THE UNIVERSITY OF MICHIGAN COLLEGE OF ENGINEERING

High Altitude Engineering Laboratory

Departments of

Aerospace Engineering

Atmospheric and Oceanic Science

Technical Report

FEASIBILITY OF SATELLITE MEASUREMENT OF STRATOSPHERIC MINOR CONSTITUENTS BY SOLAR OCCULTATION

by

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ORA Project 011023

under contract with:

NATIONAL OCEANIC AND ATMOSPHERIC ADMINISTRATION

GRANT NG-10-72

administered through

OFFICE OF RESEARCH ADMINISTRATION ANN ARBOR

October 1973

<u>ensm</u> umra 51

ABSTRACT

The determination of stratospheric concentration of minor constituents by satellite solar occultation is examined. The method is shown feasible for ozone up to 50 km, water vapor up to 50 km, nitrous oxide up to 30 km, methane up to 50 km and carbon monoxide up to 20 km. Transmittance calculations for these and other gasses are presented for optimal spectral regions. Calculations of extinction by aerosols in the lower stratosphere show a dominant effect in the window regions near 10 μ m. Several inversion techniques are developed and examples of profiles retrieved by different methods are compared. Computer programs are described to calculate the transmittances by the use of a band model and by the line-by-line integration technique.

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Chapter 1. Introduction

The purpose of the work performed under this grant is to examine the feasibility of determining stratospheric concentrations of minor constituents and/or pollutants from satellite measurements of infrared absorption during solar occultation. Before such a task can be undertaken it is important to have some estimates of typical distributions of the constituents either from actual measurements or from theoretical models involving chemistry, photochemistry, diffusion etc. It is also necessary to have the capability of calculating the infrared spectral absorption along a tangent path through the atmosphere once the distribution of the atmospheric constituents has been specified, i.e., we require to know the spectral line parameters for each constituent absorbing in a given spectral region.

Our earlier report (Drayson, et al., 1972) contained a survey of the stratospheric distribution and the spectral properties of the minor constituents. For several molecules the optical masses along a tangent path were calculated for several tangent altitudes and for some molecules the absorptions along the tangent paths were roughly estimated from available laboratory data or approximate calculations. The report also considered stratospheric aerosols whose distributions are of considerable interest and which also may interfer with the absorption by molecular constituents.

In this report we describe the progress made in the continuation of the investigation. In Chapter 2 we examine more closely the absorption by stratospheric molecules with the main emphasis on the more abundant of the minor constituents, for two reasons:

i) The absorption by the more abundant minor constituents

is large even averaged over spectral intervals several wavenumbers wide, so that a comparitively simple instrument of medium spectral resolution could be employed for satellite measurement.

ii) The spectral absorption properties of these molecules are known comparitively well. In particular several of them appear on the magnetic tape of line parameters compiled by AFCRC (McClatchey et al., 1973).

Transmittance calculations have been made either by the use of a band model or by a line-by-line integration computer program (described in the Appendix). In general we have not attempted to determine the accuracy of the spectral line parameters, although an exception was made in the case of ozone.

The extinction of solar radiation by stratospheric aerosols is examined in Chapter 3. The aerosols are important for two reasons:

- i) They may interfer with a sounding of a molecular constituent so that an accurate estimate of the extinction by the aerosol alone is required to determine the vertical profile of the molecular component.
- ii) The distribution of dust and aerosols in the stratosphere is known to be a factor that influences the climate at the surface and a continuous monitoring would aid our understanding of this problem as well as processes within the stratosphere itself.

In Chapter 4 we consider the inversion problem, i. e. how to determine the vertical profile of the constituents from the occultation measurements. In the absense of noise the problem is compartively simple but in a realistic situation some smoothing constraints must be applied to prevent domination of the solution by the noise present. Several different techniques are examined and compared.

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- McClatchey, R. A., W. S. Benedict, S. A. Clough, D. E. Burch, R. F. Calfee, K. Fox, L. S. Rothman and J. S. Garing (1973), AFCRL Atmospheric Absorption Line Parameters Compilation, AFCRL Environmental Research Paper No. 434.

Chapter 2. Stratospheric Absorption by Molecular Constituents.

2.1 Introduction

The previous report dealt primarily with 1) the distributions of stratospheric minor constituents, 2) the locations of and available data on the infrared bands, and 3) a crude estimate of the maximum absorption one might expect from these various bands. These latter results were only very approximate, since they were obtained from absorption profiles given in McCaa and Shaw (1967) for the ozone bands, and in Burch et al. (1962) for other molecules, and the mass paths and pressures which were used generally did not correspond to stratospheric conditions. In addition, the measurements were all made at room temperature, and the absorption, especially in the wings of the bands, may depend strongly on temperature.

The emphasis of the present investigation has been to construct transmission curves vs. height for stratospheric tangent paths corresponding to extreme or typical distributions of the minor constituents. These transmissions correspond to small wavenumber intervals (generally 1cm⁻¹) and were chosen to represent as nearly as possible the maximum absorption in each of the bands. A band model or direct line by line integration has been used to represent the absorption and the validity of the model and/or the band parameters have been compared with experimental results. Finally, the feasibility of using the various bands for tangent-path remote soundings is discussed.

2.2 Band Model

The band model is essentially a random model, i.e., the spectral lines are assumed to be randomly distributed. In addition,

the actual number of lines is used which is a feature of the quasi-random model developed by Wyatt et al. (1962). The lines are grouped into intensity intervals, and all lines in the intervals are given a strength equal to the average of the strengths of lines within that interval. The magnitude of the intensity interval is variable. For those spectral regions for which the lines have very similar intensities, the variation in intensity is chosen small, while for the intervals whose line intensities vary over many orders of magnitude, the lines are grouped into intensity decades.

The transmission T_i is given as,

$$T_{i} = \prod_{k=1}^{J} \left\{ \frac{1}{\Delta \omega_{i}} \int_{\Delta \omega_{i}} \exp(-\beta_{k} P_{i}(\omega)) d\omega_{i} \right\}^{n_{k}}$$
 (2.1)

where $\Delta \omega_i$ is the width of the spectral interval over which the transmission is determined; $\mathbf{a}_{\mathbf{k}}$ and $\mathbf{n}_{\mathbf{k}}$ are the mean line strength and number of lines in the intensity interval, \mathbf{P}_i is the profile function, and \mathbf{u} is the mass path of the absorbing gas.

The profile function which must be used for stratospheric tangent path studies is the Voigt profile, since both collision and Doppler broadening contribute to the line profile in this height range. This profile is given by,

$$P = \frac{a}{\pi} \int_{-\infty}^{\infty} \frac{e^{-y^2}}{a^2 + [f(x) - y]^2}$$
 (2.2)

where $a = \alpha \sqrt{\ln 2}/\alpha_b$, with α_L and Δ_b being the collision and Doppler half-widths respectively. The collision half width is given for standard

temperature and pressure (t_o, P_o) and is found for any other temperature and pressure by the relation $\alpha_L = \alpha_o \, P \, \sqrt{t_o} \, / \, P_o \, \sqrt{t_o}$. The Doppler half width is calculated from $\alpha_D = (2k \, t \ln 2 \, / \, mc^2)^{1/2} \omega$, where k is Boltzmann's constant, m is the molecular mass, and c the speed of light. ω is actually line center but we assume a value equal to the center of the spectral interval; i. e., all lines in the interval are given the same Doppler half-width. This is also true for the collision half-width. The parameter $f(x) = \Delta \omega_i \sqrt{\ln 2} \cdot x/2 \alpha_D$, where x is essentially a measure of distance from line center given by $x = 2(\omega - \omega_O) / \Delta \omega_i$.

If equations (2.1) and (2.2) are combined, the transmission for a single line (represented by the quantity in brackets in (2.1), is,

$$T_{k} = \int_{0}^{\infty} \exp\left[-\frac{g_{k}u}{\alpha_{b}}\left(\frac{\ln 2}{\pi}\right)^{\frac{1}{2}}P(\alpha,f(x))\right]dx \qquad (2.3)$$

Unfortunately equation (2.3) has no analytical solution, and must be evaluated numerically. Accordingly, a three dimensional table was prepared for which the parameters and their ranges are,

-6
$$\leqslant \log (S_k u / \Delta \omega) \leqslant 6$$

-7 $\leqslant \log (a) \leqslant 3$
2 $\leqslant \log(\Delta \omega / \alpha) \leqslant 6$

The first two are evaluated at intervals of 0.1, while the interval for the latter is 1. The actual transmission for a given set of parameters is found by bilinear interpolation on the table. In order to reduce the computing time, yet maintain the necessary accuracy for this feasibility study, we have excluded the contribution to the absorption from spectral lines outside the interval of interest; this is equivalent to requiring

that the total line absorptivity fall within the specified spectral interval. Thus $\log \Delta \omega / \approx 0$ was taken as 6 and the spectral interval adjusted accordingly.

Uncertainties in the calculated transmission functions can occur from inaccurate line parameters from which the model is constructed, or from the actual model itself, i.e., the lines may not be randomly distributed. One would not expect the latter to be a major problem for the non-linear molecules since their vibration-rotation spectra are quite complex. As an example, Fig. 2.1 compares a band model calculation with an "exact line by line" calculation averaged over one-tenth wavenumber intervals. While there is some "clustering" of the lines (at, e.g. 1124.3 cm⁻¹) the band model represents an average transmission quite well. The averaging interval for the band model is also not critical as the average of the 0.5 cm⁻¹ intervals gives nearly the same transmission as the average of the 1 cm⁻¹ intervals.

The line parameters used for both the band model and line by line integration are from McClatchey et al. (1973). A magnetic tape containing these data was graciously provided. This tape containing the most recently published tabulations provides line strengths, positions half widths, and ground state energies for selected bands of ozone, water vapor, carbon monoxide and dioxide, nitrous oxide, methane and oxygen. Approximately 110,000 lines are included for wavelengths longer than 1 micrometer.

2.3 Ozone

Ozone bands and the corresponding spectral intervals chosen for the stratospheric tangent path calculations are given in Table 2.1.

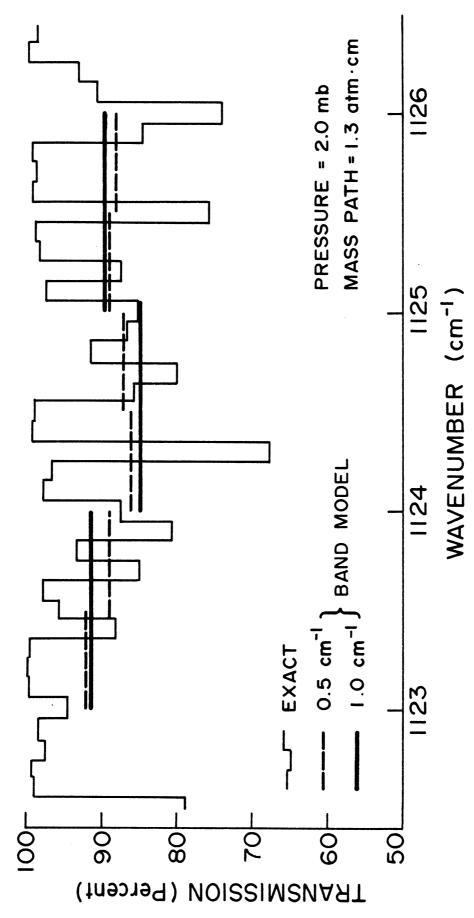


Fig. 2.1 Comparison of exact calculation and band model.

These intervals were chosen so that they give maximum or near maximum absorption for each band. McCaa and Shaw's (1967) absorption profiles were used to locate approximately these regions, and the final identification utilized the line positions and strengths as given by McClatchey et. al. (1973). It should be noted that the present analysis does not include three combination bands (1728, 1792 and 3181 cm⁻¹) discussed in the previous report. Their line parameters are not given by McClatchey et al., and we are not aware of any line listings for these bands. The 3181 cm $^{-1}$ (2 $\sqrt{1}$ + $\sqrt{3}$) band is not important for this study since our earlier work indicated that even with the maximum realistic ozone distribution, maximum absorption within the band as estimated from the McCaa and Shaw data is only 9% at 24 km. However, the 1728 cm $^{-1}$ ($\sqrt{1}$ + $\sqrt{3}$) band gives a comparable absorption but with the minimum ozone amount. The 1792 cm⁻¹ ($\sqrt{1+\sqrt{2}}$) band is intermediate to these two. Fortunately, it will be shown that the bands given in Table 2.1 provide the necessary absorption throughout the stratosphere, and it is not necessary to consider these additional bands.

Band	$ \mathbf{v}_1 $	V_2	$\sqrt{3}$	√ ₁ + √ ₃	$v_1' + v_2' + v_3''$	3 √ 3
Wavenumber (cm ⁻¹)	1124.5	717	1025	2131	2795	3046

Table 2.1 Centers of the 3 cm⁻¹ spectral intervals of tangent path calculations ozone bands selected for the stratospheric

The model atmosphere from which the tangent path absorptivities were determined is fully explained in the previous report. The USSA (1962) was assumed and ozone distributions corresponding to the largest and smallest amounts one might expect to observe were constructed. These extreme ozone mass paths for these heights as well

as the tangent path pressures and temperatures are given in Table 2.2. The latter were evaluated from a Curtis Godson approximation, i.e., they were weighted by the ozone mass path.

Tangent Height	Pressure	Temperature	Mass Path (atm-cm)
(km)	(mb)	(^O K)	
12	88.5 - 110.	218	45.0 - 7.1
20	37.9 - 37.7	220	24.7 - 5.6
30	8.3 - 8.4	232	6.8 - 1.2
40	2. 0 - 1. 6	255	1.6 - 0.28
50	. 56 56	266	0.43 - 0.074

Table 2.2 Curtis-Godson pressures and temperatures for selected tangent heights for extreme ozone amounts. The temperatures are the same for both extreme ozone mass paths.

1123 - 1126 cm
$$^{-1}$$
 (\mathbf{V}_1 band)

The 1123 - 1126 cm⁻¹ spectral interval contains 63 lines of the $\sqrt{1}$ band in the McClatchey et al. data. Line strengths range over four orders of magnitude at room temperature. A collision half width of 0.110 cm⁻¹ is given.

A comparision between the band model and experimental profiles of McCaa and Shaw (1967) is shown in Table 2.3. Note that the transmissions, when averaged over a 3 cm⁻¹ interval which is

Pressure (mb)	20	20	67	400
Mass Path (atm-cm)	1.3	2. 9	4. 2	12. 7
1123 - 1124	. 92	. 87	. 75	. 38
1124 - 1125	. 85	. 78	. 53	. 23
1125 - 1126	. 90	. 86	. 76	. 31
Average Experimental (McCaa and Shaw)	. 89 (.88) . 92	.84(.83)	. 68 (.70) . 72	.31(.29)

Table 2.3 A comparison of theoretical (band model) and experimental (McCaa and Shaw, 1967) transmissivities for the 1123-1126 cm⁻¹ spectral interval. The transmissions shown in parentheses refer to an averaging interval of 0.5 cm rather than 1 cm⁻¹

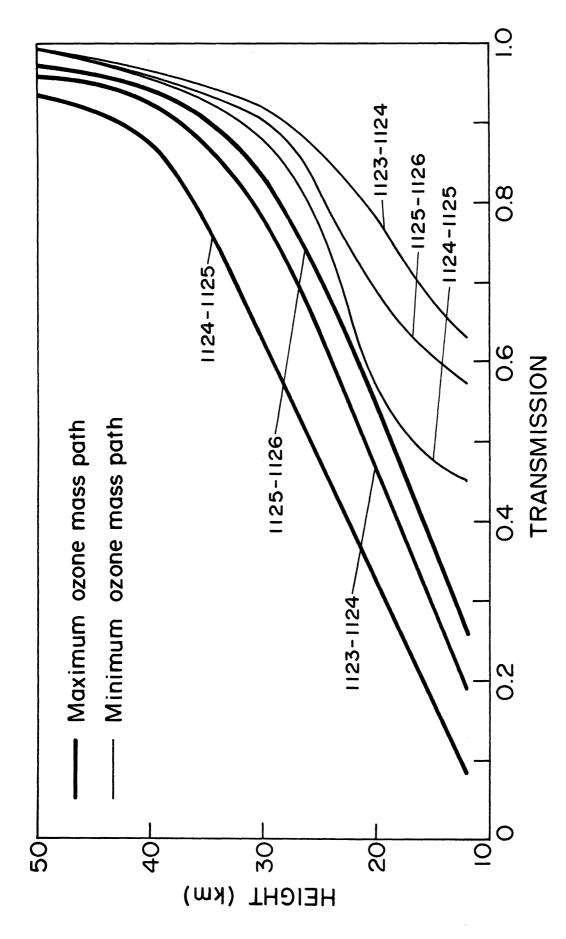


Fig. 2. 2 Stratospheric tangent path transmissivities for the spectral region 1123-1126 cm⁻¹for extreme ozone mass paths.

close to the spectral resolution of McCaa and Shaw (1967), agree to within four percent of the experimental results. This accuracy is certainly adequate to estimate the feasibility of using this band for remote soundings.

The importance of knowing the spectral resolution for these rather small intervals when comparing with experimental data is important, e.g. the absorption is larger in the 1124-1125 cm⁻¹ interval than the adjacent intervals by as much as 19% in the one case.

The band model calculation does not depend strongly on the width of the spectral subintervals over which the individual transmissions are calculated. For example, if a 0.5 cm⁻¹ rather than a 1 cm⁻¹ interval is used, the average transmission is within 0.02 of the 1 cm⁻¹ subinterval (shown in parentheses in Table 2.3).

The stratospheric tangent path transmissivities for the three 1 cm $^{-1}$ spectral intervals for extreme ozone amounts (Table 2.1) are shown in Fig. 2.2. If the spectral resolution is 3 cm $^{-1}$ or less, and if enough energy is available, then this $\sqrt[4]{1}$ band in the spectral region near 1124.5 cm $^{-1}$ should be adequate for tangent path remote soundings, at least to the midstratosphere. Of course, a larger spectral resolution would increase the transmission and lower the effective height.

715.5 - 718.5 cm
$$^{-1}$$
 ($\sqrt{2}$ band)

One would generally not consider the $\sqrt{2}$ band for remote sensing of ozone because of its strong overlap with the $\sqrt{2}$ band of carbon dioxide, centered about 667 cm $^{-1}$. The integrated band strength is only about 18 atm $^{-1}$ cm $^{-2}$ (McCaa and Shaw, 1967) while the $\sqrt{2}$ band

of carbon dioxide is about 214 atm⁻¹cm⁻² (Drayson, 1973). Nevertheless, a comparison of the band model transmissions with the spectra of McCaa and Shaw (1967) was made for completeness. The spectral region of maximum absorption was taken as 715.5 to 718.5 cm⁻¹. That this band is highly structured can be observed from both the experimental profiles of McCaa and Shaw and the data of McClatchey et al. In Table 2.4 is given the number of lines for each 1 cm⁻¹ interval as well as the mean line strengths for each intensity subinterval; these distributions were used in the band model calculations.

715.5 - 716.5 cm ⁻¹	716.5 - 717.5 cm ⁻¹	717.5 - 718.5 _{cm} -1
.0327 (5)	. 0254 (12)	. 0163 (7)
.0089 (9)	.0085 (14)	. 0035 (6)
.0020 (1)	.0018 (4)	. 0010 (1)

Table 2.4 Mean line strengths (atm $^{-1}$ -cm $^{-2}$) and numbers of lines (parentheses) used in the band model study for the 715.5 to 718.5 cm $^{-1}$ spectral region of the $\sqrt{2}$ band of ozone.

A comparison of the band model transmissivities with the McCaa and Shaw absorption profiles is given in Table 2.5. The obvious clustering of the lines is apparent from the rather large variation in transmissions among the three spectral intervals. The average of these results gives a transmission about ten percent smaller than the experimental spectra indicate. However, because of the clustering, a small discrepancy in the location of band center or a spectral interval somewhat larger than 3 cm⁻¹ would increase the band model transmissions. We have not analyzed further this difference because, as explained previously, one would not choose this band for remote soundings.

Pressure (mb)	20	66.6	66.6	533	533
Mass Path (atm-cm)	.84	4. 20	2.0	9.4	3.0
715.5 - 716.5 cm ⁻¹	. 832	. 599	. 709	. 164	. 508
$716.5 - 717.5 \mathrm{cm}^{-1}$. 708	. 379	. 525	. 039	. 294
717.5 - 718.5 cm ⁻¹	. 896	. 703	. 7.71	. 329	. 661
Average	. 81	. 56	. 67	. 18	. 49
Exp er im ent al (McCaa and Shaw)	. 90	. 67	. 77	. 27	. 59

Table 2.5 Comparison of band model transmissions with experimental spectra of McCaa and Shaw for the 715.5 to 718.5 cm⁻¹ spectral interval of the ∜2 ozone band.

Tangent path transmissivities for only $\sqrt{2}$ band ozone lines in the interval of 715.5 to 718.5 cm⁻¹ are shown in Fig. 2.3. If one were to include the very strong absorption by carbon dioxide, the transmission values would be much reduced, and it is likely that only in the upper atmosphere, if at all, would the transmission be large enough for remote sounding studies.

1023.5 - 1026.5 cm
$$^{-1}$$
 ($\sqrt{3}$ band)

More studies have been devoted to the $\sqrt[4]{3}$ and $\sqrt[4]{1}$ bands than any of the other ozone vibration bands. The spectra are complex and analysis is difficult because of the interaction of these bands. The line parameters of McClatchey et al. are the latest which appear in the open literature. These parameters are primarily from the work of Clough and Kneizys (1965, 1966) although some hot bands and isotopic bands have been added. Aida (1973) has also calculated line parameters but unfortunately the ground state energies are not available so that the line strengths cannot be calculated for arbitrary temperatures. The total number of lines which appears in his tabulation is about 10,000.

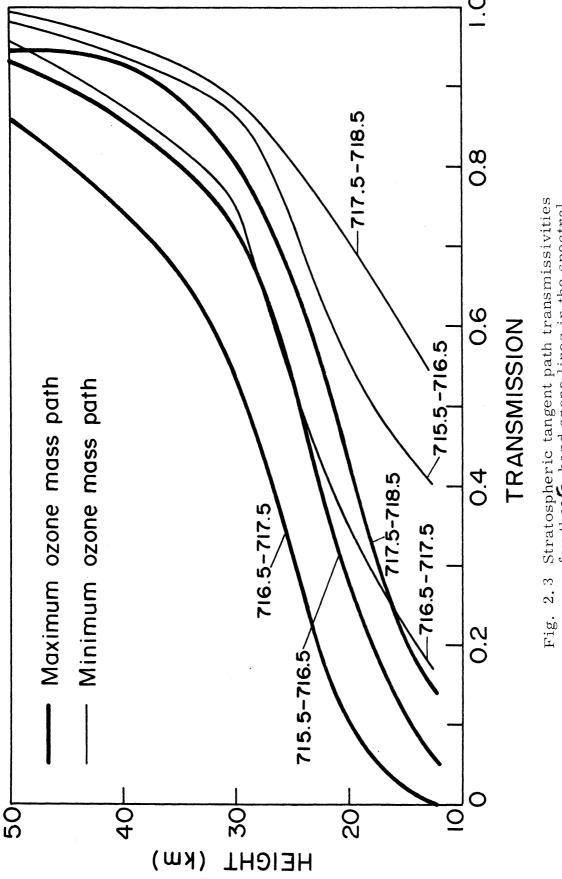


Fig. 2.3 Stratospheric tangent path transmissivities for the √2 band ozone lines in the spectral region of 715.5 - 718.5 cm⁻¹.

Although much effort has been devoted to an analysis of the $\sqrt{1}$ and $\sqrt{3}$ bands, discrepancies still exist among the calculated line parameters. The half width as given by McClatchey et al. is 0.11 cm⁻¹ (from Lichtenstein et.al., 1971), while Aida calculated a half width for each line adjusted to a mean line width of 0.078 cm⁻¹ (from Walshaw, 1955). Also the band centers for the overtone band $2\sqrt{3} - \sqrt{3}$ and the $\sqrt{3}$ band of the isotope $\sqrt{16}$ O¹⁸O are different for the two calculations. For the overtone band McClatchey et al. give a band center of 1027.096 cm⁻¹, while Aida (1973) gives 1012.1 cm⁻¹. Similarly McClatchey et al. give 1028.096 for the center of the isotopic band while Aida gives 1024.1 cm⁻¹.

Although the intensities of these bands are small (4.26 atm⁻¹cm⁻² for the overtone and 1.54 atm⁻¹cm⁻² for the isotope), they can strongly influence the absorption in some parts of the spectrum. For example, in a 1 cm⁻¹ interval, centered about 970 cm⁻¹, the total line strength as given by McClatchey et al. is about 13×10^{-3} atm⁻¹cm⁻², while Aida's results give a strength of 40×10^{-3} atm⁻¹cm⁻². Much of this discrepancy can be resolved if the $2\boldsymbol{\sqrt{3}}$ - $\boldsymbol{\sqrt{3}}$ band is given the same center in both calculations. For example if the band center in the McClatchey et al. data is shifted down 14.9 cm⁻¹ to agree with that of Aida, then the total line strength from the McClatchey et al. data is about 41×10^{-3} cm⁻² atm⁻¹, agreeing well with that of Aida. A comparison of transmissions with experimental data of McCaa and Shaw indicates better agreement when the $2\sqrt{3}$ - $\sqrt{3}$ band is centered at 1012.1 cm⁻¹; for example at 20 mb and a mass path of 4.62 atm-cm, the transmission in the interval 969.5 to 970.5 is 0.94 for the unshifted data, while a shift of the $2\sqrt{3}$ - $\sqrt{3}$ band gives a transmission of 0.83. The latter agrees much better with the value of 0.80 as given by McCaa and Shaw (1967).

Band model transmissions for the 1023.5 to 1026.5 cm⁻¹ spectral interval are compared with experimental data from McCaa and Shaw in Table 2.6. The difference approaches ten percent in some cases. For this model the half width was chosen as 0.08 cm⁻¹ and the distribution of mean line strengths (averaged over an intensity interval of 0.4) is shown in Table 2.7.

Pressure (mb)	20	20	20	66.6	66. 6
Mass Path (atm-cm)	12.6	2.6	. 45	. 41	. 87
1023.5 - 1024.5	. 012	. 228	. 652	. 493	. 344
1024.5 - 1025.5	.006	. 177	. 603	. 415	. 277
1025.5 - 1026.5	.013	. 243	.670	.515	. 296
Average	.010	. 216	. 641	. 474	. 305
Experimental (McCaa and Shaw)	. 02	. 19	. 55	. 48	. 22

Table 2.6 Comparison of band model and experimental transmissivities in the 1023.5 to 1026.5 cm⁻¹ intervals for the \gamma_3 ozone band.

1023.5 - 1024.5	1024.5 - 1025.5	1025.5 - 1026.5
. 739 (6)	. 797 (7)	. 783 (5)
. 192 (3)	. 229 (4)	. 260 (3)
. 0090 (16)	. 00986 (15)	. 0129 (14)
. 00088 (111)	. 00101 (121)	.0011 (110)
. 000045 (5)	. 000055 (9)	000049 (24)

Table 2.7 Distribution of mean line strengths and numbers of lines (in parentheses) as used in the band model calculation for the 1023.5-1026.5 cm⁻¹ spectral region of the \mathbf{V}_3 ozone band.

If the $2V_3 - V_3$ band is shifted to 1012.1 cm⁻¹ the transmissions and mean line strengths are as given in Tables 2.8 and 2.9 respectively. While the agreement is somewhat better, it is not definitive. The weak overtone lines change only slightly the overall strength in this spectral region (Compare Tables 2.7 and 2.9).

Pressure (mb)	20	20	20	66. 6	66.6
Mass Path (atm-cm)	12.6	2. 6	. 45	. 41	. 87
1023.5 - 1024.5 cm ⁻¹	. 012	. 221	. 6 2 9	. 478	. 266
$1024.5 - 1025.5 \text{ cm}^{-1}$. 006	. 166	. 578	. 399	. 206
1025, 5 - 1026, 5 cm ⁻¹	. 013	. 234	. 648	. 502	. 301
Average	. 010	. 207	. 618	. 459	. 257

Table 2.8 Band model transmissions for the 1023.5 to 1026.5 cm⁻¹ spectral interval in the 3 ozone band. Center of the 2 3 - 3 band has been shifted to 1012.1 cm⁻¹

1023.5 - 1024.5 cm	¹ 1024.5 - 1025.5 cm	⁻¹ 105.5 - 1026.5 cm ⁻¹
. 739 (6)	. 797 (7)	. 783 (5)
. 192 (3)	. 229 (4)	. 260 (3)
0107 (21)	. 0105 (23)	. 0131 (19)
.000803 (96)	. 000937 (99)	. 000999 (100)
.000034 (11)	. 000047 (14)	. 000044 (25)

Table 2.9 Distributions of mean line strengths (cm⁻² atm⁻¹) and numbers of lines (in parentheses) as used in the band model calculations given in Table 2.8

These calculations presented in Tables 2.6 and 2.8 were made with a half width of 0.08 cm⁻¹ which corresponds to the mean half width given by Aida (1973). If the half width is 0.11, the value given by McClatchey et al., then the transmissions are as shown in Table 2.10. The distribution of line strengths corresponds to Table 2.9. It is not obvious which half width is more appropriate. For the mass paths of 2.6, 0.45, and 0.87 atm-cm, the half width of 0.11 cm⁻¹ gives better agreement while for the other mass paths, the best agreement is found for a width of 0.08 cm⁻¹. Actually the only significant difference between the theoretical and experimental transmissivities is for the mass path of 0.41 atm-cm, where our band model value is about 0.07 smaller than the value from McCaa and Shaw.

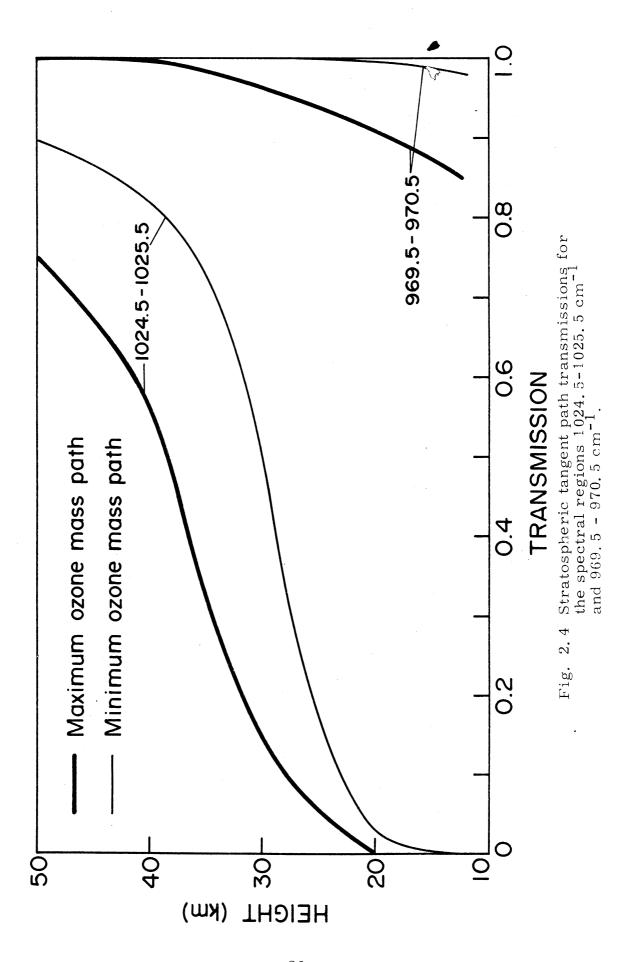
Pressure (mb)	20	20	20	66.6	66.6
Mass Path (atm-cm)	12.6	2.6	. 45	. 41	. 87
1023.5 - 1024.5cm ⁻¹	. 007	. 199	. 600	. 429	. 235
$1024.5 - 1025.5 \text{cm}^{-1}$. 003	. 14	. 525	. 35	.168
1025.5 0 1026.5cm ⁻¹	. 007	. 209	. 601	. 454	. 258
Average	. 005	. 182	. 575	. 411	, 220

Table 2.10. Band model transmissions for the 1123.5 to 1126.5 cm interval in the \(\mathbf{Y} \)3 ozone band corresponding to line strength parameters as given in Table 2.9 with half width of 0.11 cm

A calculation was also made for the $\sqrt{3}$ isotope $^{16}\text{O}^{18}\text{O}$ shifted down 4 cm $^{-1}$, to 1024.1 cm $^{-1}$, in agreement with Aida. The transmissions in the 1023.5 to 1024.5 cm $^{-1}$ interval changed by less than one percent.

Stratospheric tangent path transmissivities for two 1 cm⁻¹ spectral intervals, at 1024.5 - 1025.5 cm⁻¹ corresponding to a region of maximum absorption, and 969.5 - 970.5 cm⁻¹ located in the wing, are shown in Fig. 2.4. The region of maximum absorption in the V_3 band can be used for remote sounding from the midstratosphere at least to the stratopause. However in the low stratosphere, the transmission is small, and a spectral region in the wing of the band could be used. It appears that a wavenumber somewhat greater than 970 cm⁻¹ should be appropriate.

The agreement in transmission between experimental and our band model results is better for the $\sqrt[4]{3}$ and $\sqrt[4]{1}$ bands than for the others investigated; one would expect this to be the case since more work, both theoretical and experimental, has been done on these bands.



Fortunately the $\sqrt[4]{3}$ band appears to be the most desirable for remote sensing work. The band is strong enough so that one could choose a number of spectral intervals within the band so that soundings could be made throughout the stratosphere.

There are a number of disadvantages to using this band which should be mentioned. The line density is so large that direct line by line calculations are probably not feasible, and some empirical or band model approach might have to be employed. Secondly, there are still discrepancies among the theoretical line parameter tabulations which need to be resolved, e.g., the half widths and centers of isotope and overtone bands. The weaker lines may not be important near band center, but in the wings these lines become extremely important because of their strong temperature dependence. To illustrate, we show in Table 2.11, the transmission in two spectral intervals, the one at 1025 cm⁻¹ being a region of the band corresponding to maximum absorption and containing many strong lines, and the 970 cm⁻¹ region on the wing of the band. For example, at 300K the strongest lines in the 1025 cm⁻¹ region are about one-hundred times stronger than in the 970 cm⁻¹ region and at 200 K this difference increases to about one-thousand. The strongest lines are less temperature dependent and this is clearly shown in Table 2.11 where the transmission for the 1025 cm⁻¹ region varies by less than one percent, while the variation for the wing region is about forty-eight percent. Thus the line parameters must be accurately known because the stratospheric temperature range is similar to that given in Table 2.11. It is unfortunate that there are no low temperature ozone measurements against which we can compare our theory.

An additional disadvantage in using this spectral region is that the aerosol absorption especially in the low stratosphere is quite large. This problem is discussed in Chapter 3.

Temperature	300	275	250	225	200	
969.5 - 970.5	. 466	. 605	. 637	. 876	. 952	
1024.5 - 1025.5	. 147	. 145	. 147	. 152	. 153	

Table 2.11. Effect of temperature on transmission in the spectral intervals of 969.5-970.5 (20mb and 26 atm·cm) and 1024.5-1025.5 cm⁻¹ (20mb and 2.6 atm·cm)

2129.5 - 2132.5 cm
$$^{-1}$$
 ($\boldsymbol{\sqrt{1}}$ + $\boldsymbol{\sqrt{3}}$)

A comparison of the band model calculations for the V_1 + V_3 band with the absorption profiles of McCaa and Shaw is shown in Table 2.12. The band model transmissivities represent averages over 1 cm⁻¹ spectral intervals, centered about 2130, 2131 and 2132 cm⁻¹. Note that in all but the last case, the model transmissivities are smaller than the experimental results, in one case by as much as twenty-eight percent.

Mass Path (atm·cm) Pressure (mb)	13.8 20	4. 5 20	0, 87	4. 8 66. 6	0. 2 3 66. 6
2129.5 - 2130.5 cm ⁻¹ 2130.5 - 2131.5 cm ⁻¹ 2131.5 - 2132.5 cm ⁻¹	. 172	. 303 . 243 . 279	. 564 . 593 . 778	. 180 . 214 . 269	. 862 . 873 . 938
Average	. 20(.23)	. 27(.29)	. 64(.64)	. 22(.25)	. 89(89)
Experimental (McCaa & Shaw)	. 33	. 55	. 82	. 30	. 85

Table 2.12. Comparison of band model transmissivities with the experimental study of McCaa and Shaw (1967) for the spectral interval 2129.5 to 2132.5 cm⁻¹ for the 71 + 73 ozone band. The transmissions in parentheses refer to a single spectral interval extending from 2129.5 cm⁻¹ to 2132.5 cm⁻¹.

This discrepancy is probably not due to experimental resolution since the transmissions of all three spectral intervals are less than the experimental values. The discrepancy is also not due to a difference in band center, since the line parameters were chosen so as to give minimum transmission in the band and the experimental results do not yield such small values at any wavenumber within the band. In addition, the experimental results include the effect of the CO fundamental at 2143 cm⁻¹; McCaa and Shaw state that the absorptance of this band was never greater then twenty percent. This effect, although small, would make the experimental ozone transmissivities even higher, giving a larger disagreement with the band model.

The band model also does not appear responsible for the discrepancy. Two possible sources of error were the averaging interval and the assumed intensity subintervals. The former was checked by applying the band model to a single interval extending from 2129.5 to 2132.5 cm⁻¹, and the transmissions are shown in parentheses in Table 2.12; the agreement is within three percent. Also rather than grouping the lines into intensity decades, which yielded two intensity subintervals, they were grouped for intervals of 0.2, 0.4, 0.6 and 0.8, as well. The various intensity intervals are shown in Table 2.13 for the 2129.5 to 2130.5 cm⁻¹ interval, and the effect on the transmission is shown in Table 2.14. The uncertainty in the transmission is less than five percent. Similar results were found for the other two spectral intervals.

¹ For an intensity interval of 0.4, for example, and if S_m is the strongest line in the spectral interval, then the intensity intervals would be S_m to 0.4 S_m , 0.4 S_m to (0.4)² S_m , (0.4)² S_m to (0.4)³ S_m , etc.

0.1	0. 2	0. 4	0.6	0.8
. 002 (29) . 0028 (6)	.026 (24) .0045 (11)	.030 (17) .010 (14) .0022 (4)	.035 (10) .020 (13) .0055 (10) .0019 (2)	.044 (3) .030 (10) .018 (9) .008 (6) .003 (7)

Table 2.13. Distributions of line intensities for various line strength intervals for the 35 spectral lines in the 2129.5 to 2130.5 cm ⁻¹ spectral interval of the ₹1 + √3 ozone band.

Mass Path (atm·cm)	13.8 20	4. 5 20	0.87	4. 8 66. 6	0. 23 66. 6
Pressure (mb)	20	20	20	00.0	00.0
0.1	.185	. 303	.564	.18	. 862
0. 2	. 185	. 321	.604	.161	. 868
0.4	. 191	. 32 5	. 581	. 207	. 856
0.6	. 200	. 327	. 558	. 171	. 866
0.8	.197	. 310	.570	. 204	. 869

Table 2.14. Band model transmissivities for the 2129.5 to 2130.5cm⁻¹ ozone band distributions of line intensities as given in Table 2.13. Compare with Table 2.12.

There is still much uncertainty in the line parameters for this band and we suspect this is the reason for the discrepancy between the band model and experimental results. McClatchey et al. (1973) state that the line positions up to J=20 and $\rm K_a$ =4 are accurate to 0.3cm⁻¹ with "the error in line position significantly greater for higher quantum numbers." Although the total band intensity as used by McClatchey et al. agrees with the experimentally determined value of 32 atm⁻¹cm⁻² of McCaa and Shaw, nevertheless, an incorrect distribution of intensities of these lines could cause the lower transmission. In any case, it is o obvious that our present knowledge of the γ_1^r + γ_3 band is not adequate for application to remote sensing.

Stratospheric tangent path transmissivities for the spectral interval 2129.5 to 2132.5 cm⁻¹ are presented in Fig. 2.5. If the line parameters could be improved, then this band could be used for remote sensing at least in the lower stratosphere.

3044.5 - 3047.5 cm⁻¹ (3
$$\sqrt{3}$$
)

A similar comparison of the 3044.5 - 3047.5 cm⁻¹ spectral interval with the McCaa and Shaw results is shown in Table 2.15.

Pressure (mb) Masspath (atm·cm)	20	66	400	400	400
	14.6	1.4	19.1	6. 1	14. 3
3044. 5 - 3045. 5	58	92	24	67	33
3045. 5 - 3047. 5	51	90	22	64	32
3046. 5 - 3047. 5	53	90	16	62	28
Average	. 54	. 90	. 21	. 64	. 31
Experimental (McCaa and Shaw)	76	93	49	76	56

Table 2.1 . Comparison of band model transmissivities with experimental results of McCaa and Shaw (1967) for the 3044.5 to 3047.5 cm⁻¹ spectral interval for the 3 3 ozone band.

As in the prior case the band model transmissivities are much smaller and the discrepancy is probably also due to the uncertainties in the line parameters. Few details on the calculation of the line parameters for this band are given, but McClatchey et al. do state that the line positions are accurate only to ± 5 cm⁻¹, which is certainly not adequate for application to remote sensing.

Stratospheric tangent path transmissivities for the region of maximum absorption in this band is shown in Fig. 2.6. If one takes into account that the computed transmissivities are probably smaller than is

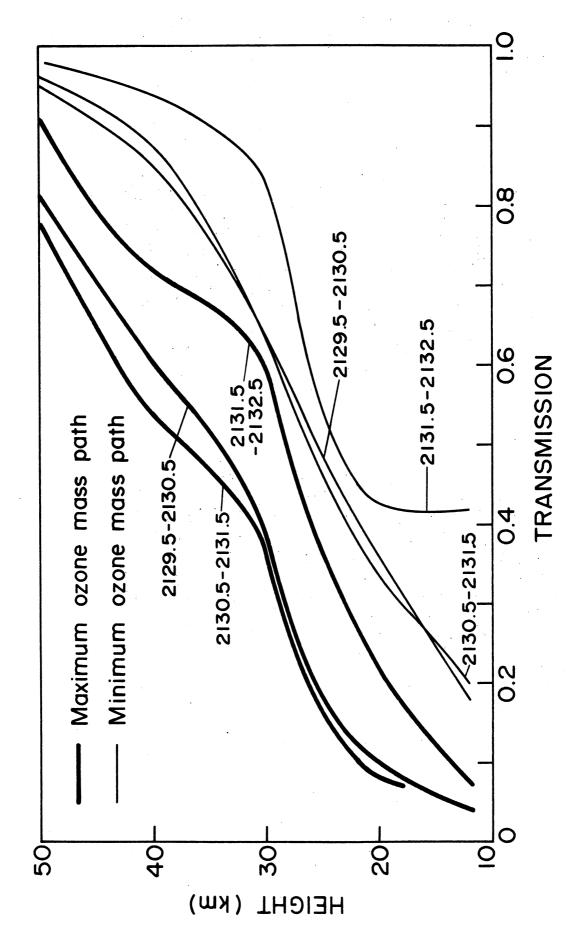


Fig. 2.5 Stratospheric tangent path transmissions for the spectral interval $3044.5 - 3047.5 \text{ cm}^{-1}$.

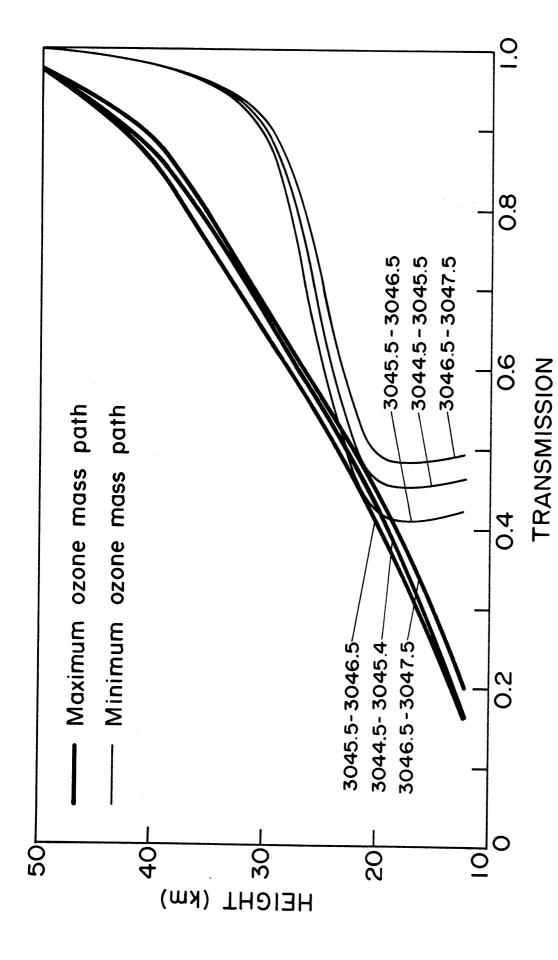
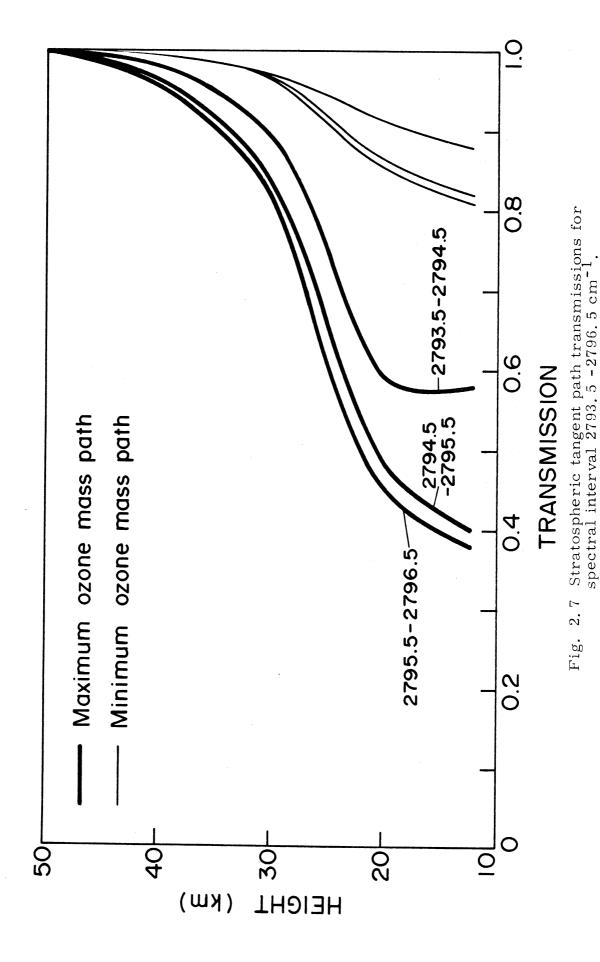


Fig. 2.6 Stratospheric tangent path transmissions for the spectral interval $3044.5-3047.5~\rm cm^{-1}$.



the actual case (see Table 2.15), then only in the low stratosphere could this band be useful for remote sensing of ozone.

2793.5 - 2796.5 cm⁻¹ (
$$\sqrt{1} + \sqrt{2} + \sqrt{3}$$
)

Band model transmissivities for this combination band are also much smaller than the experimental values, and are compared in Table 2.16. The line parameters were calculated by McClatchey et al. from a rigid rotor analysis and include lines for J less than 25 and $\rm K_a$ less than 6. The discrepancy may again be due to the distribution of intensities among the lines.

Pressure (mb)	20	66. 6	66.6	400	400
Mass Path (atm·cm)	14.6	1. 2	4. 5	14.3	19.1
2793.5 - 2794.5 cm ⁻¹	. 82	1.00	. 95	. 83	. 79
$2794.5 - 2795.5 \text{ cm}^{-1}$. 73	1.00	.92	. 74	. 68
2795.5 - 2796.5 cm ⁻¹	. 70	1.00	.91	. 71	. 65
Average	. 74	1.0	. 93	. 76	. 71
Experimental (McCaa & Shaw)	. 90	. 99	. 97	. 88	. 83

Table 2.16. Comparison of band model and experimental transmissivities for the 2793.5 to 2796.5 cm⁻¹ spectral interval in the $\gamma_1 + \gamma_2 + \gamma_3$ ozone band.

Stratospheric tangent path transmissivities are given in

Fig. 2.7. As indicated in Table 2.16, these transmissions are probably too small; thus even in the region of maximum absorption of this band, the absorption would be small, making remote soundings difficult.

2.4 Water Vapor

Calculations similar to those for ozone have been carried out for regions of maximum or near maximum absorption in three water vapor bands. The spectral regions are given in Table 2.17.

Band	$\mathbf{v}_{2}^{\mathbf{r}}$	$\mathbf{V}_{1},\mathbf{V}_{3, \text{ etc.}}$	$V_2 + V_3$, $3V_2$, $V_1 + V_2$, etc.
Wavenumber (cm ⁻¹)	1660-1675	3743-3753	5335-5355

Table 2.17. Spectral intervals of selected water vapor bands used in stratospheric tangent path transmission calculations.

The spectral intervals of 3743-3753 cm⁻¹ and 5335 - 5355 cm⁻¹ contain lines of numerous bands and a few of these are listed above. According to McClatchey, et al., the line positions are generally accurate to 0.01 cm⁻¹. Half widths for the individual lines are given, although for this analysis, we assumed a mean half width of 0.08 cm⁻¹. The spectral interval of 1660-1675 cm⁻¹ contains 59 lines and was subdivided into three 5 cm⁻¹ intervals. The spectral region around 3700 cm⁻¹ is highly structured and the interval was divided into two 5 cm⁻¹ subintervals; the total number of lines is 82. The 5335 to 5355 cm⁻¹ interval was divided into two 10 cm⁻¹ subintervals containing 110 lines. These spectral intervals were chosen so as to be compatible with the experimental resolution of Burch et al. (1962), whose data were used for comparison with the band model calculations.

The model atmosphere used for deducing the tangent path transmissivities is given in Table 2.18. The extreme mass paths were taken from the previous report.

Tangent Height (km)	Pressure	Temperature	Mass Path
	(mb)	K	(atm·cm)
12	134 - 113	217 - 218	72. 0 - 33. 1
20	38.2 - 31.8	220 - 221	40. 9 - 9. 45
30	8.31 - 8.5	232 - 231	14. 5 - 2. 01
40	2.0 - 2.06	255	2. 85 46
50	.56575	266 - 267	. 64 12

Table 2.18. Curtis-Godson pressures and temperatures for selected tangent heights for extreme water vapor mass paths.

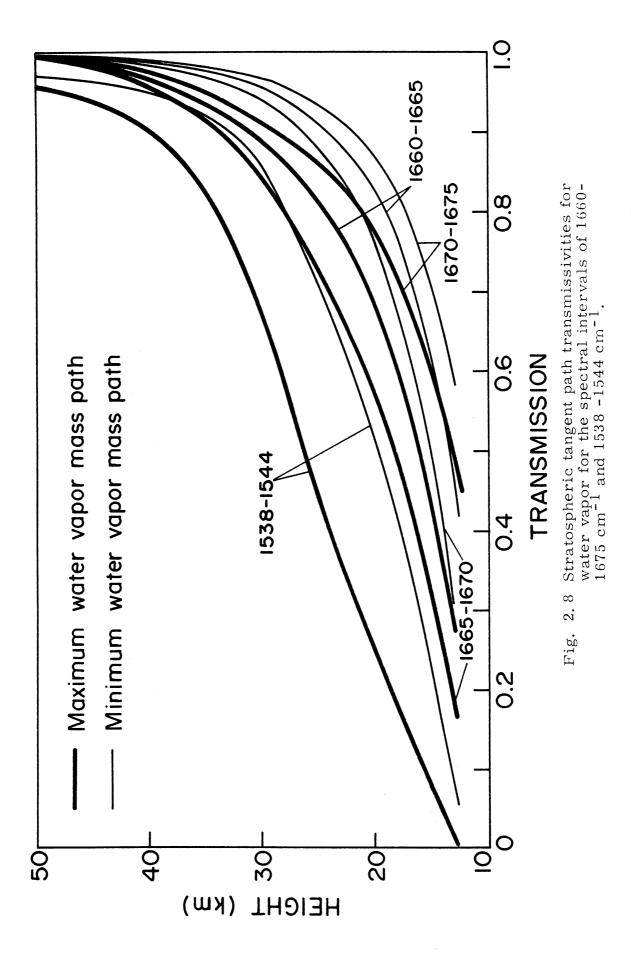
 $1660 - 1675 \text{ cm}^{-1}$ (\checkmark_2)

A comparison of the band model transmissions with the experimental data of Burch et al. (1962) for the 1660 - 1675 cm⁻¹ spectral interval is shown in Table 2.19. The agreement is excellent with the average of the band model results agreeing to within three percent of the experimental values. The absorption profiles are complex as can be seen from Table 2.19; in the one case the absorption varies by twenty-six percent in adjacent spectral intervals. Thus the spectral interval must be carefully chosen if this band is to be used for remote sensing.

Mass Path (atm·cm)	2.12	2 1. 9	44.7	43.8	95.8
Pressure (mb)	18.7	140	50.6	140	1070
					
1660 - 1665	.944	. 591	.623	. 445	. 000
1665 - 1670	.926	. 444	. 456	. 275	.000
1670 - 1675	.946	. 665	.698	. 536	. 007
Experimental (Burch et al.)	.94	. 57	. 62	. 42	. 0

Table 2. 19. A comparison of band model transmissivities with data of Burch et al. (1962) for the water vapor spectral interval of 1660 to 1675 cm⁻¹ (γ_2).

The stratospheric tangent path transmissions for two spectral regions in the $\sqrt[4]{2}$ band are given in Fig. 2.8. The 1538 - 1544 cm⁻¹ region is representative of maximum absorption in the band. The transmission is near one-hundred percent in the upper stratosphere and remote soundings are questionable. A smaller spectral interval would be desirable if the available energy is adequate. Numerous other spectral regions in this band would be adequate for remote soundings at least up to the midstratosphere, e.g., the 1660 - 1675 region, which is also shown in Fig. 2.8.



2

$3743 - 3753 \,\mathrm{cm}^{-1}$ spectral region

As mentioned previously, this spectral region contains lines of many bands, and the absorption spectra are extremely complex (see, e.g, Burch et al., 1962). Also Burch et al. give the resolution of their absorption profiles as approximately 10 cm⁻¹; thus there is probably an uncertainty of at least a few wavenumbers. Both these factors make comparison of the band model transmissions with their data rather difficult. However, we have attempted a comparison which is shown in Table 2.20. The band model transmissions are significantly

Pressure (mb)	1150	1043	151.	9 2 .	36.7
Mass Path (atm-cm)	135	4. 42	146.	4. 42	4. 42
3743 - 3748 cm ⁻¹	0	. 09	0	. 51	. 64
3748 - 3753 cm ⁻¹	0	.10	0	. 51	.60
Experimental (Burch et al.)	0	. 26	. 03	. 57	. 78

Table 2.20 Comparison of band model and experimental transmissitivities for water vapor lines in the 3743 to 3753 cm⁻¹ spectral interval.

lower but this was anticipated since the spectral interval was chosen to maximize the absorption. The spectral interval could be increased about 2 cm⁻¹ without significantly increasing the absorption, and this increase would be well within the resolution range. Thus the comparison neither justifies nor negates the band model and/or line parameters.

Tangent path transmissivities are shown in Fig. 2.9. If the contribution to the transmission from other molecular species is not large, then this band could be used for remote sensing of water vapor, at least in the lower stratosphere.

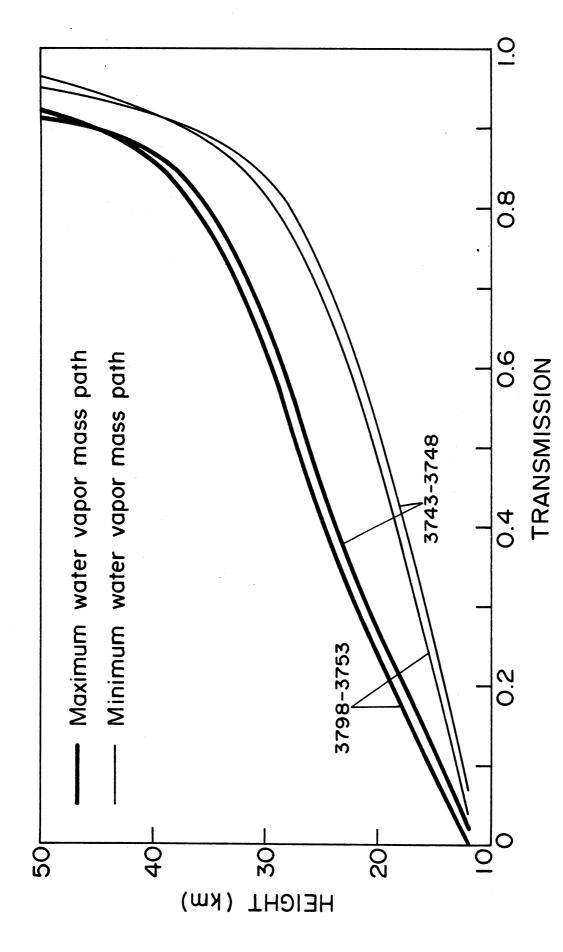


Fig. 2.9 Stratospheric tangent path transmissivities for the 3743-3753 cm⁻¹ spectral region.

5335 - 5355 cm⁻¹ spectral region

Results of the analysis for this spectral region are quite similar to those for the 3743 - 3753 cm⁻¹ region. The band model transmissions are smaller than Burch et al's results, but again, the model was chosen to give maximum absorption, which appears as a narrow peak in the Burch et al. absorption profile. Also the resolution is given as "approximately 20 cm⁻¹, and if it is only slightly larger, the transmission will decrease significantly. The tangent path transmissivities are given in Fig. 2.10, and indicate that this band is not suitable for remote sensing of water vapor. Only in the low stratosphere is there significant absorption and in this height range the 1600 cm⁻¹ spectral region could be used which contains fewer lines from other molecular species.

2.5 Methane

Although an extensive analysis on the feasibility of detecting methane by the solar occultation technique has not as yet been completed, our preliminary study seems promising. The strongest bands are the $\sqrt[4]{3}$ (3019 cm⁻¹) and $\sqrt[4]{4}$ (1306 cm⁻¹) fundamentals with strengths of 370 and 204 atm⁻¹cm⁻² respectively. A difficulty is that the line parameters need improvement, especially in extending the calculations to higher rotational quantium numbers and improving the intensities. Thus a detailed comparison with experimental transmissivities has not been made.

The stratospheric tangent path transmission for a single spectral interval is given in Fig. 2.11 which represents a region of maximum absorption in the $\sqrt[4]{4}$ band. This band model calculation

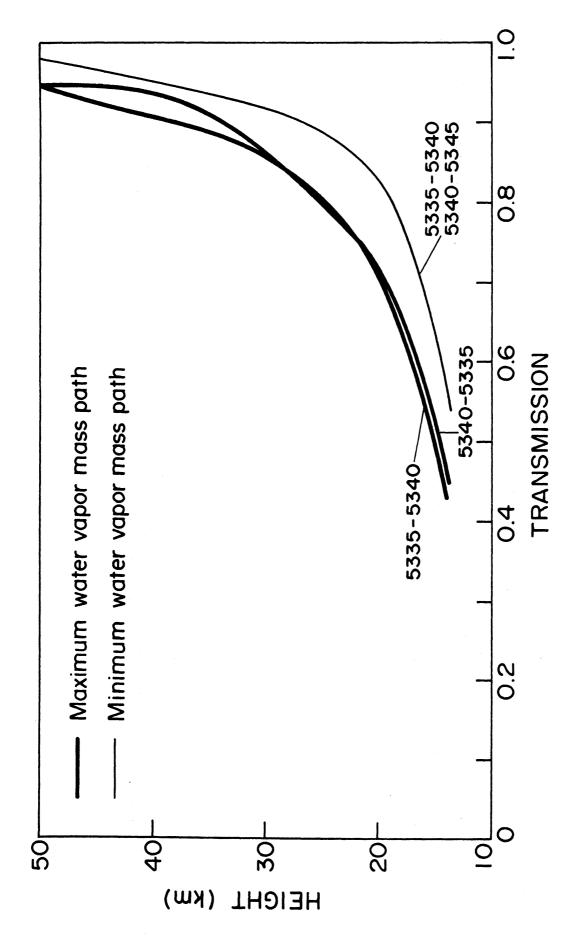


Fig. 2.10 Stratospheric tangent path transmissivities for water vapor in the 5335-5345 cm⁻¹ region.

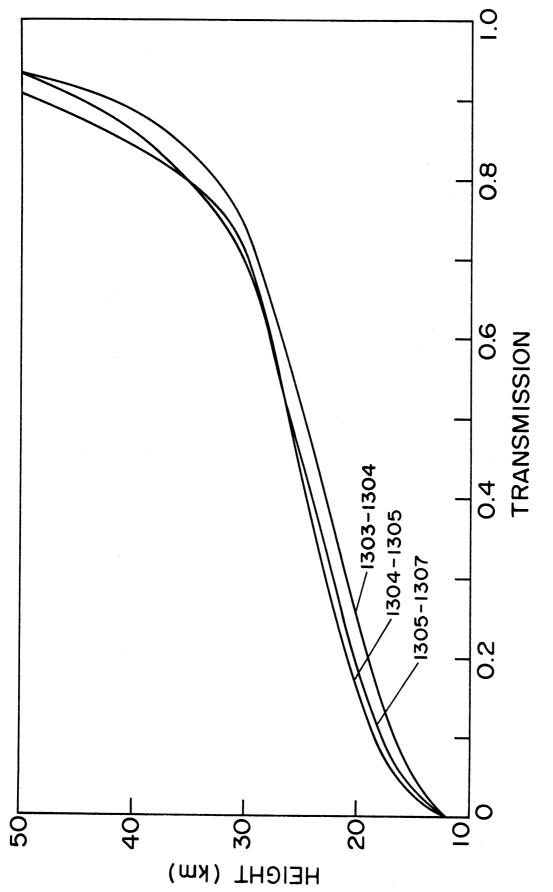


Fig. 2.11 Stratospheric tangent path transmissivities for the 1304-1307 cm⁻¹ region of methane.

indicates that remote sensing may be feasible throughout much of the stratosphere. One must keep in mind, however, that the tabulation of McClatchey et al. excludes numerous weak lines which may significantly alter the atmospheric absorption.

None of the stronger bands of methane is in a spectral region free from interference by other molecules. Nitrous oxide absorbs in the ν_4 band and ozone overlaps the ν_3 band so that these gasses would have to be sounded simultaneously. The best region would appear to be in the ν_4 Q-branch between 1304 and 1307 cm⁻¹ (see Fig. 2.11). The width of this channel is critical and there is overlap with N₂O. At 1350 cm⁻¹ the absorption by CH₄ is less by about a factor of two, but the problem of overlap is less severe. Alternatively the Q-branch of the ν_3 band (3016 - 3019 cm⁻¹) can be used while the region near 2960 cm⁻¹ has less absorption but also less interference by ozone.

2.6 Carbon Monoxide

Assuming various constituent profiles, calculations of atmospheric transmittances have been made. Table 2.21 shows the effect of slight changes in concentration of CO on the atmospheric transmittance. The calculations shown are for 2 model CO profiles, at a resolution of 5 cm $^{-1}$ at the spectral region 2173 cm $^{-1}$ near the peak of the R branch of the fundamental 4.6 μ m band. The second model constituent profile is 10% higher than the profile in the first model.

The line parameters used in the calculations are from Kunde (1968). Column 4 in Table 2. 21 shows the transmission with the increased CO concentration. At low altitudes (where the spectral line

is essentially Lorentz broadened) the absorption has increased by about 5% and this is consistent with the result obtained using a strong line approximation, in which the absorption is proportional to the square root of the optical mass. At higher altitudes the increase in absorption is less than 5% because Doppler broadening becomes important, and as the line centers are completely absorbed, there is lesser wing contribution. This result can be expected to hold for other molecules in spectral regions where the lines are non-overlapping along the absorption paths.

The region near 2173 cm⁻¹ also contains absorption lines of carbon dioxide and nitrous oxide. No attempt has been made to calculate the absorption by these gasses but some interference can be expected because of the low stratospheric mixing ratios of CO. The 2-0 band of CO is much weaker and would be difficult to use. Hence the region near 2173 cm⁻¹ appears to be the best choice for a CO measurement.

Tangent Height km	CO concentration Model 1 Vol. Mix.Ratio ppm		Atmospheric Transmission with Model 2 (10%inc.of CO)	Perc.Increase of Absorption
70	1.0	_	-	-
60	0.08	-	-	-
50	0.05	. 99825	. 99821	2. 29
40	0.02	.99784	. 99779	2.31
30	0.02	.99618	.99604	3.66
20	0.02	.98384	.98305	4 . 8 9
10	0.1	. 85910	. 85196	5.07

Table 2.21 Atmospheric Absorption by CO

2.7 Nitrous Oxide N₂O

The line parameter tape (McClatchey et. al. 1973) contains spectral line parameters for $\rm N_2O$. The molecule is linear. The theory of its spectrum is well understood. In addition, many experimenters have investigated the absorption properties of the stronger absorption bands, so that the parameters on the tape should be fully adequate for the calculations described here.

The strongest of all the $\rm N_2O$ bands is the $\,\nu_3$ centered near 2223.8 cm $^{-1}$, and is a factor of seven more intense than the next strongest band, the $\,\nu_1$ centered at 1284.9 cm $^{-1}$. The maximum stratospheric absorption by the $\,\nu_3$ band occurs at the peak of the P and R-branches is near 2210 and 2236 cm $^{-1}$ respectively. Calculations in these two spectral regions were made using the line-by-line program described in the Appendix. Carbon dioxide also absorbs in this region and similar calculations were made of the transmittance of this gas. Carbon monoxide lines of the 1-0 band also occur near 2210 cm $^{-1}$ but these are weak and were not considered here. Water vapor absorption is small under stratospheric conditions.

Figure 2.12 shows the transmittances for $\rm N_2$ O and $\rm CO_2$ for 4 cm⁻¹ intervals centered at 2210.5 and 2236.5 cm⁻¹. The $\rm N_2O$ concentrations are from Table 4.1.3 of our earlier report (Drayson et.al., 1972) and the U.S. Standard Atmosphere (1962) has been used. The $\rm CO_2$ concentration is assumed constant at 320 ppm V.

The $\rm N_2O$ transmittances are almost identical for the two intervals but the $\rm CO_2$ transmittance is remarkably higher at 2210.5 cm⁻¹ making this the clear choice of a spectral region to sound $\rm N_2O$. It should be pointed out that there may be some uncertainty in the line

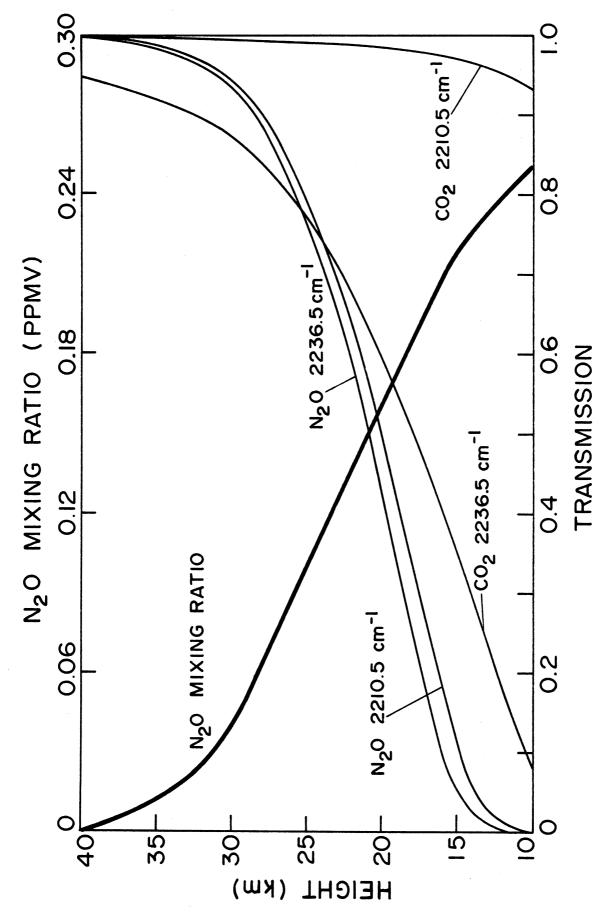


Fig. 2.12 Stratospheric Tangent path transmittance of $\rm N_2O$ and $\rm CO_2\cdot$

parameters of CO₂ since hot bands dominate the absorption in these regions and the intensities of the bands have a higher degree of uncertainty than the fundamentals. At 2236.5 cm⁻¹ the carbon dioxide band with the most intense lines appears to have been included twice on the tape so the transmittance may in fact be higher than indicated.

Another possible spectral region for sounding N_2O is near 1270 cm⁻¹ (R-branch of the ν , band) which gives considerably less absorption and has some interference by CH_4 absorption. The ν_2 band is much weaker than either the ν_1 or ν_3 bands but has the advantage of closely spaced lines in the Q-branch near 590 cm⁻¹. However absorption by CO_2 is again strong and a rough estimate showed the CO_2 absorption to be at least as large as the N_2O throughout the stratosphere.

The peak of the P-branch of the ν_3 band of N_2O near $2210~{\rm cm}^{-1}$ appears to be the best spectral region for sounding N_2O . The instrument resolution and exact wavenumber are not critical factors and the interference by other molecules is minimal.

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Chapter 3. Extinction of Infrared Solar Radiation by Aerosols on a Tangent Path Through the Stratosphere

3.1 Introduction

In order to determine the effect of aerosols on a beam of infrared radiation, it is necessary to know the complex index of refraction of the aerosol and its particle size distribution. Since the stratospheric aerosol probably contains several or all of the following constituents; H_2SO_4 , $(NH_4)_2SO_4$, H_2O_2 , HNO_3 , $NOHSO_4$ and HNO_3 - H_2SO_4 - H_2O (Remsberg, 1971) a precise calculation would involve knowing the relative amounts, particle size distribution and complex index of refraction of each of these constituents.

As an initial calculation, the infrared extinction due to two greatly simplified models of stratospheric aerosol, containing only aqueous solutions of sulfuric acid (Remsberg, 1973), was determined.

3.2 The Aerosol Model

The stratospheric aerosol model discussed by Remsberg (1973) was used in this calculation. It is a bi-model distribution described by the equations (see also fig. 3.1):

$$\frac{dN}{d(\log r)} = 10^4 \qquad 0.03 \le r \le 0.05 \,\mu\text{m} \qquad (3.1)$$

$$\frac{dN}{d(\log r)} = 10^{+3.72} r^{+4.19} \qquad 0.1 \le r \le 0.3 \,\mu\text{m} \qquad (3.2)$$

$$\frac{dN}{d(\log r)} = 10^{-0.474} r^{-3.82} \qquad 0.3 \le r \le 1 \,\mu\text{m} \qquad (3.3)$$

The particle number density in each size range, obtained by integrating the above equations, and the mass density in each size range, obtained from:

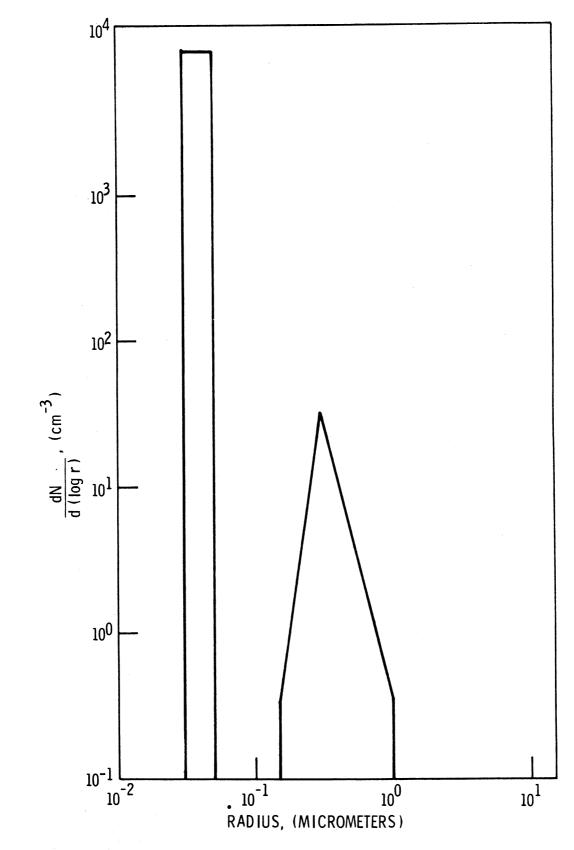


Fig. 3.1 Bi-model aerosol size distribution used for tangent path extinction calculations (after Remsberg, 1973).

$$M = \frac{4}{3} \int_{r_1}^{r_2} \pi^3 \frac{dN(r)}{dr} dr$$
 (3.4)

with the density of sulfuric acid, $f = 1.8 \text{ g/cm}^3$, are:

r,μm.	.0305	.13	.3 - 1
N, cm3	2219.4	7.99	3. 76
M, gr.cm.	1.077.10 ⁻¹²	0.414·10 ⁻¹²	2. 258· 10 ⁻¹²

The model contains a fairly large number of Aitken nuclei, however not as many as indicated by DeBary and Rossler (1970). The mass density M is intermediate between values given by DeBary and Rossler and by Lazrus (1971). The model, then may represent an average condition in the stratosphere. Larger numbers of particles would exist after volcanic explosions.

The relative altitude distribution f_k used for this calculation is shown in figure 3. 2 and is similar to that measured by Chagnon and Jung (1961). In the altitude range 17-22 km., the number of particles is the exact number (N_{max}) given by the equations 3. 1 to 3. 3. At all other altitudes the total number is scaled by the ratio given in figure 3. 1 (i. e. $N = f_k N_{max}$) however the relative size distribution is not changed. Note that the aerosol density has been assumed to be constant in one kilometer layers.

The length of a slant path through a 1 km spherical shell layer in the atmosphere is given by (neglecting refraction) (Drayson, et. al. 1972).

$$\Delta X_{k} = 2 \left(\sqrt{R_{k+1}^{2} - R_{o}^{2}} - \sqrt{R_{k}^{2} - R_{o}^{2}} \right)$$
 (3.5)

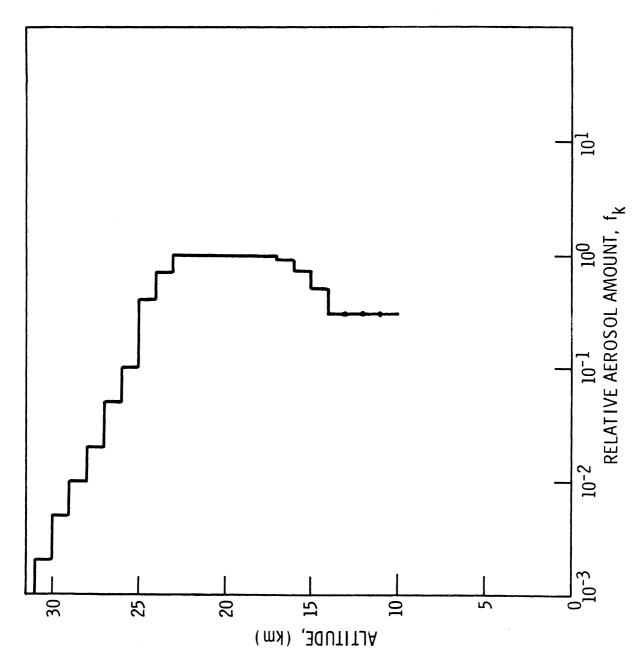


Fig. 3.2 Relative altitude distribution of aerosols, f_k , used for tangent path extinction calculations.

between the altitudes specified by radial distances R_{k+1} and R_k . The total amount of aerosol traversed along the tangent path is:

$$D = \sum_{k} f_{k} \Delta X_{k}$$
 (3.6)

where D has units equal to km, of aerosol of number density given by equations 3.1 to 3.3. That is, equivalent km. of aerosol at the concentration N_{\max} . A curve of the values of D versus tangent altitude is given in figure 3.3. It can be noticed that the shape of D vs. tangent altitude is vaguely similar to the curve of f_k vs. altitude.

3.3 Optical Characteristics of Aqueous $H_2 SO_4$

Values of the real and imaginary parts of the complex index of refraction of 75% and 90% aqueous solutions of $\rm H_2SO_4$ (Remsberg, 1971) are given in table 3.1 and figures 3.4 and 3.5 for the wavenumber range 750 to 1570 cm $^{-1}$.

Extinction coefficients for the aerosol of size distribution specified above, calculated from the relation:

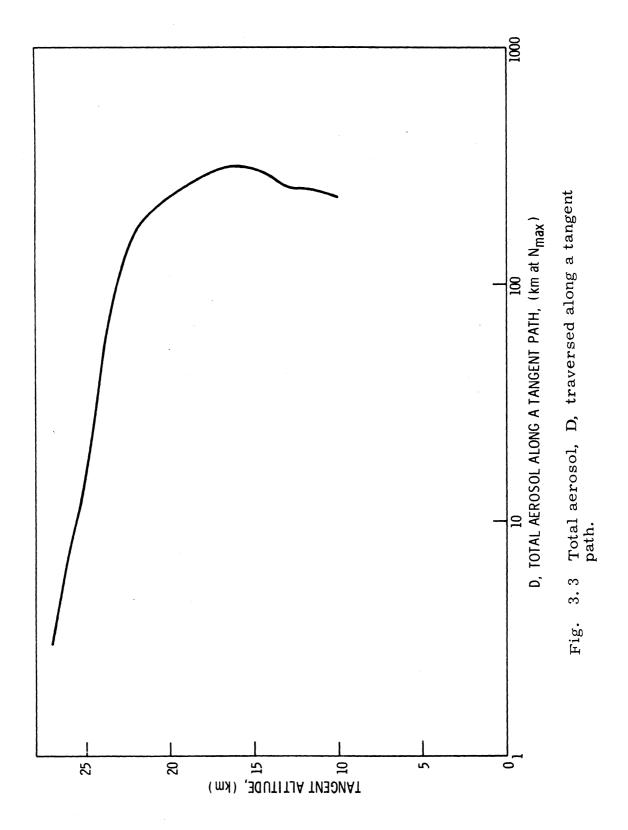
$$B_{\text{ext}}(\lambda) = \int_{r_1}^{r_2} \pi^2 Q_{\text{ext}}(r, \lambda, \hat{n}) \frac{dN(r)}{dr} dr \qquad (3.7)$$

where $Q_{\rm ext}$ (r, λ , \hat{n}) is the efficiency factor calculated from Mie theory of scattering, are given by Remsberg(1973) for 75% and 90% H_2SO_4 for the wavenumber range 750 to 1150 cm⁻¹ (see figures 3.6 and 3.7).

Approximate extinction coefficients for the range 1150 to 1570 cm⁻¹ were determined using relations given by Remsberg (1973), i.e.:

TABLE 3.1 $\label{eq:constants} \text{Optical Constants } (\mathring{n} = \text{n-ik}) \text{ of Aqueous } \text{H}_2\text{SO}_4$

	u	1. 51173	7.17	900	550	190	743	365	$\frac{110}{2}$	902	654	. 5662	937	. 7968	525	1.92317	433	072	684		. 7985	. 7719	702	822	1.83406	598		352	1.94322	459	1.92861	190	1.86844	7 . 7	1.81158	683	359	013	687	369	135	1.59681	838				
	뇌	37559	20	5	4,	45	\sim	25	25	82	02	0	31	22	30	22	11	29	23	46	37	72	07	30	. 55422	48	26	58	15	65	. 33020	8	. 23288	5	8	86	61	64	27	.16121	99	13					
4	FREQ	33.	1023.7	4.	. 2	ci.		si.	7	_;	۲.	ς.	θ.	_;	9	б	4	8	æ	6	S.	ω.	4.	_;	4.	7	6	Ξ.	۲.		0	4.	865.3	6		ო.	٥.	6	3	۲.	0	4;	۲.				
90% H ₂ SO	u	(7)	9	ഗ	1, 18325	1.11536	1.01961	. 99501	1.01282	1.06756	0	1, 15374	1, 24597	1,27375	1,30709	1,32172	1,30987	1, 29498	1,25624	1, 24231	1, 23318	1, 21762	\sim	1.24946	1.27660	_	1,38008	1, 43635	1,49979	1.54355	1,58053	1,60280	1.61745	1.63732	1.66145	1.67053	9	1,64046	-	~	$^{\circ}$		-	1,52266			
	k	. 06519	8	33	04000	08932	.16894	. 22500	.35646	. 43227	. 46363	48821	47339	46908	43757	38449	35226	33114	34575	38496	42762	49547	. 54171	. 60234	.63789	. 67201	69005	. 70626	. 68149	. 67557	. 63875	. 62270	. 60050	. 56369	. 49683	. 45509	. 41969	. 38950	61	582	. 39423	030	256	. 40177			
	FREQ	70.	0.	93.	56.	4.	15.	08.	95.	84.	77.	71.	58.	52.	42.	33	5 2	10	85.	.99	47.	24.	14.	02.	195.	90.	80.	72.	63.	56.	48.	40.	1136.8	33.	20.	11.	02.	94.	82.	72.	65.	56.	48.	1040.6			
	u	1, 29568	1.34542	1. 26802	1, 19644	1.12007	1.11362	1.13369	1,16010	1, 21735	1, 31945	1,40849	1, 49183	1, 59253	1.63027	1 62611	1 59725	1 57582	1.55688	1.56030	1 60811	1.63656	1, 76056	1.82434	1,88088	1,88976	1,87327	1,83372	1,77328	1, 73457	1, 67112	1.64740	1,62958	1,67483	1, 73149	1, 78764	24	398.	. 834	808	808	· u,	751	1. 72780		6	1.64731
75% H ₂ SO ₄	Դ	.14352	. 13326	48	89	77	20	27	20	92	46	99	96	45	83	42	5.5	8	4	29	62	46	81	41	38	70	30	53	15	89	98	27	. 48341	72	97	88	57	41	29	8	11	61	7	36	34	39	515
	FREQ									209.	184		150	13.5	114	104	094	200	070		050	053		032	019.		004.						920.3														



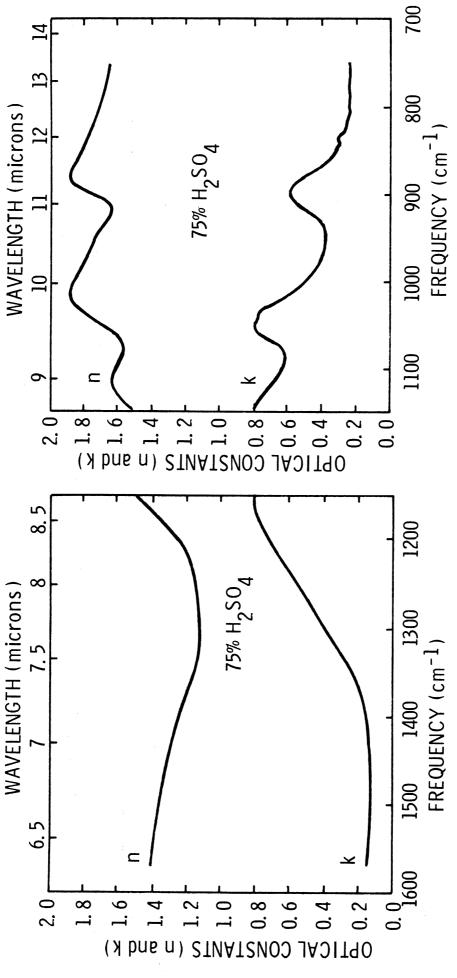
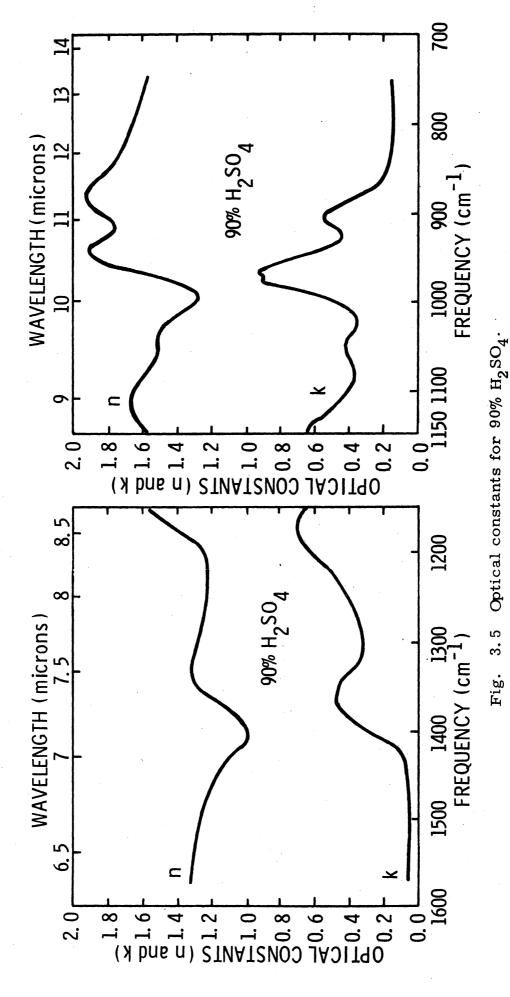


Fig. 3.4 Optical constants for 75% $\rm H_2SO_4$.

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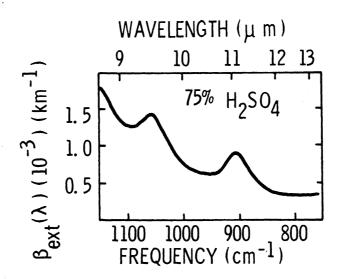


Fig. 3.6 Spectral extinction coefficient for 75% H_2SO_4 (Remsberg 1971).

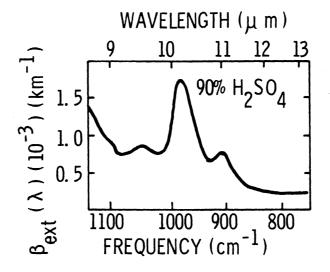


Fig. 3.7 Spectral extinction coefficient for 90% H_2SO_4 (Remsberg 1971).

$$Q_{\text{ext}} = Q_{\text{abs}} + Q_{\text{sca}} \approx Q_{\text{abs}}$$
 (3.8)

since:

$$Q_{sca} < Q_{abs}$$
 (3.9)

in the wavenumber range of interest. Also:

$$Q_{abs} \approx 24 \, \text{nk} \quad \left(\frac{2 \, \text{Tr}}{\lambda}\right) \int (n^2 - k^2 + 2)^2 + 4n^2 k^2 \int^{-1} (3.10)$$

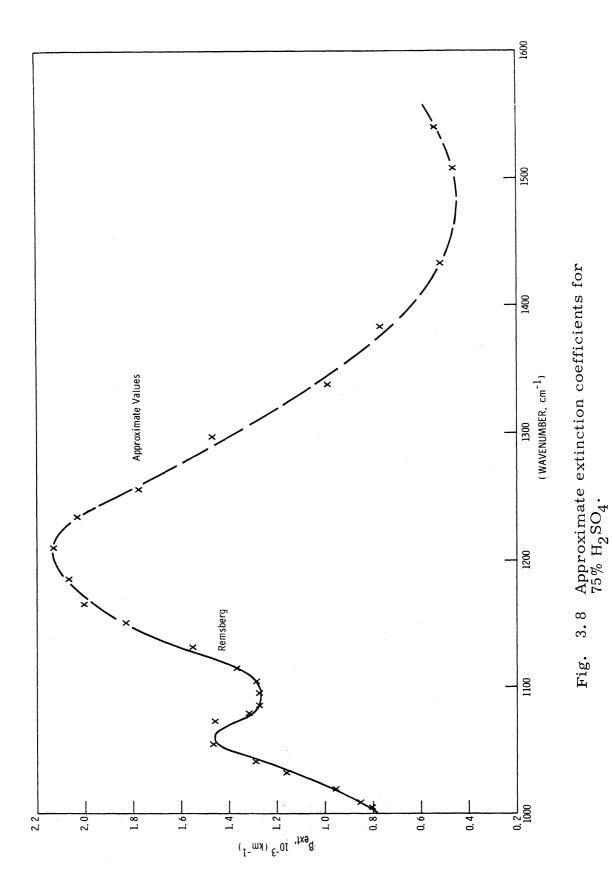
$$B_{ext}(\lambda) \approx \frac{48 \, \text{Tnk}}{\lambda} \int (n^2 - k^2 + 2)^2 + 4n^2 k^2 \int^{-1} r^2 \int_{r_1}^{r_2} \pi^3 \frac{dN(r)}{dr} dr$$

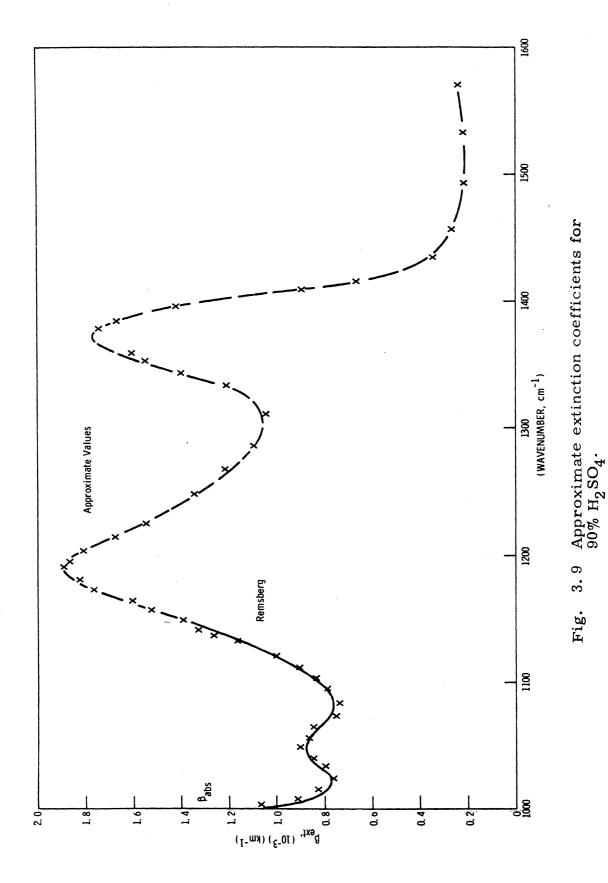
$$(3.11)$$

then:

$$\frac{B_{\text{ext}}^{(\lambda_1)}}{B_{\text{ext}}^{(\lambda_2)}} = \frac{\left\{\frac{nk}{\lambda} \left[(n^2 - k^2 + 2)^2 + 4n^2 k^2 \right]^{-1} \right\}}{\left\{\frac{nk}{\lambda} \left[(n^2 - k^2 + 2)^2 + 4n^2 k^2 \right]^{-1} \right\}}$$
(3.12)

Approximate extinction coefficients for 75% and 90% $\rm{H_2SO_4}$ were calculated from equation 3.12, using Remsbergs $\rm{B_{ext}}$ at 1150 cm⁻¹ as a reference value. The approximate extinction coefficients calculated in this fashion are shown in figures 3.8 and 3.9, Remsbergs values and the approximate values are compared in the wavelength range 1000-1150 cm⁻¹. Note the excellent agreement in the range of overlap between the two sets of values.





3.4 Infrared Transmissivities along Tangent Paths

The infrared transmissivity of a tangent path through the aerosol layer was calculated by the equation:

$$T(\lambda) = \exp \left[-B_{\text{ext}}(\lambda) \cdot \sum_{k} f_{k} \Delta X_{k} \right]$$
 (3.13)

for several paths tangent in the range of altitudes 16-26.6 km. The results are shown in figures 3.10 and 3.11 for 75% and 90% $\rm H_2SO_4$, respectively.

3.5 The Extinction of Infrared Solar Radiation

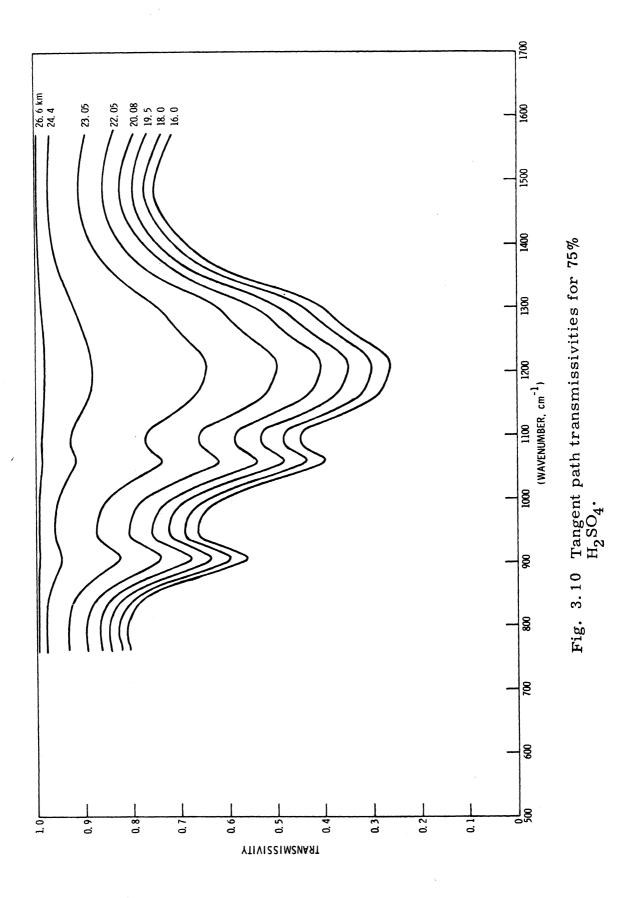
The extinction, due to the aerosol models described above, of solar infrared radiation along paths through the earth's atmosphere was calculated from the equations

$$I(\lambda) = T(\lambda) \cdot B(\lambda, T_S)$$
 (3.14)

where I(λ) is the spectral intensity (spectral radiance) of the solar radiation after traversing a tangent path through the earth's atmosphere, $T(\lambda)$ is the transmissivity defined above and $B(\lambda, T_S)$ is the radiance of the photosphere of the sun, assumed to be a blackbody at temperature $T_S = 5036^{\circ} K$ (Saiedy and Goody, 1959). Figures 3.12 and 3.13 show the results for tangent paths at altitudes of 16 to 26.6 km for 75% H_2SO_4 and 90% H_2SO_4 .

Discussion of Results:

The results shown above indicate the significant difference between the absorption of 75% and 90% aqueous solutions of $\rm H_2SO_4$, each with the same particle size distribution and with the same relative



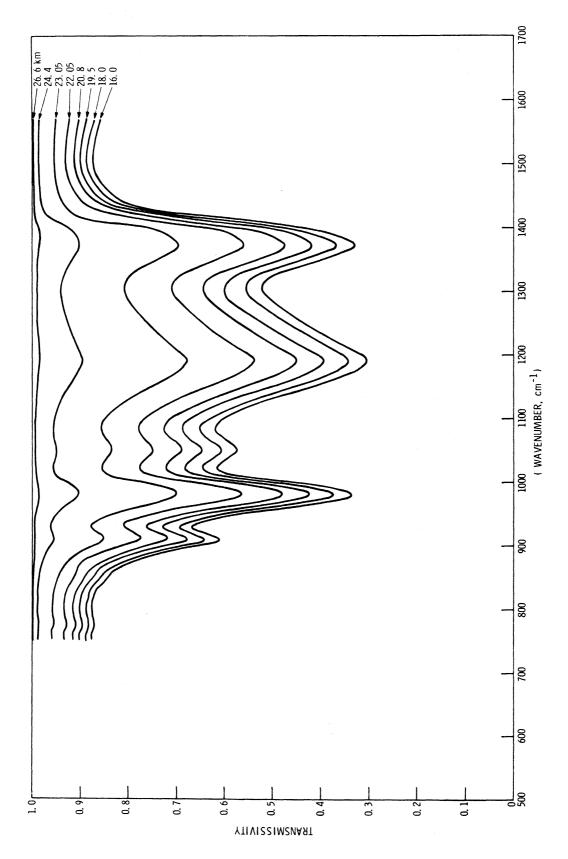


Fig. 3.11 Tangent path transmissivities for 90% $\rm H_2SO_4.$

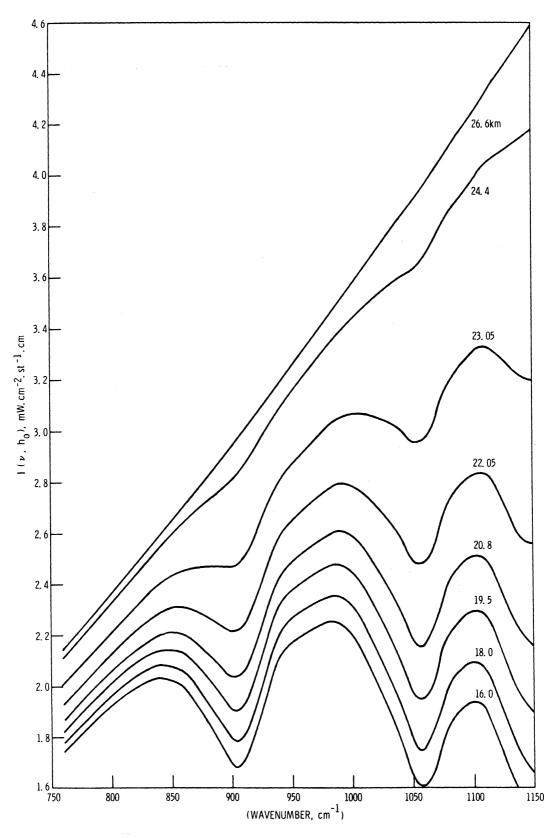


Fig. 3.12 Extinction of solar infrared radiation, by aerosols, on tangent paths through the earth's atmosphere (75% H₂SO₄).

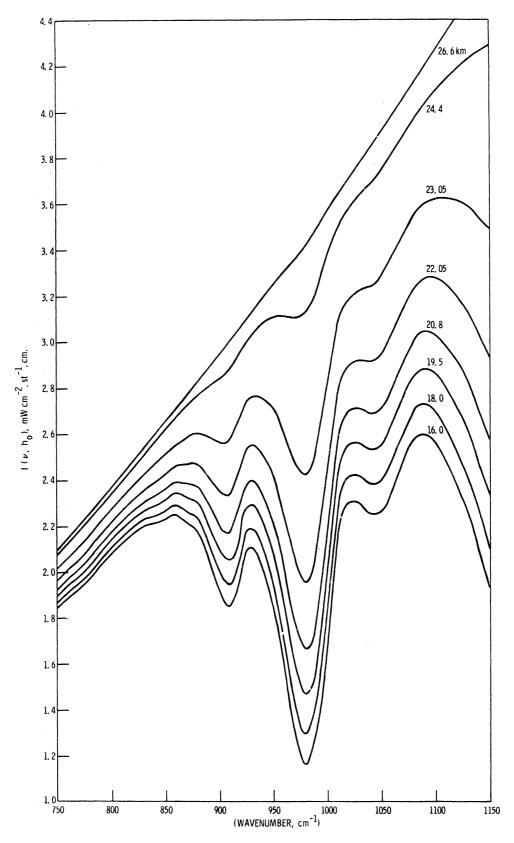


Fig. 3.13 Extinction of solar infrared radiation, by aerosols, on tangent paths through the earth's atmosphere (90% $\rm H_2SO_4$).

number distribution as a function of altitude. The differences in complex index of refraction are reflected in turn in extinction coefficients, transmissivities for tangent paths through the atmosphere and in solar radiation intensities after traversing tangent paths.

The 75% $\rm H_2SO_4$ aerosol shows strong absorption bands centered at 900 cm⁻¹, 1060 cm⁻¹ and 1200 cm⁻¹. There is strong absorption near these wavenumbers for 90% $\rm H_2SO_4$ as well (the bands are shifted slightly, they appear to be centered at 908 cm⁻¹, 1050 cm⁻¹ and 1150 cm⁻¹). In addition, 90% $\rm H_2SO_4$, shows great absorption at 980 cm⁻¹ and 1375 cm⁰¹.

Measurements of solar radiation in the window region of the spectrum through tangent paths in the atmosphere should provide an excellent measurement of the extinction of stratospheric aerosols, although the absorption at 1050 cm $^{-1}$ will be almost completely masked by absorption due to the ν_3 band of $\rm O_3$ at 1042 cm $^{-1}$. The absorption of either 75% $\rm H_2SO_4$ or 90% $\rm H_2SO_4$ at the 900 cm $^{-1}$ wavenumber region should be clearly noticeable in window region measurements.

The 980 cm $^{-1}$ and 1375 cm $^{-1}$ absorption may also be recognizable in tangent path spectra although the former may be interfered with by the 1042 cm $^{-1}$ O_3 , 961 cm $^{-1}$ CO_2 and the 884 cm $^{-1}$ HNO $_3$ absorption regions, and the latter may conflict with 1594 H $_2$ O, 1306 CH $_4$, 1285 N $_2$ O and 1333 HNO $_3$.

3.6 Additional Calculations and Improvement of the Model

Additional calculations should be made for 75% and 90% ${
m H_2SO_4}$ with other aerosol size distributions. A mixture, in equal amounts, of 75% and 90% ${
m H_2SO_4}$ should also be considered.

The exact nature of this mixture is an interesting problem in itself. Would such a mixture contain 50% of each 75% and 90% aqueous ${\rm H_2SO_4}$ for each particle size? Or would the smaller sizes tend to be mostly or all 90% ${\rm H_2SO_4}$, with larger sizes being 75% ${\rm H_2SO_4}$? Calculations can be made for both possibilities, however the physical process describing the formation of the aerosol particles should shed some light on this question.

The aerosol model should be improved by adding the effects of the other most likely constituents $(\mathrm{NH_4})_2\mathrm{SO}_4$, $\mathrm{H_2O}_2$, HNO_3 , NOHSO_4 , and HNO_3 - $\mathrm{H_2SO}_4$ - $\mathrm{H_2O}_2$.

The altitude range of the model should be increased to include effects at 50 km, where a secondary aerosol layer may cause noticeable absorption on tangent paths through the atmosphere (Elliott, 1970).

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Chapter 4. INVERSION PROCEDURES

4.1 Introduction

This chapter deals with the inversion procedures, by which the atmospheric concentration of the absorbing species can be obtained from the solar occultation measurements of the radiant intensity I. The problems of inversion for atmospheric temperature from radiance measurements have been studied by many authors. (Kaplan 1959, King 1964, Wark and Fleming 1966, Smith 1972, Chahine 1968, Gille 1968, Burn and Uplinger 1970, Rodgers 1970, Wark 1970, McKee and Cox 1973). Inference of water vapor and ozone from radiance measurements have been reported by Yamamoto and Tanaka (1966), Venkateswaran et al. (1961), Conrath (1969), House and Ohring (1969), Prabhakara et al. (1970), Smith (1970).

For the solar occultation experiment the maximum intensity (I_{∞}) is obtained when the measurement is made at maximum tangent heights and there is essentially no atmospheric absorption. The problem reduces to one of obtaining the concentration of species from the atmospheric transmittances ($T = I/I_{\infty}$), since emission from the atmosphere is very small and can be safely neglected in comparison to the total intensity. Rayleigh scattering at the spectral regions we are interested in is also small. Mie scattering by aerosols becomes important below tangent heights of approximately 30 km. and has to be included in the calculations. (See Chapter 3)

We have seen from the previous chapters how the calculation of the atmospheric transmittance is very complicated. Not only is the distribution of absorbing constituents required for such a calculation but also the atmospheric pressure and temperature distribution is required. Calculations of transmittances for the $15\mu\mathrm{m}$ band of CO_2 have been published by Drayson (1966) and Kunde (1967). These calculations require a detailed knowledge of the line positions, strengths, widths of the spectral lines in the region studied and also involve a large amount of computer time for the calculations. Therefore in cases where no such detailed knowledge of the spectral band is available or when use of large amounts of computer times is prohibitive, simplified calculations of atmospheric transmittance using Band Models have been used. (Goody 1964).

Because of this factor we have decided to try out the inversion procedures assuming that the transmittances can be calculated by the strong line approximation where the absorption is proportional to the square root of the optical mass.

$$T = 1 - 2 \cdot \sqrt{S \cdot \overline{u} \alpha / \delta}$$
 (4.1)

where S, α and δ are the strength, half-width and spacing between lines and \overline{u} the optical mass, is the sum over all layers along line of sight

$$\overline{u} = \sum u \tag{4.2}$$

The half-width is proportional to pressure

$$\alpha = \alpha_0 \cdot \overline{p} \tag{4.3}$$

where \overline{p} is the equivalent or mean pressure for the entire path

$$\overline{p} = \sum_{i} p. u / \sum_{i} u$$
 (4.4)

and similarly \overline{t} is the equivalent temperature

$$\overline{t} = \sum_{i} t \cdot u / \sum_{i} u$$
 (4.5)

However it is easy to incorporate the detailed calculation of transmittances instead of the above strong line approximation at a latter stage.

4.2 Geometry and Technique

Consider one absorbing constituent in the spectral region of interest and the atmosphere, spherically stratified and symmetric is divided into n thin concentric spherical shells. Horizontal gradients in temperature and pressure have been considered in the calculations by Davis (1969). Measurements of radiant intensity are made at n tangent heights where the line of sight from satellite to the sun passes through an increasing amount of atmosphere and number of shells as occultation proceeds. The tangent height is defined as the minimum altitude of the line of sight from the earth's surface. The pressure temperature and mixing ratio of constituent is assumed constant within each shell. For all inversion methods an assumption of the absorber concentration above the top most shell is necessary for accurate inversion at the upper tangent heights.

We have measured transmittances

$$T_{m_i}$$
, $i = 1$, n (4.6)

and we are to determine the mixing ratio in each of these shells.

$$C_{i}$$
, $i = 1$, n (4.7)

One can formulate mathematically

$$T_{m_i} = F_i (C_j, j i) i = 1, n$$
 (4.8)

where the function \boldsymbol{F}_i depends on tangent height and hence the temperature and pressure variations in the atmosphere. There is not contribution from the atmosphere below the tangent ray and thus for the shell

at the top of the atmosphere

$$T_{m_1} = F_1 (C_1)$$
 (4.9)

Figure 4. 1 shows the geometry of the occultation experiment.

4.3 Methods of Inversion

"Onion Peeling"

The onion peeling method developed by Russell (1970), McKee et al. (1969), Russell and Drayson (1972) starts the inversion at the topmost layer, and after the concentration in the first shell is obtained the procedure is carried out for the next lower shell and so on until the lowest shell.

We assume a concentration C_1 for the topmost shell and calculate $\boldsymbol{T}_{\boldsymbol{c}_1}$. If the assumed concentration is close to the actual, that we can make a linear approximation between measured

transmittance
$$T_{m_1}$$
 and calculated transmittance T_{c_1}

$$T_{m_1} = T_{c_1} + \left[\frac{\partial T_{c_1}}{\partial C_1}\right] \cdot \Delta C_1 \qquad (4.10)$$

The partial derivative is calculated and the perturbation parameter is determined from

$$\Delta C_{1} = \Delta T_{1} / \left[\frac{\partial T_{C_{1}}}{\partial C_{1}} \right]$$
 (4.11)

where
$$\Delta T_1 = T_{m_1} - T_{c_1}$$

This value of ΔC_1 is added to the original assumed concentration \mathbf{C}_{1} and the process if repeated until a desired convergence criteria is met. The procedure is next carried out for shell 2. It is convenient to assume the initial guess for C2 equal to the above C1 obtained

after inversion. The process is repeated and continues downwards one shell at a time to the lowest shell.

The measurements $T_{m_{\hat{1}}}$ inevitably contain errors, like radiant intensity bias errors, scale errors and random noise errors. Besides these there are errors in the determination of tangent heights, atmospheric pressures, temperatures and knowledge of absorption line parameters, etc. The effect of random noise errors can be reduced by either smoothing the input transmittances or smoothing the retrieved profile.

Eigenvectors and Smoothing Matrix Methods

The method of eigenvectors has been developed by Mateer (1964) and used by Russell and Drayson (1973). We can write n equations.

$$\Delta T_{i} = \sum_{k=1}^{n} \frac{\partial T_{c_{i}}}{\partial C_{k}} \cdot \Delta C_{k}$$
 (4.12)

or in matrix form

$$\Delta T = B \cdot \Delta C \tag{4.13}$$

The least squares solution is given by

$$\Delta C = (B'B)^{-1} \cdot (B' \cdot \Delta T) \tag{4.14}$$

$$B' \cdot \Delta T = \sum_{i=1}^{n} b_i \cdot v_i$$
 (4.15)

where b_i are constants for each eigenvector. The constants b_i are determined by solving the $\, n \,$ above equations. We have

$$\Delta C = (B' \cdot B)^{-1} \cdot B' \cdot \Delta T$$

$$= (B' \cdot B)^{-1} \cdot \sum_{i=1}^{n} b_{i} v_{i} = \sum_{i=1}^{n} \frac{b_{i}}{\lambda_{i}} \cdot v_{i}$$

$$(4.16)$$

Now the errors in measurements incorporated in \mathbf{T}_{m_i} and the errors in calculations incorporated in \mathbf{T}_{c_i} , the partial derivatives $\frac{\partial^T c_i}{\partial C_k}$, B, B' are all contained in the constants \mathbf{b}_i . Therefore we can write

$$\Delta C = \sum_{i=1}^{n} \frac{b_{i}'}{\lambda_{i}} \cdot v_{i} + \sum_{i=1}^{n} \frac{e_{i}}{\lambda_{i}} \cdot v_{i}$$
 (4.17)

where b_i' are values of constants with no error, and e_i are the error terms. If λ_i are ordered in decreasing magnitude, for larger i, λ_i may be very small, and error terms will then be large. Inclusion of eigen-vectors v_i corresponding to the smaller λ_i gives the details of the solution which may or may not be due to noise, and cause instability or erroneous results when noise is present. We therefore truncate and use only a limited number of terms, so as to control the noise. The selection of where to truncate depends on a priori knowledge of the amount of noise present. To trucate too much would mean inferior results due to elimination of valid information.

Another technique of smoothing (Wark and Fleming 1966) is to introduce a smoothing matrix H and a smoothing parameter γ . The selection of appropriate values for H and γ has been discussed in papers by Phillips (1962) and Twomey (1963). The solution is given by

$$\Delta C = (B' \cdot B + \gamma H)^{-1} \cdot B' \cdot \Delta T \qquad (4.18)$$

Increasing smoothing by increasing γ , makes the solution more dependent on matrix γ H. If H is the identity matrix, the method is related to the eigenvector expansion since the eigenvectors of B'B + γ H are the same as those of B'B and the eigenvalues are λ_i + γ . The eigenvector expansion is not truncated but is replaced by the expression

$$\Delta C = \sum_{i=1}^{n} \frac{b_i}{\lambda_i + \gamma} \cdot v_i \qquad (4.19)$$

However the eigenvalues never become smaller than γ and the problem of amplification of the noise may be controlled by choosing a sufficiently large value of γ .

If the matrix B'B is non-singular, solution with γ = 0 corresponds exactly to the eigenvector method with all terms included.

Kalman-Bucy Filter

Gray et al. (1973) have discussed a technique of smoothing using the Kalman Bucy filter. This technique (as also the above two methods) is efficient when the initial guess of constituent density C_i is close to the actual value and the linear relation between T_{m_i} and T_{c_i} is valid. The method assumes an initial guess of concentration C_i and updates this state vector after each measurement by calculating the "filter gain" (Newell and Gray 1972) vector K_i

$$K_{i} = P_{i-1} \cdot B'_{i} \left[B_{i} \cdot P_{i-1} \cdot B'_{i} + R \right]^{-1} \qquad (4.20)$$
where B'_{i} is the transpose of vector $B_{i} = \begin{bmatrix} \frac{\partial T_{c_{i}}}{\partial C_{1}}, \frac{\partial T_{c_{i}}}{\partial C_{2}} & \frac{\partial T_{c_{i}}}{\partial C_{i}}, 0 \dots \end{bmatrix}$

R is the noise covariance and P_{i-1} is the covariance matrix which is originally assumed and updated after each measurement by

$$P_{i} = P_{i-1} - K_{i} \cdot B_{i} \cdot P_{i-1}$$
 (4.21)

71

The state vector is updated

$$C_{i} = C_{i} + K_{i} \cdot \Delta T_{i}$$
 (4.22)

The three matrix methods, i. e. the truncated eigenvector expansion, the smoothing matrix and the Kalman Bucy filter, have a common characteristic. The initial guess of the concentration profile is modified only if the measurements indicate a real deviation from the initial profile. Thus if the absorption is very small at the upper levels the measurements contain mostly noise and little information and the inversions show little modification of the initial guess at these levels. Similarly if the absorption is almost complete at the lower levels the measurements also contain little information on the concentrations and the initial guess again retained.

Abel Equation

The Abel integral equation

$$X_{i} = 2 \int_{r_{i}}^{\infty} \frac{x(r) \cdot r \cdot dr}{\sqrt{r^{2} - r_{i}^{2}}}$$
 (4. 23)

has been inverted (Roble and Hays 1972) and the inversion for constituent profiles has been tried. The values of $X_i = (\overline{u}_i . \overline{p}_i)$ are determined from the measured transmittances T_m .

$$X_{i} = \overline{u}_{i} \cdot \overline{p}_{i} = \left\{ (1 - T_{m_{i}}) \cdot \delta / 2 \right\}^{2} / (S \cdot \alpha_{o}) \quad (4.24)$$

The solution for x (r) is given by

$$f(\mathbf{r}) = -\frac{1}{\pi} \int_{\mathbf{r}}^{\infty} \frac{dX_i / dr_i}{\sqrt{r_i^2 - r^2}} \cdot dr_i$$
 (4. 25)

where x(r) is the product of C and p.

The values for X_i are discrete, since measurements are made at selected tangent heights only. Between individual data points, X_i is assumed to have an exponential variation given by

$$X_{i}(r) = A_{i} \exp \left[-B_{i}(r-r_{i})\right]$$
 (4. 26)

where the coefficients A_i and B_i are chosen to fit the data with desired amount of smoothing incorporated . Thus for smoothing M/2 data points on either side of the i-th data point, A_i and B_i are calculated so as to fit the data from (i-M/2) to (i + M/2) in a least squares sense with a minimum variance.

$$\sigma_i^2 = \sum_{k=(i-M/2)}^{(i+M/2)} \left[X_k - A_i \exp \left\{ -B_i (r_k - r_i) \right\} \right]^2$$
 (4.27)

Now the derivative dX/dr near the i-th data point is given by

$$\frac{dX}{dr} = -A_i \cdot B_i \exp \left\{ -B_i (r-r_i) \right\}$$
 (4.28)

Substituting the above expression and replacing the integral by a finite sum, the solution for $x(r_{\ell})$ can be written as

$$x (r_{\ell}) = \frac{1}{\pi} \sum_{i=\ell}^{1} A_{i} \cdot B_{i} \int_{r_{i}}^{r_{i}} \frac{\exp \left[-B_{i} (r-r_{i})\right]}{\sqrt{r^{2}-r_{\ell}^{2}}} \cdot dr$$
 (4. 29)

where
$$r_{\ell} = r_{\ell}$$
, $r_{i} = (r_{i} + r_{i+1})/2$ and $r_{i} = (r_{i-1} + r_{i})/2$

Roble and Norton (1972) have discussed the evaluation of the integral in the above equation. From the values of x, the constituent profile C is obtained.

It is important to note that the use of the Abel Integral equation as developed in this section is dependent on the strong line approximation contained in equation (4. 24). In the other inversion

methods the approximation was used as a convenience in testing the procedures to avoid lengthy transmittance calculations but is an essential part of the development of the Abel equation inversion. The prospects appear poor for modification to the more general situation where the strong line approximation is not valid. In order to do this we have to find an X_i which is a function of the measured transmittance and an x(r) which is a function of the concentration to use in equation (4.23). However transmittance is expressed as an integral over wavenumber of the monochromatic transmittance, which is itself an exponential of integral along the line of sight.

Robel and Hays (1972), working in the UV spectral region, were able to overcome this difficulty by assuming that the monochromatic transmittance was independent of wavelength over small wavelength regions and that other spectral parameters were independent of altitude. Both these approximations are invalid in the infrared region of the spectrum.

The errors in $T_{m_{\hat{1}}}$ will cause $X_{\hat{1}}$ and correspondingly the coefficients $A_{\hat{1}}$ and $B_{\hat{1}}$ to have included error terms. Roble and Hays (1972) have given expressions for the standard deviation of the retrieved constituent density errors due to statistical errors in the measurements.

4.4 Results and Discussion

Inversion for ${\rm CO_2}$ concentration in a 10 shell model atmosphere is tried as a first step. The atmosphere between 70 and 20 km. is divided into 10 shells each 5 km. thick. The atmospheric pressure and temperature at the mid-altitude of shell (from standard atmospheric tables) is used as the assumed constant pressure and

temperature in each shell. Assuming CO_2 mixing ratio of 320 ppm., "measured" transmittances T_{m_i} are generated at spectral region of 655 cm⁻¹ where S= 3.2 cm⁻¹(atm·cm)⁻¹ and α_0 = 0.07 atm⁻¹cm⁻¹.

The T_{m_1} are used in the inversion procedures to obtain the CO_2 mixing ratio in the atmosphere. The results are shown in Table 1. The onion peeling method requires an initial guess of mixing ratio at the topmost shell and is taken as 300 ppm. The other methods shown in Table 1 require an initial guess of the concentrations in all shells, and this guess is taken as 300 ppm. All techniques retrieve the 320 ppm. mixing ratio of CO_2 above 30 km. In the Kalman-Bucy filter technique a noise R= 1. E-14 is used to obtain results shown in Table 1.

In the eigenvector method, the last two eigenvalues are zero. As no noise in measurements (T_{m_i}) is assumed, we use the first eight eigenvectors for the calculation. In the smoothing matrix γ = 160, is used to obtain solution shown in Table 4.1. Further decrease in γ will improve the solution for the top 3 levels.

At tangent heights of 25 km. and below the atmosphere is opaque. (T_m =0) and retrievel of concentration of CO_2 in the last two shells is not possible because of lack of information.

Using the onion peeling technique, there is no retrievel for the bottom two shells because the partial derivative in the expression for C_i is zero. In the matrix methods as discussed earlier, the initial guess of concentration in the last two shells is retained as the measurements contain no information on the concentration.

To study the effect of random noise, the generated T_{m_i} are rounded off to the second decimal place, and the inversion procedures

are tried using the same initial guesses of CO₂ mixing ratio. The onion peeling method retrieves the concentration profile fairly accurately between altitudes 50 and 30 km. At the top of the atmosphere there is larger error because here even for comparatively large changes in mixing ratio of CO₂, the transmittance does not change very significantly. No smoothing of retrieved profile is incorporated in the results shown for the onion peeling method, so that the noise dominates.

The results from the eigenvectors method using 5 eigenvectors to calculate the solution are shown in Table 1. The 10 eigenvalues and eigenvectors of matrix B'B are shown in Table 4.2. We see that eigenvalues λ_9 and λ_{10} are 0, and λ_8 is approximately 10^4 times smaller than λ_1 and the inclusion of the smaller eigenvalues λ_8 and λ_7 in the calculation contributes little to actual solution but will greatly increase the error terms. Truncation after 5 eigenvectors gives a solution which appears the closest to the actual solution we desire of 320 ppm., the maximum deviations being + 19 and -20 ppm. The improvement and subsequent worsening of solution as the number of eigenvectors(and eigenvalues) used is increased is shown in Table 3. The retrievel of CO_2 profile is best between 50 and 30 km. where the information content of data is maximum. An idea of the information content of the measurements can be obtained by studying the eigenvectors and locating the largest terms in each vector.

Results from the smoothing matrix method, using the identity matrix for H and γ = 6800. are shown in Table 1. Various other values for γ are tried. The value 6800. corresponds to the 5-th eigenvalue λ_5 of (B'B) and we see the solution is very close to that obtained from the eigenvector method truncated after 5 eigenvector terms.

In performing the eigenvector and smothing matrix methods we tacitly have assumed a linear approximation for the relationship between T_{m_i} , T_{c_i} and C_i . If our initial guess of constituent profile is not close to the actual, such an approximation is not valid. It is desirable to perform an itterative procedure similar to the one carried out in the onion-peeling method. For each new itteration, the initial guess of concentration is the one calculated in the previous itteration. The itterative procedure is continued until a desired convergence criteria is met.

The solutions from the Kalman Bucy filter technique are consistent with results from the other methods (Table 1). A noise of R=1.E-12 is used in Table 1 for inversion using $T_{m_{\hat{1}}}$ with random error. The selection of the initial covariance matrix and the value of R for given data and the effect of these quantities on the inversion is being studied.

A similar set of calculations for CO inversion in a 10 shell model atmosphere from 55 to 5 km. with 5 km. thick shells are shown in Table 4. Results of inversion for ${\rm CO_2}$ in a 22 shell atmosphere using the Abel equation technique are shown in Table 5. Results from Abel equation inversion for ${\rm CO_2}$ using a 10 shell atmosphere with 5 km. thick shells (not included) are poor because of the assumptions made in calculating ${\rm T_{m_i}}$.

By using the simple closed form expression for calculation of transmittances T_{c_i} , we were able to calculate the partial derivatives $\delta\,T_{c_i}\,/\delta\,C_K$ quite easily. When using the more detailed methods for calculating T_{c_i} , the partial derivatives have to be calculated by using the finite defference approximation $\frac{\delta\,T_{c_i}}{\delta\,C_K}$. This

requires calculating the transmittance with a small perturbation of assumed concentration in the shells. This procedure is very time consuming when the exact expressions for transmittance are used.

As seen above there are a variety of methods for inverting and smoothing of data. A particular technique may be ideal in some situations. In the inversion using the Abel equation no initial estimate of the constituent profile is necessary. This method although has some advantages is very difficult to apply in the case where we do not assume a simple closed form expression for transmittance. The technique using the Kalman Busy filter requires the additional calculations of the covariance matrices which is a drawback for quick calculations, although providing a more detailed description of the information content of the measurements. The smoothing matrix and eigenvector methods are very similar. The smoothing matrix method is the faster and more efficient technique while the eigenvector method gives more insight into the information content of the measurements. The onion reeling method is very simple and easy to apply. Incorporating smoothing of input transmittances or smoothing of retrieved constituent profiles, reduces the effect of random errors on the inversion.

The effect of other errors like bias and scale errors etc. will be further studied. Selection of an initial estimate of the constituent profile, which should be close to actual constituent profile, required for some of the inversion techniques is sometimes difficult to make. We have assumed n measurements, and n tangent heights. It would be preferable to have more measurements, from which the

random error component can be minimized. The selection of a model atmosphere and especially the thickness of shells is being further studied. Thick shells give coarse results with all the atmospheric fine structure of constituent profile hidden. Dividing the atmosphere into very thin shells is preferred but in some of the methods this could cause instability. Depending on the constituent profile, a model atmosphere consisting of shells of suitably varying thickness can be constructed, giving the fine structure by having thin shells where required, and eliminating problems of instability by having thick shells where necessary. Newell and Gray (1972) using the Kalman-Bucy filter point that in some cases to prevent premature convergence, the tangent height data was sampled in coarse intervals repeatedly. The above mentioned techniques can easily be extended to retrieve two and more constituents simultaneously. Study of inversion of aerosols and selection of the optimum amount of smoothing for given data and separation of noise from measurements will be continued.

TABLE 4.1

Inversion for CO_2 Mixing Ratio

T Calculated at 655 cm $^{-1}$ Using S = 3.2 cm $^{-1}$ (atm. cm) $^{-1}$, α_0 = 0.07 and Mixing Ratio of CO₂ of 320 ppm.

m	Smoothing Kalman	Matrix Filter	$\gamma = 6800$ R=1, E-12	306 478	314 488	301 297	321 340	324 333	313 317	316 318	323 325	300 300	300 300
Mixing Ratio ppm	Eigen-	Vector	(5 terms)	300	301	307	339	328	313	316	323	300	300
4		Onion	Peeling	505	4 92	270	339	32,9	313	316	324	1	ı
	${ m T}_{ m mi}$ with	Error		66.	86.	26.	. 94	68.	61.	.57	. 08	0	0
	Kalman	Filter	R=1. E-14	320	322	322	323	323	322	322	322	300	300
tio ppm	Smoothing	Matrix	γ=160	311	316	319	320	320	320	320	320	300	300
Mixing Ratio ppm	Eigen.	Vector	(8 terms)	320	319	320	320	320	320	320	320	300	300
		Onion	Peeling	320	320	320	320	320	320	320	320	•	1
		$T_{ m mi}$. 99204	. 98389	. 96887	. 94144	.89160	. 78849	. 56759	.08438	0	0
		Tangent Ht	km	65	09	55	20	45	40	35	30	25	20
		Shell	•,1	1	7	က	4	2	9	7	80	6	10

TABLE 4.2

Eigen Values and Eigen Vectors of Matrix B'B

 CO_2 Inversion

	1	2	င	4	5	9	2	8	6	10
Eigen values										
λi	1.8 x 10 ⁺⁶	1.8 x 10 ⁺⁶ 3.9 x 10 ⁺⁵	9.0 x 10 ⁴	2.3×10^4	6.8×10^3	1.9×10^3	5.5×10^2	1.6 x 10 ²	0	0
	000.0	0.000	00000	0,002	0.007	0.030	0,155	0, 988	0.0	0.0
	000°0	00000	0,002	0.008	0.032	0.152	0.975	-0.157	0.0	0.0
	0000	0,001	0.007	0.035	0,160	0.974	-0.158	-0.006	0.0	0.0
Eigen Vectors V.	0,001	900 0	0.030	0.167	0.971	-0.167	-0.007	-0.001	0.0	0.0
-	0.004	0.024	0.141	0.974	-0.174	-0.007	-0.001	-0.000	0.0	0.0
	0.020	0.125	0, 981	-0.146	900 0-	-0,001	-0.000	-0.000	0.0	0.0
	0.117	0,985	-0.129	900 -0-	-0,001	-0.000	-0.000	-0.000	0.0	0.0
	0,993	-0.118	-0.005	-0,001	-0,000	-0, 000	-0.000	-0.000	0.0	0.0
	0.0	0.0	-0.0	0.0	-0.0	0.0	-0.0	-0.0	1.000	0.0
	0.0	0.0	-0.0	0.0	-0.0	0.0	-0.0	-0.0	0.0	1,000

TABLE 4.3

Inversion of CO_2 Using Method of Eigen Vectors $\mathrm{T}_{\mathrm{mi}} \quad \mathrm{With \; Random \; Error}$

				Mixir	Mixing Ratio ppm.	ppm.				
No. Shell Of Eigen vectors included	1	2	က	4	5	9	2	8	6	10
1	300	300	300	300	300	301	303	325	300	300
23	300	300	300	300	300	302	318	323	300	300
က	300	300	300	301	303	318	316	323	300	300
4	300	300	301	306	334	314	316	323	300	300
ശ	300	301	307	339	328	313	316	323	300	300
9	300	301	305	340	328	313	316	323	300	300
7	330	492	274	338	328	313	316	323	300	300
8	479	468	273	338	328	313	316	323	300	300
6	ı	ı	i	1	ı	ı	1	1	1	ı
10	ı	ı	ı	ı	1	ı	ı	1	1	1

TABLE 4.4

Inversion for CO Mixing Ratio

T Calculated at 2173 cm $^{-1}$ using S = 9.0 cm $^{-1}$ (atm $^{-1}$ cm $^{-1}$) and α_{o} = .065

s Kalman Bucy Filter R = 1, E - 17	.118	.105	.0815	. 0502	. 0201	. 0217	.0351	. 0474	. 0613	. 081
Eigen Vectors Method (9 terms)	.129	.105	. 082	. 0502	. 0201	. 0218	. 0359	. 0479	. 0617	. 081
Onion Peeling	.119	.107	. 0821	. 0502	. 0202	. 0223	. 0360	. 048	. 0617	1
Initial guess of mixing ratio	.13	.11	. 081	.051	. 021	.03	. 041	.051	90.	. 081
Tmi with error used in inversion methods	866•	966•	. 993	686.	. 985	. 97	. 92	62.	. 52	0
T mi	. 99799	. 99611	. 99310	. 98905	. 98507	. 96582	. 91533	. 78508	. 52498	0
Mixing ratio ppm assumed for calculating Tmi	.12	.10	80.	. 05	. 02	. 03	. 04	• 05	90.	. 08
Tangent ht	50	45	40	35	30	25	20	15	10	5
Shell	.	73	က	4	2	9	7	80	6	10

TABLE 4.5

Inversion Using the Abel Equation

22 Shell Model Atmosphere

Smoothing Parameter M = 2

${ m CO_2}$ mixing ratio	ı	ľ	ı	74	165	232	183	158	294	350	273	304	332	331	339	340	336	339	338	ı	•	•
T_{mi}	. 997	966 •	. 995	. 994	. 993	. 992	. 991	686.	. 987	986	. 984	. 981	626.	926.	. 973	696	. 965	096.	. 955	. 949	. 942	. 934
Tangent ht km	69	89	19	99	65	64	63	. 62	61	09	59	58	57	56	55	54	53	52	51	20	49	48
Shell		2	က	4	လ	9	7	80	6	10	11	12	13	14	15	16	1.7	18	19	20	21	22

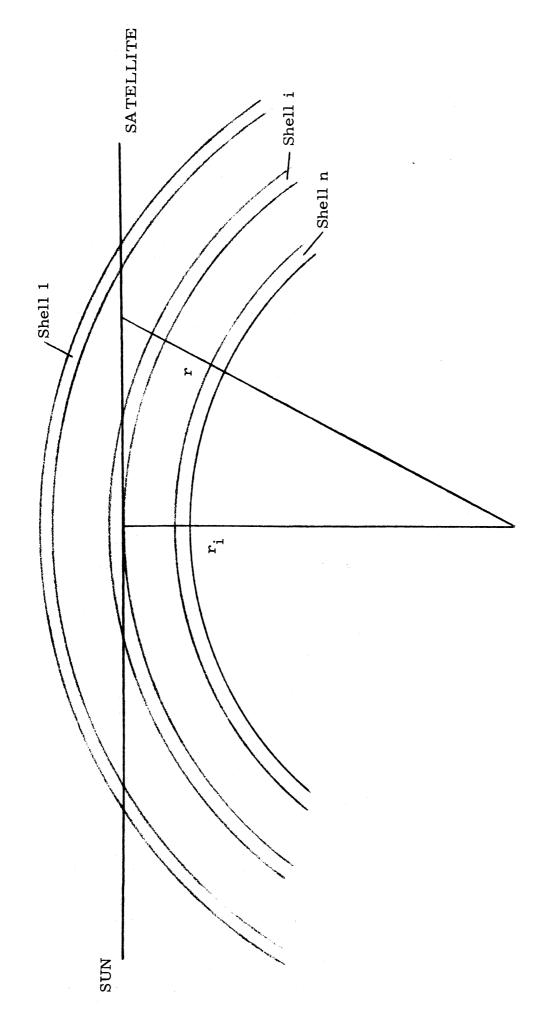


Figure 4.1 Geometry of Solar Occultation Experiment

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Chapter 5. Discussion and Calculations.

Although this study is not yet complete it is already evident that useful measurements of stratospheric distribution of some minor constituents can be made from a satellite using the solar occultation technique in the infrared spectral region. Furthermore comparatively simple instrumentation of medium spectral resolution (a few wavenumbers) may be employed for the more abundant of the minor molecular constituents such as water vapor, carbon dioxide, methane, nitrous oxide, ozone and perhaps carbon monoxide and nitric acid. Details of the absorption in different spectral regions have been given in the second chapter and recommendations on the spectral intervals to make measurements have been made for most of the molecules. Carbon dioxide has not been included in the chapter as it would probably be difficult to improve on our present knowledge of its stratospheric concentration. It is possible, however, that measurements in the Q-branch near 668 cm⁻¹ or in the 4.3 μ m band could yield information on the lower mesospheric distribution. Similarly nitric acid vapor has not been included, in this case because of the difficulty in determining its stratospheric absorption. The most promising spectral regions appear to be the Q-branches near 879 and 897 cm⁻¹, although special care is needed to distinguish between nitric acid absorption and extinction by aerosols.

In most of the stratospheric absorption calculations a band model was employed. In the majority of our future calculations we expect to use the line-by-line integration method for greater accuracy, although errors introduced by the band model do not affect the feasibility aspect of the study. For some of the molecules the more sophisticated technique may not be justified at the present time because of the inadequacy

of the spectral line parameters needed as input to the computer programs. This is certainly true for most of the ozone bands and probably for methane also. It is clear that a careful and comprehensive comparison between theoretical and laboratory data is required, not only for room temperature measurements but also for measurements taken at stratospheric temperatures. 220 K is a representative temperature in the lower stratosphere and few absorption measurements have been taken under these conditions. We recommend that laboratory absorption measurements of this nature be undertaken.

Sulphuric acid aerosols in the lower stratosphere have been shown to give large values of extinction between about 800 and 1600 cm⁻¹, the exact characteristics depending on their concentration, size distribution, etc. This is encouraging for those who would like to study the aerosols, but adds another uncertainty to the determination of the concentrations of the molecular constituents. We need to be able to predict the extinction by the aerosols, possible by measureing the extinction in a spectral region close to that chosen for the molecule. The extinction calculations described are for realistic values of parameters but need to be extended to different ranges of size, concentration, composition, height distributions and spectral regions.

Several different inversion techniques have been developed and tested but it is not yet apparent how best to incorporate the smoothing which is necessary to prevent the domination of noise. We expect to use the inversion programs to study the effect of many sources of error and will eventually be able to predict uncertainties in the concentrations of the retrieved profiles. A major problem will be the computation of the transmittances in the inversion program, made difficult by the large amount of computer time needed to calculate them accurately.

For the reasons stated in the first chapter we have largely confined our discussions to the more abundant of the minor constituents. Other molecules such as NO and NO_2 are of great interest but their absorption is smaller and would require more sophisticated instrumentation. We plan to examine some of these but may be limited by the absence of adequate spectral data, both theoretical and experimental.

APPENDIX

Computer Programs for Line-by-Line Transmittance Calculations

The computer programs written for the line-by-line calculation of atmospheric transmittances for the occultation geometry have been adapted from the already existing programs for slant path transmittance which assumed a plane parallel atmosphere. The atmosphere is divided into concentric shells and the regions between shells are assumed to be homogeneous. The program calculates the optical masses for each tangent height path in each region and uses them to compute the monochromatic transmittance along the tangent path. Refractive effects have not been incorporated but this would be easy to do since they would affect slightly the optical masses. Integration over wavenumber intervals of 0.1 cm⁻¹ is accomplished by numerical quadrature.

The following is a brief description of the input/output of the programs which are written in Fortran IV. Two programs are used:

- 1. SETUPV This program processes the line parameter data and outputs quadrature intervals, wing contributions, etc.
- 2. HSLANV computes the transmittances using the data out putted by SETUPV.

Input / Output of SETUPV

Line 23	Input of line	e parameters from binary file or tape.
	BNUS (I)	Line wavenumber (cm ⁻¹), rounded to two decimal places
	TS (J, I)	Line intensities at 6 temperatures 300, 275, 250, 225, 200, 175 K corresponding to J = 1, 6.
	AR (I)	Line halfwidth (cm $^{-1}$) at 1 atm. and 300K.

Line 34. ANUZ The starting wavenumber (cm⁻¹)

NUMBER The number of 1 cm⁻¹ intervals for which transmittance calculations are to be made.

All output statements write data to be used by HSLANV

Input/Output of HSLANV

Line 29. Namelist NAM1.

PCRIT Pressure (mb) below which Voigt profile is

used

WTM Molecular weight of the molecule

NQI, NQC Gaussian quadrature parameters, have value

of 2 or 4 giving maximum efficiency and

lowest accuracy or less efficiency and greater

accuracy respectively.

KMAX The number of tangent heights calculated.

Altitude Z (km), pressure P(mb), temperature T(K) and concentration CONC must be specified at the (K + 1) bounding shells, starting with the highest altitude. CONC is mixing ratio by volume for IS = 1, or number density mol cm⁻³ for all other values of IS.

Line 49.5. Prints the parameters inputted in line 29.

Line 82. Namelist NAM2.

ANUZ and NUMBA correspond to ANUZ and NUMBER in program SETUPV.

All other input statements use the output from SETUPV.

Line 397. ANUZ center of 1 cm⁻¹ interval for which calculation is made.

TRAN (J, K) transmittance for tangent altitude

Z(K + 1) and pressure P(K + 1) for 10 intervals averaged over 0.1 cm⁻¹. J = 1 corresponds to interval (ANUZ - 0.5, ANUZ - 0.4), J = 2 to the next highest etc.

```
1
       C THIS PROGRAM IS CALLED SETUPY FORTRAN IV
 2
              COMMCN NCSTRG, L, NCINT, NOIN, NEND, IWARN
              EQUIVALENCE (ST(1), TS(1))
 3
 4
              DIMENSION NOSTRG(10), L(100), NOINT(72), NEND(144), IWARN(10)
 5
              DIMENSION ISTRGL(100),
                                                 BNUS(2200), INUS(2200), IABOVE(100),
             11BELOW(1CO),D(2200),SM(18),ISS(2200),ST(13200),AR(2200),TS(6,2200)
 6
             1 , IVST (2200)
 7
 8
              DATA 11,12,10NE,13,KID,1STC,1C,JJ/8*1/
 9
              DATA JJJ, ITWO/4,0/
10
         200 FORMAT (F6.2,6E10.4)
11
         201 FORMAT(F7.2,15)
12
         202
              FORMAT(F7.2,6E10.4,F6.4,I9)
          281 FORMAT (215, F6.1)
13
14
         250
              FORMAT(F7.2, 12, 214, 1112, 1011/(6E10.4))
         252 FCRMAT (9(212,14))
15
          253 FORMAT (2413)
16
17
          203 FORMAT (12)
18
              DIST=3.5
19
              MS=2200
20
              IDIST=DIST*100.
22
              DO 301 I=1,MS
23
              READ(7, END=1301) BNUS(I), (TS(J,I), J=1,6), AR(I)
24
         301
              ISS(I) = (I-1)*6
25
              CALL ERROR
25.5
         1301 MS=I-1
25.6
              MSP=MS+1
26
              INUS(MSP) = 100000000
27
              DO 303 I=1,MS
28
              IF (ST(JJJ)-.1) 304,304,305
29
          305 \text{ IVST(JJ)} = I
30
              JJ = JJ+1
          304 JJJ = JJJ+6
31
32
          303 INUS(I)=(BNUS(I)+.001)*1CC.
33
              JJ = JJ-1
          802 READ (5,201, END=1000) ANUZ, NUMBER
34
35
         1802 CONTINUE
36
              NU Z= ANU Z+.001
37
              NUZZ = (NUZ/1C) * 10
38
              AVNU=NUZZ
39
              AVNU=4.5+AVNU
40
              NUZY=NUZZ*100
41
              NUZX=NUZY-IDIST
42
              IS=IONE
43
              DO 600 I=IS.MS
              IF (NUZX-INUS(I)) 601,601,600
44
45
          601 ICNE = I
46
              GO TO 602
47
          600 CCNTINUE
48
              IONE = MSP
49
              ITWO1=MS
50
              GO TO 607
51
          602 NUZV=NUZY+900+IDIST
52
              IS=MAXO(ITWO.1)
53
              DO 603 I=IS.MS
54
              IF (NUZV-INUS(I)) 604,603,603
          604 ITW01=I-1
55
56
              GO TO 607
57
         603 CONTINUE
58
              ITWO1=MS
59
          607 CONTINUE
```

```
IOUT=MAXO(ITWO+1, IONE)
60
61
               ITWO=ITWO1
               NUZY=NUZY-50
62
               WRITE (6,281) IONE, ITWO, AVNU
63
               IF (IDUT-ITWO) 611,611,610
64
          611 WRITE (6,202) (BNUS(I), (TS(J,I),J=1,6),AR(I),I,I=IOUT,ITWO)
65
66
          610 CONTINUE
          801 NUZ=(ANUZ-.499)*100.
67
               DO 311 K=ISTO, MS
68
               IF (INUS(K)-NUZ) 311,313,313
69
70
          313 \text{ IST} = K
 71
               GO TO 312
 72
           311 CONTINUE
 73
               IST=MSP
 74
           312 NUZ = ANUZ+.001
 75
               NU ZM=NU Z *100-60
 76
               IF (KID.GT.JJ) GO TO 762
               DO 320 K = KID,JJ
77
 78
               KK = IVST(K)
 79
               KD = K
               IF (INUS(KK)-NUZM) 32C,32C,322
80
           320 CCNTINUE
81
               KD=JJ+1
 82
          322 \text{ KID} = \text{KD-1}
 83
               IF (KID .EQ. 0) KID=1
 84
 85
           762 II=1
 86
               ITOTAL = 0
 87
               IIS = 1
88
               JTOTAL = 0
 89
               DO 351 J=1,10
 90
               INUZM = NUZM + 10*J
 91
               MICNU = INUZM+5
92
           331 IF (JJ-KID) 445,446,446
 93
           445 [WARN(J)=1
 94
               GO TO 336
 95
           446 KAD=IVST(KID)
 96
               IF (MIDNU-INUS(KAD)-10) 332,332,333
 97
           333 \text{ KID} = \text{KID+1}
 98
               GO TO 331
99
           332 IWARN(J) = 1
100
               IF (IABS(MIDNU-INUS(KAD))-10) 335,336,336
101
           335 \text{ IWARN}(J) = 0
102
           336 CCNTINUE
103
               NOSTRG(J) = 0
               I = 0I
104
           400 IF (IST-MSP) 410,351,351
105
           410 JALFA=INUS(IST)-INUZM
106
107
               IF (JALFA-10) 350,350,351
           350 L(IIS) = JALFA
108
               NOSTRG(J) = NOSTRG(J)+1
109
               JTCTAL = JTCTAL+1
110
               ISTRGL(IIS) = IST
111
112
               IF (JALFA-10) 352,353,352
           353 IABOVE(IIS)=-1
113
               IBELOW(IIS) = 1
114
               IF (INUS(IST)-INUS(IST-1)-1) 354,354,355
115
116
           354 \text{ IBELOW(IIS)} = 0
117
           355 IIS = IIS+1
               GC TO 351
118
119
           352 IF (JALFA) 356,356,357
```

```
120
          356 IABOVE(IIS)=1
121
               IBELOW(IIS) =-1
               IF (INUS(IST+1)-INUS(IST)-1) 358,358,359
122
123
          358 [ABOVE(IIS)=0
          359 GO TO 360
124
          357 IABOVE(IIS)=1
125
               IBELOW(IIS)=1
126
127
               IF (INUS(IST+1)-INUS(IST)-1) 361,361,362
          361 IABOVE(IIS)=0
128
          362 IF (INUS(IST)-INUS(IST-1)-1) 363,363,364
129
          363 IBELOW(IIS)=0
130
131
          364 CONTINUE
132
          360 IIS = IIS+1
133
               IST = IST+1
134
               GO TO 400
135
          351 CONTINUE
               ISTO=IST
136
137
               BNU=ANUZ-DI ST
               IS=MAXO(1, I1)
138
               DO 460 I=IS, MS
139
               IF (BNU-BNUS(I)) 461,460,460
140
          461 I1 = I-1
141
142
               GO TO 462
          460 CONTINUE
143
               II=MS
144
145
          462 BNU=ANUZ+DIST
146
               IS=12
147
               DO 463 I=IS.MS
               IF (BNU-BNUS(I)) 464,464,463
148
          464 I2 = I
149
               GO TO 465
150
151
           463 CONTINUE
152
               I2=MSP
153
           465 IFIRST = I1+1
154
               ILAST = I2-1
               KK = 0
155
156
               DO 370 M1=1,3
               Y = M1 - 2
157
               BNU = ANUZ+Y/2.
158
159
               DATA DXX/50./
               ISIS=0
160
               IF (I1) 401, 401, 402
161
162
        402
               DO 371 I=1, I1
163
               DXY=BNUS(I)-BNU
164
               D(I)=DXY*DXY
165
               IF(D(I).GT.DXX) ISIS=I
166
        371
               CONTINUE
167
         401
               ISIS=ISIS+1
               IF (MS-I2) 403,1401,1401
168
         403
               ISIT=MS
169
               GO TO 1403
170
               DO 372 I=12,MS
171
        1401
172
               DXY=BNUS(I)-BNU
173
               D(I)=DXY*DXY
174
               ISIT=I
175
               IF (D(I).GT.DXX) GO TO 1404
176
        372
               CONTINUE
177
               GO TO 1403
178
         1404
               ISIT=ISIT-1
179
        1403 DO 370 K=1,6
```

```
S=0.
180
               KK=KK+1
181
               IF (I1-ISIS)1405,4C6,4C6
182
               DO 373 I=ISIS, I1
183
        406
               ISUB=ISS(I)+K
184
               S=S+ST(I SUB) *AR(I)/D(I)
185
        373
186
        1405
               IF (ISIT-12)370,4C5,405
        405
               DO 374 I=12, ISIT
187
               ISUB = ISS(I)+K
188
           374 S=S+ST(ISUB) *AR(I)/D(I)
189
190
           370 \text{ SM(KK)} = S
191
               CALL GRONK
               WRITE (6,250) ANUZ, JTOTAL, IFIRST, ILAST, (NOSTRG(I), I=1,10
192
              1), NO IN, (NO INT(I), I=1,10), (SM(I), I=1,18)
193
           380 IF (JTOTAL) 383,383,382
194
           382 WRITE (6,252) (IBELOW(I), IABOVE(I), ISTRGL(I), I=1, JTOTAL)
195
196
           383 IF (NOIN) 385,385,384
           384 NON = NOIN*2
197
198
                WRITE (6,253) (NEND(I), I=1, NCN)
199
           385 CCNTINUE
200
               NUMBER=NUMBER-1
201
                IF (NUMBER) 802,802,306
           306 ANUZ=ANUZ+1.0
202
203
               NUZ=ANUZ+0.1
                IF (NUZ-(NUZ/10)*10) 1802,1802,801
204
          1000 STOP
205
206
               FND
                                                                                        GRONK 01
207
                SUBROUTINE GRONK
               COMMON NCSTRG, L, NOINT, NOIN, NEND, IWARN
208
209
               DIMENSION NOSTRG(10), L(100), NOINT(72), NEND(144), IWARN(10)
210
               KK = 1
                M1 = 1
211
               DO 300 I = 1,10
212
               MINIT = MI
213
214
               M = 0
215
                J = NOSTRG(I)
               IF (J) 301,301,302
216
           301 \text{ NEND(M1)} = 0
217
218
                NEND(M1+1) = 10
                M1 = M1+2
219
               M = 1
220
               GO TO 320
221
222
           302 K = 1
223
                IF (L(KK)-2) 330,303,303
224
           303 \text{ NEND(M1)} = 0
225
               NEND(M1+1) = L(KK)-1
226
                M1 = M1+2
227
                M = M+1
           330 IF(K-J) 304,34C,304
228
           304 IF (L(KK+1)-L(KK)-2) 305,305,306
229
230
           306 NEND(M1) = L(KK)+1
231
                NEND(M1+1) = L(KK+1)-1
                M1 = M1+2
232
                M = M+1
233
           305 K = K+1
234
                KK = KK+1
IF(K-J) 330,340,330
235
236
           340 IF (L(KK)-8) 307,307,350
237
           307 \text{ NEND(M1)} = L(KK)+1
238
239
                NENC(M1+1) = 10
```

```
240
                  N = M+1
  241
                  M1 = M1+2
             350 KK = KK+1
  242
   243
              320 CONTINUE
                  IF (IWARN(I)) 311,311,312
  244
   245
              311 MZERO = M
                  JJ=1
   246
   247
             201 IF (JJ-MZERO) 321,321,380
              321 IF (NEND(MINIT+1)-NEND(MINIT)-3) 360,360,323
   248
   249
              323 M=M+2
   250
                  IX=NEND(MINIT+1)-NEND(MINIT)
   251
                  I1 = (IX + 1)/3
   252
                  I2=(2*IX+1)/3
   253
                  MALL = M1 - MINIT -1
                  DO 37C II=1, MALL
   254
   255
                  MSUB = MI-II
              370 NEND (MSUB+4) = NEND (MSUB)
   256
   257
                  NEND (MINIT+1)=NEND(MINIT)+11
   258
                  NEND (MINIT+2)=NEND(MINIT+1)
   259
                  NEND(MINIT+3)=NEND(MINIT)+12
   260
                  NEND(MINIT+4)=NEND(MINIT+3)
   261
                  M1 = M1 + 4
   262
                  MINIT=MINIT+4
   263
              360 MINIT = MINIT+2
   264
                  JJ = JJ + 1
                  GO TO 201
   265
   266
              380 CCNTINUE
              312 \text{ NOINT(I)} = M
   267
              300 CONTINUE
   268
                  M1 = M1-1
   269
   270
                  NDIN = M1/2
                  RETURN
   271
   272
                  END
END OF FILE
```

```
PROGRAM HSLANV FORTRAN IV
              MODIFIED FOR 2 OR 4 POINT CUADRATURE
 2
              CCMMON ANU, ANUZ, SEC, SN, TRAN, WWA, II, IST, JMAX, KADD, KSLA, KMAX, M.
 3
                    KMESS, KSTOP, IE, AVNU, KCFIT, K, P, ZEN, AL2, AL, ALP, X, Y, ZERO, LS, ANZ,
 4
                  ANY, C, JUMP, AR, GNU, ARR, GNUU, ST
 5
 5.5
               CCMMON /ADD/ CC(630)
               DIMENSION ANU(250), IST(250), ANZ(250), ANY(250), C(35), SEC(10),
 6
                    SN(150), ST(8750), TRAN(2800), TE(8), P(36), AL2(35), AL(35),
 7
                     ALP (35), X(35), Y(35), ZERO (35), JUMP (35)
 8
              2
               DIMENSION BNU(250), IBELOW(2CC), ENDPT(200), ENGTH(36), SM(18), T(36),
 Q
                     TM(35), WAB(4), ISTRGL(100), [A(250), ITN(35), NOINT(10),
10
              1
                     NOSTRG(10), IABGVE(100), X1 (35), Y1 (35), ZERO1(35), B(6), WA(4)
11
               DIMENSION AR (250), GNUU(20), ARR(250), GNU(20)
12
               DIMENSION CONC (36), Z (36), XX (35)
12.5
               NAMELIST /NAM1/ PCRIT, WTM, KMAX, NQI, NQC, CONC, Z, IS, P, T
13
14
               NAMELIST /NAM2/ NUMBA, ANUZ
15
          902 FORMAT (215,F6.1)
         904
               FORMAT (F7.2, 6E10.4, F6.4)
16
         905 FORMAT (F7.2, 12, 214, 1112, 1011/(6E10.4))
17
          906 FORMAT (5(212,14))
18
19
          907 FORMAT (24F3.2)
         800 FORMAT(F10.1,F10.2,416/(F8.1,F10.2,2E14.4))
20
          801 FORMAT (216/(10F8.3))
21
               DATA NQI/2/, NQC/2/, WTM/44./
21.4
               DATA ENDPT/.C,.001,.002,.003,.005,.01/
21.5
               DATA ACIST/.8/, ANDIST/.099/, PCRIT/100./, PPP/1013.25/, PC 02/.032/
22
               KCRIT=0
23
24
               TTT=298.0
               AAA=1.0
25
               IShCH=1
26
               I1 = 0
27
               PIE=3.1415927
28
29
               READ (5,NAM1)
29.5
               KSLA=1
               NC C=NQC * 5
30.4
               NCB=NQC * 4
30.5
31
               II=1
32
               DO 100 I=1,5
               CALL GAUSSN(ENDPT(I), ENDPT(I+1), GNU(II), ENGTH(II), NQC)
33
         100
               II=II+NQC
34
35
               DO 101 I=1.NCC
               GNUU(I) = GNU(I) * GNU(I)
36
37
           101 ENGTH(I) = ENGTH(I) *10.0
38
               DOP=3.581136E-7/SQRT(WTM)
               ALCG2=ALCG(2.)
39
40
               ALOG 2 = SQRT (ALOG 2)
               ROOTPI=SQRT(PIE)
41
45
               KMESS=10*(KMAX-1)
               KO=KMAX*KSLA
46
47
               KL CT = KO * 10
48
               KADD = KMA X * 10
               KPLUS=KMAX+1
49
               WRITE(6,800) PCRIT, WTM, NQI, NQC, KMAX, IS, (Z(K), T(K), P(K),
49.5
49.6
              1 CONC(K), K=1, KPLUS)
50
                \Delta \Delta \Delta = \Lambda \Delta \Delta / PPP
51
                ALPHA=AAA*AAA*TTT
               DO 102 I=1,225
52
53
                JA = I - 1
                IST(I) = KMAX + JA
54
55
           102 IA(I)=6*JA
```

```
55.1
               KZ=1
56
               DO 103 K=1,KMAX
57
               TA = (T(K) + T(K+1))/2.
58
               PA = (P(K) + P(K+1))/2.
               AL 2(K) = ALPHA/TA*PA*PA
59
               AL(K) = SQRT(AL2(K))
60
               ALP(K)=AL(K)/PIE
61
               C(K) = (CONC(K) + CONC(K+1)) * .5
62
               IF (IS.EC.1) C(K)=C(K)*PA/(TA*1.38054E-19)
62.1
               ZZ=(6378.+Z(K+1))*2.
62.2
62.3
               DC 1033 I=1.K
               HH=Z(I)-Z(K+1)
62.4
62.5
         1033 XX(K)=SQRT(HH*(ZZ+FH))
62.6
               XX(K+1) = 0.
62.7
               CO 1034 I=1,K
62.8
               CC(KZ) = (XX(I) - XX(I+1)) * C(I) * 8.176E-15
62.9
         1034 KZ=KZ+1
               IF (PA-PCRIT) 104,105,105
63
64
          104 \text{ JUMP}(K)=1
65
               KCRIT=K
               AD=DOP*SCRT (TA)
66
67
               X1(K)=ALCG2/AD
68
               Y1(K) = AL(K) * X1(K)
69
               ZERO1(K)=X1(K)/ROOTPI
70
               GO TO 106
          105 JUMP(K)=0
71
72
          106 TAA=TA-275.
73
               DO 107 N=2.5
               IF (TAA) 107,107,108
74
75
          108 ITN(K)=N
76
               GO TO 109
77
          107 TAA=TAA+25.0
78
               ITN(K)=5
79
          109 TN=ITN(K)
80
               TP=325.-25.*TN
          103 TM(K)=(TA-TP)/25.
81
          190 READ (5, NAM2)
82
83
               WRITE (6,NAM2)
84
               IS5=4
 85
          110 READ (5,902) IFIRST, ILAST, AVNU
 86
               DO 111 K=1,KCRIT
 87
               X(K)=X1(K)/AVNU
 88
               Y(K) = Y1(K) / AVNU
 89
           111 ZERO(K)=ZERO1(K)/AVNU
 90
               IJ=IFIRST-1
 91
               IMAX=ILAST-IJ
92
               GO TO (401,402), ISWCH
 93
          401 IJKL=1
 94
               GO TO 403
          402 IJK=ILASTA-IFIRST+1
 95
 96
               IF (IJK) 401,401,404
97
           404 ISHIFT=IMAXA-IJK
98
               IF (ISHIFT) 410,410,411
           411 DO 405 I=1,IJK
99
100
               J=I+ISHIFT
101
               AR(I) = AR(J)
102
               ARR([)=ARR(J)
103
          405 BNU(I)=BNU(J)
104
               ISHIFT=I SHIFT*KMAX
105
               IJKJ=IJK*KMAX
```

```
106
               DO 406 I=1,IJKJ
               J=I+ISHIFT
107
          406 ST(I)=ST(J)
108
109
          410 IJKL=IJK+1
          403 IF (IMAX-IJKL) 412,413,413
110
          413 ISUB=IST(IJKL)
111
               DO 450 I=IJKL, IMAX
112
               READ (5,904) BNU(I), (B(J), J=1,6), AR(I)
113
               ARR(I) = AR(I) * AR(I)
114
               DO 451 K=1.6
115
               B(K) = B(K) * AR(I)
116
          451 B(K) = ALOG(B(K))
117
               DO 450 K=1,KMAX
118
119
               ISUB=ISUE+1
120
               JA = ITN(K)
121
               S1=B(JA-1)
122
               S2=B(JA)
123
               S3=B(JA+1)
          450 ST(ISUB) = (EXP(S2+((S1+S3-S2-S2)*TM(K)+S1-S3)*TM(K)/2.))*ALP(K)
124
125
           412 ILASTA=ILAST
               IMAXA= IMAX
126
127
               ISWCH=2
128
           120 READ (5,905) ANUZ, JTOTAL, I1, I2, (NOSTRG(I), I=1,10), NOIN, (NOINT(I),
                    I=1,10),(SM(I),I=1,18)
129
               IF (JTOTAL) 600,600,601
130
           601 READ (5,906) (IBELOW(I), IABCVE(I), ISTRGL(I), I=1, JTOTAL)
131
132
           600 NCN=NOIN*2
133
               IF (NDIN) 602,602,603
134
           603 READ (5,907) (ENDPT(I), I=1,NON)
135
           602 CONTINUE
               I1=I1-IJ
136
137
               12=12-1J
               IE (1) = [1
138
139
               IE(6)=12
140
               DO 130 K=1,KMAX
               DO 130 N=1,3
141
142
               JA=IA(N)+ITN(K)
143
               SUM1 = SM(JA-1)
               SUM2=SM( JA )
144
145
               SUM3=SM(JA+1)
               ISUB=IST(N)+K
146
147
           130 SN(ISUB)=(SUM2+((SUM3+SUM1-2.*SUM2)*TM(K)+SUM1-SUM3)*TM(K)/2.0)
148
              1
                    *ALP(K)
149
               M1=1
               M2=1
150
               IF (I1-I2) 170,170,171
151
152
           170 CONTINUE
153
               CO 121 I=I1, I2
154
               A=BNU(I)-ANUZ
155
               IF (A) 122,122,123
           122 N=(A-.005)*100.
156
157
               GO TO 125
158
           123 N=(A+.005)*100.
159
           125 A=N
           121 ANL(I)=A/100.
160
           171 CONTINUE
161
162
               DO 124 N=1,KLOT
           124 TRAN(N)=C.O
163
               DO 303 M=1,10
164
               ANUO=M-6
165
```

```
ANUD=ANUO/10.
166
167
                ANUA=ANUC+.05
                IEA=LGOP(I1, I2, ANUA-ADIST, ANU)
168
                IE(1)=IEA-1
169
                IE(6)=LOGP(IEA, I2, ANUA+AD(ST, ANU)
170
171
               CALL LUOKBY(ANUA, I1, I2, 3, ANUA)
172
                IE(1)=IE(1)+1
                IE(6) = IE(6) - 1
173
174
               NOIE=NOINT(M)
                IF (NCIE) 180,180,181
175
176
           181 CONTINUE
                DO 306 MM=1,NOIE
177
                KSTOP=KMAX+1
178
                CALL GAUSSN(ENDPT(M1), ENDPT(M1+1), WAB, WA, NQI)
179
180
                DO 200 III=1,NCI
181
                II=III
                BAC =WAB(II)+ANUO
182
183
                WWA=WA(II)*10.
                IEA=LOOP(IE(1), IE(6), BAD-.2, ANU)
184
185
                IE(2)=IEA-1
                IE(5)=LOCP(IEA, IE(6), BAD+.2, ANU)
186
           200 CALL LOOKBY(BAD, IE(1), IE(6), 1, 10. *WAB(II) -. 5)
187
           306 M1 = M1 + 2
188
189
           180 CONTINUE
190
                NOIE=NOSTRG(M)
                IF(NCIE) 182, 182, 183
191
192
           183 CONTINUE
                DO 309 MM=1,NOIE
193
194
                LS=ISTRGL(M2)-IJ
195
                FREQ=ANU(LS)
                IE(3)=LOCP(IE(1), IE(6), FREQ-.199, ANU)
196
197
                1E(2) = 1E(3) - 1
                IE(7)=LOOP(IE(3), IE(6), FREQ-ANDIST, ANU)-1
198
199
                IE(8)=LOCP(LS+1, IE(6), FREC+ANDIST, ANU)
200
                IE(5)=LOCP(IE(8), IE(6), FREC+.199, ANU)
                IE(4) = IE(5) - 1
201
202
                IXI = (FREC-ANUA) *1CC.1
203
                BAD=IXI
204
                CALL LCCKEY (FREQ, IE(1), IE(6), 0, 8AD/10.)
205
                IE(7) = IE(7) + 1
206
                IE(8) = IE(8) - 1
207
                IE(3)=LS-1
208
                IE(4)=LS+1
209
                IF (IBELOW(M2)) 141, 142, 143
210
          142
                ISLBB=NCB
                GU TO 144
211
          143
                ISUBB=NCC
212
           144 DO 145 III=1, ISUBB
213
214
                II=III
215
                BAC=FREQ-GNU(II)
                WWA=ENGTH(II)
216
            145 CALL LOOKBY (BAD, IE(7), IE(8), 2, -GNU(11) * 50.)
217
218
            141 IF (IABOVE(M2)) 146,147,148
219
           147
                ISUBB=NCB
220
                GC TO 149
           148 ISLBB=NCC
221
222
           149 DC 150 III=1, ISUBB
223
                III=II
224
                BAC=FREQ +GNU(II)
                WWA=ENGTH(II)
225
```

```
150 CALL LOOKBY (BAD, IE(7), IE(8), 2, GNU(II) *50.)
226
          146 CONTINUE
227
          309 M2=M2+1
228
229
           182 CONTINUE
          303 CONTINUE
230
               CALL PRIPUN(IS5)
231
               NUMBA=NUMBA-1
232
               IF (NUMBA) 151,151,152
233
           151 GO TO 190
234
           152 NU Z = ANU Z + 1 . 1
235
               IF (NUZ-(NUZ/10)*10)110,110,120
236
               END
237
238
               SUBROUTINE GAUSS (AA, BB, C, D)
               DIMENSION C(4),D(4)
239
               B=88
240
241
               A = AA
               X1=.8611363116
242
243
               X2=.3399810436
               Y1=.3478548451
244
               Y2=.6521451549
245
               X = (1.-X1)*.5
246
               Y=(1.+X1)*.5
247
248
               C(1)=B*X+A*Y
               C(4) = B*Y + A*X
249
250
               X=(1.-X2)*.5
251
               Y=(1.+X2)*.5
252
               C(2) = B*X+A*Y
               C(3)=B*Y+A*X
253
                \Delta = (B-A)*.5
254
255
               D(1)=Y1*A
               D(4)=D(1)
256
                D(2)=Y2*A
257
258
               D(3) = D(2)
259
                RETURN
260
                END
                FUNCTION LOOP(IA, IB, ZA, ZB)
261
                DIMENSION ZB(250)
262
                IF (IA-IB) 100,100,101
263
         101
                LOOP=IA
264
265
                RETURN
                CONTINUE
         100
266
                CO 202 I=IA, IB
267
                IF (Z8(I)-ZA) 202,202,103
268
         103
                LOOP=I
269
270
                RETURN
                CONTINUE
         202
271
                LOOP = IB + 1
272
                PETURN
273
274
275
                FUNCTION VOIGT (XIN, YIN)
                REAL*4 HH(2)/.8049141,.8131283E-01/,XX(2)/.5246476,1.650680/,A(42)
276
                  /0.0,.2,0.,-.184,0.0,.15584,0.0,-.121664,0.0,.8770816E-1,0.0,-.5
277
                  851412E-1,0.0,.3621573E-1,0.0,-.2084976E-1,0.0,.1119601E-1,0.0,-
278
                 .5623190E-2,0.0,.264 & 763E-2,0.0,-.1173267E-2,0.0,.4899520E-3,0.0
279
               4 ,-.1933631E-3,0.C,.7228775E-4,0.0,-.2565551E-4,0.0,.8662074E-5,0.
280
                 0,-.2787638E-5,0.0,.8566874E-6,0.0,-.2518434E-6,0.0,.7093602E-7/
281
                                                                                        VOIGTOO3
282
                DIMENSION RA(32),CA(32),RB(32),CB(32),B(44),AK(5),AM(5),DY(4)
283
                X = X T N
                Y = YIN
                                                                                         VOIGT010
284
                X2 = X*X
                                                                                        VOIGTO11
285
```

```
VOIGT012
286
               Y2 = Y*Y
               IF (X-7.0) 200,201,201
                                                                                    VOIGT013
287
          200 IF (Y-1.) 202,202,203
                                                                                    VOIGT014
288
                                                                                    VOIGT015
289
          203 \text{ RA(1)} = 0.
              CA(1) = 0.
                                                                                    VOIGT016
290
                                                                                    VOIGT017
291
              RE(1) = 1.
              CB(1) = 0.
                                                                                    VOIGT018
292
                                                                                    VOIGTO19
              RA(2) = X
293
                                                                                    VOIGT020
              CA(2) = Y
294
                                                                                    VOIGT021
              RB(2) = .5-X2+Y2
295
              CB(2) = -2.*X*Y
                                                                                    VOIGT022
296
297
              CB1 = CB(2)
                                                                                    VOIGT023
              UV 1=0.
                                                                                    VOIGT025
298
299
              DC 250 J=2.31
JMINUS = J-1
                                                                                    VOIGT026
                                                                                    VOIGT027
300
301
               JPLUS = J+1
                                                                                    VOIGT028
              FLOATJ = JMINUS
                                                                                    VOIGT029
302
               RB1 = 2.*FLOATJ+RB(2)
                                                                                    V01GT030
303
               RA1 = -FLOATJ*(2.*FLCATJ-1.)/2.
                                                                                    VOIGTO31
304
305
               RA(J+1)=RB1*RA(J)-CB1*CA(J)+RA1*RA(J-1)
               CA(J+1)=RB1*CA(J)+CB1*RA(J)+RA1*CA(JMINUS)
306
               RB(J+1) = RB1 * RB(J) + CB1 * CB(J) + RA1 * RB(J-1)
307
               CB(J+1)=RB1*CB(J)+CB1*RB(J)+RA1*CB(J-1)
308
               309
              1CB(JPLUS)*CB(JPLUS))
                                                                                    VOIGT037
310
               IF (ABS(UV-UV1)-1.E-6) 251,25(,250
311
          250 UV1=UV
                                                                                    VOIGT039
312
                                                                                    VOIGTO40
313
          251 VOIGT=UV/1.772454
                                                                                    VOIGTO41
314
               RETURN
           202 IF (X-2.) 301,301,302
                                                                                    VOIGT042
315
           301 AINT = 1.
                                                                                    VOIGT043
316
                                                                                    VOIGT044
317
               MAX = 12.+5.*X2
318
               KMAX = MAX-1
                                                                                    VOIGT045
               K0=0
319
320
               DO 303 K=KO,KMAX
                                                                                    VOIGT047
               \Delta J = M\Delta X - K
321
          303 AINT = AINT*(-2.*X2)/(2.*AJ+1.)+1.
                                                                                    VOIGT048
322
               U = -2.*X*AINT
                                                                                    VOIGT049
323
                                                                                    VOIGT 050
               GO TO 304
324
325
          302 IF (X-4.5) 305,306,306
                                                                                    VOIGTO51
                                                                                    VOIGT052
           305 B(43)=0.
326
               B(44) = 0.
                                                                                    VOIGT053
327
                                                                                    VOIGT054
328
               J = 42
                                                                                    VOIGT055
329
               00 \ 307 \ K = 1,42
               B(J) = .4*x*B(J+1)-B(J+2)+A(J)
                                                                                    VOIGT056
330
                                                                                    VOIGT057
           307 J = J-1
331
               U = B(3) - B(1)
                                                                                    VOIGT058
332
                                                                                    VOIGT059
333
               GO TO 304
334
           306 \text{ AINT} = 1.0
                                                                                    VOIGTO60
               MAX = 2.+40./X
                                                                                    VOIGT061
335
               AMAX = MAX
                                                                                     VOIGT062
336
                                                                                    VOIGT063
337
               DO 308 K=1,MAX
               AINT = AINT*(2.*AMAX-1.)/(2.*X2)+1.
                                                                                    VOIGTO64
338
339
           308 \text{ AMAX} = \text{AMAX} -1.
                                                                                     VOIGT065
                                                                                    VOIGT 066
              U = -AINT/X
340
341
           304 V = 1.772454*EXP(-X2)
                                                                                     VOIGT067
342
               H = .02
                                                                                    VOIGT068
               JM = Y/H
                                                                                     VOIGT069
343
               IF (JM) 310,311,310
                                                                                     VDIGTO70
344
                                                                                    VOIGTO71
345
           311 H=Y
```

```
346
           310 Z = 0.
                                                                                           VOIGTO72
347
                L = 0
                                                                                           VOIGT073
348
                CY(1) = 0.
                                                                                           VOIGTO74
349
           312 \text{ DY(2)} = H/2.
                                                                                           VOIGT075
                DY(3) = DY(2)
350
                                                                                           VOIGT 076
351
                DY(4) = H
                                                                                           VOIGT077
352
           318 \text{ AK(1)} = C.
                                                                                           VOIGT078
353
                \Delta M(1) = 0.
                                                                                           VOIGT079
                DO 313 J=1.4
354
                                                                                           VOIGT080
355
                YY = Z+DY(J)
                                                                                           VOIGT081
356
                UU = U + .5 * AK(J)
                                                                                           VOIGT082
357
                VV = V + .5 * AM(J)
                                                                                           VOIGT083
358
                AK(J+1) = 2.*(YY*UU+X*VV)*H
                                                                                           VOIGT084
                AM(J+1) = -2.*(1.+X*UU-YY*VV)*H
359
                                                                                           VOIGT085
                IF (J-3) 313,314,313
360
                                                                                           VOIGT086
361
           314 AK(4)=2.*AK(4)
                                                                                           VOIGT087
362
                AM(4) = AM(4) + AM(4)
                                                                                           VOIGT088
363
           313 CONTINUE
                                                                                           VOIGT089
364
                Z=Z+H
                                                                                           VOIGT090
365
                L = L+1
                                                                                           VO IGT091
366
                U = U + .1666667 * (AK(2) + 2. * AK(3) + AK(4) + AK(5))
                                                                                           VOIGT092
                V = V + .1666667 * (AM(2) + AM(3) + AM(3) + AM(4) + AM(5))
367
                                                                                           VOIGT093
                IF(JM) 315,320,315
368
                                                                                           VOIGT094
369
           315 IF (L-JM) 318,317,320
                                                                                           VOIGT095
370
           317 \text{ AJM} = \text{JM}
                                                                                           VOIGT096
                H=Y-AJM+H
371
                                                                                           VOIGT097
                GC TO 312
372
                                                                                           VOIGT098
373
           320 VOIGT= V/1.772454
                                                                                           VOIGT099
374
                RETURN
                                                                                           VOIGT100
375
           201 F1 = 0.
                                                                                           VOIGT101
376
                DO 330 J=1,2
                                                                                           VOIGT 102
           330 F1=F1+HH(J)/(Y2+(X-XX(J))*(X-XX(J)))+HH(J)/(Y2+(X+XX(J))*(X+XX(J))*(X+XX(J)) VCIGT103
377
378
                                                                                           VOIGT104
379
                VOIGT=Y*F1/3.1415927
                                                                                           VOIGT105
380
                RF TURN
                                                                                           VOIGT106
381
                END
                                                                                           VOIGT 107
382
             PRIPUN HAS BEEN MODIFIED FOR USE WITH SLANTV
                SUBROUTINE PRIPUN(IS5)
383
384
               COMMON ANU, ANUZ, SEC, SN, TRAN, WWA, II, IST, JMAX, KADD, KSLA, KMAX, M,
                     KMESS, KSTOP, IE, AVNU, KCRIT, K, P, ZEN, AL2, ALP, X, Y, ZERO, LS, ANZ,
385
386
                   ANY,C,JUMP,AR,GNU,ARR,GNUU,ST
               DIMENSION ANU(250), IST(250), ANZ(250), ANY(250), C(35), SEC(10),
387
388
                     SN(150), ST(8750), TRAN(10,280), IE(8), P(36), AL2(35), AL(35),
389
                     ALP(35),X(35),Y(35),ZERO(35),JUMP(35)
               DIMENSION BNU (250), IBELOW (200), ENDPT(200), ENGTH(36), SM(18), T(36),
390
391
                     TM(35), WAB(4), ISTRGL(100), IA(250), ITN(35), NOINT (10),
392
                     NOSTRG(10), [ABOVE(100), X1(35), Y1(35), ZERO1(35), B(6), WA(4)
393
               DIMENSION AR(250), GNUU(20), ARR(250), GNU(20)
394
         900
               FORMAT (16H1 INTERVAL IS ,F6.1//(1H ,10F9.6,F10.2,I5))
395
                IS5=1
396
                KMID=KMAX*KSLA
397
                WRITE (6,900) ANUZ, ((TRAN(J,K),J=1,10),P(K+1),K,K=1,KMID)
398
                 WRITE(8) ANUZ, ((TRAN(J, K), K=1, KMID), J=1, 10)
399
                RETURN
400
                ENC
             LOCKBY HAS BEEN MODIFIED FOR USE WITH SLANTV
401
        C
402
                SUBROUTINE LOOKBY(FREQUE, IIII, III2, II4, Z)
               COMMON ANU, ANUZ, SEC, SN, TRAN, WWA, II, IST, JMAX, KADD, KSLA, KMAX, M,
403
404
                     KMESS, KSTOP, IE, AVNU, KCRIT, K, P, ZEN, AL2, AL, ALP, X, Y, ZERO, LS, ANZ,
                   ANY, C, JUMP, AR, GNU, ARR, GNUU, ST
405
```

```
COMMON /ADD/CC(630)
405.5
               DIMENSION ANU(250), IST(250), ANZ(250), ANY(250), C(35), SEC(10),
406
                     SN(150), ST (8750), TRAN(2800), IE(8), P(36), AL2(35), AL(35),
407
                     ALP(35),X(35),Y(35),ZERO(35),JUMP(35)
4C8
               DIMENSION AR(250), GNUU(2C), ARR(250), GNU(20)
409
               DIMENSION COEF (35)
409.5
               DIMENSION SZ(105), SA(105)
410
               FREQ=FREQUE
411
412
               111=1111
               112=1112
413
414
               14=114+1
               ZZ=Z
415
416
               ZZZ=ZZ*2.
417
               KP=2
               GO TO (1CO,101,102,103),14
418
419
        100
               CELTA=.01
420
               GO TO 104
421
         103
               DELTA=.05
         104
422
               IC=-1
               GO TO 403
423
424
         101
               IY = IE(2) + 1
425
               IZ=IE(5)-1
426
         102
               J'SLANT=M+KMESS
427
               F=0.
         403
428
               IF (III-II2) 180,180,181
         180
               DO 200 I=II1,II2
429
                ANZ(I) = ABS (ANU(I)-FREQ)
430
         200
431
                ANY(I) = ANZ(I) * ANZ(I)
432
         181
               CONTINUE
                KPP=2
433
                DG 202 KK=1,KMAX
434
435
                K=KK
436
               GO TO (110,111,111,113), [4
437
           111 CONTINUE
         501
                GO TO (121,121,122),14
438
         113
                SNI=SN(K)
439
440
                JA=K+KMAX
441
                SN2=SN(JA)
442
                JA=JA+KMAX
                SN3=SN(JA)
443
                GO TO 105
444
445
         122
                SN1=SZ(KP-1)
                SN2=SZ(KP)
446
447
                SN3=SZ(KP+1)
448
                GO TO 105
         121
                CONTINUE
449
450
         110
                SN 1= SA(KPP-1)
                SN2=SA(KPP)
451
452
                SN3=SA(KPP+1)
                KPP=KPP+3
453
                SRE= ((SN3+SN1-SN2-SN2)*ZZZ+SN3-SN1)*ZZ+SN2
454
         105
455
                GO TO (130,131,132,133),14
456
         131
                IF (JUMP(K))134,134,135
                SRE=SRE+RNTZ(II1, II2)
457
         134
458
                GO TO 136
                SRE=SRE+RNTZ(III, IE(2))+RNTZ(IE(5), II2)+XED(IY, IZ)
459
         135
460
                GO TO 136
         132
                IF (JUMP(K))137,137,138
461
                SRE=SRE+RNT Z(III, IE(3))+RNT Z(IE(4), II2)
         137
462
463
                AKNU=AR(LS) *AL(K)
```

```
IB=IST(LS)+K
464
               SRE=SRE+ST(IB)/(GNLU(II)+AL2(K)*ARR(LS))
465
               GO TO 136
466
               SRE=SRE+XED(III, IE(3))+XED(IE(4), II2)
467
               IB=IST(LS)+K
468
               SRE=SRE+ST(IB)/ALP(K)/AR(LS)*VOIGT(GNU(II)*X(K),Y(K)*AR(LS))*
469
                   ZERO(K)
470
          136 CUEF(K)=SRE
471
472
473
474
475
476
               GO TO 202
477
478
         130
               IF (JUMP(K)) 150,150,151
         150
               SZZ=RNTZ(II1, IE(7))+RNTZ(IE(8), II2)
479
480
               GO TO 152
         151
               SZZ=RNTZ(II1, IE(2))+RNTZ(IE(5), II2)+XED(IE(3), IE(7))+XED(IE(8), IE(
481
482
              14))
483
         152
                SZ(KP)=SZZ+SRE
484
               GO TO 202
485
           133 SA(KP)=SRE+RNTZ(III, IE(1))+RNTZ(IE(6), II2)
               KP = KP + 3
         202
486
487
                GC TO (160,1661,1661,160),14
          1661 JSLANT=M
487.1
487.2
               KX=1
                DO 503 J=1,KMAX
487.3
487.4
                F=0.
487.5
               DO 502 K=1.J
487.6
               F=F-CC(KX)*COEF(K)
487.7
          502
               KX=KX+1
                TRAN(JSLANT)=TRAN(JSLANT)+WWA*EXP(F)
487.8
487.9
          503
               J SLANT=J SLANT+10
                GO TO 161
487.95
488
         160
                IC = IC + 1
489
                ID = IC + 1
490
               GO TO (170,171,172), ID
491
         170
                KP=1
492
                FREQ=FREQ-DELTA
493
                IF (14-1) 173,174,173
494
         174
                ZZ = ZZ - .1
495
                GO TO 175
                ZZ=FREQ
496
         173
497
         175
                ZZZ=ZZ*2.
498
                GO TO 403
499
               KP=3
         171
500
                FREQ=FREQUE+DEL TA
501
                IF (I4-1) 176,177,176
502
         177
                ZZ=Z+.1
                GO TO 178
503
504
         176
                ZZ=FREQ
                222=22*2.
505
         178
                GO TO 403
506
507
         172
               CONTINUE
508
         161
                RETURN
509
                END
                XED HAS BEEN MODIFIED FOR USE WITH SLANTY
510
               FUNCTION XED(IA, IB)
511
512
               COMMON ANU, ANUZ, SEC, SN, TRAN, WWA, II, IST, JMAX, KADD, KSLA, KMAX, M,
513
                     KMESS, KSTOP, IE, AVNU, KCRIT, K, P, ZEN, AL2, AL, ALP, X, Y, ZERO, LS, ANZ,
```

```
514
                      ANY, C, JUMP, AR, GNU, ARR, GNUU, ST
                 2
                  DIMENSION ANU(250), IST(250), ANZ(250), ANY(250), C(35), SEC(10),
  515
  516
                        SN(150), ST(8750), TRAN(2800), IE(8), P(36), AL2(35), AL(35),
                 1
  517
                        ALP(35),X(35),Y(35),ZERO(35),JUMP(35)
                  DIMENSION AR(250), GNUU(20), ARR(250), GNU(20)
  518
  519
                  IF (IA-IE) 100,100,101
  520
            100
                  KUP=IST(IA)+K
  521
                  SUM= 0.0
  522
                  XA = X(K)
   523
                  YA=Y(K)
   524
                  DO 102 I=IA.IB
   525
                  SUM=SUM+ST(KUP) *VOIGT(ANZ(I) *XA, YA*AR(I))/AR(I)/ALP(K)
  526
            102
                  KUP=KUP+KMAX
  527
                  XED=SUM*ZERG(K)
   528
                  RETURN
            101
  529
                  XEC=0.0
   530
                  RETURN
   531
                  END
   532
           С
                  RNTZ HAS BEEN MODIFIED FOR USE WITH SLANTV
   533
                  FUNCTION RNTZ(IA, IB)
   534
                  COMMON ANU, ANUZ, SEC, SN, TRAN, WWA, II, IST, JMAX, KADD, KSLA, KMAX, M,
                        KMESS, KSTOP, IE, AVNU, KCRIT, K, P, ZEN, AL 2, AL, ALP, X, Y, ZERO, LS, ANZ,
   535
   536
                 2
                      ANY, C, JUMP, AR, GNU, ARR, GNUU, ST
   537
                  DIMENSION ANU(250), IST(250), ANZ(250), ANY(250), C(35), SEC(10),
   538
                        SN(150), ST(8750), TRAN(2800), IE(8), P(36), AL2(35), AL(35),
   539
                        ALP(35),X(35),Y(35),ZEPO(35),JUMP(35)
   540
                   DIMENSION AR(250), GNUU(20), ARR(250), GNU(20)
   541
                   IF (IA-IB) 100,100,101
   542
            100
                  KUP=IST(IA)+K
   543
                   SUM=0.0
   544
                   A=AL 2(K)
   545
                   DO 102 I=IA, IB
   546
                   SLM=SUM+ST(KUP)/(ANY(I)+A*ARR(I))
   547
            102
                   KUP=KUP+KMAX
   548
                   RNT7=SUM
   549
                   RETURN
                  RNTZ=0.0
   550
            101
   551
                   RETURN
   552
                   END
   553
                   SUBROUTINE GAUSSN(AA,BB,C,D,N)
   554
                   DIMENSION C(4),D(4)
   555
                   DATA A/.2886751/
                   IF (N.EQ.4) GO TO 100
   556
   557
                   IF (N.EQ.2) GO TO 200
   558
                   WRITE(6,950) N
   559
                   STCP
                  FORMAT('O WRONG QUADRATURE: N=1.14)
   560
             950
   561
             200
                  CC=(AA+BB)*.5
   562
                   DC=BE-AA
   563
                   DD =DC * A
   564
                   C(1) = CC - DD
   565
                   C(2) = CC + DD
                   D(1)=DC * .5
   566
                   C(2)=D(1)
   567
   568
                   RETURN
                   CALL GAUSS(AA,BB,C,D)
   569
             100
   570
                   RETURN
   571
                   END
END OF FILE
```

