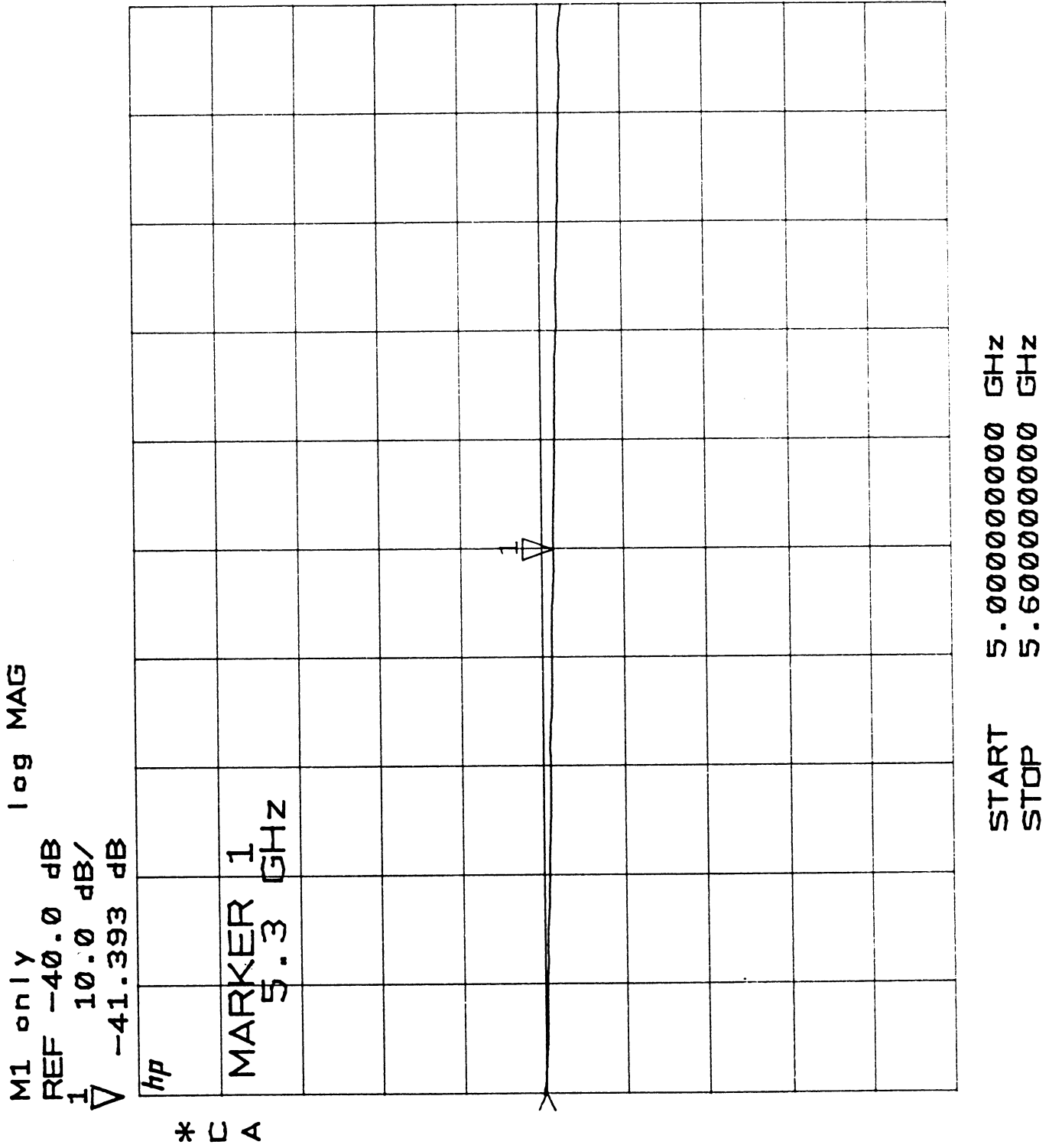


Figure 2.11: S₂₁ Frequency Domain Response of the C-Band Delay Line



With Δp now known, the delay D can be found through the simple relationship

$$D = \frac{\Delta p}{c}$$

where c is the speed of light in free space. L_{\min} , the minimum length of line needed, is

$$L_{\min} = Dv_{\text{coax}} = \frac{\Delta p(0.69c)}{c} = 46.02m = 150.99ft$$

Note that v_{coax} is the velocity of the wave within a coaxial medium. The minimum length of line required is approximately 151 feet, yet in actuality, all of the L- and C-band SAPARCs developed for this project use line lengths of 200 feet (therefore guaranteeing a sufficient delay). Figures 2.9 and 2.10 show the coil of delay line and its corresponding S_{11} time domain response for the C-band SAPARC.

At C-band frequencies, the losses associated with any delay line tend to be quite severe. These losses were minimized by using 0.141 inch semirigid microporous coaxial cable (manufactured in 25 ft-long pieces by Precision Tube, Inc.). The total attenuation resulting from the eight 25 ft-long sections was measured with a Hewlett Packard 8510 Network Analyzer, and was found to be approximately 41.4 dB (see Figure 2.11). Note that the measured loss and the losses quoted by the manufacturer, namely 22 dB, differed by almost 20 dB. It is assumed that this difference results from the losses associated with the 16 connectors.

2.3.2 Amplifiers

The role of amplification in a PARC is to increase the RCS of the antenna system and to compensate for the losses associated with the PARC's delay line and other passive components. The amplifier gain of a SAPARC system must be chosen such that the amplifier operates in the linear region. Amplifier saturation may occur for two reasons: 1. saturation due to high levels of input power received from the SAR platform, and 2. saturation due to feedback oscillations. The latter of the two results from a finite receive

and transmit channel isolation (determined by the performance of the OMT and horn antenna).

2.3.2.1 Input Power Calculations

In order to insure that the amplifiers would not be saturated by the received RF, a number of preliminary calculations were made using the Friis transmission formula and known system parameters for JPL's AIRSAR and NASA's Shuttle Imaging Radar (SIR-C). Tables 2.2 and 2.3, respectively, summarize the JPL AIRSAR and NASA SIR-C parameters.

Peak Power	$P_t = 1 \text{ kW (60 dBm)}$
Average Power	$P_t = 19 \text{ W (42.79 dBm)}$
Wavelength	$\lambda = 0.0566 \text{ m}$
Antenna Gain	$G = 23.3 \text{ dB}$
Altitude	15,000 - 40,000 ft (4,572 - 12,192 m)
Incidence Angles	20° - 70°
Pixel Resolution	3.03 m or 12.01 m (1 or 4 Look Azimuth) 6.67 m (Slant Range)

Table 2.2: JPL AIRSAR Parameters

Peak Power	$P_t = 2.2 - 2.25 \text{ kW (63.42 - 63.52 dBm)}$
Wavelength	$\lambda = 0.0566 \text{ m}$
Antenna Gain	Unknown (Assume $G \approx 20 \text{ dB}$)
Altitude	200 - 225 km
Incidence Angles	15° - 55°
Pixel Resolution	10 - 60 m Range Resolution

Table 2.3: SIR-C Parameters

For JPL's AIRSAR system, the following Friis transmission calculations are applicable. Figure 2.12 depicts the geometry of a typical fly-by, where h is the height of the platform and R is the corresponding range (i.e. distance between the SAR and the calibration unit). The values used in this calculation are for the "worst case" scenario with respect to possible amplifier saturation. Therefore, the dimensions correspond to the case where the maximum amount of power will be received by the SAPARC.

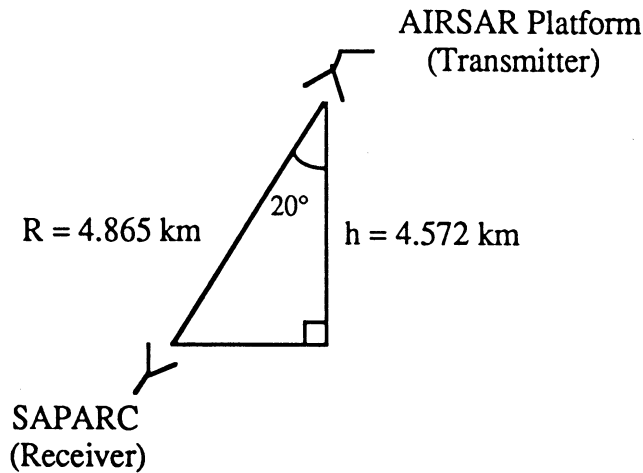


Figure 2.12: JPL AIRSAR Fly-by Geometry

The general form of the Friis transmission formula is

$$P_R = P_T \left(\frac{\lambda}{4\pi R} \right)^2 G_T G_R \quad [4]$$

whereas

$$R = \frac{h}{\cos(\theta)} = 4.8654 \text{ km}$$

$$P_T = 1 \text{ KW} = 60 \text{ dBm}$$

$$\left(\frac{\lambda}{4\pi R} \right)^2 = \left(\frac{0.0566 \text{ m}}{4\pi(4.8654 \text{ km})} \right)^2 = -120.67 \text{ dB}$$

$$G_T = 23.3 \text{ dB}$$

$$G_R \approx 15 \text{ dB}$$

Therefore, the maximum input power received by the first stage amplifier will be

$$P_R = 60 + 23.3 + 15 - 120.67 = -22.37 \text{ dBm}$$

Similarly, NASA's SIR-C system, shown in Figure 2.13, will yield the following results.

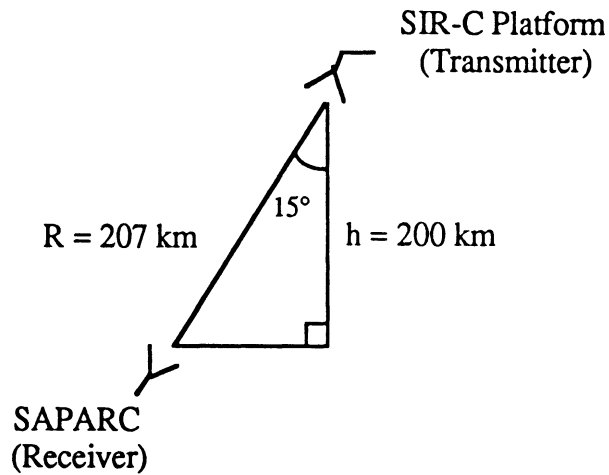


Figure 2.13: NASA SIR-C Fly-by Geometry

The Friis transmission formula gives

$$P_R = P_T \left(\frac{\lambda}{4\pi R} \right)^2 G_T G_R \quad [4]$$

whereas

$$R = \frac{h}{\cos(\theta)} = 207.05 \text{ km}$$

$$P_T = 2.25 \text{ KW} = 63.52 \text{ dBm}$$

$$\left(\frac{\lambda}{4\pi R} \right)^2 = \left(\frac{0.0566 \text{ m}}{4\pi(207.05 \text{ km})} \right)^2 = -153.25 \text{ dB}$$

$$G_T \approx 20 \text{ dB}$$

$$G_R \approx 15 \text{ dB}$$

Therefore, the maximum input power received by the first stage amplifier will be

$$P_R = 63.52 - 153.25 + 20 + 15 = -54.73 \text{ dBm}$$

The gain of the first stage amplifier (i.e. the pre-amplifier) is at most 44 dB (see Appendix B). Hence, the first stage amplifier must be capable of producing the following output power levels in order to insure operation within the linear range of the amplifier.

$$\text{AIRSAR } P_{out} = P_R + G_{preamp} = -22.37 \text{ dBm} + 44 \text{ dB} = 21.63 \text{ dBm}$$

$$\text{SIR-C } P_{out} = P_R + G_{preamp} = -54.73 \text{ dBm} + 44 \text{ dB} = -10.73 \text{ dBm}$$

As shown in Figure 2.2, an additional attenuator of 10 dB was added to the front end of the pre-amplifier as an extra precaution to deter possible saturation during AIRSAR calibrations. Note that the 1 dB compression point for this amplifier is approximately 15 dBm.

Adding an attenuator "in front" of the amplifier degrades the signal to noise ratio; however, in this case, the signal level is much higher than the thermal noise, thus the effect of the additional attenuator is negligible. As will be pointed out in the next section, the noise inherent within the loop can lead to internal oscillations. Therefore, minimizing the noise will theoretically lead to a maximization of G_{Loop} . Yet, in light of the seriousness of amplifier saturation, it was agreed that the benefits resulting from this potentially lower noise performance could not outweigh the assurance that the pre-amplifier is operating within its proper linear range.

2.3.2.2 Feedback Oscillations

An equally serious problem can arise when the system is driven into a state of feedback oscillation. Section 2.3.2.1 alluded to the fact that noise inherent within the system can be amplified just as easily as any incoming RF signal. Oscillations result whenever the amplified noise exceeds the isolation of the antenna system. For the C-band SAPARC design, the net G_{Loop} gain must not exceed 42 dB (the antenna system's cross polarization isolation).

Since G_{Loop} must be less than 42 dB, it follows that

$$G_{Loop} = G_{Amp} + L_{Line} < 42 \text{ dB}$$

Rearranging this equation gives

$$G_{Amp} < G_{Loop} + L_{Line} = 42 \text{ dB} + 42 \text{ dB}$$

Therefore

$$G_{Amp} < 84 \text{ dB}$$

Due to the relatively high loss of the delay line, a second amplifier is needed to help boost the signal before it is transmitted back to the SAR platform. As was done with the preamplifier, care must be taken to insure that the second stage amplifier is not driven into saturation. For this reason, the 1dB compression point of the power amplifier was chosen to be 29 dBm.

2.3.3 Attenuation Switches

The principle goal of the attenuation switch (see Figure 2.2 and Appendix C, pg. 6) is to reduce the loop gain thereby allowing the SAPARC to be used for both JPL AIRSAR and NASA SIR-C missions with the maximum allowable RCS. As pointed out in Section 2.3.2.1, JPL's AIRSAR, which flies at significantly lower altitudes than SIR-C, has a correspondingly higher risk for saturating the SAPARC's amplifiers. Conversely, an excessively large G_{Loop} can lead to the saturation of the SAR platform's own receiver.

The original goal was to insert (via the microwave switches) a 10 dB pad within the G_{Loop} path for AIRSAR calibrations. This pad could then be "switched out" for SIR-C applications; however, it was found that the system would occasionally slip into a feedback oscillation mode whenever the 10 dB pad was out of the G_{Loop} line. These oscillations occurred most prevalently whenever the amplifiers were not warmed up, thus implying that the loop gain was right on the fringe of its maximum limit (the amplifiers can exhibit a 1-2 dB drift in gain between initial turn-on and steady state / room temperature operation). Reducing the loop gain by 3 dB eliminated this problem altogether for operating temperatures of 20° C and greater. (See section 3.3 for cold

weather operation). Hence, for SIR-C usage, the Mini-Microcircuits switches insert a 3 dB attenuator into the loop, whereas a 10 dB attenuator is inserted for the JPL AIRSAR calibrations.

The Miteq pre-amplifier and power amplifier tandem provide approximately 96 dB of gain, which is well above the limit shown above in Section 2.3.2.2 (see Appendix B). Hence, this explains why an attenuator must be added in front of the first stage amplifier since doing so makes G_{Loop} less than the cross polarization isolation of the antenna system. It would appear as if a 13 dB (i.e. $96\text{dB} - 13\text{ dB} = 83\text{ dB} < G_{amp\ max} = 84\text{ dB}$) attenuator is required; however, a trial and error approach showed that a 3 dB attenuator is sufficient to prevent feedback oscillations.

Note that the results shown throughout this report reflect the SAPARC's operation within the SIR-C mode. Similar results can easily be found for the AIRSAR case by simply subtracting 7 dB from the overall SIR-C RCS measurements.

2.4 Control and RF Detection Circuitry

The control and RF detection circuitry serves a two-fold purpose. First, it provides the necessary switching and timing functions for the various power loads; secondly, the circuits display the operating status of the entire system, thereby alerting the user of changes in battery capacity and calibration readiness. The system is comprised of three major components: the Control Printed Wiring Assembly (PWA), the Detection PWA, and the Control Panel. A more detailed description of each of these subsystems is given in the following sections.

2.4.1 Control Circuitry / Control Panel

The single antenna PARCs developed through this project feature custom made control and detection circuits. The features of the control circuitry are as follows:

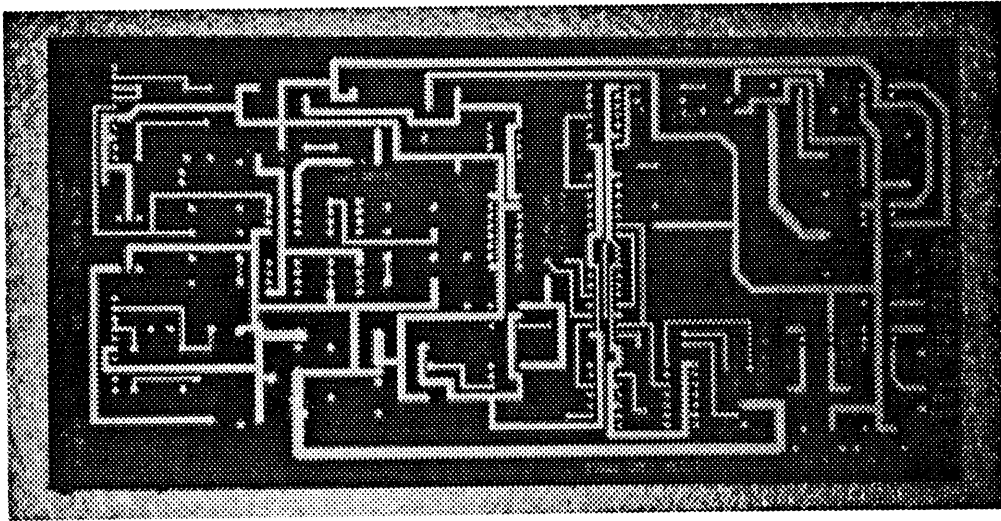


Figure 2.14: SAPARC Control Printed Wiring Assembly (Unstuffed)

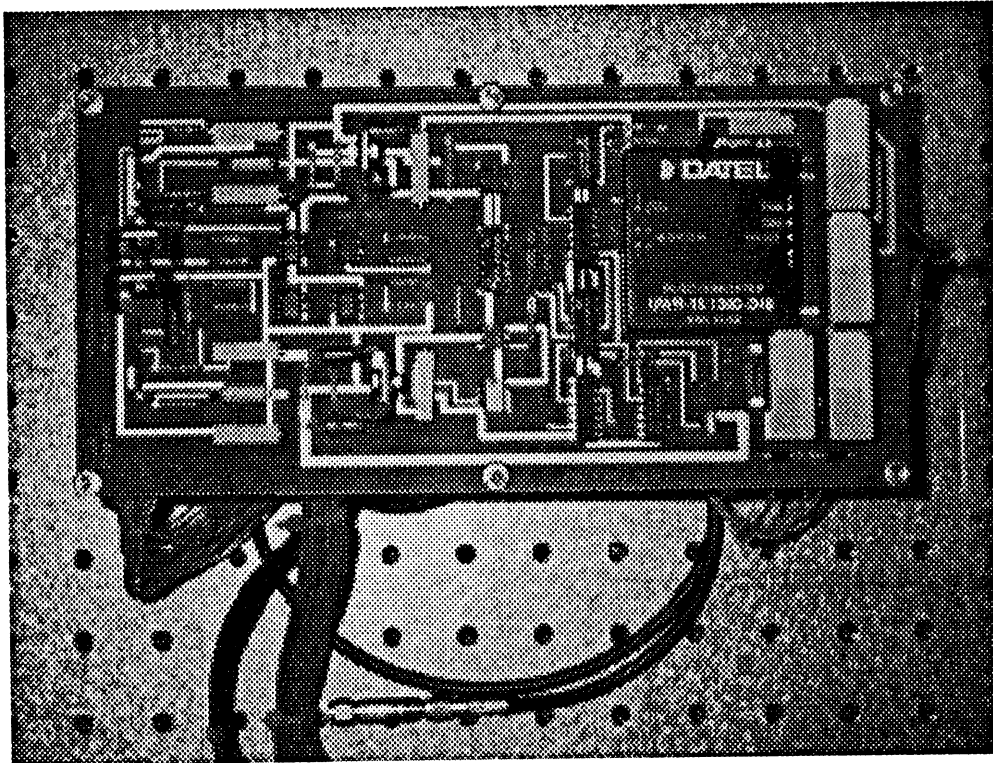


Figure 2.15: SAPARC Control Printed Wiring Assembly (Stuffed)

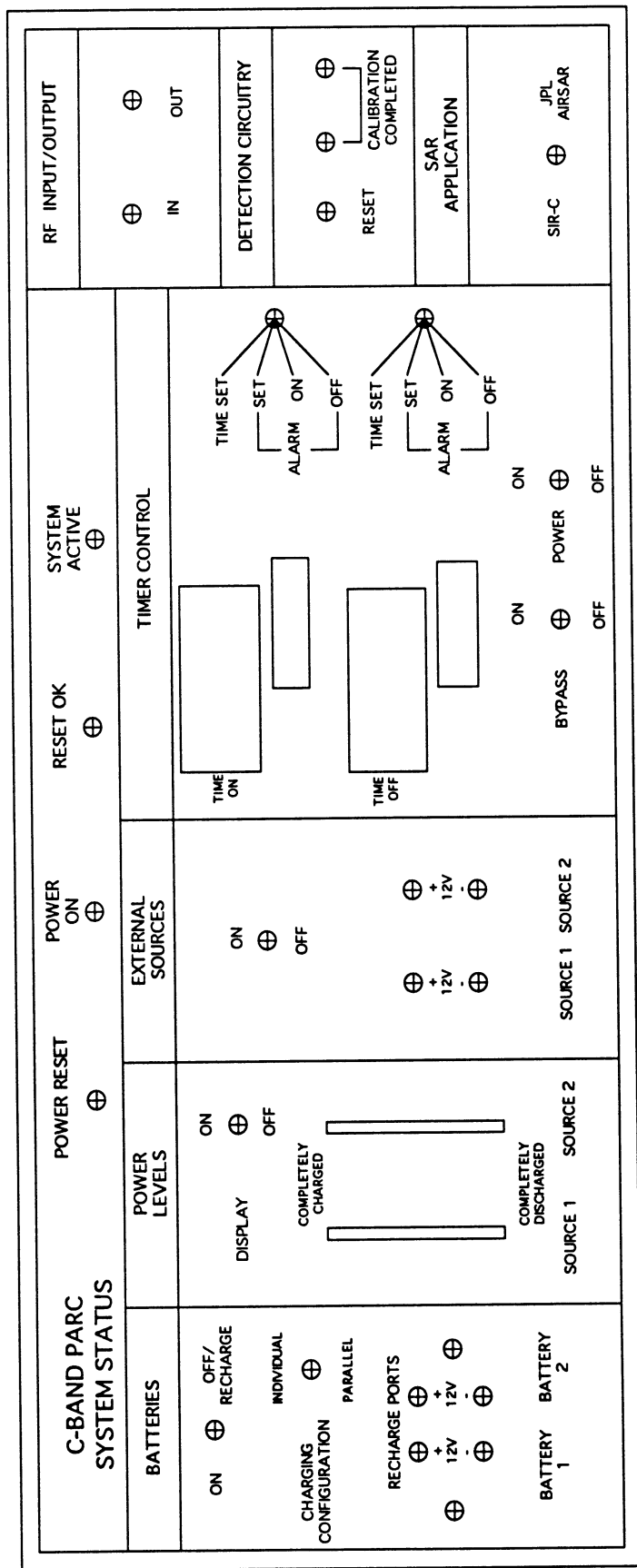


Figure 2.16: Blueprint of the SAPARC Control Panel

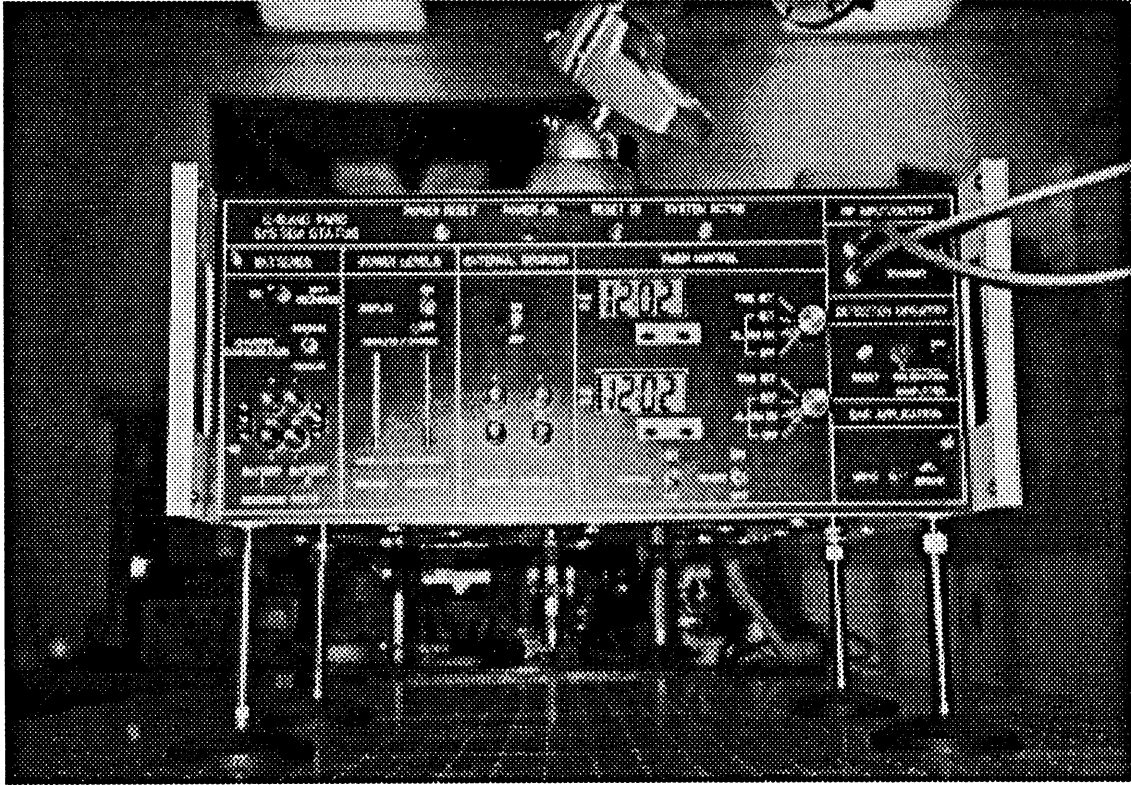


Figure 2.17: SAPARC Front Control Panel

- LED Battery Power Monitor
- Battery Over-discharge Protection
- Automatic System Activation Timers
- Voltage Regulation
- Auxiliary Switching Capability
- External Source Hook-up
- Recharge Ports for Internal Sources
- Easy Detachability for Maintenance

Most of the circuitry (for the functions listed above) is mounted on the Control PWA. This board was designed with EE Designer, a PWA layout software package which can be run on most IBM pc's. The PWA was then manufactured by L. Ross industries in Ann Arbor. (See Figures 2.14 and 2.15).

As a final note, the entire Control PWA / Detection PWA combination can be removed from the system chassis by disconnecting the 50 - pin connector. Before doing so, however, it is advised that the user first disconnect the internal supplies by removing the 7A fuses; the "BATTERIES" switch must then be turned on, and the "POWER RESET" button depressed (for 10 seconds) so that all residual charge held by the internal capacitance of the system can be safely discharged. (See Figure 2.16 and 2.17, both of which depict the front control panel).

2.4.1.1 LED Battery Power Monitor

The LED display mounted on the control panel is driven by a differential amplifier circuit which monitors the gradual drop in voltage of each separate lead acid battery (see Appendix C, pg. 3). Preliminary tests showed that this drop is a linear function of time, whereby the safe operating range exists between $10V \leq V \leq 12.5V$ (refer to the battery operating curves given in Figures 3.12, 3.13, and 3.14). The entire system becomes fully loaded whenever the LED display is activated, thus yielding a more accurate measurement of the battery's remaining capacity. Note that under room temperature conditions, the Yuasa 7 A-hr 12V batteries can operate for up to 5.5 hours (under a full load of 1.2A) before the lower operating voltage threshold is reached. Colder temperatures will significantly limit this capacity; at $-10^{\circ}C$, the system can only operate for 4.5 hours before the same lower threshold causes the system to shut down.

The LED display is currently set to measure a voltage range of $10.5V \leq V \leq 12.5V$ for each supply. This range can be adjusted for supplies 1 and 2 by tweaking the potentiometers R8 and R17, respectively.

2.4.1.2 Battery Over-discharge Protection

In conjunction with the LED bar graph display, the discharge protection circuitry similarly monitors the supply voltages through the use of comparators (see Appendix C, pg. 4). When the lower voltage threshold is reached (i.e. 10V), power to the entire system will be shut off, thus protecting the lead acid batteries from excessive discharging. (The battery's capacity is severely degraded whenever this lower voltage threshold is exceeded for extended periods of time.) This lower threshold can be easily adjusted by tweaking potentiometers R3 and R15 (for supplies 1 and 2, respectively).

2.4.1.3 Automatic System Activation Timers

The system's built-in activation timers can control the operation interval for the SAPARC. In almost all practical situations, the SAPARC needs to be on for a relatively short period of time which can be programmed using the activation timers, thus prolonging the SAPARC's use by conserving battery capacity (see Appendix C, pp. 5-6). Two separate clocks are used: one for activating the high load components, and one for deactivating the entire circuit. The wiring design consists of a number of buffers and opto-isolators which connect the output of the timers (i.e. piezo-electric connections) with the rest of the control circuitry. Note that these connections were made with shielded 20 gauge wire; the first prototype, which did not use shielded wire, experienced occasional transient responses resulting from the switching of the high load components (e.g. amplifiers, heater, etc.). Proper shielding and the use of opto-isolators eliminated this problem altogether.

The timer activation mode can be bypassed for manual operation as well. In the manual mode, the system loads are all activated for immediate and constant operation, thus making this mode ideal for testing purposes. When deploying the SAPARC within a field environment, one should use the bypass in order to insure that the system cannot be

driven into a feedback state. Feedback oscillations will occur whenever an object is placed within the SAPARC's antenna beam pattern. Hence, a low-lying tree branch or other similar object may drive the system into an oscillation state. Using the bypass allows the user to "see" if any objects are within range of causing such problems. If the system can operate correctly in the bypass state, then the user will have confidence that the SAPARC will also work while in the automatic mode.

As a last note, the activation timers are independently powered by small cell 1.25V batteries. These cells can be easily replaced by removing the top cover on the SAPARC chassis. A small plastic cover on the clock units must also be removed in order to gain access to the battery compartments.

2.4.1.4 Voltage Regulation

The various subsystems within the SAPARC require supply voltages of $\pm 15V$, $\pm 8V$, and $+5V$. The $+5V$ and $\pm 8V$ regulation is performed by basic 7800 series regulators, whereas the $\pm 15V$ modes are supplied from DC-DC converters (one on the Detection PWA, and the second on the Control PWA - see Appendix C, pp. 3,4, and 7). The $+15V$ DC-DC converter possesses an efficiency of greater than 80%; hence, the converter outperforms conventional voltage regulation by a considerable margin (i.e. in terms of efficient power use). It should also be noted that conventional regulators cannot supply the relatively large amount of current which is required for the operation of the amplifiers and other possible auxiliary loads.

2.4.1.5 Auxiliary Switching Capability

As mentioned above, the Control PWA is configured so that additional loads can be added (and thus controlled) as the user sees fit (see Appendix C, pg. 2). The voltage output for these auxiliary ports includes $\pm 15V$ and $+24V$. Possible loads include recording devices which can monitor the RF power levels received during SAR fly-bys, thereby providing a means for measuring the pattern of the SAR's illuminating footprint.

The Detection PWA does provide a correlation between detected RF and a specific DC output voltage. This capability may be utilized for use with recording devices. Heaters can also be connected to this circuit; however, testing has shown that their use is of little value for reliable temperature stabilization. (See section 2.5).

2.4.1.6 External Source Hook-up

The user can bypass the internal battery supplies by employing the use of the external hook-up jacks located on the front control panel (see Figures 2.16 and 2.17, as well as Appendix C, pg. 1). If external sources are to be used, simply flip the "EXTERNAL SOURCES" switch to the ON position. Hit the "POWER RESET" pushbutton and continue the system operation in the normal fashion. As a final note, **DO NOT CONNECT THE GROUNDS FROM THE EXTERNAL BATTERIES TOGETHER.**

2.4.1.7 Recharge Ports

The user can also recharge the internal batteries via the recharging ports located on the front control panel (see Figures 2.16 and 2.17, as well as Appendix C, pg. 1). Two different port types are provided for the support of varying recharging devices. When recharging, have the "BATTERIES" switch in the OFF / RECHARGE position. The "CHARGING CONFIGURATION" switch permits the user to charge the batteries individually or together in a parallel mode.

2.4.2 Detection Circuitry

The Detection PWA was acquired from an existing two-antenna PARC system developed by Applied Microwave (see Appendix C, pg. 7). This subsystem monitors the power levels which exist at the output of the power amplifier. The threshold for this detection has been set low enough ($P_{\min \text{ detection}} = -48.6 \text{ dBm}$) so that oscillations as well as SAR fly-bys can be recorded. In the original circuit design, a detection would illuminate a

small red bulb; in addition to this, a .25A circuit breaker switch (which serves as a permanent recording device) has been added to signal the user that a successful calibration is complete. Note that the circuit breaker takes approximately 60 seconds to trip once a detection is made.

When deploying the SAPARC, the user must be certain that feedback oscillations will not occur during the calibration. Therefore, one must always monitor the detection lamp during final setup preparations. (Recall that the SAPARC system is extremely sensitive to adjacent objects which may reside within the antenna's beamwidth. These objects include nearby bushes, tree limbs, etc.). If a feedback scenario is present, simply press the RESET to clear the Detection PWA circuitry. Continue to re-position the SAPARC as needed so that no errant detections are made.

2.5 Temperature Stabilization

During the initial design phase, one of the primary goals was to develop a system which was insensitive to changes in the ambient temperature. It was assumed that the most sensitive devices would be those which are active, namely the preamp and power amp. To this end, a 24W hybrid heater had been placed on the amplifier combination. Unfortunately, the temperature stabilization tests showed that the most sensitive device was the passive delay line, and not the amplifiers as first suspected. The following test results demonstrate this fact:

<u>Component</u>	Ambient Temp (20° C) <u>Measurement</u>	Lower Extreme (-10° C) <u>Measurement</u>	Difference in <u>Measurement</u>
Power Amp Gain (with heater)	51.12 dB	50.46 dB	0.66 dB
Preamp Gain (with heater)	43.33 dB	42.67 dB	0.66 dB
Delay Line Loss	42.53 dB	39.39 dB	3.14 dB
Total Line Loss (without amps) (with 10dB pad)	53.94 dB	49.67 dB	4.27 dB

Table 2.4: Thermal Variations of Key SAPARC Components

As shown above, temperature stabilization would require either a number of high power heaters or a variable attenuator / gain feedback circuit. The former of these alternatives is somewhat impractical since it would require excessive amounts of battery power. Similarly, the latter option is too expensive for a practical implementation.

An acceptable solution requires a mapping of the G_{Loop} component of the RCS as a function of temperature. Such a mapping is shown in Section 3.3. The goal, then, is to accurately record the system's temperature during an actual field test. The temperature (recorded as a function of time) will then be compared to the G_{Loop} vs. Temperature chart from Section 3.3. Hence, an accurate description of the system's total RCS can be calculated for the exact fly-by time of the SAR platform.

An automatic measurement is obtained through the use of a Dickson 24-hour Temperature Recorder. This device is nestled within the delay line loop located at the base of the SAPARC chassis. For an actual field deployment scenario, the user must activate the temperature recorder while noting the exact time of initial operation. Once this is done, the user is free to leave the deployment area while the rest of the equipment remains in its automated mode.

2.6 Assembled Prototype

Figures 2.18 a-c show the SAPARC in its completed state. Note how the horn antenna is detachable for quick and easy transport of the device.

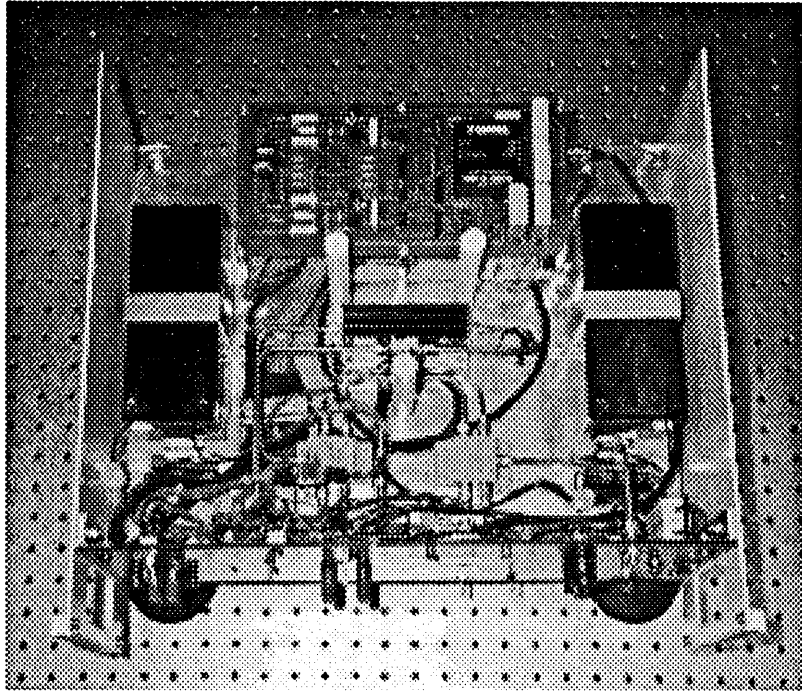


Figure 2.18a: Internal Components of the C-Band SAPARC

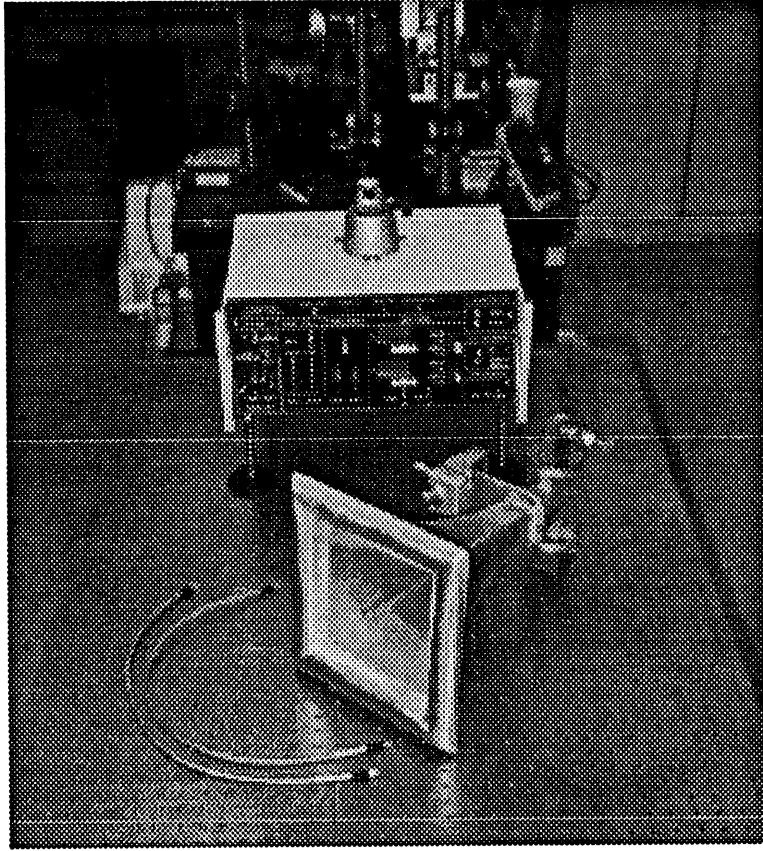


Figure 2.18b: C-Band SAPARC Disassembled For Transport

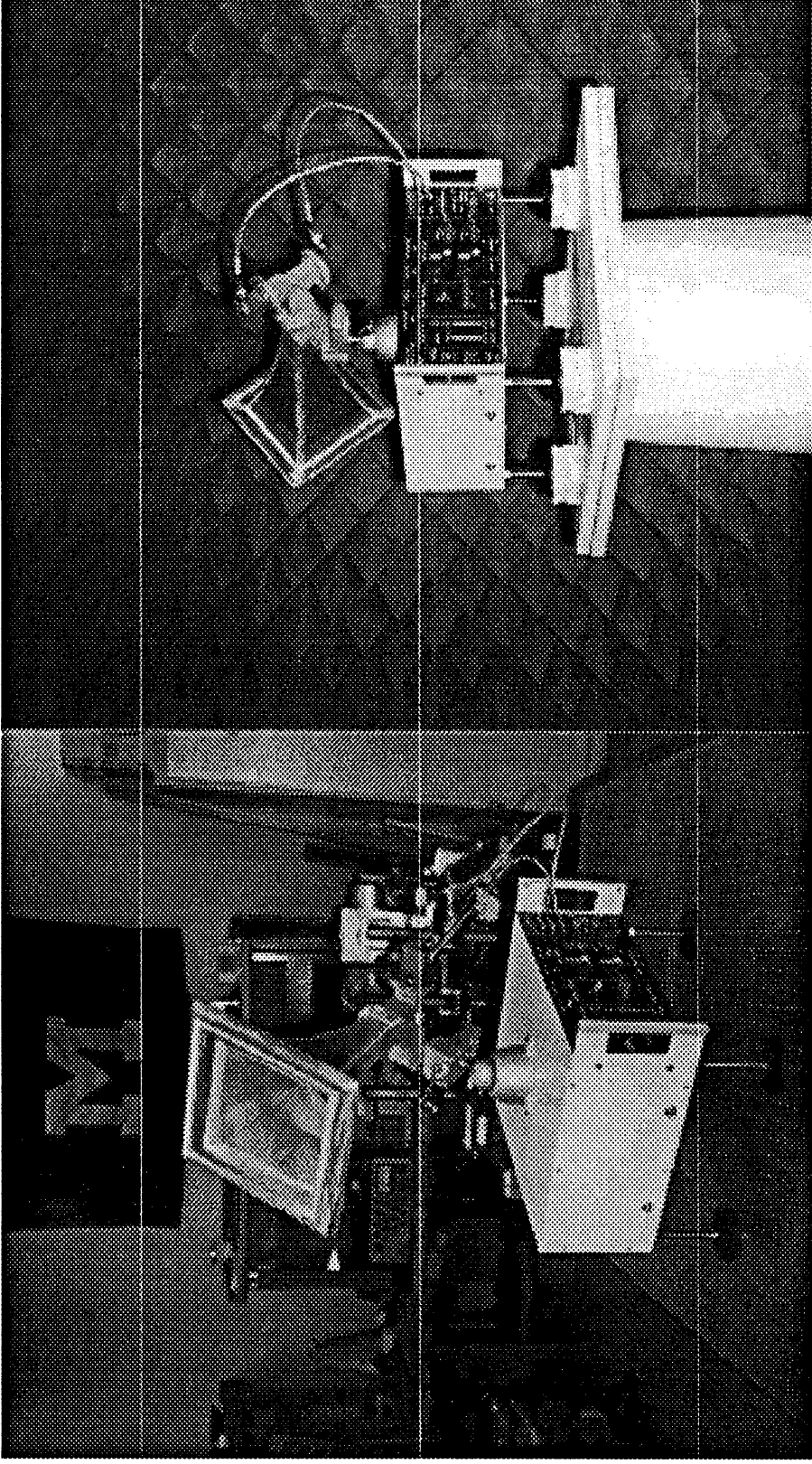


Figure 2.18c: Fully Assembled C-Band SAPARC

CHAPTER III

EXPERIMENTAL RESULTS

As mentioned in Chapter 1, the accuracy of a SAR calibration is highly dependent upon the measured performance of the calibration device. Hence, the measurements taken in accordance with this project must adhere to the following goals:

- Accurate measurement of the scattering matrix for the 0° and 45° antenna orientations.
- 0.2 dB accuracy in the mapping of the thermal gain variations.
- Overall characterization of SAPARC performance with respect to field deployment conditions, including extremes in temperature, all-weather performance, and battery capacity.

3.1 G_{Loop} Measurements

Figures 3.1 and 3.2 depict the S_{21} frequency responses of G_{Loop} for room temperature operation (22°C). For this measurement, a 50 dB attenuator was placed on the receive channel of the SAPARC in order to prevent amplifier saturation. The frequency response for this attenuator is similarly shown in Figure 3.3. From these measurements, G_{Loop} is found to be 44.08 dB. However, as section 3.3 will show, G_{Loop} is highly dependent upon the SAPARC's operating temperature. To find the correct value of G_{Loop} for each SAR calibration, one must refer to the thermal variation chart shown in Figure 3.14.

The SAPARC anechoic chamber tests were performed at room temperature

(approximately 22° C). Figure 3.9 (SAPARC RCS for the 0° Orientation) shows that the maximum achievable value for the RCS is 40 dBsm. Using this data in conjunction with the theoretical equation given in section 2.1, the gain of the C-band antenna system is found to be 15.93 dB. The following calculations demonstrate this result.

$$\sigma = G_{Loop} \frac{G_T G_R \lambda^2}{4\pi}$$

where

$$\begin{aligned} \sigma &\approx 40dBsm \\ G_{Loop} &= 44.08dB \\ G_T = G_R &= G_{Antenna} \\ \frac{\lambda^2}{4\pi} &= \frac{(0.0566m)^2}{4\pi} = -35.94dB \end{aligned}$$

Rearranging the equation gives

$$\begin{aligned} G_{Antenna} &= \sqrt{\frac{\sigma}{G_{Loop} \frac{\lambda^2}{4\pi}}} = \frac{1}{2}(40.0dBsm - 44.08dB + 35.94dB) \\ G_{Antenna} &= 15.93dB \end{aligned}$$

The equations above demonstrate how the user can easily find the RCS of the SAPARC for any given operating temperature. In other words, when the operating temperature is known, the corresponding value of G_{Loop} will also be known, and hence so will the RCS of the SAPARC unit. The equations are similarly applicable to the 45° SAPARC orientation. For this case, simply subtract the 6 dB difference from the 0° orientation antenna results described above.

3.2 Anechoic Chamber Tests

The University of Michigan Radiation Laboratory maintains a fully equipped 60-foot-

long, tapered anechoic chamber which is used for conducting antenna pattern measurements and for measuring the scattering characteristics of man-made and natural targets. This chamber is ideal for making accurate measurements of the SAPARC's RCS within a relatively noise-free environment.

A major component of the Radiation Laboratory's polarimetric radar measurement facility is the LCX POLARSCAT system. The parameters of the C-band subsystem are as follows:

Center Frequency	5.3 GHz
Frequency Bandwidth	0.5 GHz
Antenna Type	Dual Polarized Pyramidal Horn
Antenna Gain	25.3 dB
Beamwidth	8.0°
Far Field ($2d^2 / \lambda$)	5.8 m
XPOL Isolation	45 dB
Calibration Accuracy	± 0.3 dB
Measurement Precision (N>100)	± 0.4 dB
Phase Accuracy	$\pm 3^\circ$

Table 3.1: C-Band POLARSCAT Parameters

A large percentage of this system consists of Hewlett Packard components, including an HP 8753 Network Analyzer and HP 9000 Computer with an additional disc drive. Using computer control, polarimetric measurements of the phase and magnitude responses can be taken with respect to changes in target elevation and azimuth angles (Figure 3.4).

The chamber experiments required a center frequency of 5.3 GHz with a 600 MHz bandwidth. Calibrations were performed by using a 14" metallic sphere in accordance with a calibration technique developed by Sarabandi [5] (See Appendix E). Time gating was also employed, whereby a gate span of 10 ns (centered on the target's response) provides an automatic subtraction of background scatterers.

Figure 3.1: Frequency Domain Response of G_{Loop}

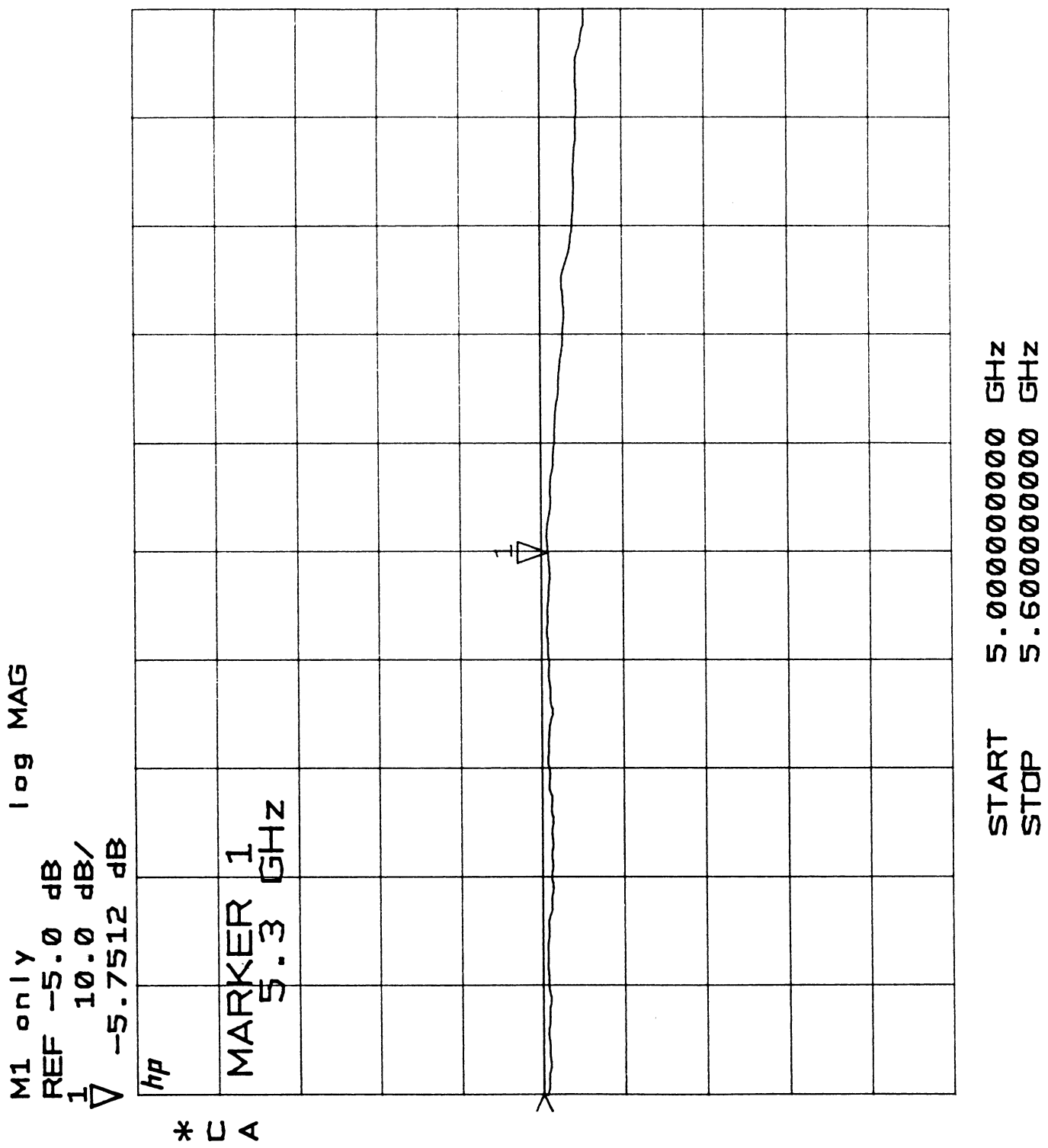


Figure 3.2: Detailed Frequency Domain Response of G_{Loop}

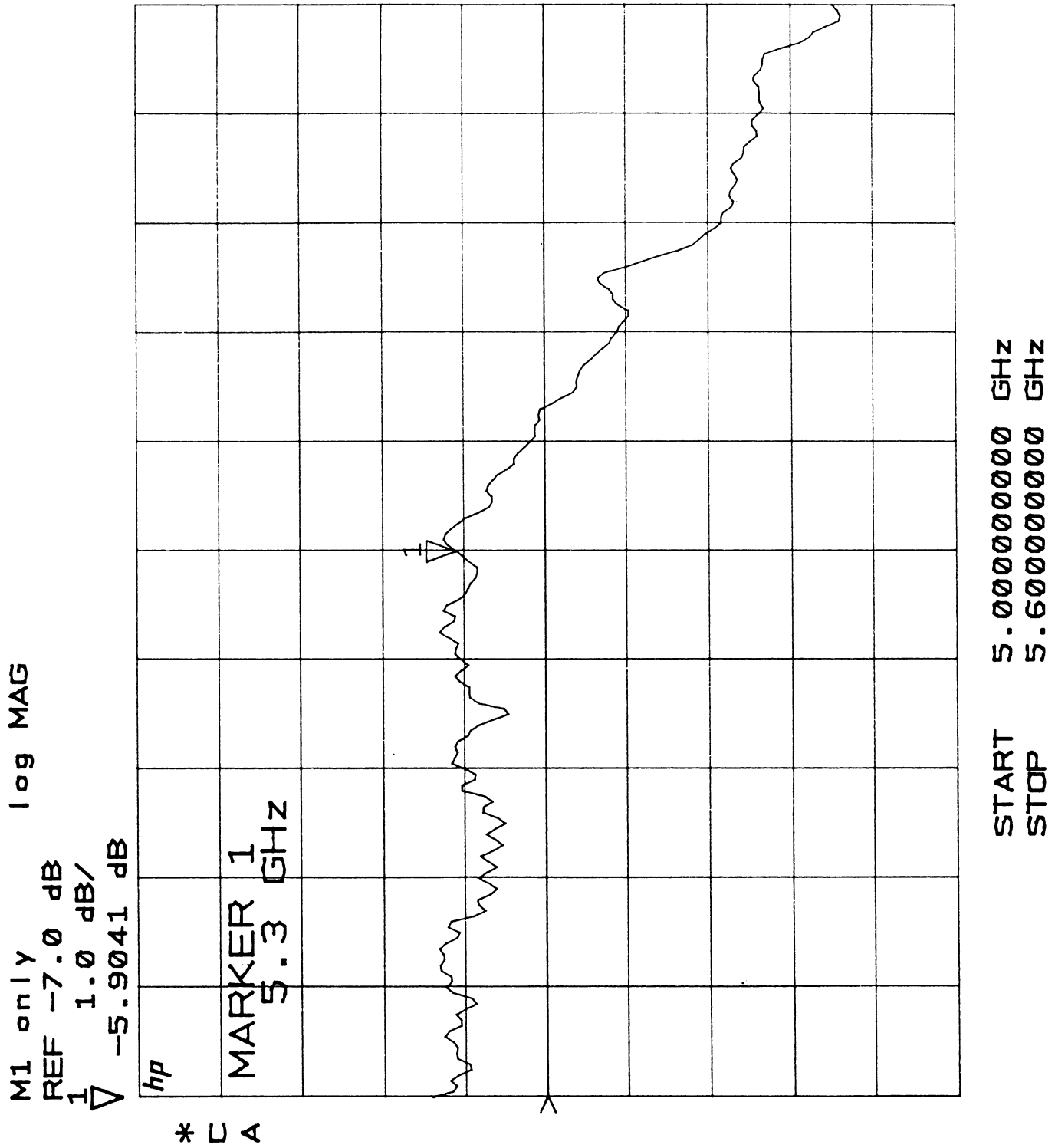
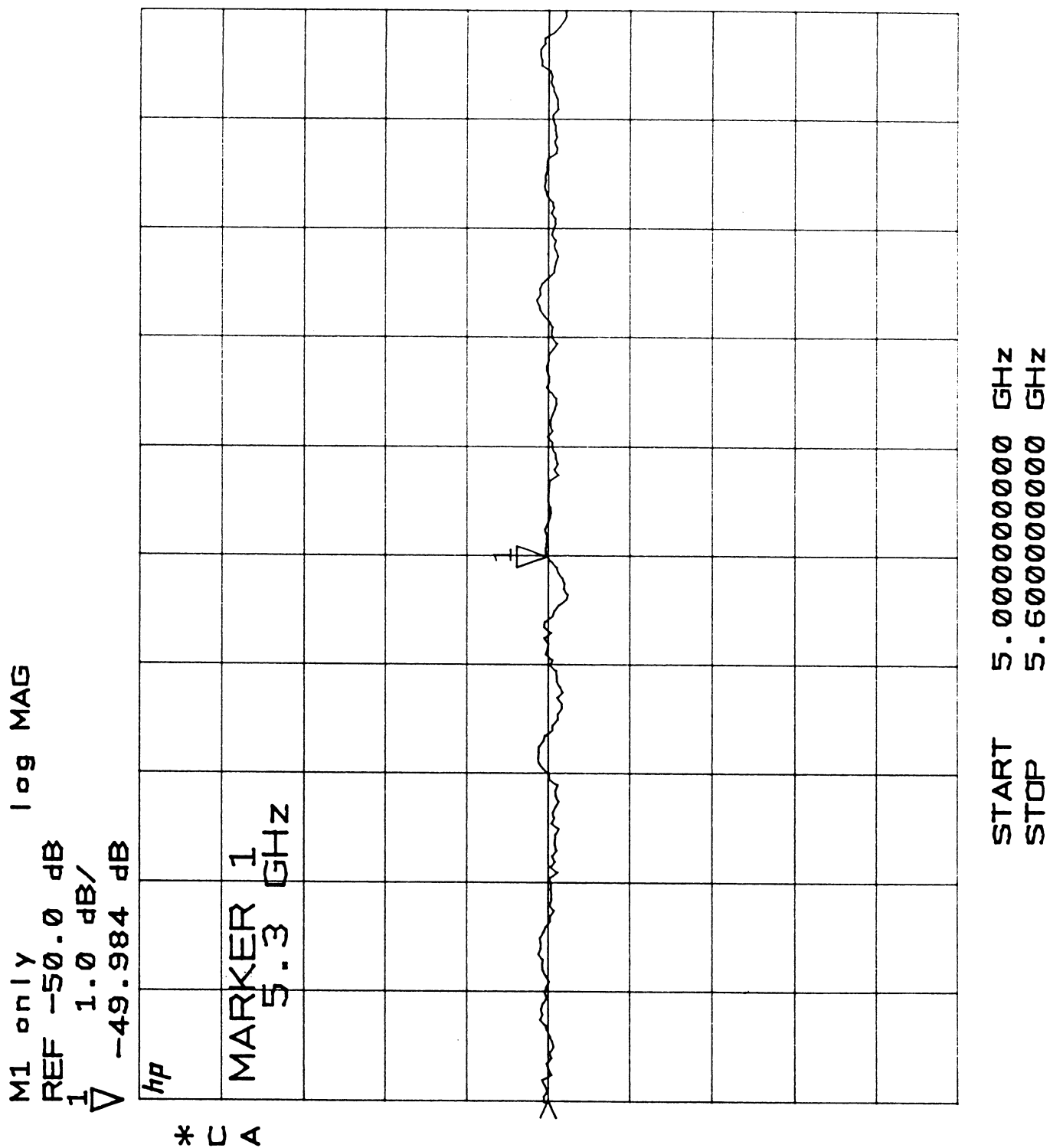


Figure 3.3: Frequency Domain Response of the 50 dB Attenuator



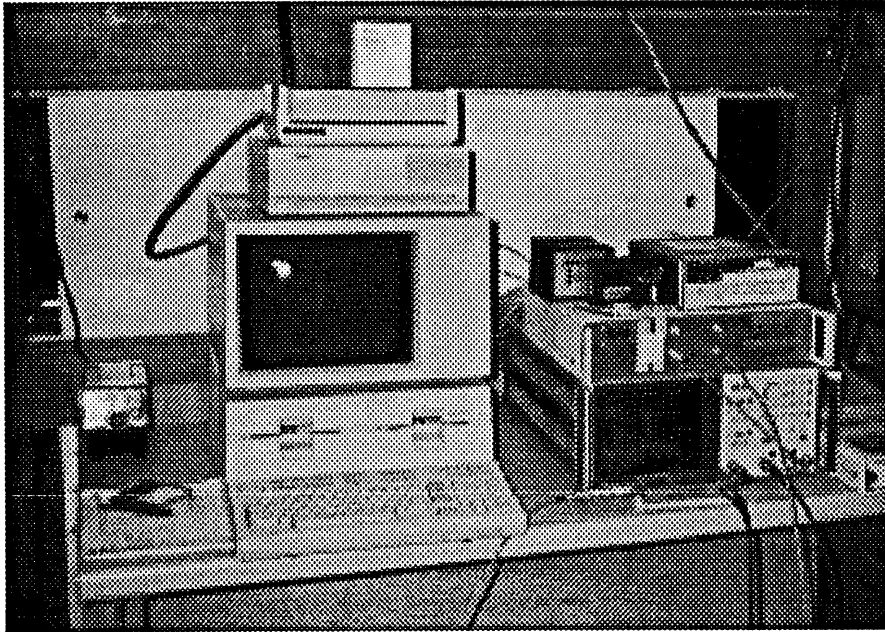


Figure 3.4: C-Band POLARSCAT Test Equipment

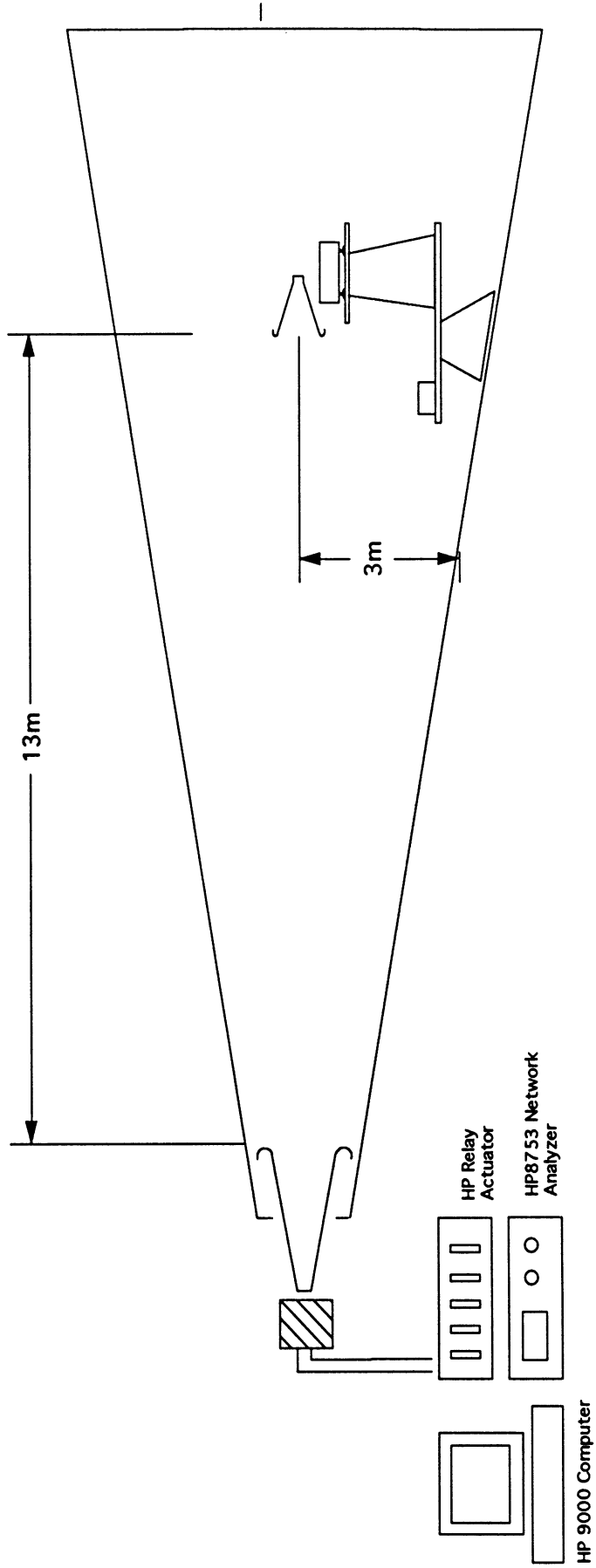
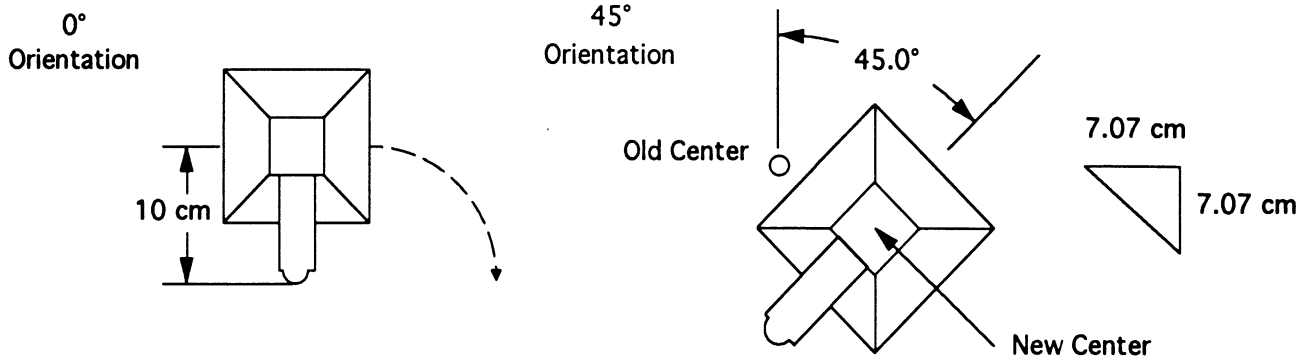


Figure 3.5: Anechoic Chamber Measurements at the University of Michigan's Radiation Laboratory



Note : SAPARC must be moved up by 7.07 cm and mounted to the left by 7.07 cm

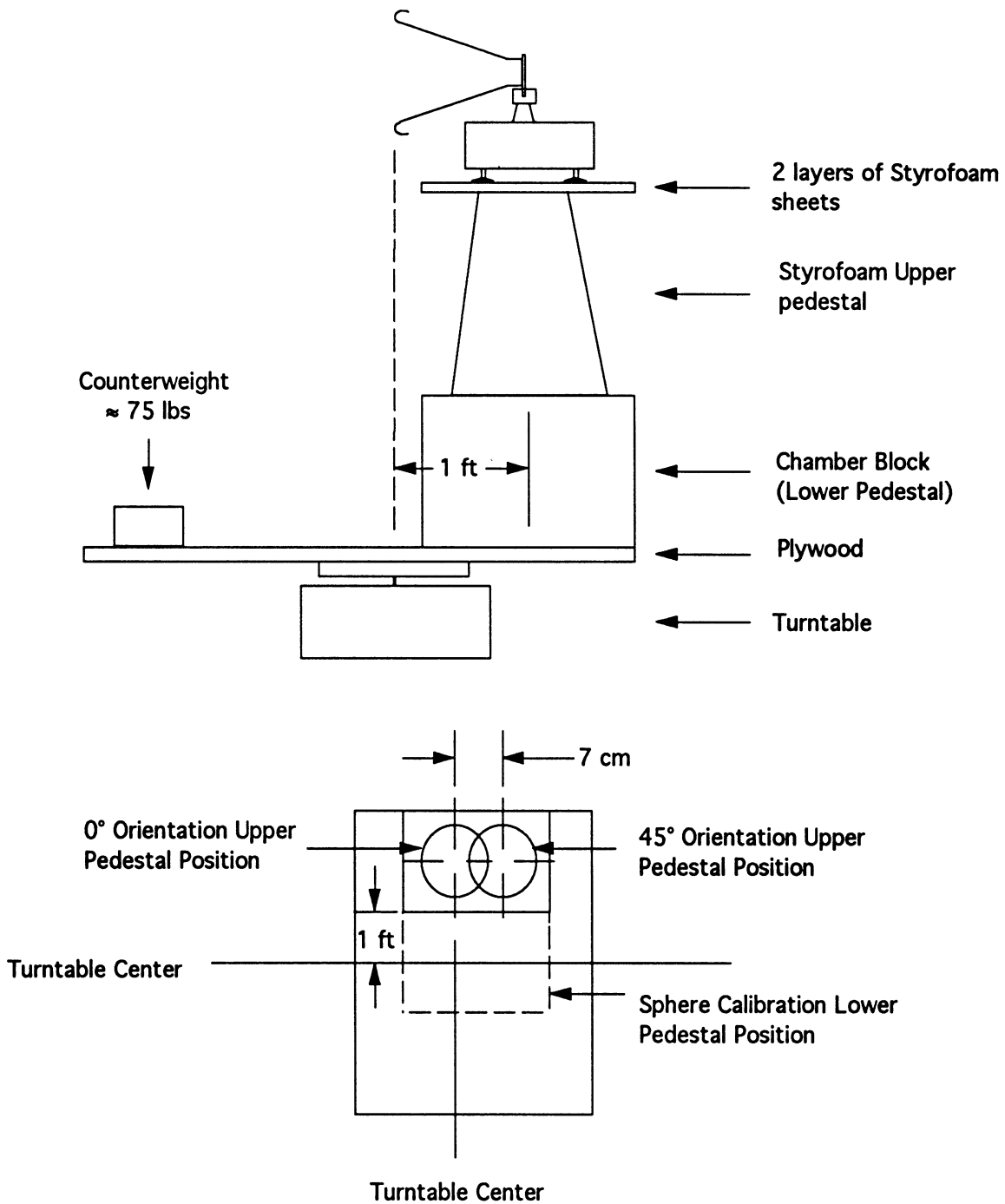


Figure 3.6: 0° and 45° Orientation Modifications

A block diagram of the measuring facility is given in Figure 3.5. Figure 3.6 shows the configurations used for the 0° and 45° Orientation tests.

3.1.1 SAPARC Time Domain Response

Section 2.3 mentioned that a SAR calibration can be enhanced by time shifting the PARC's radar response so that it appears to originate over a dark background (refer to Figure 2.8). Recall that a 200 foot delay line is incorporated into the SAPARC design to accomplish such a feat. The effect of this delay is clearly shown in Figure 3.7, the time domain response of the C-band SAPARC system. As an addendum, Tables 3.2 and 3.3 provide an identification and quantification of the five markers given in Figure 3.7.

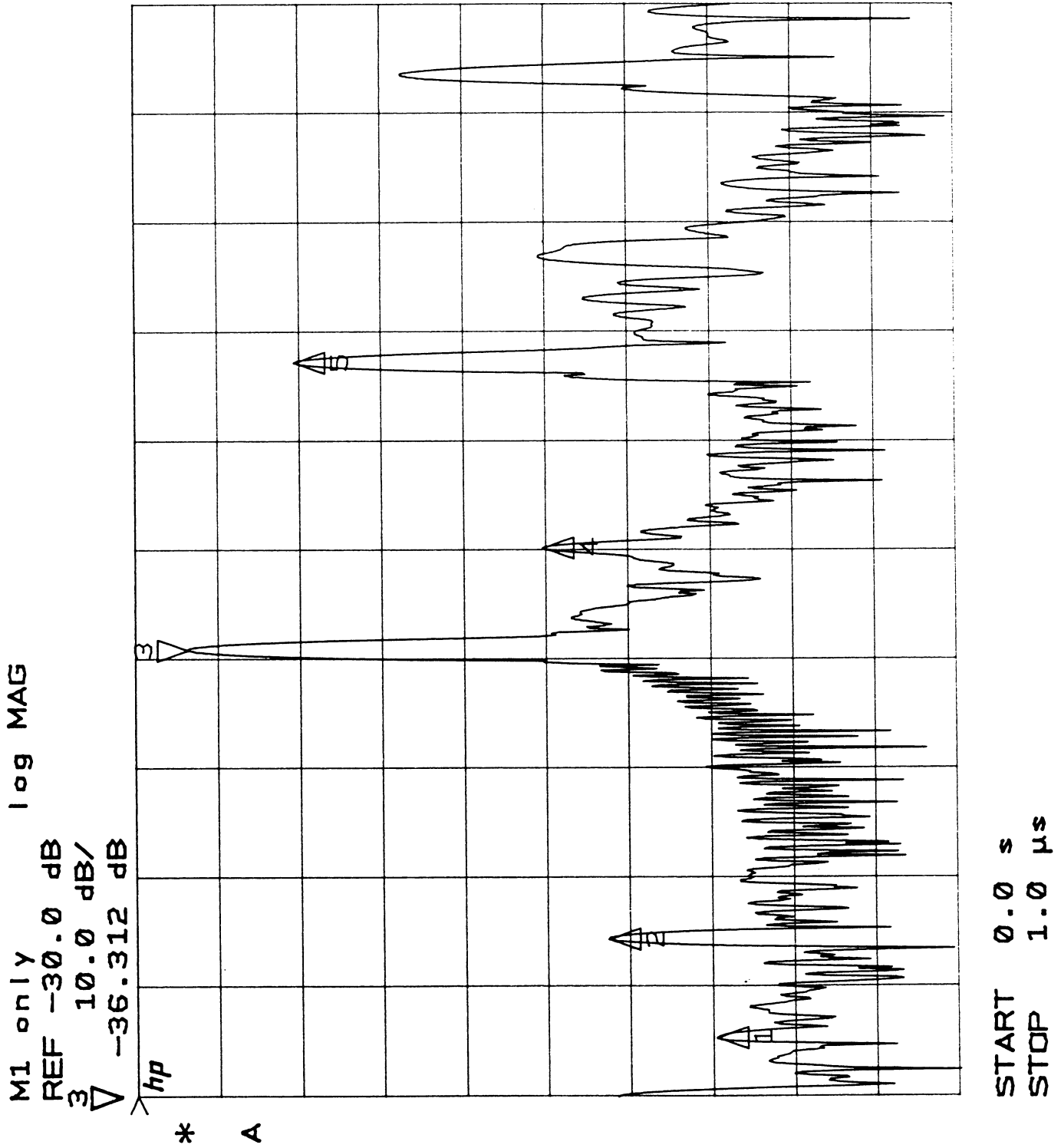
<u>Marker</u>	<u>Identification</u>
1	Leakage (i.e. cross talk) between the receive and transmit horns used in the measurement
2	Backscatter from the SAPARC's antenna and chassis (physical location of the SAPARC)
3	Primary time-delayed SAPARC response
4	First delayed multipath reflection
5	Response due to the <i>ringing</i> of the SAPARC unit

Table 3.2: Marker Identification for Figure 3.2

<u>Marker</u>	<u>Magnitude (dB)</u>	<u>Time Delay (ns)</u>		<u>Electrical Distance (m)</u>	
		<u>Measured</u>	<u>Referenced to Marker 1</u>	<u>Measured</u>	<u>Referenced to Marker 1</u>
1	-100.39	53.75	0.00	16.11	0.00
2	-87.40	143.75	90.00	43.10	26.99
3	-36.31	408.75	355.00	122.54	106.43
4	-79.59	502.50	448.75	150.65	134.54
5	-49.37	672.50	618.75	201.61	185.50

Table 3.3: Magnitude and Position Values for the Markers Shown in Figure 3.2

Figure 3.7: SAPARC Time Domain Response



The values given in Tables 3.2 and 3.3 lead to a number of important conclusions. First, the electrical length of the delay line is found to be the difference between markers 2 and 3, namely 265 ns. This, in turn, corresponds to an electrical length of 79.44 m; hence, the SAPARC's SAR response has effectively been translated by nearly 80 m (i.e. approximately 260 feet). Also note the ringing effect (marker 5) where a replica of the original SAR response is periodically repeated every 263.75 ns, or 79.1 m. The subsequent replicas are a product of the limited isolation of the OMT. During the transmission of the first SAR response, a small amount of leakage RF makes its way through the SAPARC loop where it is amplified, delayed, and re-transmitted as another SAR response. Figure 3.7 shows how each of the recurring responses will decay by approximately 13 dB; hence, this process continues until the net amount of leakage becomes negligible. When processing the imaging data, the ringing effect inherent with each SAPARC allows for easy identification and location of the calibration system, thus providing another advantage over passive calibration devices.

Marker 4 shows the delayed response of the first multipath reflection. The distances between markers 1 and 2 and markers 3 and 4 are virtually identical; therefore, it is believed that the response labeled by marker 4 corresponds to a component of the original signal which experienced multiple reflections from the SAPARC horn / chassis and the receive / transmit antennas on the radar platform. In other words, this signal originally reached the SAPARC unit where it was then reflected back towards the radar platform. Once reaching the platform, the signal was then reflected back again towards the SAPARC. Upon reaching the SAPARC for the second time, the signal was received, delayed, amplified, and re-transmitted back to the radar platform. Similar multipath signals are shown throughout Figure 3.7.

As a final point, the SAPARC provides an exceptional signal to noise ratio (SNR). The difference between the SAR response (labeled as marker 3) and the anechoic chamber's noise floor is over 70 dB. A 50 dB signal to clutter ratio (i.e. the difference between markers 2 and 3) is also shown to be quite extraordinary. These relatively large values of SNR will prove to be very beneficial for actual SAR calibrations.

3.1.2 0° Orientation Test

The 0° orientation of a SAPARC refers to the case when there is no polarization mismatch between the radar's antenna and the SAPARC antenna. In this mode, the SAPARC provides a calibration of σ_{hv} , where a received vertically polarized signal is amplified, delayed, and transmitted back to the radar with a horizontal polarization. The phasor polarizations are given in Figure 3.8.

Figure 3.9 demonstrates the measured azimuthal pattern response for this orientation. As shown, the SAPARC yields a maximum RCS response of 40 dBsm with a 15° half-power beamwidth (for the σ_{hv} case). (Note that the traditional convention of listing the target's polarimetric RCS as σ_{xy} , where x and y refer to the received and transmitted polarizations, respectively, is used.) A cross polarization isolation of 38 dB exists between σ_{hv} and σ_{vv} , σ_{hh} , thereby giving credence to the excellent cross polarization isolation performance of the horn / OMT design described in section 2.2.

As a final point, the σ_{vh} response reveals the "noise floor" inherent with this measurement. This RCS response is characterized by a 100% polarization mismatch for both the radar and SAPARC antennas, and hence the extremely low RCS response of -40 to -60 dBsm is expected.

3.1.3 45° Orientation Test

The 45° orientation is accomplished by rotating the SAPARC horn as demonstrated in Figure 3.10. Doing so allows a complete calibration of the Scattering Matrix since each transmit and receive combination, namely σ_{vv} , σ_{hh} , σ_{hv} , and σ_{vh} , yields the same RCS azimuthal pattern response with a half-power beamwidth of 15°. Figure 3.11 depicts the RCS azimuthal pattern response for the 45° orientation. Note how each trace is symmetric and virtually equal over a 40° beamwidth, as expected. Also note how the peak RCS of 34 dBsm is exactly 6 dB below the 0° orientation response of 40 dBsm. Again, this result is in excellent agreement with the theoretical expectations (the two 45° polarization mismatches, one for transmit and the second for receive, correspond to a total loss in power of $1/2 \cdot 1/2 = 1/4 = 6$ dB).

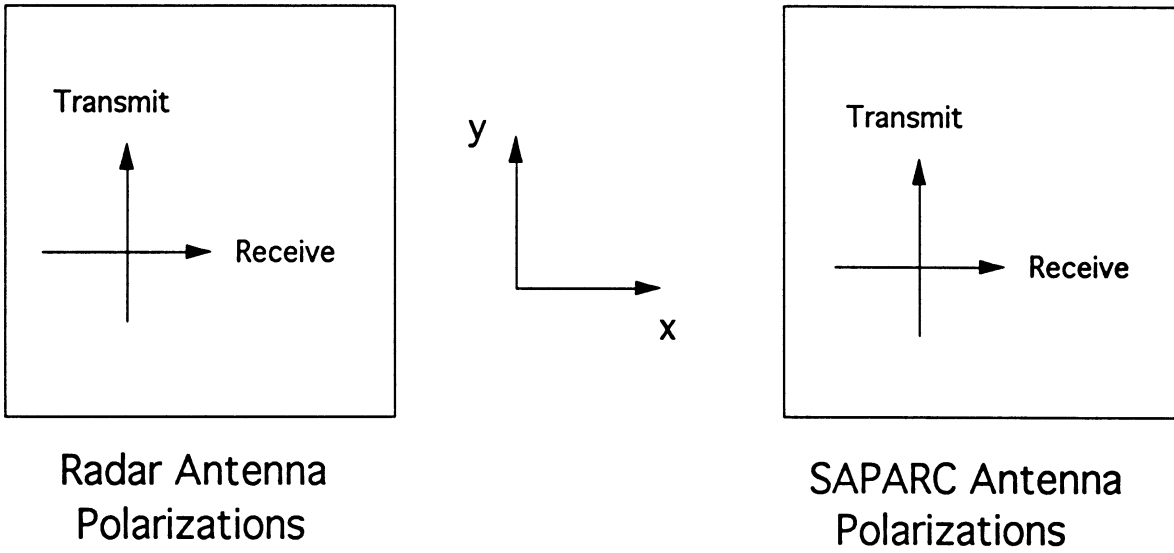
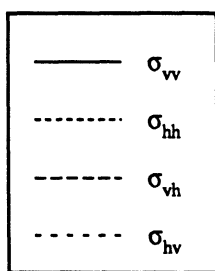
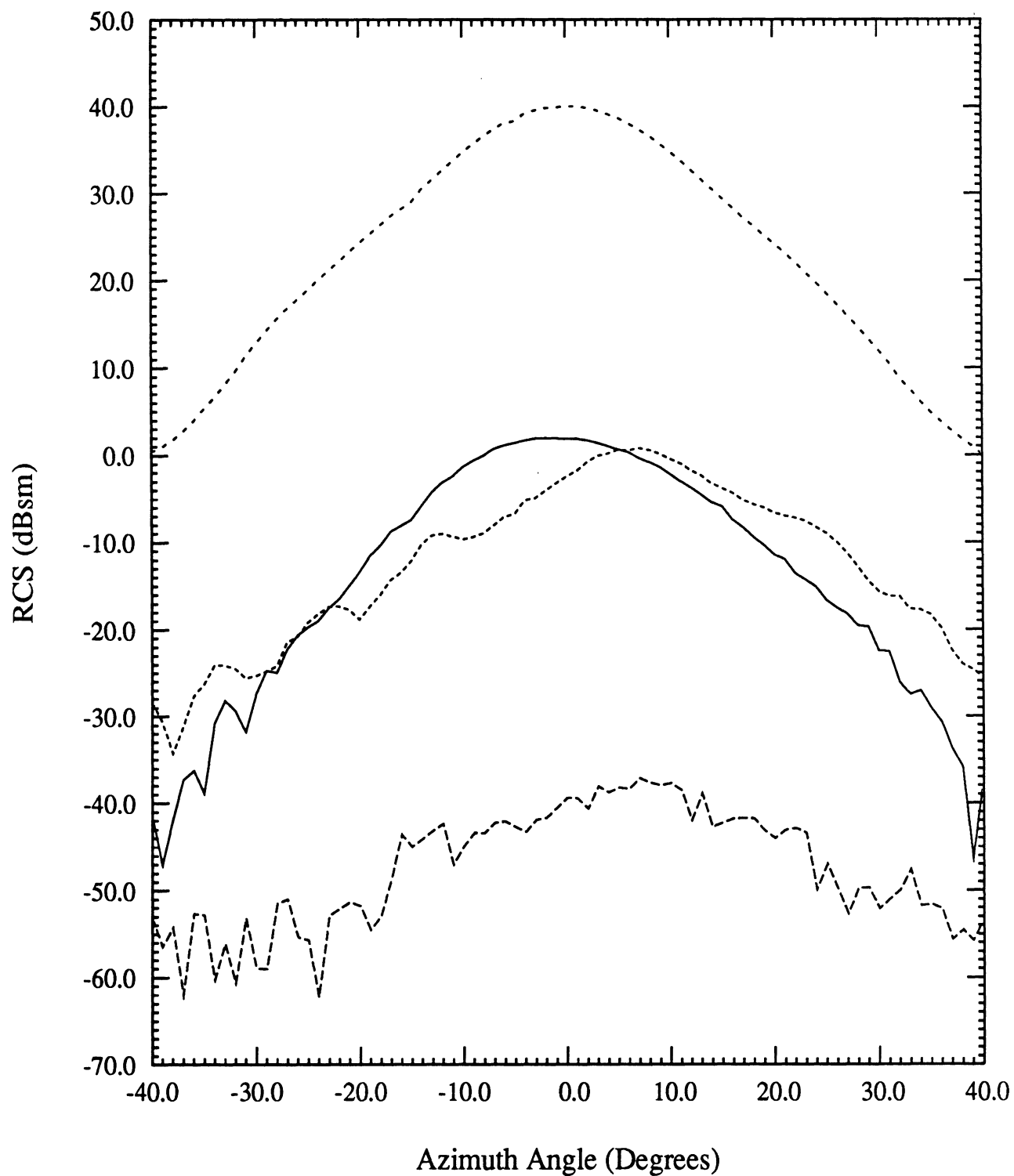
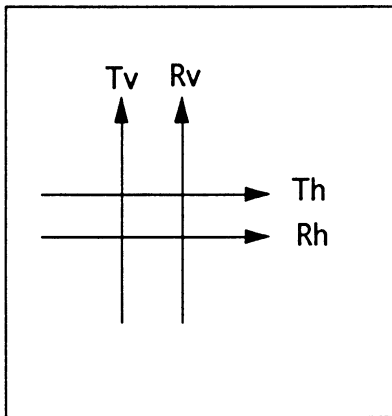


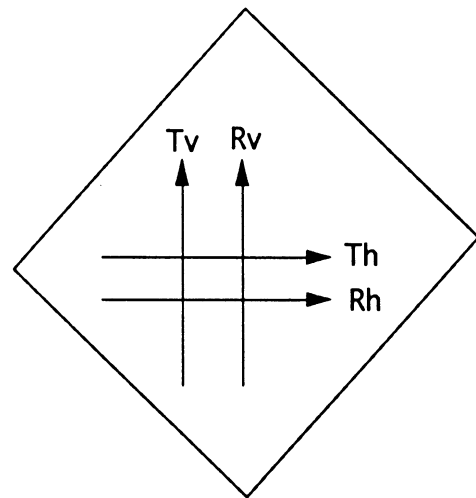
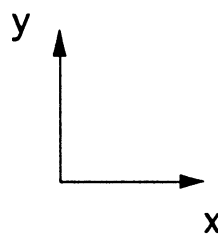
Figure 3.8: SAPARC 0° Orientation Phasor Polarizations

Figure 3.9: SAPARC 0° Orientation RCS Azimuthal Patterns (SIR-C Mode)





Radar Antenna
Polarizations



SAPARC Antenna
Polarizations

- Tv: Transmit Vertically Polarized Wave Component
- Rv: Receive Vertically Polarized Wave Component
- Th: Transmit Horizontally Polarized Wave Component
- Rh: Receive Horizontally Polarized Wave Component

Figure 3.10: SAPARC 45° Orientation Phasor Polarizations

Figure 3.11: SAPARC 45° Orientation RCS Azimuthal Patterns (SIR-C Mode)

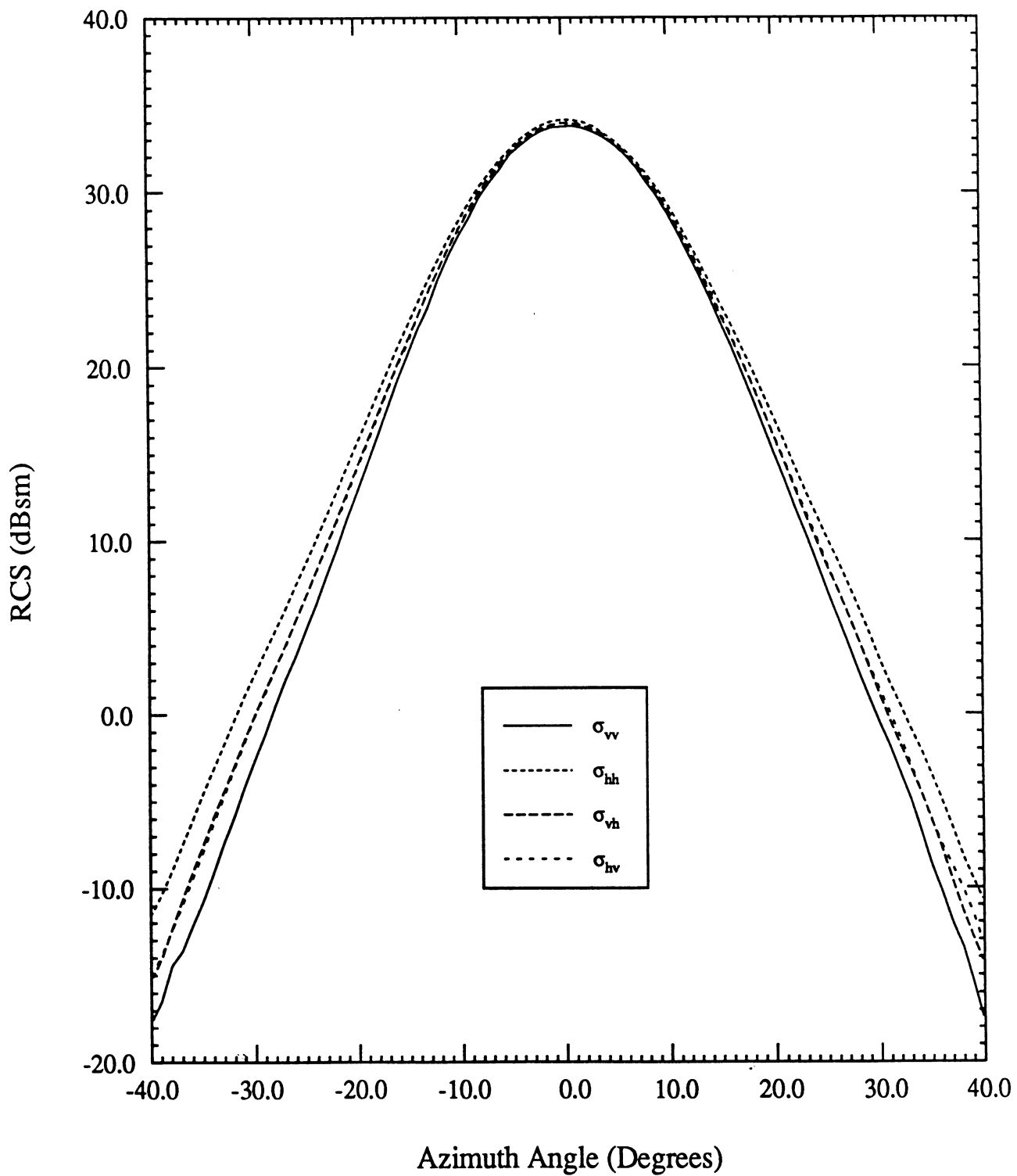
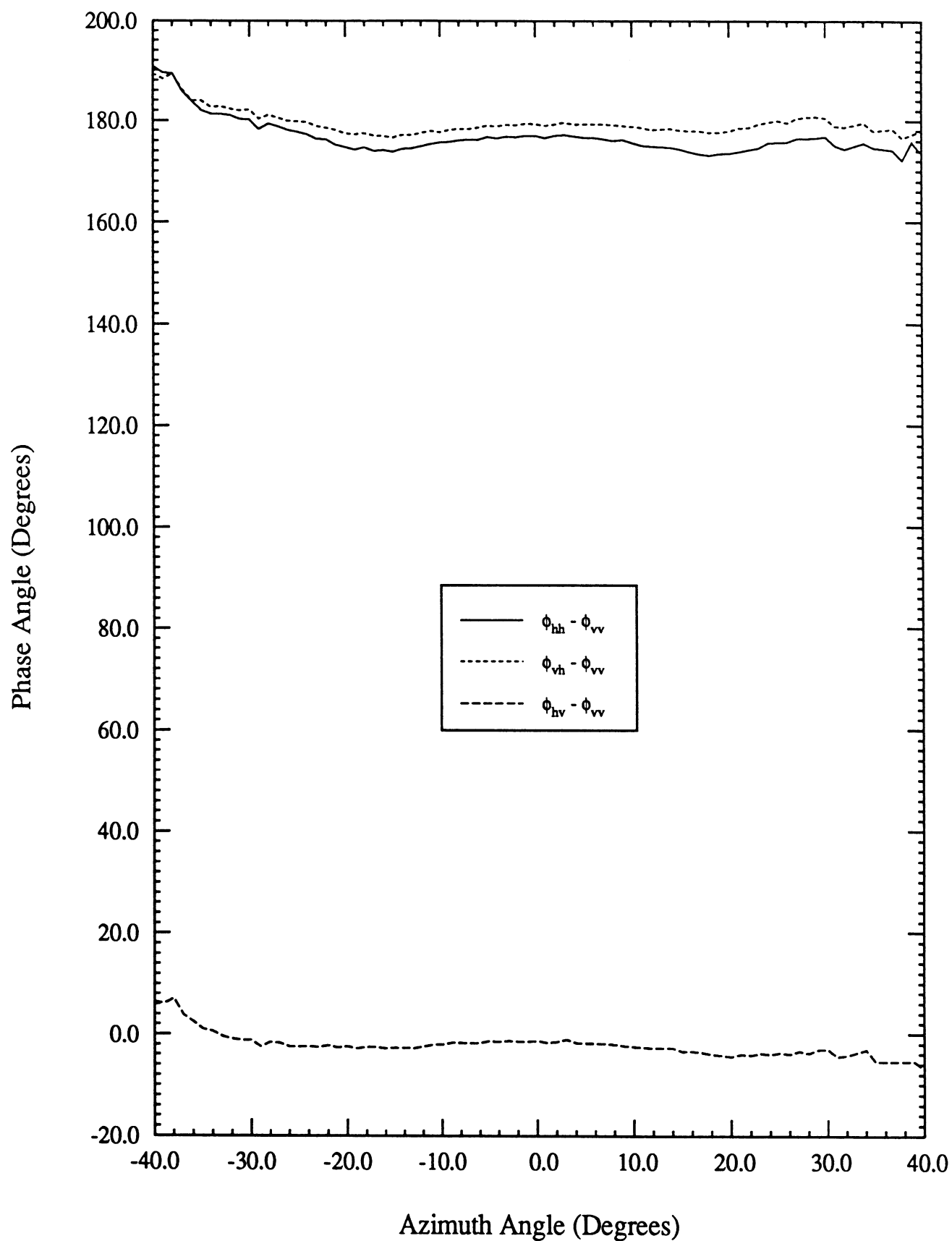
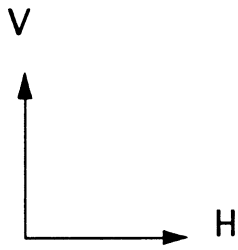
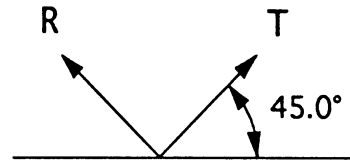
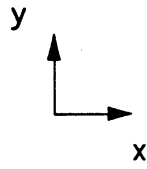


Figure 3.12: SAPARC 45° Orientation Phase Patterns (SIR-C Mode)





Radar Antenna

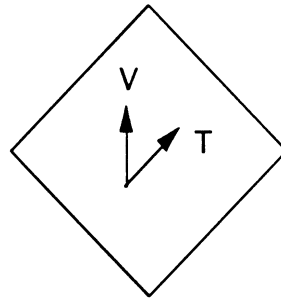
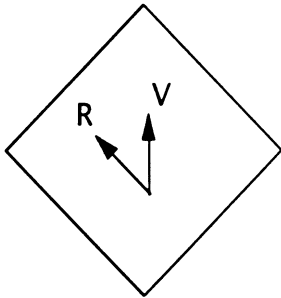


SAPARC Antenna

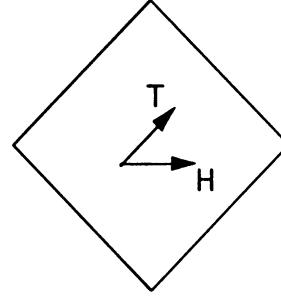
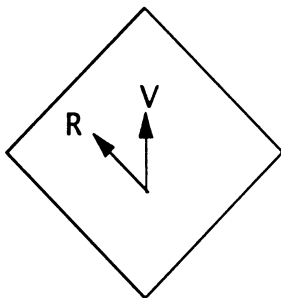
SAPARC Receive

SAPARC Transmit

ϕ_{vv}



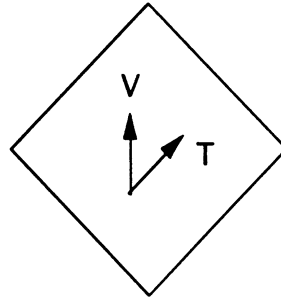
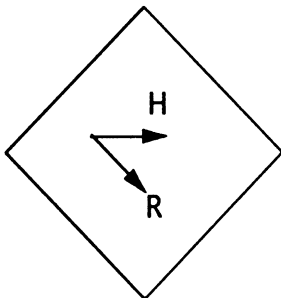
ϕ_{hv}



$$\phi_{hv} - \phi_{vv} = 0^\circ$$

R Component In Phase
T Component In Phase

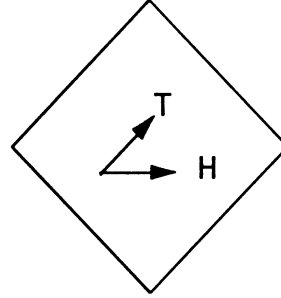
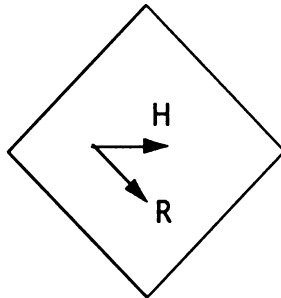
ϕ_{vh}



$$\phi_{vh} - \phi_{vv} = 180^\circ$$

R Component 180° Out of Phase
T Component In Phase

ϕ_{hh}



$$\phi_{hh} - \phi_{vv} = 180^\circ$$

R Component 180° Out of Phase
T Component In Phase

Figure 3.13: Phasor Diagrams for the 45° Orientation

The phase responses shown in Figure 3.12 are also noteworthy. Theoretically, we expect

$$\phi_{hv} - \phi_{vv} = 0^\circ$$

$$\phi_{hh} - \phi_{vv} = \phi_{vh} - \phi_{vv} = 180^\circ$$

over an 80° beamwidth. The phase diagrams in Figure 3.13 help to explain these results.

Section 2.2 referred to the drawbacks encountered when using a two-antenna PARC system; more specifically, these problems include pattern asymmetry and ripples in the phase and magnitude responses. Figure 2.3 is an example of one two-antenna system tested by Sarabandi and Oh [1]. By comparing Figure 2.3 with those in Figures 3.11 and 3.12, one can easily see the notable SAPARC improvements in magnitude and phase performance.

3.3 Thermal Gain Testing

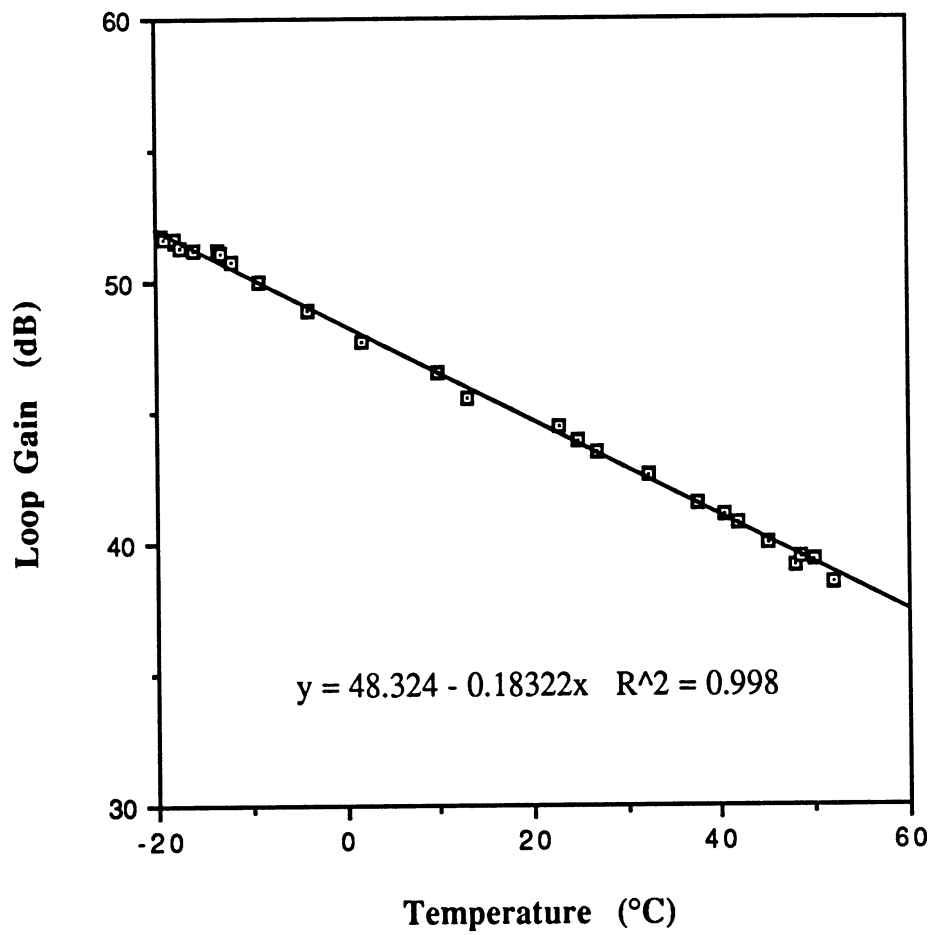
Section 2.5 alluded to the fact that PARC's are susceptible to gain variations due to changes in the ambient temperature. Countering these thermal gain variations is a formidable task; therefore, it is much easier to compensate for the changes in the SAPARC's RCS by mapping the G_{Loop} dependency on ambient temperature.

The thermal gain tests were performed at ERIM (Environmental Research Institute of Michigan) where a temperature-controllable refrigerator could be obtained. Figure 3.14 reflects the results of the experiment whereby G_{Loop} is plotted over a temperature range of -20°C to 50°C .

The user of the device must remember, however, that component aging may alter the overall performance of G_{Loop} . Therefore, periodic calibrations of G_{Loop} vs. temperature is recommended.

As a final note, special precautions must be taken when operating the SAPARC in cold weather scenarios. Currently, the system is configured to provide the

Figure 3.14: C-Band SAPARC Thermal Gain Variations



maximum allowable RCS for temperatures of 20°C or greater (see section 2.3.3). However, Figure 3.14 clearly shows how G_{Loop} can increase by as much as 7 dB for temperatures below 20°C. Therefore, the user is encouraged to use the JPL AIRSAR mode of operation whenever cold operating temperatures are anticipated. Recall that the AIRSAR mode uses a microwave switch to insert 7 dB of attenuation into the loop, thereby providing the needed cold weather protection against feedback oscillations.

3.4 Field Deployment Conditions

3.4.1 Battery Capacity

The SAPARC units developed through this project require two 12V, 7 Amp•H lead acid batteries. The power demands on Supply 2 (see Appendix C, pg. 1) is given as follows:

<u>SAPARC Operating Condition</u>	<u>Current Draw</u>	<u>Power Demand</u>
Timing Circuitry On	0.37 A	4.44 W
System Active	1.09 A	13.08 W
System Active with LED Display On	1.20 A	14.40 W

Table 3.4: Power Demands on Supply 2

Figure 3.15 (1 A case) depicts the capacity performance of the Yuasa 12V battery used in the SAPARC design. Figure 3.16 shows the results for the full load case (i.e. a current draw of 1.2 A). Under full load conditions, the SAPARC can operate (at temperatures above 20°C) for up to 5.5 hours; longer operating times are achievable when using the Activation Timers.

Figure 3.17 shows the marked decrease in capacity during cold weather operation. During this test, the Yuasa 12V battery was subjected to a temperature of -10°C while providing a current of 1.2 amps. Under these conditions, the SAPARC's full load operating time is reduced by one hour; therefore, the user must take special precautions when planning to operate the SAPARC in cold climates.

Capacity Test: Yuasa 7.0 AH

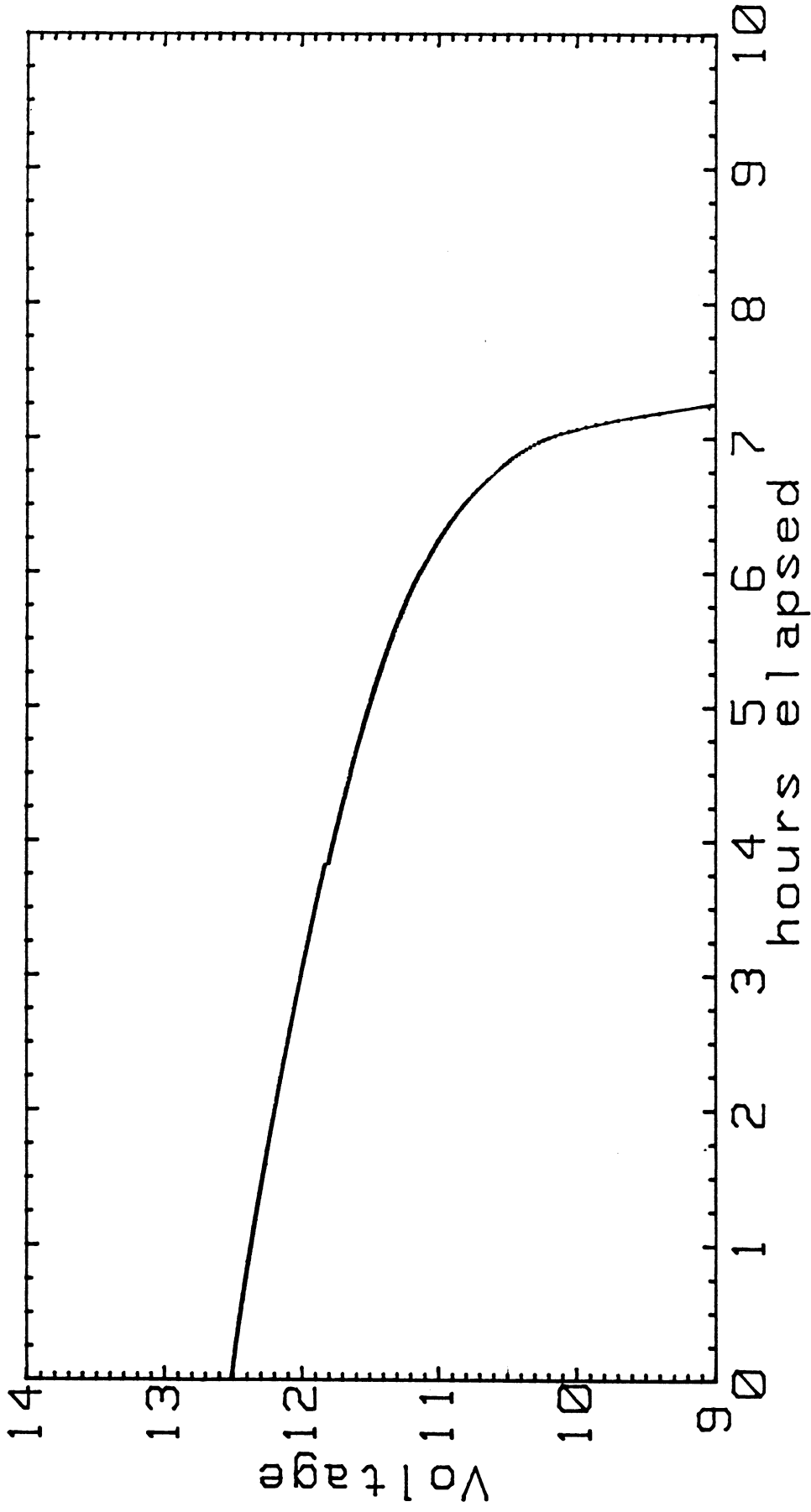


Figure 3.15: Battery Capacity Test (1.0A Load, 22°C)

Capacity Test: Yuasa 7.0 AH

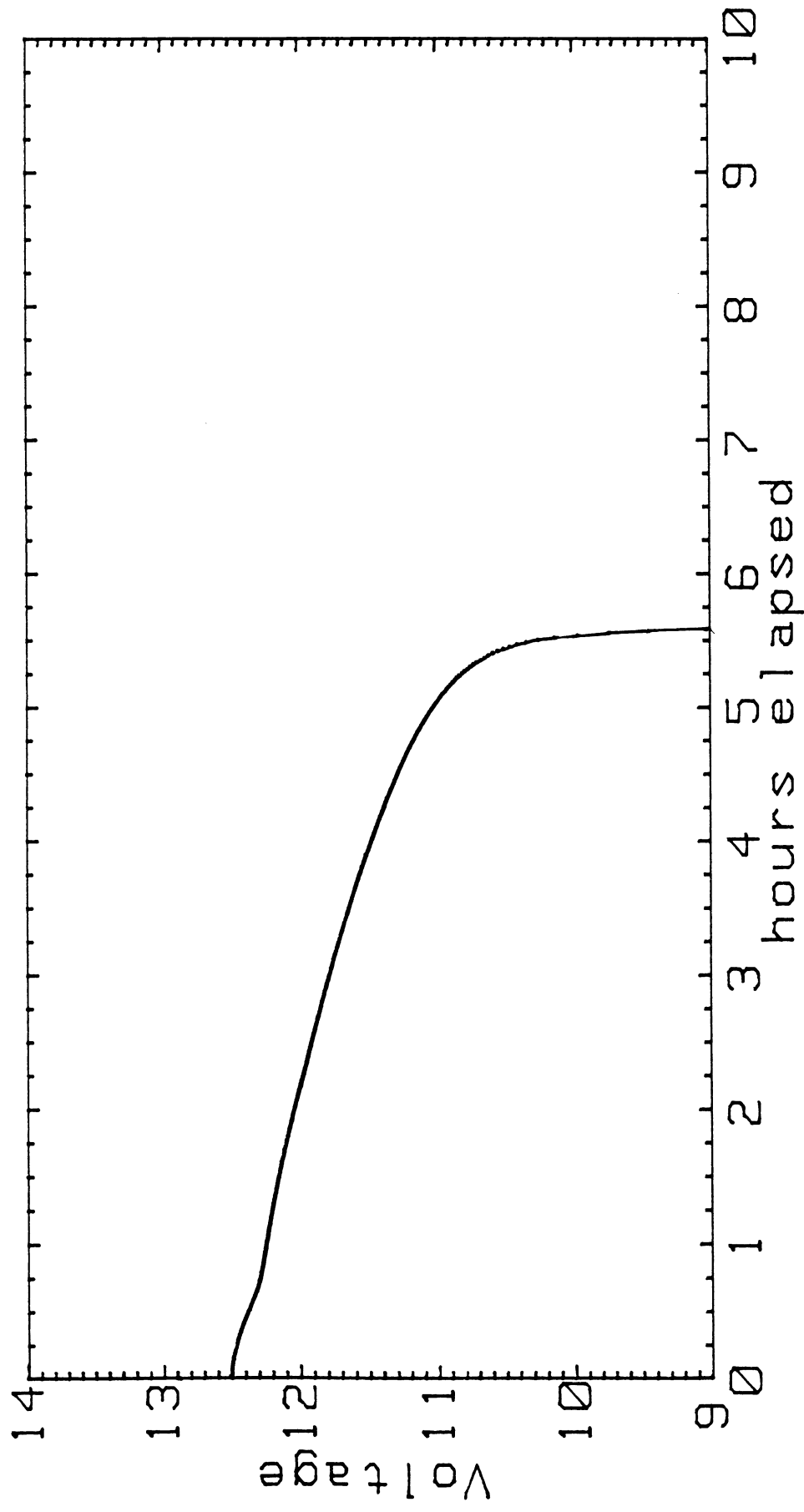


Figure 3.16: Battery Capacity Test (1.2A Load, 22°C)

Capacity Test: Yuasa 7.0 AH

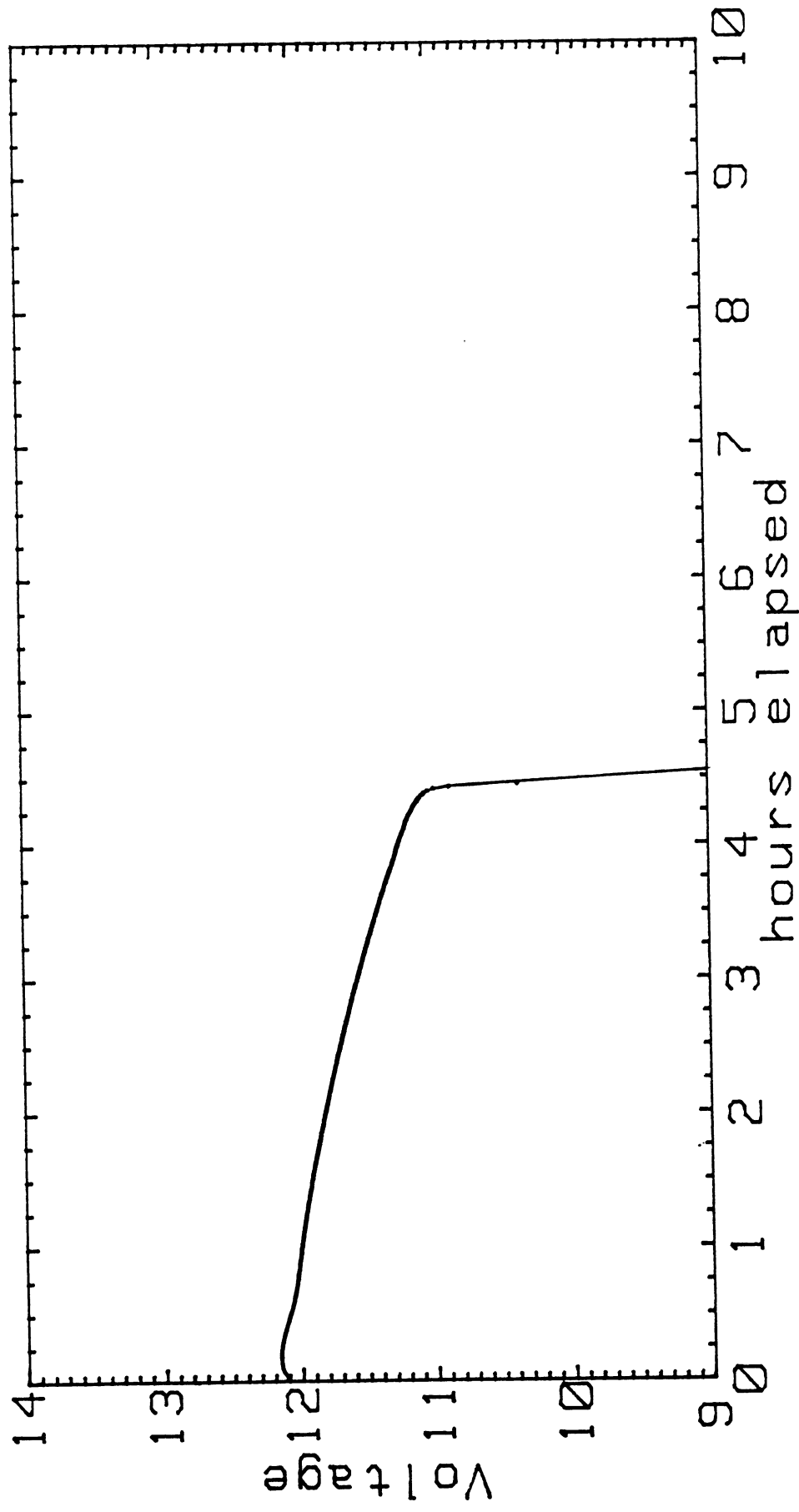


Figure 3.17: Cold Weather Battery Capacity Test (1.2A Load, -10°C)

3.4.2 All-Weather Performance

Ideally, the SAPARC can be used in all types of weather; of course, there are a number of practical limitations which concern the aperture on the horn antenna. Obviously, rain and snow can accumulate inside the horn / OMT, and thus the calibration would be ruined. In order to compensate for this occurrence, a polyethylene film (e.g. Saran Wrap) was placed over the aperture to serve as a radome. This film was very effective in keeping water out of the horn / OMT combination; however, an accumulation of water droplets on the radome eventually lead to a feedback oscillation scenario (see Sections 2.3.2.2 and 2.4.2). Therefore, applying a thin-filmed polyethylene radome is suggested for weatherproofing the horn, OMT, and waveguide adapters. Yet, do not expect the SAPARC to operate correctly in adverse weather conditions.

As a sidenote, if the rainfall ceases and the radome is allowed to dry, the SAPARC will "break-out" of its oscillation mode and return to its normal operating condition. The only notable change is that the detection circuitry will be triggered prematurely. Finally, the chassis of the SAPARC unit should be shrouded with a rain tarp to prevent excess exposure to the elements.

CHAPTER IV

CONCLUDING REMARKS

The report outlines the design and performance characteristics of the first single antenna polarimetric active radar calibrator (SAPARC) prototype developed for NASA's SIR-C mission at the University of Michigan's Radiation Laboratory. In addition to this specific unit, a second C-band and two L-band versions are currently being constructed as part of a continuation of this project.

This first C-band prototype possesses a nominal RCS of 34 dBsm with a 3 dB beamwidth of 15°. One of its best attributes, however, is the fact that it can outperform conventional PARCs through its implementation of a single dual-polarized antenna. More specifically, the pattern asymmetry and phase and magnitude ripples are eliminated through the use of this design.

In addition to these RF characteristics, the prototype is also noteworthy in that it provides a number of features which accommodate prolonged operation intervals and useful system status updates. In the future, subsequent modifications to this basic design will hopefully lead to more accurate and convenient calibrations of SAR platforms.

APPENDIX A

OMT SPECIFICATIONS

CUSTOMER UNIV OF Mich
 CUSTOMER P.O. NO. NT3622
 TESTED BY SLH
Ricky Chen

PART NO. _____
 ATL. REF. NO. 7756
 DATE 2/20/92

TEST RESULTS

ORTHOGONAL MODE JUNCTION

catalog number: 0-1370

serial number	frequency in MHz	VSWR		ISOLATION	
		H port	E port		
42	5200	A	1.10	< 1.05	50+
		B	1.11	1.06	
		C	1.06	< 1.05	
		D	< 1.05	1.06	
	5900	E	1.06	< 1.05	

serial number	frequency in MHz	VSWR		ISOLATION	
		H port	E port		
		A			
		B			
		C			
		D			
		E			

		A			
		B			
		C			
		D			
		E			

		A			
		B			
		C			
		D			
		E			

		A			
		B			
		C			
		D			
		E			

		A			
		B			
		C			
		D			
		E			

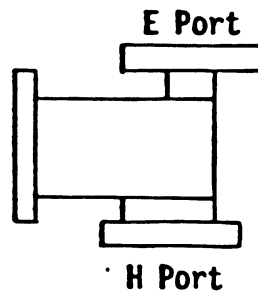
		A			
		B			
		C			
		D			
		E			

		A			
		B			
		C			
		D			
		E			

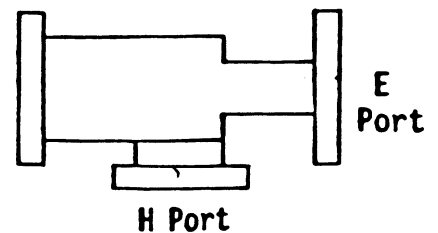
		A			
		B			
		C			
		D			
		E			

		A			
		B			
		C			
		D			
		E			

specification limits 1.15 maximum 1.15 maximum 50 dB minimum



Style 1



Style 2

E-145



APPENDIX B

AMPLIFIER SPECIFICATIONS



100 Davids Drive, Hauppauge, N.Y. 11788-2034

PROJECT No: P38858
 MODEL No: AFS5-05000560-60-8P-5
 SERIAL No: 249372
 CUSTOMER: UNIVERSITY OF MICHIGAN
 P.O. No: F33091

TEL: (516) 436-7400
 TELEX: 6718148
 FAX: 516-436-7430

IMPORTANT - MUST USE HEAT SINK IF CASE TEMPERATURE EXCEEDS 70°C

SPECIFICATIONS AT +23° C:			
FREQUENCY:	5.0 to 5.6 GHz	OUTPUT POWER @ 1dB GAIN COMPRESSION:	+8 dBm
MIN. GAIN:	40 dB	VOLTAGE:	+15 VOLTS
MAX. GAIN FLATNESS:	+/- 1 dB	MEASURED CURRENT:	150 mA
MAX. VSWR INPUT:	2 :1	MAX. NOISE FIGURE:	6.0 dB
MAX. VSWR OUTPUT:	2 :1	HOUSING No:	113110

NOTE: TEST DATA TAKEN WITH CASE TEMP. OF +23°C

FREQUENCY (GHz)	GAIN (dB)	VSWR		NOISE FIGURE (dB)	OUTPUT POWER (dBm) (@ 1dB GAIN COMPRESSION)
		IN	OUT		
5.0	44.0	1.28	1.71	1.30	+14
5.1	44.5	1.31	1.69	1.26	+14
5.2	44.6	1.32	1.65	1.39	+15
5.3	44.4	1.34	1.56	1.45	+15.5
5.4	44.2	1.35	1.50	1.61	+15
5.5	43.4	1.38	1.38	1.39	+16
5.6	42.6	1.36	1.29	1.46	+16

TESTED BY: Donald Maurice
 (DONALD MAURICE)

DATE: 06/02/92



MITEQ

Project P38859

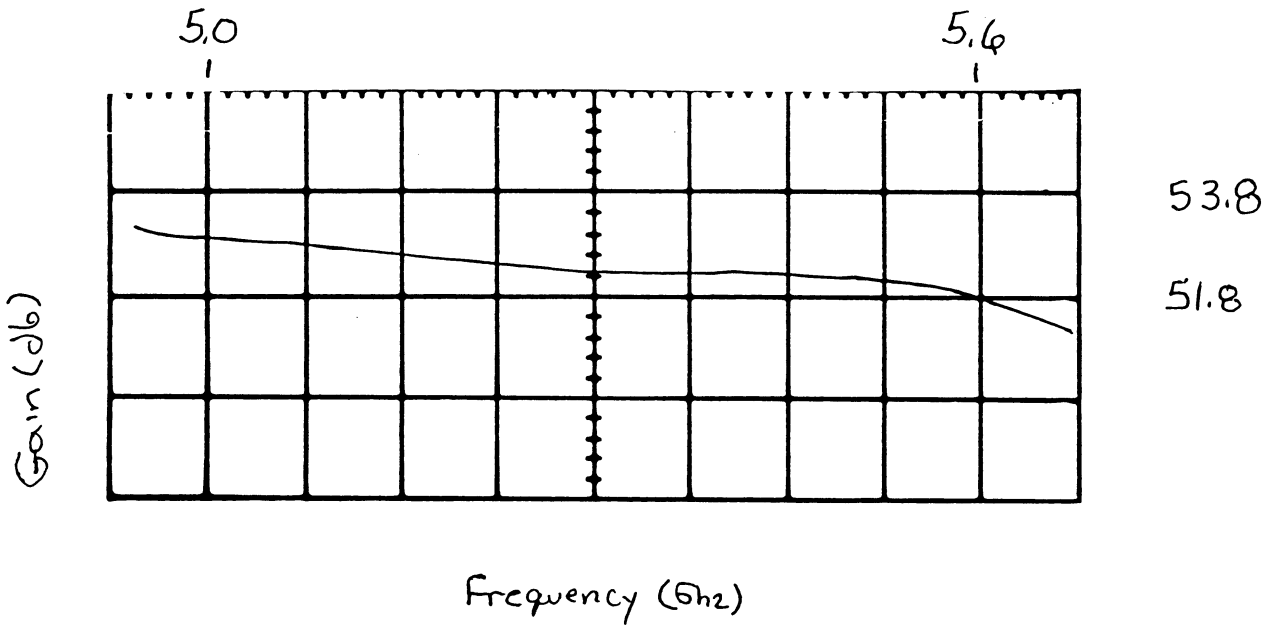
Internal Transfer _____


Customer P/N _____

Model AMF-5B-5056-29P

Serial No. 249167

GAIN BANDWIDTH



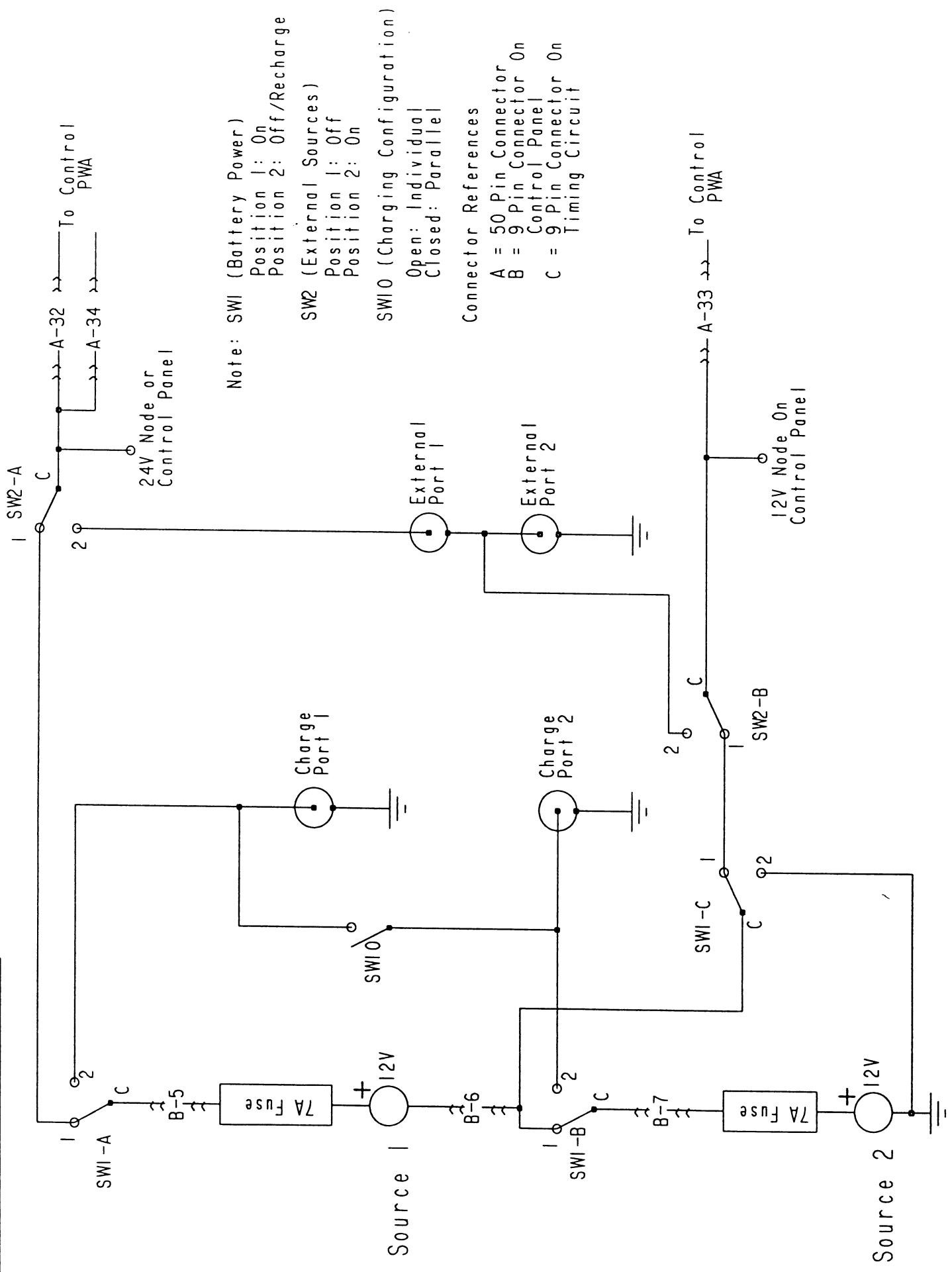
Tested By 

Date 4/6/92

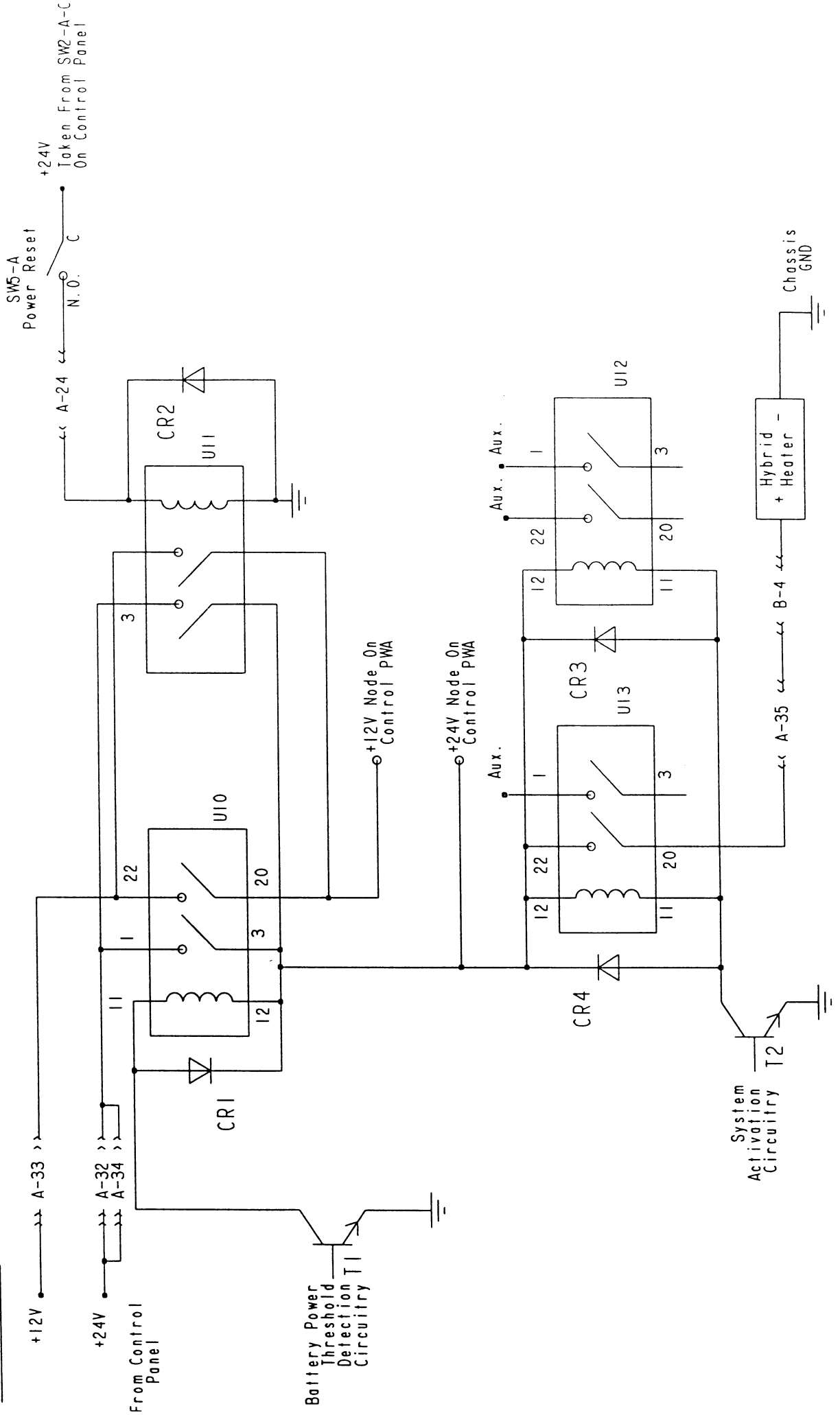
APPENDIX C

CONTROL CIRCUITRY SCHEMATICS

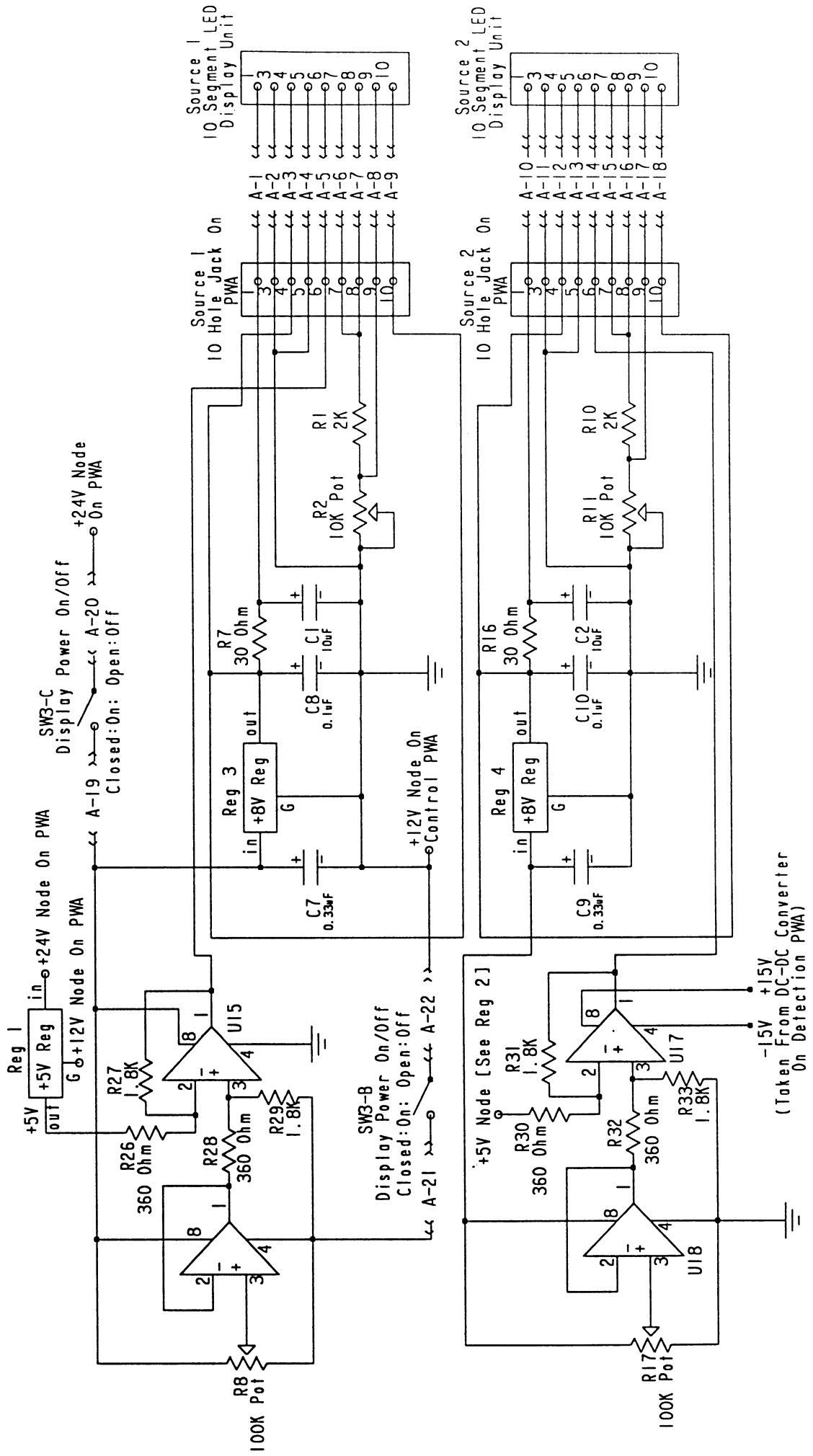
Control Panel Power Connections



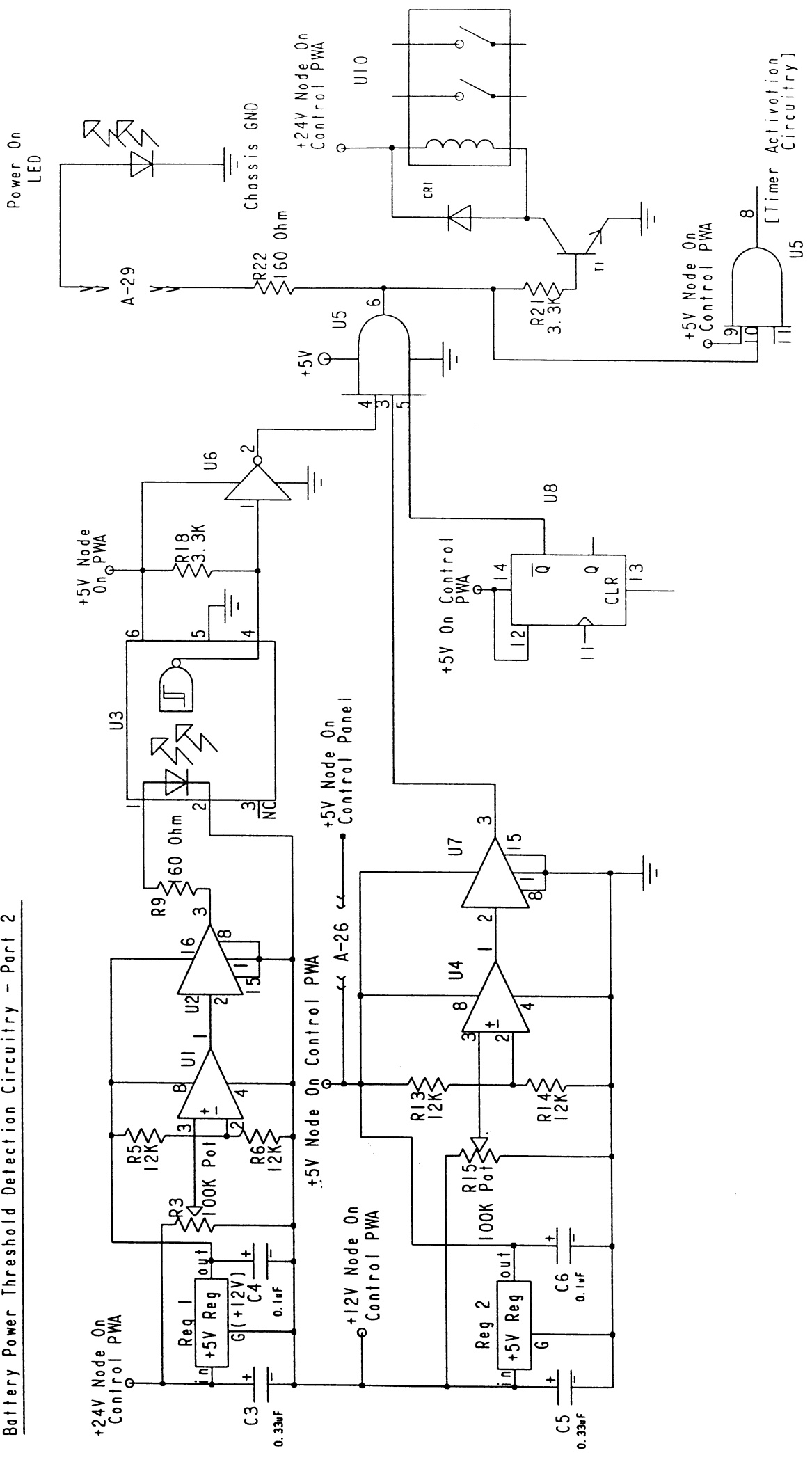
Relay Circuitry



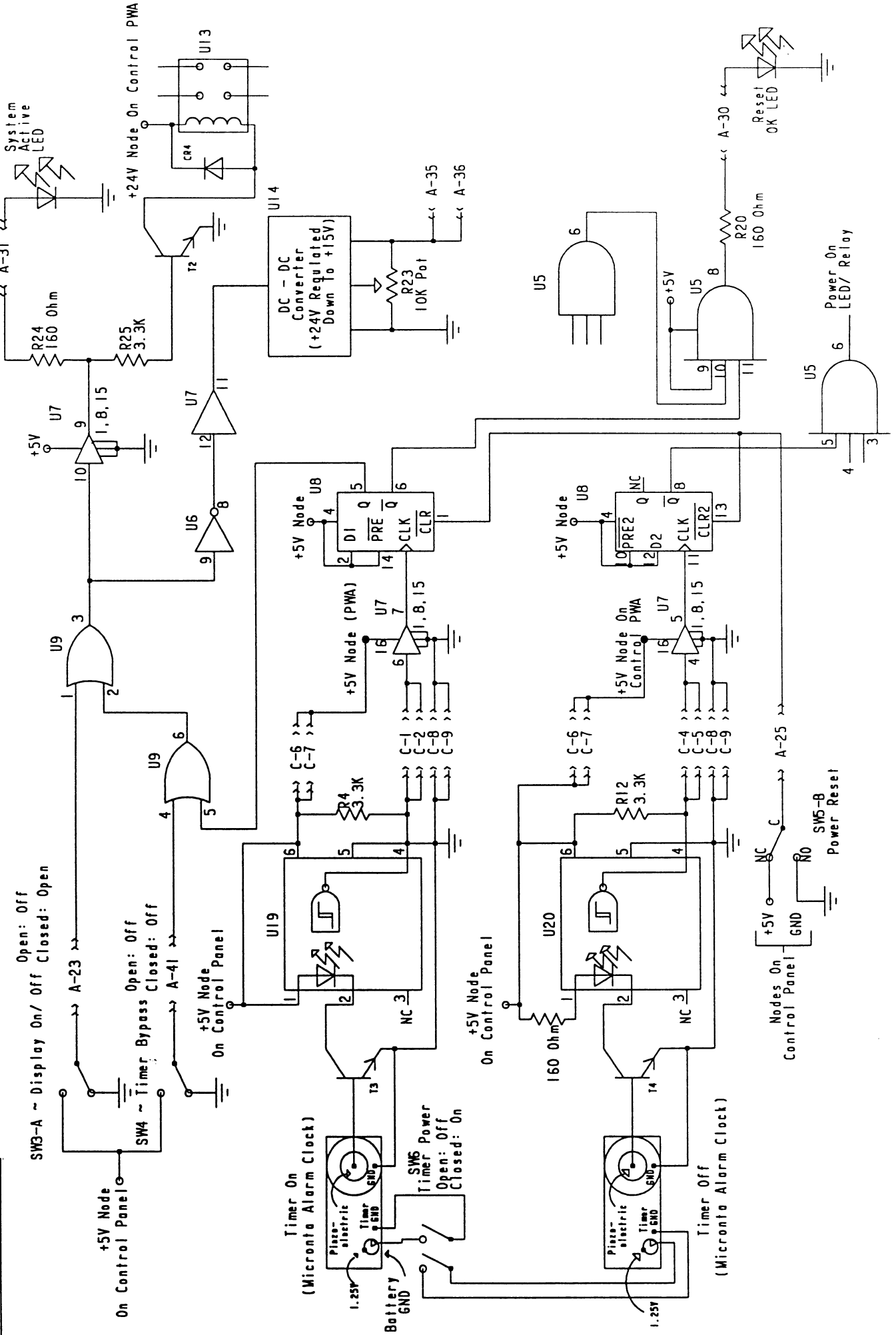
Battery Power Threshold Detection Circuitry



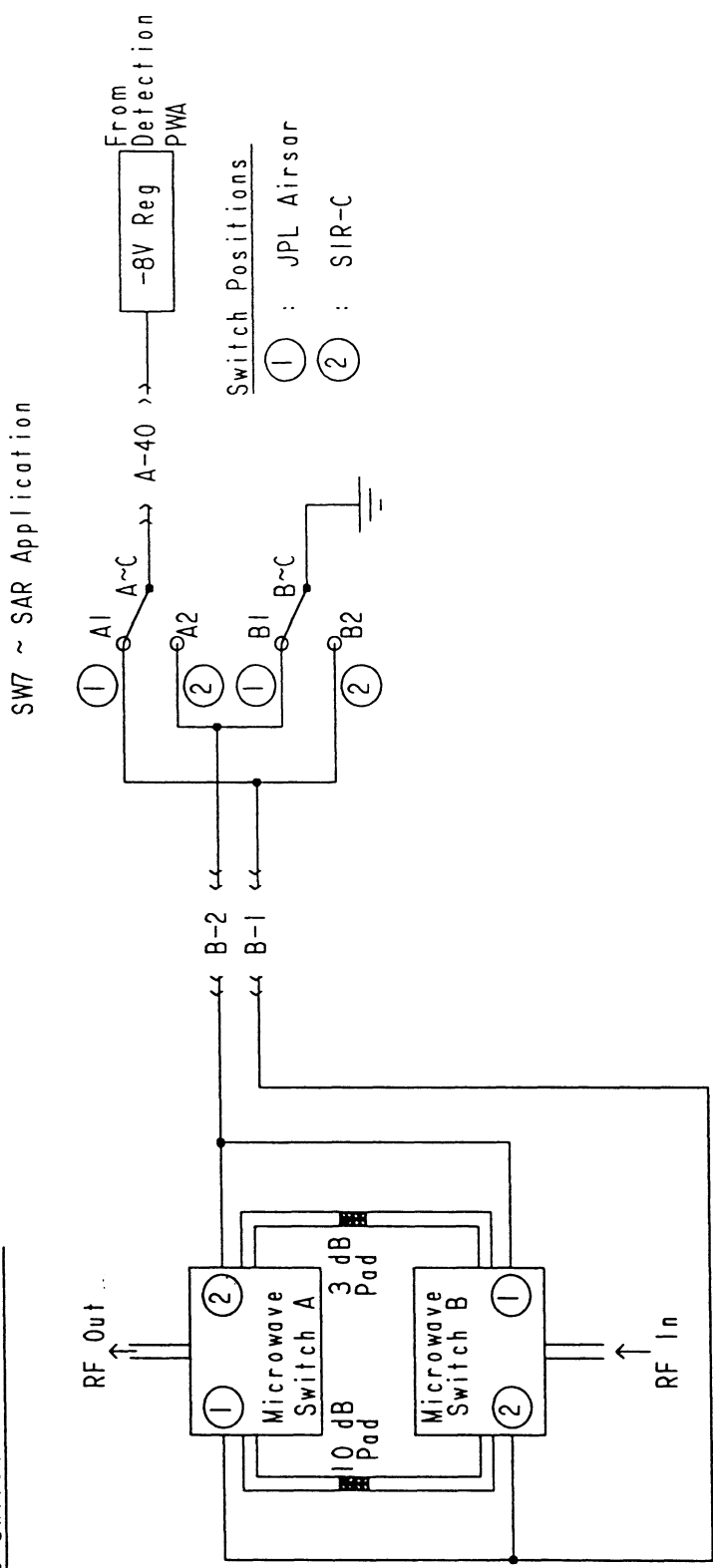
Battery Power Threshold Detection Circuitry - Part 2



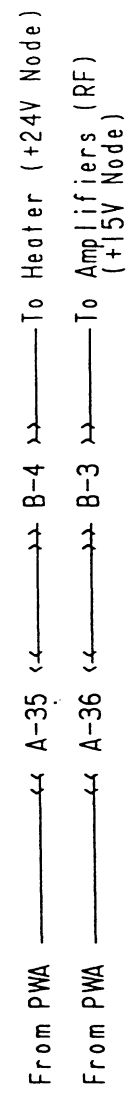
Timer Activation Circuitry



Microwave Switch Connections



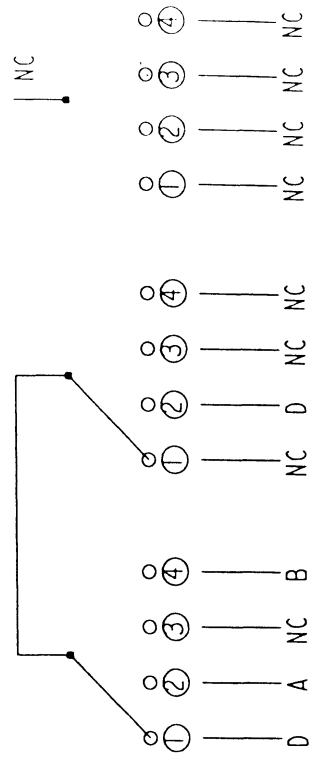
RF Amps/ Heater Connections



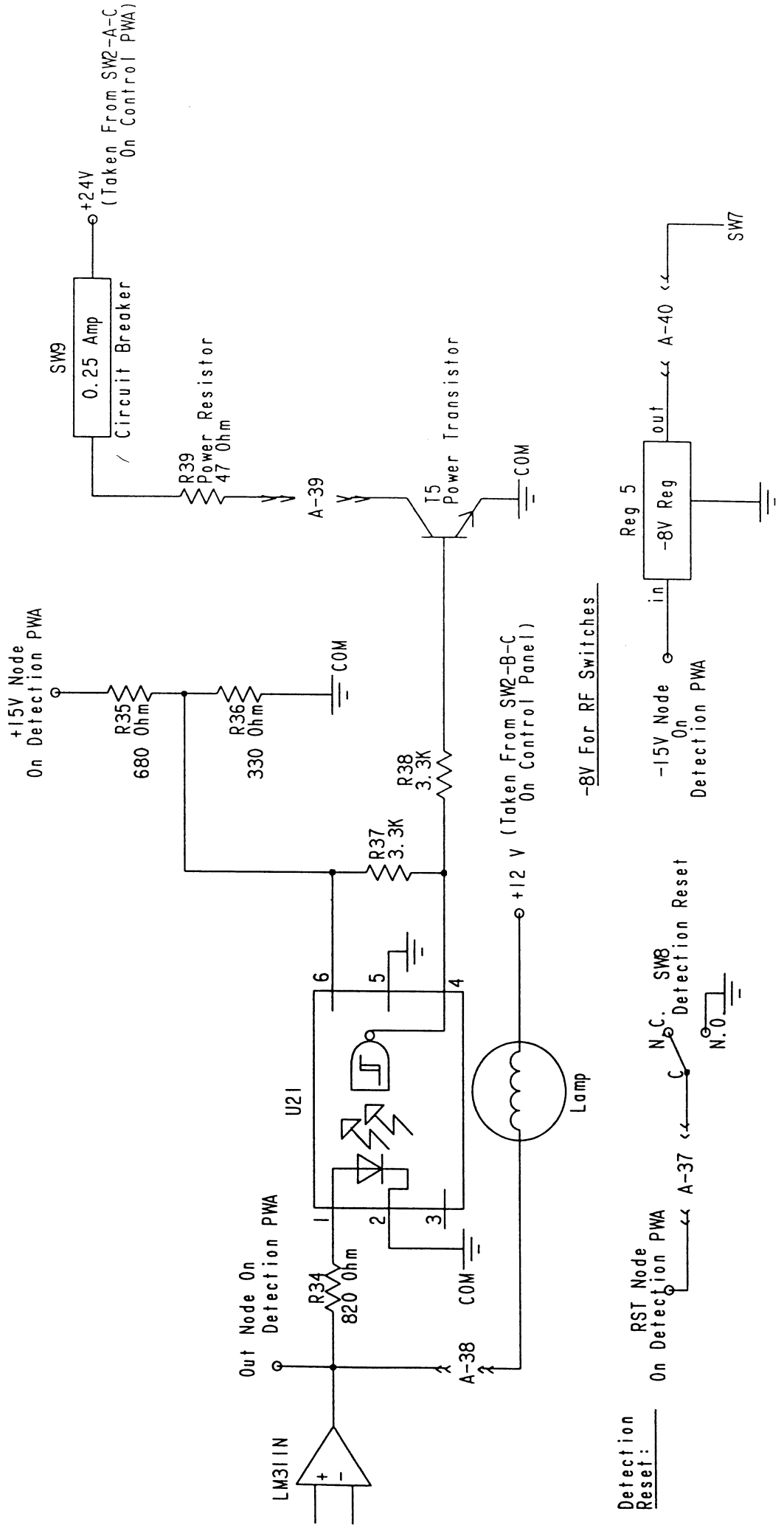
Timer Switch Replacement

Connection Pads Inside Of Timer	Positions	Function	Connected Pads	Position
A	1	Time Set	C, D	1
B	2	Alarm Set	A, C, D	2
C	3	Run - Alarm On	C	3
D	4	Run - Alarm Off	B, C	4

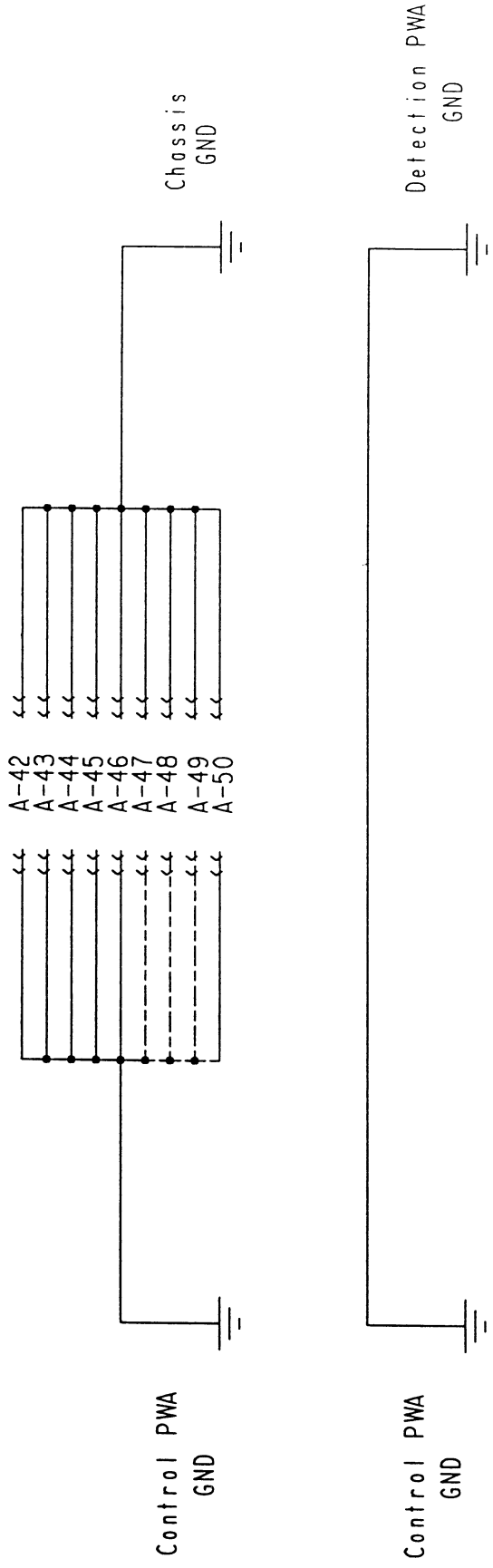
SW11 & SW12 (Timer Controls)
3 Pole - 4 Position Rotary Switch



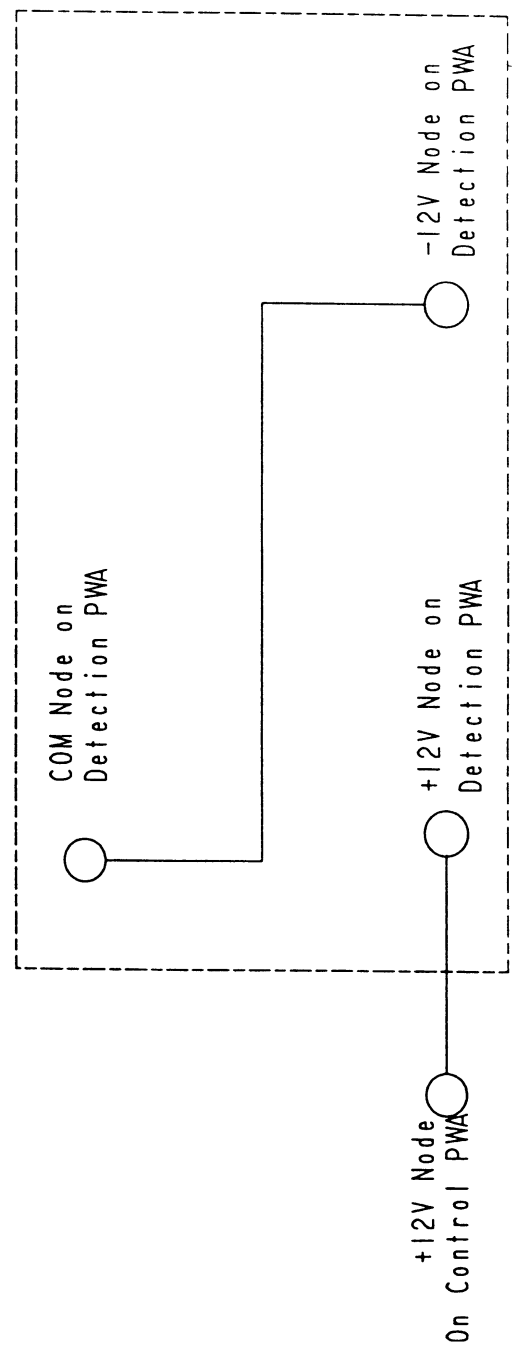
Modifications Made To Applied Microwave's Detection Circuitry



GROUND CONNECTIONS



POWER CONNECTIONS



APPENDIX D

CROSS POLARIZATION ISOLATION TESTS

14" Calibration Sphere

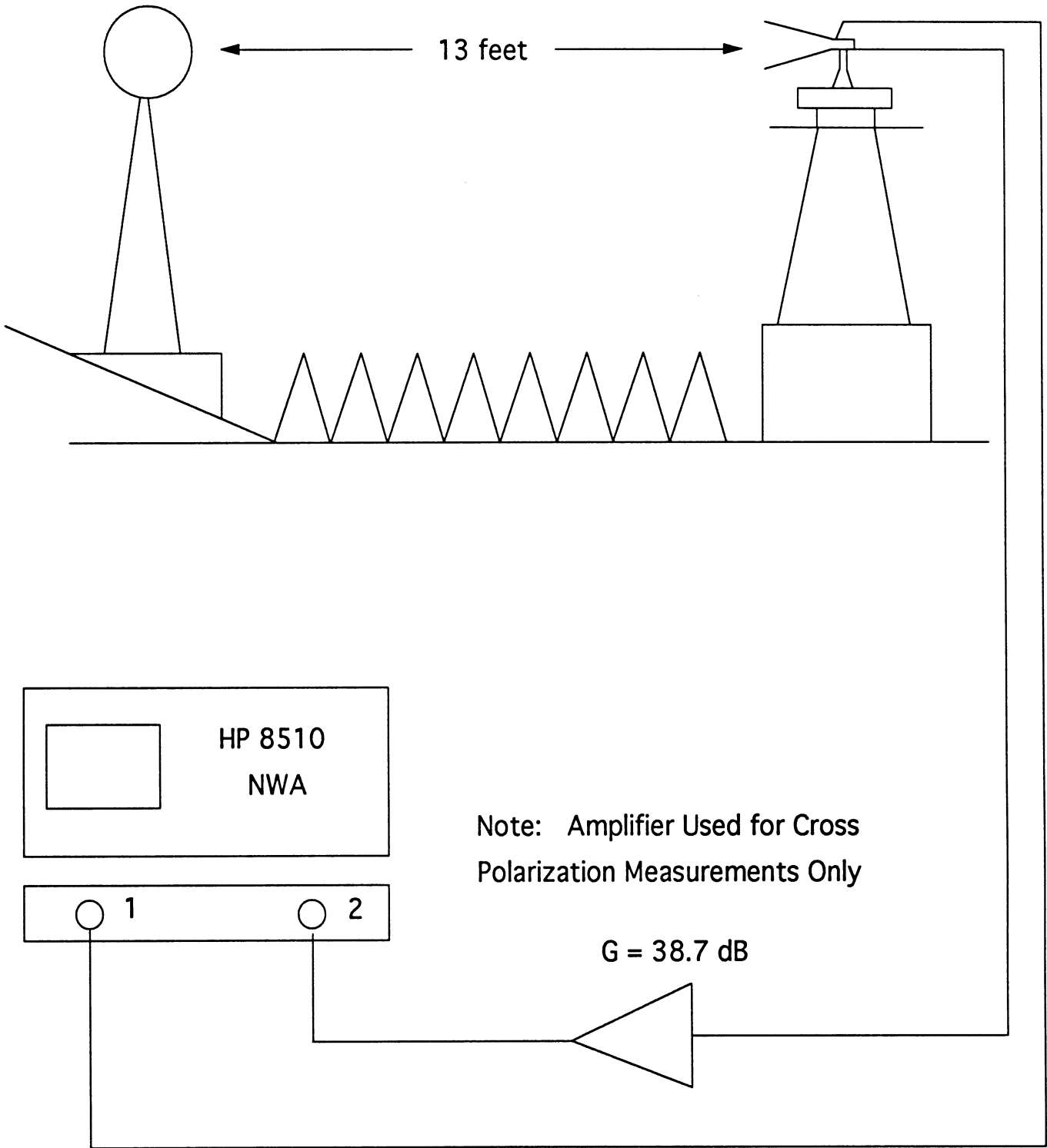


Figure D.1: Cross Polarization Isolation Test Measurements

Figure D.2a: S_{VV} Time Domain Plot of a 14" Calibration Sphere

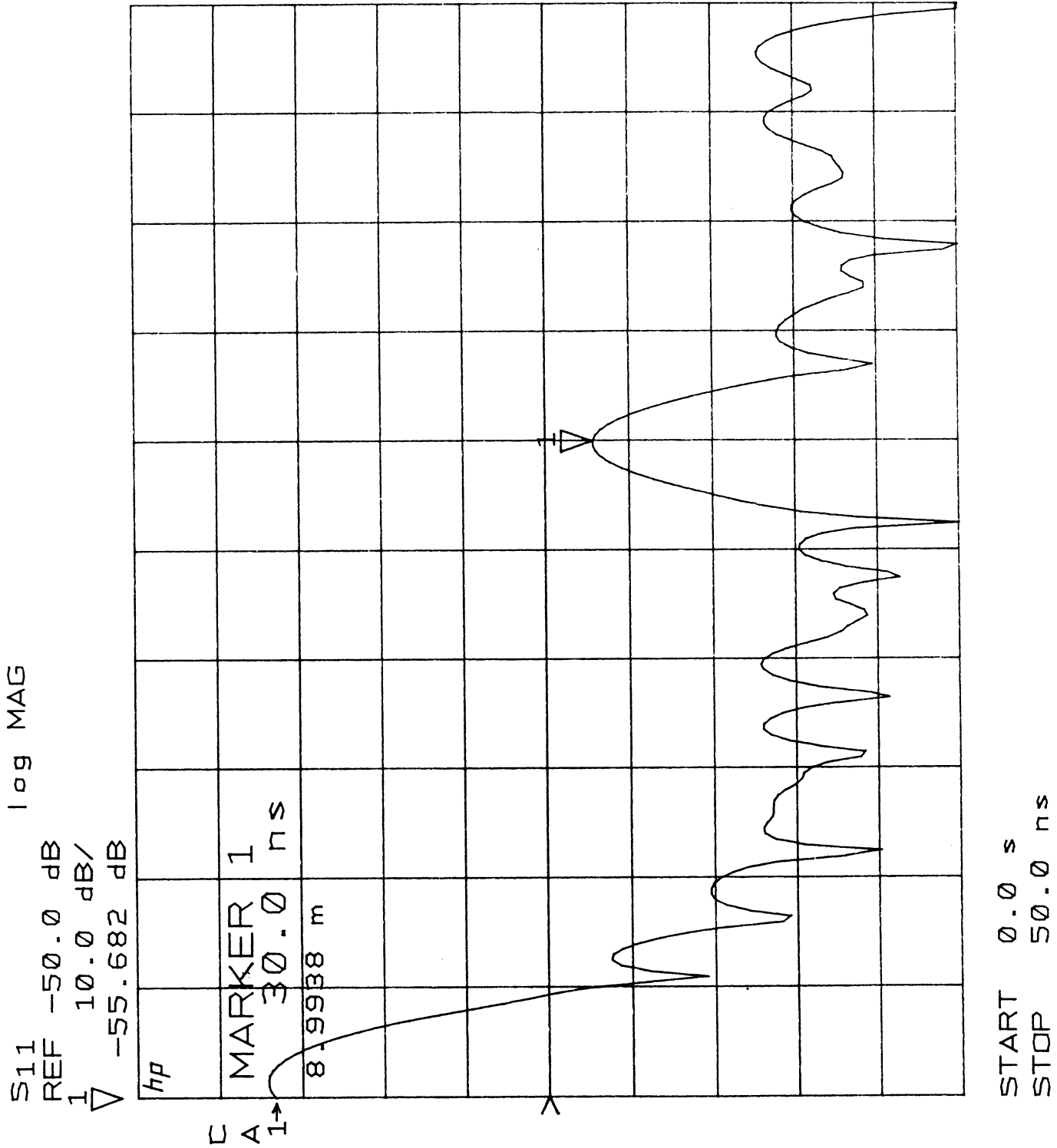


Figure D.2b: S_{VV} Frequency Domain Plot of a 14" Calibration Sphere
(With Background Subtraction)

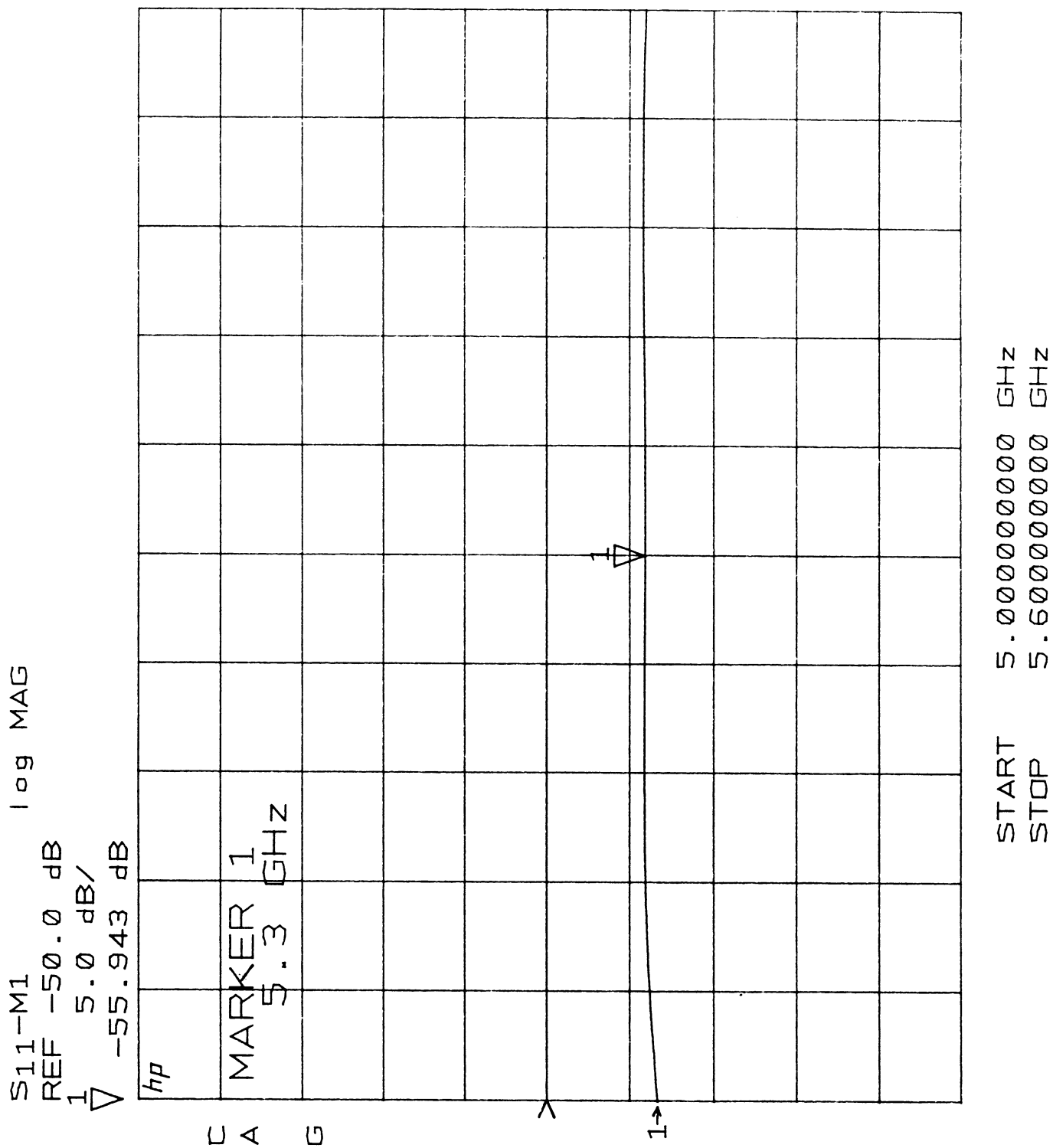


Figure D.2c: S_{hh} Time Domain Plot of a 14" Calibration Sphere

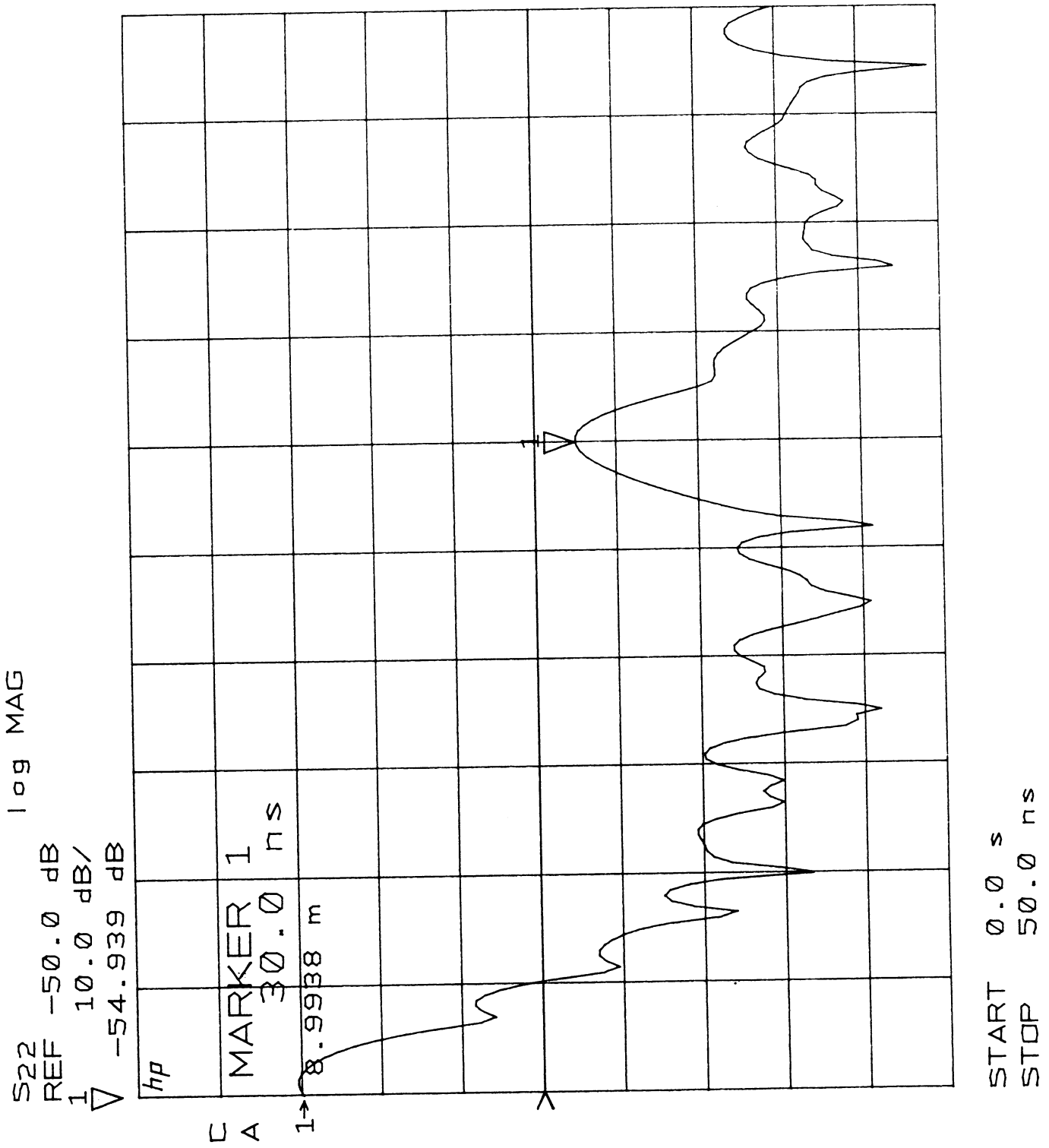


Figure D.2d: S_{hh} Frequency Domain Plot of a 14" Calibration Sphere
(With Background Subtraction)

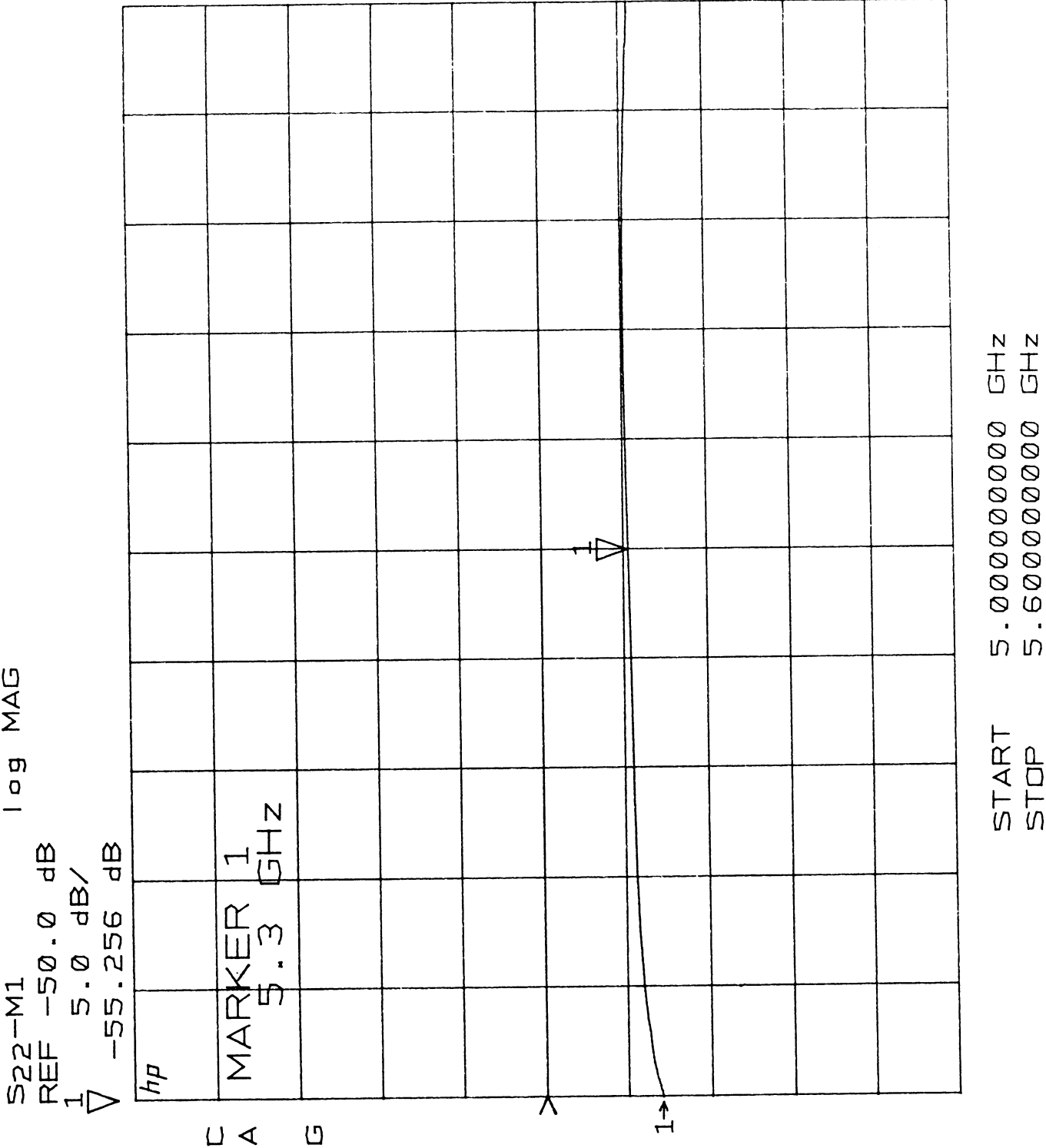


Figure D.2e: S_{hv} Time Domain Plot of a 14" Calibration Sphere

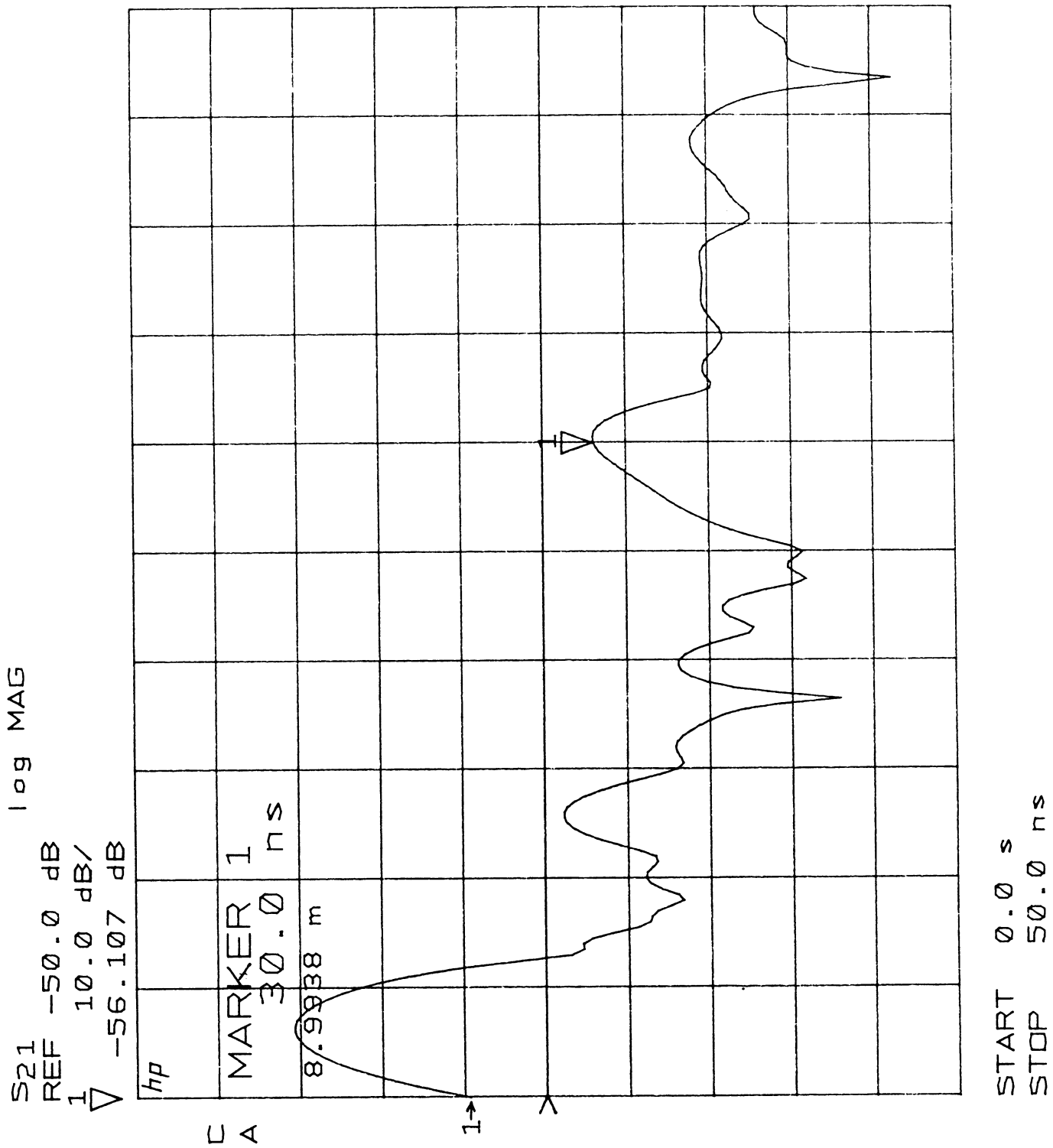


Figure D.2f: S_{hv} Frequency Domain Plot of a 14" Calibration Sphere
(With Background Subtraction)

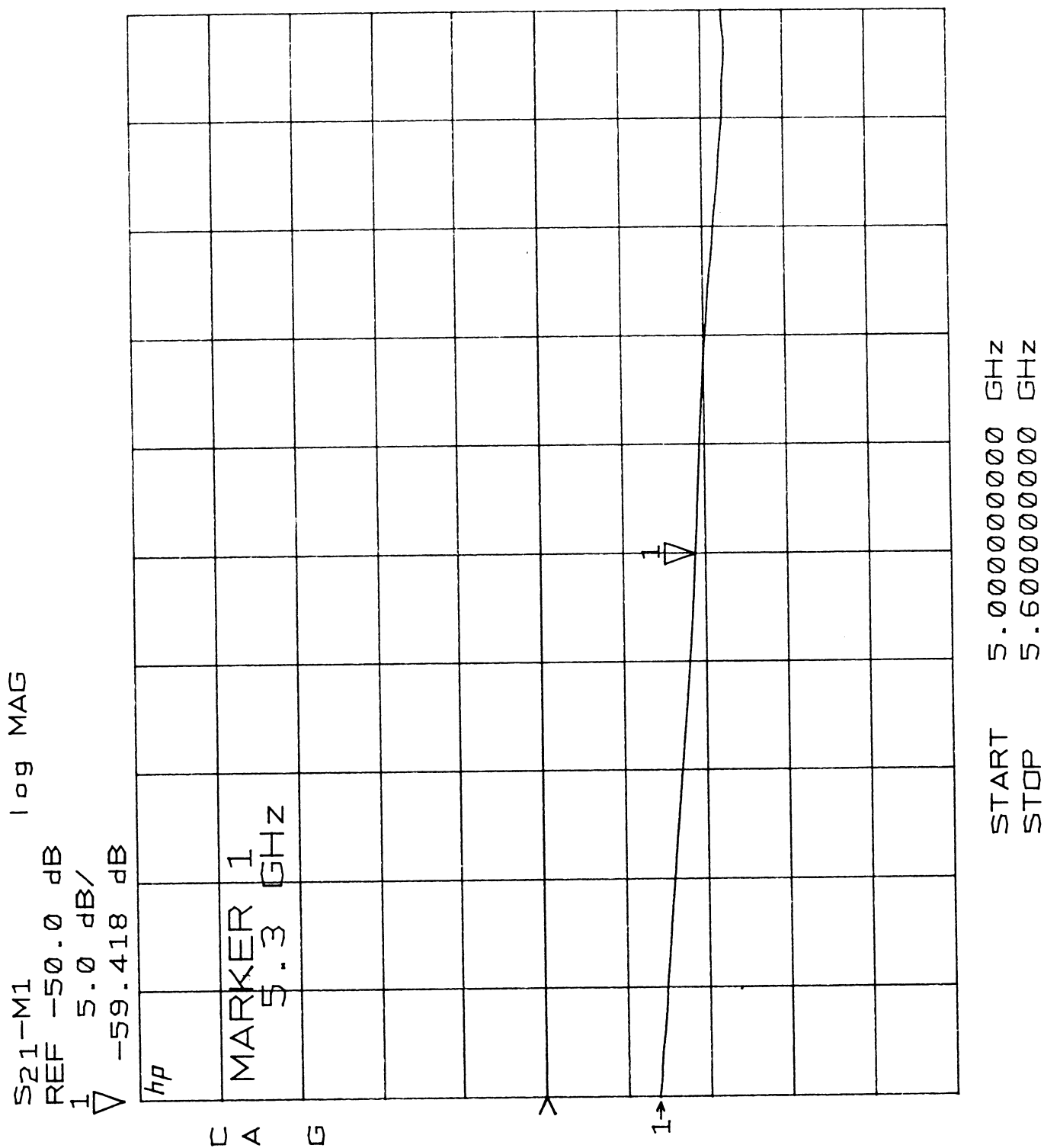


Figure D.2g: S_{vh} Time Domain Plot of a 14" Calibration Sphere

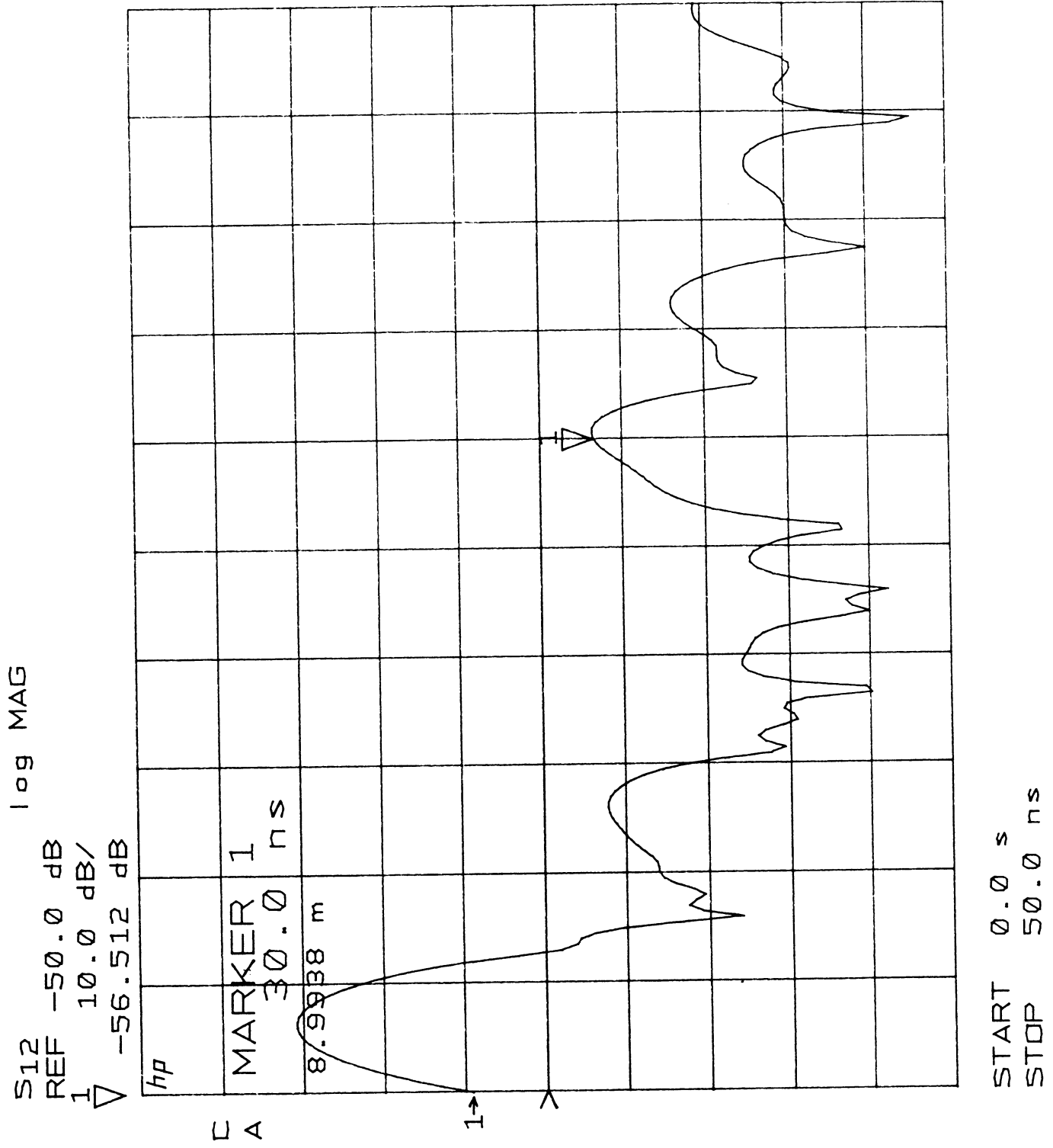
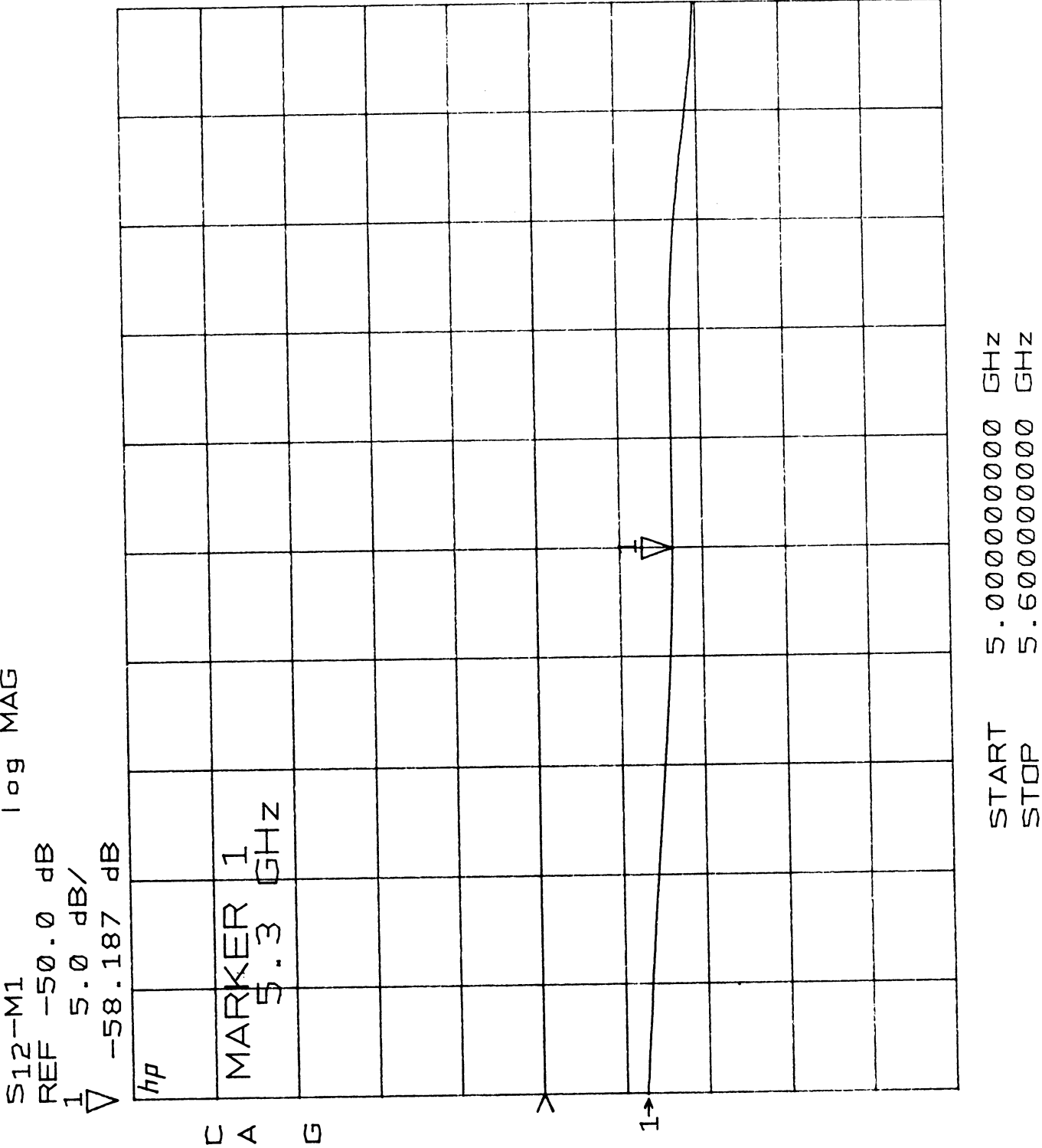


Figure D.2h: S_{vh} Frequency Domain Plot of a 14" Calibration Sphere
(With Background Subtraction)



APPENDIX E

**MEASUREMENT AND CALIBRATION
PROGRAMS**

```

C *****
C
C Appendix E
C HPUX Data File Conversion Program
C
C JPL AIRSAR / NASA SIR-C SAPARC Project
C
C James J. Ahne
C Radiation Laboratory
C Department of Electrical Engineering and Computer Science
C University of Michigan, Ann Arbor, MI 48109-2122
C *****
C
C Read raw data and write converted data for Calibration by a Sphere.
C
C COMPLEX TARGET(81,4,20)
C REAL RAW(42)
C INTEGER NPTS,NTRACE
C CHARACTER POL(4)*2
C
C DATA POL//VV','HH','HV','VH'/
C
C Read raw real data and convert to complex data for calculation.
C
C OPEN(1,FILE='152319gc')
C NP=4
C NPTS=20
C NTRACE=81
C DO 10 IT=1,NTRACE
C DO 10 IP=1,NP
C READ(1,*) (RAW(K),K=1,NPTS*2)
C DO 14 J=1,NPTS
C J2=J+2-1
C TARGET(IT,IP,J)=CMPLX (RAW (J2),RAW (J2+1))
C 14
C 10 CONTINUE
C
C CLOSE(1)
C
C Open files for outputs.
C
C OPEN(10,FILE='cparc_sirc_45saf')
C
C DO IT=1,NTRACE
C DO IP=1,NP
C WRITE(10,*)'NT=' ,IT,'POL=' ,POL(IP)
C DO I=1,NPTS
C WRITE(10,*)TARGET(IT,IP,I)
C ENDDO
C ENDDO
C
C CLOSE(10)
C
C STOP
C END
C *****
C
C FUNCTION PHASE(Z)
C *****

```

```

COMPLEX Z
PI=4.*ATAN(1.)
X=REAL(Z)
Y=AIMAG(Z)
PHASE=(180./PI)*ATAN2(Y,X)
RETURN
END

```

C

```

C *****
C Appendix E
C Scatterometer Calibration Program
C
C JPL AIRSAR / NASA SIR-C SAPARC Project
C
C James J. Ahne
C Radiation Laboratory
C Department of Electrical Engineering and Computer Science
C University of Michigan, Ann Arbor, MI 48109-2122
C *****
C (THIS PROGRAM CALIBRATES THE SCATTERMETERS USING THE NEW METHOD)
C
C COMPLEX C,A,A11,A12,A21,A22
C COMPLEX EVV0(20),EHH0(20),EVH0(20),EVM0(20)
C COMPLEX EVVM(20),EHM(20),EVHM(20),EVM(20)
C COMPLEX EVVS(150,20),EHS(150,20),EHVS(150,20),EHSV(150,20)
C COMPLEX EVVU(150,20),EHU(150,20),EVHU(150,20),EHVU(150,20)
C COMPLEX S11(150,20),S22(150,20),S12(150,20),S21(150,20)
C complex SIG11,SIG22,SIG12,SIG21
C character*1,char
C COMPLEX S0(20)
C open(9,file='sph_14')
C open(10,file='sph_dat.22')
C open(11,file='mnt_dat.22')
C open(12,file='sap_bg') Background Data - Not Applicable For Parc
C open(13,file='cparc_sirc_45saf')
C PI=4.*ATAN(1.)
C ndata=20
C ntrace=81
C cir=(0.6945+1.333i)/(1.994+2.424i)
C READ THEORETICAL VALUE OF SPHERE
C DO I=1,ndata
C READ(9,*)DUM,S0(I)
C ENDDO
C SPHERE DATA
C READ(10,103)
C DO I=1,ndata
C READ(10,*)evv0(I)
C ENDDO
C READ(10,103)
C DO I=1,ndata
C READ(10,*)ehh0(I)
C ENDDO
C READ(10,103)
C DO I=1,ndata
C READ(10,*)evhu(I)
C ENDDO
C DO I=1,ndata
C READ(10,*)evh0(I)
C ENDDO
C READ(11,103)
C DO I=1,ndata
C READ(11,*)evvm(I)
C EVV0(I)=EVV0(I)-evvm(I)
C ENDDO
C READ(11,103)
C DO I=1,ndata
C READ(11,*)ehhm(I)
C *****
C Ehho(I)=Ehh0(I)-ehhm(I)
C ENDDO
C READ(11,103)
C DO I=1,ndata
C READ(11,*)ehvm(I)
C Ehv0(I)=Ehv0(I)-ehvm(I)
C ENDDO
C READ(11,103)
C DO I=1,ndata
C READ(11,*)evhm(I)
C EVH0(I)=Evh0(I)-evhm(I)
C ENDDO
C do i=1,ndata
C print *,20*log10(cabs(evv0(i))),20*log10(cabs(ehv0(i))),
C 20*log10(cabs(evh0(i))),20*log10(cabs(ehh0(i)))
C enddo
C pause
C BACKGROUND DATA
C do itrace=1,ntrace
C READ(12,103)
C DO I=1,ndata
C READ(12,*)X,Y
C EHHS(ITRACE,I)=CMPLX(X,Y)
C ENDDO
C READ(12,103)
C DO I=1,ndata
C READ(12,*)X,Y
C EHVS(ITRACE,I)=CMPLX(X,Y)
C ENDDO
C READ(12,103)
C DO I=1,ndata
C READ(12,*)X,Y
C EVVS(ITRACE,I)=CMPLX(X,Y)
C ENDDO
C UNKNOWM DATA
C DO ITRACE=1,ntrace
C READ(13,103)
C FORMAT(1X)
C DO I=1,ndata
C READ(13,*)evvu(itrace,i)
C EVVU(ITRACE,I)=CMPLX(X,Y)-EVVS(ITRACE,I)
C ENDDO
C READ(13,103)
C DO I=1,ndata
C READ(13,*)ehhu(itrace,i)
C EHHU(ITRACE,I)=CMPLX(X,Y)-EHHS(ITRACE,I)
C ENDDO
C READ(13,103)
C DO I=1,ndata
C READ(13,*)evhu(itrace,i)
C EVHU(ITRACE,I)=CMPLX(X,Y)-EHVS(ITRACE,I)
C ENDDO
C READ(13,103)
C DO I=1,ndata
C READ(13,*)evhu(itrace,i)
C EVHU(ITRACE,I)=CMPLX(X,Y)-EVHS(ITRACE,I)
C ENDDO
C *****

```

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calib.ftn

```

C do itrace=1,ntrace
C print *,20*alog10(cabs(evvu(ITRACE,4))),
C 20*alog10(cabs(ehvu(ITRACE,4))),
C 20*alog10(cabs(evhu(ITRACE,4))),
C 20*alog10(cabs(ehhu(ITRACE,4)))
C
C enddo
C
C This is a calibration based on cl=c2
C
C DO ITRACE=1,NTRACE
C DO I=1,Ndata
C A=EVHO(I)*EVHO(I)/(EVVO(I)*EHHO(I))
C C=(1-CSQRT(1-A))/CSQRT(A)
C A11=(EVVO(ITRACE,I)/EVVO(I))*(1+C**2)*S0(I)
C A22=(EHHU(ITRACE,I)/EHHO(I))*(1+C**2)*S0(I)
C A12=(EVHU(ITRACE,I)/EVHO(I))*(2*C)*S0(I)
C A21=(EVVO(ITRACE,I)/EVHO(I))*(2*C)*S0(I)
C S12(ITRACE,I)=(A12+C**2*A21-C*(A11+A22))/(1-C**2)**2
C S21(ITRACE,I)=(A21+C**2*A12-C*(A11+A22))/(1-C**2)**2
C S11(ITRACE,I)=(A11+C**2*A22-C*(A12+A21))/(1-C**2)**2
C S22(ITRACE,I)=(A22+C**2*A11-C*(A12+A21))/(1-C**2)**2
C ENDDO
C PRINT *,ITRACE
C ENDDO
C open(15,file='cparc_sirc_am_45af')
C open(16,file='cparc_sirc_ph_45af')
C
C The variable I now sets the frequency (for 20 data points,
C use I=10 -- chooses the center frequency)
C I=10
C
C print*,input psi'
C read*,psi
C psi=psi*3.1415/180.
C sig11=s11(41,10)*cos(psi)**2-sin(psi)*cos(psi)*(s12(41,10)
C +s21(41,10))+s22(41,10)*sin(psi)**2
C sig22=s11(41,10)*sin(psi)**2+sin(psi)*cos(psi)*(s12(41,10)
C +s21(41,10))+s22(41,10)*cos(psi)**2
C sig12=sin(psi)*cos(psi)*(s11(41,10)-s22(41,10))-sin(psi)**2
C +s21(41,10)+cos(psi)**2*s12(41,10)
C sig21=sin(psi)*cos(psi)*(s11(41,10)-s22(41,10))-sin(psi)**2
C +s12(41,10)+cos(psi)**2*s21(41,10)
C print*,cabs(sig11),cabs(sig22),cabs(sig12),cabs(sig21)
C read*,jnk
C if(jnk.eq.0)goto 10
C
C angmax=40.0
C angmin=-40.0
C print*, ntrace
C dang=(angmax-angmin)/(ntrace-1)
C do itr=1,ntrace
C ang=angmin+(itr-1)*dang
C
C sig11=s11(itr,i)*cos(psi)**2-sin(psi)*cos(psi)*(s12(itr,i)
C +s21(itr,i))+s22(itr,i)*sin(psi)**2
C sig22=s11(itr,i)*sin(psi)**2+sin(psi)*cos(psi)*(s12(itr,i)
C +s21(itr,i))+s22(itr,i)*cos(psi)**2
C sig12=sin(psi)*cos(psi)*(s11(itr,i)-s22(itr,i))-sin(psi)**2
C +s21(itr,i)+cos(psi)**2*s12(itr,i)
C sig21=sin(psi)*cos(psi)*(s11(itr,i)-s22(itr,i))-sin(psi)**2
C +s12(itr,i)+cos(psi)**2*s21(itr,i)
C s11(itr,i)=sig11
C s22(itr,i)=sig22

```

```

C
C s12(itr,i)=sig12
C s21(itr,i)=sig21
C WRITE(15,*)ANG,10.*ALOG10(4.*PI*cabs(S11(ITR,I))**2)
C ,10.*ALOG10(4.*PI*cabs(S22(ITR,I))**2)
C ,10.*ALOG10(4.*PI*cabs(S12(ITR,I))**2)
C ,10.*ALOG10(4.*PI*cabs(S21(ITR,I))**2)
C
C WRITE(16,*)ANG,PHASE(S22(ITR,I)/S11(ITR,I))
C ,PHASE(S12(ITR,I)/S11(ITR,I))
C ,PHASE(S21(ITR,I)/S11(ITR,I))
C
C ENDDO
C STOP
C END
C*****
C
C FUNCTION PHASE(Z)
C*****
C COMPLEX Z
C PI=4.*ATAN(1.)
C X=REAL(Z)
C Y=AIMAG(Z)
C PHASE=(180./PI)*ATAN2(Y,X)
C if(phase.lt.-100.0) phase=phase+360
C RETURN
C END

```

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27:28:45

c_parc

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*****
Appendix E
HP Basic Scatterometer Measurement Program
JPL AIRSAR / NASA SIR-C SAPARC Project
James J. Ahne
Radiation Laboratory
Department of Electrical Engineering and Computer Science
University of Michigan, Ann Arbor, MI 48109-2122
*****
10 ! *****
20 ! L/C/X POLARIMETER MEASUREMENT PROGRAM
30 ! FILE: SAPARC_4
40 ! *****
50 ! LAST EDIT: Sep 22, 1992 Change for C-Band SAPARC measurements
60 ! *****
80 OPTION BASE 1
90 COM /Paths/ @Nwa, @Nwa_data1, @Nwa_data2, Network_analyzer, @Hplb, @Relay
100 COM /Constants/ Vel, Zero(3), Exec Keys(2)
110 COM /System_config/ INTEGER Printer_flag, Debug_flag, Version$(12), Mode$(10), Out_typ
120 COM /Sys_1/ Freq$(3), Bell$(1), Targets$(30), Ref_targets$(30)
130 COM /Sys_2/ Pol$(4), Pol$(4), Polaws$(3,4), [8]
140 COM /Sys_3/ INTEGER F_disp, P_disp
150 COM /Sys_4/ Drive_a$(15), Drive_b$(15), Drive_cs(15), INTEGER Preamble, Bytes
160 COM /Sys_5/ INTEGER Nskip, Ndata
170 COM /Sys_6/ Ref_angle, Angle, Angle$(10), Beam(3), INTEGER Npts, Ntrace, Average_factor
180 COM /Sys_7/ INTEGER Meas_flag(3)
190 COM /Com4/ INTEGER Rotation_state, REAL Inc_angle, Current_angle, Start_angle, Stop_angle, Old_home_angle, INTEGER Sets_per_pos
200 COM /Status/ INTEGER SC, Connect_flg, E_flg, Debug_flg, Responses$(80)
210 !
220 !
230 INTEGER F,I,J,P,T, Meas_flag_old(3), Exit_flag, Nt, Net, Nskh, Npt
240 DIM Sky_cal_files$(3), [14], Old_target_names$(30)
250 DATA "L", "C", "X"
260 DATA "VV", "HH", "HV", "VH"
270 DATA 1.25, 1.2, 1.5
280 DATA .3, .6, .5
290 DATA 12.5, 9.0, 6.2
300 DATA "?B3456", "?A34B56", "?A4B356", "?A3B456"
310 DATA "?B3456", "?A56B34", "?A6B345", "?A5B346"
320 DATA "?A34B56", "?B3456", "?A3B456", "?A4B356"
330 DATA "1, 700, 0", "1, 700, 1", "MEMORY, 0, 7"
340 DATA 200E-9, 200E-9, 200E-9
350 DATA 10E-9, 10E-9, 10E-9
360 READ Freq$(*)
370 READ Pol$(*)
380 READ Freq_cent(*)
390 READ Freq_span(*)
400 READ Beam(*)
410 READ Polws$(*)
420 READ Drive_a$, Drive_b$, Drive_cs
430 READ Gate_cent(*), Gate_span(*)
440 PRINT Meas_flag(*)
450 ! Set up error handling routine.
460 !
470 !
480 LOAD KEY "NOKEY:MEMORY, 0, 1"
*****
490 MASS STORAGE IS "JIM_CPARC:, 700, 0"
500 !
510 !
520 ! Initialize important parameters.
530 !
540 DEG
550 Rotation_state=-1
560 Current_angle=0.
570 MAT Meas_flag= (1)
580 Mode$="FAST ACQ"
590 F_disp=2
600 P_disp=3
610 Printer_flag=0
620 !
630 HP bus init
640 IF Printer_flag=1 THEN Out_type$="PRINT/DISC"
650 !
660 Vel=2.99792458E+8
670 Ntrace=81
680 Npts=401
690 Nskip=20
700 Ndata=20
710 Average_factor=4
720 Angle$="0"
730 Angle=0
740 Ref_angle=0
750 Target$=""
760 Sound$="ON "
770 Debug_flag=0
780 Bell$=CHR$(7)
790 Exec_keys=CHR$(255) & CHR$(88)
800 Version$="Version 8.0 "
810 Exit_flag=0
820 Print_banner1
830 !
840 System_memory=VAL(SYSTEMS("AVAILABLE MEMORY"))
850 IF FNASK("INITIALIZE RAM DISK?") THEN
860 INITIALIZE Drive_cs, 0
870 INITIALIZE Drive_cs, INT((System_memory)/512)
880 ELSE
890 ASSIGN @Is it there TO Drive_cs; RETURN Out come
900 IF Outcome=0 THEN
910 CAT Drive_cs; NO HEADER, COUNT Entries
920 IF Entries=0 THEN INITIALIZE Drive_cs, 0
930 END IF
940 ASSIGN @Is it there TO *
950 END IF
960 !
970 Config and poll
980 OUTPUT @Nwa; "TIMTRANON; LOGM; CONT; "
990 OUTPUT @Nwa; "POIN401; "
1000 ! OUTPUT @Relay; "?B1256A34"
1010 Series_init
1020 !
1030 !
1040 start_loop: !
1050 !
1060 Print_banner4
1070 ON KEY 0 LABEL " ", FNTrap_level GOSUB Null
1080 ON KEY 1 LABEL " REFERENCE CAL", FNTrap_level GOSUB Ref_target
1090 ON KEY 2 LABEL " TARGET RUN ", FNTrap_level GOSUB Acq_target
1100 ON KEY 3 LABEL " SET FREQUENCY", FNTrap_level GOSUB Freq_set
1110 ON KEY 4 LABEL " ANGLE ", FNTrap_level GOSUB Set_angle
1120 ON KEY 5 LABEL " TARGET NAME ", FNTrap_level GOSUB Set_target
```

```

1130 ON KEY 6 LABEL " # OF TRACES ",FNTRAP_level GOSUB Set_traces
1140 ON KEY 7 LABEL " # OF POINTS ",FNTRAP_level GOSUB Set_points
1150 ON KEY 8 LABEL " # OF AVERAGES ",FNTRAP_level GOSUB Set_average
1160 ON KEY 9 LABEL " QUIT ",FNTRAP_level GOTO Quit_fast_acq
1170 GOSUB Allocate_matrix
1180 LOOP
1190 EXIT IF Exit_flag=1
1200 END LOOP
1210 GOSUB Deallocate_mtx
1220 Exit_flag=0
1230 GOTO_Start_loop
1240 !
1250 Null: RETURN
1260 !
1270 !-----
1280 !
1290 Ref_target: ! Acquire a reference target data set.
1300 !
1310 OFF KEY
1320 Clear_crt
1330 OUTPUT @Nwa;"TIMDTRANON; LOGM; GATEOFF;";
1340 OUTPUT @Nwa;"AUTO; ELED 100NS; STAR ONS; STOP 300NS;";
1350 PRINT TABXY(1,10);"Please point scatterometer assembly to reference target.";
1360 PRINT TABXY(1,12);"Press CONTINUE when ready..."
1370 PAUSE
1380 GOSUB Set_Gates
1390 OUTPUT @Nwa;"TIMDTRANOFF; POLA; AVERFACT";VAL$(Average_factor);";
1400 OUTPUT @Nwa;"AVEROON"
1410 INPUT "Enter the reference target angle: ",Ref_angle
1420 !
1430 ! Get the reference target response.
1440 !
1450 FOR T=1 TO Ntrace
1460 FOR F=1 TO 3
1470 IF Meas_flag(F) THEN
1480 Freq_set(F)
1490 Freq_sw(F)
1500 OUTPUT @Nwa;"GATEOFF;";
1510 OUTPUT @Nwa;"GATECENT";VAL$(Gate_cent(F));"S;";
1520 OUTPUT @Nwa;"GATESPAN";VAL$(Gate_span(F));"S;";
1530 OUTPUT @Nwa;"GATEON;";
1540 OUTPUT @Nwa;"TIMDTRANOFF;POLA;";
1550 FOR P=1 TO 4
1560 Pol_sw(F,P)
1570 OUTPUT @Nwa;"FORM3;NUMG";VAL$(Average_factor+1);";WAIT"
1580 OUTPUT @Nwa;"WAIT; OUTPPFORM;";
1590 ENTER @Nwa_data1;Preamble,Bytes,Trace(*)
1600 MAT Target_response(P,*)= Trace
1610 NEXT P
1620 FOR P=1 TO 4
1630 Nst=INT(Nt/Nskip)
1640 Target_data(T,P,Nst)=Target_response(P,Nt)
1650 NEXT T
1660 ! Get the target response.
1670 !
1680 NEXT P
1690 END IF
1700 NEXT T
1710 NEXT T
1720 Store_file(Target_data(*),"REF",FNTime_stamp,F)
1730 !
1740 ! Get the reference target mount response.
1750 !
1760 BEEP

```

```

1770 PRINT TABXY(1,10);"Please remove the reference target from its mount."
1780 PRINT TABXY(1,12);"Press CONTINUE when ready..."
1790 PAUSE
1800 Clear_crt
1810 PRINT TABXY(1,14);"Data for the mount is being collected ...."
1820 FOR T=1 TO Ntrace
1830 FOR F=1 TO 3
1840 IF Meas_flag(F) THEN
1850 Freq_set(F)
1860 Freq_sw(F)
1870 OUTPUT @Nwa;"GATEOFF;";
1880 OUTPUT @Nwa;"GATECENT";VAL$(Gate_cent(F));"S;";
1890 OUTPUT @Nwa;"GATESPAN";VAL$(Gate_span(F));"S;";
1900 OUTPUT @Nwa;"GATEON;";
1910 FOR P=1 TO 4
1920 Pol_sw(F,P)
1930 OUTPUT @Nwa;"FORM3;NUMG";VAL$(Average_factor+1);";WAIT"
1940 OUTPUT @Nwa;"WAIT; OUTPPFORM;";
1950 ENTER @Nwa_data1;Preamble,Bytes,Trace(*)
1960 MAT Target_response(P,*)= Trace
1970 NEXT P
1980 Nskh=Nskip+1
1990 FOR P=1 TO 4
2000 FOR Nt=Nskh TO Npts STEP Nskip
2010 Nst=INT(Nt/Nskip)
2020 Target_data(T,P,Nst)=Target_response(P,Nt)
2030 NEXT Nt
2040 NEXT P
2050 END IF
2060 NEXT F
2070 NEXT T
2080 Store_file(Target_data(*),"MNT",FNTime_stamp,F)
2090 Pol_sw(F_disp,P_disp)
2100 DISP "Reference target mount response saved."
2110 Exit_flag=1
2120 RETURN
2130 !
2140 !
2150 !
2160 Acq_target: !
2170 !
2180 OFF KEY
2190 Clear_crt
2200 OUTPUT @Nwa;"TIMDTRANON; LOGM; GATEOFF;";
2210 OUTPUT @Nwa;"ELED 100NS; STAR ONS; STOP 300NS;";
2220 PRINT TABXY(1,10);"Please point scatterometer assembly at surface target."
2230 PRINT TABXY(1,12);"Press CONTINUE when ready..."
2240 PAUSE
2250 GOSUB Set_Gates
2260 OUTPUT @Nwa;"TIMDTRANOFF; POLA; AVERFACT";VAL$(Average_factor);";
2270 OUTPUT @Nwa;"GATEOFF;AVEROON;";
2280 !
2290 ! Get the target response.
2300 !
2310 FOR T=1 TO Ntrace
2320 !
2330 ! Get angles
2340 !
2350 IF T=1 THEN
2360 Rotation_state=-1
2370 ELSE
2380 Rotation_state=2
2390 END IF
2400 SELECT Rotation_state

```



```

2410 CASE -0
2420 Clear crt
2430 PRINT TABXY(1,4);"When ready for measurement, press CONTINUE."
2440 BEEP
2450 PAUSE
2460 Clear crt(3,16)
2470 PRINT TABXY(1,4);"Collecting data..."
2480 CASE ELSE
2490 PRINT TABXY(1,4);"Current angle is ";Current_angle;" degrees."
2500 Rotate_target
2510 WAIT 1
2520 Clear crt(3,16)
2530 PRINT TABXY(1,4);"Collecting data ..."
2540 END SELECT
2550 FOR F=1 TO 3
2560 IF Meas_flag(F) THEN
2570 Freq_set(F)
2580 Freq_sw(F)
2590 OUTPUT @Nwa;"GATEOFF;"
2600 OUTPUT @Nwa;"GATECENT";VALS(Gate_cent(F));"S;"
2610 OUTPUT @Nwa;"GATESPAN";VALS(Gate_span(F));"S;"
2620 OUTPUT @Nwa;"GATECOON; WAIT;"
2630 PRINT Npts,Ntrace,Ndata,Nskip
2640 FOR P=1 TO 4
2650 Pol_sw(F,P)
2660 OUTPUT @Nwa;"NUMG";VALS(Average_factor);";WAIT; FORM3; OUTPFORM;"
2670 ENTER @Nwa_data1;Preamble,Bytes,Trace(*)
2680 MAT Target_response(P,*)= Trace
2690 NEXT P
2700 Nskh=Nskip+1
2710 FOR P=1 TO 4
2720 FOR Nt=Nskh TO Npts STEP Nskip
2730 Nst=INT(Nt/Nskip)
2740 Target_data(T,P,Nst)=Target_response(P,Nt)
2750 NEXT Nt
2760 NEXT P
2770 END IF
2780 NEXT F
2790 PRINT "# OF TRACES LEFT=",Ntrace-T
2800 NEXT T
2810 Store_file(Target_data*), "GND",FNTIME_stamp$,F)
2820 DISP "Surface target data saved."
2830 BEEP
2840 Rotation_state=4
2850 Rotate_target
2860 WAIT 5
2870 BEEP
2880 OUTPUT @Nwa;"CONT;";
2890 Exit_flag=1
2900 RETURN
2910 !
2920 !-----
2930 !
2940 Freq_set: GOSUB Deallocate_mtrx
2950 OFF KEY
2960 MAT Meas_flag_old= Meas_flag
2970 MAT Meas_flag= (0)
2980 !
2990 ! Exit_flag=0
3000 ! ON KEY 0 LABEL " L BAND "
3010 ! ON KEY 1 LABEL " C BAND "
3020 ! ON KEY 2 LABEL " X BAND "
3030 ! ON KEY 4 LABEL " STORE "
3040 ! ON KEY 5 LABEL "
3050 ! ON KEY 6 LABEL "
3050 ! ON KEY 7 LABEL "
3060 ! ON KEY 8 LABEL "
3070 ! ON KEY 9 LABEL " CANCEL
3080 ! LOOP
3090 ! EXIT IF Exit_flag=1
3100 ! END LOOP
3110 GOSUB Set_c
3120 GOTO store_band
3130 RETURN
3140 Set_l:
3150 Meas_flag(1)=1
3160 F_disp=1
3170 RETURN
3180 Set_c:
3190 Meas_flag(2)=1
3200 F_disp=2
3210 RETURN
3220 Set_x:
3230 Meas_flag(3)=1
3240 F_disp=3
3250 RETURN
3260 Store_band: Print_banner4
3270 Exit_flag=1
3280 GOSUB Allocate_matrix
3290 RETURN
3300 Cancel_band: !
3310 MAT Meas_flag= Meas_flag_old
3320 Exit_flag=1
3330 GOSUB Allocate_matrix
3340 RETURN
3350 !
3360 !-----
3370 !
3380 Set_angle: !
3390 INPUT "Enter measurement angle: ",Angle
3400 Angle$=VALS(Angle)&CHR$(179)&" " ! Degree sign.
3410 Print_banner4
3420 RETURN
3430 !
3440 !-----
3450 !
3460 Set_target: !
3470 LINPUT "Enter target type or name: ",target$
3480 Target$=TRIMS(Target$)
3490 Target$=Target$&RPT$( " ",30-LEN(Target$) )
3500 Print_banner4
3510 RETURN
3520 !
3530 !-----
3540 !
3550 Set_traces: !
3560 INPUT "Enter the number of traces( or angles) desired( >=3 ): ",Ntrace
3570 GOSUB Deallocate_mtrx
3580 GOSUB Allocate_matrix
3590 Print_banner4
3600 RETURN
3610 !
3620 !-----
3630 Set_points: !
3640 INPUT "Enter the number of sample points (Npts,201): ",Npts
3650 OUTPUT @Nwa;"POIN "&VALS(Npts)&";"
3660 INPUT "Enter the data points to be stored (Ndata,10):",Ndata
3670 Nskip=INT(Npts/Ndata)
3680 Bytes=16*Ndata

```

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c_parc

```

3690 Print_banner4
3700 GOSUB Deallocate_mtrx
3710 GOSUB Allocate_matrix
3720 RETURN
3730 !
3740 !
3750 !
3760 Set_average: !
3770 INPUT "Enter averaging factor: ",Average_factor
3780 Print_banner4
3790 RETURN
3800 !
3810 !
3820 !
3830 Allocate_matrix: ! Allocate storage space for data.
3840 !
3850 System_memory=VAL(SYSTEM$( "AVAILABLE MEMORY" ))
3860 Avail_traces=MIN(Ntrace,INT(System_memory-50000-3*4*16.*Npts)/(3*4*16.*Ndata))
3870 IF Avail_traces<Ntrace THEN
3880 BEEP
3890 PRINT TABXY(1,16);"Memory has capacity for only ";Avail_traces;" traces."
3900 PRINT "Press CONTINUE key to continue"
3910 PAUSE
3920 Ntrace=Avail_traces
3930 END IF
3940 ALLOCATE COMPLEX Trace(Npts),Target_response(4,Npts)
3950 ALLOCATE COMPLEX Target_data(Ntrace,4,Ndata)
3960 RETURN
3970 Deallocate_mtrx: ! Return to main program.
3980 !
3990 DEALLOCATE Target_response(*),Trace(*)
4000 DEALLOCATE Target_data(*)
4010 RETURN
4020 !
4030 !
4040 !
4050 Set_gates: ! Set gate centers and spans.
4060 !
4070 FOR F=1 TO 3
4080 IF Meas_flag(F) THEN
4090 Freq_set(F)
4100 Freq_sw(F)
4110 P=3
4120 Pol_sw(F,P)
4130 OUTPUT @Nwa;"TIMDTRANON; LOGM;"
4140 OUTPUT @Nwa;"ELED 100NS; STAR 0NS; STOP 300NS; WAIT;"
4150 OUTPUT @Nwa;"FORM3; OUTPACTI;"
4160 ENTER @Nwa;Gate_cent(F)
4170 OUTPUT @Nwa;"MARKOFF;"
4180 OUTPUT @Nwa;"CONT.;"
4190 OUTPUT @Nwa;"GATESPAN";VAL$(Gate_span(F));"S;"
4200 OUTPUT @Nwa;"GATECENT";VAL$(Gate_cent(F));"S;"
4210 OUTPUT @Nwa;"KEY41; KEY59; KEY58; KEY59;"
4220 LOCAL @Nwa
4230 DISP "Adjust gate center to suit, and press CONTINUE."
4240 PAUSE
4250 OUTPUT @Nwa;"OUTPACTI;"
4260 ENTER @Nwa;Gate_cent(F)
4270 OUTPUT @Nwa;"GATESPAN";VAL$(Gate_span(F));";"
4280 OUTPUT @Nwa;"KEY41; KEY59; KEY58; KEY4;"
4290 LOCAL @Nwa
4300 DISP "Adjust gate span to suit, and press CONTINUE."
4310 PAUSE
4320 OUTPUT @Nwa;"OUTPACTI;"
4330 !
4340 !
4350 !
4360 !
4370 !
4380 !
4390 !
4400 Quit_fast_acq: ! End of program
4410 DISP "PROGRAM EXIT"
4420 GOSUB Deallocate_mtrx
4430 LOAD KEY "EDITKEY:MEMORY,0,1"
4440 STOP
4450 END
4460 !
4470 !
4480 !
4490 !
4500 DEF FNask(Prompt$)
4510 OFF KEY
4520 DISP Prompt$;
4530 Yn$=UPC$(Yn$(1,1))
4540 SELECT Yn$
4550 CASE "Y"
4560 RETURN 1
4570 CASE "N",""
4580 RETURN 0
4590 CASE ELSE
4600 RETURN 0
4610 END SELECT
4620 FNEND
4630 !
4640 !
4650 !
4660 DEF FNFileloc$(Files$,Dir$)
4670 INTEGER C ! for the location of the ':' in Dir$ (minus 1)
4680 LET C=POS(Dir$,";")-1
4690 IF C<=0 THEN
4700 RETURN TRIM$(Files&Dir$)
4710 ELSE
4720 RETURN Dir$(1,C)&RPT$( "/" ,Dir$(C,C)<>"/" )&Files&Dir$(C+1,LEN(Dir$))
4730 END IF
4740 FNEND ! Fileloc
4750 !
4760 !
4770 !
4780 DEF FNTime_stamps(OPTIONAL Time_format)
4790 !
4800 DIM Time_digits$(4),Year_digits$(6)
4810 DIM Machine_time$(8),Machine_dates$(11)
4820 REAL Time_date_now
4830 !
4840 Time_date_now=TIMEDATE
4850 Machine_dates$=DATES$(Time_date_now)
4860 Machine_times$=TIME$(Time_date_now)
4870 Time_digits$=Machine_times$(1,2)&Machine_times$(4,5)
4880 Year_digits$(1,2)=Machine_dates$(10,11)
4890 IF Machine_dates$(1,1)=" " THEN Machine_dates$(1,1)="0"
4900 !
4910 SELECT Machine_dates$(4,6)
4920 CASE "Jan"
4930 Year_digits$(3,4)="01"
4940 CASE "Feb"
4950 Year_digits$(3,4)="02"
4960 CASE "Mar"

```

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c_parc

```
4970 Year_digits$(3,4)="-03"  
4980 CASE "-"Apr"  
4990 Year_digits$(3,4)="-04"  
5000 CASE "-"May"  
5010 Year_digits$(3,4)="-05"  
5020 CASE "-"Jun"  
5030 Year_digits$(3,4)="-06"  
5040 CASE "-"Jul"  
5050 Year_digits$(3,4)="-07"  
5060 CASE "-"Aug"  
5070 Year_digits$(3,4)="-08"  
5080 CASE "-"Sep"  
5090 Year_digits$(3,4)="-09"  
5100 CASE "-"Oct"  
5110 Year_digits$(3,4)="-10"  
5120 CASE "-"Nov"  
5130 Year_digits$(3,4)="-11"  
5140 CASE "-"Dec"  
5150 Year_digits$(3,4)="-12"  
5160 END SELECT  
5170 I  
5180 Year_digits$(5,6)=Machine_dates$(1,2)  
5190 SELECT NPAR  
5200 CASE -0  
5210 RETURN Year_digits$(5,6)&Time_digits$  
5220 CASE -1  
5230 IF Time_format=1 THEN  
5240 RETURN Year_digits&Time_digits$  
5250 END IF  
5260 IF Time_format=2 THEN  
5270 RETURN Year_digits$(3,6)&Time_digits$  
5280 END IF  
5290 END SELECT  
5300 FNEND  
5310 I  
5320 I  
5330 I  
5340 DEF FNTrap_level  
5350 RETURN VAL(SYSTEMS("SYSTEM PRIORITY")+1)  
5360 FNEND  
5370 I  
5380 I  
5390 I  
5400 SUB Config_and_poll  
5410 COM /Paths/ @Nwa,@Nwa_data1,@Nwa_data2,Network_analyzer,@Hpiib,@Relay  
5420 COM /System/ System_memory  
5430 I  
5440 I Find out what's out there.  
5450 I  
5460 ALLOCATE Device_list$(0:31) [20]  
5470 ALPHA PEN 4  
5480 KBD LINE PEN 3  
5490 KEY LABELS PEN 5  
5500 Clear_crt  
5510 Network_analyzer=0  
5520 ALLOCATE Na_ids$(80)  
5530 System_memory=VAL(SYSTEMS("AVAILABLE MEMORY")) ! How much memory for RAM-DISK  
5540 PRINT "AVAILABLE MEMORY: ";System_memory;" BYTES"  
5550 ON TIMEOUT 7,4 GOTO No_na  
5560 Is_na: OUTPUT @Nwa;"FORM4:"_OUTPIDEN;"  
5570 ENTER @Nwa_data2;Na_ids$  
5580 IF POS(Na_ids$,"8510A") THEN Network_analyzer=1  
5590 IF POS(Na_ids$,"8510B") THEN Network_analyzer=2  
5600 IF POS(Na_ids$,"8720A") THEN Network_analyzer=3  
5610 IF POS(Na_ids$,"8720B") THEN Network_analyzer=4  
5620 IF POS(Na_ids$,"8753A") THEN Network_analyzer=5  
5630 IF POS(Na_ids$,"8753B") THEN Network_analyzer=6  
5640 LOCAL @Nwa  
5650 PRINT  
5660 PRINT Na_ids$  
5670 PRINT Network_analyzer  
5680 I Clear_crt  
5690 PRINT  
5700 PRINT  
5710 IF Network_analyzer=0 THEN  
5720 I  
5730 I  
5740 No_na:  
5750 BEEP  
5760 OFF CYCLE  
5770 PRINT TABXY(1,5);"There is no active network analyzer on the HPIB bus."  
5780 PRINT TABXY(1,6);"Please check connections, and press the RUN key."  
5790 PRINT  
5800 PRINT TABXY(1,7);"If you DO NOT want to use a network analyzer, press the  
CONTINUE key."  
5810 PAUSE  
5820 END IF  
5830 I  
5840 Check_hpib: ! Check the rest of the bus  
5850 ON TIMEOUT 7,.01 GOTO Nothing  
5860 I  
5870 FOR Device=700 TO 731  
5880 DISP "Checking for device at address: ";Device  
5890 Device_list$(Device-700)="NOTHING"  
5900 ASSIGN @What_is_it TO Device  
5910 Outcome=SPOLL(@What_is_it)  
5920 Device_list$(Device-700)="SOMETHING"  
5930 PRINT Device;"SOMETHING HERE";"spoll: ";Outcome  
5940 ASSIGN @What_is_it TO *  
5950 Nothing: ! Skip to next device  
5960 NEXT Device  
5970 I  
5980 OFF TIMEOUT 7  
5990 ASSIGN @What_is_it TO *  
6000 IF Device_list$(1)="SOMETHING" THEN  
6010 DISP "Position the printer to Top-Of-Form and press CONTINUE..."  
6020 PAUSE  
6030 PRINTER IS PRT  
6040 PRINT CHR$(27)&"&llll"; ! Set Page Breaks  
6050 Printer_flag=1  
6060 PRINTER IS CRT  
6070 END IF  
6080 DEALLOCATE Na_ids$  
6090 DEALLOCATE Device_list$(*)  
6100 ABORT @Hpiib  
6110 SUBEXIT  
6120 SUBEND  
6130 I  
6140 I  
6150 I  
6160 SUB Hp_bus_init  
6170 COM /Paths/ @Nwa,@Nwa_data1,@Nwa_data2,Network_analyzer,@Hpiib,@Relay  
6180 COM /Sys.1/ Freq$(*) ,Freq_cent(*),Freq_span(*),Gate_cent(*),Gate_span(*)  
6190 COM /Sys.2/ Pol$(*) ,Polsw$(*)  
6200 COM /system_config/ INTEGER Printer_flag,Debug_flag,Version$,Modes,Out_type$,Sound$,Bell$,Target$,Ref_target$  
6210 I  
6220 I This subroutine configures the HP-IB bus and presets the HP8510.
```

```

6230 !
6240 ASSIGN @Hpb TO 7
6250 ASSIGN @Nwa TO 716
6260 ASSIGN @Nwa_data1 TO 716;FORMAT OFF
6270 ASSIGN @Nwa_data2 TO 716;FORMAT ON
6280 ASSIGN @Relay TO 710
6290 REMOTE @Hpb
6300 ABORT @Hpb
6310 CLEAR @Nwa
6320 IF Debug_flag=1 THEN OUTPUT @Nwa;"DEBUON;"
6330 IF Debug_flag=0 THEN
6340 OUTPUT @Nwa;"DEBUOFF;"
6350 OUTPUT @Nwa;"ITL ";&Freq$(2)&" BAND ***
6360 END IF
6370 SUBEND
6380 !
6390 !*****
6400 !
6410 SUB Series_init
6420 COM /System config/ INTEGER Printer_flag,Debug_flag,Out_types,Sound
s,Balls,Targets,Ref targets$
6430 DIM Input${80}
6440 !
6450 ! This subroutine prints a header for the printout and sets the system
6460 ! date and time.
6470 !
6480 IF Printer_flag=1 THEN PRINTER IS PRT
6490 PRINT CHR$(12)
6500 Set clock
6510 ! LINPUT "ENTER MEASUREMENT SERIES TITLE",Input$
6520 ! Preface$="&RPT$( " ",9)
6530 ! PRINT RPT$( " ",70)
6540 ! PRINT Preface&Input$
6550 ! LINPUT "ENTER OPERATOR NAME",Input$
6560 ! PRINT Preface&Input$
6570 PRINTER IS CRT
6580 PRINT
6590 PRINT
6600 PRINT Preface&"MEASUREMENT SERIES STARTED AT "&TIMES(TIMEDATE)
6610 PRINTER IS CRT
6620 SUBEND
6630 !
6640 !*****
6650 !
6660 SUB Set clock
6670 OPTION BASE 1
6680 INTEGER I
6690 DIM Chronos{12},Months{12}{3}
6700 Exec_key$=CHR$(255)&CHR$(88)
6710 READ Months{*}
6720 DATA "JAN","FEB","MAR","APR","MAY","JUN","JUL","AUG","SEP","OCT","NOV","DEC"
6730 OUTPUT KBD;"SCRATCH KEY "&Exec_key$;
6740 Clear_crt
6750 PRINT "
6760 PRINT " Current system date: ";DATES(TIMEDATE)
6770 PRINT " Current system time: ";TIMES(TIMEDATE)
6780 PRINT
6790 Ask: LINPUT "Enter date and time (YMMDDHHMSS) ":";Chronos$
6800 IF Chronos$="" AND DATES(TIMEDATE)<" 1 Mar 1900" THEN
6810 Clear_crt
6820 SUBEXIT
6830 END IF
6840 Year$=VAL$(1900+VAL(Chronos{1,2}))
6850 IF (VAL(Chronos{3,4})<=0 OR VAL(Chronos{3,4})>12) THEN
6860 BEEP

```

```

5860 PRINT "Incorrect month value."
5870 GOTO Ask
5880 END IF
5890 Year$=Month$(VAL(Chronos{3,4}))&" "&Year$
5900 Year$=Chronos{5,6}&" "&Year$
5910 SET TIMEDATE (DATE(Year$))
5920 IF (VAL(Chronos{7,8}))>23 THEN
5930 BEEP
5940 PRINT "Incorrect hour value."
5950 GOTO Ask
5960 END IF
5970 Day$=Chronos{7,8}&" ":"
5980 IF VAL(Chronos{9,10})>59 THEN
5990 BEEP
6000 PRINT "Incorrect minute value."
6010 GOTO Ask
6020 END IF
6030 Day$=Day$&Chronos{9,10}&" ":"
6040 IF (LEN(Chronos)>10 AND LEN(Chronos)=12) THEN
6050 IF VAL(Chronos{11,12})>59 THEN
6060 BEEP
6070 PRINT "Incorrect seconds value."
6080 GOTO Ask
6090 END IF
6100 Day$=Day$&Chronos{11,12}
6110 ELSE
6120 Day$=Day$&"00"
6130 END IF
6140 SET TIME TIME(Day$)
6150 Clear_crt
6160 SUBEXIT
6170 SUBEND
6180 !
6190 !*****
6200 !
6210 SUB Fix error
6220 SELECT ERRN
6230 CASE ELSE
6240 PRINTER IS CRT
6250 PRINT "ERROR ";ERRN
6260 PRINT ERRMS
6270 PRINT " PROGRAM IS PAUSED. FIX ERROR, IF POSSIBLE, AND CONTINUE."
6280 PAUSE
6290 END SELECT
6300 SUBEND
6310 !
6320 !*****
6330 !
6340 SUB Clear_crt (OPTIONAL INTEGER Start_line,Num_of_lines)
6350 !
6360 !
6370 !
6380 !
6390 !
6400 !
6410 !
6420 !
6430 !
6440 !
6450 !
6460 !
6470 !
6480 !
6490 !

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c_parc

```
7500 SUB Print_banner1
7510 Clear_crt
7520 PRINT
7530 PRINT
7540 PRINT TABXY(3,16);*****
7550 PRINT TABXY(4,16);**
7560 PRINT TABXY(5,16);**
7570 PRINT TABXY(6,16);**
7580 PRINT TABXY(7,16);**
7590 PRINT TABXY(8,16);**
7600 PRINT TABXY(9,16);**
7610 PRINT TABXY(10,16);**
7620 PRINT TABXY(11,16);**
7630 PRINT TABXY(12,16);*****
7640 SUBEXIT
7650 SUBEND
7660 !
7670 !
7680 !
7690 SUB Print_banner2
7700 PRINT "Don't use Print_banner2."
7710 SUBEND
7720 !
7730 !
7740 !
7750 SUB Print_banner3
7760 PRINT "Don't use Print_banner3."
7770 SUBEND
7780 !
7790 !
7800 !
7810 SUB Print_banner4
7820 COM /Paths/ @Nwa,@Nwa_data1,@Nwa_data2,Network_analyzer,@Hpbib,@Relay
7830 COM /Constants/ Vel,Zero(*),Exec_keys
7840 COM /System_config/ INTEGER Printer_flag,Debug_flag,Version$,Mode$,Out_types,Soun
ds,Bell$,Target$,Ref_target$
7850 COM /Sys_1/ Freq$(*),Freq_cent(*),Gate_span(*),Gate_span(*)
7860 COM /Sys_2/ Pol$(*),Polsw$(*)
7870 COM /Sys_3/ INTEGER F_disp,P_disp
7880 COM /Sys_4/ Drive_a$,Drive_b$,Drive_cs,INTEGER Preamble,Bytes
7890 COM /Sys_5/ INTEGER Nskip,Ndata
7900 COM /Sys_6/ Ref_angle,Angle,Beam(*),INTEGER Npts,Ntrace,Average_factor
7910 COM /Sys_7/ INTEGER Meas_flag(*)
7920 !
7930 !
7940 OFF KEY
7950 Clear_crt
7960 PRINT
7970 PRINT
7980 PRINT " PARAMETER CURRENT VALUE"
7990 PRINT "
FREQUENCY
";
8000 PRINT "
";
8010 FOR F=1 TO 3
8020 IF Meas_flag(F) THEN PRINT Freq$(F); "
";
8030 NEXT F
8040 PRINT "
"
8050 PRINT "
ANTENNA ANGLE
";
8060 PRINT "
TARGET TYPE
";
8070 PRINT "
MEASUREMENT MODE
";
8080 PRINT "
CURRENT DISPLAY
";
8090 PRINT "
";
8100 PRINT "
";
8110 PRINT "
";
8120 PRINT "
";
8130 PRINT "
";
8140 PRINT "
";
8150 PRINT "
";
8160 SUBEXIT
8170 SUBEND
8180 !
8190 !
8200 !
8210 SUB Store_file(COMPLEX Matrix(*),File_types$,Filename$,INTEGER F)
8220 COM /Sys_1/ Freq$(*),Freq_cent(*),Freq_span(*),Gate_cent(*),Gate_span(*)
8230 COM /Sys_2/ Pol$(*),Polsw$(*)
8240 COM /Sys_5/ INTEGER Nskip,Ndata
8250 COM /Sys_6/ Ref_angle,Angle,Beam(*),INTEGER Npts,Ntrace,Average_factor
8260 COM /Sys_7/ INTEGER Meas_flag(*)
8270 COM /System_config/ INTEGER Printer_flag,Debug_flag,Version$,Mode$,Out_types,So
unds,Bell$,Target$,Ref_target$
8280 !
8290 !
8300 !
8310 INTEGER Records_per_set,T
8320 REAL Bytes_per_set
8330 DIM Suffix$(2)
8340 ALLOCATE COMPLEX Trace(Ndata)
8350 !
8360 !
8370 DISP "Saving file."
8380 SELECT File_types$
8390 CASE ="SKY" ! Sky data.
Bytes_per_set=16*Ndata
Records_per_set=4*SUM(Meas_flag)*Ntrace
Suffix$="SA"
ELSE
FOR F=1 TO 3
IF Meas_flag(F)=1 THEN
Mf=F
END IF
NEXT F
Suffix$="S"&F&Freq$(Mf)
END IF
GOSUB Save_hpux
GOSUB Save_traces
CASE ="REF"
Bytes_per_set=16*Ndata
Records_per_set=4*SUM(Meas_flag)*Ntrace
IF SUM(Meas_flag)=3 THEN
Suffix$="RA"
ELSE
FOR F=1 TO 3
IF Meas_flag(F)=1 THEN
Mf=F
END IF
NEXT F
Suffix$="R"&F&Freq$(Mf)
END IF
GOSUB Save_hpux
GOSUB Save_traces
CASE ="MNT"
Bytes_per_set=16*Ndata
8400 !
8410 !
8420 !
8430 !
8440 !
8450 !
8460 !
8470 !
8480 !
8490 !
8500 !
8510 !
8520 !
8530 !
8540 !
8550 !
8560 !
8570 !
8580 !
8590 !
8600 !
8610 !
8620 !
8630 !
8640 !
8650 !
8660 !
8670 !
8680 !
8690 !
8700 !
8710 !
8720 !
8730 !
8740 !
```

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```
8750 Records_per_set=4*SUM(Meas_flag)*Ntrace
8760 IF SUM(Meas_flag)=3 THEN
8770   Suffix$="MA"
8780 ELSE
8790   FOR F=1 TO 3
8800     IF Meas_flag(F)=1 THEN
8810       Mf=F
8820     END IF
8830   NEXT F
8840   Suffix$="M"+Freq$(Mf)
8850 END IF
8860 GOSUB Save_hpux
8870 GOSUB Save_traces
8880
8890
8900 CASE ="GND"
8910 Bytes_per_set=16*Ndata
8920 Records_per_set=Ntrace*4+SUM(Meas_flag)
8930 IF SUM(Meas_flag)=3 THEN
8940   Suffix$="GA"
8950 ELSE
8960   FOR F=1 TO 3
8970     IF Meas_flag(F)=1 THEN
8980       Mf=F
8990     END IF
9000   NEXT F
9010   Suffix$="C"+Freq$(Mf)
9020 END IF
9030 GOSUB Save_hpux
9040 GOSUB Save_traces
9050
9060 END SELECT
9070 DEALLOCATE Trace(*)
9080
9090
9100 Save_averaged: ! Save the reference data file.
9110
9120
9130 IF NOT Debug_flag THEN
9140   CREATE BDAT Filenames$&Suffix$&Drive_c$,Records_per_set,Bytes_per_set
9150 END IF
9160 Base_record=0
9170 FOR F=1 TO 3
9180   IF Meas_flag(F)=1 THEN
9190     IF Debug_flag THEN
9200       ASSIGN @Disc TO PRT
9210       OUTPUT @Disc;"FILE: ", Filenames$, Suffix$
9220       OUTPUT @Disc USING Image_1;Version$, Freq_cent(F), Freq_span(F)
9230       OUTPUT @Disc USING Image_2;Ndata, Average_factor
9240       OUTPUT @Disc USING Image_3;Ref_targets$, T
9250     FOR P=1 TO 4
9260       OUTPUT @Disc USING Image_4;Pol$(P), Gate_cent(F), Gate_span(F)
9270     MAT Trace= Matrix(1,P,*)
9280     OUTPUT @Disc;Trace(*)
9290   NEXT P
9300 ELSE
9310   ASSIGN @Disc TO Filenames$&Suffix$&Drive_c$;FORMAT OFF
9320   OUTPUT @Disc, Base_record+1;Version$, Freq_cent(F), Freq_span(F)
9330   OUTPUT @Disc, Base_record+1;Ndata, Average_factor
9340   OUTPUT @Disc, Base_record+1;Ref_targets$, T
9350   FOR P=1 TO 4
9360     OUTPUT @Disc, Base_record+P;Pol$(P), Gate_cent(F), Gate_span(F)
9370     MAT Trace= Matrix(1,P,*)
9380     OUTPUT @Disc, Base_record+P;Trace(*)
```

```
9390 NEXT P
9400 Base_record=Base_record+4
9410 END IF
9420 END IF
9430 NEXT F
9440 ASSIGN @Disc TO *
9450 RETURN
9460
9470
9480
9490 Save_hpux: ! Save data in HP-UX format.
9500
9510 IF NOT Debug_flag THEN
9520   CREATE Filenames$&Suffix$&Drive_c$,240000
9530 END IF
9540 IF Debug_flag THEN
9550   ASSIGN @Disc TO PRT
9560   FOR T=1 TO Ntrace
9570     FOR F=1 TO 3
9580       IF Meas_flag(F)=1 THEN
9590         FOR P=1 TO 4
9600           MAT Trace= Matrix(T,P,*)
9610           OUTPUT @Disc;Trace(*)
9620         NEXT P
9630       END IF
9640     NEXT F
9650   NEXT T
9660 ELSE
9670   ASSIGN @Disc TO Filenames$&Suffix$&Drive_c$;FORMAT ON
9680   FOR T=1 TO Ntrace
9690     FOR F=1 TO 3
9700       IF Meas_flag(F)=1 THEN
9710         FOR P=1 TO 4
9720           MAT Trace= Matrix(T,P,*)
9730           OUTPUT @Disc;Trace(*)
9740         NEXT P
9750       END IF
9760     NEXT F
9770   NEXT T
9780 END IF
9790 ASSIGN @Disc TO *
9800 RETURN
9810
9820
9830
9840
9850 Save_traces: ! Save the ground target data file.
9860
9870 IF NOT Debug_flag THEN
9880   CREATE BDAT Filenames$&Suffix$&Drive_c$,Records_per_set,Bytes_per_set
9890   Base_record=0
9900 END IF
9910 IF Debug_flag THEN
9920   ASSIGN @Disc TO PRT
9930   OUTPUT @Disc;"FILE: ", Filenames$, Suffix$
9940   OUTPUT @Disc USING Image_5;Ndata, Ntrace
9950   OUTPUT @Disc USING Image_3;Target$
9960   FOR T=1 TO Ntrace
9970     FOR F=1 TO 3
9980       IF Meas_flag(F)=1 THEN
9990         OUTPUT @Disc USING Image_1;Version$, Freq_cent(F), Freq_span(F)
10000       MAT Trace= Matrix(1,P,*)
10010       OUTPUT @Disc USING Image_4;Pol$(P), Gate_cent(F), Gate_span(F), T
10020     END IF
```

```

10030 MAT Trace= Matrix(T,P,*)
10040 OUTPUT @Disc;Trace(*)
10050 NEXT P
10060 END IF
10070 NEXT F
10080 NEXT T
10090 ELSE
10100 ASSIGN @Disc TO Filename$Suffix$Drive_c$;FORMAT OFF
10110 OUTPUT @Disc,1;Ndata,Ntrace
10120 OUTPUT @Disc,1;Target$
10130 FOR T=1 TO Ntrace
10140 FOR F=1 TO 3
10150 IF Meas_flag(F)=1 THEN
10160 OUTPUT @Disc,Base_record+1;Version$,Freq_cent(F),Freq_span(F)
10170 FOR P=1 TO 4
10180 OUTPUT @Disc,Base_record+P;Pol$(P),Gate_cent(F),Gate_span(F),T
10190 MAT Trace= Matrix(T,P,*)
10200 OUTPUT @Disc,Base_record+P;Trace(*)
10210 NEXT P
10220 Base_record=Base_record+4
10230 END IF
10240 NEXT F
10250 NEXT T
10260 END IF
10270 ASSIGN @Disc TO *
10280 RETURN
10290 !-----
10300 !-----
10310 !-----
10320 Image 1:IMAGE (1X,12A,5X,"FREQ CENTER: ",2D.4D,5X,"FREQ SPAN: ",2D.4D)
10330 Image 2:IMAGE ("NUMBER OF POINTS: ",5D,5X,"NUMBER OF AVERAGES: ",5D)
10340 Image 3:IMAGE ("TARGET: ",30A,"GATING TARGET TYPE: ",2D)
10350 Image 4:IMAGE ("POLARIZATION: ",2A,5X,"GATE CENTER: ",SD.14DE,/,5X,"GATE SPAN: ",S
D.14DE,"TRACE: ",3D)
10360 Image 5:IMAGE ("NUMBER OF POINTS: ",5D,5X,"NUMBER OF TRACES: ",5D)
10370 Image 6:IMAGE (5X,SD.14DE,5X,SD.14DE)
10380 SUBEND
10390 !-----
10400 !-----
10410 !-----
10420 SUB Freq_set (INTEGER Ifreq)
10430 COM /Paths/ @Nwa,@Nwa_data1,@Nwa_data2,Netwrk_analyzer,@Hplb,@Relay
10440 COM /Sys_1/ Freq$(*) ,Freq_cent(*) ,Freq_span(*) ,Gate_span(*)
10450 !
10460 ! This subroutine sets the transmit frequency for the HP8753.
10470 !
10480 IF Ifreq=1 THEN
10490 OUTPUT @Nwa;"POWEO"
10500 ELSE
10510 OUTPUT @Nwa;"POWE-10"
10520 END IF
10530 SELECT Netwrk_analyzer
10540 CASE =3,=4,=5,=6
10550 OUTPUT @Nwa;"TIMDTRANOFF;"
10560 CASE =1,=2
10570 OUTPUT @Nwa;"FREQ;"
10580 END SELECT
10590 OUTPUT @Nwa;"CENT %VAL$(Freq_cent(Ifreq))&" GHZ;"
10600 OUTPUT @Nwa;"SPAN %VAL$(Freq_span(Ifreq))&" GHZ;"
10610 SUBEND
10620 !-----
10630 !-----
10640 !-----
10650 SUB Freq_sw (INTEGER Ifreq)

```

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10660 COM /Paths/ @Nwa,@Nwa_data1,@Nwa_data2,Netwrk_analyzer,@Hplb,@Relay
10670 SELECT Ifreq
10680 CASE 1
10690 OUTPUT @Relay;"?A2B1"
10700 CASE 2
10710 OUTPUT @Relay;"?A1B2"
10720 CASE 3
10730 OUTPUT @Relay;"?B12"
10740 END SELECT
10750 WAIT .1
10760 SUBEND
10770 !-----
10780 !-----
10790 !-----
10800 SUB Pol_sw (INTEGER Ifreq,Ipoll)
10810 COM /Paths/ @Nwa,@Nwa_data1,@Nwa_data2,Netwrk_analyzer,@Hplb,@Relay
10820 COM /Sys_1/ Freq$(*) ,Freq_cent(*) ,Freq_span(*) ,Gate_span(*)
10830 COM /Sys_2/ Pol$(*) ,Polsw$(*)
10840 !
10850 ! This subroutine sets the transmit and receive polarization by
10860 ! sending the proper command over the HP1B to the polarization
10870 ! relays.
10880 !
10890 OUTPUT @Relay;Polsw$(Ifreq,Ipoll)
10900 OUTPUT @Nwa;"TITL "" %Freq$(Ifreq)&" BAND - "%Pol$(Ipoll)&"""
10910 WAIT .1
10920 SUBEND
10930 !-----
10940 !-----
10950 !-----
10960 SUB Rotate_target
10970 OPTION BASE 1
10980 COM /Com4/ INTEGER Rotation_state,REAL Inc_angle,Current_angle,Start_angle,Stop_ang
le,Old_home_angle,INTEGER Sets_per_pos
10990 COM /Status/ INTEGER Sc,Connect_flg,E_flg,Debug_flg,Responses(80)
11000 INTEGER Fs_flag,SS_flag,Speed,Imc_status,Confirm_answer
11010 !
11020 !
11030 Confirm_answer=1
11040 Imc_status=0
11050 Debug_flg=0
11060 Fs_flag=-1
11070 Ss_flag=-1
11080 Clear_crt(3,16)
11090 !
11100 !
11110 SELECT Rotation_state
11120 CASE =-1
11130 IF FNASK("Do you wish to use the rotator?") THEN
11140 Connect_flg=0
11150 GOSUB Init_imc
11160 GOSUB Init_graph_pos
11170 GOSUB Manual_loop
11180 PRINT "Set Auto Mode Please....."
11190 ELSE
11200 Rotation_state=0
11210 GCLEAR
11220 GRAPHICS OFF
11230 END IF
11240 CASE =0
11250 SUBEXIT
11260 CASE =1
11270 GOSUB Check_position
11280 GOSUB Print_angles

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11290 GOSUB Manual_loop
11300 CASE =2
11310 GOSUB Check_position
11320 GOSUB Auto
11330 CASE =3
11340 GOSUB Check_position
11350 GOSUB Manual_loop
11360 GOSUB Auto
11370 CASE =4
11380 GOSUB Check_position
11390 GOSUB Go_home
11400 CASE =5
11410 GOSUB Check_position
11420 Rotation_state=1 ! Switch to manual mode.
11430 END SELECT
11440 SUBEXIT
11450 !
11460 !
11470 Init_Imc: ! Initialize the IMC unit.
11480 GOSUB Check_4_fault
11490 PRINT TABXY(1,3); "INITIALIZING IMC"
11500 Clear_crt(4,15)
11510 Comm("4WB") ! Set warm boot (clear flags).
11520 PRINT TABXY(1,4); "WB"
11530 Comm("4EB") ! Clear IMC buffer.
11540 PRINT TABXY(1,4); "EB"
11550 Encoder_ratio=4096 ! 32000
11560 Comm("4ER"&VAL$(Encoder_ratio)) ! Load encoder ratio.
11570 PRINT TABXY(1,4); "ER"&VAL$(Encoder_ratio)
11580 IF FNASK("Do you wish to set home at the current position?") THEN
11590 Comm("4RS"; Confirm_answer)
11600 ENTER Responses; Old_home_angle
11610 Old_home_angle=Old_home_angle/93.3
11620 Comm("4PIZ0") ! Set IMC at 0.
11630 PRINT TABXY(1,4); "PIZ"&RPTS(" ", LEN(VAL$(Encoder_ratio)))
11640 Comm("4PIA0") ! Set IMC at 0.
11650 PRINT TABXY(1,4); "PIA"
11660 Current_angle=0
11670 END IF
11680 Comm("4SP100") ! Set speed to (50pps).
11690 PRINT TABXY(1,4); "SP "&RPTS(" ", LEN(VAL$(Encoder_ratio)))
11700 Comm("4AC500") ! Set acceleration (500pps^2).
11710 PRINT TABXY(1,4); "AC"
11720 Comm("4DC500") ! Set deceleration (500pps^2).
11730 PRINT TABXY(1,4); "DC"
11740 GOSUB Check_position
11750 Rotation_state=1
11760 Clear_crt
11770 !
11780 !
11790 PRINT TABXY(1,4); "DONE INITIALIZING IMC"
11800 PRINT TABXY(1,5); "Turntable currently in manual mode."
11810 PRINT TABXY(1,6)
11820 Print_angles: !
11830 PRINT TABXY(1,7); "Current angle is: "; Current_angle; " degrees."
11840 PRINT TABXY(1,8); "Starting angle is: "; Start_angle; " degrees."
11850 PRINT TABXY(1,9); "Stopping angle is: "; Stop_angle; " degrees."
11860 RETURN
11870 !
11880 !
11890 Manual_loop: ! Main activation loop.
11900 LOOP
11910 ON KEY 0 LABEL "FAST SLEW CW ", FNTrap_level GOSUB Fs_cw
11920 ON KEY 1 LABEL "FAST SLEW CCW ", FNTrap_level GOSUB Fs_ccw
11930 ON KEY 5 LABEL "SLOW SLEW CW ", FNTrap_level GOSUB Ss_cw
11940 ON KEY 6 LABEL "SLOW SLEW CCW ", FNTrap_level GOSUB Ss_ccw
11950 ON KEY 2 LABEL "MANUAL CONTROL", FNTrap_level GOSUB Manual
11960 ON KEY 3 LABEL "TARGET GO HOME", FNTrap_level GOSUB Go_home
11970 ON KEY 4 LABEL "STOP ROTATION ", FNTrap_level GOSUB Stop_turn
11980 ON KEY 7 LABEL "SET AUTO MODE ", FNTrap_level GOSUB Set_auto
11990 ON KEY 8 LABEL "SET TARGET HOME", FNTrap_level GOSUB Set_position
12000 ON KEY 9 LABEL "RETURN ", FNTrap_level GOTO Quit
12010 GOSUB Check_position
12020 END LOOP
12030 !
12040 !
12050 !
12060 Fs_cw: ! Fast slew clockwise.
12070 IF Fs_flag<0 THEN
12080 Comm("4SP500")
12090 Comm("4SFN")
12100 Fs_flag=-1*Fs_flag
12110 Clear_crt(3,15)
12120 PRINT TABXY(1,15); "ROTATING CW (FAST)"
12130 ELSE
12140 Comm("4ST")
12150 Fs_flag=1*Fs_flag
12160 Clear_crt(3,15)
12170 PRINT TABXY(1,15); "ROTATION STOPPED"
12180 GOSUB Check_position
12190 END IF
12200 RETURN
12210 !
12220 !
12230 !
12240 Fs_ccw: ! Fast slew counterclockwise.
12250 IF Fs_flag<0 THEN
12260 Comm("4ST")
12270 Comm("4SP500")
12280 Comm("4SRN")
12290 Fs_flag=-1*Fs_flag
12300 Clear_crt(3,10)
12310 PRINT TABXY(1,15); "ROTATING CCW (FAST)"
12320 ELSE
12330 Comm("4ST")
12340 Fs_flag=1*Fs_flag
12350 Clear_crt(3,15)
12360 PRINT TABXY(1,15); "ROTATION STOPPED"
12370 GOSUB Check_position
12380 END IF
12390 RETURN
12400 !
12410 !
12420 !
12430 Ss_cw: ! Slow slew clockwise.
12440 IF Ss_flag<0 THEN
12450 Comm("4ST")
12460 INPUT "Speed? ", Sp
12470 Comm("4SP"&VAL$(INT(Sp)))
12480 Comm("4SFN")
12490 Ss_flag=-1*Ss_flag
12500 Clear_crt(3,15)
12510 PRINT TABXY(1,15); "ROTATING CW (SLOW)"
12520 ELSE
12530 Comm("4ST")
12540 Ss_flag=1*Ss_flag
12550 Clear_crt(3,15)
12560 PRINT TABXY(1,15); "ROTATION STOPPED"

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12570 GOSUB Check_position
12580 END IF
12590 RETURN
12600 !
12610 !-----
12620 !
12630 Ss_cw:! Slow slew counterclockwise.
12640 IF Ss_flag<0 THEN
12650 INPUT "Speed?",Sp
12660 Comm("4SP" & VAL$(INT(Sp)))
12670 Comm("4SRN")
12680 Ss_flag=-1*Ss_flag
12690 Clear crt(3,15)
12700 PRINT TABXY(1,15);"ROTATING CCW (SLOW) "
ELSE
12710 Comm("4ST")
12720 Ss_flag=-1*Ss_flag
12730 Clear crt(3,15)
12740 PRINT TABXY(1,15);"ROTATION STOPPED"
12750 GOSUB Check_position
12760 END IF
12770 RETURN
12780 !
12790 !-----
12800 !
12810 !
12820 Manual: INPUT "ANGLE (IN DEGREES)=?",Inc_angle
12830 INPUT "SPEED? (-100--500 RECOMMENDED) ",Speed
12840 Comm("4SP" & VAL$(Speed))
12850 SELECT Rotation_state
CASE =4
GOSUB Go_home
Rotation_state=2
GOTO Auto
CASE ELSE
Angle2=Inc_angle*93.3
Angle1=INT(Angle2)
IF Angle2-Angle1>=.5 THEN Angle1=Angle1+1
Current_angle=Current_angle+Inc_angle
Inc_angles=VAL$(Angle1)
Comm("4IM" & Inc_angle$)
Comm("4RFT")
END SELECT
12980 Imc_status=0
12990 Clear crt(3,7)
13000 PRINT TABXY(1,14);"ROTATING TARGET, PLEASE WAIT."
13010 !
13020 !-----
13030 !
13040 WHILE NOT BIT(Imc_status,0)
13050 Comm("4RS",Confirm_answer)
13060 ENTER Response;Imc_status
13070 PRINT TABXY(1,15);DVAL$(Imc_status,2)
13080 GOSUB Check_position
13090 WAIT 1
13100 END WHILE
13110 Imc_status=0
13120 !
13130 !-----
13140 Clear crt(3,16)
13150 PRINT TABXY(1,16);"CURRENT TARGET POSITION IS ";Current_angle;" DEGREES."
WAIT 2 ! Wait for target settling.
13160 RETURN
13170 !
13180 !-----
13190 !
13200 !
13210 Stop_turn:Comm("4ST")
13220 WHILE NOT BIT(Imc_status,0)
13230 Comm("4RS",Confirm_answer)
13240 ENTER Response;Imc_status
13250 WAIT .1
13260 END WHILE
13270 Clear crt(3,16)
13280 PRINT TABXY(1,15);"ROTATION STOPPED"
13290 GOSUB Check_position
13300 Imc_status=0
13310 RETURN
13320 !
13330 !-----
13340 !
13350 Set_auto: Comm("4SP500")
13360 GOSUB Check_position
13370 Clear crt(3,16)
13380 PRINT TABXY(1,3);"Current starting angle: ";Start_angle;" degrees"
13390 PRINT TABXY(1,4);"Current increment angle: ";Inc_angle;" degrees"
13400 PRINT TABXY(1,5);"Current stopping angle: ";Stop_angle;" degrees"
13410 PRINT TABXY(1,6);"Current rotation speed: ";Speed
13420 PRINT TABXY(1,7);RPTS(" ",80)
13430 PRINT TABXY(1,8);"Rotator positioned at: ";Current_angle;" degrees"
13440 INPUT "Enter starting angle value (degrees): ",Start_angle
13450 INPUT "Enter increment angle (degrees): ",Inc_angle
13460 INPUT "Enter stopping angle (degrees): ",Stop_angle
13470 INPUT "Enter rotation speed of target (~500 recommended): ",Speed
Speed=INT(Speed)
Comm("4SP" & VAL$(Speed))
IF ABS(Start_angle-Current_angle)>.1 THEN
PRINT TABXY(1,9);RPTS(" ",80)
PRINT TABXY(1,10);"Rotating target to starting angle..."
Temp_angle=Inc_angle
GOSUB Auto
Inc_angle=Temp_angle
END IF
Rotation_state=2
13580 Clear crt
13590 PRINT TABXY(1,20);"Turntable is in automatic mode. (press the RETURN soft
key)"
13610 RETURN
13620 !
13630 !-----
13640 !
13650 Set_position:INPUT "LOCK IN CURRENT TARGET POSITION AS REFERENCE POSITION?",Yn$
IF Yn$="Y" OR Yn$="y" THEN
Comm("4RS",Confirm_answer)
ENTER Response;Old_home_angle
Old_home_angle=Old_home_angle/93.3
Comm("4PIA0") ! Set absolute position to zero.
Comm("4PI20") ! Set incremental position to zero.
Current_angle=0
ELSE
PRINT "POSITION WAS NOT SET."
END IF
13750 RETURN
13760 !
13770 !-----
13780 !
13790 !
13800 Go_home: IF Speed<200 THEN Speed=200
13810 Comm("4SP" & VAL$(Speed))
13820 Comm("4AM0") ! Move to zero absolute position.

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13830 Comm("4RAN") ! Initiate movement.
13840 Comm("4MM") ! Make sure the move is completed.
13850 Imc_status=0
13860 Clear_crt(3,15)
13870 PRINT TABXY(1,14);"ROTATING TARGET TO HOME POSITION, PLEASE WAIT."
13880 WHILE NOT (BIT(Imc_status,0) AND BIT(Imc_status,5))
13890 GOSUB Check_status
13900 PRINT TABXY(1,15);"CURRENT STATUS: ";DVALS(Imc_status,2)
13910 GOSUB Check_position
13920 WAIT .1
13930 END WHILE
13940 Clear_crt(3,16)
13950 PRINT TABXY(1,15);"TARGET AT HOME POSITION."
13960 GOSUB Check_position
13970 Imc_status=0
13980 RETURN
13990 ! -----
14000 !
14010 !
14020 Check_status: ! Keep an eye on the Whedco controller status.
14030 Comm("4RS",Confirm_answer)
14040 ENTER Responses;Imc_status
14050 RETURN
14060 ! -----
14070 !
14080 !
14090 Check_position: ! Get the current turnstile position in degrees.
14100 Comm("4RP",Confirm_answer)
14110 ENTER Responses;Motor_position
14120 Current_angle=Motor_position/93.3
14130 Current_angle=Current_angle+Inc_angle
14140 PRINT TABXY(1,16);"CURRENT TARGET POSITION IS ";Current_angle;" DEGREES."
14150 GOSUB Draw_positions
14160 RETURN
14170 ! -----
14180 !
14190 !
14200 Check_4_fault: ! Check the IMC for a fault condition and correct or
14210 ! notify the user if necessary.
14220 !
14230 Comm("4FC",Confirm_answer)
14240 ENTER Responses;Faults
14250 SELECT Faults
14260 CASE ="power failure" ! Loss of power
14270 RETURN
14280 CASE ="Force DAC" ! Force DAC command was given
14290 BEEP
14300 PRINT "Force DAC command was given..."
14310 DISP "Press CONTINUE to resume..."
14320 PAUSE
14330 RETURN
14340 CASE ="Over-current" ! Over-current condition exists.
14350 BEEP
14360 PRINT "An over-current condition has been detected on the IMC."
14370 PRINT
14380 PRINT "Cycle the power to the IMC until the OV-CUR LED goes out"
14390 DISP "Press CONTINUE to reinitialize the IMC"
14400 PAUSE
14410 GOSUB Init_imc
14420 RETURN
14430 END SELECT
14440 RETURN
14450 !

```

```

14460 ! -----
14470 !
14480 Init_graph_pos: ! Creates a graphical depiction of where the target is.
14490 !
14500 GINIT
14510 GCLEAR
14520 GRAPHICS ON
14530 SHOW 0,100,0,100
14540 PENUP
14550 MOVE 90,70
14560 PEN 1 ! Draw circle
14570 POLYGON 12,360,360
14580 PENUP
14590 MOVE 90,70 ! Draw old home orientation.
14600 PEN 2
14610 DRAW 90+11*COS(Old_home_angle),70-11*SIN(Old_home_angle)
14620 PENUP
14630 MOVE 90,70 ! Draw current home orientation.
14640 PEN 4
14650 DRAW 90,58
14660 PENUP
14670 MOVE 90,70 ! Draw current target orientation.
14680 PEN 3
14690 X_pos=90+11*COS(Current_angle)
14700 Y_pos=70-11*SIN(Current_angle)
14710 DRAW X_pos,Y_pos
14720 RETURN
14730 ! -----
14740 !
14750 !
14760 Draw_positions: ! Draws out the angular orientations.
14770 MOVE 90,70 ! Draw old home orientation.
14780 PEN 2
14790 DRAW 90-11*SIN(Old_home_angle),70-11*COS(Old_home_angle)
14800 PENUP
14810 MOVE 90,70 ! Draw current home orientation.
14820 PEN 4
14830 DRAW 90,58
14840 PENUP
14850 DISABLE
14860 MOVE 90,70 ! Draw current target orientation.
14870 PEN -3
14880 DRAW X_pos,Y_pos
14890 MOVE 90,70
14900 PEN 3
14910 X_pos=90-11*SIN(Current_angle)
14920 Y_pos=70-11*COS(Current_angle)
14930 DRAW X_pos,Y_pos
14940 PENUP
14950 ENABLE
14960 RETURN
14970 ! -----
14980 !
14990 !
15000 Quit: !
15010 SUBEXIT
15020 SUBEND
15030 ! -----
15040 ! *****
15050 ! *****
15060 SUB Comm(C$,OPTIONAL INTEGER Confirm_answer)
15070 ! PROGRAM MODULE: Comm
15080 !
15090 !

```

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c_parc

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15100 | PURPOSE: Modified version of the Comm module to be used
15110 | for direct two way communication with the WHEDCO
15120 | IMC stepping motor controller.
15130 |
15140 | UPDATE: 3.0 Version 3.0 checks to see if the card being used
15150 | is the HP98628A (Datacomm) or the HP98626A (Serial).
15160 | Depending on which card is used, the appropriate
15170 | registers are selected.
15180 |
15190 | OPTION BASE 1
15200 | COM /Status/ INTEGER Sc,Connect_flg,E_flg,Debug_flg,Responses
15210 | INTEGER Baud_rate,B,Num_chars,Response_flg,Index1
15220 | DIM Input$(256),Term$(256),In$(256) BUFFER,From_232$(256)
15230 | DIM Num_chars$(6),Num_ltr$(6),Out$(256) BUFFER
15240 | DIM White_print$(1),CrLf$(2)
15250 | IF Debug_flg THEN PRINT TABXY(1,1);"ENTERING Comm *
15260 | ON ERROR GOSUB Error
15270 |
15280 |
15290 |
15300 | IF Connect_flg THEN After_init
15310 | Sc=30
15320 | ASSIGN @Find_it TO Sc;RETURN Outcome
15330 | IF Outcome=0 THEN
15340 | ASSIGN @Find_it TO *
15350 | CONTROL Sc,0;1 ! Reset RS-232 interface.
15360 | CONTROL Sc,3;1 ! Async link protocol.
15370 | CONTROL Sc,0;1 ! Set Async toggle.
15380 | CONTROL Sc,8;1+2 ! Set RTS and DTR lines.
15390 | CONTROL Sc,16;0 ! Disable connection timeout.
15400 | CONTROL Sc,17;0 ! Disable no activity timeout.
15410 | CONTROL Sc,18;0 ! Disable NO CARRIER timeout.
15420 | CONTROL Sc,19;0 ! Disable transmit timeout.
15430 | CONTROL Sc,20;14 ! TX baud speed = 9600
15440 | CONTROL Sc,21;14 ! RX baud speed = 9600
15450 | CONTROL Sc,22;0 ! No handshake with Whedco.
15460 | CONTROL Sc,23;0 ! No hardwired handshake.
15470 | CONTROL Sc,34;2 ! 7 bits/character.
15480 | CONTROL Sc,35;0 ! 1 stop bit.
15490 | CONTROL Sc,36;1 ! ODD parity.
15500 | Connect_flg=1
15510 | ELSE
15520 | Sc=8
15530 | ASSIGN @Find_it TO *
15540 | ASSIGN @Find_it TO Sc;RETURN Outcome
15550 | IF Outcome<>0 THEN
15560 | PRINT "RS-232 card not installed. Please install and reboot.*
15570 | ASSIGN @Find_it TO *
15580 | STOP
15590 | END IF
15600 | ASSIGN @Find_it TO *
15610 | RESET Sc
15620 | CONTROL Sc,0;1 ! Reset the RS-232 interface.
15630 | CONTROL Sc,3;Baud_rate ! Set the baud rate.
15640 | CONTROL Sc,4;8+2 ! UART 8 bits/char. ODD parity.
15650 | CONTROL Sc,5;3 ! UART DTR line active.
15660 | CONTROL Sc,12;128+32+16 ! Disable CD,DSR,CTS
15670 | STATUS Sc,3;B ! Confirm speed to user.
15680 | Connect_flg=1
15690 | END IF
15700 | After_init:1
15710 | White_print$=CHR$(136)
15720 | CrLf$=CHR$(13)&CHR$(10)
15730 | PRINT CHR$(128)&CHR$(136); ! Set up the screen.

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```

15740 | ASSIGN @Screen TO CRT
15750 | ASSIGN @Kbd TO KBD
15760 | ASSIGN @Rx TO BUFFER In$
15770 | ASSIGN @Tx TO BUFFER Out$
15780 | ASSIGN @Uart_out TO Sc
15790 | ASSIGN @Uart_in TO Sc
15800 | Response_flg=0
15810 | Response$=""
15820 |
15830 |
15840 | ENABLE INTR Sc ! Enable interrupt on card.
15850 | TRANSFER @Tx TO @Uart_out;CONT ! Enable transfer buffers.
15860 | TRANSFER @Uart_in TO @Rx
15870 | ON INTR Sc,FNTrap_level GOSUB Read_loop ! Process card interrupts.
15880 | IF CSC<>"*" THEN
15890 | GOSUB Send_com ! Send command out to controller.
15900 | ELSE
15910 | GOTO Quit ! If null command, exit quick.
15920 | END IF
15930 |
15940 |
15950 |
15960 | Wait_for_it:WHILE NOT Response_flg
15970 | GOSUB Read_loop
15980 | IF NPAR=2 THEN
15990 | LOOP
16000 | GOSUB Read_loop
16010 | IF (POS(Response$,"**")) THEN
16020 | Response$=Response$POS(Response$,"**"),LEN(Response$)
16030 | )
16040 | Response_flg=1
16050 | END IF
16060 | EXIT IF ((Response_flg=1) AND (POS(Response$,CrLf$)))
16070 | END LOOP
16080 | ELSE
16090 | WHILE NOT ((POS(Response$,"**")) OR (POS(Response$,"?")))
16100 | GOSUB Read_loop
16110 | END WHILE
16120 | Index1=POS(Response$,"**")
16130 | IF Index1=0 THEN ! Must be a "?" (Whedco command error).
16140 | ! Must be a "?" (Whedco command error).
16150 | E_flg=1 ! Notify via error flag.
16160 | Response_flg=1
16170 | ELSE
16180 | ! Normal command interpretation.
16190 | E_flg=0
16200 | Response_flg=1
16210 | END IF
16220 | END IF
16230 | END WHILE
16240 | GOTO Quit
16250 |
16260 |
16270 | Read_loop: Read in serial data from Whedco.
16280 |
16290 | STATUS @Rx,4;Num_chars ! Number of characters to
16300 | IF Num_chars=0 THEN RETURN ! receive, if 0 try again.
16310 | Num_chars$="#",&VAL$(Num_chars)&"A" ! Set up the IMAGE for ENTER.
16320 | ENTER @Rx USING Num_chars$;From_232$ ! Transfer contents.
16330 | Response$=Response$&From_232$ ! Build up dialogue.
16340 | RETURN ! Update pointers.
16350 |
16360 |

```

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