

THE UNIVERSITY OF MICHIGAN  
College of Engineering  
Department of Mechanical Engineering  
Cavitation and Multiphase Flow Laboratory

Report No. UMICH 306090-1-F

CAVITATION - EROSION RESISTANCE FOR CAST AND WELD DEPOSITED  
CORROSION RESISTING STEELS FOR BIRDSBORO CORPORATION

by  
(Niranjan)  
N. R. Bhatt  
F. G. Hammitt

Financial Support Provided by:

Birdsboro Corporation  
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## ABSTRACT

Cavitation - corrosion tests have been conducted in a vibratory facility (20 kHz, 2 mil double amplitude) upon cast and weld deposited corrosion resisting steels at a water temperature of 120<sup>o</sup>F and a pressure of 1 atm to provide damage rates for the different materials provided by Birdsboro in terms of MDPR and incubation period. Correlations of loss rates with mechanical properties are also shown with correlation coefficient and factorial standard error.

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## I. INTRODUCTION

The objective of this project was to provide cavitation damage test data for various stainless-steel type materials (supplied by Birdsboro Corporation) of interest for use in applications where intense cavitation exists. Our modified cavitation damage vibratory system, using a baffle-plate around the vibrating specimen was used to obtain more uniformity in damage and greater repeatability of damage rate. It was found in preliminary tests<sup>(1)</sup> that increased repeatability was in fact achieved with this method as compared to the conventional vibratory test arrangement. The tests were run at 120<sup>o</sup>F rather than at room-temperature since damage rates are considerably greater at that temperature and hence test time is minimized.

The properties of the materials tested are listed in Table I along with damage rates and MDPR\*. The modified cavitation damage vibratory system provides 2 mil double amplitude at 20 kHz. The test conditions and test procedure used are specified in Table II.

## II. EXPERIMENTS AND RESULTS

### A. Experimental Facilities

The modified experimental facility<sup>(1)</sup> differs from that used in the conventional vibratory test<sup>(2, 3, e. g.)</sup> only in that the specimen is positioned within and concentric with a circular hole in a baffle-plate. The radial clearance with the baffle plate must be a minimum (3 mils was used in the present test). The arrangement is shown in Fig. 1. The horn, transducer assembly, and flange are unchanged from the conventional arrangement, but the baffle-plate is mounted firmly to the flange to maintain the required parallelism and flushness with the specimen face, the

---

\* MDPR = Mean Depth of Penetration Rate = Vol. Loss Rate/Spec. Ar.

desired distance from the flange, and the concentricity with the horn and specimen axis. It was found that optimum uniformity of damage occurs in the flush condition (measured when horn is not operating). Water level in the test vessel is maintained 1-1/2 in. above the top surface of the baffle-plate.

The specific vibratory facility, to which the baffle-plate arrangement was later added, was designed for high-temperature tests with various fluids<sup>(3)</sup> and hence includes a sealed flange which also supports the horn. Hence, tests at higher than atmospheric temperature and pressure are not inconvenient if this were desired for future work.

Horn amplitude is monitored by a power meter provided in the driver unit. This unit in turn is calibrated for each specimen with a Fotonic Sensor (MTI Inc., Latham, New York) accurate to about 5% of the desired amplitude. Frequent measurements indicate that frequency remains constant to the order of 0.1% of the desired value. Temperature is automatically controlled by the heater power control to the water bath surrounding the vessel. Air content of the test water (distilled) was maintained at an approximately constant value, somewhat less than saturation at STP, by using a 30-minute pre-run with a dummy specimen to achieve an equilibrium air content somewhat less than saturated. Experience has shown that an air content so obtained remains relatively constant throughout a test. For each weighing of specimens, a wash and dry procedure is used as explained in Table II, where other facility procedures and parameters are listed.

### B. Experimental Results

The raw data for all 99 specimens are tabulated in the Appendix, and have been plotted in terms of weight loss vs. time of exposure. Fig 2 through 31 comprise a separate curve sheet

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for each material, with separate curves for each specimen.

The materials have been stamped from A-1, 2, 3, to Z-1, 2, 3 and A'-1, 2, 3 to C'-1, 2, 3. The corresponding material name and number can be found in Table I where all other pertinent information is included. Of the materials tested, A'-1, 2, 3, AM355 stainless steel was found to be most resistant to cavitation and G-1, 2, 3, 25CN carbon steel was found to be least resistant. The factor between these extremes is about  $\times 5$  in terms of maximum MDPR. The materials are rearranged accordingly to resistance ranking in Table III. The materials have been numbered 1 through 30 according to increasing order of maximum MDPR, i. e., volume loss rate. The most resistant is No. 1 (AM 355 Stainless steel)\* etc. This numbering system has been used throughout all the Tables and Figures.

The raw data has been plotted on each of the individual material curve sheets (Fig. 2-31) as weight loss vs. time of exposure. For each specimen, the test has been continued until the maximum weight loss rate had been reached, as determined by subsequent reduction in rate. Normally, seven hours sufficed for all the materials. Hourly measurements of weight loss were made. The maximum weight loss rate and MDPR are taken from these averaged curves. Individual incubation periods are found for each specimen by extrapolating the maximum damage rate portion of the curve to zero loss. The reciprocal of the average maximum MDPR (or weight loss rate) considering all specimens tested is taken as the unit of merit for each material on which the individual listing of the material from 1 to 30 is based. The pertinent individual specimen values and averaged values are listed in Tables I and III.

As is well known, the damage rate usually follows a characteristic S-type curve for tests of this sort, characterized by an initial period of small or zero measurable weight loss followed by a period of relatively constant weight loss rate, and then

\* It is interesting to note that there is a factor of more than 3 in MDPR between the various types of stainless steel themselves (excluding carbon steel).

a period of decreasing weight loss rate. Eventual fluctuations of the weight loss rate may occur, or the rate may continue to decrease with additional exposure. It is our belief, generally shared by most investigators at the present time, that the maximum volume loss rate is the most significant parameter for comparison of specimens. The incubation period may also be of prime importance in applications where it is more desirable that little or no cavitation damage be incurred than that an eventual minimum damage rate exist. Hence, incubation period has also been tabulated. The most and least resistant materials are the same according either to MDPR or Incubation Period. Some of the relative rankings are quite similar as #6 and 8, #21, 22, 23, and 25 for example, and perhaps others. Others, however, are very different. The reasons for these differences at the present time are unknown, but perhaps later more detailed study of the photomicrographs and test results may shed some light (Tables I and II).

Fig 32 to 37 are photographs of typical specimens of each material at or near the conclusion of the test. The MDP value and time of exposure at the time of the photograph are shown in the figure legends. Some differences in uniformity and pitting and damage patterns are evident from an examination of these photos, though a direct comparison is not possible, since the accumulated volume loss is less for the more resistant materials. Fig. 38 through 61 are photomicrographs of the grain structure for each material supplied by Birdsboro.

One classical goal of cavitation damage research is to find a usable correlation between cavitation damage resistance ( $1/\text{MDPR}$ ) and easily measurable mechanical properties of the material. This goal appears elusive, perhaps because cavitation attack is on a micro-scale and involves very high rates of loading (duration is order or one microsecond) whereas the conventional mechanical properties involve macro-failures of the materials, and the loading is relatively very gradual compared to cavitation attack. Due to the apparent lack of a good correlation with standard mechanical properties, it appears that a more detailed consideration of the surface reaction to cavitation must be made if an ability to predict cavitation resistance is to

be attained, or the capability of designing materials specifically for this purpose. A more detailed study of the grain structures (Fig. 38--61) may be useful for this purpose. Of course it may well be more feasible to simply test the cavitation resistance directly as was done in the present instance.

### C. Data Correlations

Computer correlations have been made wherein the present materials, as well as a group of tool steels and another of miscellaneous metallic alloys which we had previously tested are included. The results are shown in Table IV (A, B, C.) and in Fig. 62--63. Table IV-A is for the Birdsboro materials alone, IV-B for all materials (including Birdsboro) and IV-C for all materials excepting Birdsboro.

The best correlation of damage resistance for the Birdsboro materials alone is with Brinell hardness (BHN). This parameter has often been used in the past for predicting purposes and has the strong advantage of simplicity. Recent tests have often shown that ultimate resilience (UR) or a combination between (UR) and strain energy (SE) or (BHN) was the most successful (4, e. g.). It is noted (Table IV-C) that this is still the case for the materials we have tested excluding the Birdsboro materials, i. e. a set of predominantly stainless steels. It is also interesting to note that while the correlation coefficients for the Birdsboro materials are not particularly impressive, the scatter is very small (factorial standard error of estimate = 1.26), compared with the other data sets, i. e. the total material set and that excluding the Birdsboro materials (Tables IV-B, C).

Finally, it should be mentioned that Strain Energy (SE)<sup>\*</sup>, which has often been suggested in the past as a correlating parameter, is considerably worse in all regards than the other possibilities which are included in these tables.

\* Area under conventional stress-strain curve

### III. CONCLUSIONS

The minimum cavitation volume loss rate (MDPR) was found for material AM 355 Stainless Steel and the maximum for material 25 CM Carbon Steel. The factor in MDPR between these materials is about 5. The same relative ranking for these two end materials is maintained for incubation period, and the factor is about 6. The relative rankings for some of the materials with either of these two merit parameters is quite similar, and for others it is quite different (Table III).

Although the mechanical properties of these materials cover only a relatively small range, the reciprocal volume loss rates can be quite accurately correlated in terms of Brinell Hardness. Ultimate resilience, which had been quite successful for other material sets, is much less so for the present set which is composed predominantly of stainless steels. The reason for this difference is not known but may be disclosed by further study of the results along with the photomicrographs. This may allow the development of an even more useful grading parameter for these materials, perhaps involving grain size as well as hardness.

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TABLE I

U of M No.	Material No. and Name	Hardness (Rockwell-C) R <sub>c</sub>	Hardness (Brinell) BHN	Tensile Strength T.S. psi	Yield Strength Y.S. psi	%Elongation 2 in.	%Area Reduction at 70°F	Density gm/cm <sup>3</sup> at 70°F	Elastic Modulus E psi	Weight Loss Rate mg/hr	MDPR mils/hr	Incubation Period hr.	Ave. WLR Ave. MDRP
A-1	Grad CF 8									23.00	0.7728	1.00	
A-2	Heat E - 4012		150	82700	52600	53%	7.75			19.00	0.6384	1.00	21.83
A-3	A-1, A-2, A-3; A-4, A-5, A-6, A-7, A-8, A-9, A-10.		150	82700	52600	53%	7.75			23.50	0.7896	1.00	.7336
A-4	Grad CF-8		150	82700	52600	53%	7.75			19.50	0.6552	1.00	
A-5			150	82700	52600	53%	7.75			19.00	0.6384	1.00	20.33
A-6			150	82700	52600	53%	7.75			22.25	0.7560	1.00	.6832
A-8	Grad CF-8		150	82700	52600	53%	7.75			21.75	0.7308	1.00	
A-9			150	82700	52600	53%	7.75			23.50	0.7896	1.00	22.66
A-10			150	82700	52600	53%	7.75			22.75	0.7644	1.00	.7616
C-1	CA7M		160	66800	33150	44.0%	8.00			14.347	0.4670	0.9	
C-2	Stainless		160	66800	33150	44.0%	8.00			15.642	0.5091	0.65	15.35
C-3	Heat # C-808 Sol. quenched from 2000°		160	66800	33150	44.0%	8.00			16.071	0.5231	0.35	.4997
GA15#1	CA-15									19.90	0.6808	0.70	
CA15#2										20.80	0.7116	0.65	20.35
D-1	CA6NM		241	118950	105950	18.0%	53.8%			12.666	0.4329	0.35	
D-2	Stainless		241	118950	105950	18.0%	53.8%			8.783	0.3001	0.90	10.05
D-3	Heat #E-4967,		241	118950	105950	18.0%	53.8%			8.712	0.2977	0.70	0.3435
E-1	CF 8		150	73220	39850	63.5%	7.75			22.00	0.7392	0.70	
E-2	Stainless		150	73220	39850	63.5%	7.75			29.60	0.9906	1.25	23.70
E-3	Heat # E 4957		150	73220	39850	63.5%	7.75			19.50	0.6552	1.00	.7950
F-1	CF 8		150	77750	41150	57.0%	7.75			22.70	0.7627	0.75	26.511
F-2	Stainless		150	77750	41150	57.0%	7.75			30.32	1.0188	0.9	.8907
F-3	Heat #88406		150	77750	41150	57.0%	7.75			--	--	--	
G-1	25 CM		140	76450	43500	33.0%	51.3%			42.62	1.4121	0.5	
G-2	Carbon Steel		140	76450	43500	33.0%	51.3%			34.60	1.146	0.00	38.21
G-3	Heat # E 4945		140	76450	43500	33.0%	51.3%			37.42	1.2365	0.25	1.264
H-1	45 A 7		311	1500850	121250	12.5%	41.2%			10.40	0.3445	1.00	
H-2	Carbon		311	1500850	121250	12.5%	41.2%			15.02	0.4976	1.35	12.71
H-3	Heat # F-5144		311	1500850	121250	12.5%	41.2%			11.00	0.900	0.80	.4221
I-1	CA - 15	23°	220	103200	83500	21.0%	43.3%			18.00	0.6158	0.85	
I-2	Heat # F-5144		220	103200	83500	21.0%	43.3%			19.40	0.6637	0.55	18.63
I-3			220	103200	83500	21.0%	43.3%			18.50	0.6329	0.65	.6374

TABLE I (cont. 1)

J-1	CA-15	187	91550	75300	29.0%	60.3%	7.612	14.00	0.5097	0.65
J-2	LO CR, LO ST							12.68	0.4338	0.75
J-3	Heat F-5264							14.09	0.4820	0.00
K-1	CA-15	285	133950	120900	17.0%	51.1%	7.612	12.10	0.4139	0.875
K-2	CO CR, LO SF							11.33	0.3876	0.95
K-3	Heat E-5036							10.70	0.3660	0.5
L-1	CF 8	150	80000	45000	42.5%		7.75	15.74	0.5288	0.85
L-2	Stainless							15.20	0.5107	1.25
L-3	Heat # F-5580							18.40	0.6183	0.95
M-1	CF-8	150	79000	49950	45.0%		7.75	18.46	0.6202	0.5
M-2	Sol. quench.							17.32	0.5819	0.65
M-3	2000 F							19.01	0.6387	0.70
N-1	Arcos Stainlend	240	145550	115850	3.5%	10.6%	7.62	14.72	0.4946	0.30
N-2	13-4 Ni							16.36	0.5497	0.5
N-3	(For welding GAGNM as weld.							16.30	0.5477	0.00
O-1	Arcos Stainlend	240	132550	70650	17.0%	45.3%	7.62	18.24	0.6223	0.5
O-2	13-4 Ni							16.38	0.5598	0.75
O-3	Stress Relieved 1175 F							14.26	0.4873	0.60
P-1	304-L Sol)	156	72700	43800	68.0%		7.90	17.60	0.5800	0.40
P-2	Quenched 2050 F							17.50	0.5767	0.00
P-3								17.70	0.5833	0.60
Q-1	304-L	156	77450	37450	64.00%		7.90	20.20	0.6657	0.25
Q-2	Sensitized							--	--	0.25
Q-3	1250 F							16.00	0.5376	0.70
R-1	CF 8 M	160	78200	47950	50.00%		7.75	17.00	0.5712	0.55
R-2	Sol. quenched							16.25	0.5456	0.75
R-3	2050							16.10	0.5409	0.80
S-1	CF 8 M	160	78250	44250	36.00%		7.75	16.10	0.5809	0.625
S-2	As cast							15.75	0.5292	0.625
S-3								14.80	0.5025	0.75
T-1	CE 30	225	91700	60600	24.5%		7.67	14.80	0.5025	0.75
T-2	Water quenched							13.65	0.4635	0.75
T-3	2000 F							15.15	0.5144	0.60
U-1	CE 30	225	88.250	52600	28.0%		7.67	15.70	0.5331	0.50
U-2	As cast							Broken	--	--
U-3								17.00	0.550	0.51
V-1	308-L	160	72850	42350	54.0%		8.00	20.00	.650	0.00
V-2	Water quenched							20.00	.650	0.60
V-3	2000 F							16.50	.5439	0.49
W-1	308-L	160	73900	52500	49.0%		8.00	16.50	.5439	1.00
W-2	As welded							16.50	.5439	0.75
W-3								16.50	.5439	0.75

TABLE I (cont.)

X-1	308 Wire	160	90250	66650	34.0%	8.00	17.50	.552	0.75	18.25
X-2	As welded						19.00	.620	1.51	.585
X-3							Broken	--	--	--
Y-1	308 Wire	160	83500	53050	44.0%	8.00	18.50	.600	0.60	18.50
Y-2	Sol. quenched						18.50	.600	0.60	.6010
Y-3	2000 F						18.50	.600	0.60	.6010
Z <sub>1</sub> -1	E 410 Stainless	230	150000	92250	2.5%	7.0%	10.00	.340	0.75	10.40
Z <sub>1</sub> -2	As welded						10.50	.340	0.50	.337
Z <sub>1</sub> -3							10.70	.348	0.60	.337
Z <sub>2</sub> -1	E 410	230	112200	95750	18.0%	52.7%	20.00	.679	0.40	17.50
Z <sub>2</sub> -2	Stress Relieved						19.00	.645	0.60	.593
Z <sub>2</sub> -3	1300 F						13.50	.457	0.40	.593
A'-1	AM 355	350	179900	154300	17.0%	52.2	7.50	.247	1.00	7.66
A'-2	Stainless						6.00	.198	1.75	.253
A'-3							9.50	.314	1.50	.253
B'-1	CF 8 C	150	77550	43450	50.0%	7.75	18.50	.665	0.90	16.66
B'-2	Sol. quenched						16.00	.555	1.00	16.66
B'-3	Heat 2050 F						15.50	.539	1.10	.586
C'-1	CF 8 C	150	77050	39400	47.0%	7.75	13.00	.437	0.75	13.00
C'-2	As cast						13.00	.437	0.75	13.00
C'-3							13.00	.437	0.75	0.437



## TABLE II

### TEST PROCEDURE

1. Baffle-plate installed with axial clearances so that baffle-plate and specimen surface are flush with power off.
2. 4-1/2" distilled water depth, fresh each day with a 30 minute deaeration run (with dummy specimen) before start of actual tests to achieve equilibrium air content conditions for actual tests.
3.  $120^{\circ}\text{F} \pm 3^{\circ}\text{F}$  water temperature attained.
4. 1.69 psig (16.69 psia) air pressure in vessel.
5. Run at power settings to attain 2 mil double amplitude at 20 kHz.
6. Run in 1 hour increments to a cumulative time of 7 hours, or at least until maximum damage rate is attained.
7. Wash in acetone, then in methanol, then dry 5 minutes in vacuum at ambient temperature.
8. Torque applied to specimen is 90 in. lb., to achieve uniform and snug fit.

TABLE III  
NUMBERING SYSTEM

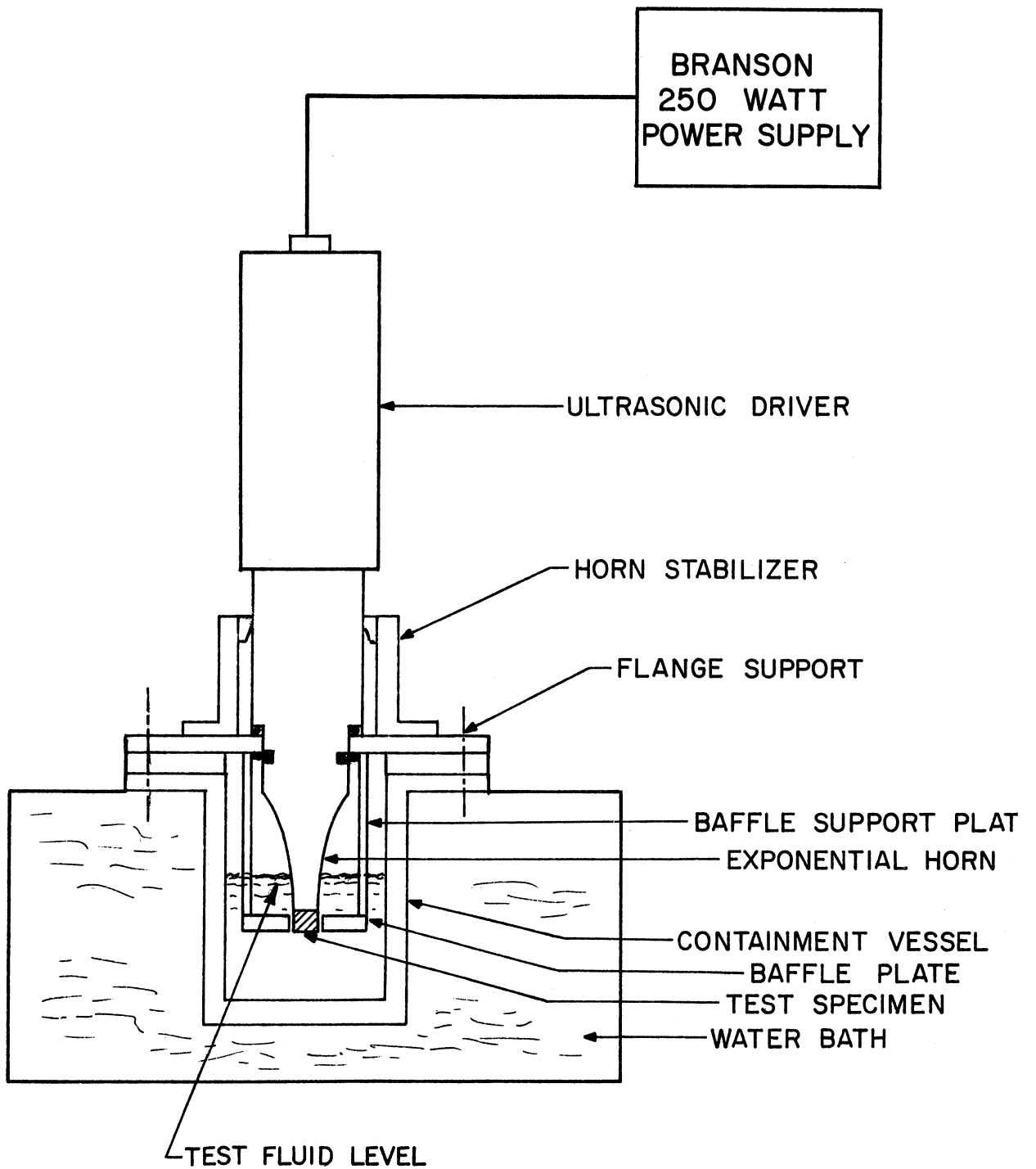
MDPR	Relative Ranking		Material Name and No.	MDPR* (mils/hr)	WLR* (mg/hr)	Incubation* Period (hrs)
	MDPR	Incubation Period				
1		1	A'1, 2, 3	0.253	7.66	1.625
2		18	Z <sub>1</sub> -1, 2, 3	0.337	10.40	0.500
3		15	D-1, 2, 3	0.3435	10.05	0.65
4		27	K-1, 2, 3	0.3891	11.37	0.625
5		19	H-1, 2, 3	0.4221	12.71	0.715
6		28	C'-1, 2, 3	0.437	13.00	0.750
7		29	J-1, 2, 3	0.4751	15.22	0.700
8		6	T-1, 2, 3	0.4903	14.41	0.750
9		8	C-1, 2, 3	0.4997	15.35	0.632
10		13	U-1, 2, 3	0.5230	15.42	0.550
11		5	S-1, 2, 3	0.5306	15.79	0.673
12		7	N-1, 2, 3	0.5370	16.31	0.400
13		24	W-1, 2, 3	0.5439	16.50	0.746
14		26	R-1, 2, 3	0.5514	16.41	0.625
15		11	L-1, 2, 3	0.5526	16.44	1.070
16		3	O-1, 2, 3	0.5564	16.29	0.616
17		9	P-1, 2, 3	0.5800	17.60	0.500
18		4	X-1, 2, 3	0.5850	18.25	1.130
19		14	B'-1, 2, 3	0.5860	16.66	0.950
20		16	Z <sub>2</sub> -1, 2, 3	0.5930	17.50	0.460
21		23	Y-1, 2, 3	0.6010	18.50	0.600
22		21	V-1, 2, 3	0.6136	18.20	0.550
23		25	M-1, 2, 3	0.6160	19.00	0.613
24		10	I-1, 2, 3	0.6374	18.36	0.683
25		22	Q-1, 2, 3	0.6657	20.20	0.600
26		2	CA15	0.6962	20.35	0.675
27		17	A-1-10	0.7250	21.60	1.000
28		20	E-1, 2, 3	0.7950	23.70	0.950
29		12	F-1, 2, 3	0.8907	26.511	0.825
30		30	G-1,2,3	1.264	38.21	0.250

\* Average Values of several Specimens

TABLE IV (A. B. C.)

Correlation Relation	Sample Correlation Coefficient		Factorial Standard Error of Estimate	Constant Exponent	
	On Log Scale	On Linear Scale		C	n
<b>A. Birdsboro materials only</b>					
1/MDPR = C (UR) <sup>n</sup>	0.439	0.378	1.33	1.087	0.146
1/MDPR = C (URxE) <sup>2,n</sup>	0.439	0.378	1.33	0.73x10 <sup>-2</sup>	0.145
1/MDPR = C (URxBHN) <sup>n</sup>	0.511	0.446	1.31	0.530	0.142
1/MDPR = C (BHN) <sup>n</sup>	0.672	0.718	1.26	0.238x10 <sup>-1</sup>	0.876
1/MDPR = C (SE) <sup>n</sup>	0.224	0.203	1.36	0.744	0.113
<b>B. For all materials (U of M, Tool Steels and Birdsboro)</b>					
1/MDPR = C (UR) <sup>n</sup>	0.636	0.006	3.05	0.478x10 <sup>-1</sup>	0.795
1/MDPR = C (URxE) <sup>2,n</sup>	0.677	0.041	2.90	0.453x10 <sup>-9</sup>	0.576
1/MDPR = C (URxBHN) <sup>n</sup>	0.701	0.063	2.76	0.52x10 <sup>-2</sup>	0.576
1/MDPR = C (BHN) <sup>n</sup>	0.748	0.364	2.61	0.38x10 <sup>-3</sup>	0.602
1/MDPR = C (SE) <sup>n</sup>	0.072	0.174	4.20	0.964	4.08
<b>C. For all other materials (excluding Birdsboro)</b>					
1/MDPR = C (UR) <sup>n</sup>	0.743	0.077	3.75	0.11x10 <sup>-1</sup>	1.11
1/MDPR = C (URxE) <sup>2,n</sup>	0.771	0.139	3.51	0.25x10 <sup>-11</sup>	0.72
1/MDPR = C (URxBHN) <sup>n</sup>	0.780	0.127	3.43	0.16x10 <sup>-2</sup>	0.74
1/MDPR = C (BHN) <sup>n</sup>	0.761	0.338	3.60	0.32x10 <sup>-3</sup>	1.76
1/MDPR = C (SE) <sup>n</sup>	0.188	0.100	6.95	0.114	0.35

UR = Ultimate Resilience  
E = Elasticity  
BHN = Brinell Hardness  
SE = Strain Energy



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Figure 1. Schematic of Baffled Test Configuration

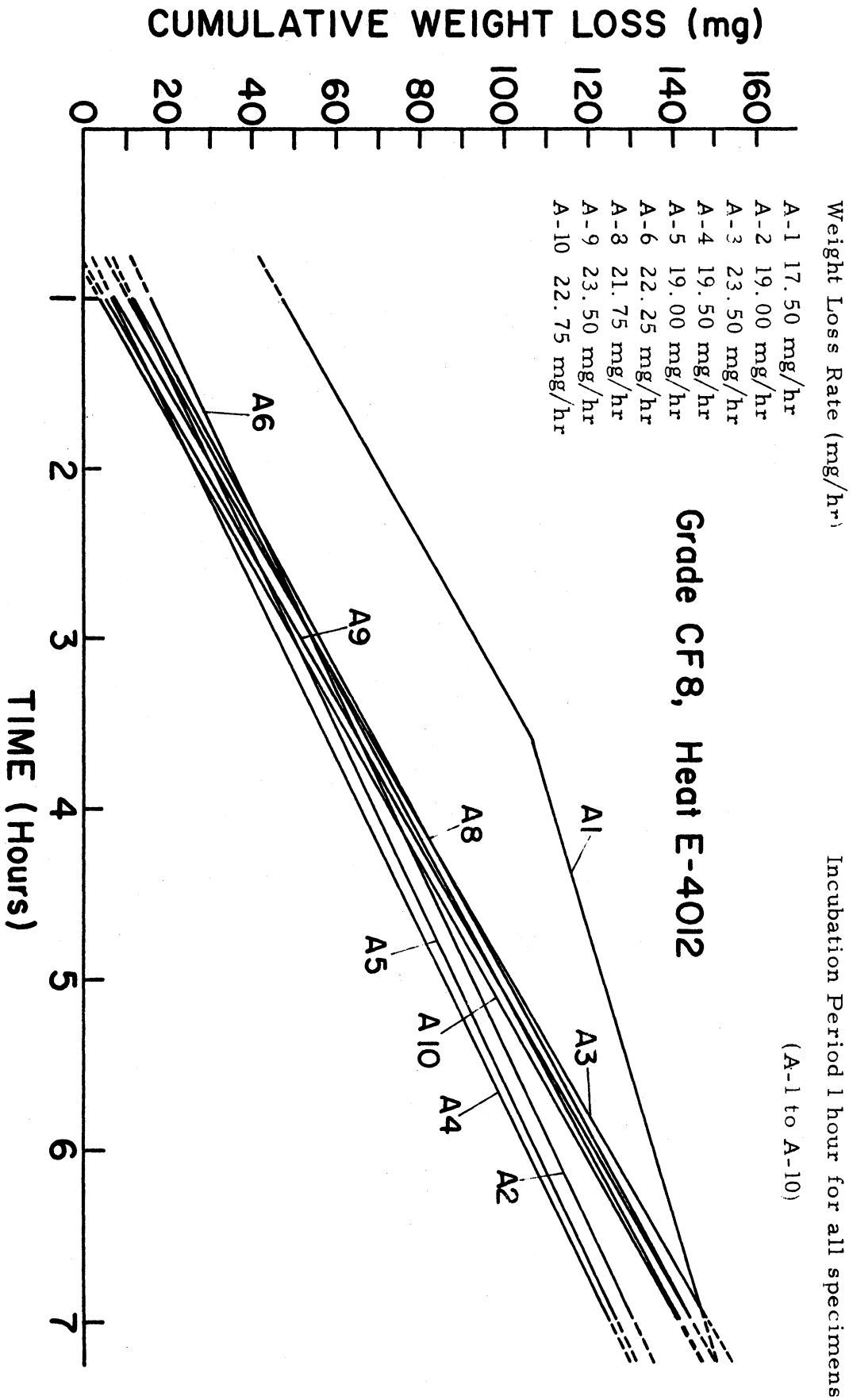
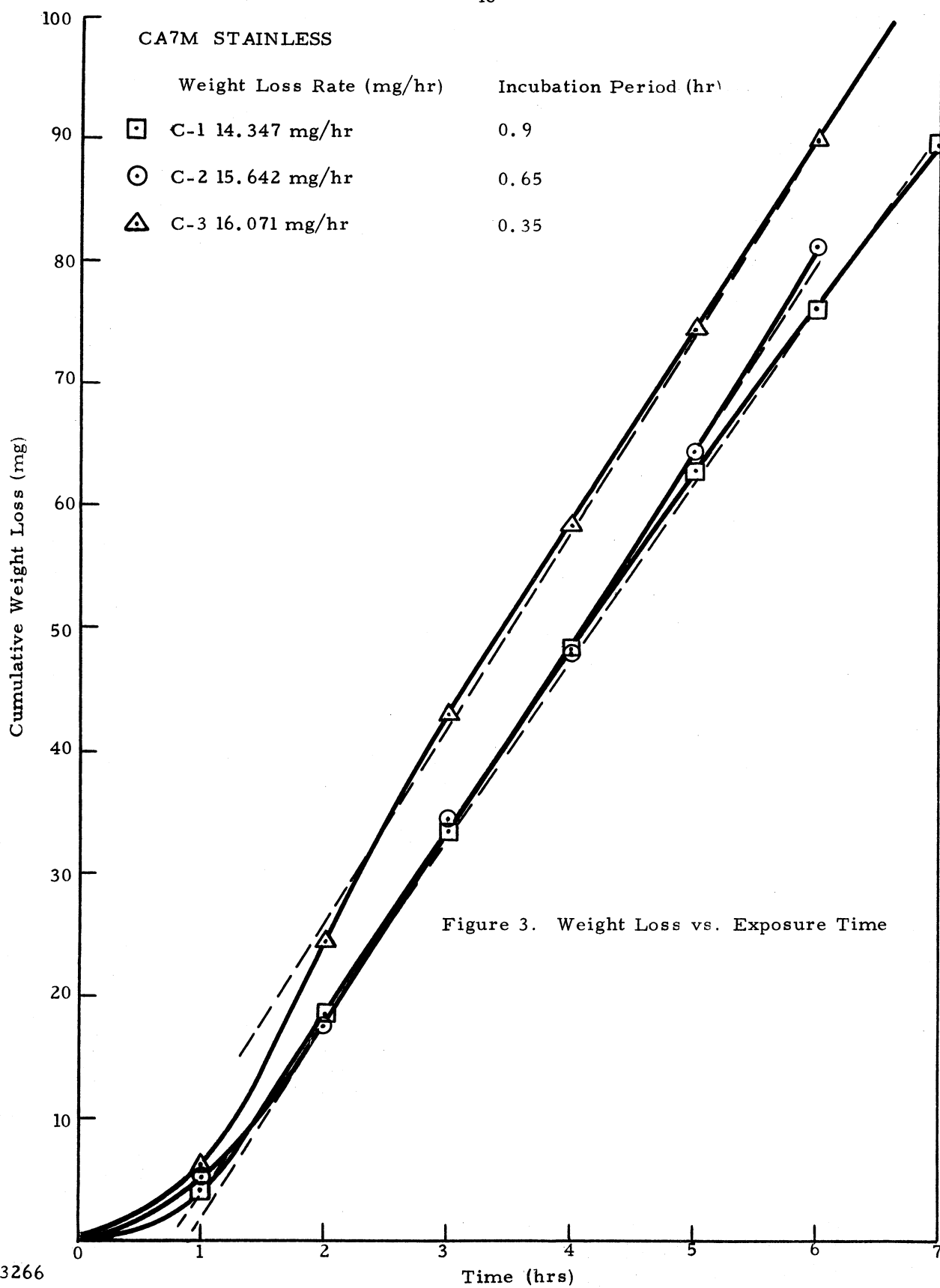


Figure 2. Weight Loss vs. Exposure Time



CA15

Weight Loss Rate (mg/hr)      Incubation Period (hr)

- CA-15 #1 19.90 mg/hr      0.70
- CA-15 #2 20.80 mg/hr      0.65

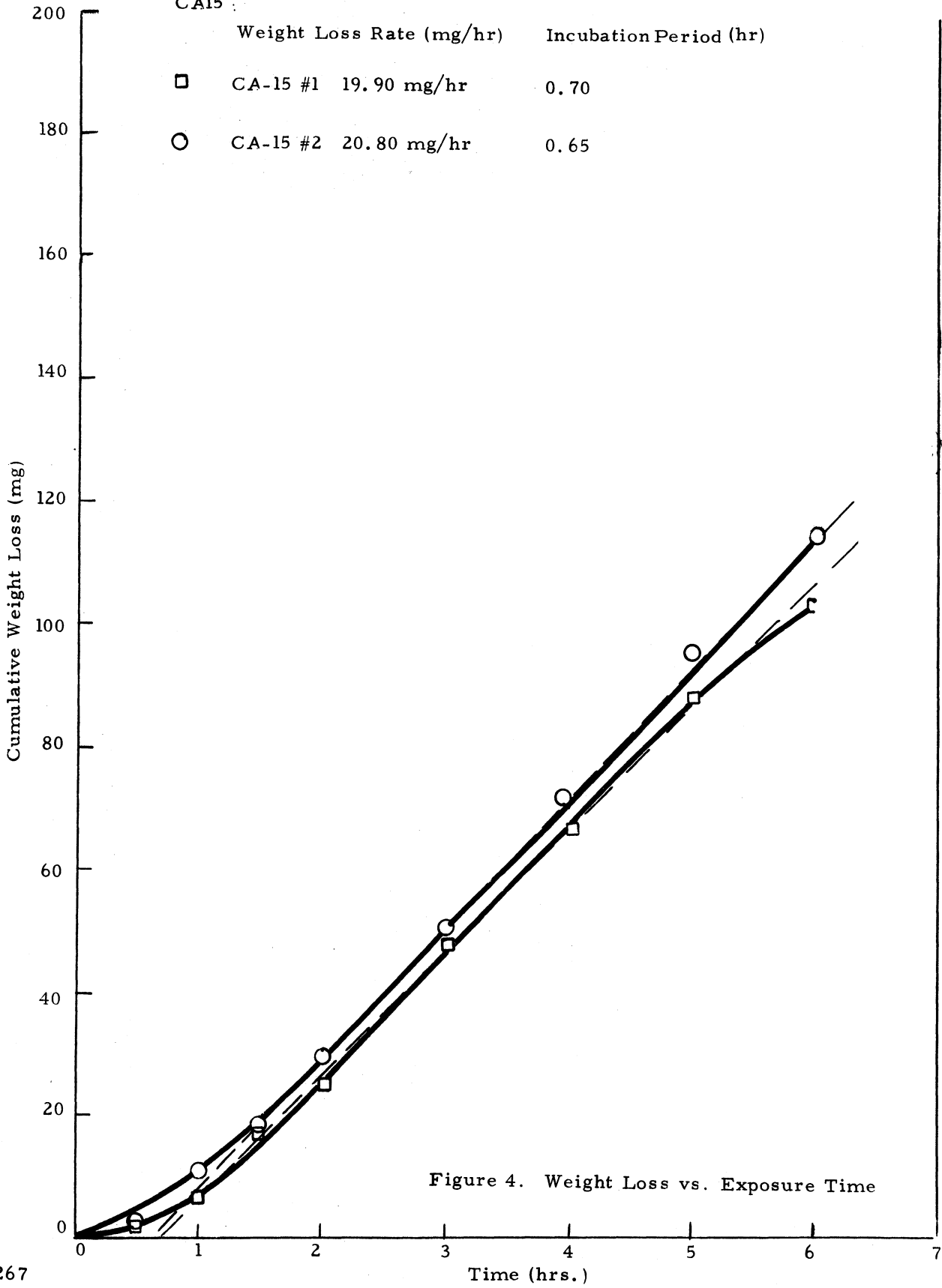
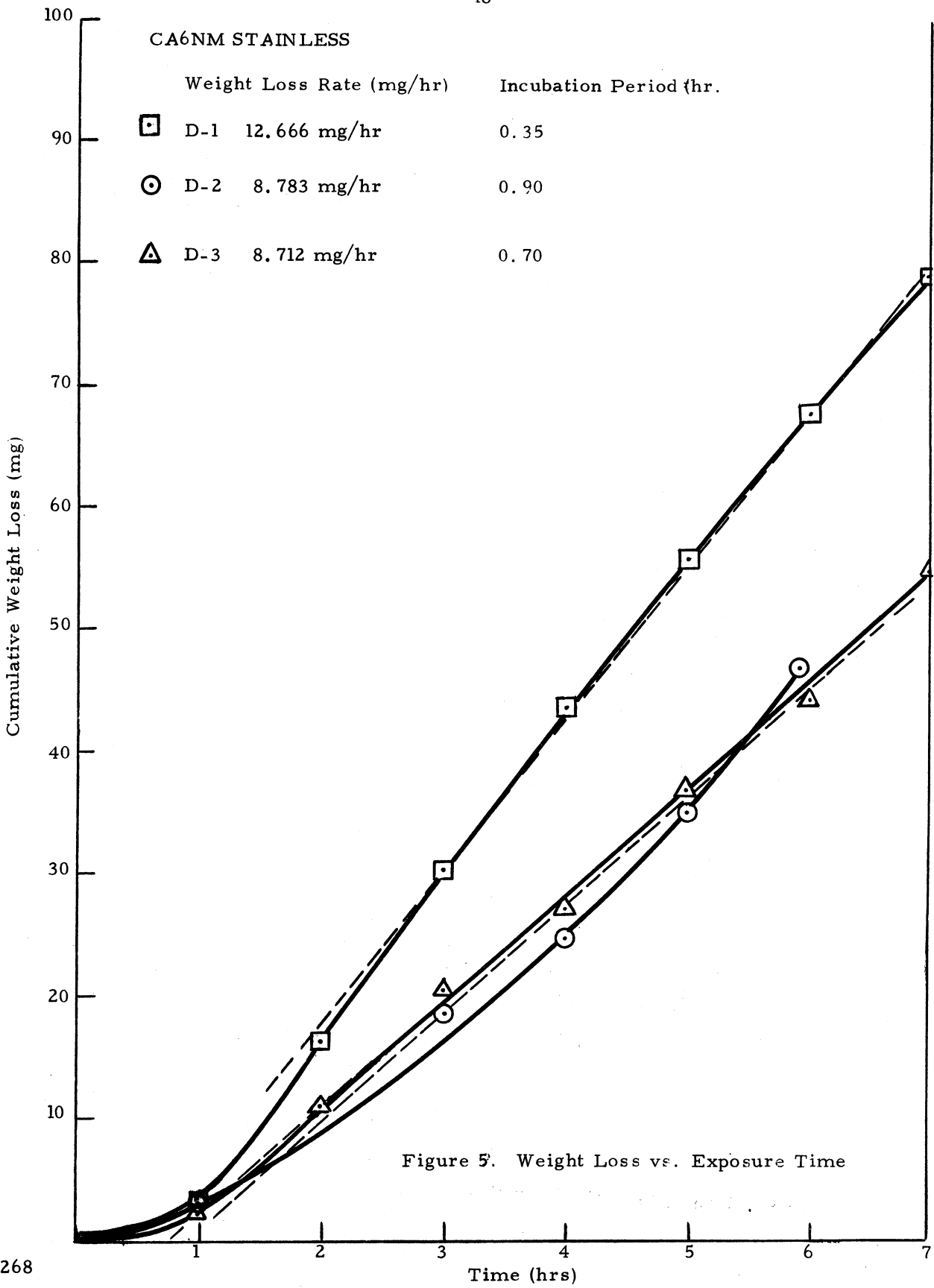


Figure 4. Weight Loss vs. Exposure Time





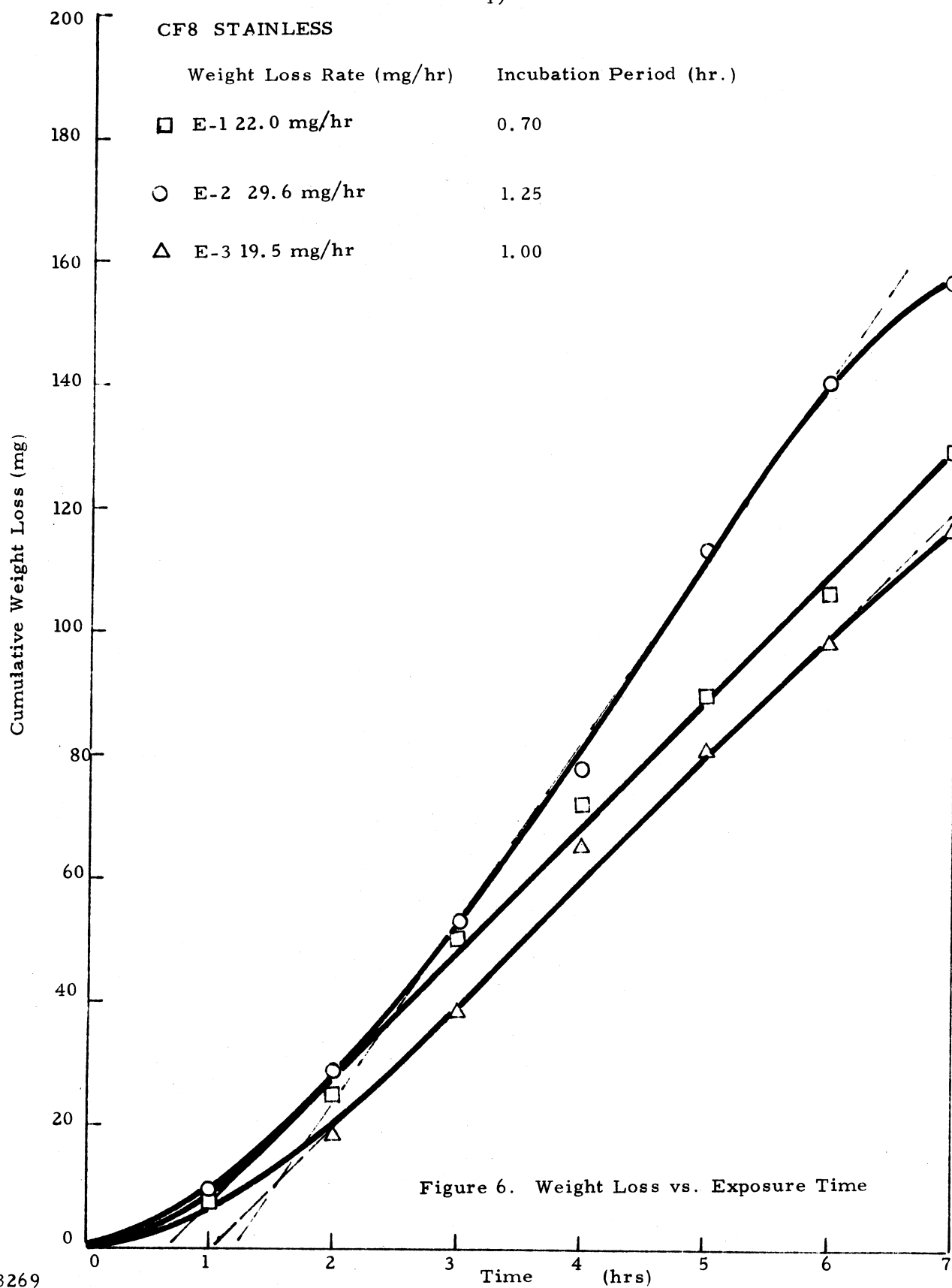
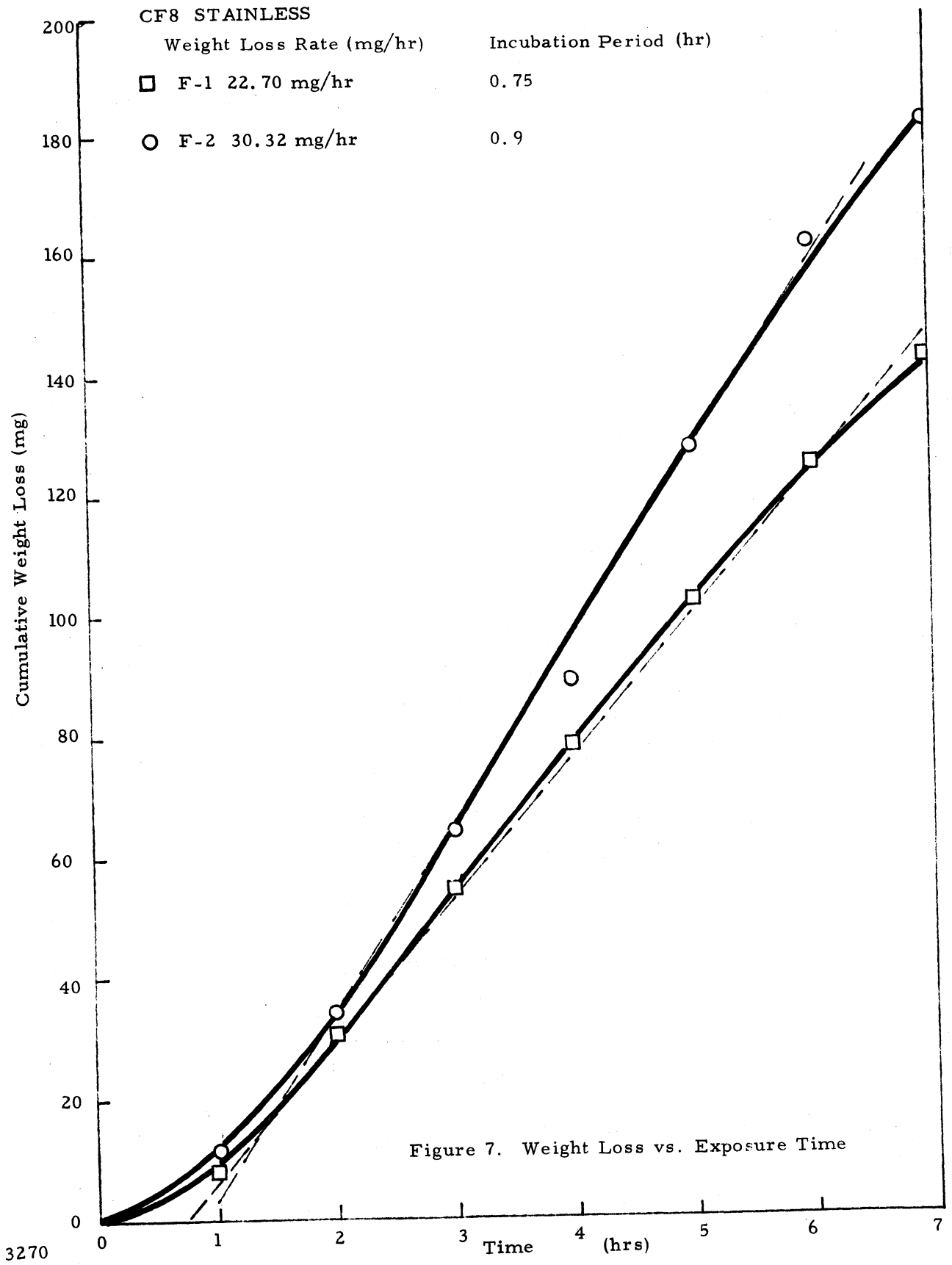


Figure 6. Weight Loss vs. Exposure Time



3270

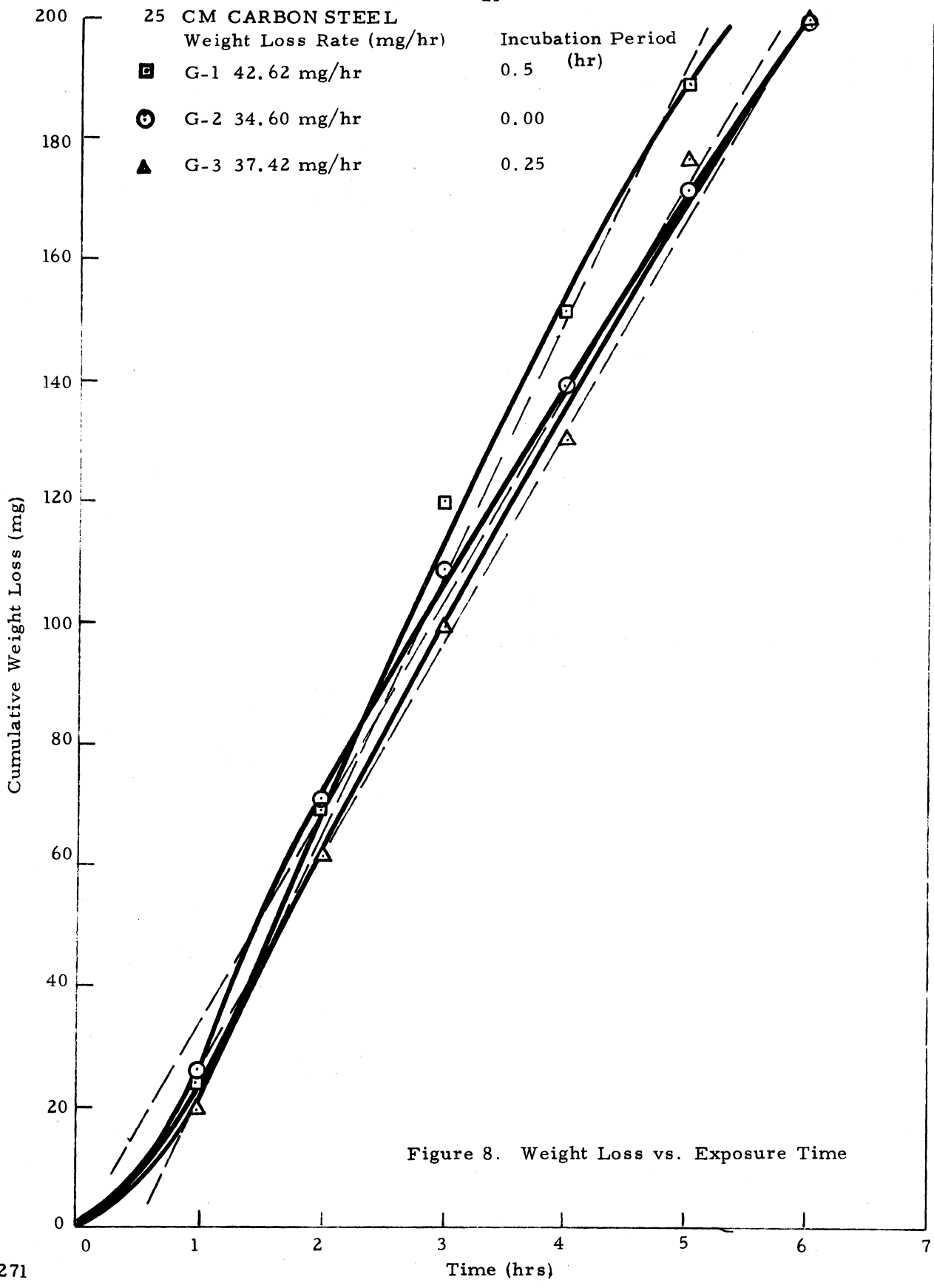


Figure 8. Weight Loss vs. Exposure Time

45 A 7 CARBON

	Weight Loss Rate (mg/hr)	Incubation Period (hr)
□ H-1	10.40 mg/hr	1.00
○ H-2	15.02 mg/hr	1.35
△ H-3	11.00 mg/hr	0.80

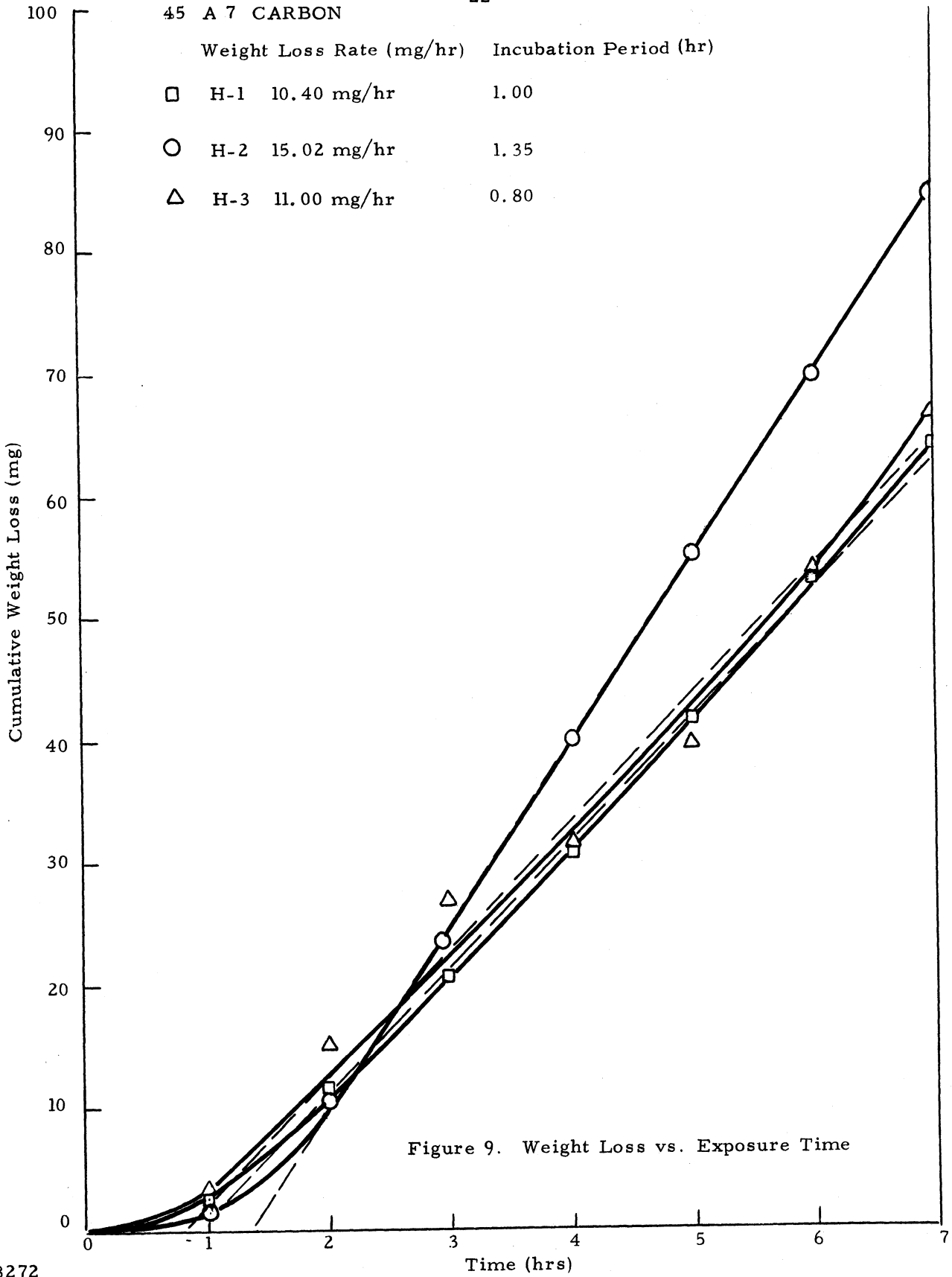
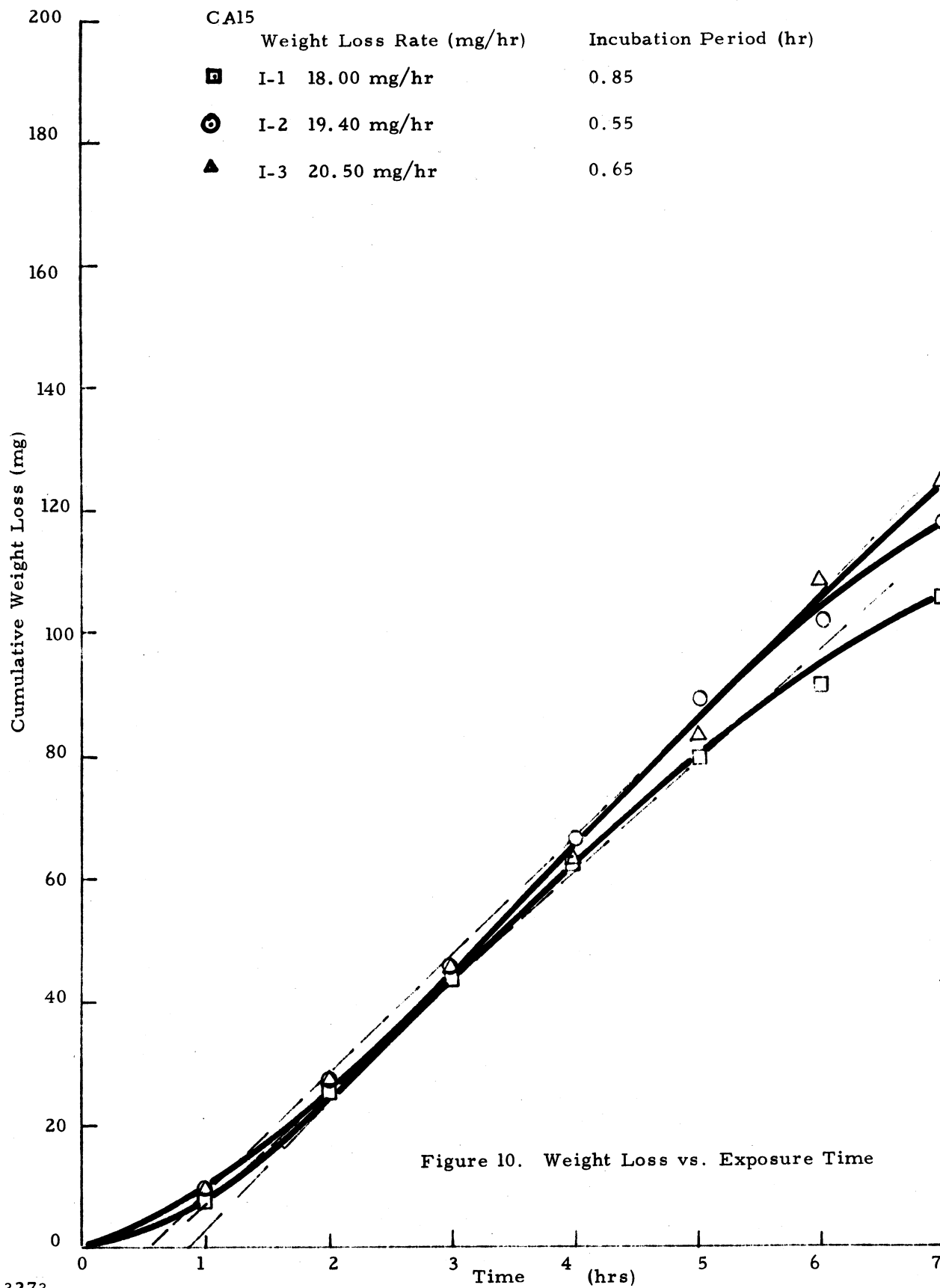
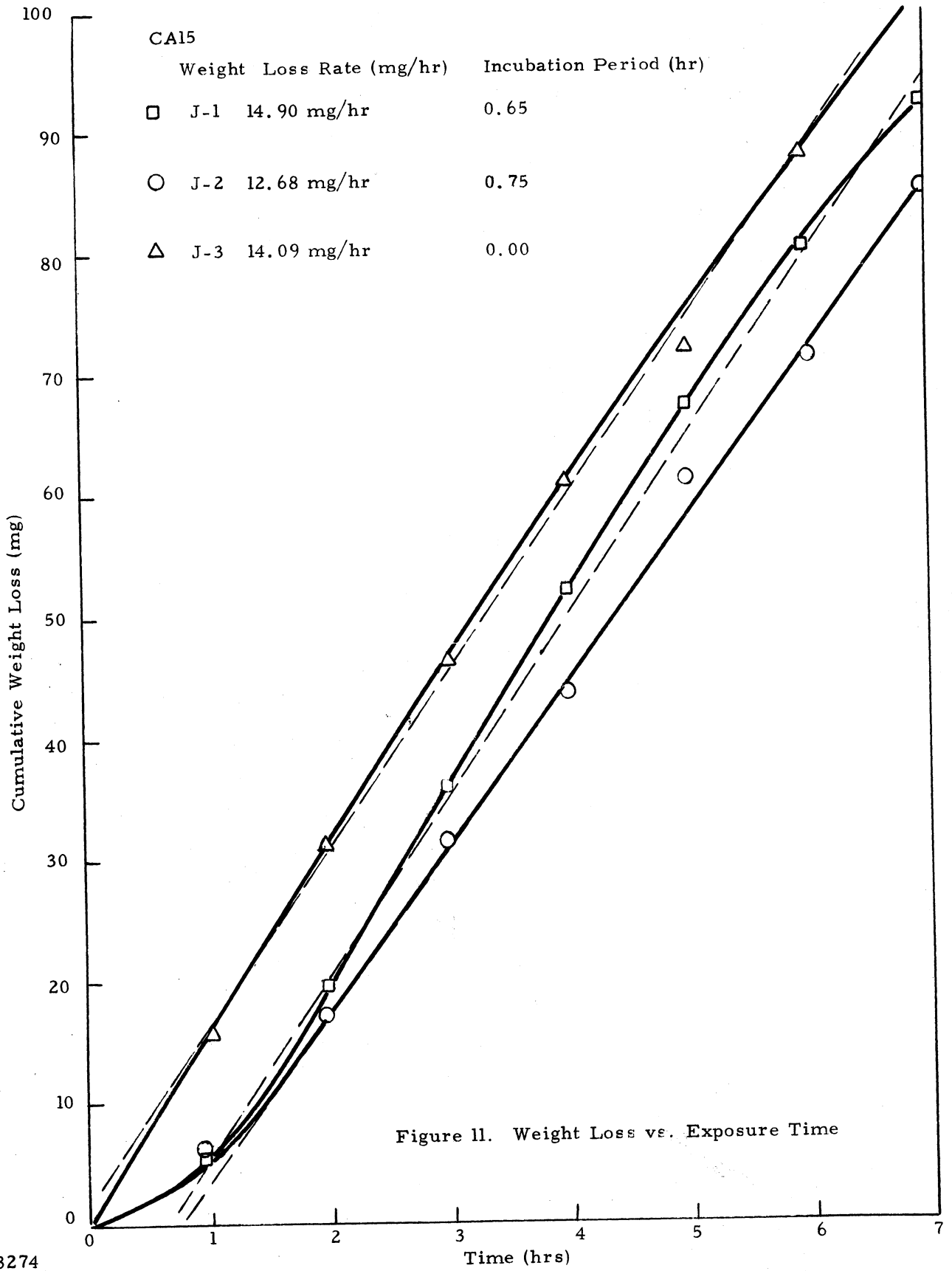
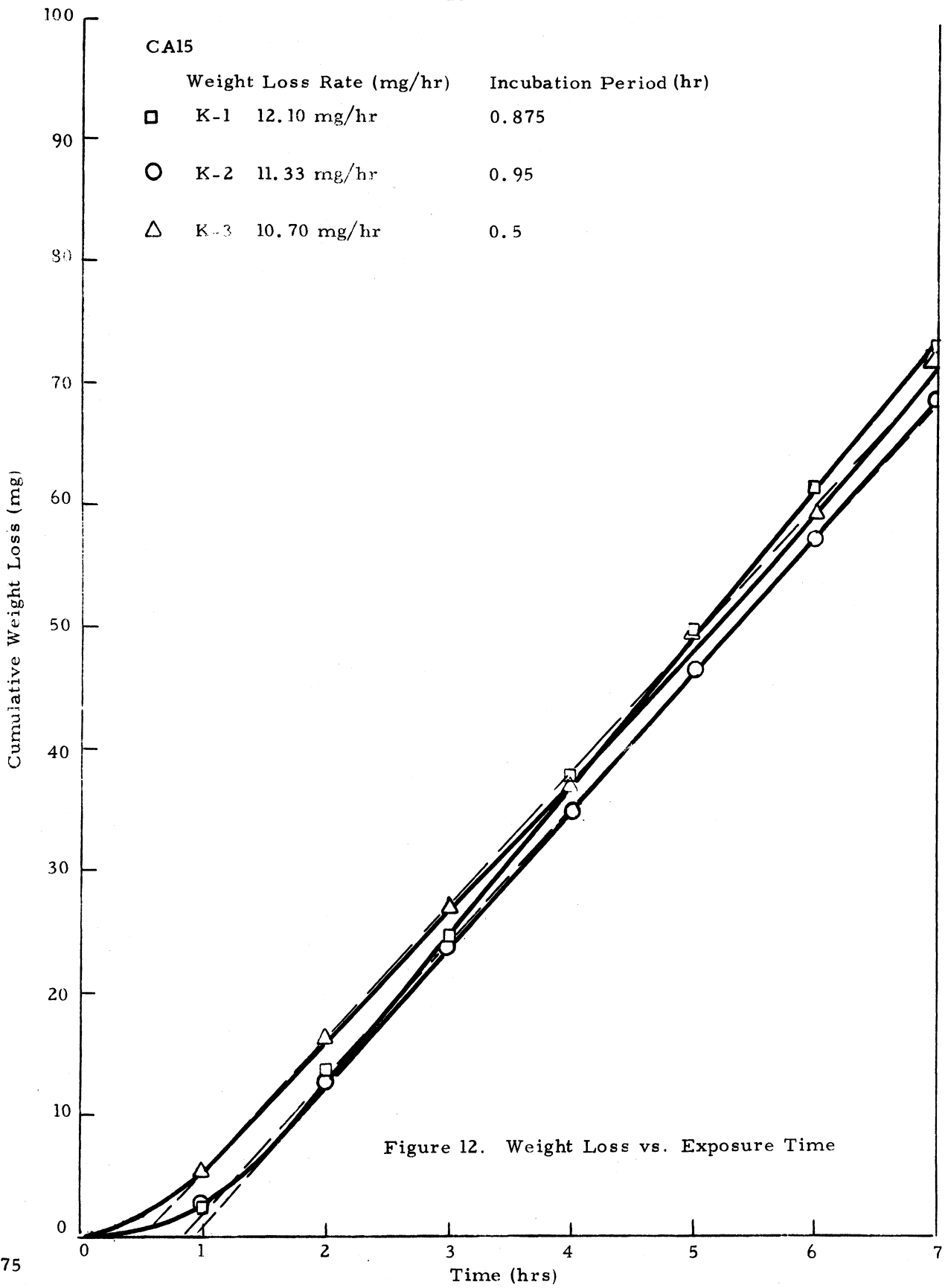
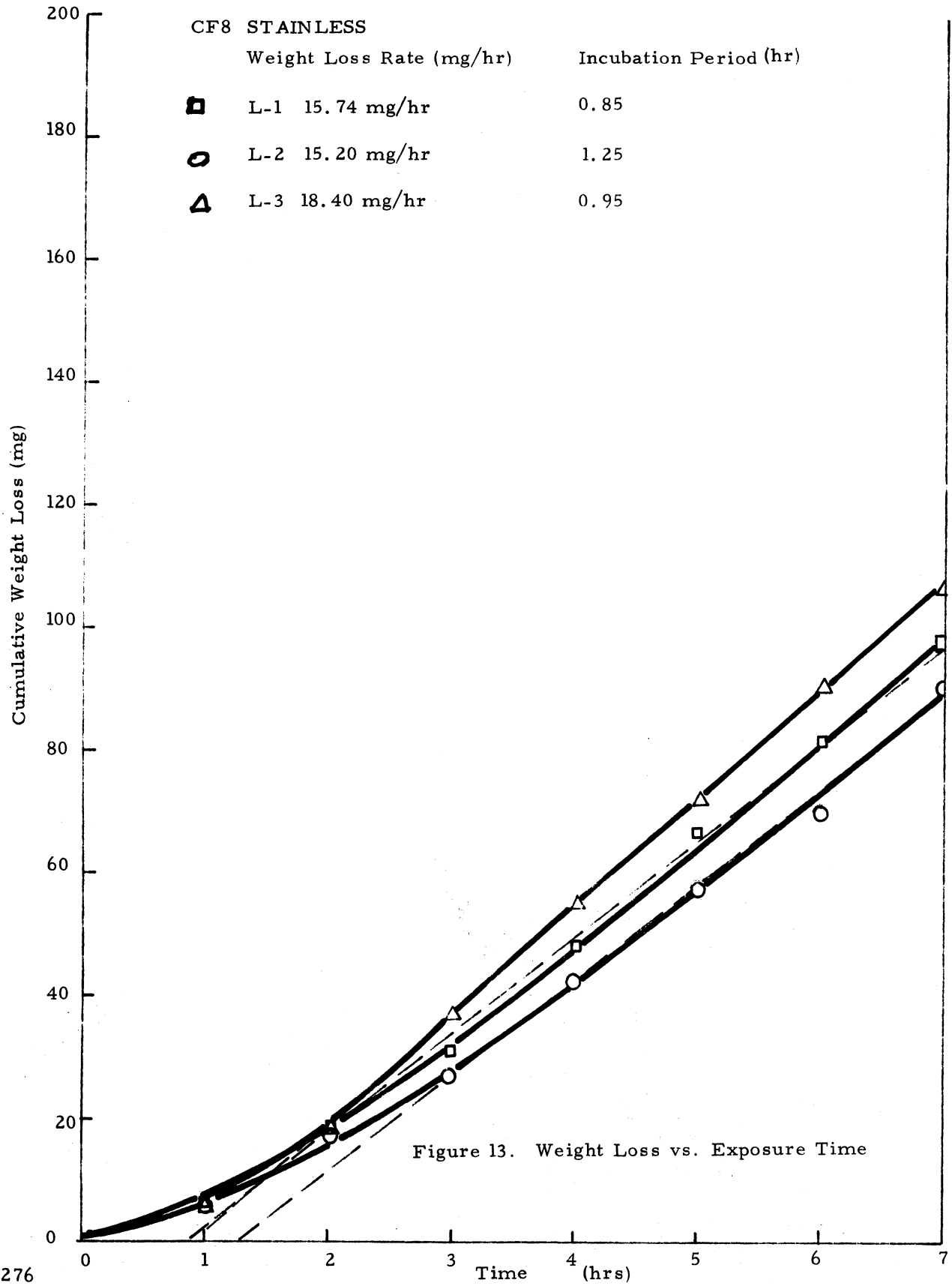


Figure 9. Weight Loss vs. Exposure Time

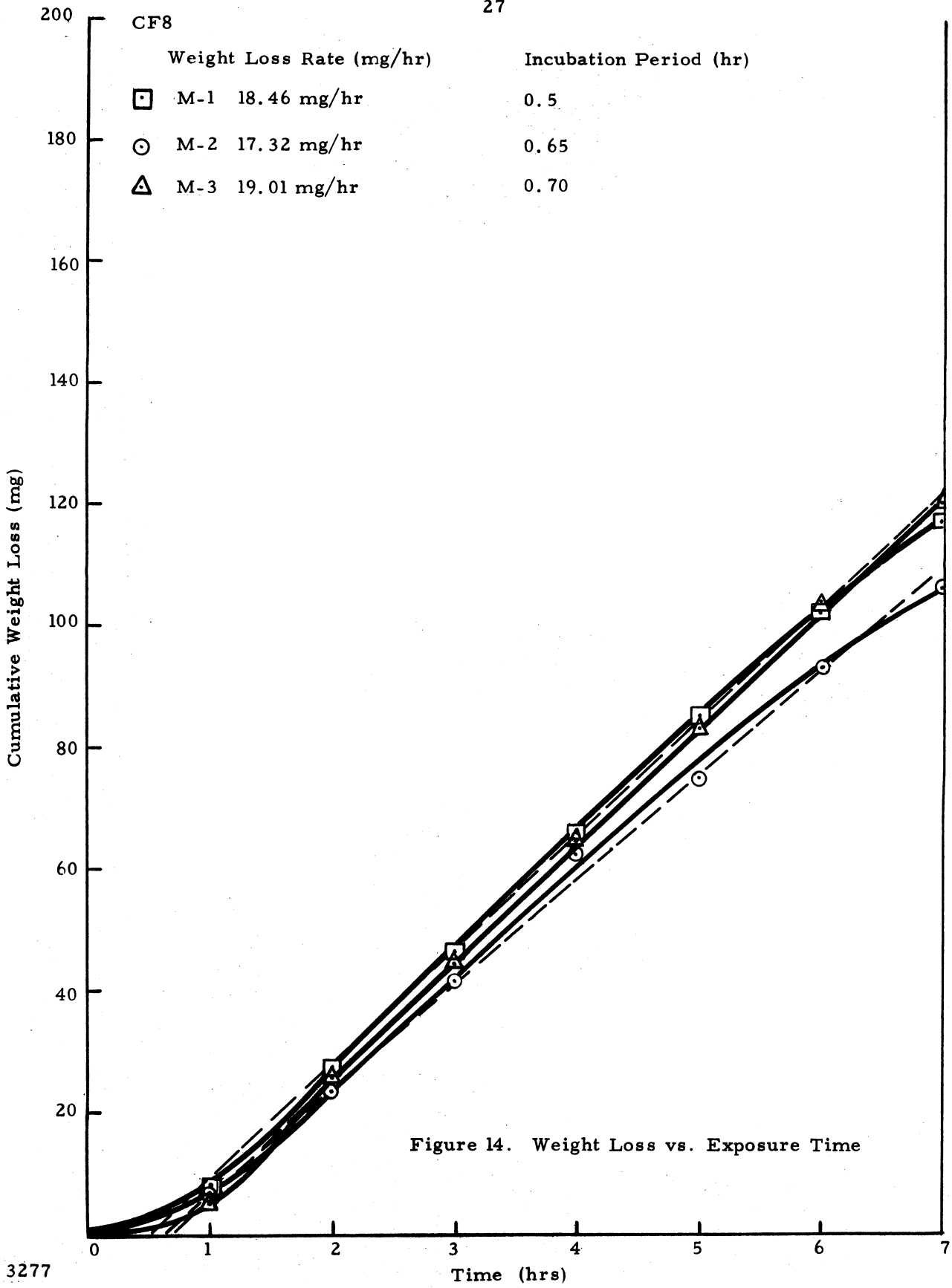












ARCOS STAINLEND

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Weight Loss Rate (mg/hr)

Incubation Period (hr)

- |   |     |             |      |
|---|-----|-------------|------|
| □ | N-1 | 14.72 mg/hr | 0.30 |
| ○ | N-2 | 16.36 mg/hr | 0.5  |
| △ | N-3 | 16.30 mg/hr | 0.00 |

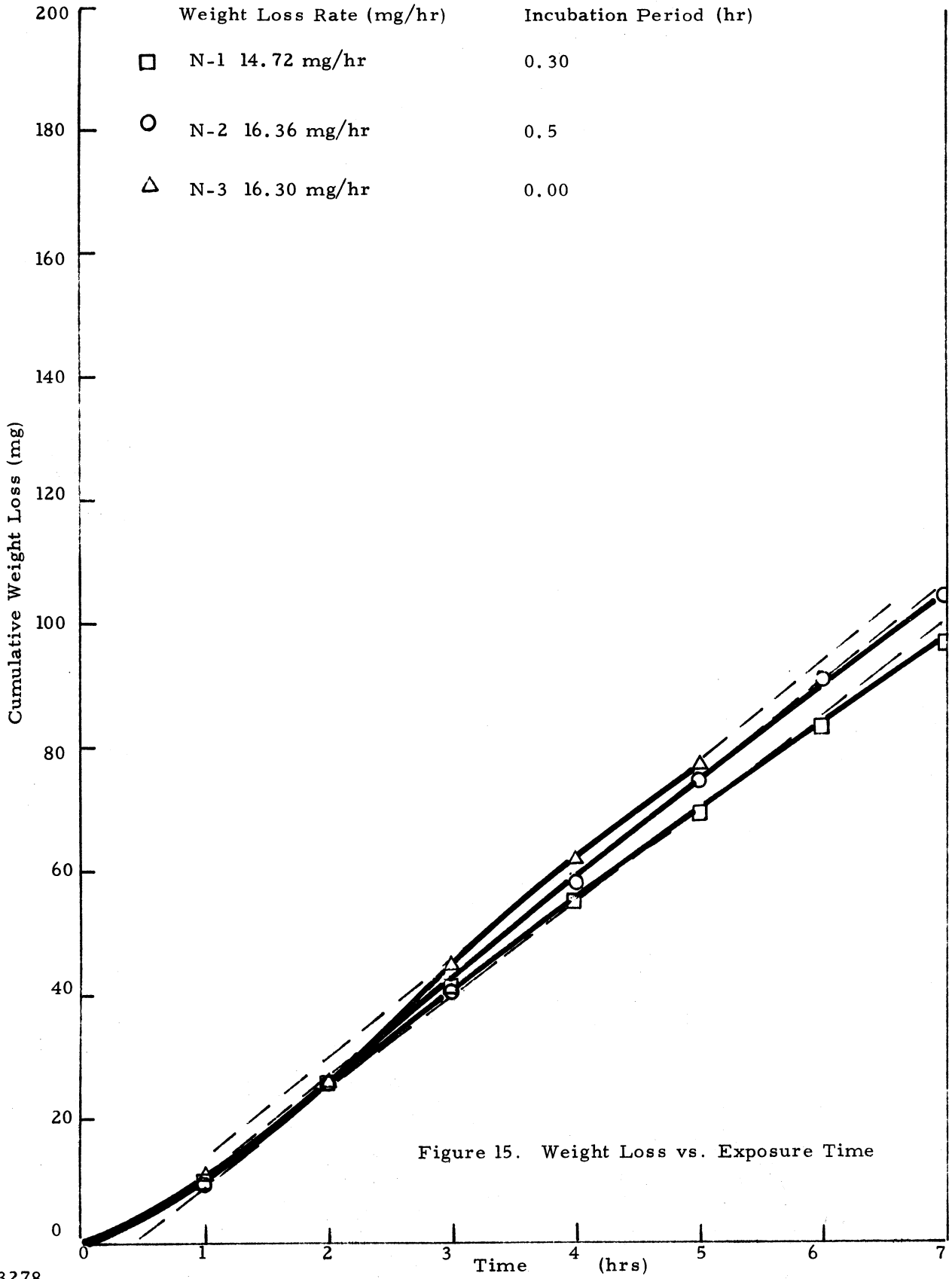
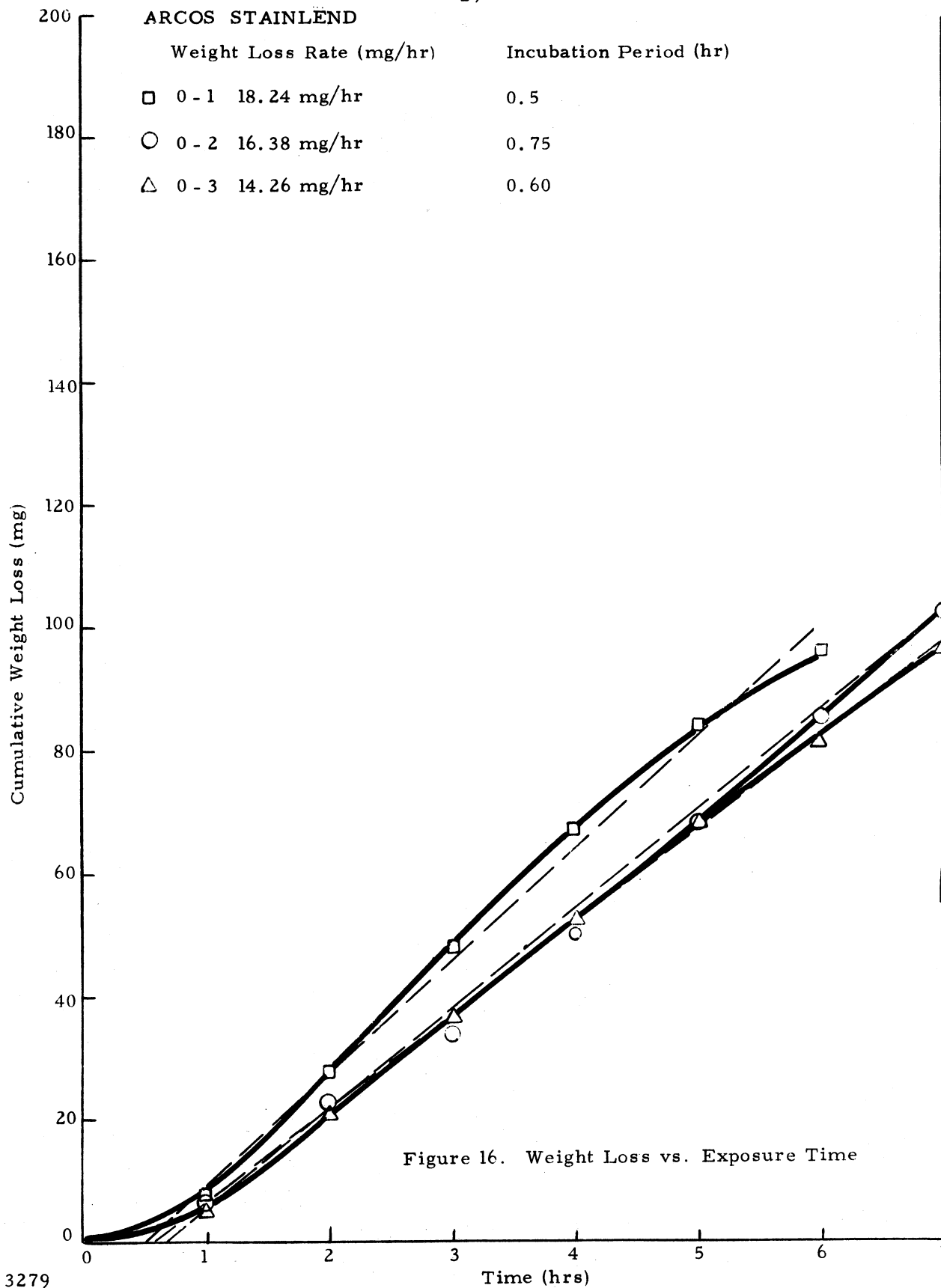
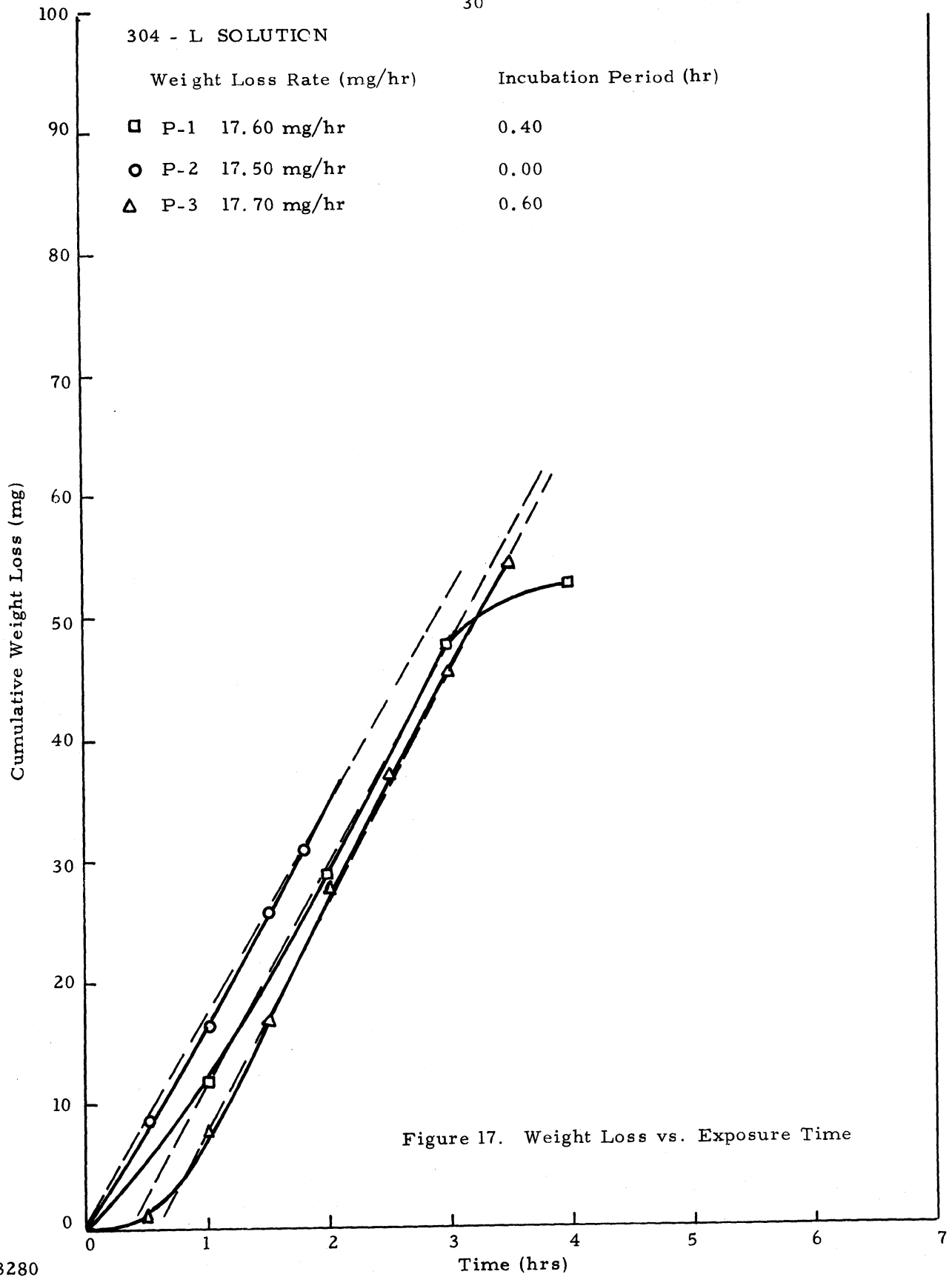
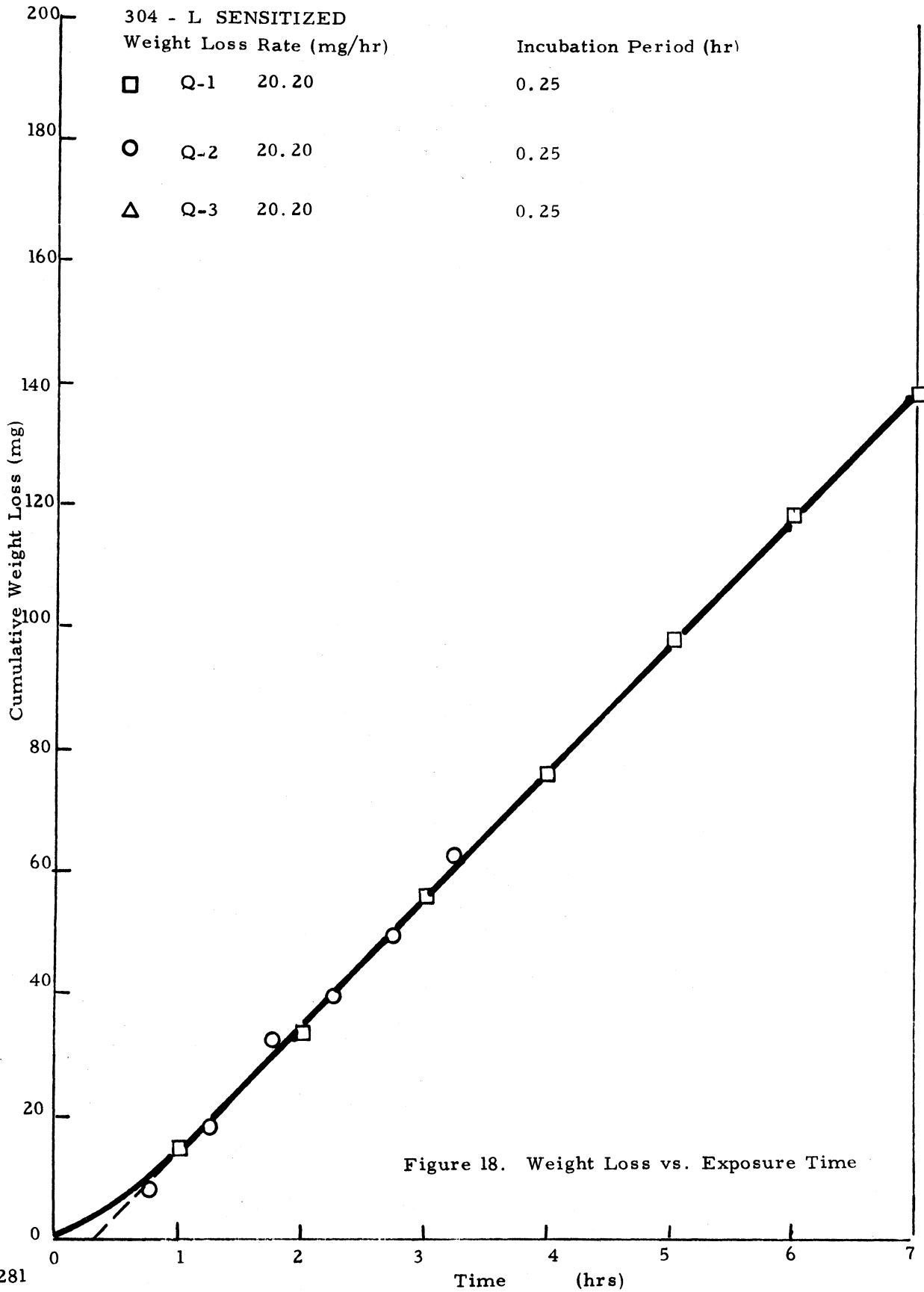
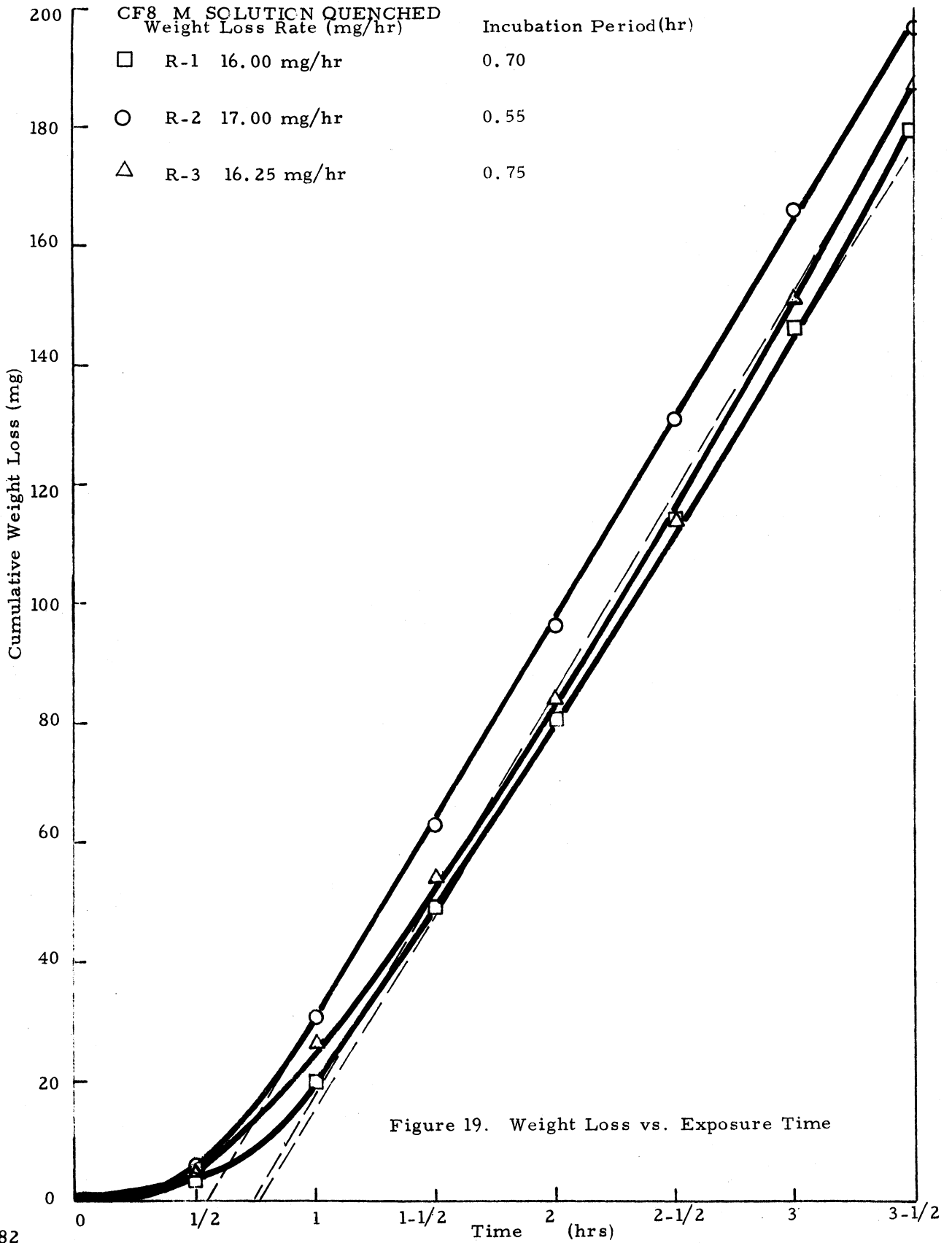


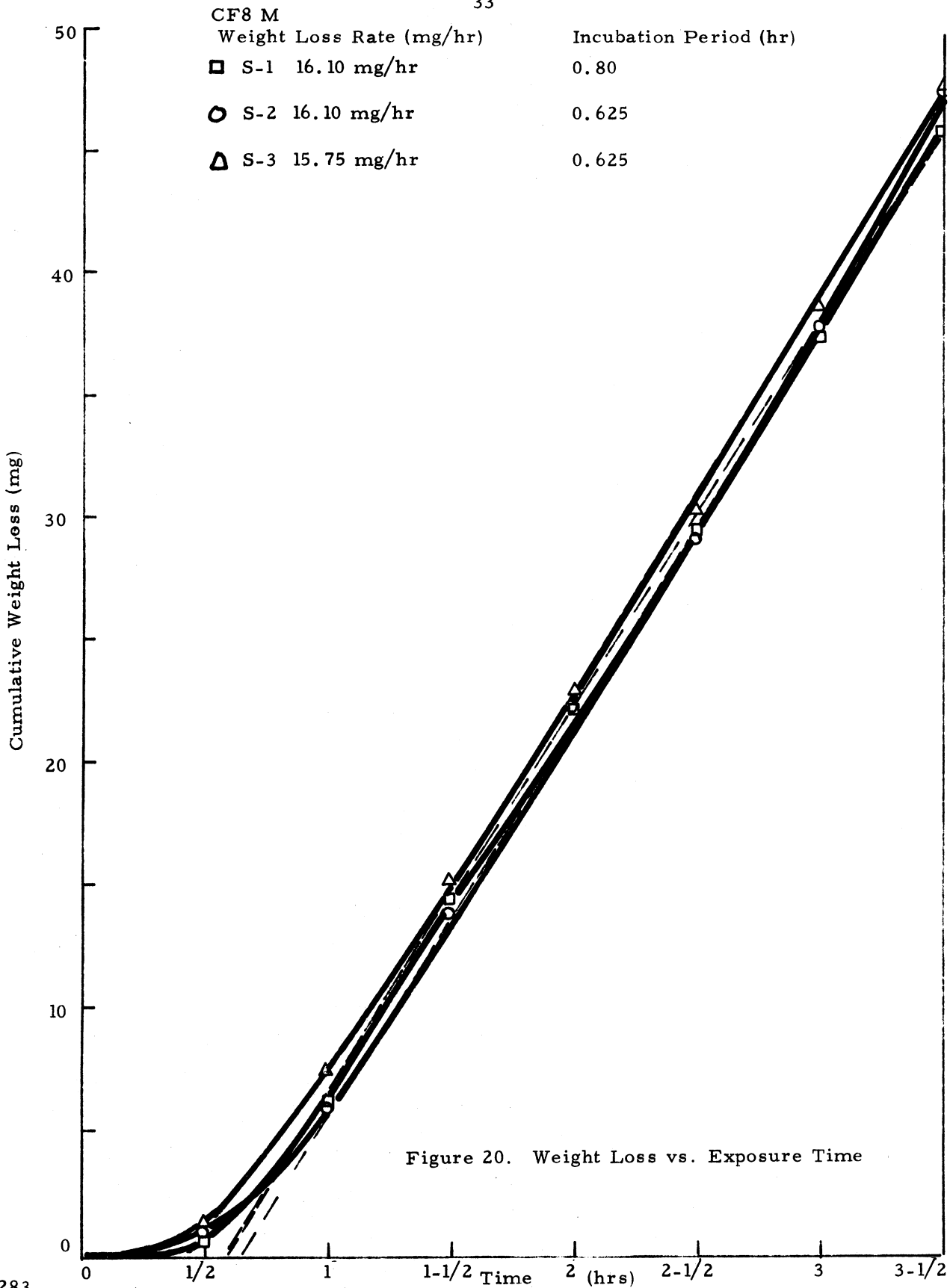
Figure 15. Weight Loss vs. Exposure Time











CE 30 WATER QUENCHED

	Weight Loss Rate (mg/hr)	Incubation Period (hr)
□ T-1	14.80 mg/hr	0.75
○ T-2	14.80 mg/hr	0.75
△ T-3	13.65 mg/hr	0.75

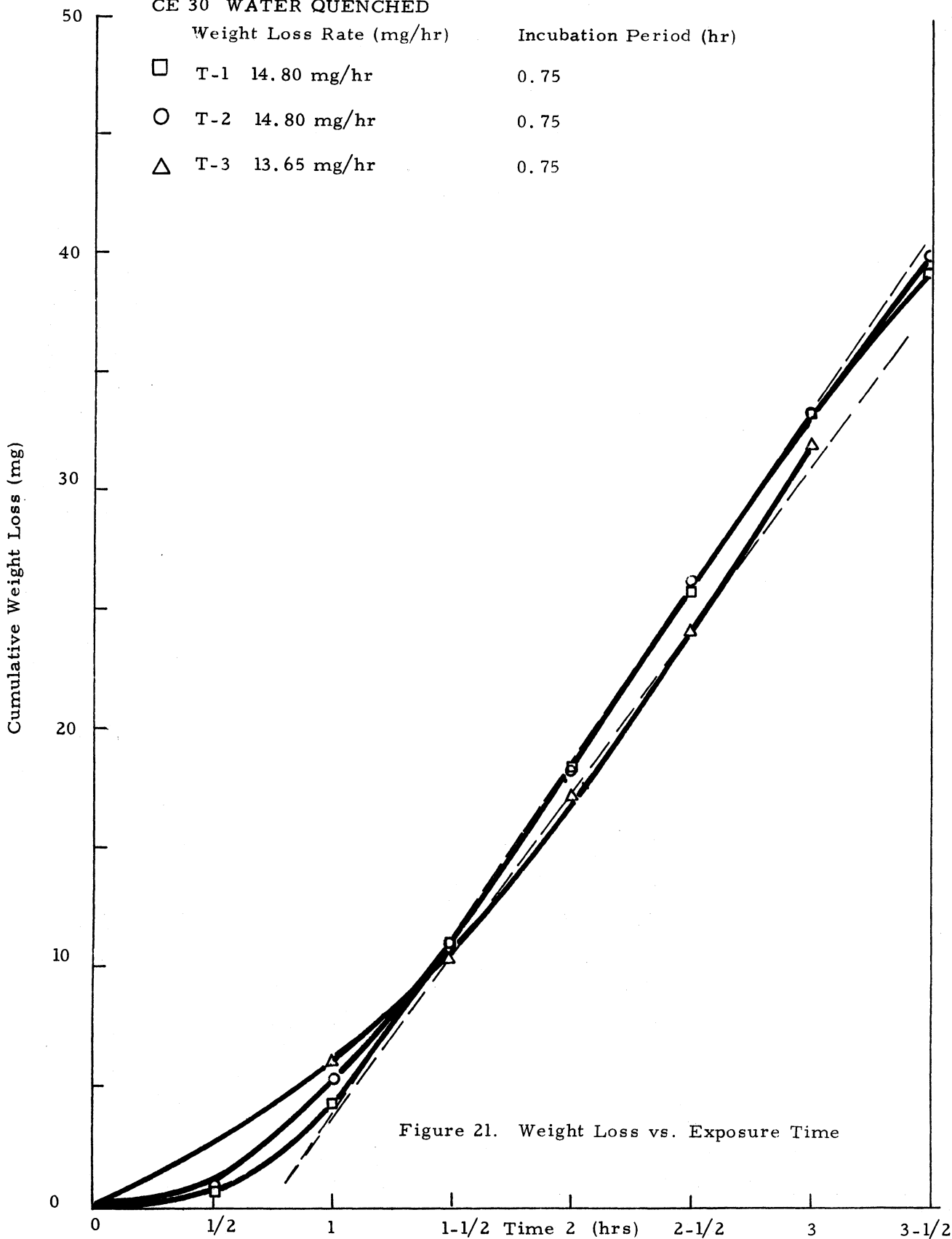


Figure 21. Weight Loss vs. Exposure Time



CE 30 AS CAST

35

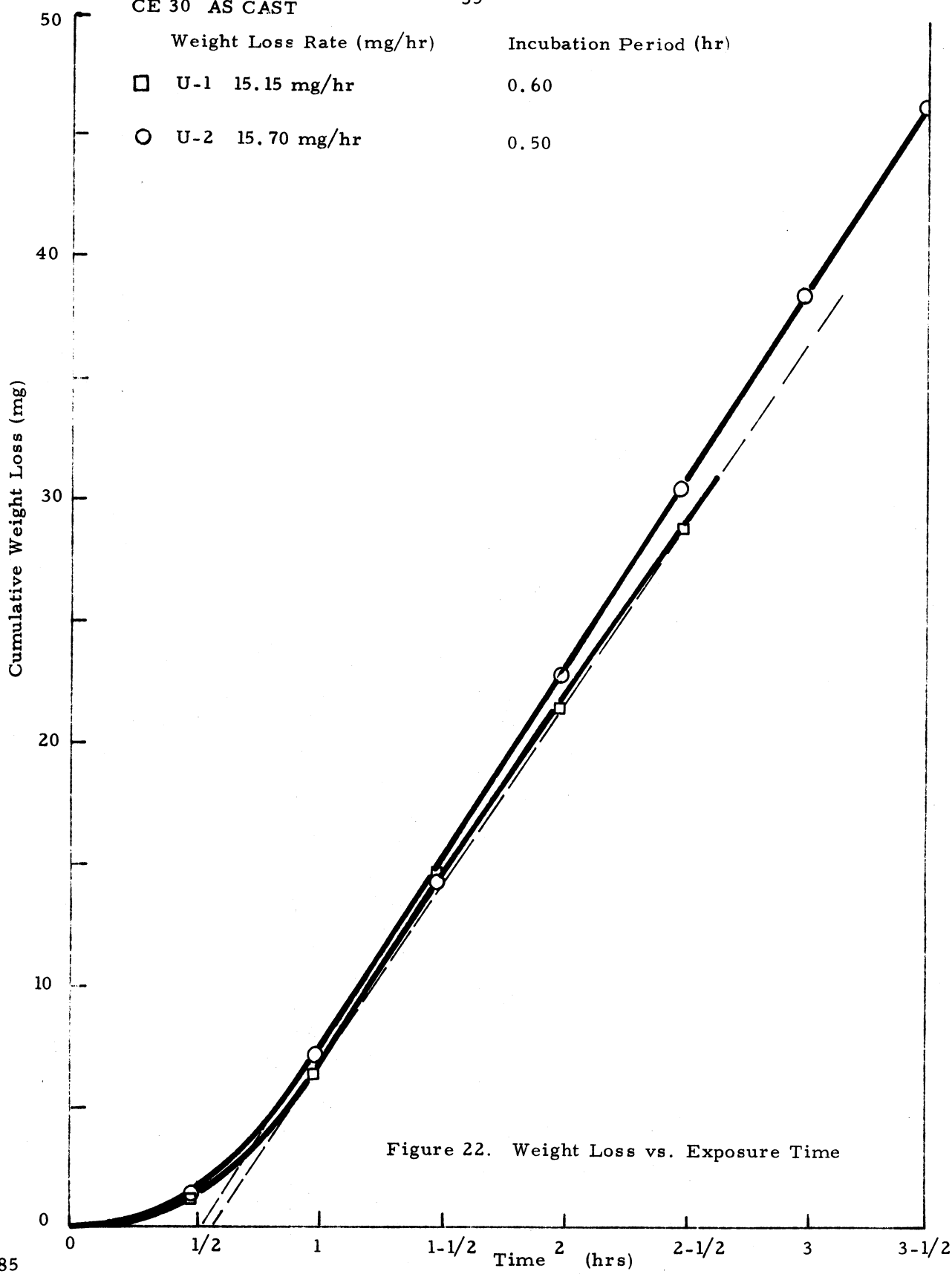


Figure 22. Weight Loss vs. Exposure Time

308 - L WATER QUENCHED

Weight Loss Rate (mg/hr)

Incubation Period (hr)

□	V-2	17.00 mg/hr	0.51
○	V-1	20.00 mg/hr	0.00
△	V-3	20.00 mg/hr	0.60

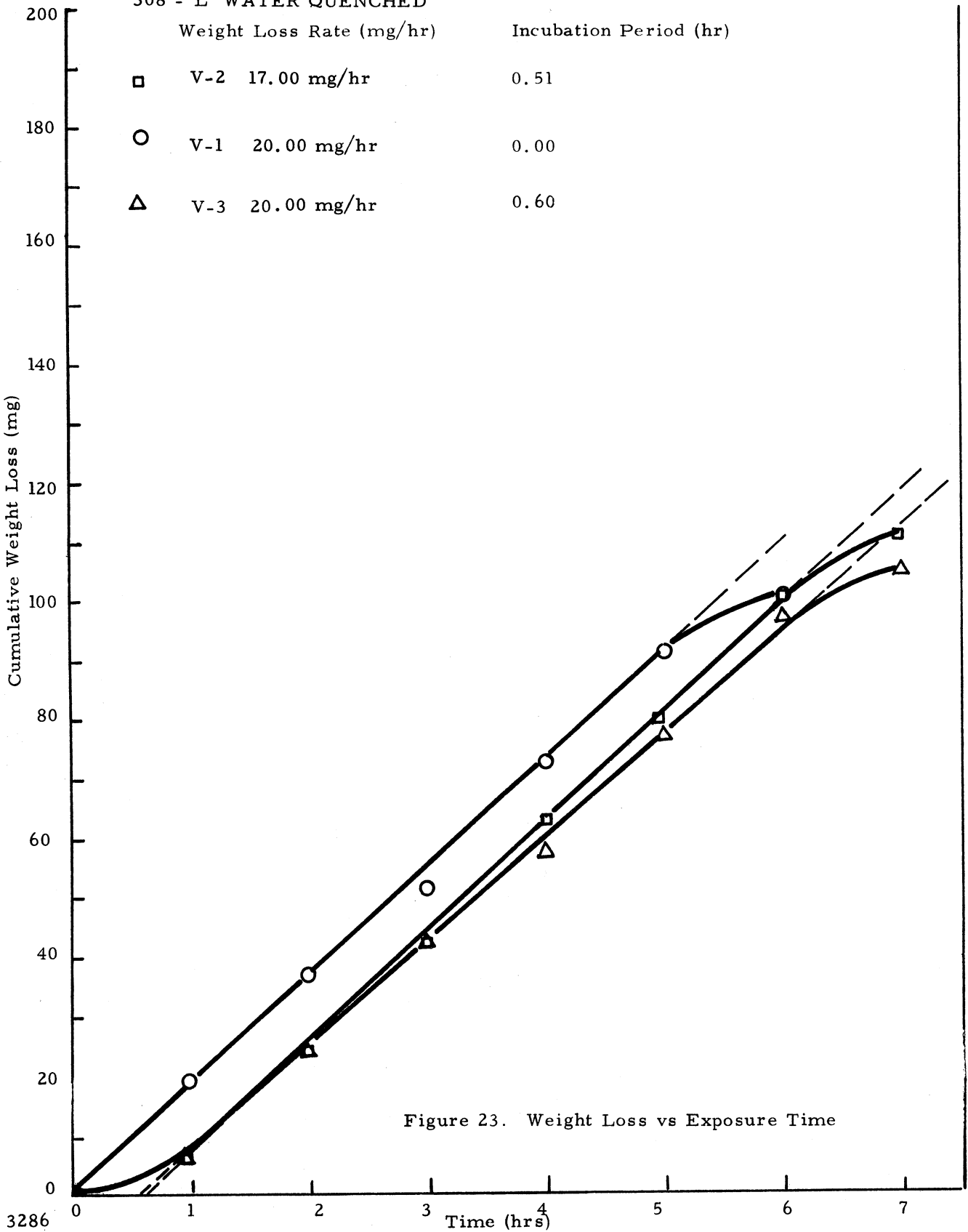


Figure 23. Weight Loss vs Exposure Time

308 - L AS WELDED

	Weight Loss Rate (mg/hr)	Incubation Period (hr)
□	W-1 16.5 mg/hr	0.49
○	W-2 16.5 mg/hr	1.00
△	W-3 16.5 mg/hr	0.75

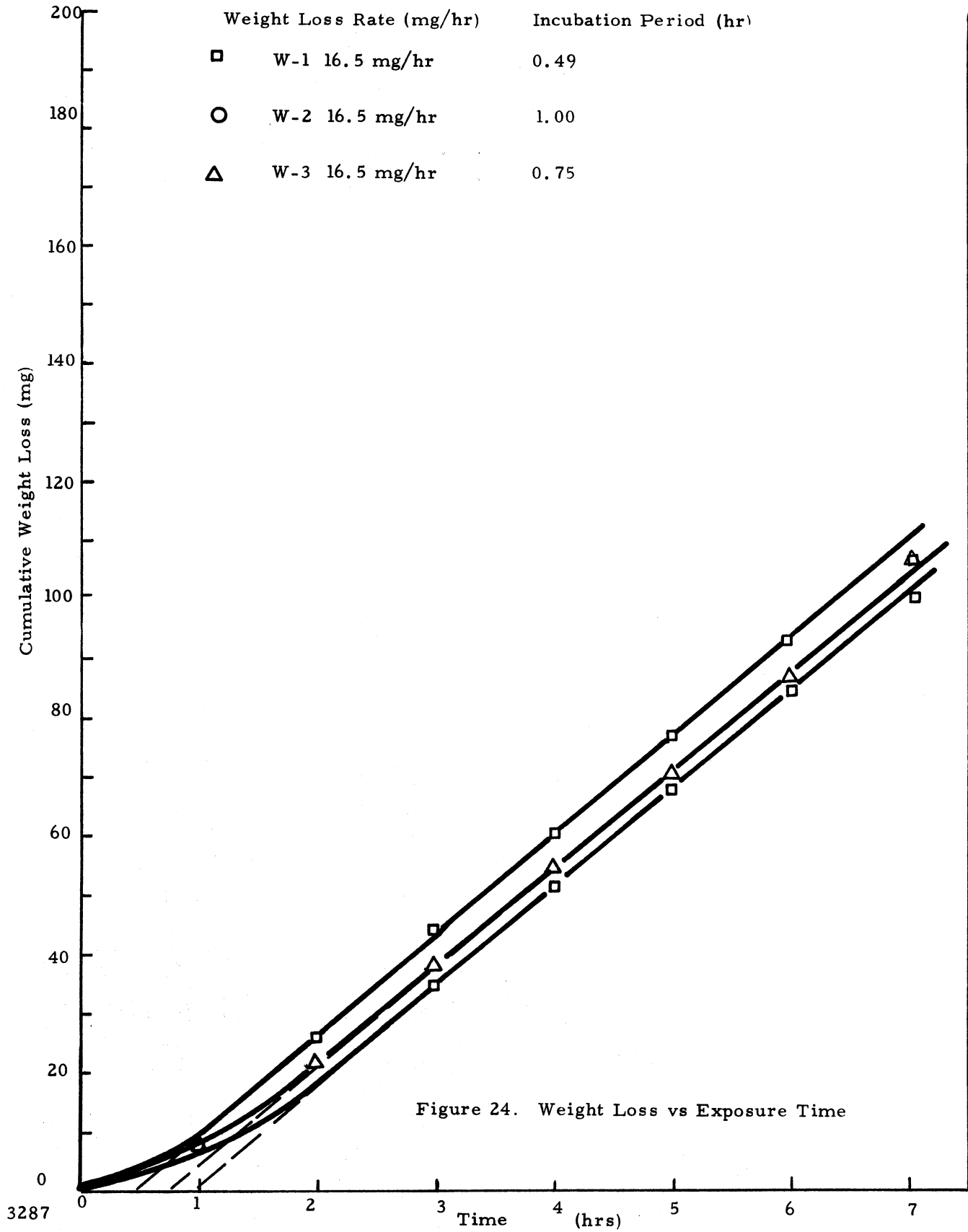


Figure 24. Weight Loss vs Exposure Time

## 308 WIRE AS WELDED

Weight Loss Rate (mg/hr)

Incubation Period (hr)

■ X-1 17.50

0.75

○ X-2 19.00

1.51

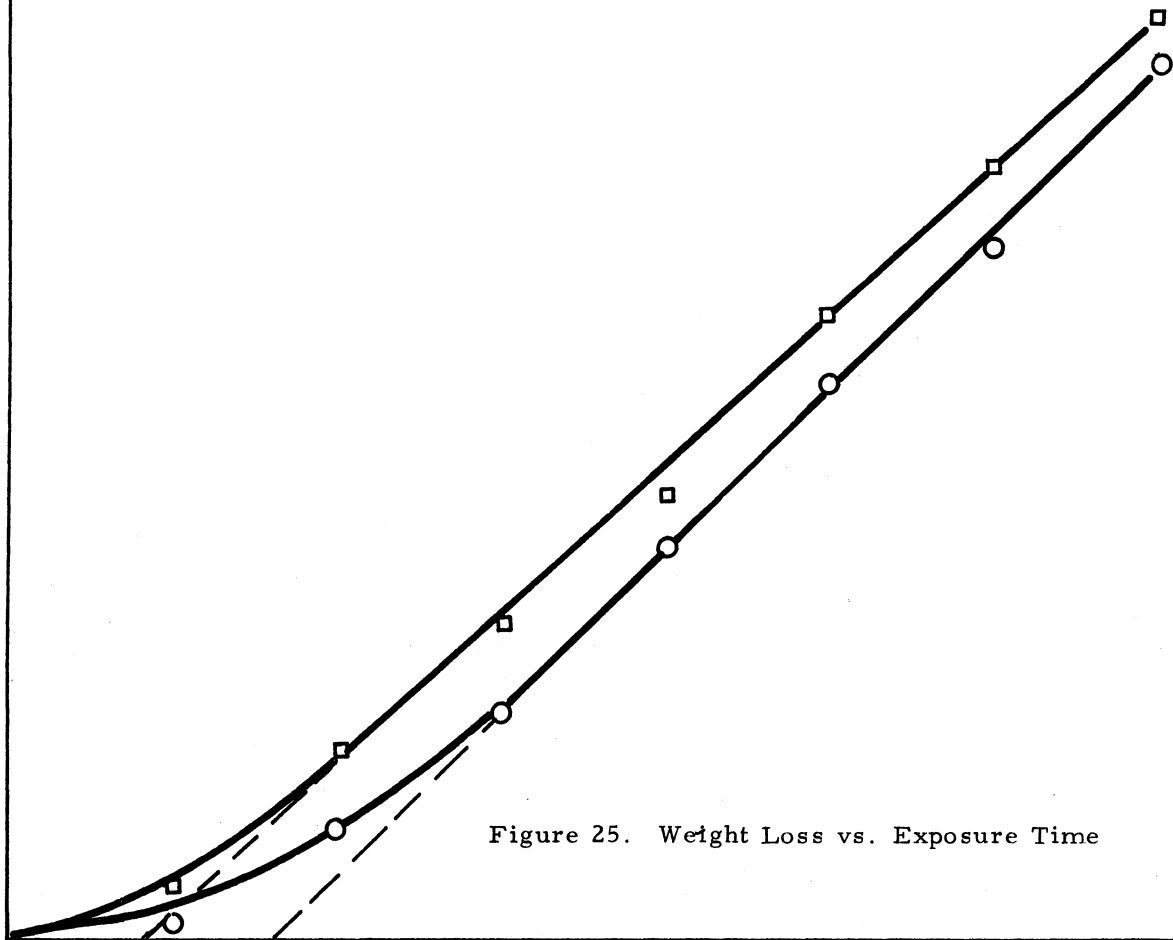


Figure 25. Weight Loss vs. Exposure Time

	Weight Loss Rate (mg/hr)	Incubation Period (hr)
△	Y-1 18.50 mg/hr	0.60
□	Y-2 18.50 mg/hr	0.60
○	Y-3 18.50 mg/hr	0.60

308 WIRE SOLUTION QUENCHED

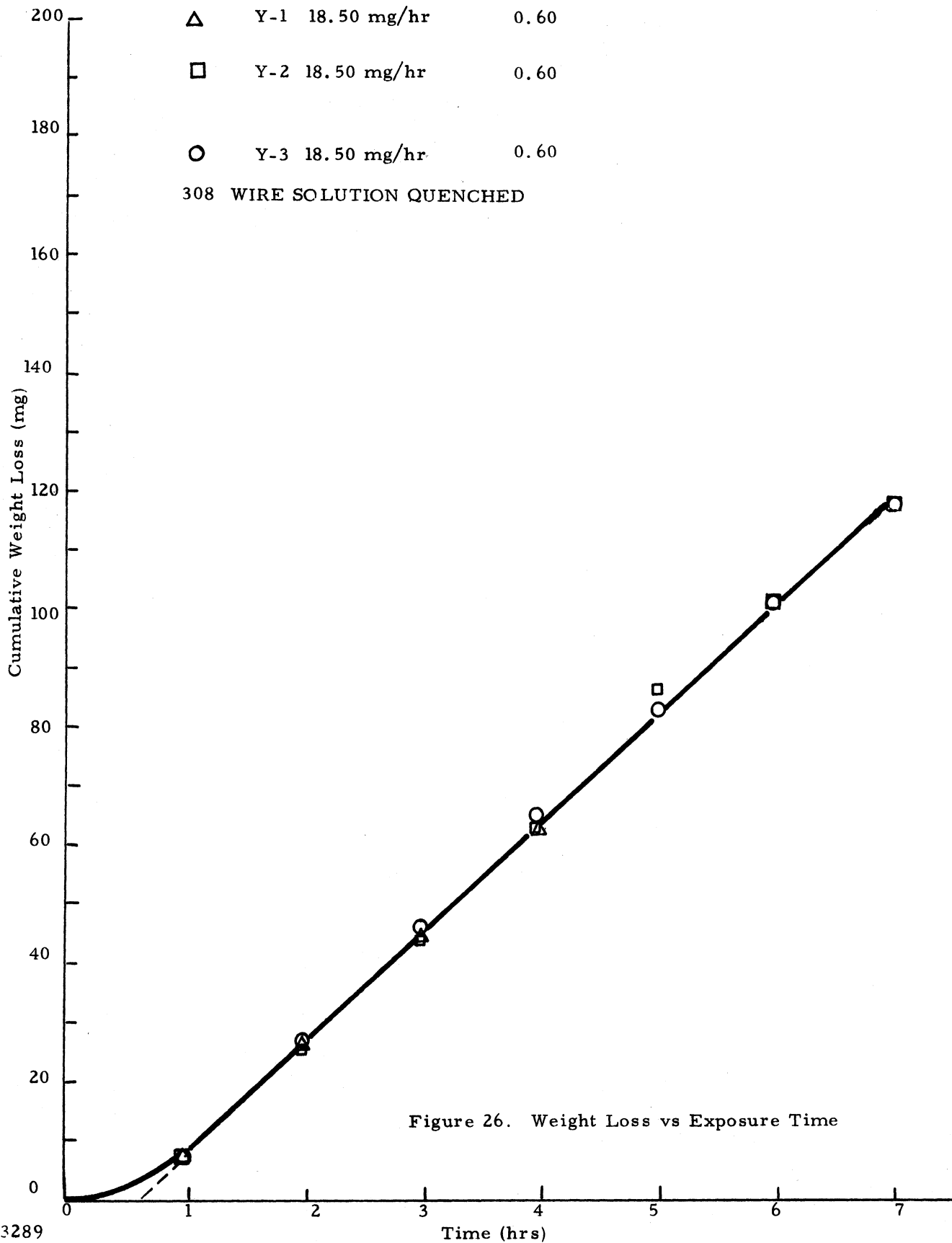


Figure 26. Weight Loss vs Exposure Time

E 410 STAINLESS AS WELDED

Weight Loss Rate (mg/hr)

Incubation Period (hr)

- Z<sub>1</sub>-1 10.00 mg/hr 0.75
- Z<sub>1</sub>-2 10.50 mg/hr 0.50
- △ Z<sub>1</sub>-3 10.70 mg/hr 0.60

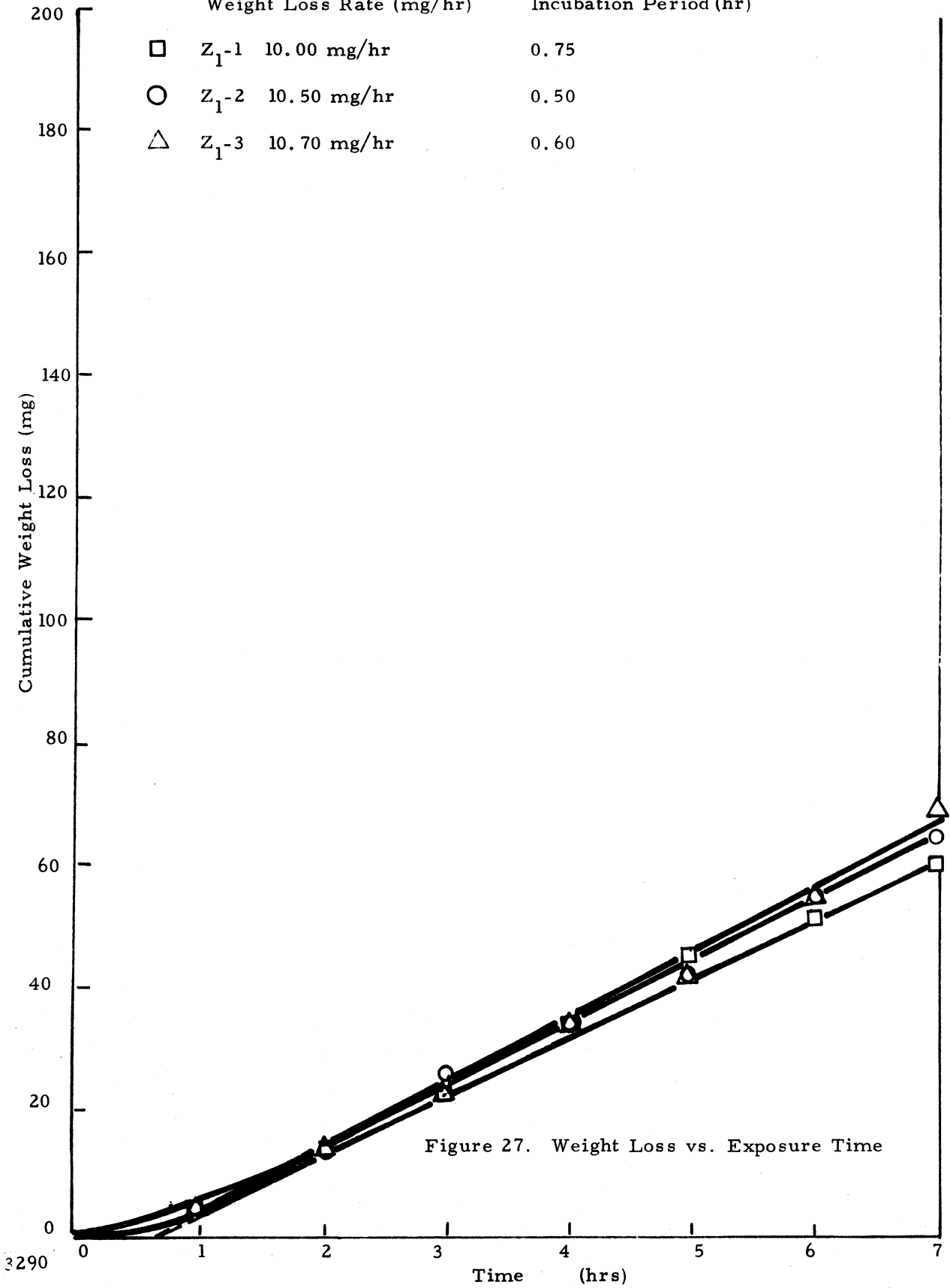


Figure 27. Weight Loss vs. Exposure Time

E 410 STRESS RELIEVED

	Weight Loss Rate (mg/hr)	Incubation Period (hr)
□	Z <sub>2</sub> -1 20.0 mg/hr	0.40
○	Z <sub>2</sub> -2 19.0 mg/hr	0.60
△	Z <sub>2</sub> -3 13.5 mg/hr	0.40

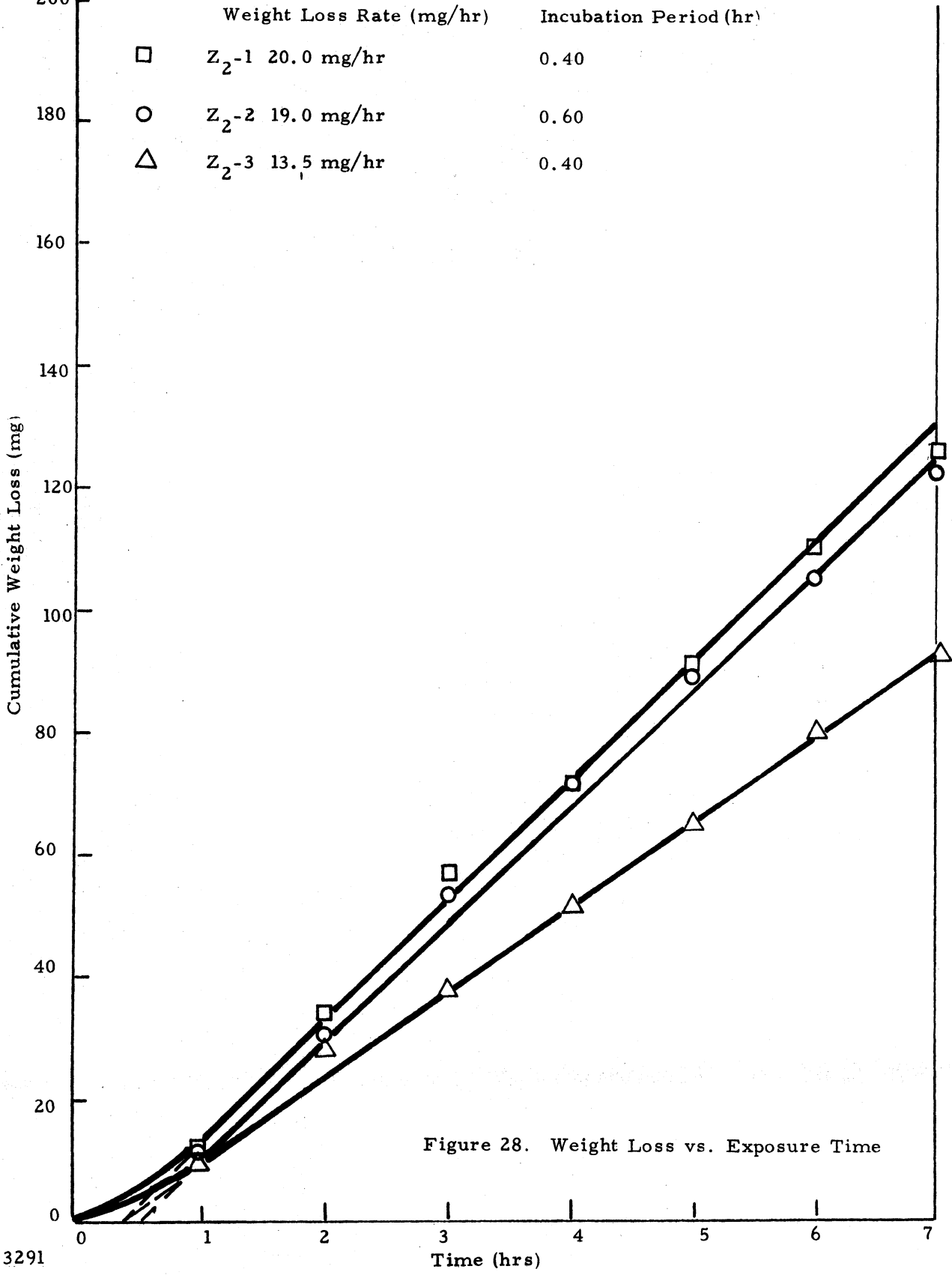


Figure 28. Weight Loss vs. Exposure Time

AM 355 STAINLESS

	Weight Loss Rate (mg/hr)	Incubation Period (hr)
□ A'-1	7.5 mg/hr	1.00
△ A'-2	6.0 mg/hr	1.75
○ A'-3	9.5 mg/hr	1.50

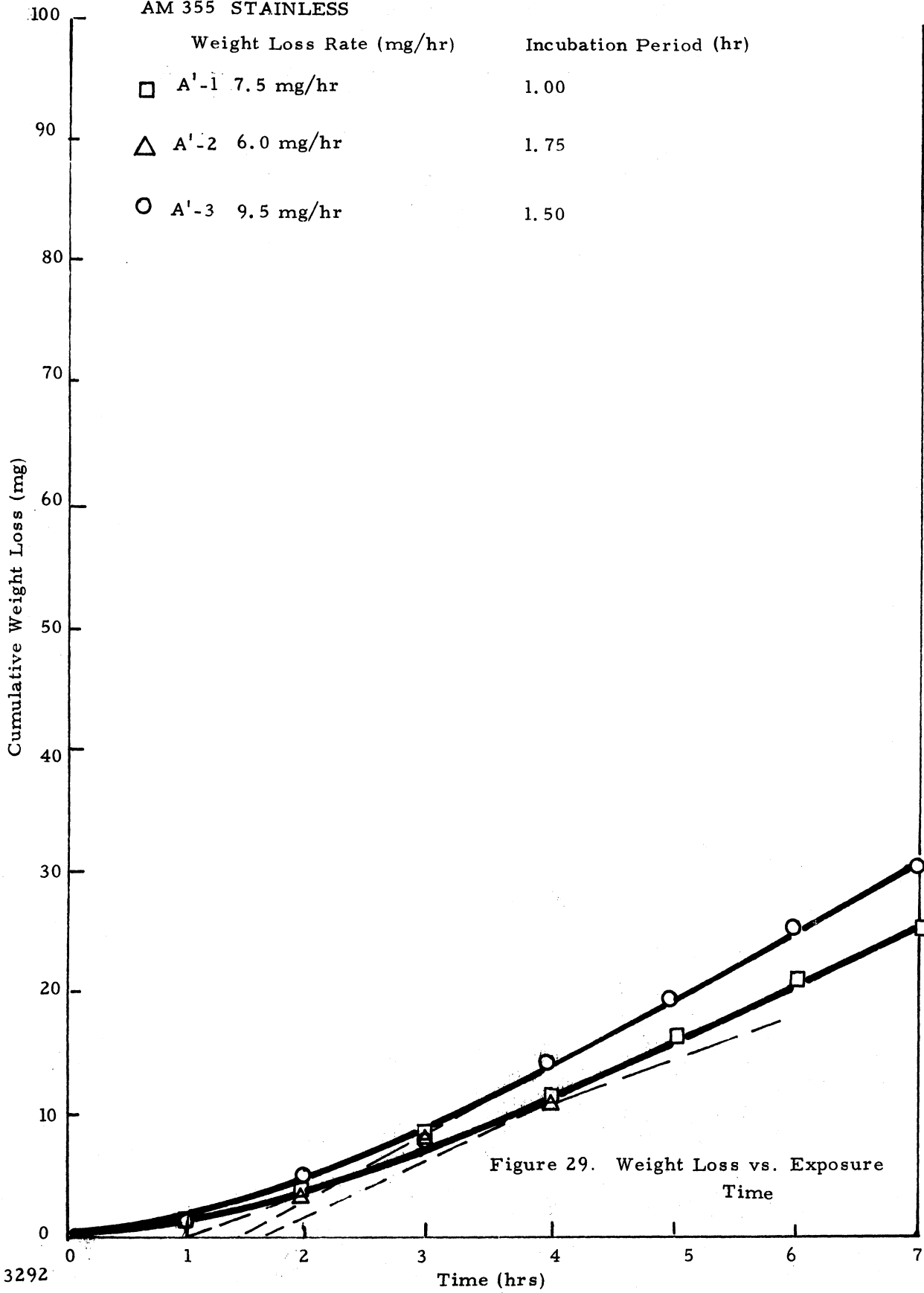
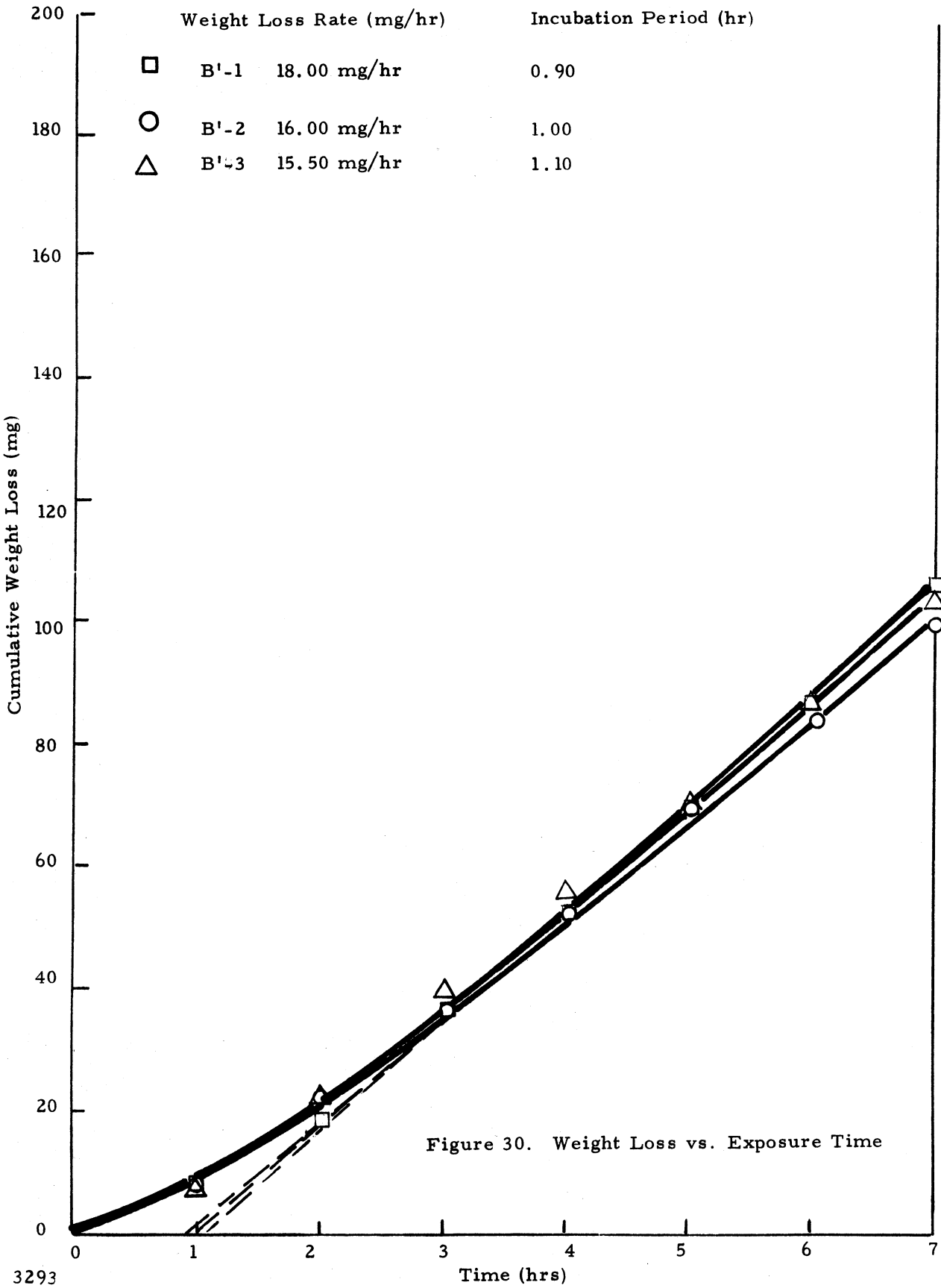
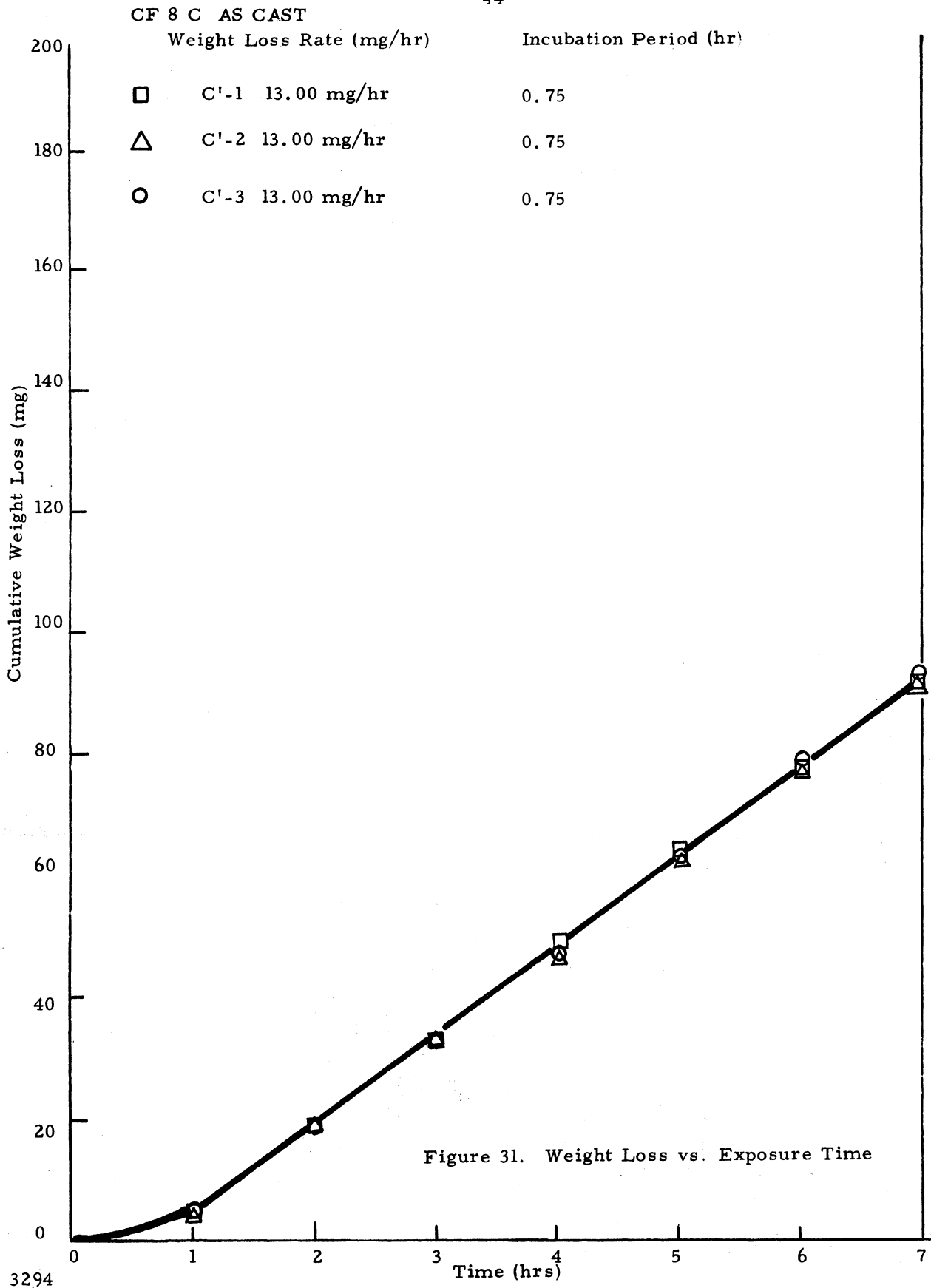


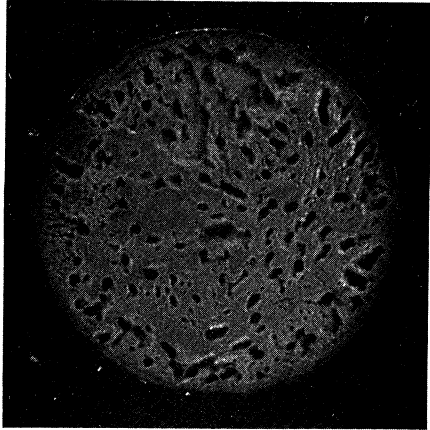
Figure 29. Weight Loss vs. Exposure Time



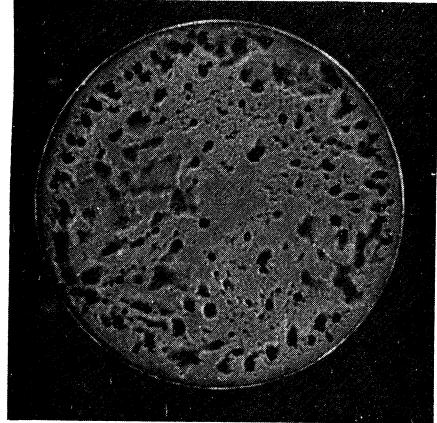
CF 8 C SOLUTION QUENCHED



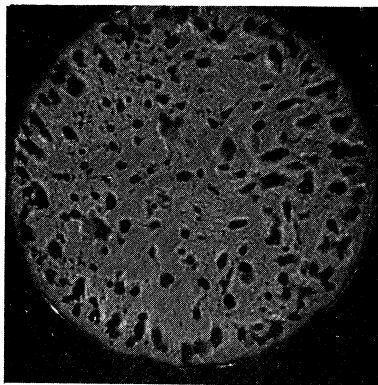




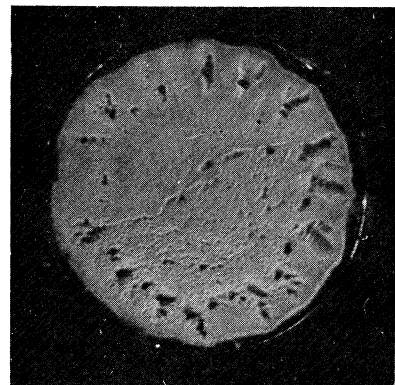
A-2 Grad CF 8  
WLR 23.00 mg/hr  
7 hr. exposure



A-4 Grad CF 8  
WLR 19.50 mg/hr  
7 hr. exposure

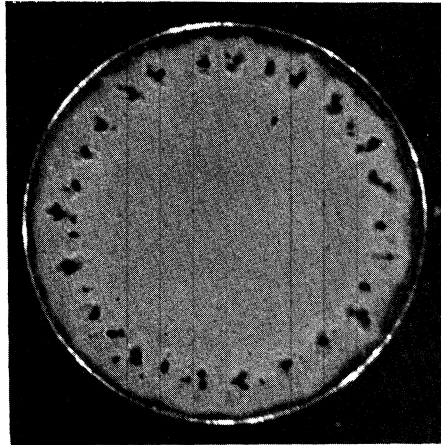


A-10 Grad CF 8  
WLR 22.75 mg/hr  
7 hr. exposure

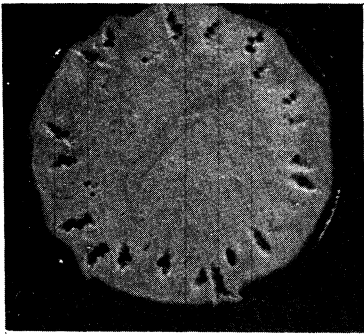


C-2 CA7M Stainless  
WLR 15.642 mg/hr  
7 hr. exposure

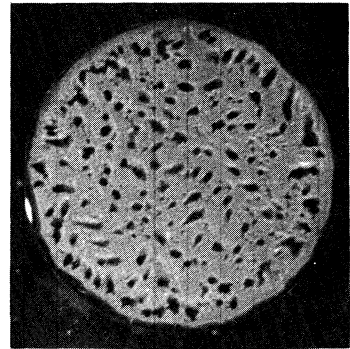
Figure 32. Photographs of Damaged Specimens A-C



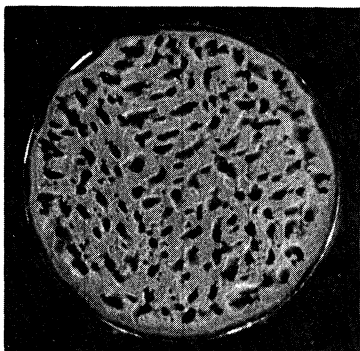
CA 15 #1  
WLR 19.90 mg/hr.  
7 hr. exposure



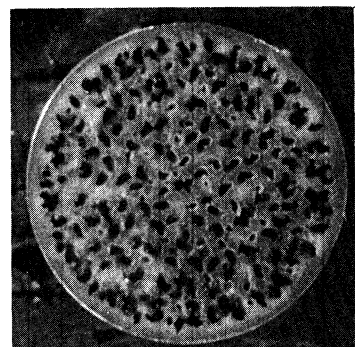
D-1 CA6NM Stainless  
WLR 12.666 mg/hr.  
7 hr. exposure



E-1 CF 8 Stainless  
WLR 22.00 mg/hr  
7 hr. exposure

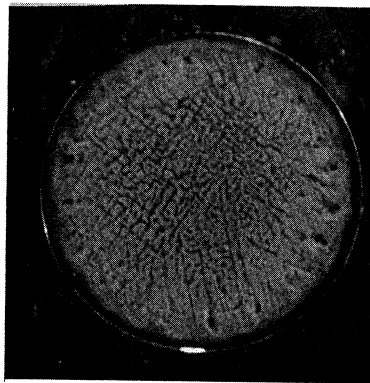


F-1 CF 8 Stainless  
WLR 22.70 mg/hr  
7 hr exposure

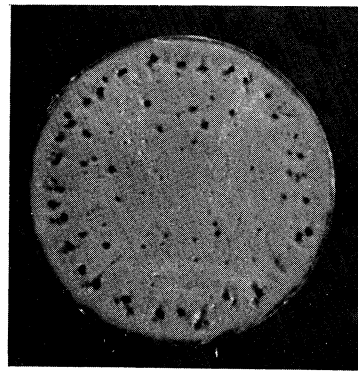


G-2 25 CN Carbon Steel  
WLR 34.60 mg/hr  
7 hr. exposure

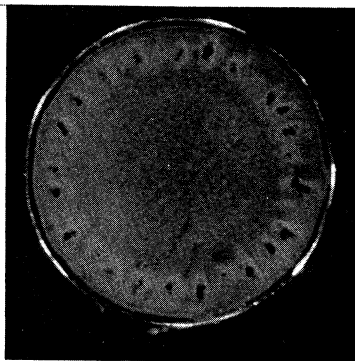
Figure 33. Photographs of Damaged Specimens CA-G



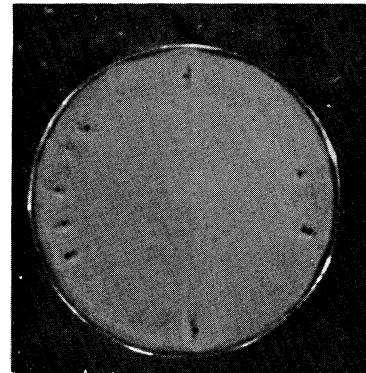
H-2 45 A 7 Carbon  
WLR 15.02 mg/hr  
7 hr. exposure



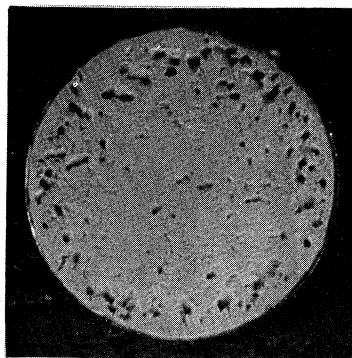
I-3 CA 15  
WLR 18.50 mg/hr  
7 hr. exposure



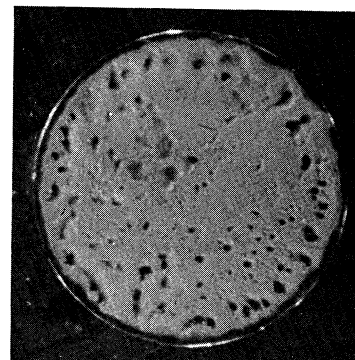
J-3 CA 15  
WLR 14.09 mg/hr  
7 hr. exposure



K-3 CA 15  
WLR 10.70 mg/hr  
7 hr. exposure



L-2 CF 8 Stainless  
WLR 15.20 mg/hr  
7 hr. exposure

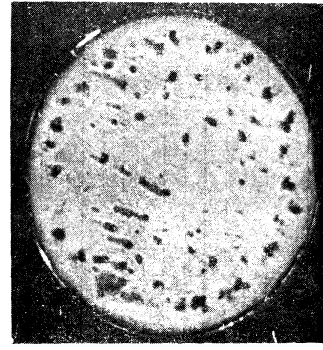


M-2 CF 8  
WLR 17.32 mg/hr  
7 hr. exposure

Figure 34. Photographs of Damaged Specimens H-M



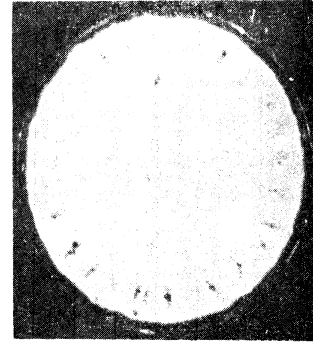
N-2 Arcos Stainlend  
WLR 16.36 mg/hr  
7 hr. exposure



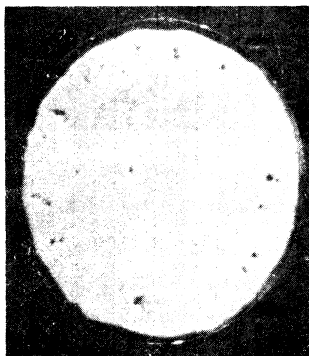
Q-2 Arcos Stainlend  
WLR 16.38 mg/hr  
7 hr. exposure



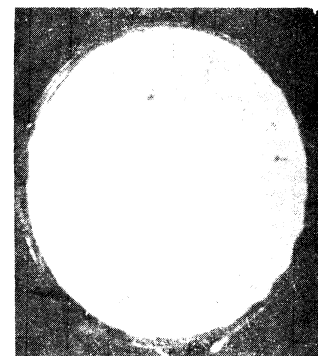
P-3 304-L Sol.  
WLR 17.70 mg/hr  
7 hr. exposure



Q-2 304-L Sensitized  
WLR 20.20 mg/hr  
7 hr. exposure

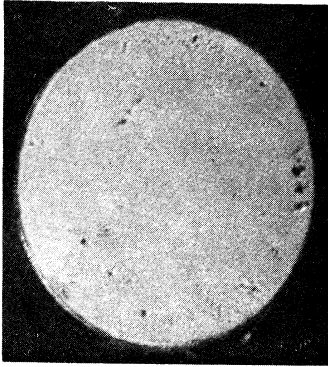


R-3 CF 8 M Sol. quenched  
WLR 16.25 mg/hr  
7 hr. exposure

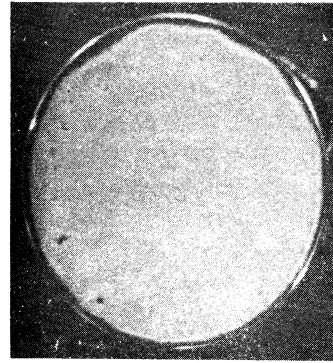


S-2 CF 8 M  
WLR 16.10 mg/hr  
7 hr. exposure

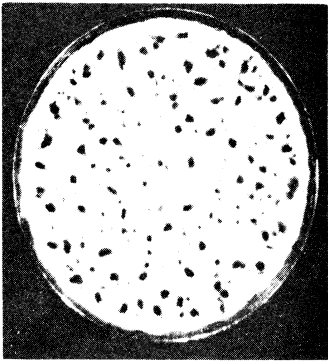
Figure 35. Photographs of Damaged Specimens N-5



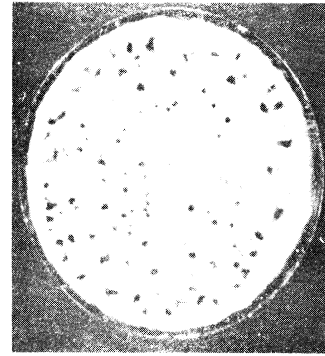
T-2 CE 30 Water quenched  
WLR 14.80 mg/hr  
7 hr. exposure



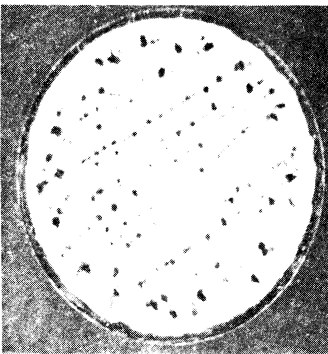
U-1 CE 30 As cast  
WLR 15.15 mg/hr  
7 hr. exposure



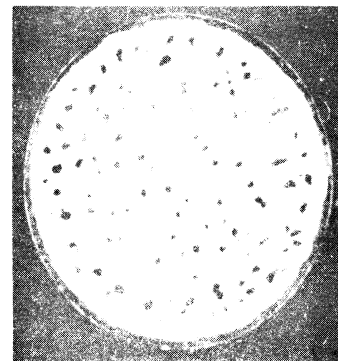
V-2 308-L Water quenched  
WLR 20.00 mg/hr  
7 hr. exposure



W-2 308-L As welded  
WLR 16.50 mg/hr  
7 hr. exposure

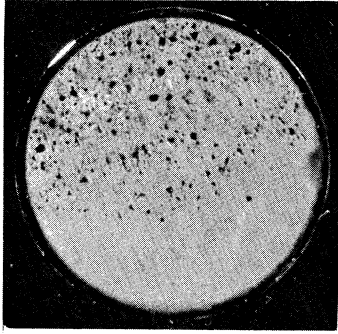


X-1 308 Wire as welded  
WLR 17.50 mg/hr  
7 hr. exposure

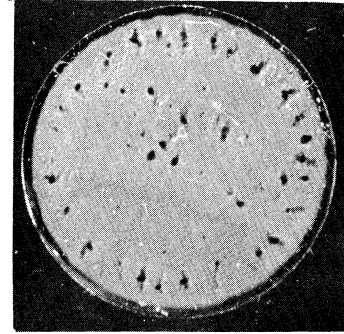


Y-2 308 Wire sol. quenched  
WLR 18.00 mg/hr  
7 hr. exposure

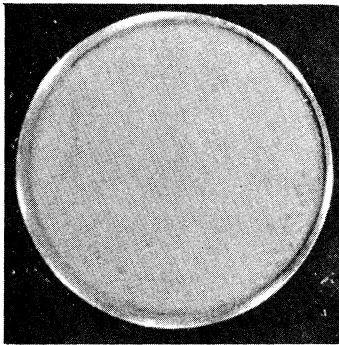
Figure 36. Photographs of Damaged Specimens (1-3)



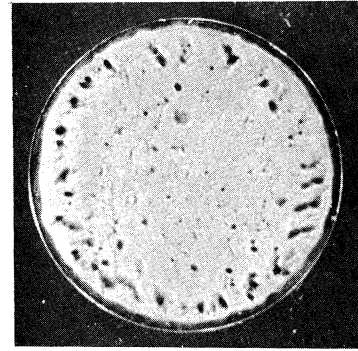
Z<sub>1</sub>-3 E 410 Stainless as welded  
WLR 10.70 mg/hr  
7 hr. exposure



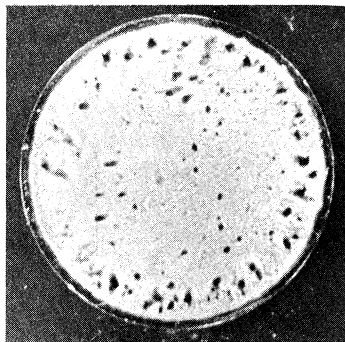
Z<sub>2</sub>-3 E 410 Stress relieved  
WLR 13.50 mg/hr  
7 hr. exposure



A'-1 AM 355 Stainless  
WLR 7.50 mg/hr  
7 hr. exposure



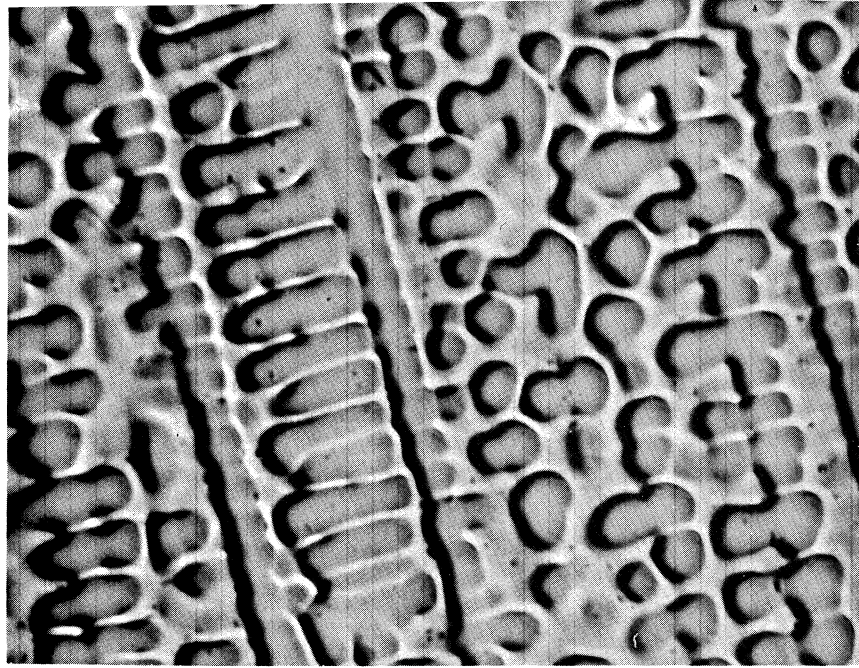
B'-2 CF 8 C Sol. quenched  
WLR 16.00 mg/hr  
7 hr. exposure



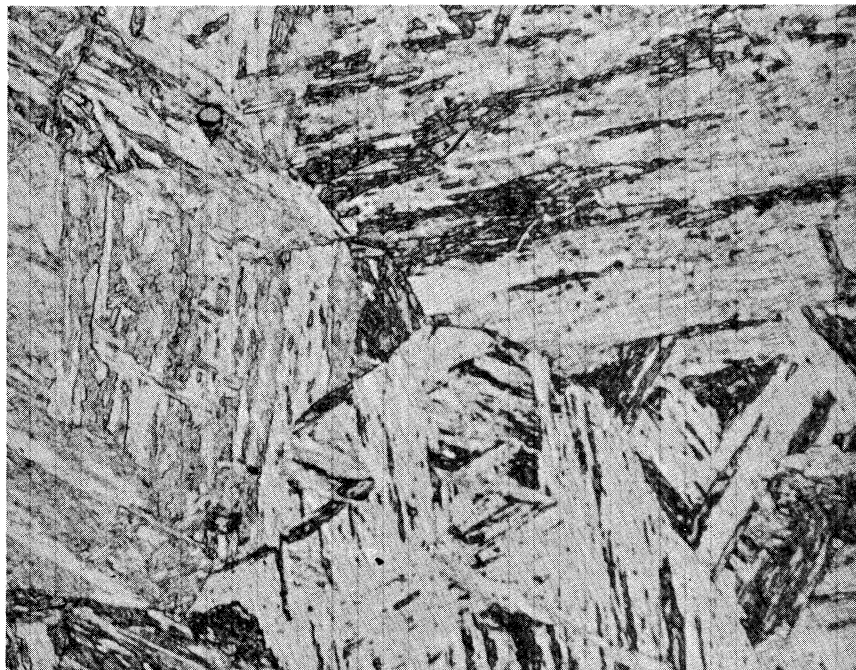
C'-2 CF 8 C As cast  
WLR 13.00 mg/hr  
7 hr. exposure

Figure 37. Photographs of Damaged Specimens Z<sub>1</sub>- C'



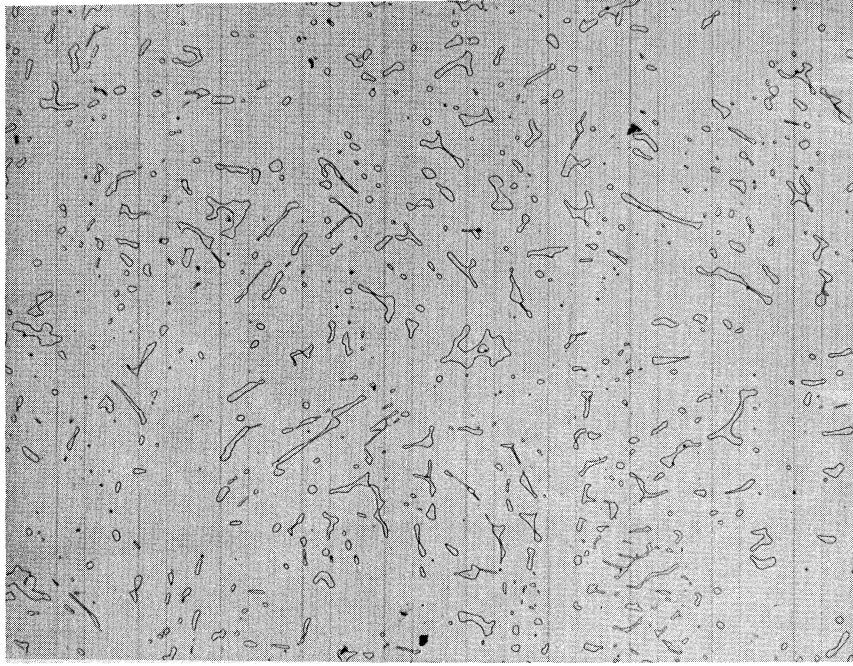


U of M No. C-1                      CN7M - Stainless Heat # C-808  
                   C-2                      Solution Quenched - 2000° F  
                   C-3                      X100 Electrolytic Etch

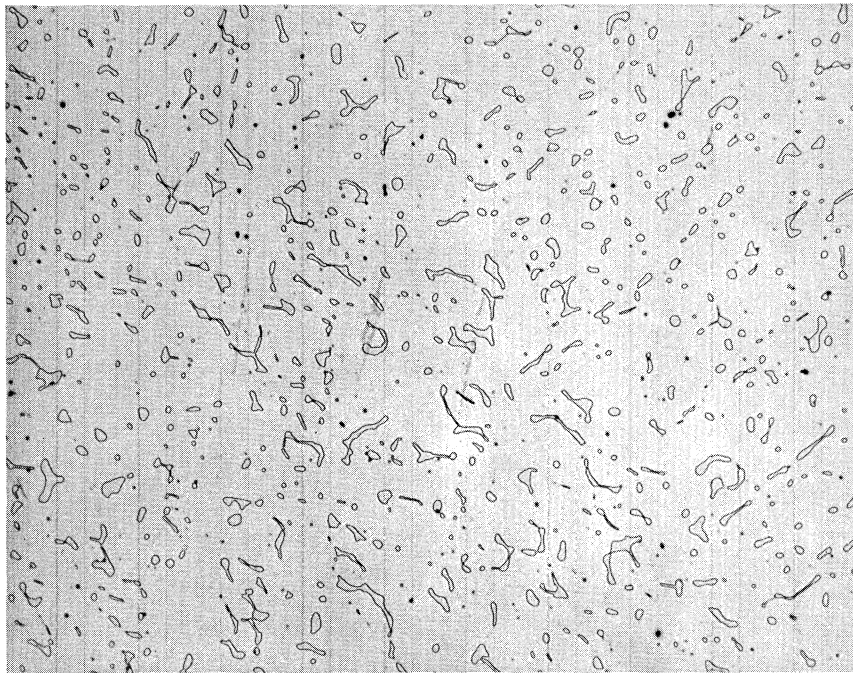


U of M No. D-1                      CA6NM (12 Cr 4 Ni) Heat #E4967  
                   D-2                      Normalized and Tempered  
                   D-3                      X 500 Ferric Chloride Etch

Figure 38. Photomicrograph of material C-1, 2, 3, and D-1, 2, 3

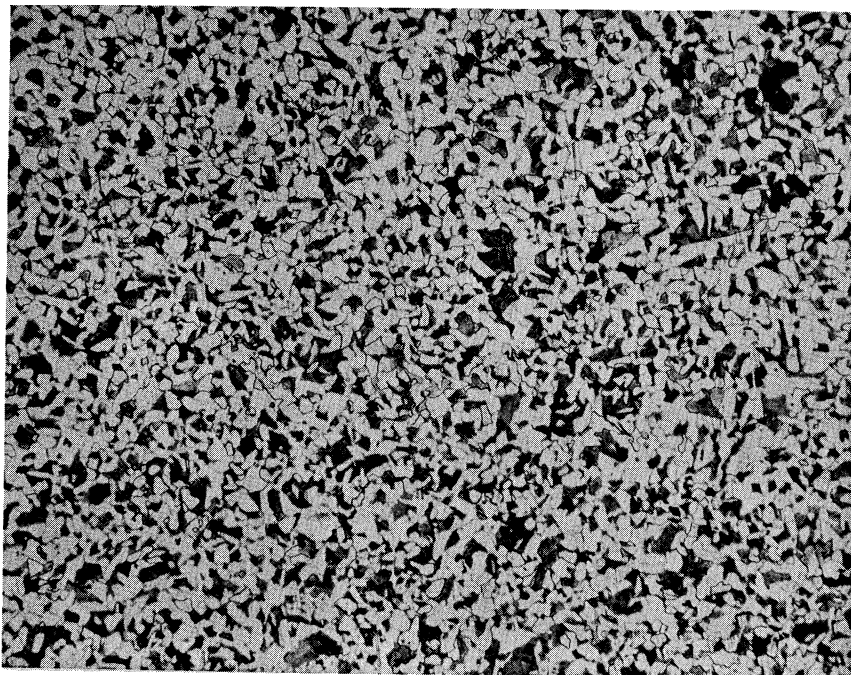


U of M No. F-1      CF8 Stainless (Vacuum Melted)  
                  F-2      Solution quenched from 2000°F  
                  F-3      X100 Electrolytic Etch



U of M No. E-1      CF8 Stainless (Air Melted)  
                  E-2      Solution quenched from 2000°F  
                  E-3      X100 Electrolytic Etch

Figure 39. Photomicrograph of material F-1, 2, 3 and E-1, 2, 3



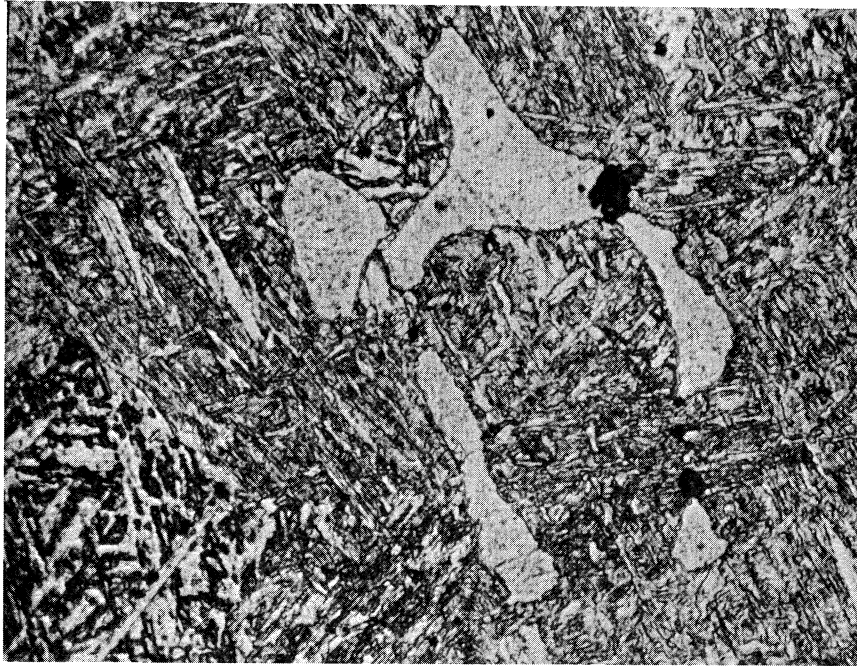
U of M No. G-1                      25CN (Carbon Steel) Normalized  
                  G-2                      and Tempered X100 2% Nital Etc  
                  G-3



U of M No. H-1                      45A7 (Carbon Chrome Moly Steel)  
                  H-2                      Normalized and Tempered  
                  H-3                      X500 2% Nital Etch

Figure 40. Photomicrograph of material G-1, 2, 3 and H-1, 2, 3



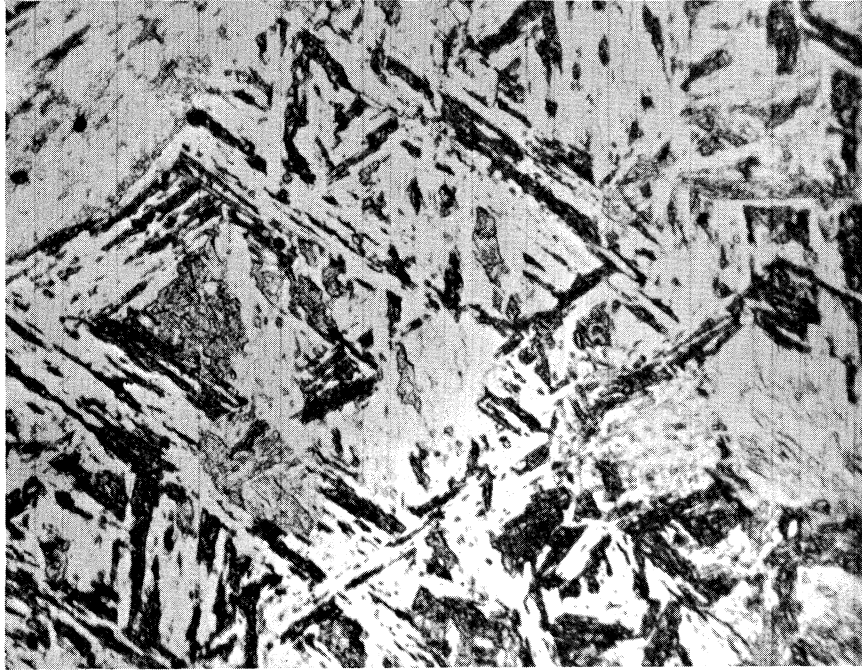


U of M No. I-1 CA-15 High Cr, High Si, structure containing Ferrite. Normal properties  
 I-2  
 I-3 X500 Ferric Chloride Etch.



U of M No. J-1 CA15 - Low Cr, Low Si, structure containing no Ferrite. Normal properties  
 J-2  
 J-3 X500 Ferric Chloride Etch

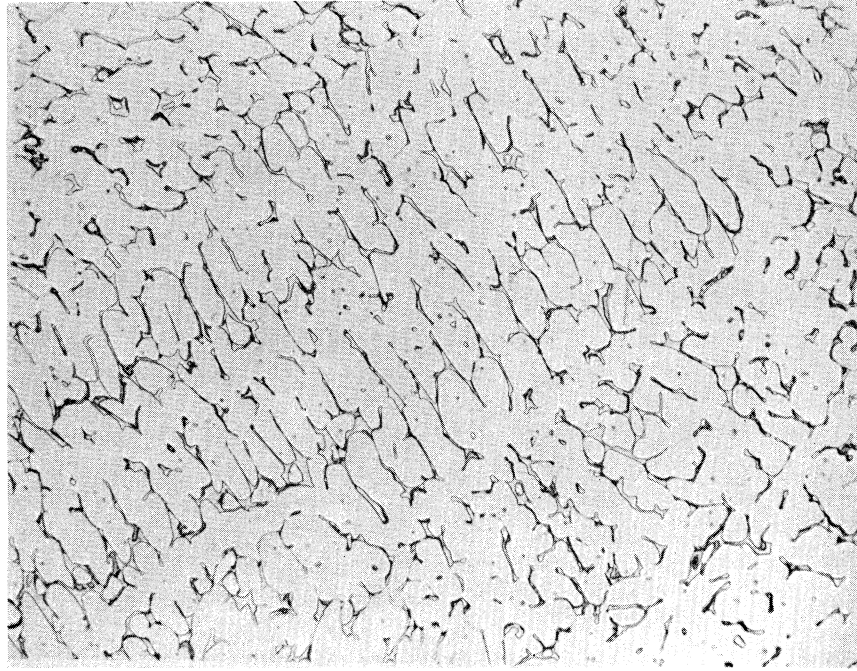
Figure 41. Photomicrograph of material I-- 1, 2, 3 and J-1, 2, 3



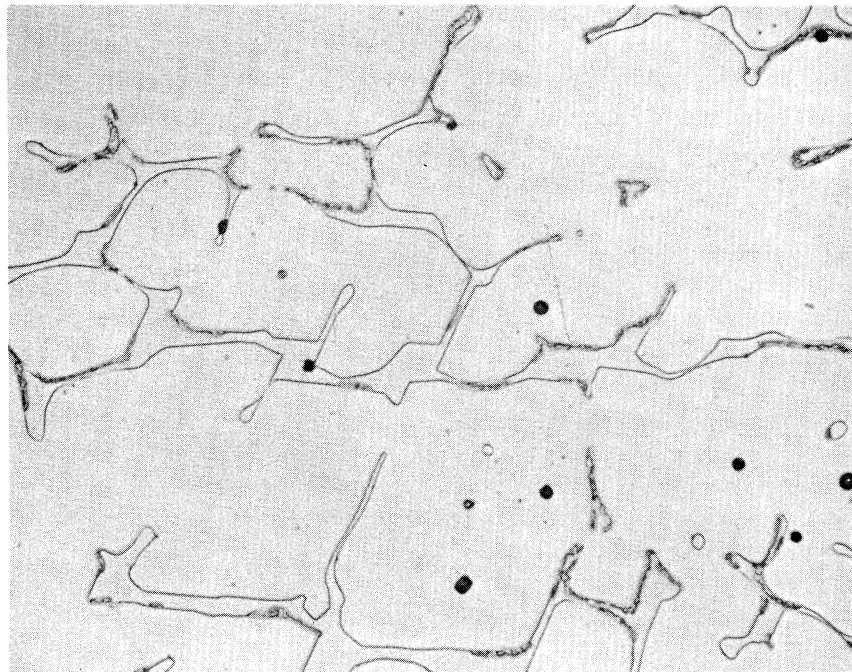
U of M No. K-1  
K-2  
K-3

CA15 - Low Cr, Low Si Structure containing no Ferrite. Heat treated to 248 - 302 BHN. (A. C. and BLH Impellers) X500 Ferric Chloride.

Figure 42. Photomicrograph of Material K-1, 2, 3

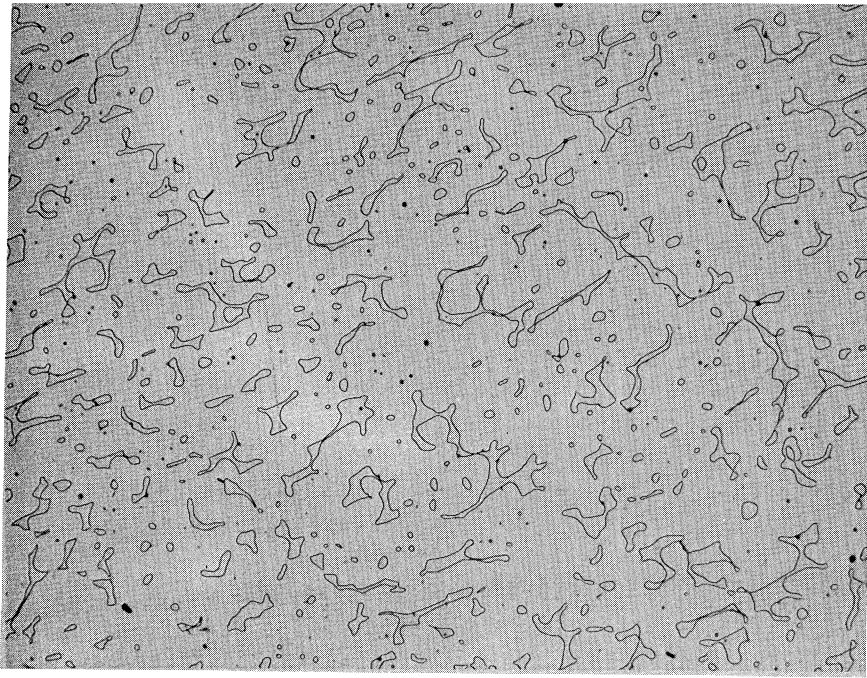


U of M No. L-1                      CF 8 Stainless - High Ferrite  
                  L-2                      (17%) As Cast X100 Electrolytic  
                  L-3                      Etch

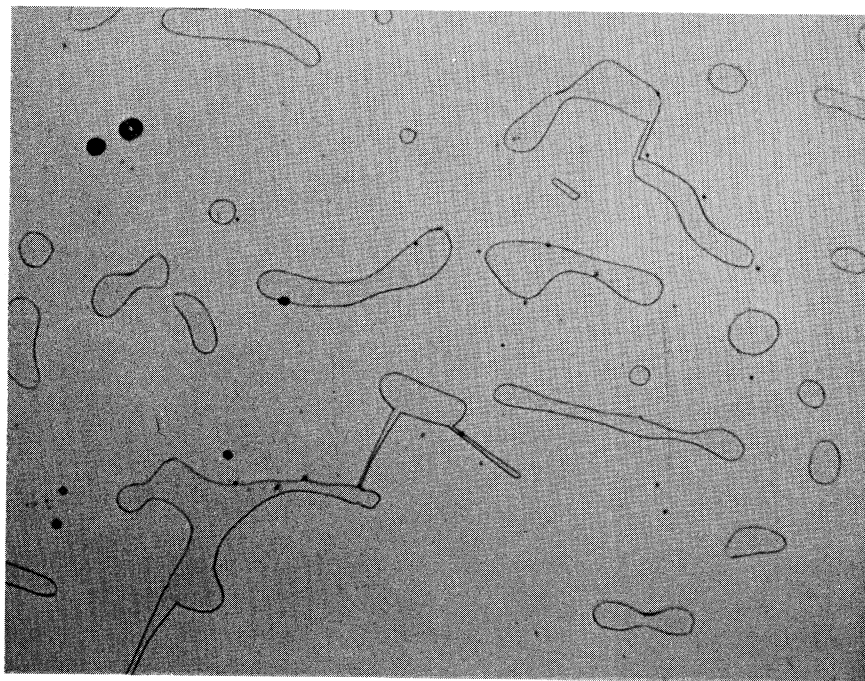


U of M No. L-1                      CF8 Stainless - High Ferrite  
                  L-2                      (17%) As Cast X500 Electrolytic  
                  L-3                      Etch

Figure 43. Photomicrograph of Material L-1, 2, 3



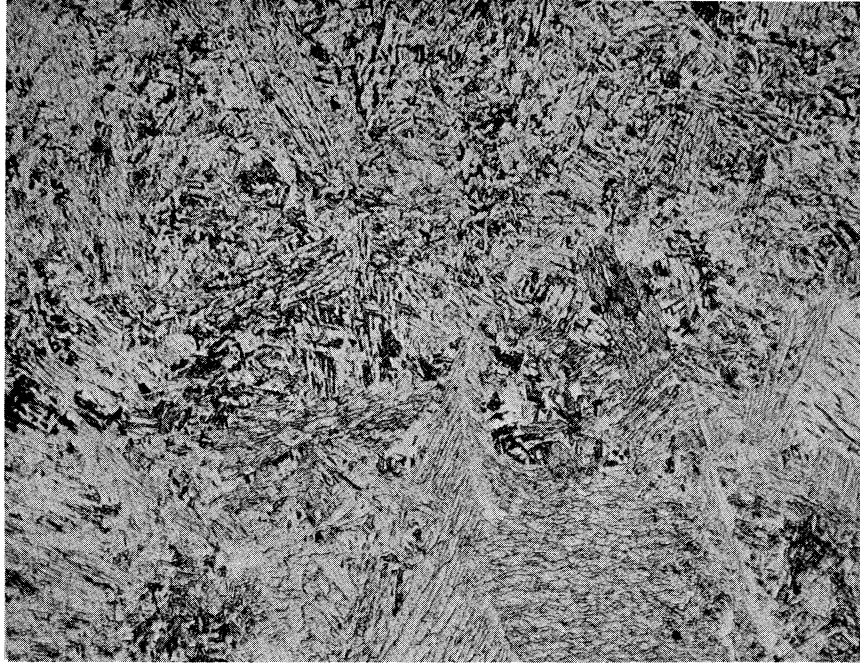
U of M No. M-1                      CF8 Stainless - High Ferrite  
                  M-2                      (17%) Sol. Quenched X100  
                  M-3                      Electrolytic Etch



U of M No. M-1                      CF8 Stainless - High Ferrite  
                  M-2                      (17%) Sol. Quenched X500  
                  M-3                      Electrolytic Etch

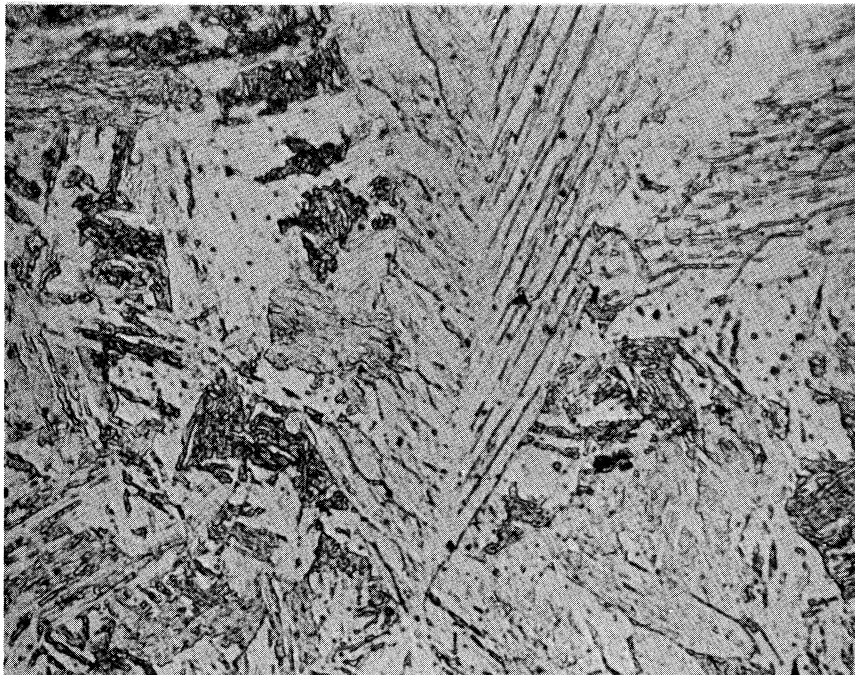
Figure 44. Photomicrograph of Material M-1,2,3





U of M No. N-1  
N-2  
N-3

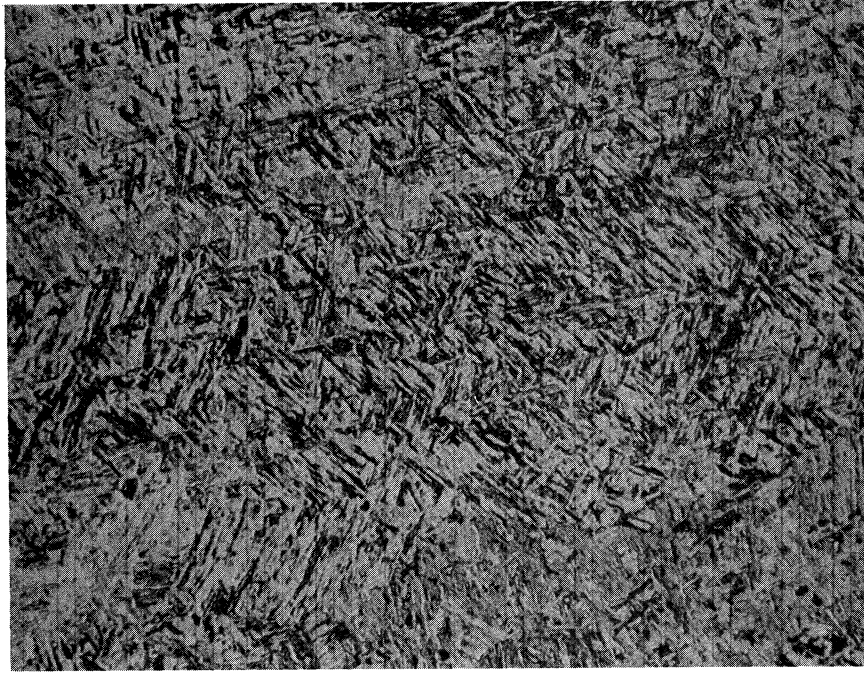
Arcos Stainlend 134 Ni As welded  
Deposit X100 Fe Cl Etch



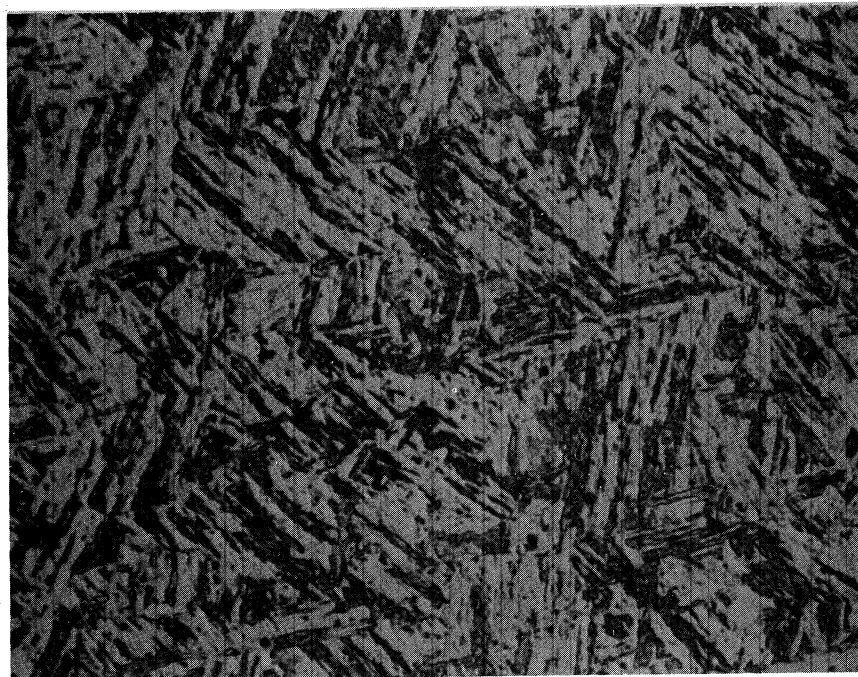
U of M No. N-1  
N-2  
N-3

Arcos Stainlend 134 Ni Deposit  
As welded X500 Fe Cl Etch



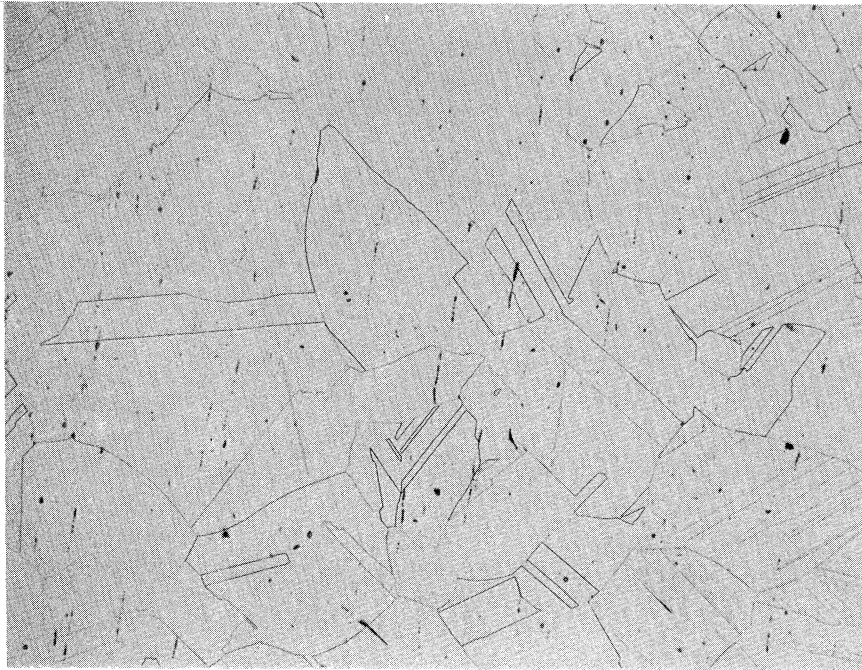


U of M No. O-1                      Stainlend 134 Ni Weld Deposit  
   O-2                                      Stress Relieved 1175<sup>o</sup>F A. C.  
   O-3                                      X100 FeCl Etch

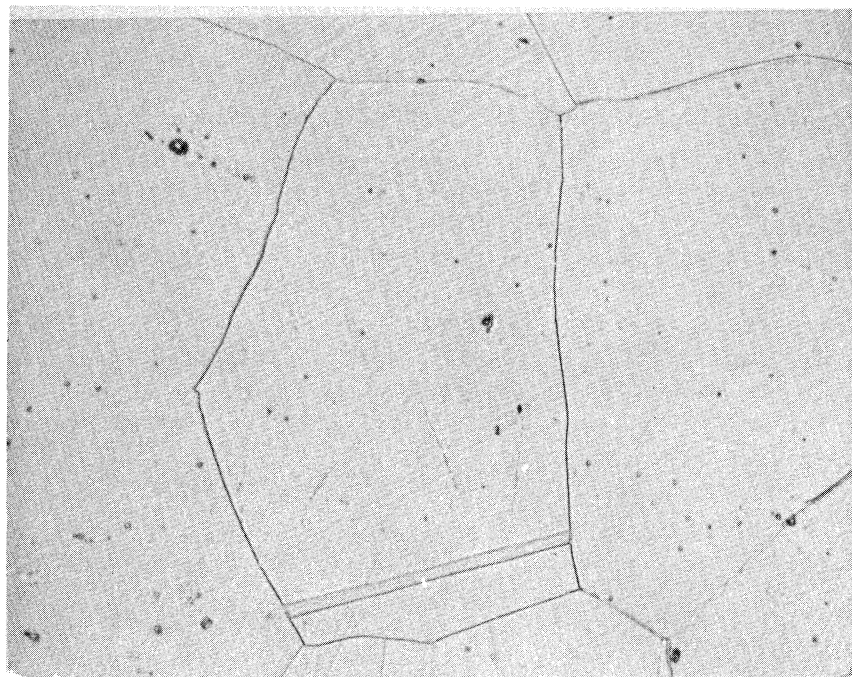


U of M No. O-1                      Stainlend 134 Ni Weld Deposit  
   O-2                                      Stress Relieved 1175<sup>o</sup>F A. C.  
   O-3                                      X500 FeCl Etch

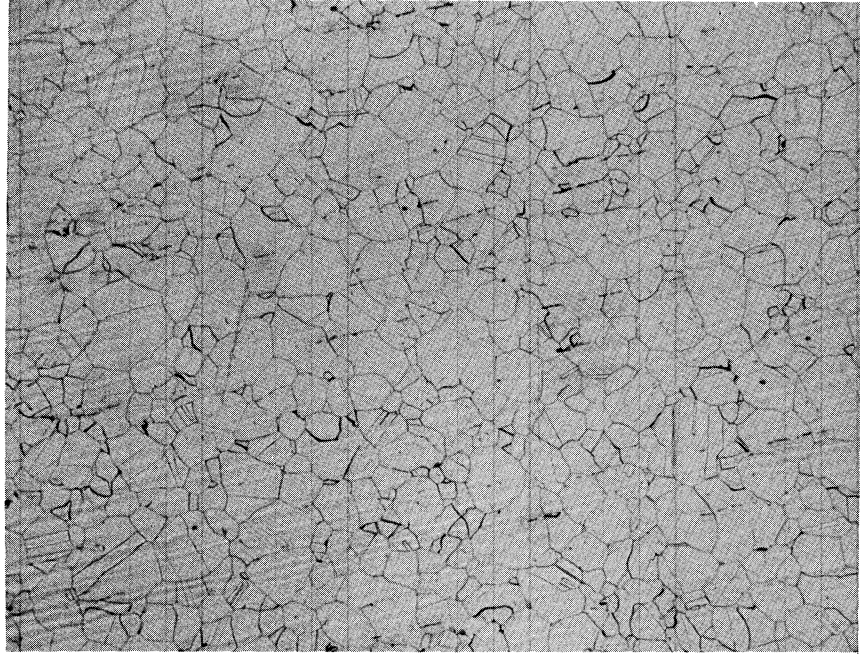
Figure 46. Photomicrograph of Material O-1, 2, 3



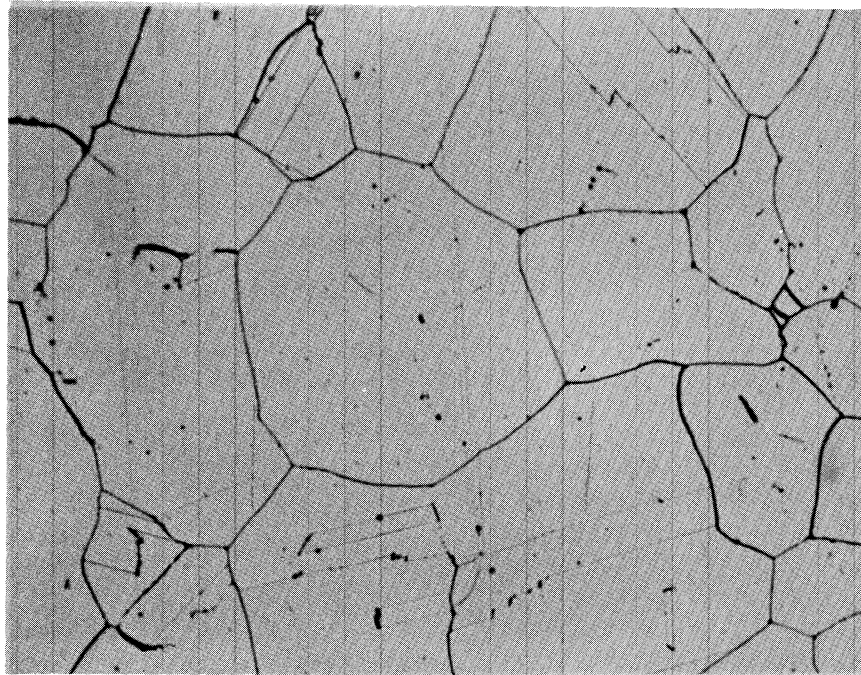
U of M No. P-1            Type 304-L Stainless Solution  
                                 P-2            Quenched 2050<sup>o</sup>F X100  
                                 P-3            Electrolytic Etch



U of M No. P-1            Type 304-L Stainless Solution  
                                 P-2            Quenched 2050<sup>o</sup>F X500  
                                 P-3            Electrolytic Etch

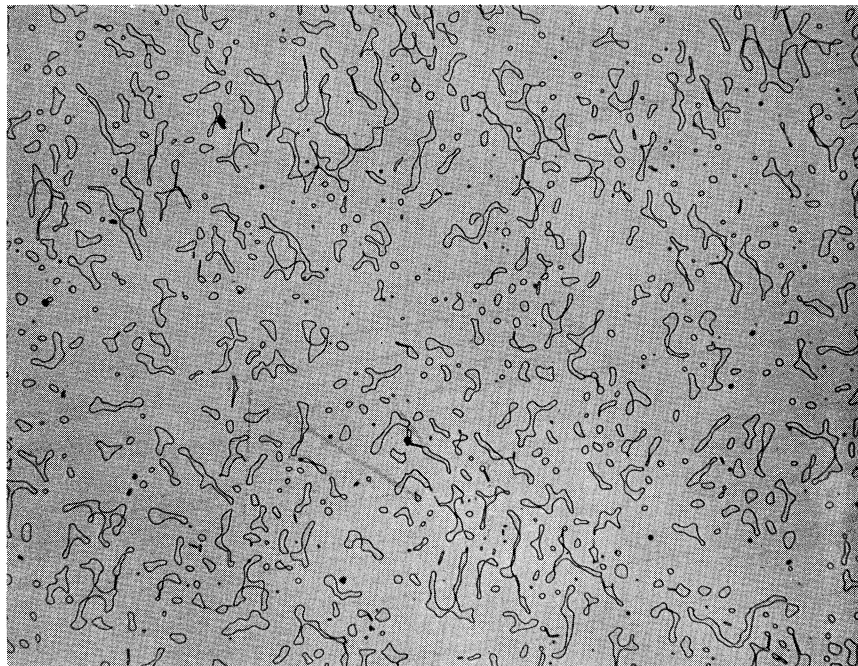


U of M No. Q-1                    304-L Stainless Sensitized  
                  Q-2                    1250<sup>o</sup>F 25 Hours X100  
                  Q-3                    Electrolytic Etch



U of M No. Q-1                    304-L Stainless Sensitized  
                  Q-2                    1250<sup>o</sup>F 25 Hours X500  
                  Q-3                    Electrolytic Etch



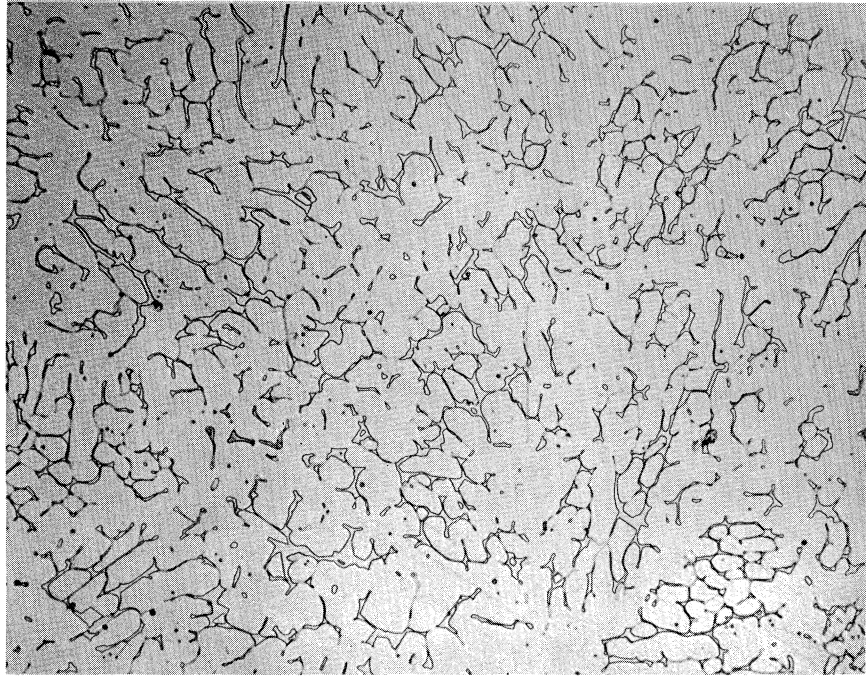


U of M No. R-1                      CF8M Stainless Solution Quenched  
   R-2                                      from 2050°F X100 Electrolytic  
   R-3                                      Etch



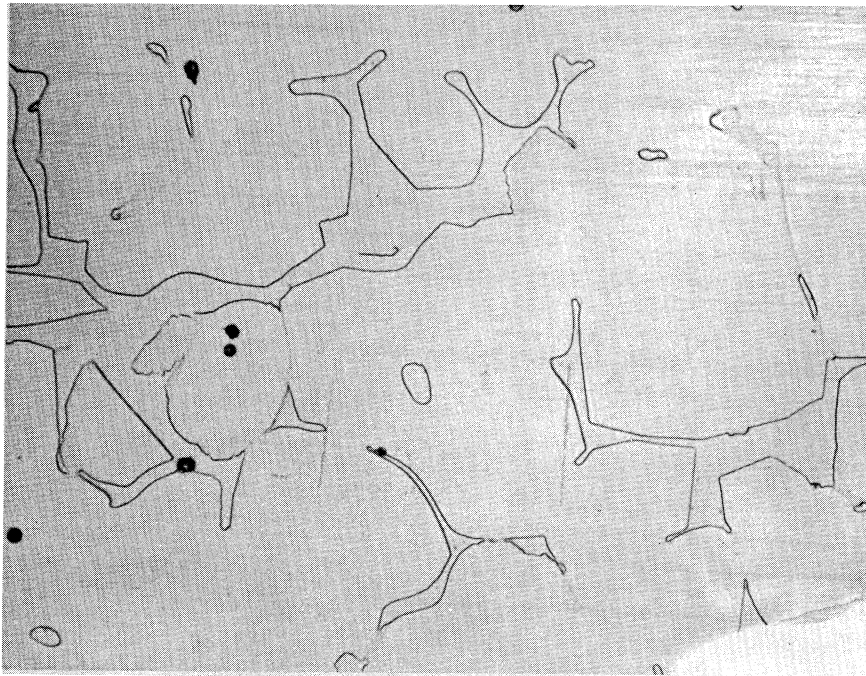
U of M No. R-1                      CF8M Stainless Solution Quenched  
   R-2                                      from 2050°F X500 Electrolytic  
   R-3                                      Etch

Figure 49. Photomicrograph of Material R-1, 2, 3



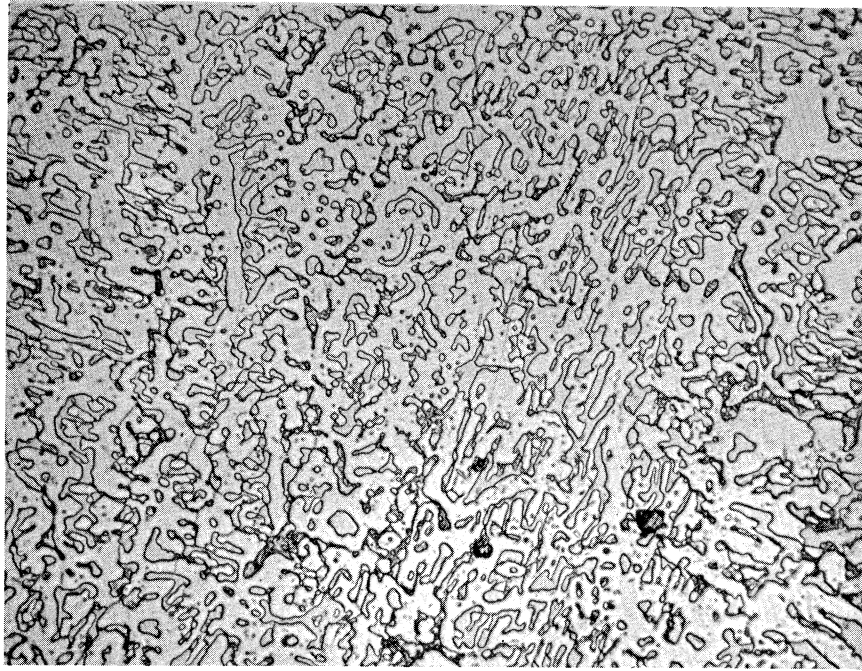
U of M No. S-1  
S-2  
S-3

CF8M Stainless As Cast X100  
Electrolytic Etch

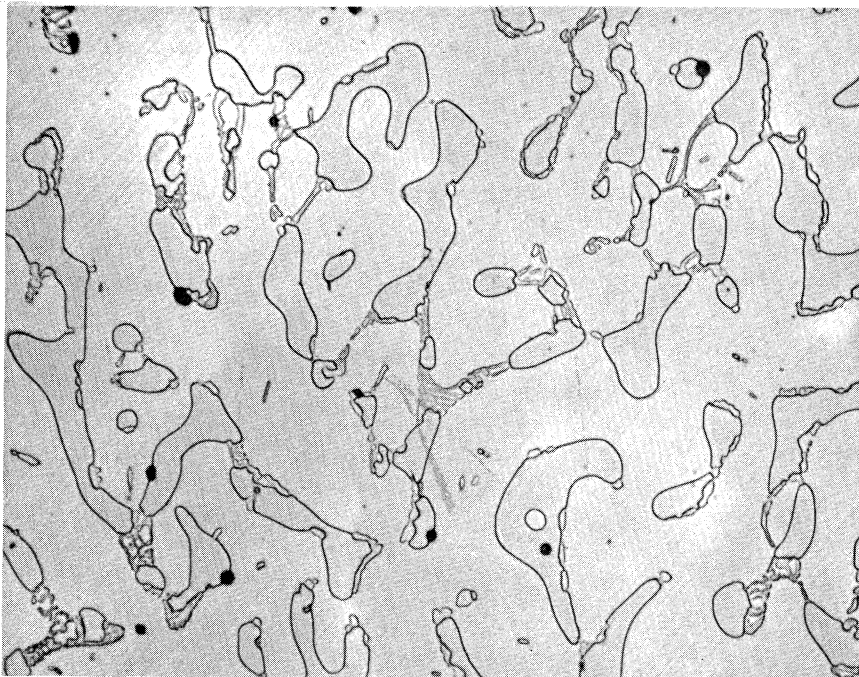


U of M No. S-1  
S-2  
S-3

CF8M Stainless As Cast X500  
Electrolytic Etch

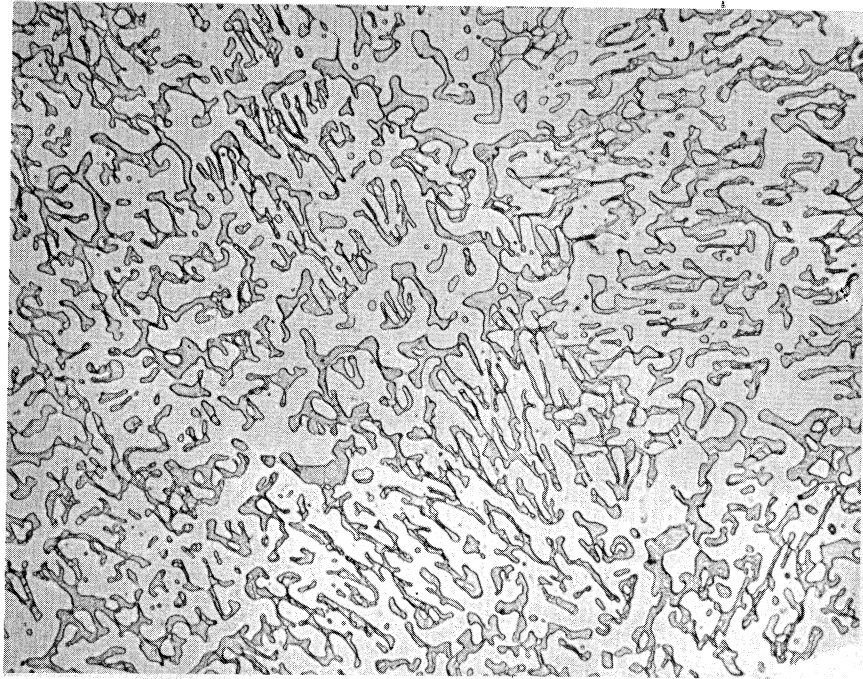


U of M No. T-1                      CE30 Stainless - Sol. Quenched  
                  T-2                      2000° F X100 Electrolytic Etch  
                  T-3

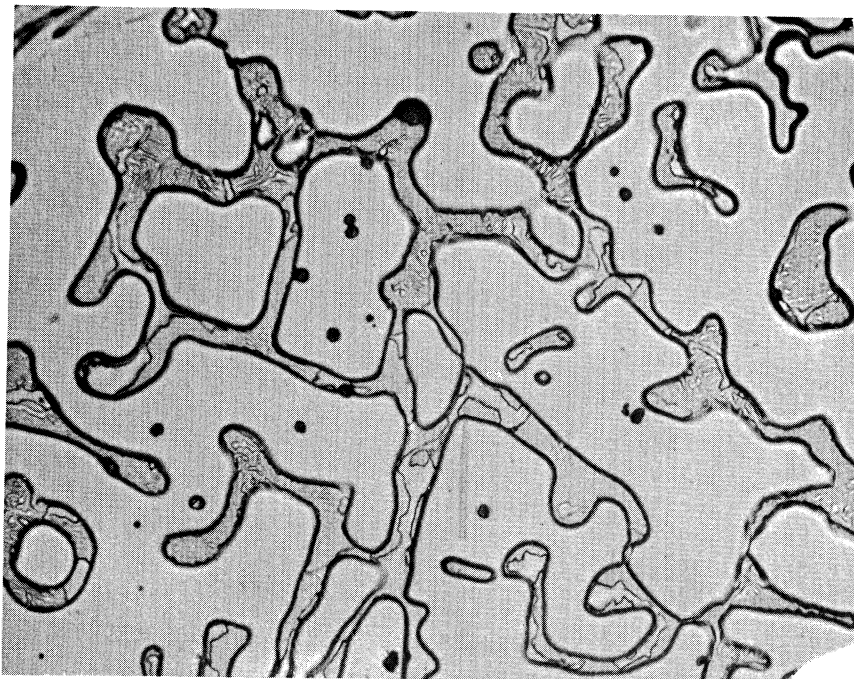


U of M No. T-1                      CE30 Stainless - Sol. Quenched  
                  T-2                      2000° F X500 Electrolytic Etch  
                  T-3

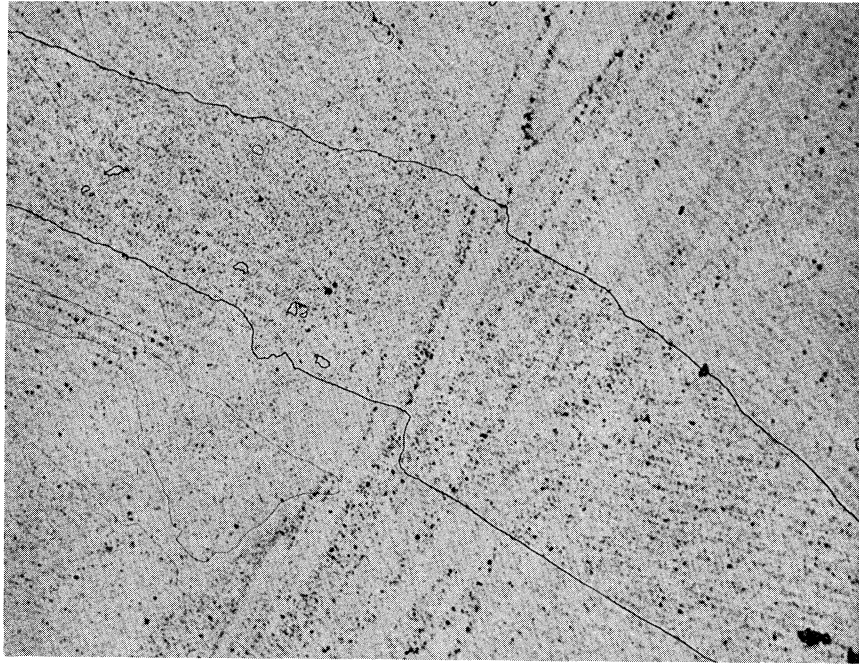




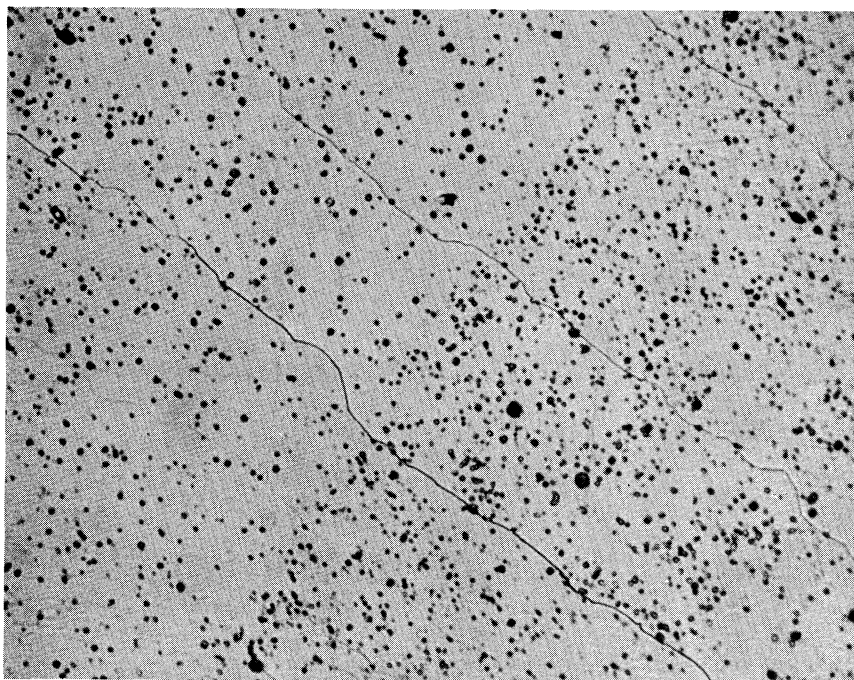
U of M No. U-1                      CE30 Stainless - As Cast X100  
                  U-2                      Electrolytic Etch  
                  U-3



U of M No. U-1                      CE30 Stainless - As Cast X500  
                  U-2                      Electrolytic Etch  
                  U-3

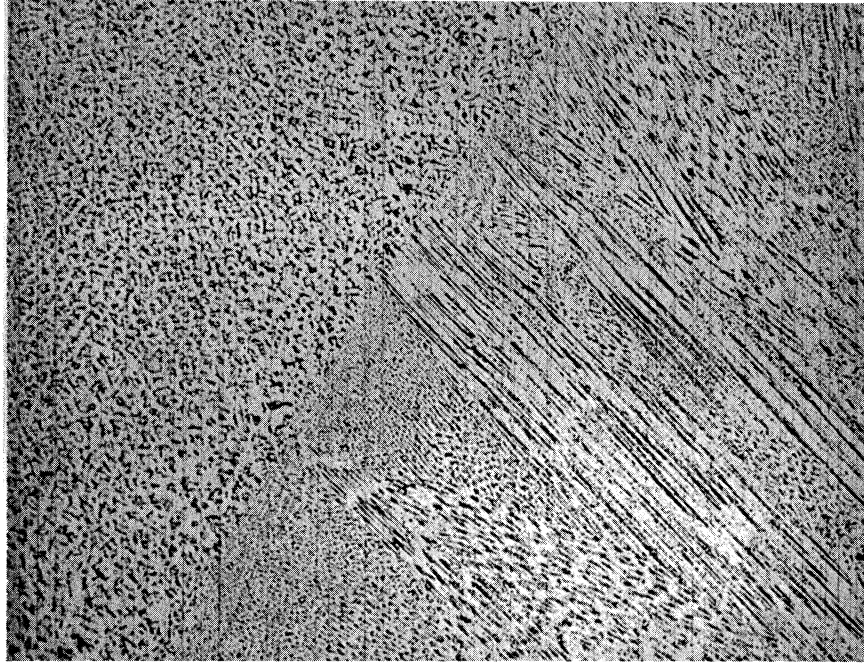


U of M No. V-1                      Weld Deposit 308 Stainless Solution  
   V-2                      Quenched 2000<sup>o</sup>F    X100 Electrolytic  
   V-3                      Etch



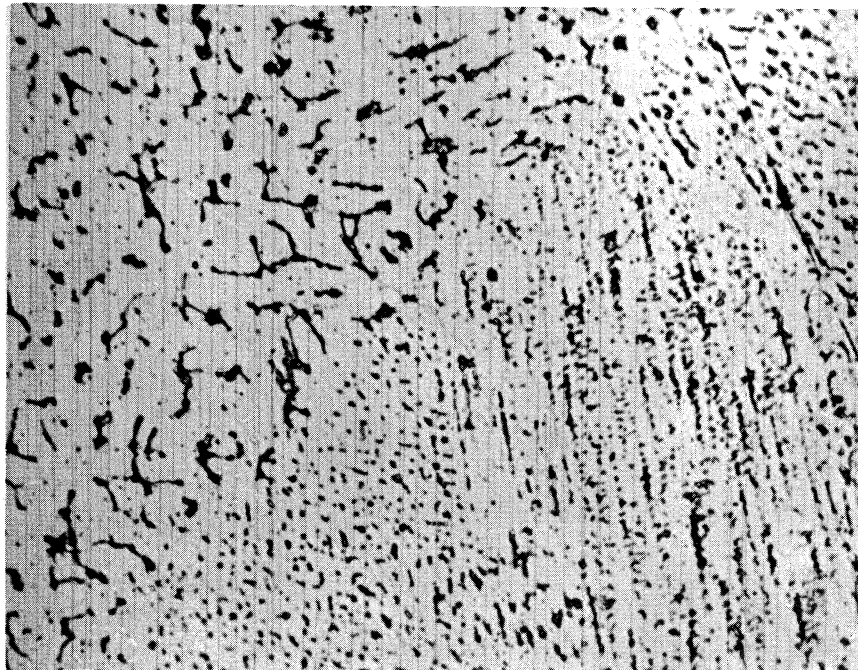
U of M No. V-1                      Weld Deposit 308 Stainless Solution  
   V-2                      Quenched 2000<sup>o</sup>F    X500 Electrolytic  
   V-3                      Etch





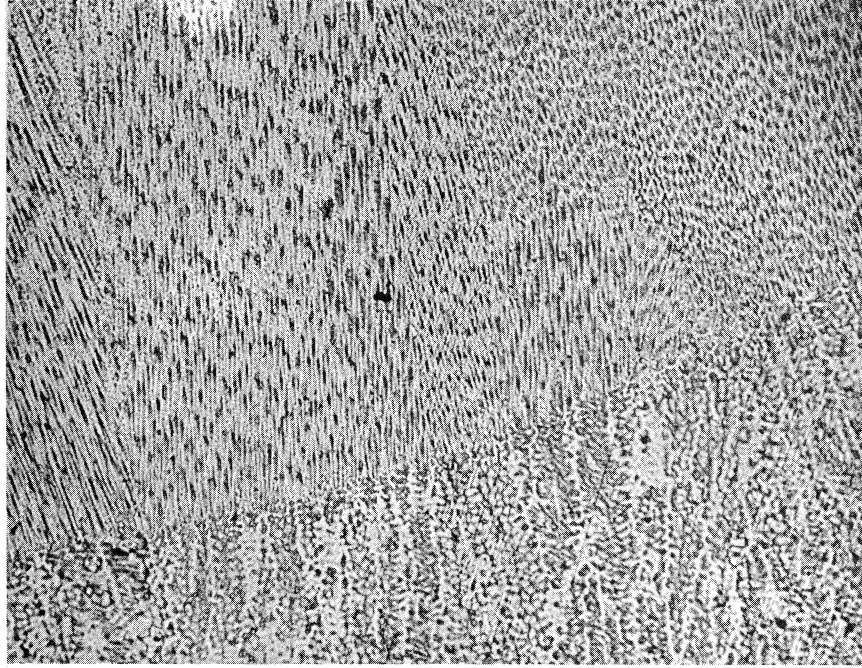
U of M No. W-1  
W-2  
W-3

Weld Deposit 308-L Stainless  
As Welded X100 Electrolytic Etch

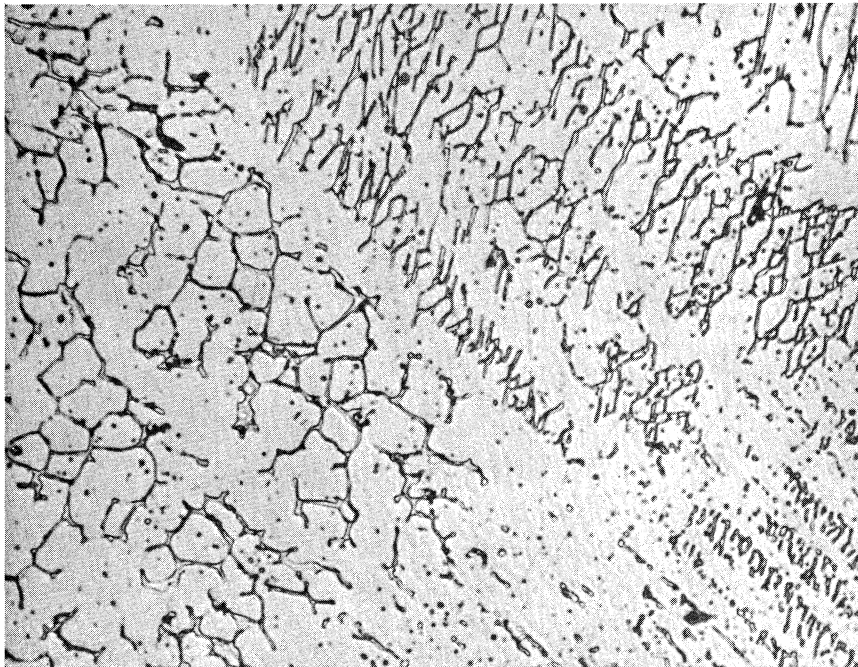


U of M No. W-1  
W-2  
W-3

Weld Deposit 308-L Stainless  
As Welded X500 Electrolytic Etch

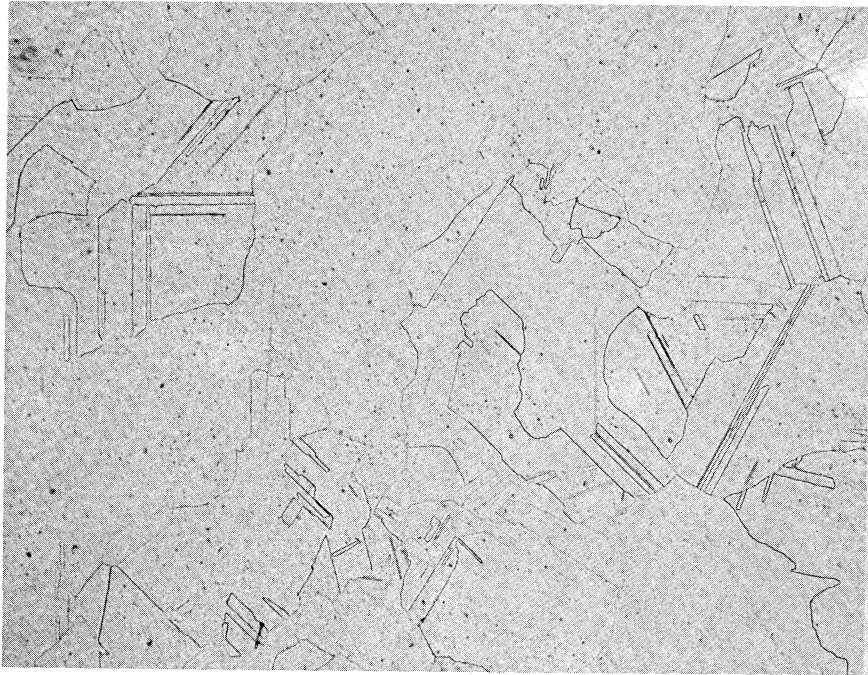


U of M No. X-1                      Weld Deposit Type 308 Stainless  
   X-2                                      As Welded X100 Electrolytic Etch  
   X-3

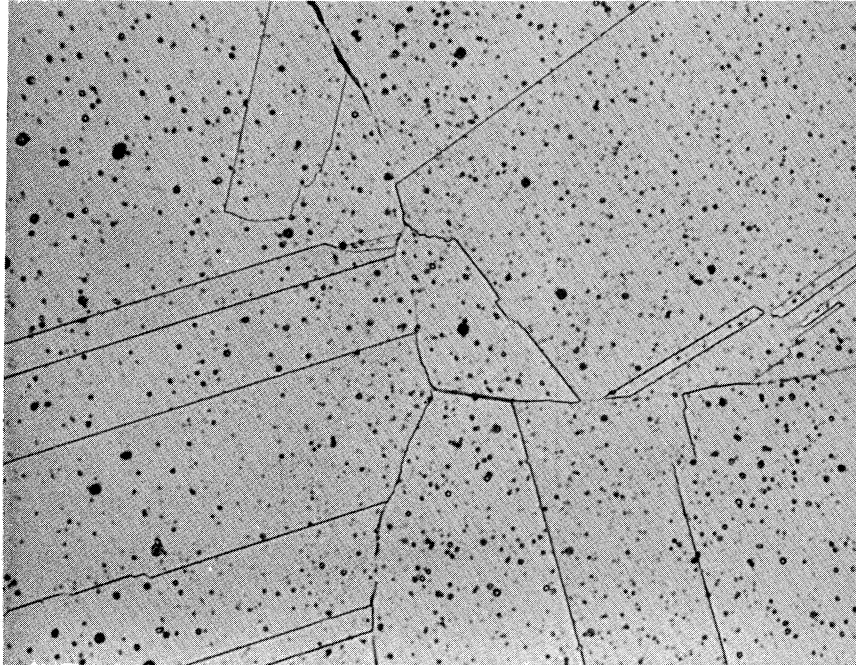


U of M No. X-1                      Weld Deposit Type 308 Stainless  
   X-2                                      As Welded X500 Electrolytic Etch  
   X-3

Figure 55. Photomicrograph of Material X-1, 2, 3

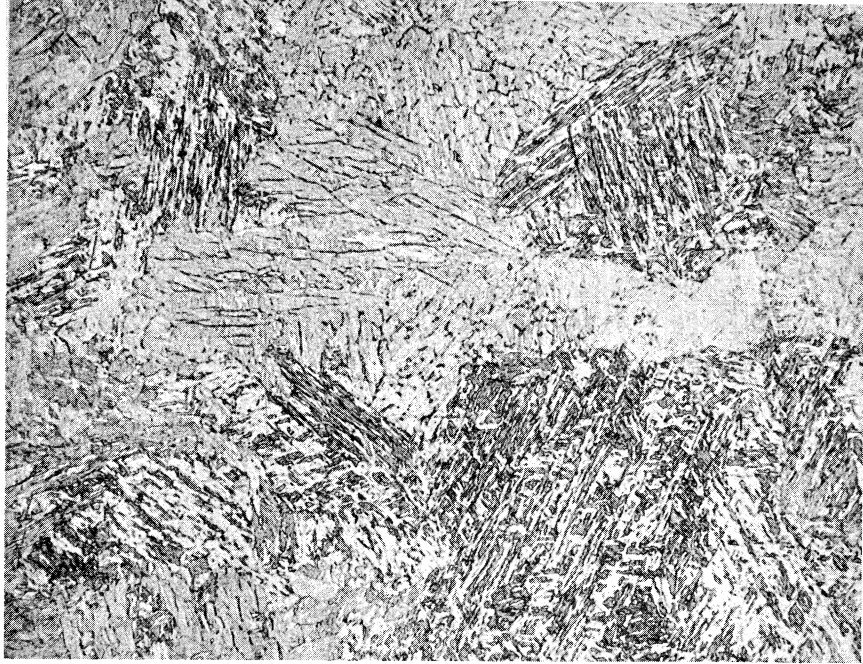


U of M No. Y-1                      Weld Deposit 308-L Stainless  
   Y-2                      Solution Quenched 2000<sup>o</sup>F X100  
   Y-3                      Electrolytic Etch



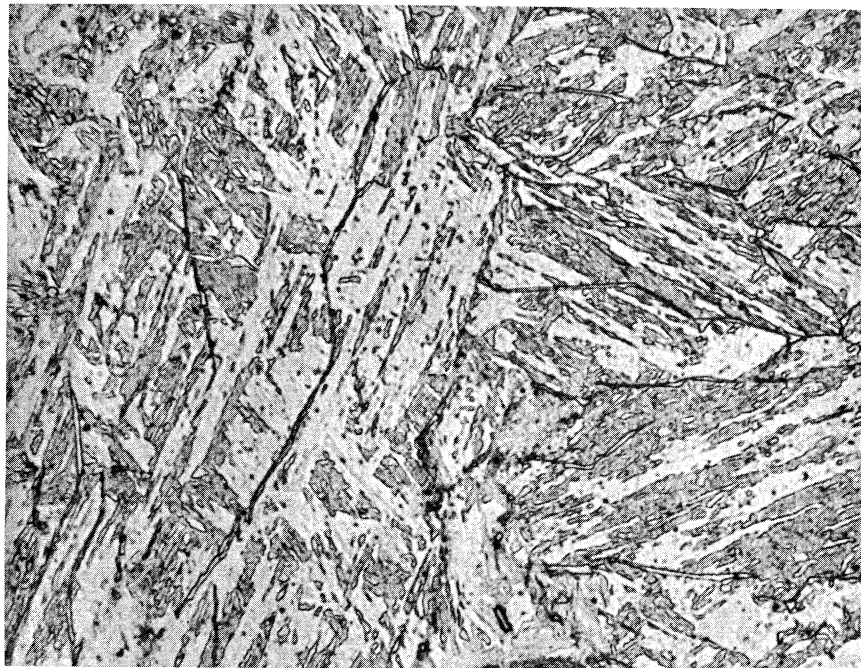
U of M No. Y-1                      Weld Deposit 308-L Stainless  
   Y-2                      Solution Quenched 2000<sup>o</sup>F X500  
   Y-3                      Electrolytic Etch





U of M No. Z<sub>1</sub>-1  
Z<sub>1</sub>-2  
Z<sub>1</sub>-3

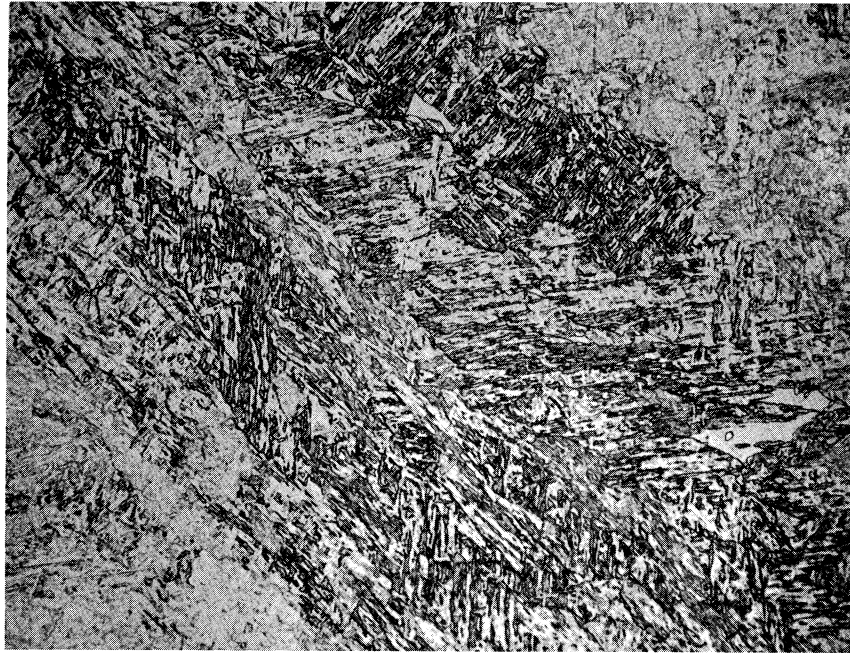
Arcos 410-15 Weld Deposit As Welded  
X100 FeCl Etch



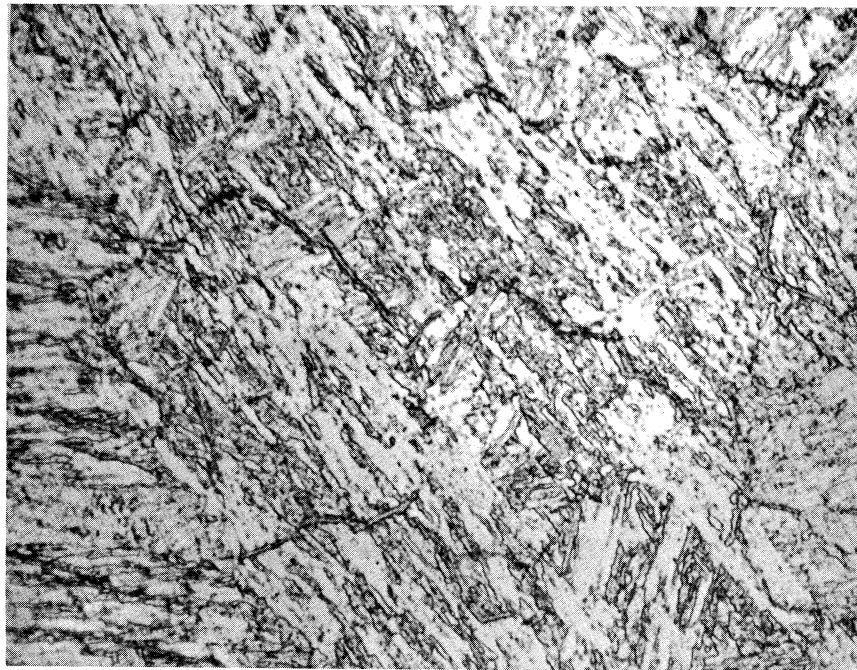
U of M No. Z<sub>1</sub>-1  
Z<sub>1</sub>-2  
Z<sub>1</sub>-3

Arcos 410-15 Weld Deposit As Welded  
X500 FeCl Etch

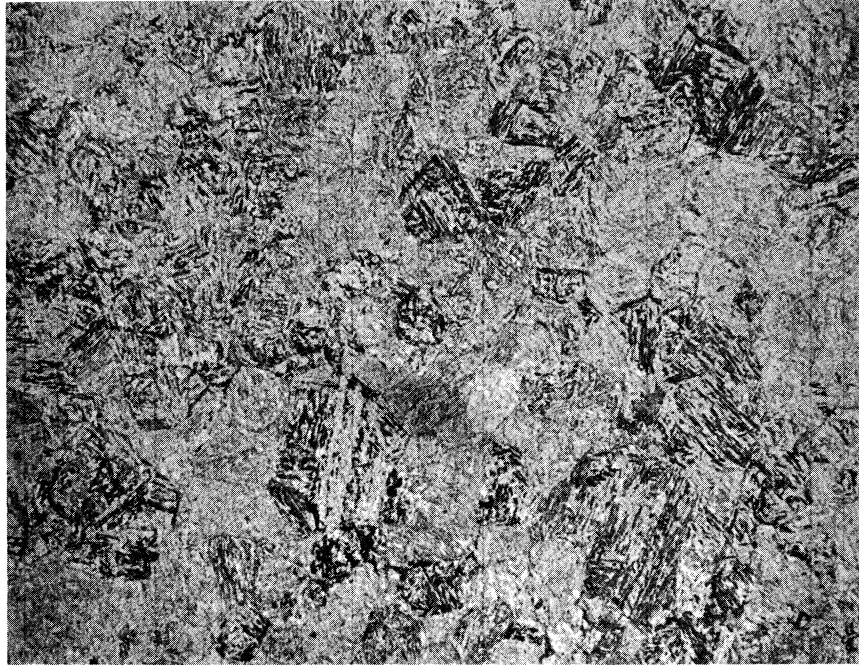
Figure 57. Photomicrograph of Material Z<sub>1</sub>-1, 2, 3



U of M No.  $Z_2$ -1      Arcos 410-15 Weld Deposit Stress  
 $Z_2$ -2      Relieved 1300<sup>o</sup>F A.C. X100 FeCl  
 $Z_2$ -3      Etch



U of M No.  $Z_2$ -1      Arcos 410-15 Weld Deposit Stress  
 $Z_2$ -2      Relieved 1300<sup>o</sup>F A.C. X500 FeCl  
 $Z_2$ -3      Etch



U of M No. A'-1  
A'-2  
A'-3

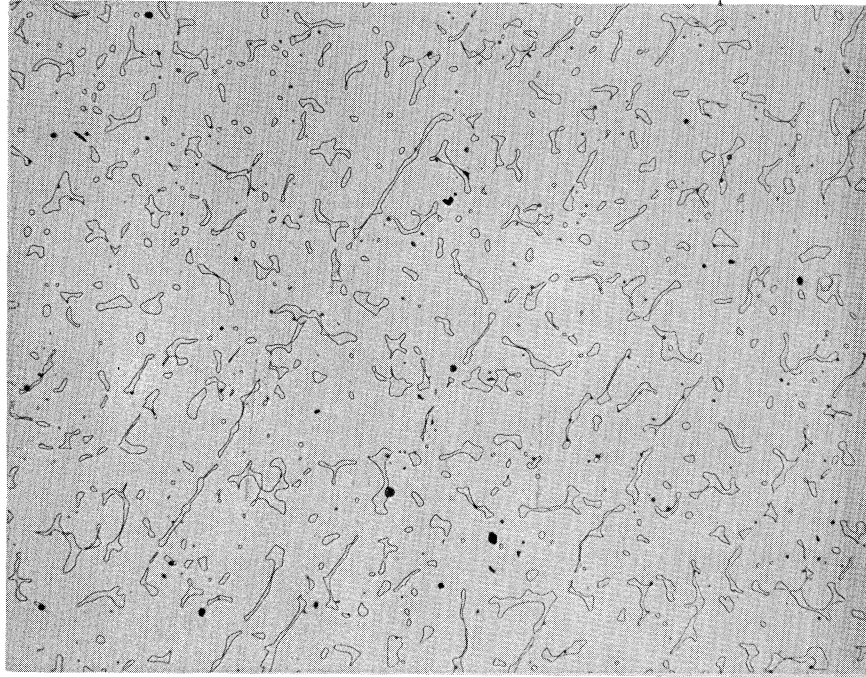
AM-355 Stainless X100 Ferric Chloride  
Etch Sample by Carpenter  
Technology Corp., Reading, Penna.



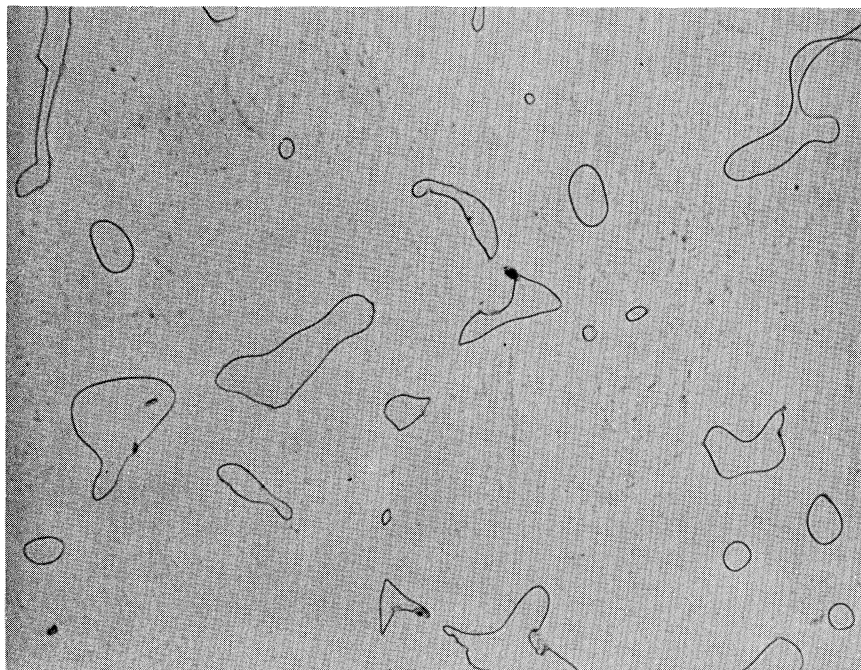
U of M No. A'-1  
A'-2  
A'-3

Am-355 Stainless X500 Ferric Chloride  
Etch Sample by Carpenter  
Technology Corp., Reading, Penna.

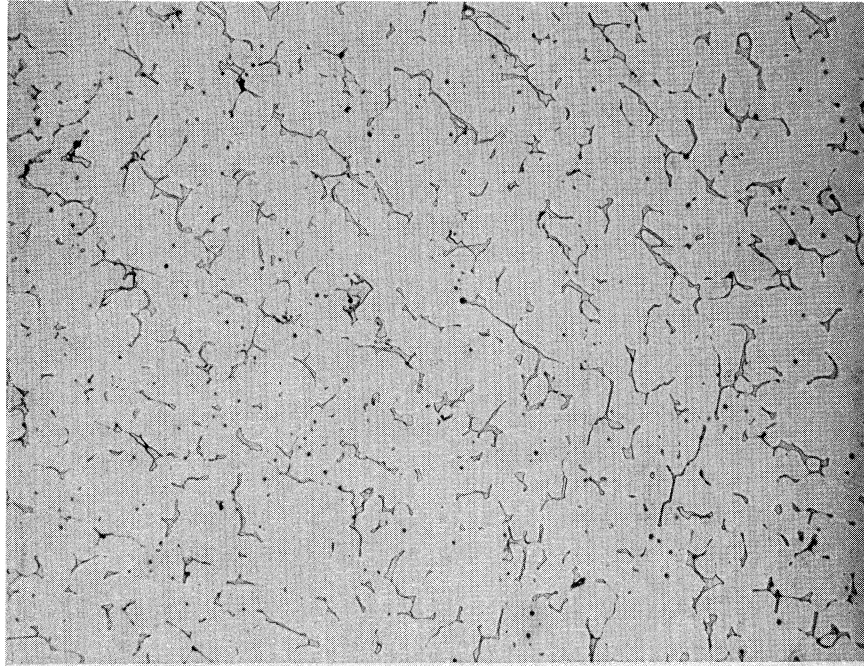




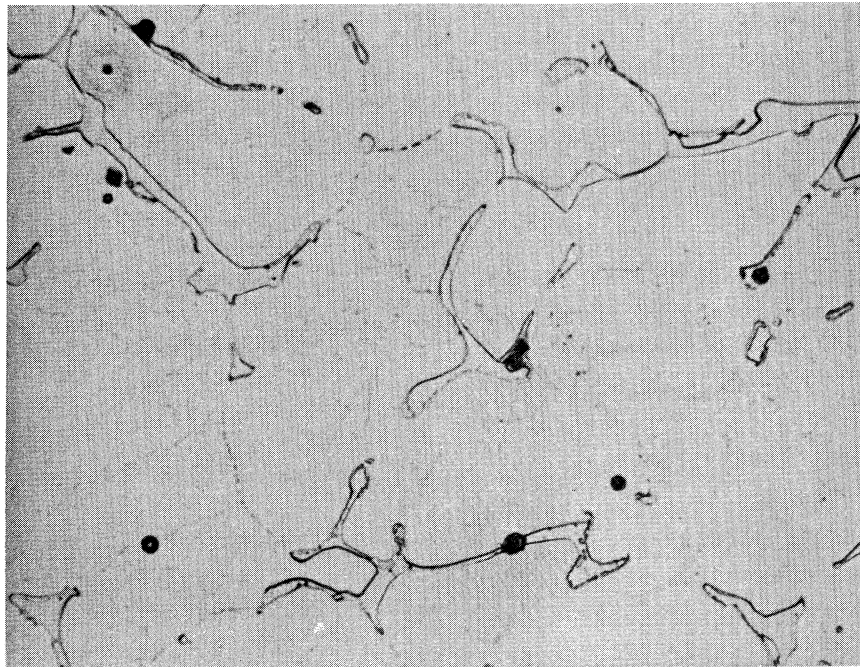
U of M No. B'-1                      CF8C Cast Stainless Steel Sol.  
                  B'-2                      Quenched 2050<sup>o</sup>F X100  
                  B'-3                      Electrolytic Etch



U of M No. B'-1                      CF8C Cast Stainless Steel Sol.  
                  B'-2                      Quenched 2050<sup>o</sup>F X500  
                  B'-3                      Electrolytic Etch



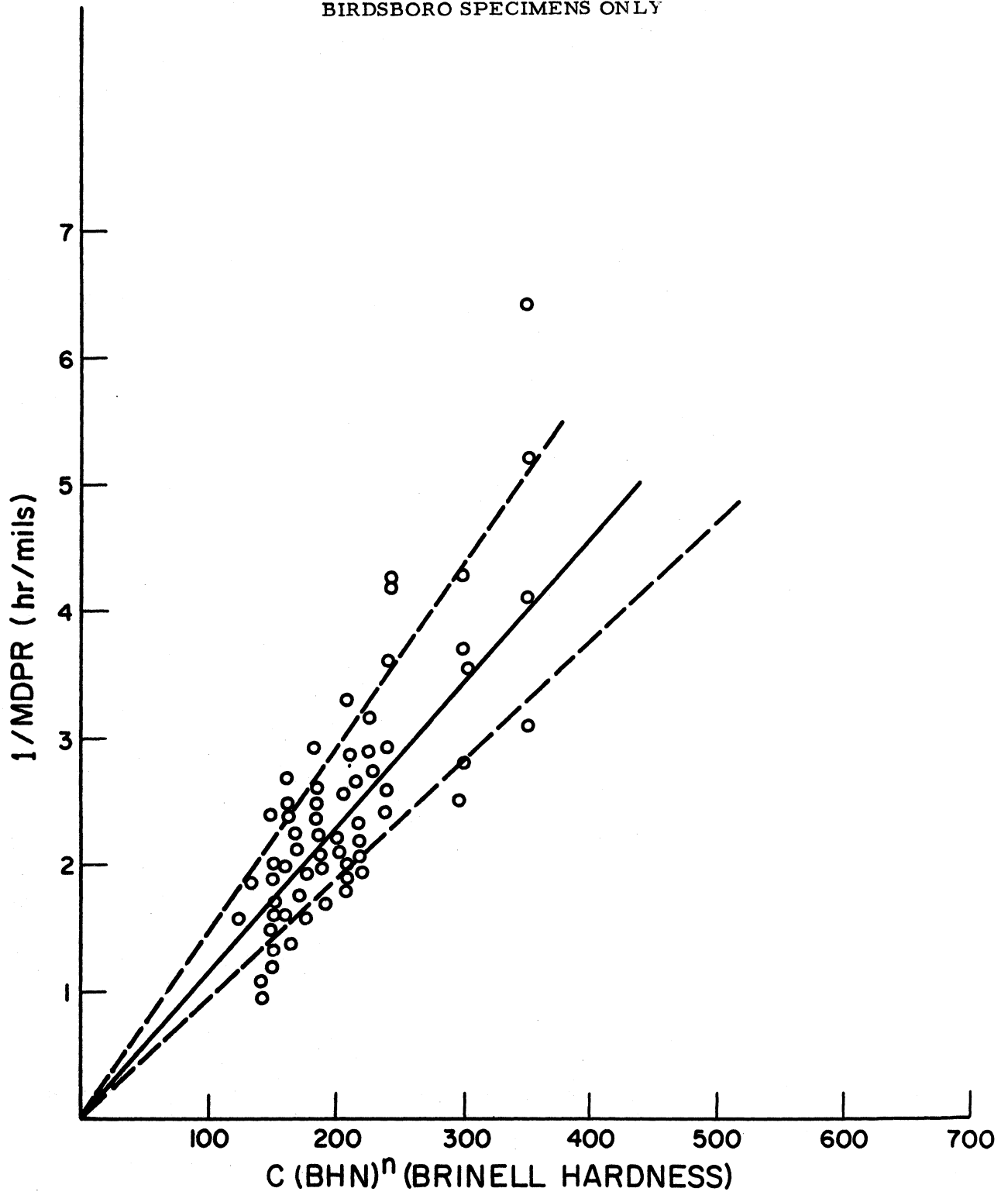
U of M No. C'-1                      CF8C Cast Stainless Steel As Cast  
   C'-2                      X100 Electrolytic Etch  
   C'-3



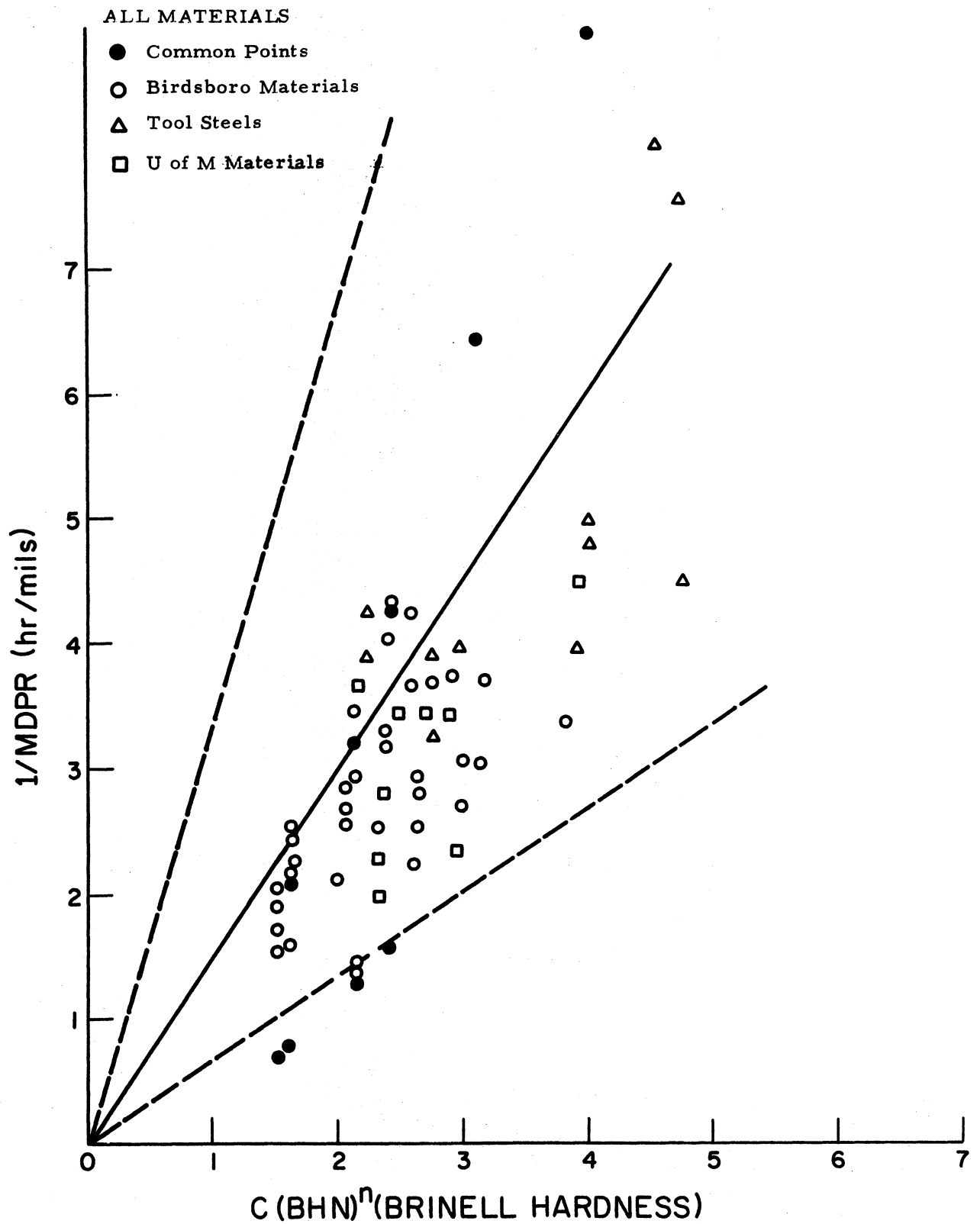
U of M No. C'-1                      CF8C Cast Stainless Steel As Cast  
   C'-2                      X500 Electrolytic Etch  
   C'-3



BIRDSBORO SPECIMENS ONLY



62. Best Fit Correlation and Standard Deviation for 98 Samples



63. Best Fit Correlation and Standard Deviation for 198 Samples









**MATERIAL DAMAGE SHEET**

<b>Material</b>
<b>Number</b> <i>E-3 Wheelhead</i>

**RUNNING CONDITIONS**

<b>Horn</b> <i>71</i>	<b>Temperature</b> <i>120</i>
<b>% Power</b> <i>40%</i>	<b>Pressure</b> <i>1.7 PSIG</i>
<b>Approx. Date</b> <i>3-21 - 3-24-70</i>	<b>Torque</b> <i>85 inch-lb</i>
<b>Prerun</b>	
<b>Surface Preparation</b> <i>polished</i>	

**BASIS FOR CALCULATIONS**

<b>Density</b>	<b>Area</b>
<b>MDP Factor</b>	

**Comments:**

DATA					
Time Interval	Cumulative Time	Weight Loss	Cumulative Weight Loss	MDP	Cumulative MDP
<i>1</i>	<i>1</i>	<i>8.50</i>	<i>8.50</i>	<i>.296</i>	<i>.296</i>
<i>1</i>	<i>2</i>	<i>10.01</i>	<i>18.51</i>	<i>.336</i>	<i>1.632</i>
<i>1</i>	<i>3</i>	<i>19.99</i>	<i>38.50</i>	<i>.672</i>	<i>1.304</i>
<i>1</i>	<i>4</i>	<i>21.75</i>	<i>60.25</i>	<i>.731</i>	<i>2.03</i>
<i>1</i>	<i>5</i>	<i>20.75</i>	<i>81.00</i>	<i>.697</i>	<i>2.73</i>
<i>1</i>	<i>6</i>	<i>17.60</i>	<i>98.60</i>	<i>.591</i>	<i>3.32</i>
<i>1</i>	<i>7</i>	<i>18.55</i>	<i>117.15</i>	<i>.623</i>	<i>3.94</i>
<i>1</i>	<i>8</i>	<i>17.10</i>	<i>134.25</i>	<i>.574</i>	<i>4.52</i>

**MATERIAL DAMAGE SHEET**

Material
Number <i>F-1</i>

**RUNNING CONDITIONS**

Horn <i>T1</i>	Temperature <i>120°</i>
% Power <i>40%</i>	Pressure <i>17.45/5</i>
Approx. Date <i>3-27-92</i>	Torque <i>85 lbs-15</i>
Prerun	
Surface Preparation <i>hand</i>	

**BASIS FOR CALCULATIONS**

Density	Area
MDP Factor	

Comments:

**DATA**

Time Interval	Cumulative Time	Weight Loss	Cumulative Weight Loss	MDP	Cumulative MDP
<i>1</i>	<i>1</i>	<i>8.60</i>	<i>8.60</i>	<i>.289</i>	<i>.289</i>
<i>1</i>	<i>2</i>	<i>22.30</i>	<i>30.90</i>	<i>.749</i>	<i>1.04</i>
<i>1</i>	<i>3</i>	<i>28.60</i>	<i>54.50</i>	<i>.793</i>	<i>1.83</i>
<i>1</i>	<i>4</i>	<i>23.63</i>	<i>78.13</i>	<i>.796</i>	<i>2.63</i>
<i>1</i>	<i>5</i>	<i>28.49</i>	<i>101.67</i>	<i>.789</i>	<i>3.42</i>
<i>1</i>	<i>6</i>	<i>22.91</i>	<i>124.58</i>	<i>.770</i>	<i>4.18</i>
<i>1</i>	<i>7</i>	<i>19.06</i>	<i>142.64</i>	<i>.607</i>	<i>4.79</i>
<i>1</i>	<i>8</i>	<i>18.46</i>	<i>161.10</i>	<i>.620</i>	<i>5.41</i>
<i>1</i>	<i>9</i>	<i>19.90</i>	<i>180.40</i>	<i>.648</i>	<i>6.06</i>







**MATERIAL DAMAGE SHEET**

<b>Material</b>	
<b>Number</b>	G-2.

**RUNNING CONDITIONS**

<b>Horn</b>	71	<b>Temperature</b>	120°
<b>% Power</b>	10%	<b>Pressure</b>	17 PSIG
<b>Approx. Date</b>	3.26 - 3.28.70	<b>Torque</b>	35 inch-lb.
<b>Prerun</b>			
<b>Surface Preparation</b>			

**BASIS FOR CALCULATIONS**

<b>Density</b>	<b>Area</b>
<b>MDP Factor</b>	

Comments:

**DATA**

Time Interval	Cumulative Time	Weight Loss	Cumulative Weight Loss	MDP	Cumulative MDP
1	1	25.90	25.90	.857	.857
1	2	45.4	71.04	1.49	2.35
1	3	37.56	108.60	1.24	3.59
1	4	30.60	139.20	1.01	4.61
1	5	33.23	172.23	1.09	5.70
1	6	26.97	199.20	.893	6.59
1	7	21.31	220.51	.705	7.30
1	8	20.13	240.40	.668	7.97
1	9	19.34	260.64	.660	8.63
1	10	18.90	279.54	.625	9.25

















**MATERIAL DAMAGE SHEET**

<b>Material</b>
<b>Number</b> 7-1 Birdsloro

**RUNNING CONDITIONS**

<b>Horn</b> 11	<b>Temperature</b> 120°
<b>% Power</b> 40% - 43%	<b>Pressure</b> 17 PSIG
<b>Approx. Date</b> 3-13 - 3-17-70	<b>Torque</b>
<b>Prerun</b>	
<b>Surface Preparation</b> Polished	

**BASIS FOR CALCULATIONS**

<b>Density</b>	<b>Area</b>
<b>MDP Factor</b>	

Comments:

**DATA**

Time Interval	Cumulative Time	Weight Loss	Cumulative Weight Loss	MDP	Cumulative MDP
1hr	1hr	5.41	5.41		
1	2	13.89	19.30		
1	3	17.00	36.30		
1	4	15.80	52.10		
1	5	14.83	66.93		
1	6	13.82	80.75		
1	7	14.25	95.00		
1	8	20.20	115.20		
1	9	14.80	130.00		
1	10	13.75	143.75		
1	11	12.90	156.65		







































































































































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