

On Stokes' Problem for a Non-Newtonian Fluid

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1. Introduction

The fluids of the differential type (cf. Truesdell and Noll [1]) are amongst the many models which have been employed to describe the non-Newtonian behavior exhibited by certain fluids. In this note we extend the work of Stokes [2] on the flow due to an oscillating plate for a special subclass of the fluids of the differential type, namely the incompressible fluids of grade three. The stress \mathbf{T} in such fluids is related to the fluid motion in the following manner (cf. Truesdell and Noll [1]):

$$\begin{aligned} \mathbf{T} = & -p\mathbf{1} + \mu\mathbf{A}_1 + \alpha_1\mathbf{A}_2 + \alpha_2\mathbf{A}_1^2 + \beta_1\mathbf{A}_3 \\ & + \beta_2[\mathbf{A}_1\mathbf{A}_2 + \mathbf{A}_2\mathbf{A}_1] + \beta_3(\text{tr } \mathbf{A}_1^2) \mathbf{A}_1, \end{aligned} \quad (1)^1$$

where μ is the viscosity, α_1 and α_2 are material moduli which are usually referred to as the normal stress moduli, p is the pressure and the kinematical tensors \mathbf{A}_1 , and \mathbf{A}_2 and \mathbf{A}_3 are defined recursively through

$$\mathbf{A}_1 = \text{grad } \mathbf{v} + (\text{grad } \mathbf{v})^T, \quad (2.1)$$

and

$$\mathbf{A}_n = \frac{d}{dt} (\mathbf{A}_{n-1}) + \mathbf{A}_{n-1}(\text{grad } \mathbf{v}) + (\text{grad } \mathbf{v})^T \mathbf{A}_1. \quad (2.2)$$

In the above equations, \mathbf{v} denotes the velocity and $\frac{d}{dt}$ the material time derivative.

2. Equation of Motion

We are interested in the flow of a fluid modeled by (1) over an infinite flat plate which is either accelerating or oscillating. Thus, we seek a solution for the

¹ Fosdick and Rajagopal [3] have studied the thermodynamics of fluids modeled exactly by (1) in detail. They show that the assumption that all motions of the fluid obey the Clausius-Duhem inequality and the requirement that the specific Helmholtz free energy be a minimum when the fluid is locally at rest imply that

$$\mu \geq 0, \quad \alpha_1 \geq 0, \quad |\alpha_1 + \alpha_2| \leq \sqrt{24\mu\beta_3}, \quad \beta_1 = \beta_2 = 0 \quad \text{and} \quad \beta_3 \geq 0.$$

In this note, in addition to studying the problem for the above range of material parameters, we also study the problem when $\alpha_1 < 0$, and $\beta_2 \neq 0$.

velocity field of the form:

$$\mathbf{v} = u(y, t) \mathbf{i}, \quad (3)$$

where u is the velocity in the x -coordinate direction and \mathbf{i} is the unit vector in the x -direction.

Substituting (1) into the balance of linear momentum

$$\operatorname{div} \mathbf{T} + \rho \mathbf{b} = \rho \frac{d\mathbf{v}}{dt},$$

and using (3) and the fact that the fluid is incompressible, we obtain (when $\beta_1 = 0$)

$$\mu \frac{\partial^2 u}{\partial y^2} + \alpha_1 \frac{\partial^3 u}{\partial y^2 \partial t} + 6(\beta_2 + \beta_3) \left(\frac{\partial u}{\partial y} \right)^2 \frac{\partial^2 u}{\partial y^2} - \rho \frac{\partial u}{\partial t} = \frac{\partial p}{\partial x}. \quad (4.1)$$

$$\frac{\partial}{\partial y} \left[(2\alpha_1 + \alpha_2) \left(\frac{\partial u}{\partial y} \right)^2 + 2\beta_2 \frac{\partial u}{\partial y} \frac{\partial^2 u}{\partial y \partial t} \right] = \frac{\partial p}{\partial y}, \quad (4.2)$$

$$0 = \frac{\partial p}{\partial z}. \quad (4.3)$$

For the problem in question the boundary conditions are

$$u(0, t) = U(t),$$

$$u \rightarrow 0 \quad \text{as} \quad y \rightarrow \infty.$$

Defining a modified pressure \check{p} through

$$\check{p} = p - \left[(2\alpha_1 + \alpha_2) \left(\frac{\partial u}{\partial y} \right)^2 + 2\beta_2 \frac{\partial u}{\partial y} \frac{\partial^2 u}{\partial y \partial t} \right],$$

we can rewrite Eqs. (4) as

$$\mu \frac{\partial^2 u}{\partial y^2} + \alpha_1 \frac{\partial^3 u}{\partial y^2 \partial t} + 6(\beta_2 + \beta_3) \left(\frac{\partial u}{\partial y} \right)^2 \frac{\partial^2 u}{\partial y^2} - \rho \frac{\partial u}{\partial t} = \frac{\partial \check{p}}{\partial x}, \quad (5.1)$$

$$0 = \frac{\partial \check{p}}{\partial y} = \frac{\partial \check{p}}{\partial z}. \quad (5.2,3)$$

Equations (5.1, 2, 3) imply that $\frac{\partial \check{p}}{\partial x}$ is at most a function of time. The conditions at $y \rightarrow \infty$ imply $\frac{\partial \check{p}}{\partial x} = 0$ and, hence,

$$\mu \frac{\partial^2 u}{\partial y^2} + \alpha_1 \frac{\partial^3 u}{\partial y^2 \partial t} + 6(\beta_2 + \beta_3) \left(\frac{\partial u}{\partial y} \right)^2 \frac{\partial^2 u}{\partial y^2} - \rho \frac{\partial u}{\partial t} = 0. \quad (6)$$

The above equation can be re-written in the following dimensionless form

$$\frac{\partial \bar{u}}{\partial \bar{t}} = \frac{\partial^2 \bar{u}}{\partial \bar{y}^2} + \bar{\alpha}_1 \frac{\partial^3 \bar{u}}{\partial \bar{y}^2 \partial \bar{t}} + \varepsilon \left(\frac{\partial \bar{u}}{\partial \bar{y}} \right)^2 \left(\frac{\partial^2 \bar{u}}{\partial \bar{y}^2} \right), \quad (7)$$

where U_0 is a reference velocity

$$\bar{\alpha}_1 = \frac{\alpha_1 U_0^2}{\rho \nu^2}, \quad \varepsilon = \frac{6(\beta_2 + \beta_3)}{\rho \nu^2}$$

and

$$\bar{u} = \frac{u}{U_0}, \quad \bar{t} = \frac{U_0^2 t}{\nu} \quad \text{and} \quad \bar{y} = \frac{U_0 y}{\nu}.$$

The appropriate boundary conditions are

$$\bar{u} = \bar{U}(t) \quad \text{at} \quad t = 0,$$

$$\bar{u} \rightarrow 0 \quad \text{as} \quad \bar{y} \rightarrow \infty.$$

Let us suppose the non-dimensional velocity \bar{u} can be expanded in power series in ε :

$$\bar{u}(t, y; \varepsilon) = \bar{u}_0(t, y) + \varepsilon \bar{u}_1(t, y) + \varepsilon^2 \bar{u}_2(t, y) + \dots \tag{8}$$

On substituting the expansion (8) for \bar{u} and equating like powers of ε , we obtain the following equations at zeroth and first powers, respectively.

$$\frac{\partial \bar{u}_0}{\partial \bar{t}} = \frac{\partial^2 \bar{u}_0}{\partial \bar{y}^2} + \alpha_1 \frac{\partial^3 \bar{u}_0}{\partial \bar{y}^2 \partial \bar{t}} \tag{9}$$

$$\bar{u}_0 = \bar{U}(t) \quad \text{at} \quad \bar{y} = 0, \tag{10.1}$$

$$\bar{u}_0 \rightarrow 0 \quad \text{as} \quad \bar{y} \rightarrow \infty, \tag{10.2}$$

and

$$\frac{\partial \bar{u}_1}{\partial \bar{t}} = \frac{\partial^2 \bar{u}_1}{\partial \bar{y}^2} + \alpha_1 \frac{\partial^3 \bar{u}_1}{\partial \bar{y}^2 \partial \bar{t}} + \left(\frac{\partial \bar{u}_0}{\partial \bar{y}} \right)^2 \left(\frac{\partial^2 \bar{u}_0}{\partial \bar{y}^2} \right), \tag{11}$$

$$\bar{u}_1 = 0 \quad \text{at} \quad \bar{y} = 0, \tag{12.1}$$

$$\bar{u}_1 \rightarrow 0 \quad \text{as} \quad \bar{y} \rightarrow \infty. \tag{12.2}$$

Introducing the similarity transformation

$$\eta = \bar{y}, \quad f_0(\eta) = \frac{\bar{u}_0}{e^{\gamma t}}, \quad f_1(\eta) = \frac{\bar{u}_1}{e^{3\gamma t}}, \tag{13}$$

we can re-write Eqs. (9) and (10) in the following manner:

$$(1 + \gamma \bar{\alpha}_1) f_0'' - \gamma f_0 = 0, \tag{14}$$

$$f_0(0) = 1, \tag{15.1}$$

$$f_0(\eta) \rightarrow 0 \quad \text{as} \quad \eta \rightarrow \infty, \tag{15.2}$$

where

$$\bar{U}(t) = e^{\gamma t}.$$

Also, Eqs. (11) and (12) can be written as

$$(1 + 3\gamma\bar{\alpha}_1) f_1'' - 3\gamma f_1 = -(f_0')^2 f_0'', \tag{16}$$

$$f_1(0) = 0, \tag{17.1}$$

$$f_1(\eta) \rightarrow 0 \text{ as } \eta \rightarrow \infty. \tag{17.2}$$

It is straightforward to verify that the solutions to (14)–(15) and (16)–(17) are, respectively

$$f_0(\eta) = \exp \left\{ -\sqrt{\frac{\gamma}{1 + \gamma\bar{\alpha}_1}} \eta \right\}, \tag{18}$$

and

$$f_1(\eta) = \frac{\gamma}{6(1 + \gamma\bar{\alpha}_1)(1 + 4\gamma\bar{\alpha}_1)} \left\{ \exp \left(-\sqrt{\frac{3\gamma}{1 + 3\gamma\bar{\alpha}_1}} \eta \right) - \exp \left(-3\sqrt{\frac{\gamma}{1 + \gamma\bar{\alpha}_1}} \eta \right) \right\}. \tag{19}$$

Since γ may be both real or imaginary, both cases are considered.

Case 1: γ is real

In this case Eq. (8) yields

$$\bar{u}(y, t; \varepsilon) = e^{\nu t} f_0(\eta) + \varepsilon e^{3\nu t} f_1(\eta) + \dots \tag{20}$$

The numerical values of $f_0(\eta)$ and $f_1(\eta)$, for various values of γ and $\bar{\alpha}_1$ are provided in Table 1. Thus, one can obtain the numerical value of \bar{u} for various values of ε . Of course, when $\varepsilon = 0$, (18) implies that there is an exact solution for the problem.

The skin friction on the plate τ_w for the problem is given by

$$\tau_w = \rho U_0^2 \{ e^{\nu t} f_0'(0) + \varepsilon e^{3\nu t} f_1'(0) + \dots \}. \tag{21}$$

It follows from (18) and (19) that

$$f_0'(\eta) = -\sqrt{\frac{\gamma}{1 + \gamma\bar{\alpha}_1}} f_0(\eta), \tag{22}$$

and

$$f_1'(\eta) = \frac{\gamma}{6(1 + \gamma\bar{\alpha}_1)(1 + 4\gamma\bar{\alpha}_1)} \left\{ 3\sqrt{\frac{\gamma}{1 + \gamma\bar{\alpha}_1}} \exp \left(-3\sqrt{\frac{\gamma}{1 + \gamma\bar{\alpha}_1}} \eta \right) - \sqrt{\frac{3\gamma}{1 + 3\gamma\bar{\alpha}_1}} \exp \left(-\sqrt{\frac{3\gamma}{1 + 3\gamma\bar{\alpha}_1}} \eta \right) \right\}. \tag{23}$$

The numerical values of $f_0'(\eta)$ and $f_1'(\eta)$ for values of γ and $\bar{\alpha}_1$, are provided in Table 1.

Case 2: γ is imaginary

In the case of an oscillating plate, i.e., when γ is imaginary, say $\gamma = i\omega$, a straightforward computation verifies

$$\bar{u}(\bar{i}, \bar{y}; \varepsilon) = \{ f_{0R} \cos \omega \bar{t} - f_{0I} \sin \omega \bar{t} \} + \varepsilon \{ f_{1R} \cos 3\omega \bar{t} - f_{1I} \sin 3\omega \bar{t} \} + \dots, \tag{24}$$

where

$$f_{0R} = e^{-\delta_R \eta} \cos \delta_I \eta \tag{25}$$

Table 1

	η	$f_0(\eta)$	$f_0'(\eta)$	$f_1(\eta)$	$f_1'(\eta)$
$\bar{\alpha}_1 = -4$ $\gamma = .5$	0.0	1.0	-0.79056942	0.0	-0.22667550
	0.5	0.67348836	-0.53243930	0.0386788	-0.00565536
	1.0	0.45358657	-0.35859167	0.02650408	-0.03017132
	2.0	0.20574078	-0.16265237	0.01367445	-0.01021715
	4.0	0.04232927	-0.03346422	0.00018575	-0.00034251
	6.0	0.00870086	-0.00688496	0.00000434	-0.00000826
	10.0	0.00036864	-0.00029144	0.00000000	-0.00000000
	15.0	0.00000708	-0.00000560	0.00000000	-0.00000000
	20.0	0.00000014	-0.00000011	0.00000000	-0.00000000
$\bar{\alpha}_1 = -2$ $\gamma = .5$	0.0	1.0	-0.74535599	0.0	-0.11916942
	0.5	0.68888711	-0.51346614	0.02377473	+0.00415646
	1.0	0.47456545	-0.35372021	0.01920771	-0.01538062
	2.0	0.22521237	-0.24367329	0.01177957	-0.01307965
	4.0	0.05072061	-0.03780491	0.00042190	-0.00060205
	6.0	0.01142291	-0.00851413	0.00002343	-0.00003412
	10.0	0.00057938	-0.00043184	0.00000007	-0.00000010
	15.0	0.00001395	-0.00001039	0.00000000	-0.00000000
	20.0	0.00000034	-0.00000025	0.00000000	-0.00000000
$\bar{\alpha}_1 = 2$ $\gamma = .5$	0.0	1.0	-0.67419986	0.0	-0.05132182
	0.5	0.71383759	-0.48126920	0.01194280	-0.00583949
	1.0	0.50956410	-0.34354805	0.01132410	-0.00537358
	2.0	0.25965557	-0.17505975	0.00536640	-0.00486598
	4.0	0.06742102	-0.04545524	0.00072008	-0.00045028
	6.0	0.01750624	-0.01180271	0.00008566	-0.00009174
	10.0	0.00118029	-0.00079575	0.00000117	-0.00000126
	15.0	0.00004055	-0.00002734	0.00000001	-0.00000001
	20.0	0.00000139	-0.00000094	0.00000000	-0.00000000

and

$$f_{0I} = -e^{-\delta_R \eta} \sin \delta_I \eta \tag{26}$$

are the real and imaginary parts of f_0 . Also,

$$f_{1R} = -\{A_R \cos m_I \eta + A_I \sin m_I \eta\} e^{-m_R \eta} + \{A_R \cos 3\delta_I \eta + A_I \sin 3\delta_I \eta\} e^{-3\gamma_R \eta}, \tag{27}$$

and

$$f_{1I} = -\{A_I \cos m_I \eta - A_R \sin m_I \eta\} e^{-m_R \eta} + \{A_I \cos 3\delta_I \eta - A_R \sin 3\delta_I \eta\} e^{-3\delta_R \eta}, \tag{28}$$

where f_{1R} and f_{1I} are the real and imaginary parts of f_1 , respectively. In the above equations

$$\delta_R = \left\{ \frac{a_1 + (a_1^2 + a_2^2)^{1/2}}{2} \right\}^{1/2}, \quad \delta_I = \frac{a_2}{\{2[a_1 + (a_1^2 + a_2^2)^{1/2}]\}^{1/2}}, \tag{29.1, 2}$$

$$m_R = \left\{ \frac{b_1 + (b_1^2 + b_2^2)^{1/2}}{2} \right\}^{1/2}, \quad m_I = \frac{b_2}{\{2[b_1 + (b_1^2 + b_2^2)^{1/2}]\}^{1/2}}, \tag{30.1, 2}$$

Table 2

η	$\Omega t = 1.5708$				$\Omega t = 3.1416$				$\Omega t = 6.2832$			
	$w_0(\eta)$	$w_1(\eta)$	$w_2(\eta)$	$w_3(\eta)$	$w_0(\eta)$	$w_1(\eta)$	$w_2(\eta)$	$w_3(\eta)$	$w_0(\eta)$	$w_1(\eta)$	$w_2(\eta)$	$w_3(\eta)$
$\bar{\alpha}_1 = -2$												
0.0	1.0	0.0	0.0	0.0	1.0	0.0	0.0	0.0	1.0	0.0	0.0	0.0
1.0	0.31116009	0.04315088	0.04315088	0.04315088	-0.53961863	-0.00164945	-0.00164945	-0.00164945	0.53962081	0.0164855	0.0164855	0.0164855
2.0	0.33581557	0.01102422	0.01102422	0.01102422	-0.19436649	-0.02819471	-0.02819471	-0.02819471	0.19436885	0.02819448	0.02819448	0.02819448
4.0	0.13054154	-0.00788366	-0.00788366	-0.00788366	0.07499422	0.00150078	0.00150078	0.00150078	-0.07499330	-0.00150061	-0.00150061	-0.00150061
6.0	0.00018816	0.00102598	0.00102598	0.00102598	0.05841424	0.00154834	0.00154834	0.00154834	-0.05841424	-0.00154836	-0.00154836	-0.00154836
10.0	-0.00763958	-0.00010041	-0.00010041	-0.00010041	-0.00435619	-0.00002961	-0.00002961	-0.00002961	0.00435614	0.00002961	0.00002961	0.00002961
15.0	0.00082469	0.00000055	0.00000055	0.00000055	-0.00000664	-0.00000287	-0.00000287	-0.00000287	0.00000665	0.00000287	0.00000287	0.00000287
20.0	-0.00006656	0.00000008	0.00000008	0.00000008	0.00003939	0.0000001	0.0000001	0.0000001	-0.00003939	-0.0000001	-0.0000001	-0.0000001
$\bar{\alpha}_1 = -4$												
0.0	1.0	0.0	0.0	0.0	1.0	0.0	0.0	0.0	1.0	0.0	0.0	0.0
1.0	0.33067138	-0.13878299	-0.13878299	-0.13878299	-0.54967557	-0.04245936	-0.04245936	-0.04245936	0.54967789	0.04246227	0.04246227	0.04246227
2.0	0.36352387	-0.07321561	-0.07321561	-0.07321561	-0.19279840	-0.09002350	-0.09002350	-0.09002350	0.19280094	-0.09002197	-0.09002197	-0.09002197
4.0	0.14017238	0.04087078	0.04087078	0.04087078	0.09497887	0.00368240	0.00368240	0.00368240	-0.09497789	-0.00368326	-0.00368326	-0.00368326
6.0	-0.00750268	0.00439193	0.00439193	0.00439193	0.06926775	-0.01226276	-0.01226276	-0.01226276	0.06926781	0.01226285	0.01226285	0.01226285
10.0	-0.00899680	0.00125829	0.00125829	0.00125829	-0.00763067	0.00057150	0.00057150	0.00057150	0.00763061	-0.00057152	-0.00057152	-0.00057152
15.0	0.00123499	-0.00001708	-0.00001708	-0.00001708	0.00034144	0.00008281	0.00008281	0.00008281	-0.00034143	-0.00008281	-0.00008281	-0.00008281
20.0	-0.00013730	-0.00000517	-0.00000517	-0.00000517	0.00002271	0.00000010	0.00000010	0.00000010	-0.00002272	-0.00000010	-0.00000010	-0.00000010
$\bar{\alpha}_1 = 2$												
0.0	1.0	0.0	0.0	0.0	1.0	0.0	0.0	0.0	1.0	0.0	0.0	0.0
1.0	0.27020173	0.02785002	0.02785002	0.02785002	-0.52753049	-0.02130391	-0.02130391	-0.02130391	0.52753238	0.02130333	0.02130333	0.02130333
2.0	0.28507951	-0.00082394	-0.00082394	-0.00082394	-0.20527844	-0.01952763	-0.01952763	-0.01952763	0.20528044	0.01952765	0.01952765	0.01952765
4.0	0.11705065	-0.00305878	-0.00305878	-0.00305878	0.03913149	0.00054134	0.00054134	0.00054134	-0.03913068	-0.00054128	-0.00054128	-0.00054128
6.0	0.01286996	0.00003569	0.00003569	0.00003569	0.04139879	0.00042337	0.00042337	0.00042337	-0.04139870	-0.00042237	-0.00042237	-0.00042237
10.0	0.00534897	0.00000194	0.00000194	0.00000194	-0.00011371	-0.00000871	-0.00000871	-0.00000871	0.00011367	0.00000871	0.00000871	0.00000871
15.0	0.00028540	0.00000002	0.00000002	0.00000002	-0.00026776	0.00000007	0.00000007	0.00000007	0.00026776	-0.00000007	-0.00000007	-0.00000007
20.0	-0.00000122	-0.00000000	-0.00000000	-0.00000000	0.00002860	-0.00000000	-0.00000000	-0.00000000	-0.00002860	0.00000000	0.00000000	0.00000000

with

$$a_1 = \frac{\bar{\alpha}_1 \omega^2}{1 + \bar{\alpha}_1^2 \omega^2}, \quad a_2 = \frac{\omega}{1 + \bar{\alpha}_1^2 \omega^2}, \quad (31.1, 2)$$

$$b_1 = \frac{9\bar{\alpha}_1 \omega^2}{1 + 9\bar{\alpha}_1^2 \omega^2}, \quad b_2 = \frac{3\omega}{1 + 9\bar{\alpha}_1^2 \omega^2}, \quad (32.1, 2)$$

$$A_R = \frac{-5\omega^2 \bar{\alpha}_1}{6[(1 - 4\omega^2 \bar{\alpha}_1^2)^2 - 25\bar{\alpha}_1^2 \omega^2]}, \quad (33)$$

and

$$A_I = \frac{-(1 - 4\omega^2 \bar{\alpha}_1^2) \omega}{6[(1 - 4\omega^2 \bar{\alpha}_1^2)^2 - 25\bar{\alpha}_1^2 \omega^2]}. \quad (34)$$

Again, when $\varepsilon = 0$ one can establish an exact solution (cf. Rajagopal [4]).

The skin friction on the plate is given by the real part of

$$\tau_\omega = \rho U_0^2 \{e^{i\omega t} [f'_{0R}(0) + i f'_{0I}(0)] + \varepsilon e^{i3\omega t} [f'_{1I}(0) + i f'_{1R}(0)] + \dots\}. \quad (35)$$

It follows from Eqs. (25)–(34) that

$$f'_{0R}(0) = -\delta_R, \quad (36)$$

$$f'_{0I}(0) = -\delta_I, \quad (37)$$

$$f'_{1I}(0) = -A_I m_I + A_R m_R + 3A_I \delta_I - 3A_R \delta_R, \quad (38)$$

and

$$f'_{1R}(0) = A_R m_I + A_I m_R - 3A_R \delta_I - 3A_I \delta_R. \quad (39)$$

In Table 2 the numerical values of

$$\bar{u}_0'(\eta) = f'_{0R}(\eta) \cos \omega \bar{t} - f'_{0I}(\eta) \sin \omega \bar{t} \quad (40)$$

and

$$\bar{u}_1'(\eta) = f'_{1R}(\eta) \cos 3\omega \bar{t} - f'_{1I}(\eta) \sin 3\omega \bar{t} \quad (41)$$

are provided for various values of $\omega \bar{t}$ and $\bar{\alpha}_1$.

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