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Fred L. Bartman



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## Abstract

This report summarizes project activity during the period 1 July, 1966 to 30 September, 1966. Progress in the analysis of data obtained on the 8 May 1966 balloon flight, post flight tests and calibrations of the F-4 MRIR and the IRIS instrument, and preparations for the next balloon flight are described.

## I Introduction

This is the 15th Quarterly Progress Report on Contract No. NASr-54(03), covering the period 1 July, 1966 to 31 September, 1966. The project effort during this time period was divided among the following tasks:

1. Analysis of Balloon Flight Data.
2. Laboratory testing of the F-4 MRIR radiometer.
3. Laboratory testing of the infra-red interferometer spectrometer.
4. Preparations for the next balloon flight.
5. Report writing.

## II Analysis of Balloon Flight Data

The evaluation of data from the 8 May 1966 balloon flight has continued. Summaries of results are given below.

### A. Balloon Performance

Balloon performance was summarized in the progress report 05863-14-P. Data on the balloon configuration, weight, the trace of the trajectory over the earth, and the NCAR altitude vs. time curve were shown.

Analysis of pressure altitude data taken by U. of Michigan instrumentation indicates a float altitude slightly different than that obtained by the NCAR photobarograph. The two sets of data are shown in figure 1. The U. of Michigan data indicates an average float altitude of 7 mb., which is about 0.7 mb. (1700 feet) higher than indicated by the NCAR instrument. The U. of Michigan data also show greater fluctuations in float altitude during the day.

The difference between these two sets of data is somewhat greater than would be expected and has not been resolved so far.

### B. Air Temperature Data

Air temperature data obtained during balloon ascent was also shown in progress report 05863-14-P. Additional data is shown in figures 2 to 6. In figure 2 air temperature data taken during the balloon ascent by U. of Michigan thermister beads is compared with air temperature data obtained with the NCAR radiosonde. The U. M. data is significantly different from the radiosonde data except in the 400-600 mb. region. This difference may be due to errors in calibration of the U. of M. beads, however, since the beads were destroyed when the balloon gondola returned to earth the difference cannot be resolved.

Figure 3, 4 and 5 show air temperature data taken by radiosondes at five Weather Bureau Stations surrounding the launch site at 1200, 1800 and 2400 G. M. T. The rather large spread of temperatures shown by this data at low altitudes and in the tropopause regions eliminates any possibility of resolving the difference in the balloon ascent data noted above.

The smooth curve of air temperature vs pressure altitude which has been adopted for transmissivity calculations is shown in figure 6.

#### C. Relative Humidity Data

Relative humidity data taken by the radiosondes at 5 stations in the vicinity of the launch site are given in tables 1 to 5. The temperature data plotted in figures 3-5 and the dew point temperature are also given for reference.

#### D. Gondola Azimuth Data

The interpretation of the "MRIR" radiometer solar radiation channel data requires a knowledge of the azimuth of the scan plane of the radiometer. Azimuth data is obtained by a Disc Instruments, Inc. Model 835 Rotoswitch, which is a photoelectric bi-directional incremental shaft encoder. The field of view of the photocell, determined by a mask with two slits, is a vertical plane. The position of the rotating vertical plane is monitored by the Rotoswitch shaft encoder. The azimuth angle between the vertical plane and a reference line on the balloon gondola is determined from the shaft encoder data for the various times at which the vertical plane passes through the sun. The azimuth of the gondola reference line is then calculated from sun azimuth data and the shaft encoder data.

Figure 7 is a plot of sun azimuth and elevation vs. time for the 8 May 1966 balloon flight. Figure 8 shows the reference line on a plan view of the gondola. Figure 9 shows the time variation of the azimuth of the gondola reference line. In this figure azimuth is measured clockwise from north, as viewed from above. Thus  $0^\circ$  azimuth is north,  $90^\circ$  is east, etc...

The gondola rotational motion indicated in figure 9, is qualitatively typical of the rotations usually obtained on our balloon flights. During the

ascent to altitude there are fairly rapid rotations, due to the torque induced at launch and to the torques induced by the changing balloon configuration as it inflates during ascent. The rotation decreases when the balloon arrives at float altitude (0840 EST on this balloon flight). Usually there are occasional small motions during the rest of the flight at float altitude, with a minimum of rotation at local noon, and with noticeable increase in rotation in the afternoon as the sun elevation angle decreases.

The rotational motions at float altitude on this balloon flight were smaller than on other U. of M. balloon flights. This decreased rotation is attributed to the ladder type suspension used on this flight. (see fig. 14 in quarterly report 05863-14-P). On previous flights the long portion of the load line was usually a single long cable, which had less resistance to rotational motions.

On this balloon flight rotational motions of the gondola were introduced deliberately at one hour intervals during the morning. Torques were applied by 10 second jets of dry nitrogen through 2 orifices located on opposite sides of the balloon gondola. The nitrogen supply was carried in a small tank at 2200 psi initial pressure and was released by electrical valves after passing through a pressure regulator which reduced the pressure to about 65 psi. The quantity of gas (14 cu ft. at 70°F and 1 atmosphere) was sufficient for 11 cycles. On this flight 6 of these occurred before launch. The results of 2 of these jets applied at 0720 and 0820 EST are not easily detected in the rotational motions because of the large rotations already existing during ascent. The rotations produced at 0920, 1020 and 1120 EST can be seen in figure 9.

#### E. Housekeeping Data

Housekeeping data obtained on the 8 May 1966 balloon flight are shown in figures 10-20. Complete data was obtained up to 0750 EST, when the failure of a stepping relay in the calibrate monitor circuit occurred. Figures 10-18 and 20 show data obtained up to this time. Figure 19 shows data obtained from three thermistors for the remainder of the flight.

Figure 10 shows temperatures measured at 3 places in the gondola battery compartment. The decrease in temperature which takes place after launch indicates that the battery compartment insulation was not as effective as it has been on previous flights. Data was not obtained for a long enough time to determine the minimum temperature obtained before the normal increase which occurs at float altitude during the day. However extrapolation of the decrease of the temperature of the bottom of the battery compartment to 0920 EST., in direct analogy to the decrease of the distribution box air temperature shown in figure 19, indicates a temperature minimum of perhaps  $8^{\circ}\text{C}$ . Although this temperature is not dangerous for battery operation, it is much lower than should be obtained with proper insulation.

Figures 11, 12 and 13 show temperatures at various locations inside and on top of the gondola. These locations are protected from the cold air in the tropopause by at least one inch of polyethelene beadboard. The cameras (fig. 11) are all protected against low temperatures by heaters with thermostats that operate at  $6^{\circ}\text{ C}$  and therefore do not go below this temperature. The decrease obtained after launch for the other locations is quite normal.

Temperatures of the IRIS (Infrared Interferometer Spectrometer) instrumentation are shown in figure 14. The head and warm blackbody temperatures are controlled. The temperature of the electronics package shows a variation which is considered to be normal for an instrument inside of the second level of the gondola.

Filter wedge instrumentation temperatures are shown in figure 15. Again, the decrease in temperature of the door and electronic package are quite normal. Since a fairly large amount of power was dissipated in the instrument itself, the filter wedge bolometer, blackbody and the edge of the bottom plate do not show much temperature decrease after launch.

MRIR temperature data is shown in figures 16-19. Figure 16 shows temperatures of the auxiliary mirror, which has no insulation, and the door motor which is only poorly insulated. The mirror temperature minimum of  $-32.5^{\circ}\text{C}$ . was the lowest temperature recorded on the balloon gondola. The

The MRIR door motor (fig. 16), the MRIR door and the MRIR (fig. 17) distribution box show successively higher temperature minima, consistant with their power dissipation and insulation. MRIR instrument temperatures are shown in figure 18 and are as expected.

Figure 19 shows the three "housekeeping" temperatures measured throughout the flight. The MRIR mirror temperatures shows the extreme temperature variations which are to be expected of an uninsulated portion of the gondola. The temperature maxima are due to direct illumination by the sun. The MRIR chopper #1 temperature indicates a minimum temperature of 9° C. and shows fluctuations due to solar heating. The distribution chassis air temperature shows an increase consistant with continuous illumination of the gondola by the sun.

Figure 20 shows voltages of the thermister power supply which remained constant as long as they were measured.

#### F. IRIS (Infrared Interferometer Spectrometer) Data Analysis

The technique of analysing the IRIS data was perfected during this quarterly work period. Details of the work included:

1. Analog interferograms were put into IBM compatible format with the use of the Meteorological Department CDC computer.

2. Individual interferograms were carefully examined and a few selected for the calculation of spectra.

3. The analytical technique of applying calibrations was developed and programs were written for this purpose.

4. After considerable effort, it was realized that the pre-flight calibrations were not valid and so in-flight calibrations were used for data analysis.

At the end of this work period, spectra had been calculated for all of the interferograms selected.

#### III Laboratory Testing of the F-4 MRIR Radiometer

The thermal channels of the F-4 MRIR have been recalibrated. These post-flight calibrations are in basic agreement with pre-flight calibrations made in February, 1966 and thus demonstrate that no serious damage was done to the instrument in the launch disaster of 26 May 1966. A portion of the data with

both scanner and electronics module at 25° C. is shown in tables 6-9.

#### IV Laboratory Testing of the (IRIS) Interferometer

Laboratory Tests of the IRIS instrument included a check of resolution and a post flight calibration. The Laboratory's large blackbody source was re-built and a new dry box was constructed for the calibrations.

The resolution check and calibrations demonstrated two facts:

- a) That the interferometer suffered no deterioration in performance during the flight.
- b) The pre-flight calibrations carried out at Bendix Systems Division and at Chrysler Missile Division were not valid because of contamination of the calibration chamber by water vapor.

As a result, data analysis of the 8 May 1966 balloon flight data has been carried out using in-flight calibration data and a new environmental chamber has been purchased for use in carrying out interferometer calibrations in the future.

#### V Preparations for the Next Balloon Flight

Work in preparation for the next balloon flight can be divided into two categories; repair of old equipment and design and construction of new equipment.

Equipment repaired included:

- a) The pressure altitude measuring unit.
- b) Cameras (repaired by J. A. Maurer Co.).
- c) Brush recorders.
- d) Thermisters for measurement of "housekeeping" temperature data.
- e) The MRIR electronics (distribution) chassis.

After the construction and testing of prototype circuits for a new gondola timing and control system, parts were ordered for the new system.

#### VI Report Writing

A paper, published in May, 1966, and not reported on in the quarterly report covering that period is "The Effect of Time Jitter in the Sampling of an Interferogram", by M. T. Surh, Applied Optics vol. 5, pp 880, May 1966.

Another paper, by S. R. Drayson and C. Young, "Intensities of the Carbon Dioxide Band in the 12-18 Micron Spectral Region," was presented at the Symposium on Molecular Structure and Spectroscopy, Ohio State University Sept., 1966. The work reported on was performed in part on this project and partly under another contract, cwb-11376.

#### VII Future Work

The main effort during the next work period will be devoted to:

- 1) Data analysis
- 2) Construction of new balloon flight instrumentation
- 3) Report Writing

TABLE I METEOROLOGICAL DATA, Lake Charles, La.

	8 May 1966 1200 GMT			8 May 1966 1800 GMT			9 May 1966 0000 GMT			9 May 1966 1200 GMT		
P(mb)	T( $^{\circ}$ C)	RH%	$T_D$ ( $^{\circ}$ C)	P(mb)	T( $^{\circ}$ C)	RH%	$T_D$ ( $^{\circ}$ C)	P(mb)	T( $^{\circ}$ C)	RH%	$T_D$ ( $^{\circ}$ C)	
1008	17.8	90	16.1	1009	27.2	57	17.8	1006	27.2	39	12.1	
994	22.1	68	15.9	996	24.8	48	13.1	807	11.0	62	4.0	
923	17.8	61	10.2	826	11.0	63	4.2	772	8.2	71	3.2	
794	7.5	99	7.4	782	6.7	86	4.5	709	5.6	35	-8.7	
696	2.5	76	-1.4	740	3.7	67	-1.9	582	-2.5	48	-12.0	
661	1.9	51	-7.2	720	3.7	47	-6.5	508	-11.2	53	-18.9	
568	-5.8	58	-13.5	708	5.5	39	-7.4	481	-14.4	63	-19.9	
536	-9.3	72	-18.1	654	2.8	45	-8.0	446	-19.2	61	-24.8	
516	-10.6	54	-26.0	538	-7.4	43	-7.4	438	-19.6	44	-28.8	
412	-23.9	33	-32.5	460	-16.5	43	-26.2	400	-24.3	18	-41.9	
400	-24.9	72	-49.6	438	-19.5	52	-26.9	292	-39.9	18	-55.2	
388	-26.7	58	-49.6	400	-24.0	38	-34.4	221	-51.5			
300	-40.0	35	-49.6	328	-36.2	20	-51.2	176	-59.7			
249	-50.2	297	-40.0	297	-40.0	18	-55.3	162	-58.4			
173	-61.2	244	-49.0	244	-49.0			156	-60.1			
164	-59.0	199	-56.0	199	-56.0			142	-58.7			
152	-61.6	193	-55.4	193	-55.4			110	-63.3			
107	-63.8	162	-62.0	162	-62.0			100	-62.8			
100	-61.6	132	-60.5	132	-60.5			72	-64.3			
69	-64.0	107	-62.2	107	-62.2			59	-60.8			
55	-59.6	100	-61.1	100	-61.1			52	-61.1			
50	-61.6	91	-59.6	91	-59.6			50	-57.5			
26	-48.0	75	-65.2	75	-65.2			38	-54.0			
14	-43.8	40	-52.8	40	-52.8			35	-55.9			
10	-37.2	26	-50.0	26	-50.0			27	-48.7			
		20	-41.7	20	-41.7			25	-49.6			
		15	-39.9	15	-39.9			16	-43.2			

TABLE 2 METEOROLOGICAL DATA, Shreveport, La.

8 May 1966 1200 GMT			8 May 1966 1800 GMT			9 May 1966 0000 GMT		
P(mb)	T( $^{\circ}$ C)	RH%	T <sub>D</sub> ( $^{\circ}$ C)	P(mb)	T( $^{\circ}$ C)	RH%	T <sub>D</sub> ( $^{\circ}$ C)	P(mb)
1000	14.9	95	14.1	1000	25.7	51	14.8	997
986	22.3	60	14.1	851	12.2	66	986	26
850	12.8	64	6.2	832	14.2	31	852	44
824	12.8	41	-0.1	602	-2.6	29	808	14.6
720	6.0	44	-5.4	486	-14.7	43	613	58
584	-7.5	44	-17.7	400	-24.7	27	458	12.9
552	-8.2	44	-18.3	342	-33.9	26	311	30
	-17.0	33		303	-40.0	28	-39.8	-4.3
400	-26.0	33	-37.6	251	-48.3	26	260	30
310	-40.0	35	-49.7	197	-56.5	20	204	14.6
259	-48.4			132	-62.8	19	160	44
207	-56.6			100	-61.0	18	130	30
171	-60.8			92	-60.3	17	115	29
162	-59.2			82	-63.5	16	96	19
136	-63.0			54	-56.7	15	79	10
108	-61.3			43	-56.7	14	29	-4.5
100	-63.3			10	-34.6	13	18.5	30
62	-62.0			8	-35.5	12	10	-36.8
37	-51.3							
	32	-52.5						
	22	-44.8						
	10	-37.7						
	7	-37.3						

TABLE 3 METEOROLOGICAL DATA, Fort Worth, Texas

P(mb)	T( $^{\circ}$ C)	RH%	T <sub>D</sub> ( $^{\circ}$ C)	8 May 1966 0600 GMT				8 May 1966 1200 GMT				9 May 1966 1800 GMT				9 May 1966 0000 GMT			
				P(mb)	T( $^{\circ}$ C)	RH%	T <sub>D</sub> ( $^{\circ}$ C)	P(mb)	T( $^{\circ}$ C)	RH%	T <sub>D</sub> ( $^{\circ}$ C)	P(mb)	T( $^{\circ}$ C)	RH%	T <sub>D</sub> ( $^{\circ}$ C)	P(mb)	T( $^{\circ}$ C)	RH%	T <sub>D</sub> ( $^{\circ}$ C)
991	19.8	78	15.9	989	16.0	90	14.4	989	26.2	51	15.2	986	27.0	48	15.0	986	16.3	54	7.0
968	22.9	57	13.9	962	21.0	51	10.5	979	23.6	39	8.8	868	16.3	1.9	-7.1	847	16.7	1.9	-9.6
868	16.0	58	7.7	840	13.3	41	0.3	844	13.5	32	-2.9	802	15.3	17	-9.6	807	11.8	46	0.5
840	14.2	41	1.1	789	9.0	71	4.0	775	11.1	21	-10.5	732	9.5	15	-15.8	704	13.3	24	-14.8
684	3.2	28	-13.5	735	7.7	21	-13.3	666	2.9	24	-15.7	722	10.8	15	-14.8	654	5.0	51	-9.1
654	0.5	44	-10.4	704	5.0	26	0	655	4.0	15	-20.3	591	1.9	1.8	-1.5	616	-18.5	642	0.2
616	-2.5	28	-18.5	654	-0.2	51	-9.1	520	-7.7	15	-20.3	476	-1.3	8	-1.8	605	-24.1	642	0.2
605	-1.5	16	-24.1	622	0.2	23	-18.5	400	-24.8	16	-43.5	400	-24.3	8	-42.0	574	-4.1	590	-3.3
574	-4.2	17	-42.1	590	-3.3	16	-25.6	400	-25.6	15	-56.8	299	-40.0	20	-54.4	400	-26.1	400	-42.5
400	-26.1	20	-42.5	400	-26.8	18	-44.0	304	-40.0	15	-56.8	226	-54.7			333	-37.0	350	-34.1
333	-37.0	20	-51.8	350	-34.1	18	-50.2	227	-54.1	18	-55.3	212	-56.1			309	-40.0	310	-40.0
309	-40.0	20	-54.5	269	-47.5	18	-55.3	200	-57.8	18	-55.3	196	-59.9			268	-46.8	269	-47.5
268	-46.8			195	-60.3			172	-63.4			172	-63.4			228	-51.8	195	-60.3
228	-51.8			185	-59.6			163	-62.6			163	-62.6			223	-51.8	185	-59.6
223	-51.8			148	-64.0			158	-59.6			158	-59.6			200	-58.0	148	-64.0
200	-58.0			141	-62.0			138	-62.1			138	-62.1			122	-64.0	122	-64.0
122	-64.0			115	-62.2			127	-60.3			127	-60.3			108	-64.0	115	-62.2
108	-64.0			108	-64.0			118	-62.9			118	-62.9			100	-64.0	108	-64.0
100	-62.3			100	-62.3			114	-62.1			114	-62.1			82	-66.0	82	-66.0
82	-66.0			82	-66.0			100	-64.8			100	-64.8			40	-57.1	40	-57.1
40	-57.1			34	-51.7			92	-63.1			92	-63.1			30	-52.9	34	-51.7
30	-52.9			18	-43.8			82	-64.5			82	-64.5			15	-41.7	18	-43.8
15	-41.7			15	-41.7			75	-62.0			75	-62.0			28	-47.5	30	-52.9
28	-47.5							65	-64.0			65	-64.0			26	-48.1	18	-43.8
26	-48.1							43	-55.5			43	-55.5			18	-43.3	18	-43.3
18	-43.3							35	-50.0			35	-50.0						

TABLE 4 METEOROLOGICAL DATA, Midland, Texas

8 May, 1966 1200 GMT			8 May, 1966 1800 GMT			9 May 1966 0000 GMT					
P(mb)	T( $^{\circ}$ C)	R.H%	T <sub>D</sub> ( $^{\circ}$ C)	P(mb)	T( $^{\circ}$ C)	R.H%	T <sub>D</sub> ( $^{\circ}$ C)	P(mb)	T( $^{\circ}$ C)	R.H%	T <sub>D</sub> ( $^{\circ}$ C)
910	14.0	71	8.8	910	26.9	30	7.8	916	31.5	19	5.0
886	19.1	44	6.6	900	24.6	27	4.4	892	29.0	18	2.3
833	18.6	18	-6.1	836	19.1	24	-1.9	700	11.1	25	
787	17.0	20	-6.1	796	18.5	22	-3.6	622	2.9	27	
633	2.8	23	-16.3	733	12.9	22		568	-3.5	27	-19.8
533	-9.4	32	-23.0	642	3.3	26	-14.4	548	-4.5	17	-25.9
523	-9.2	18	-29.3	620	0.3	39	-12.1	400	-23.1	18	-40.9
480	-13.5	17	-33.4	561	-6.4	33	-20.0	290	-40.0		
400	-24.5	21	-40.7	550	-6.4	19	-26.3	216	-57.2		
362	-29.6	19		531	-7.1	17	-28.1	165	-64.0		
304	-40.0	25	-52.5	463	-16.0	18		156	-59.1		
284	-44.0	0		400	-24.3	19	-41.5	142	-61.8		
264	-46.2			340	-34.0	21	-48.9	130	-60.8		
186	-61.1			297	-40.0	20	-54.4	100	-65.0		
173	-63.4			201	-60.0			76	-65.8		
157	-60.9			176	-61.6			58	-64.1		
146	-63.4			171	-61.1			50	-59.0		
114	-61.5			153	-63.0			38	-57.6		
100	-64.3			145	-60.5			25	-46.8		
57	-63.4			121	-60.0			10	-38.0		
48	-58.8			106	-63.4			7	-30.0		
40	-58.5			100	-62.5			5.6	-31.2		
38	-54.5			59	-62.5						
10	-35.9			54	-58.0						
8	-36.2			44	-58.5						
				34	-51.4						
				21	-44.3						
				17	-42.9						
				13.5	-36.3						
				10	-33.2						

TABLE 5 METEOROLOGICAL DATA, San Antonio, Texas

	8 May 1966 1200 GMT			8 May 1966 1800 GMT			9 May 1966 0000 GMT			9 May 1966 0600 GMT		
P(mb)	T( $^{\circ}$ C)	RH%	T <sub>D</sub> ( $^{\circ}$ C)	P(mb)	T( $^{\circ}$ C)	RH%	T <sub>D</sub> ( $^{\circ}$ C)	P(mb)	T( $^{\circ}$ C)	RH%	T <sub>D</sub> ( $^{\circ}$ C)	
982	13.3	97	12.8	982	25.0	60	16.7	979	27.2	47	14.9	
966	16.6	100	16.6	966	22.5	53	12.4	872	16.8	58	8.5	
922	14.8	90	13.3	905	16.5	71	11.2	823	12.6	65	6.2	
895	15.6	63	8.6	827	12.3	45	0.7	764	8.0	58	0.2	
839	11.1	85	8.6	758	5.7	48	-4.5	746	9.5	23	-10.6	
814	10.7	62	3.7	728	6.1	23	-13.5	708	8.2	16	-16.2	
739	4.0	62	-2.6	698	7.8	19	-14.5	704	9.1	16	-15.5	
719	3.4	35	-10.6	590	-2.2	19	-14.5	638	4.5	15	-19.9	
697	5.7	14	-19.8	400	-24.5	20	-41.2	466	-15.4	15	-15.4	
674	5.2	14	-20.2	326	-35.9	21	-41.2	400	-23.6	17	-41.9	
600	-1.2	15	-24.6	309	-38.9	23	-52.3	343	-32.5	17	-55.3	
430	-22.5	18	-40.4	200	-56.0	200	-56.0	294	-40.0	18	-55.3	
400	-25.0	18	-42.5	178	-59.6	178	-59.6	204	-57.8			
365	-25.0	0	160	-57.5	160	-57.5	160	193	-59.0			
298	-40.0	0	151	-60.6	151	-60.6	151	190	-57.6			
275	-43.9	9	140	-60.1	140	-60.1	140	172	-60.3			
215	-54.7	7	132	-61.7	132	-61.7	132	152	-60.1			
192	-59.4	4	127	-60.9	127	-60.9	127	142	-57.6			
168	-61.7	7	111	-64.2	111	-64.2	111	129	-61.9			
157	-61.5	5	100	-62.8	100	-62.8	100	112	-63.6			
151	-62.4	4	67	-66.1	67	-66.1	67	100	-67.7			
130	-61.2	2	45	-56.0	45	-56.0	45	95	-69.2			
120	-61.4	4	40	-55.7	40	-55.7	40	84	-64.9			
106	-65.2	2	31	-50.6	31	-50.6	31	62	-65.3			
100	-63.8	8						36	-51.2			
78	-64.8	3						28	-51.2			
63	-66.0	0						23	-45.2			
44	-57.5	5						17	-44.8			
18	-44.7	14										
	-43.2	14										

TABLE 6 F-4 MRIR CALIBRATION DATA  
 6.7 Micron Channel  
 Scanner 25°/Electronics 25°

<sup>o</sup> C	S. B.	S. B.	U. M.	S. B.	U. M.	S. B.	S. B.	U. M.	U. M.
	10/2/64	10/12/64	2/65	4/8/65	9/65	12/20/65	12/29/65	2/1/66	7/6/66
-93	5.20	5.25	--	4.70	4.95	4.70	4.70	5.15	--
-83	5.15	5.15	--	4.60	4.85	4.65	4.65	5.00	4.88
-73	5.00	5.10	--	4.40	4.65	4.55	4.55	4.84	4.75
-63	4.80	4.90	4.20	4.25	4.40	4.30	4.30	4.56	4.50
-53	4.50	4.55	3.95	3.95	4.05	4.10	4.10	4.25	4.13
-43	4.05	4.05	3.55	3.45	3.60	3.60	3.60	3.75	3.63
-33	3.40	3.40	2.90	2.80	3.05	3.00	3.00	3.10	2.95
-23	2.55	2.60	2.05	2.10	2.20	2.10	2.10	2.26	2.10
-13	1.50	1.50	1.00	1.05	1.10	1.10	1.10	1.15	1.00
-3	--	--	--	--	--	--	--	--	--

TABLE 7 F-4 MRIR CALIBRATION DATA  
 10-11 Micron Channel  
 Scanner 25°/Electronics 25°

	S. B.	S. B.	U. M.	S. B.	U. M.	S. B.	S. B.	U. M.	U. M.
°C	10/2/64	10/12/64	2/65	4/8/65	9/65	12/20/65	12/29/65	2/1/66	7/6/66
-93	6.30	6.25	--	6.10	6.10	6.10	6.05	--	--
-83	6.20	6.15	--	6.00	6.05	6.00	5.95	6.14	5.90
-73	6.00	6.05	--	5.90	5.90	5.85	5.80	5.96	5.80
-63	5.85	5.85	5.60	5.65	5.70	5.65	5.65	5.75	5.60
-53	5.65	5.60	5.40	5.45	5.45	5.45	5.40	5.50	5.35
-43	5.35	5.30	5.15	5.15	5.15	5.15	5.10	5.19	5.05
-33	5.00	5.00	4.80	4.85	4.80	4.85	4.85	4.85	4.70
-23	4.60	4.55	4.40	4.40	4.40	4.45	4.35	4.45	4.30
-13	4.05	4.10	3.90	4.00	3.95	3.95	3.90	3.99	3.85
-3	3.55	3.50	3.40	3.50	3.45	3.50	3.40	3.45	3.35
7	3.00	3.20	2.85	2.90	2.90	2.90	2.85	2.85	2.75
17	2.30	2.25	2.20	2.25	2.25	2.25	2.20	2.20	2.15
27	1.50	1.50	1.50	1.50	1.55	1.55	1.50	1.50	1.50
37	0.65	0.70	--	0.70	0.75	0.75	0.70	0.70	0.75
47	--	--	--	--	--	--	--	--	--

TABLE 8 F-4 MRIR CALIBRATION DATA  
 14-16 Micron Channel  
 Scanner 25°/Electronics 25°

<sup>o</sup> C	S. B. 10/2/64	S. B 10/12/64	U. M. 2/65	S. B. 4/8/65	U. M. 9/65	S. B. 12/20/65	S. B. 12/29/65	U. M. 2/1/66	U. M. 7/6/66
-93°	5.00	5.00	--	4.80	4.75	4.75	4.75	4.94	--
-83°	4.70	4.70	--	4.40	4.55	4.40	4.40	4.63	4.51
-73°	4.35	4.35	--	4.10	4.15	4.00	4.10	4.25	4.16
-63°	3.85	3.90	3.45	3.75	3.70	3.50	3.60	3.77	3.70
-53°	3.40	3.35	3.05	3.25	3.20	3.05	3.10	3.30	3.19
-43°	2.75	2.75	2.55	2.60	2.65	2.50	2.55	2.75	2.61
-33°	2.30	2.15	1.95	2.00	2.00	1.85	1.90	--	1.95
-23°	1.55	1.50	1.25	1.35	1.35	1.20	1.25	--	1.25
-13°	0.80	0.75	0.45	0.60	0.55	0.50	0.50	--	0.50
-5.5°	-0.20	-0.15	--	0.00	+0.05	+0.05	+0.05	--	--

TABLE 9 F-4 MRIR CALIBRATION DATA  
 5-30 Micron Channel  
 Scanner 25°/Electronics 25°

<sup>o</sup> C	S. B. 10/2/64	S. B. 10/12/64	U. M. 2/65	S. B. 4/8/65	U. M. 9/65	S. B. 12/20/65	S. B. 12/29/65	U. M. 2/1/66	U. M. 7/6/66
-93	5.80	5.80	--	5.70	5.80	5.65	5.70	5.98	--
-83	5.60	5.65	--	5.50	5.70	5.50	5.50	5.80	5.70
-73	5.40	5.50	--	5.35	5.55	5.35	5.35	5.60	5.50
-63	5.25	5.25	5.30	5.10	5.30	5.15	5.10	5.35	5.26
-53	5.00	5.00	5.10	4.85	5.00	4.85	4.85	5.05	5.00
-43	4.65	4.70	4.80	4.60	4.70	4.55	4.55	4.75	4.70
-33	4.30	4.35	4.40	4.25	4.30	4.20	4.25	4.40	4.33
-23	3.95	3.90	3.95	3.90	3.90	3.80	3.80	4.00	3.90
-13	3.50	3.50	3.50	3.40	3.45	3.40	3.40	3.50	3.46
-3	3.00	3.00	2.95	2.95	3.00	2.90	2.90	3.00	2.96
7	2.40	2.40	2.40	2.40	2.45	2.40	2.35	2.45	2.43
17	1.80	1.80	1.80	1.85	1.80	1.75	1.75	1.82	1.81
27	1.15	1.10	1.15	1.15	1.15	1.15	1.15	1.10	1.15
37	0.40	0.50	0.35	0.40	0.35	0.35	0.35	0.35	0.41
47	--	--	--	--	--	--	--	--	--

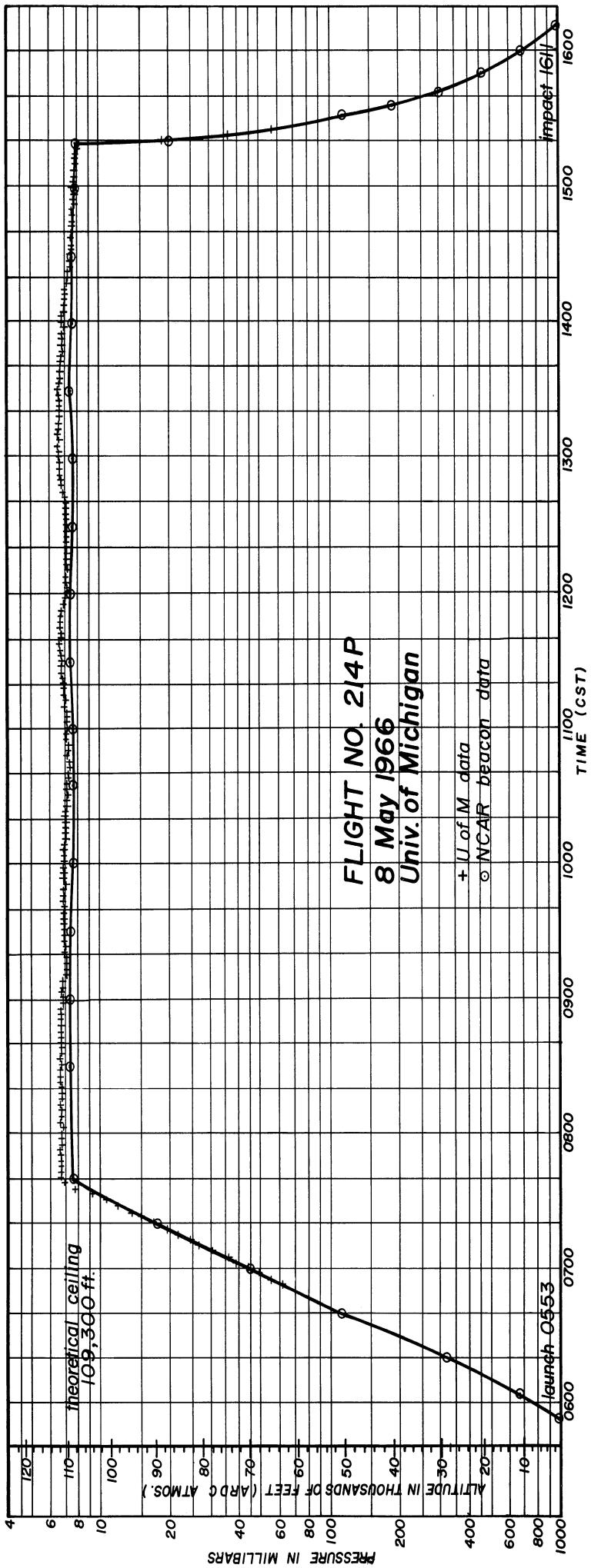


Figure 1

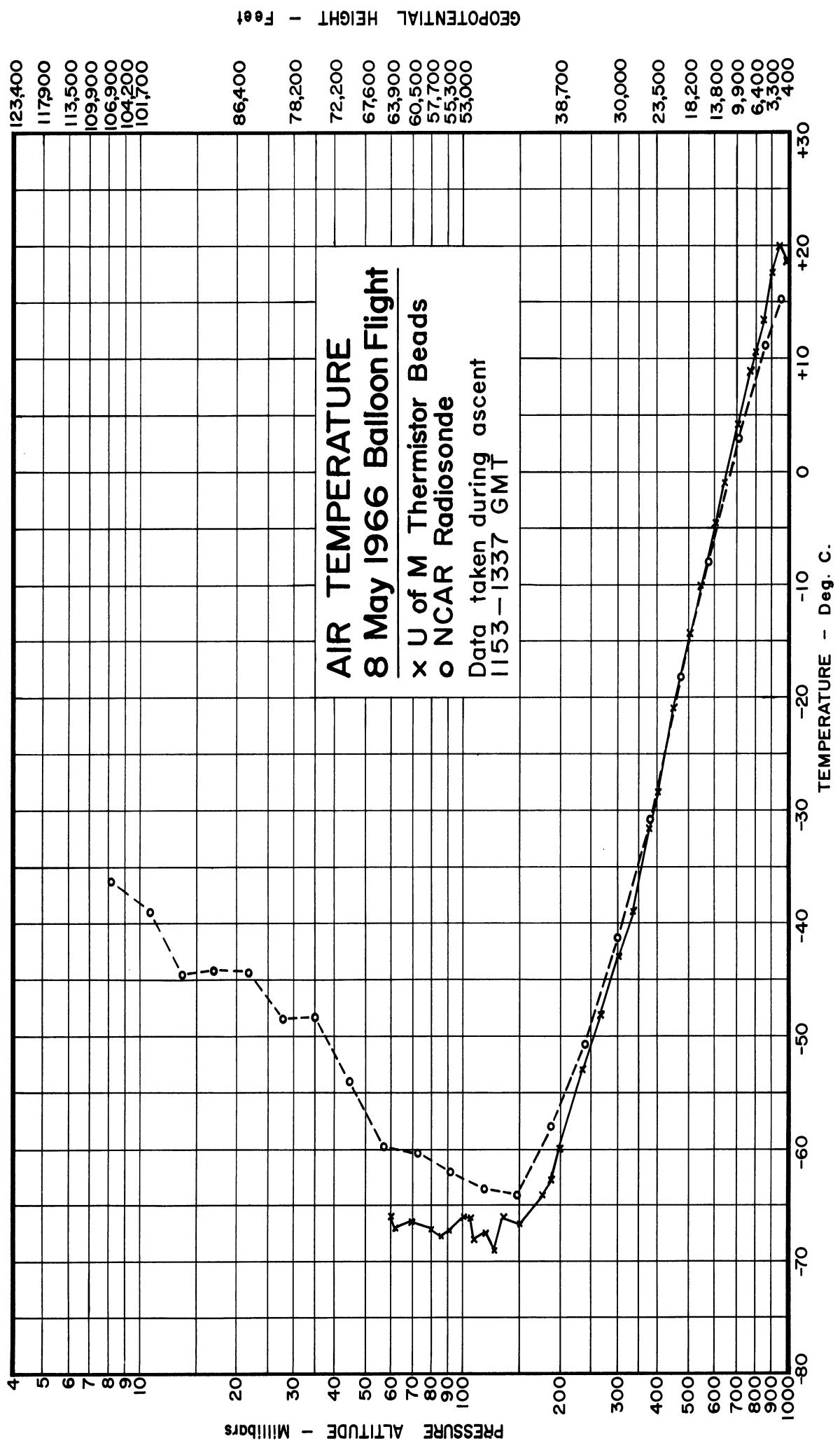


Figure 2

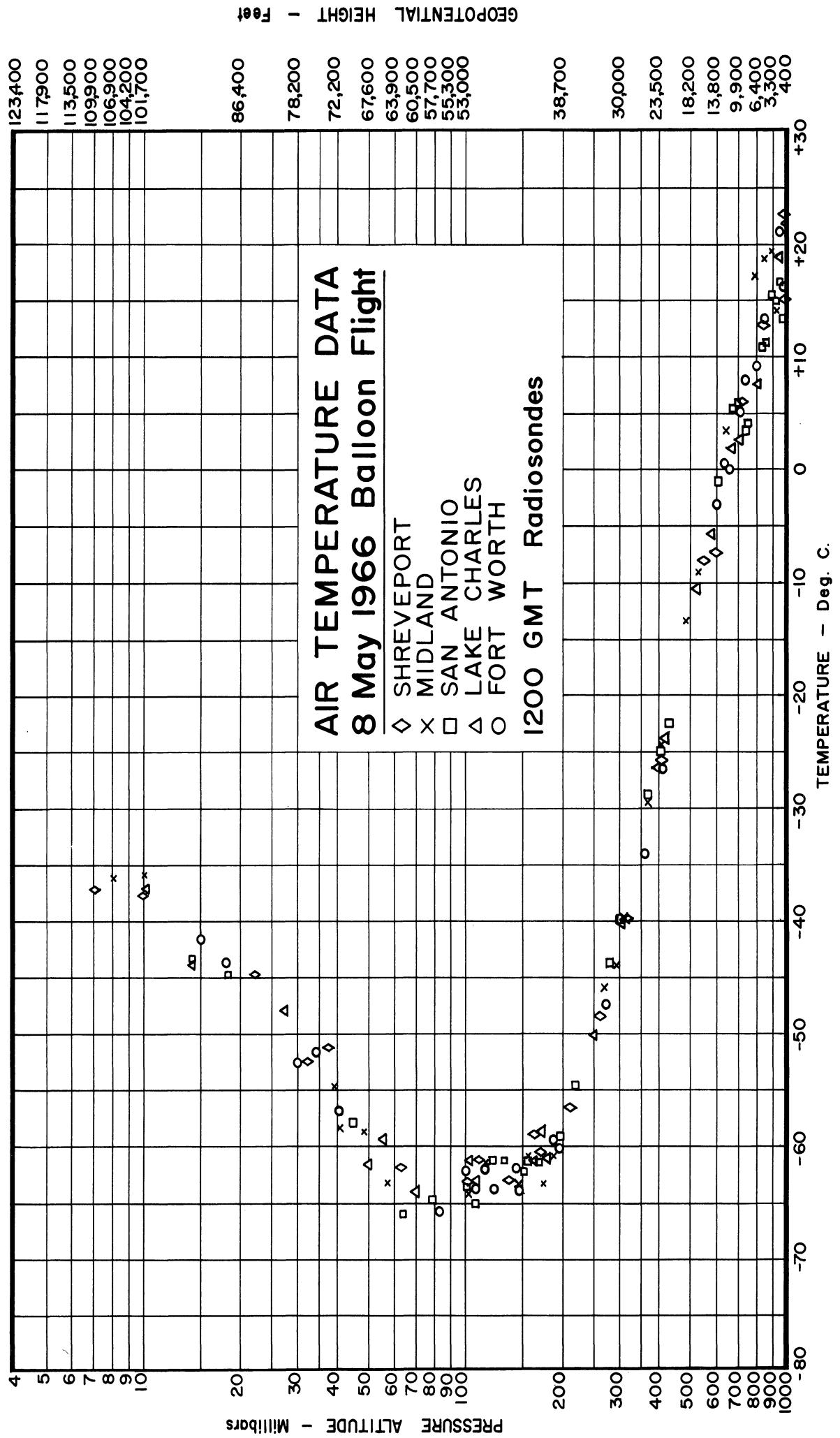


Figure 3

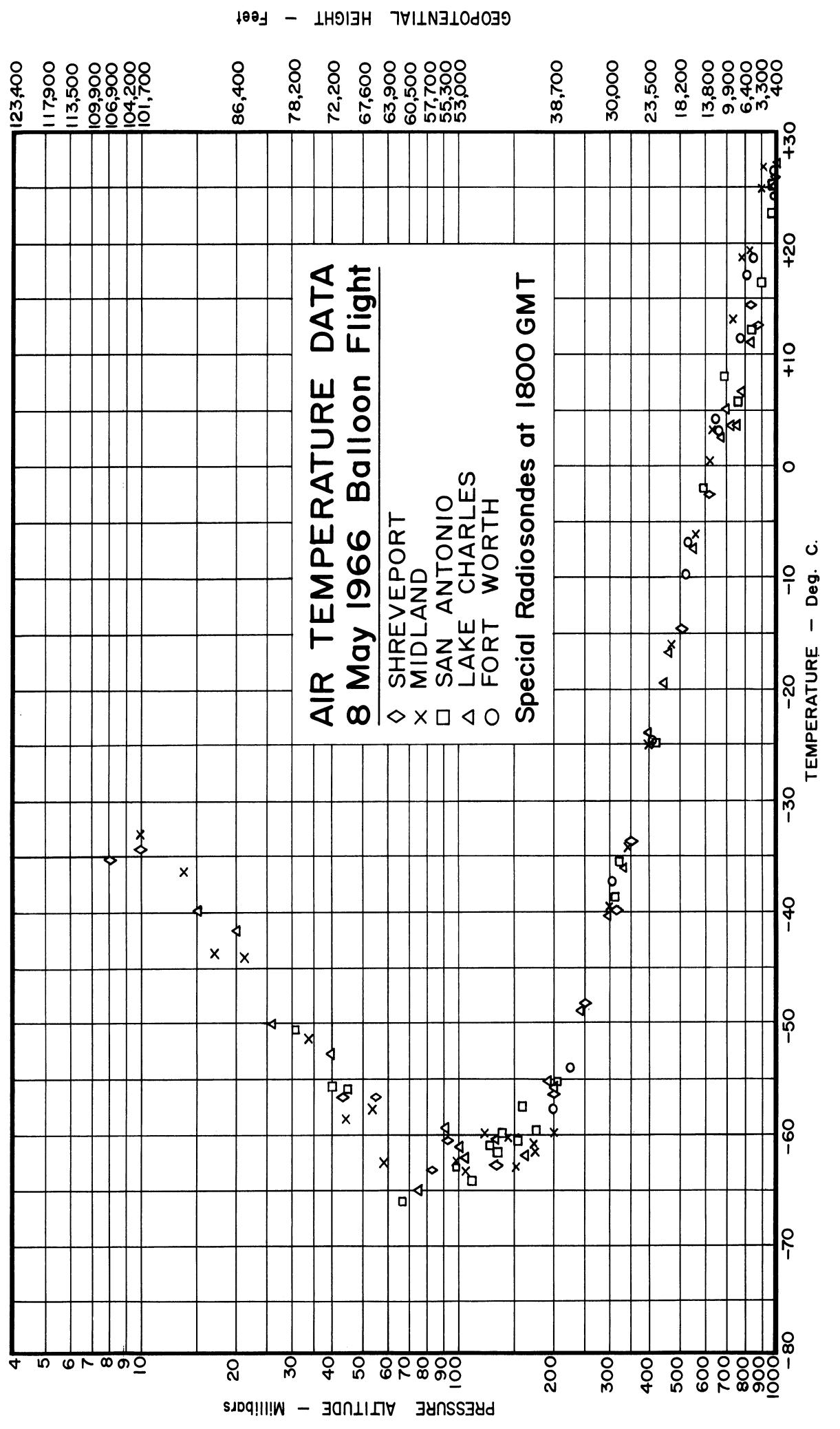


Figure 4

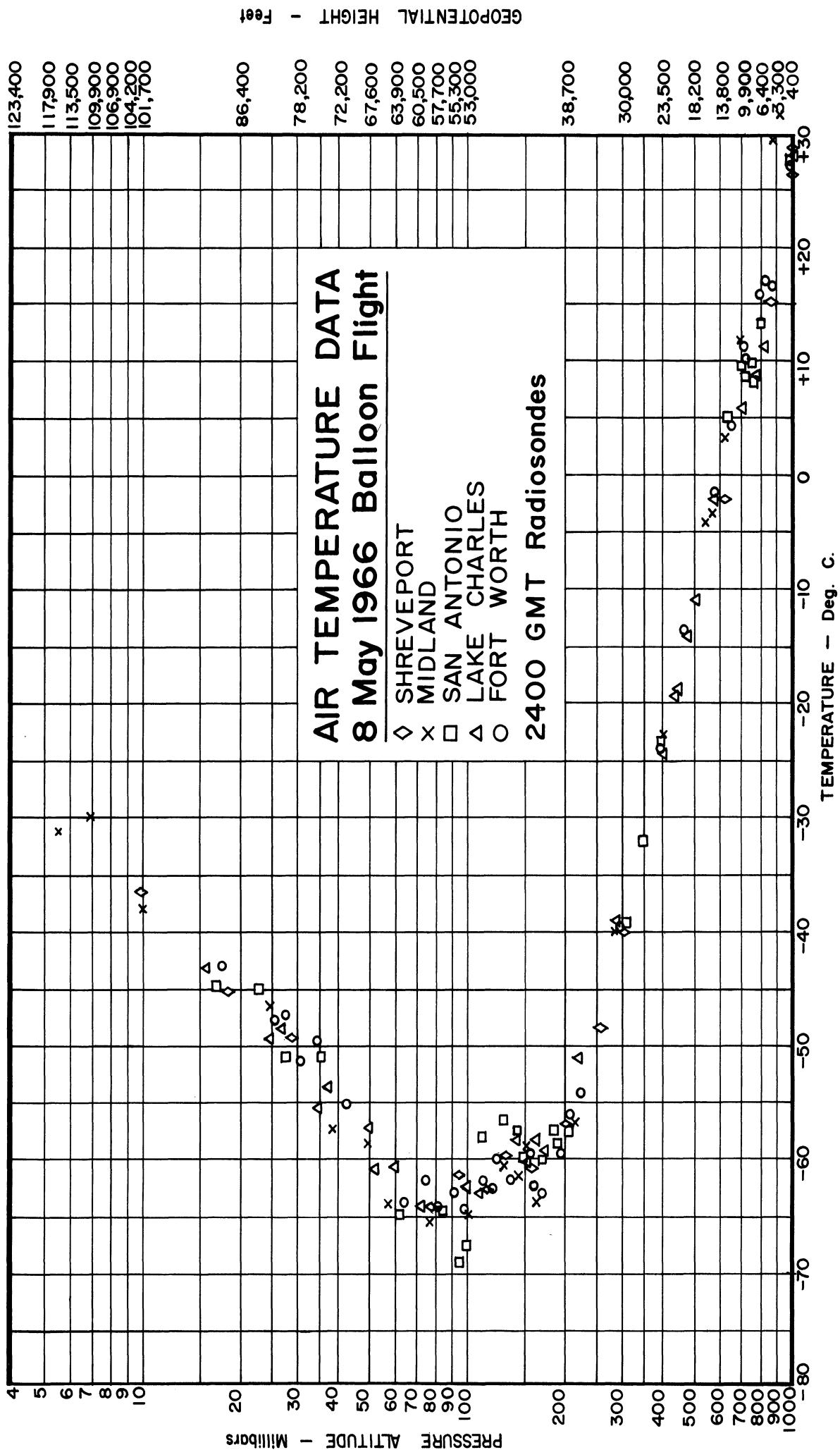


Figure 5

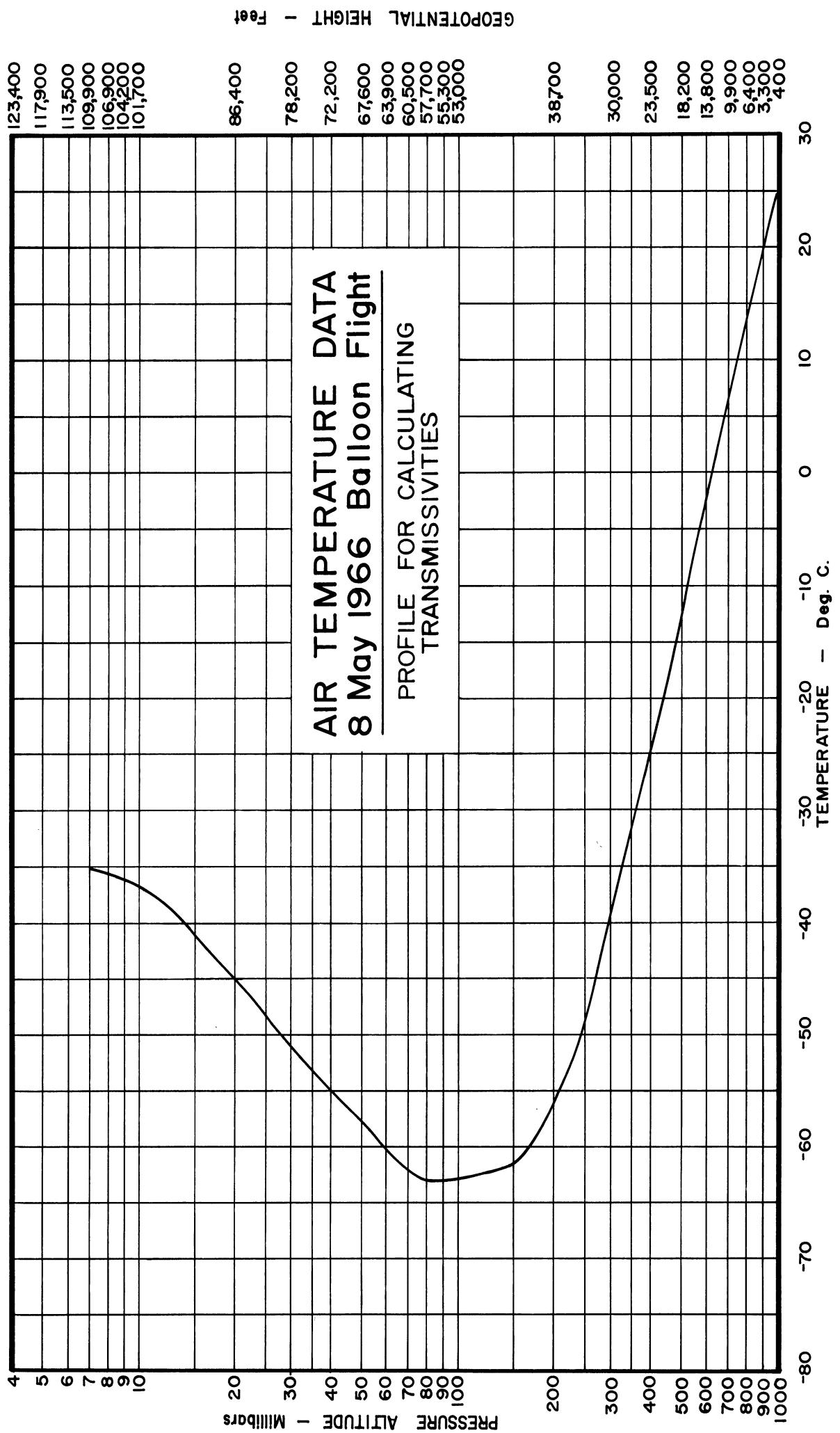


Figure 6

SUN AZIMUTH AND ELEVATION ANGLES  
8 May 1966 Balloon Flight

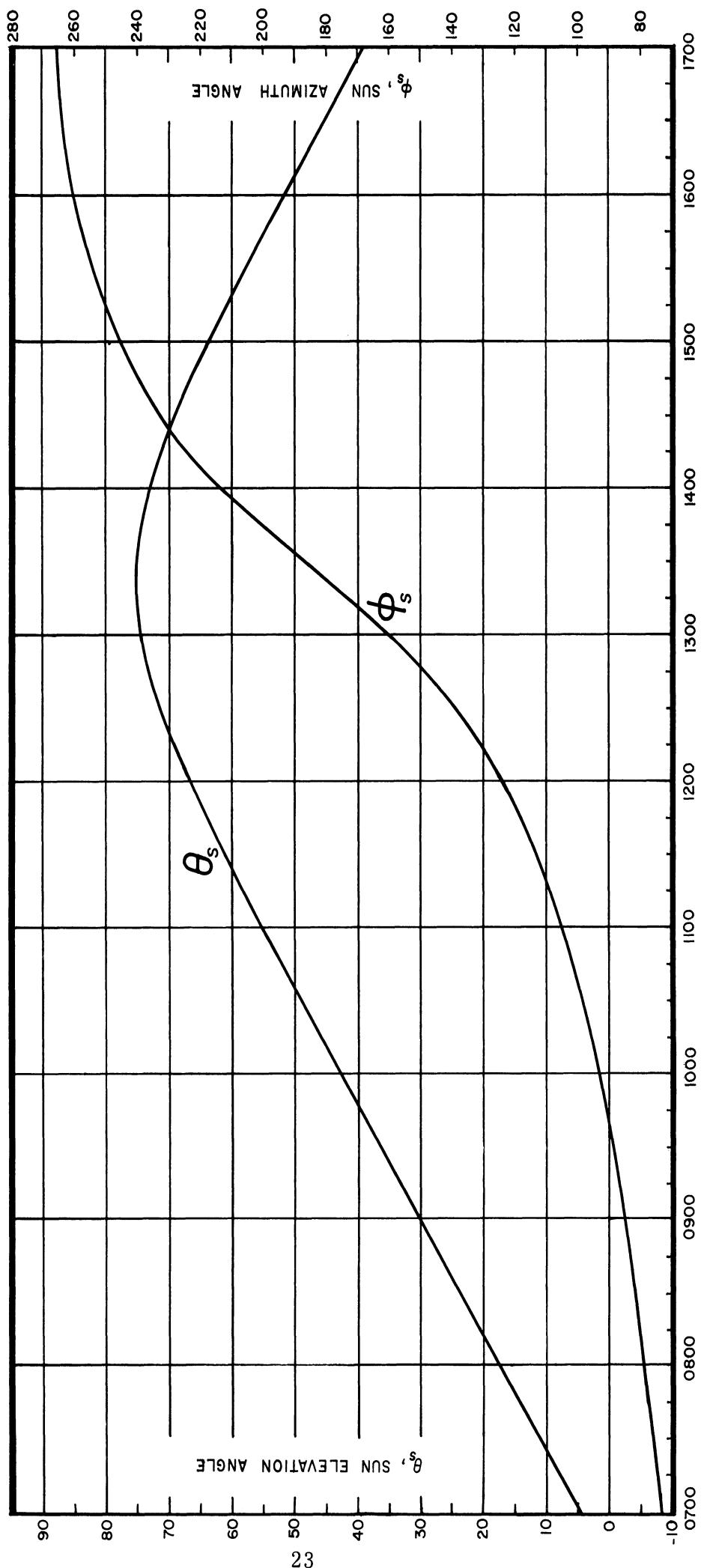


Figure 7

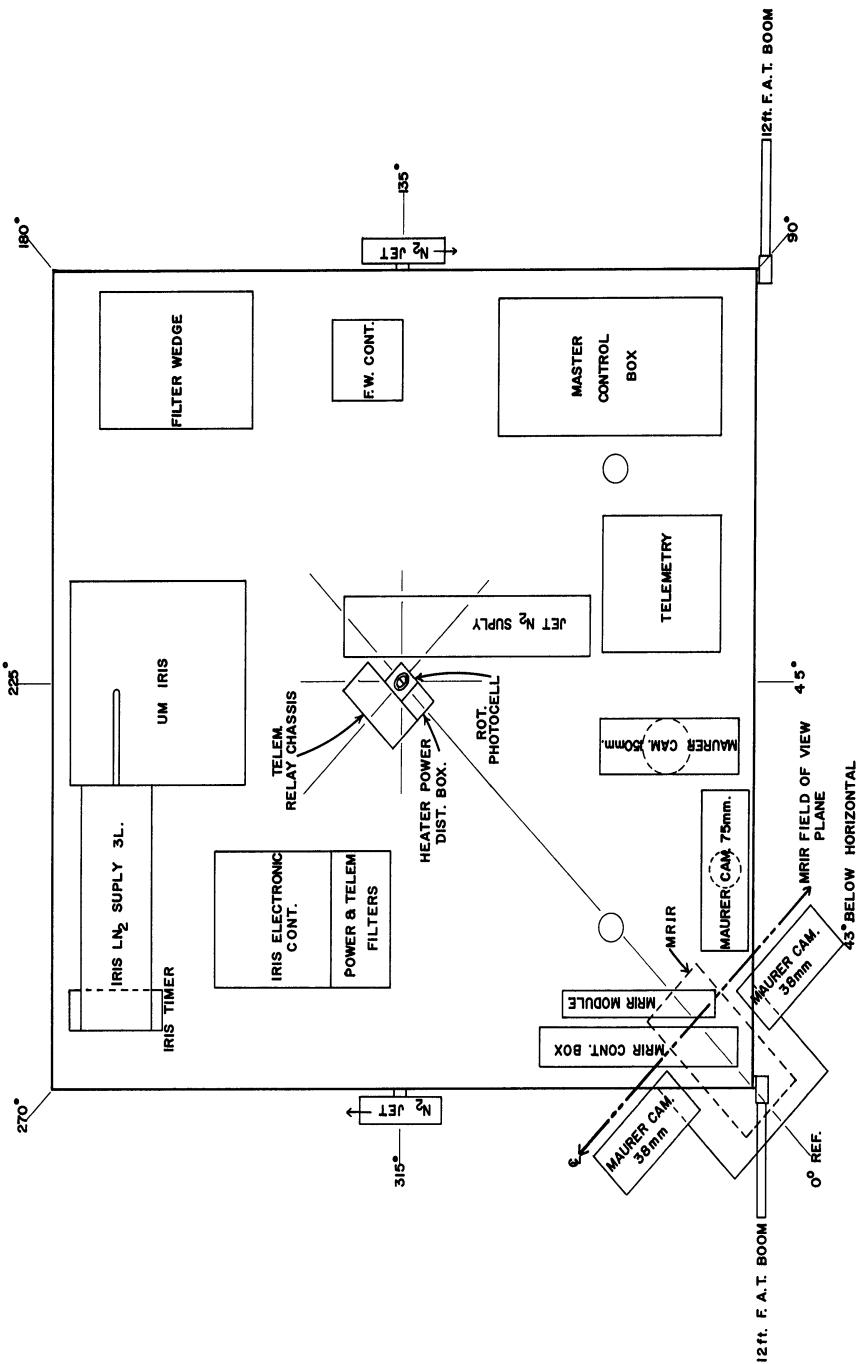
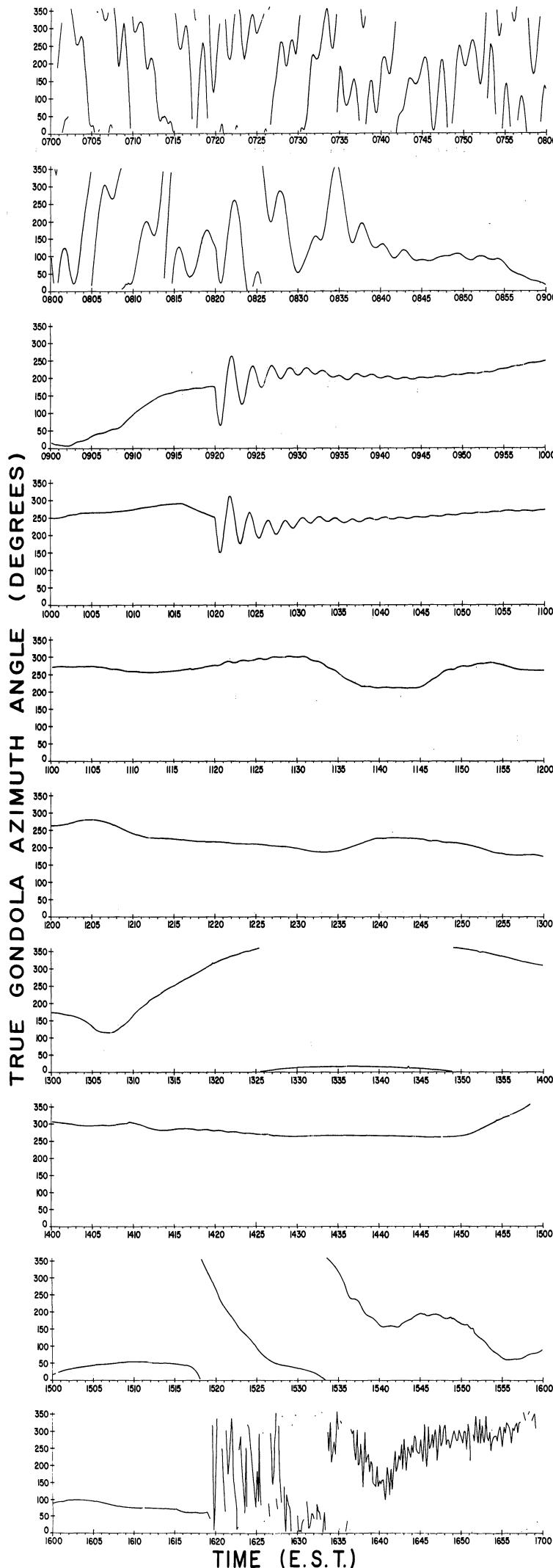


Figure 8



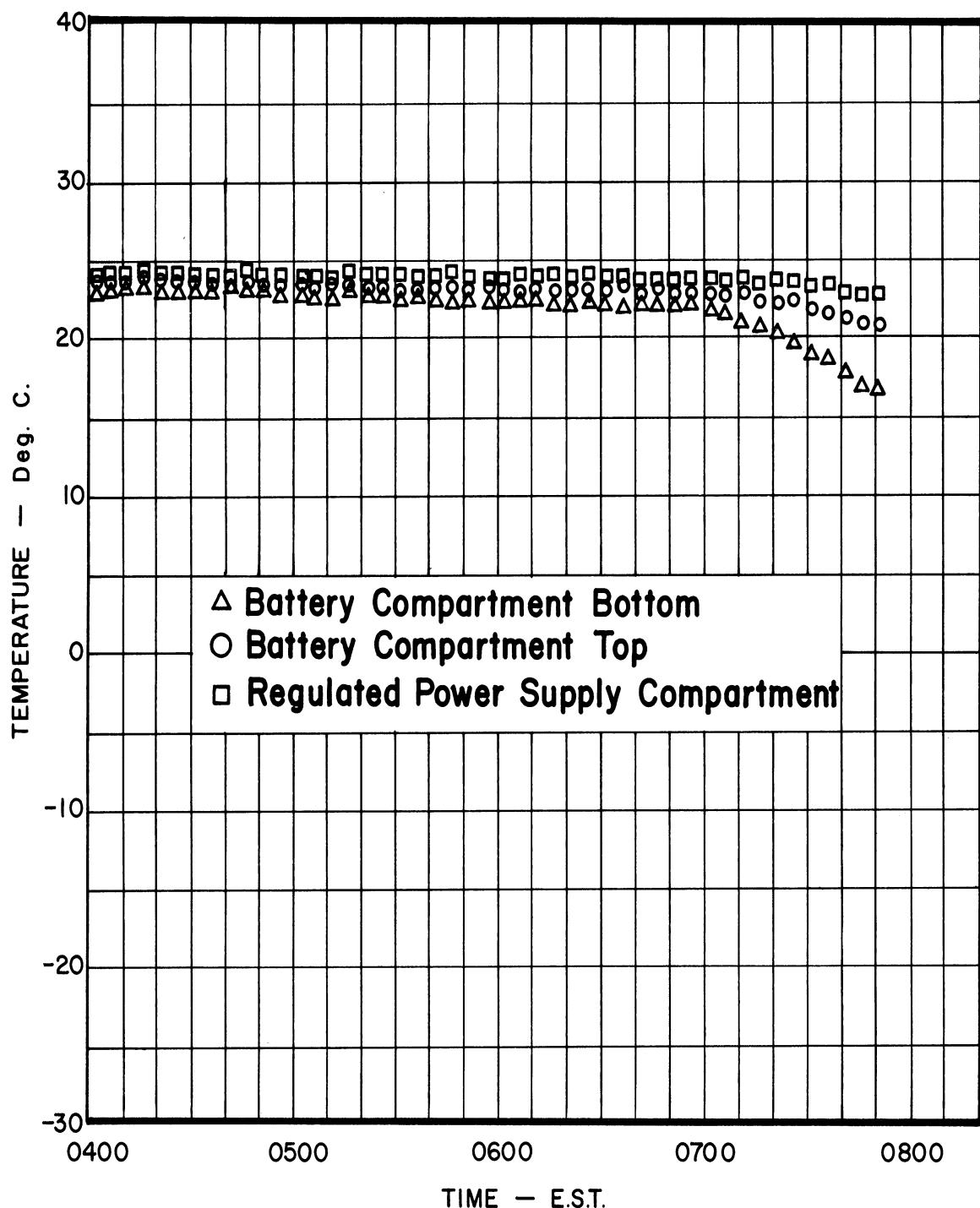


Figure 10

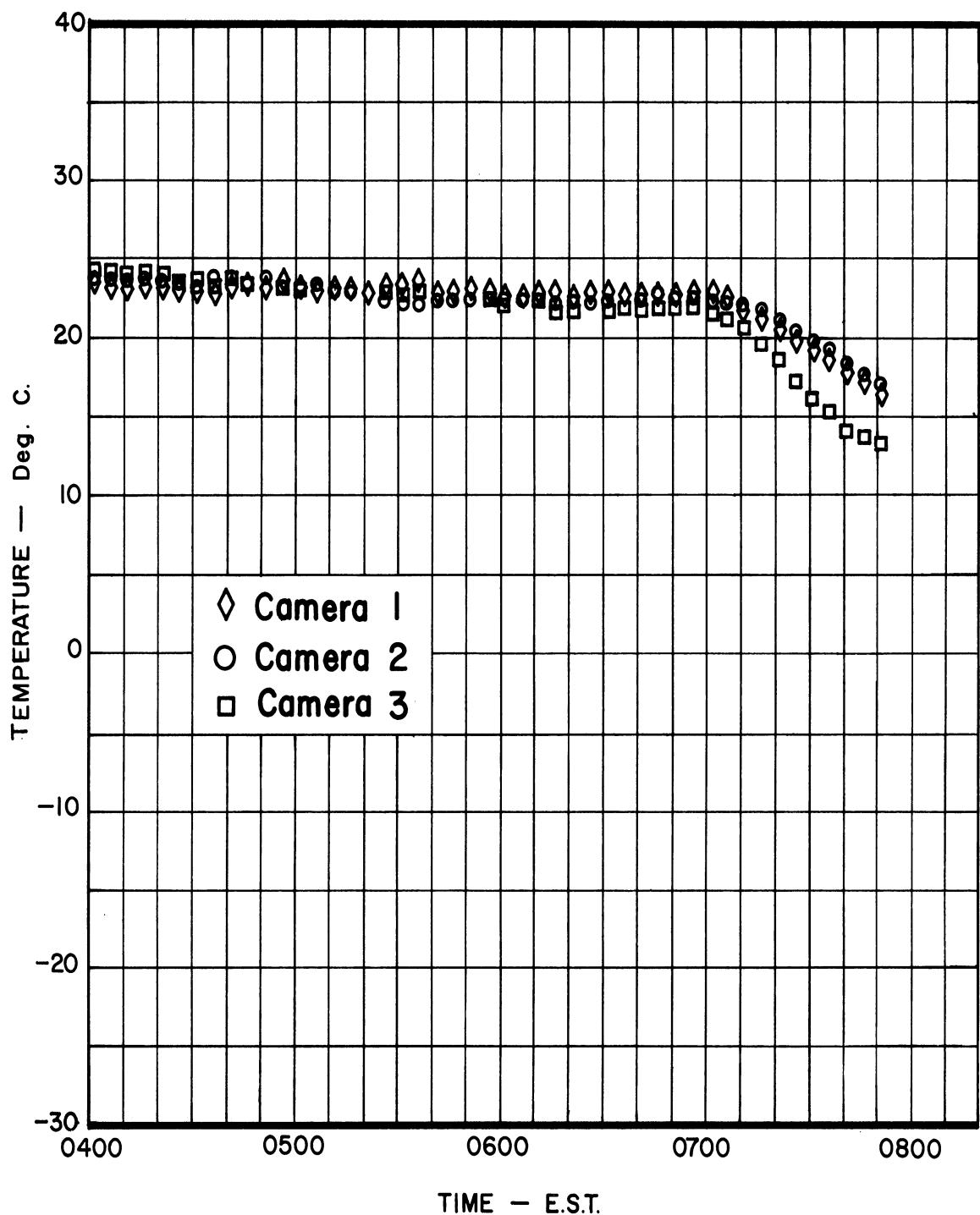


Figure 11

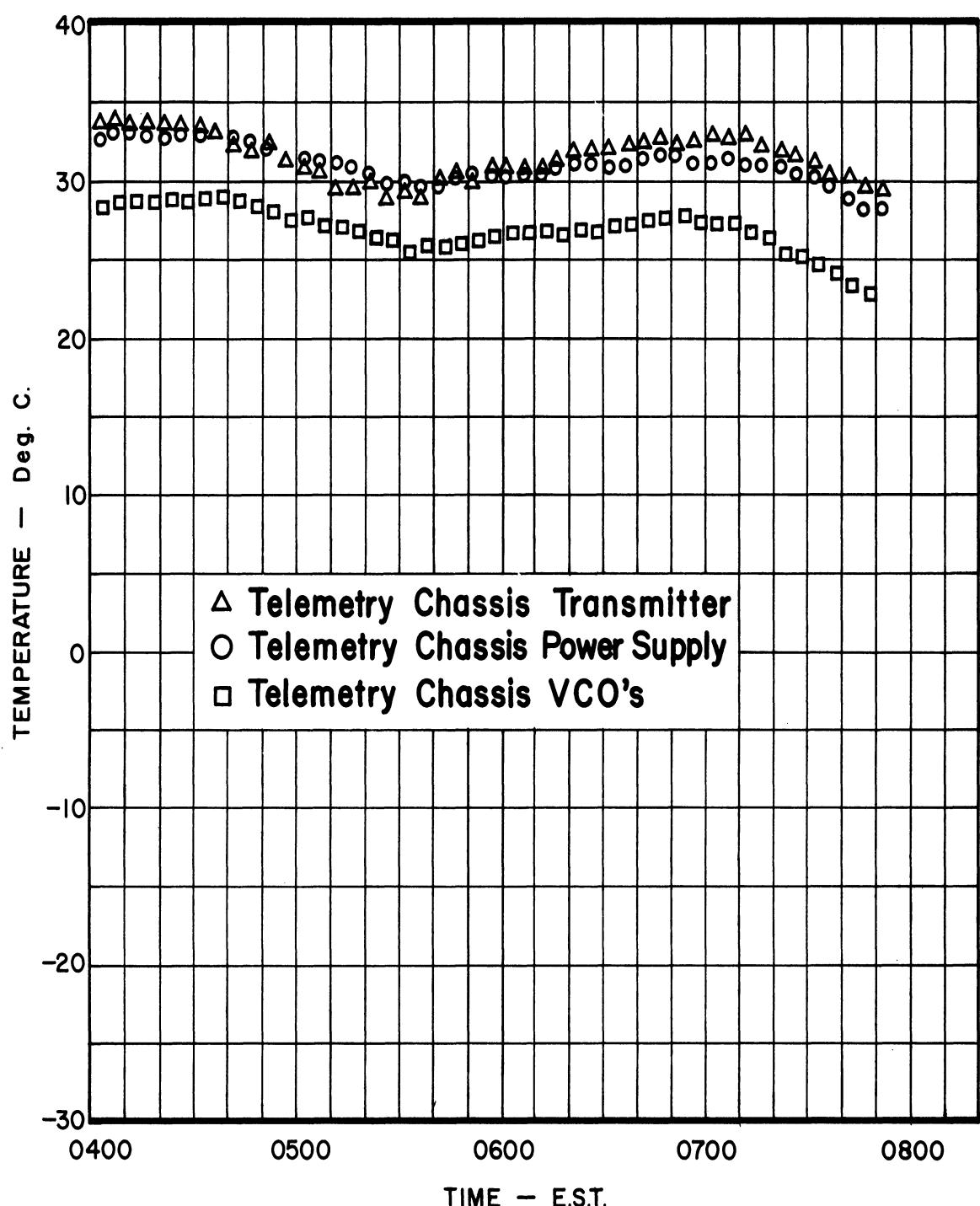


Figure 12

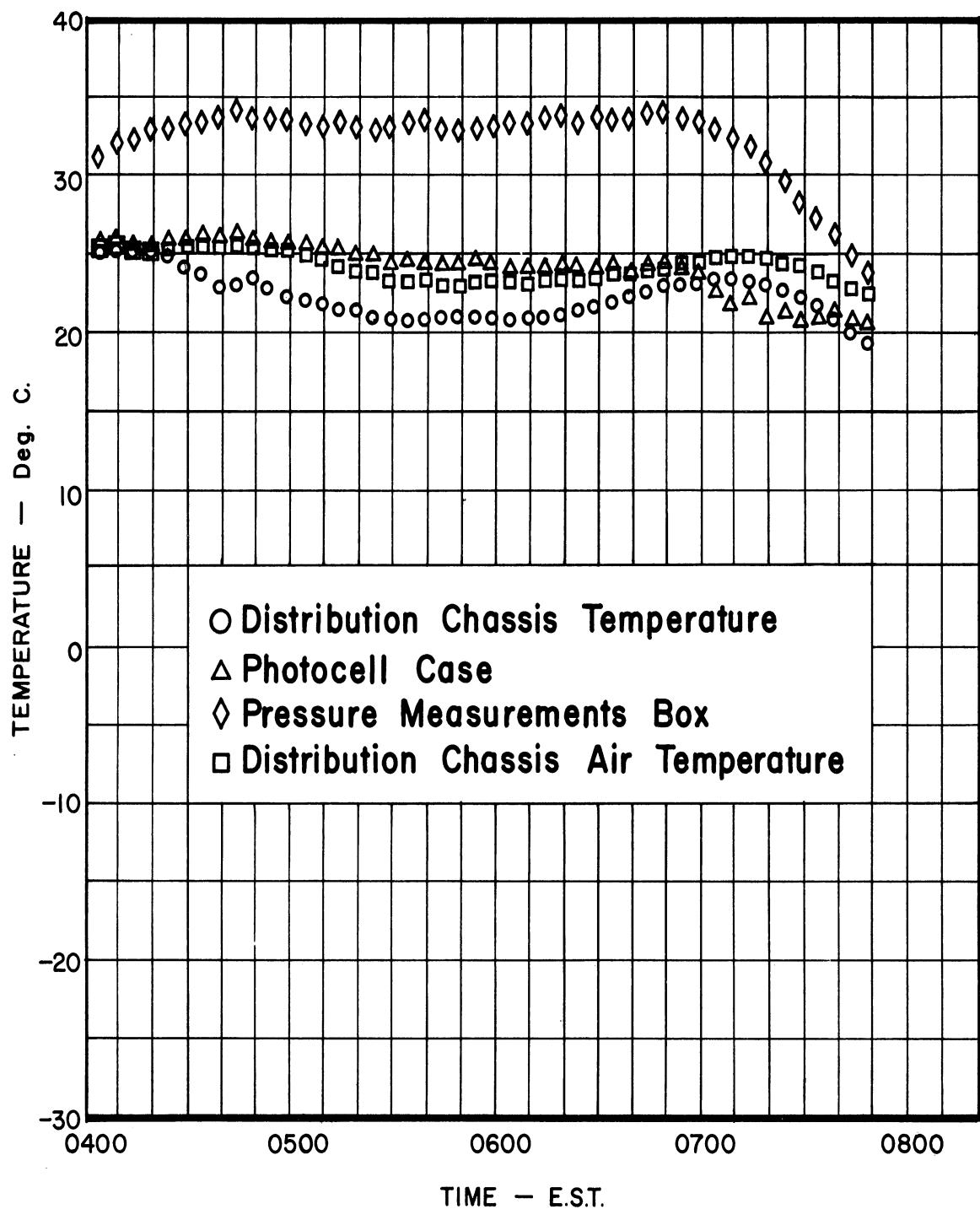


Figure 13

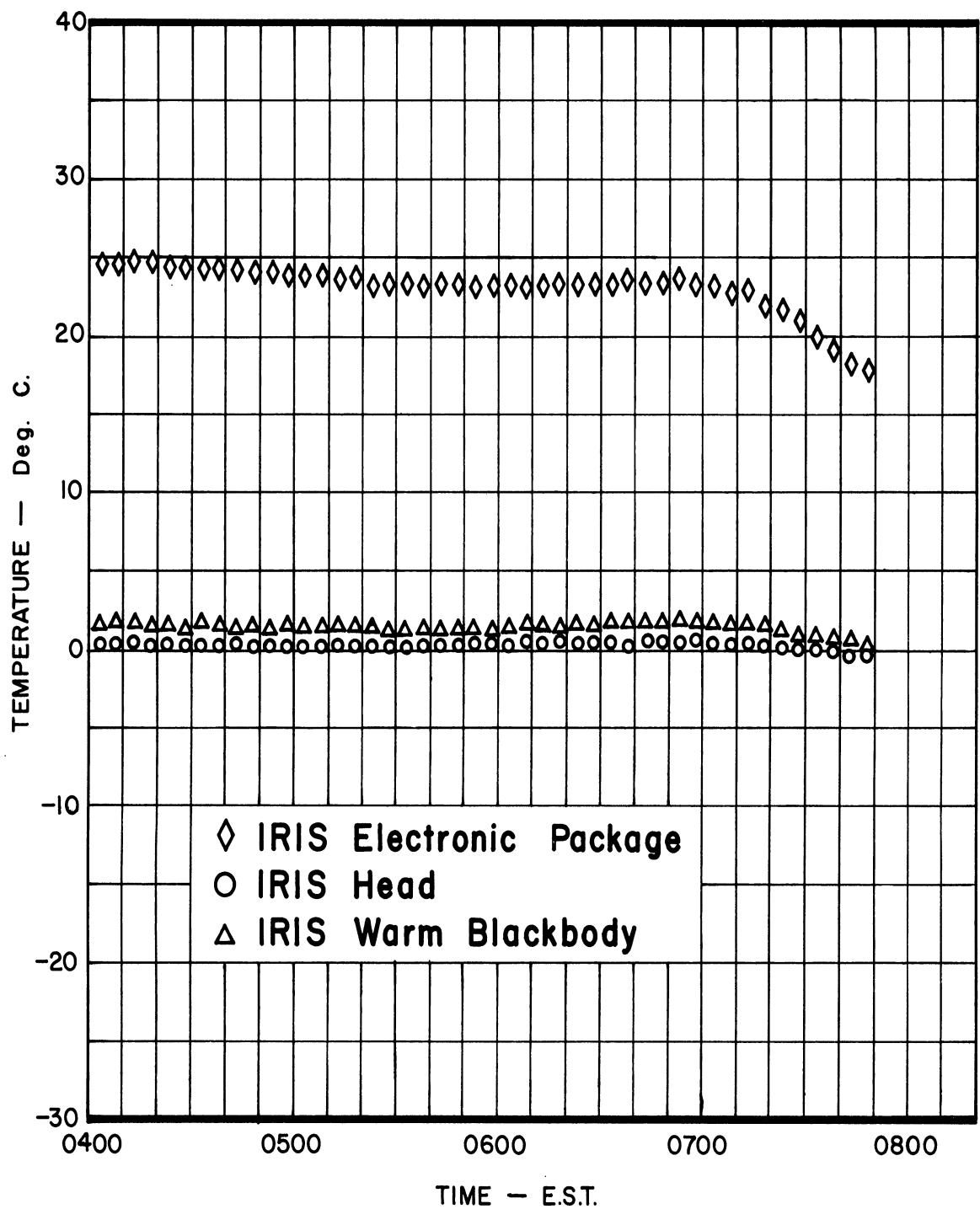


Figure 14

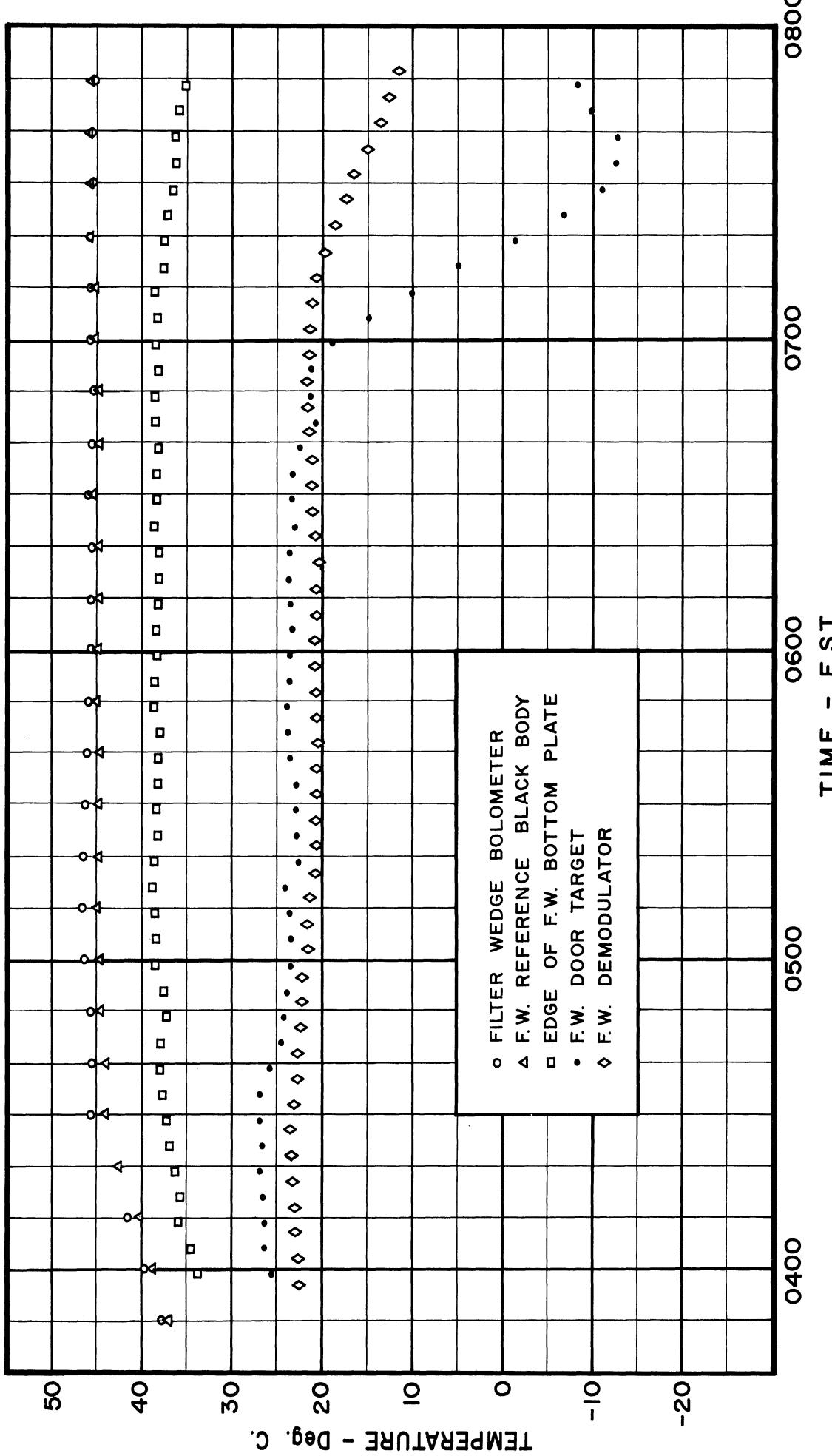


Figure 15

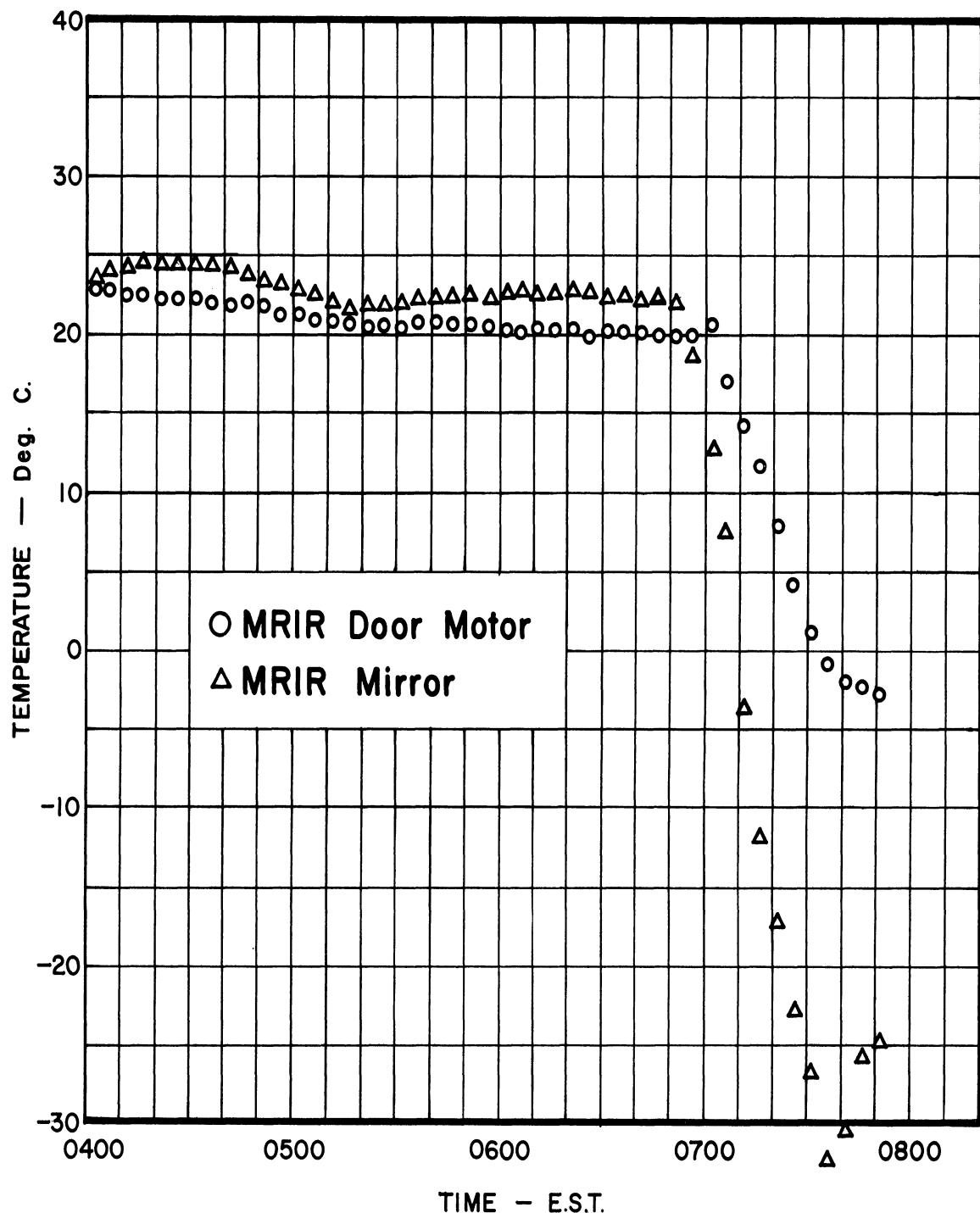


Figure 16

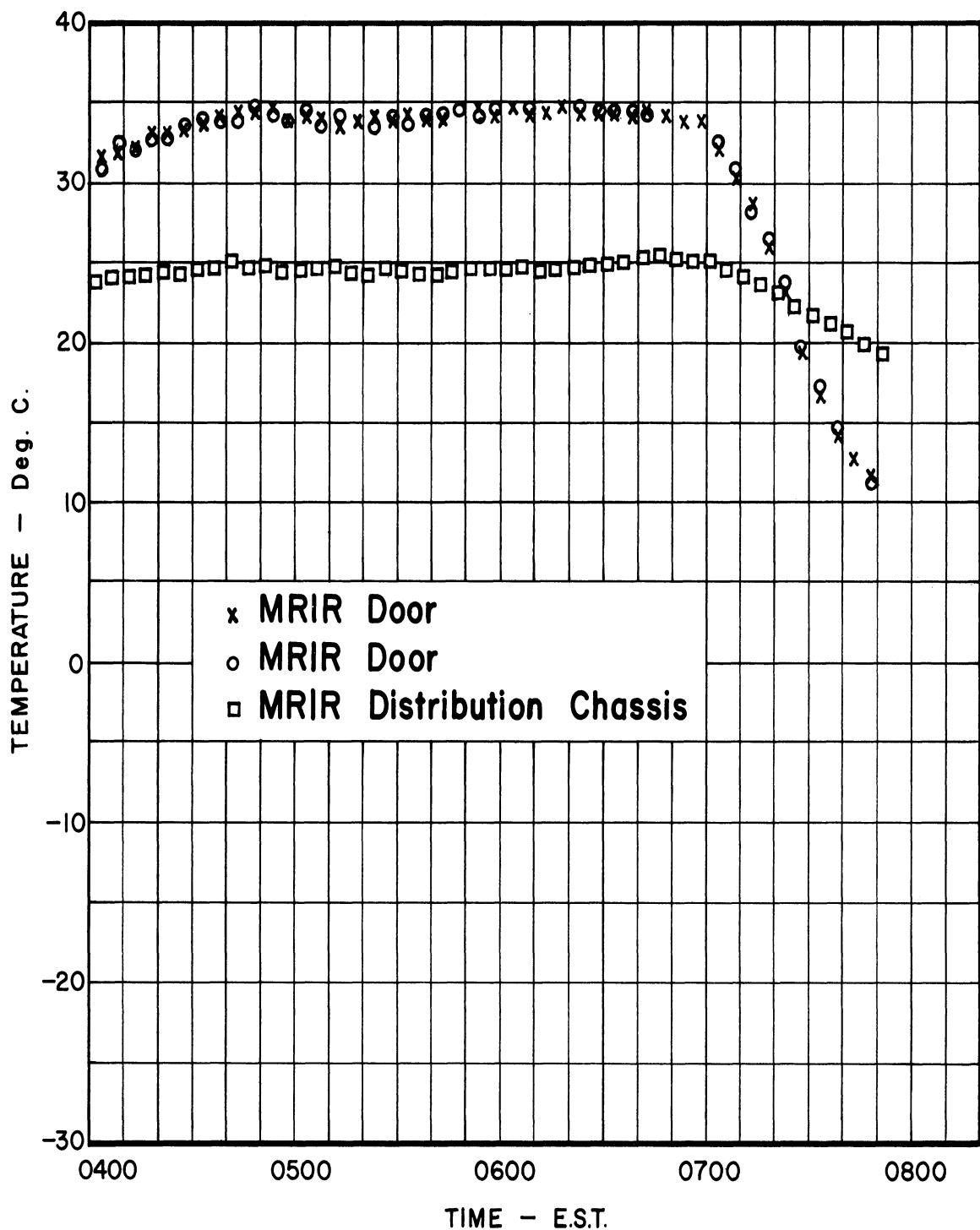


Figure 17

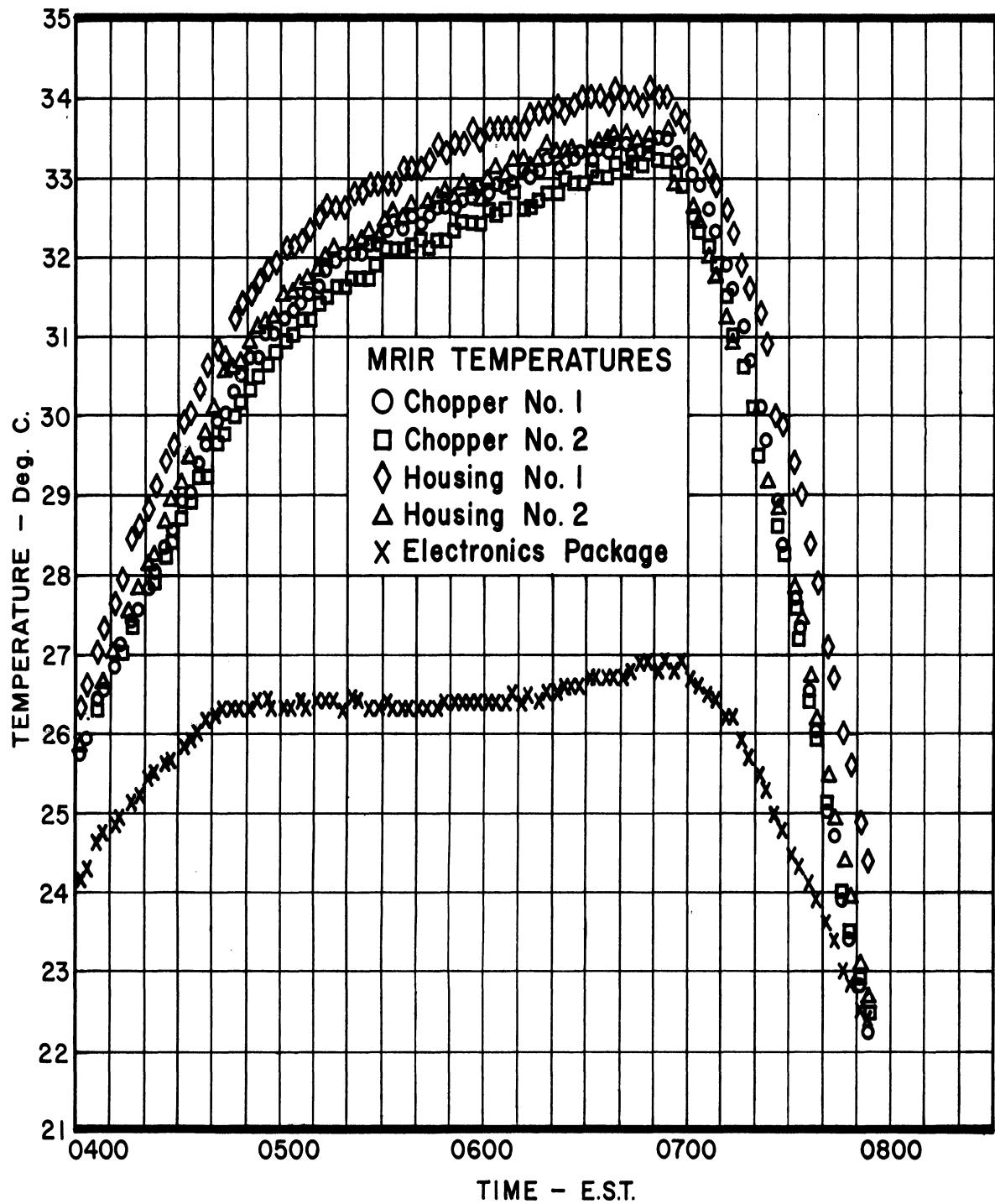


Figure 18

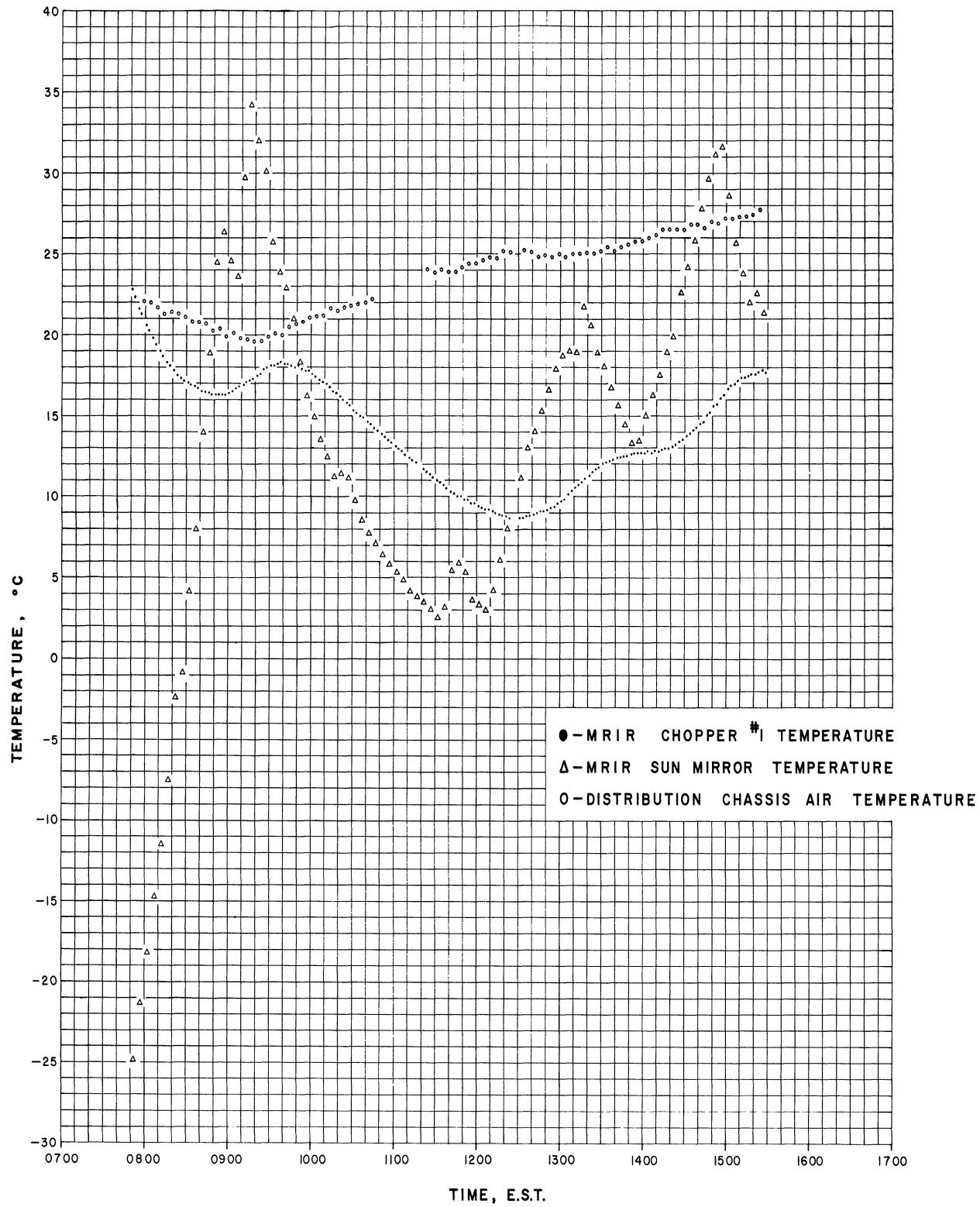


Figure 19

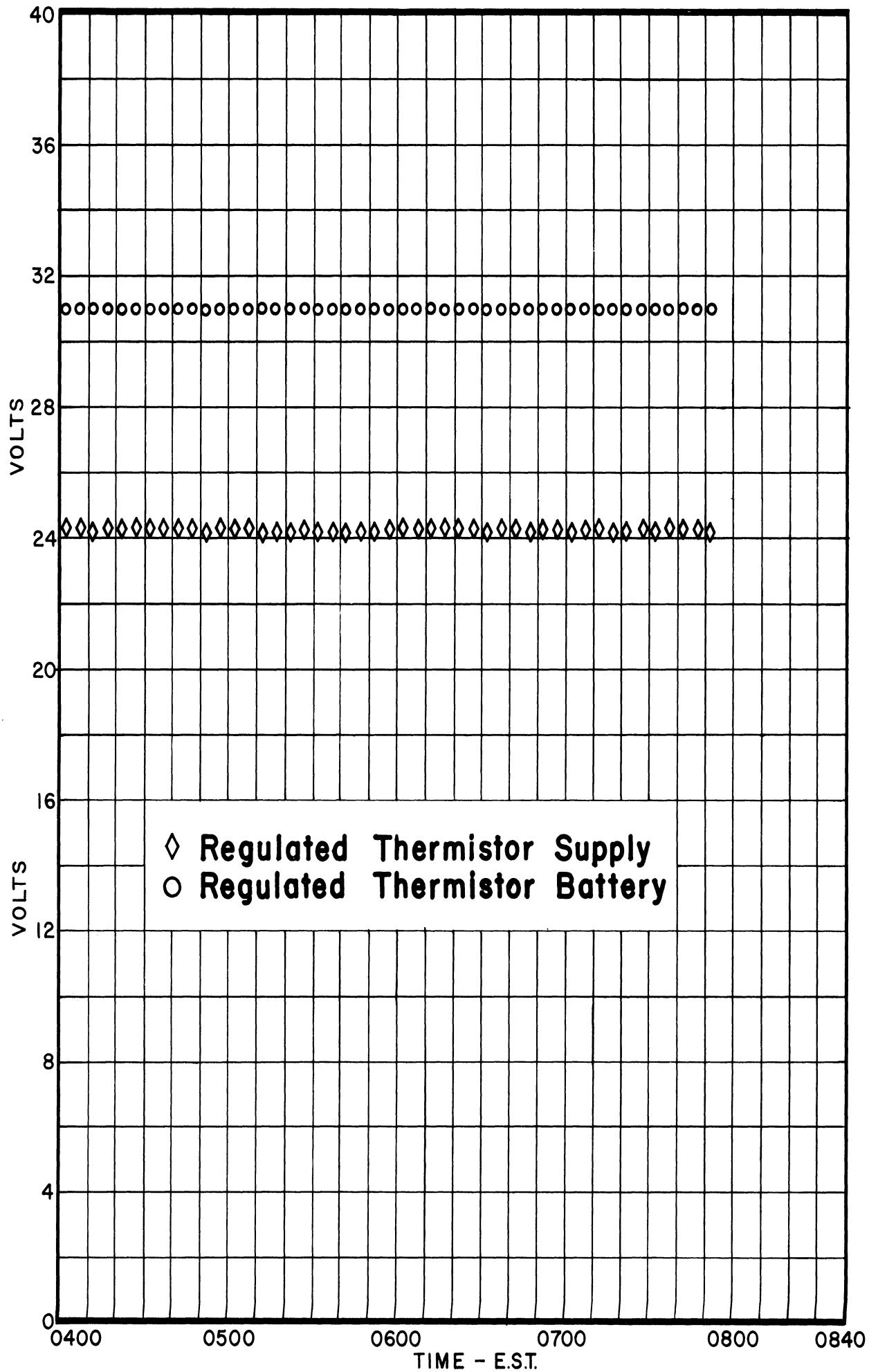


Figure 20

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