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ACOUSTIC-INDUCED CAVITATION IN LIQUID NITRALE AT 1500°F

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Internal Report 1000-1-200

Financial Support Provided by

National Science Foundation

(Grant GA-2122)

February 1968

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## ULTRASONIC-INDUCED CAVITATION IN LIQUID METALS AT 1500° F<sup>1,2</sup>

The pumping and handling of high-temperature liquid metals is of considerable importance to the space program, particularly liquid-metal Rankine cycle SNAP systems, and to several conventional nuclear power-plant concepts. For SNAP, particularly, minimization of size and weight, and maximization of temperature is of over-riding importance. Thus the fluid-handling equipment must operate in or nearly in a cavitating condition. When cavitation will occur, and the resultant quantity and quality of damage must be known. The determination of materials showing the greatest cavitation resistance at elevated temperatures to be used in such components is the present objective.

The University of Michigan Nuclear Engineering Department ultrasonic cavitation facility has been already described<sup>1,2</sup>. Recently cavitation-erosion data have been obtained for 304 stainless steel, 316 stainless steel, a tantalum alloy (Ta-SW-12), and Cu-TiR in 70% Pb-30% Bi alloy at 1500°F. The test specimens were attached to the tip of an exponential horn, generated by a pair of lead-zirconate-titanate piezoelectric crystals at  $\lambda/18$  Kc/sec. with the horn tip immersed  $\lambda/18$  inches into the molten Pb-Bi. The double amplitude at the specimen was  $\lambda/2$  mils. Test durations varied for the different materials, frequent inspections and weighings monitoring the specimen surface.

<sup>1</sup> Financial support provided by NSF Grant (G-22620).

Figure 1 shows accumulative MDP<sup>2</sup> vs. time for the various materials and typical photographs of the damaged surfaces. MDP-rate for 304 and 316 stainless steel is 11.6 mils/hour and 2.6 mils/hour, respectively. The corresponding rate for the tantalum alloy is 0.3 mils/hour (less than 304 stainless steel by  $\sqrt{\pi} \times 39$ ), and the Ch-1Zr rate was 0.1 mils/hour. The expectation that such refractory materials at elevated temperature are much more cavitation-erosion resistant than stainless steel is thus confirmed, although this was not the case at room temperature<sup>3</sup>. As yet no other comparable elevated temperature cavitation-erosion data has appeared.

Detailed examination of the 303 stainless steel experimental horn, the 316 stainless steel container vessel, and the sides of the various test specimens, all of which are not subject to cavitation-erosion damage, indicate that corrosion effects in these investigations were negligible.

Cavitation incipience (initial appearance of cavitation as local pressure is reduced) and desincidence (disappearance of cavitation as local pressure is increased) points were also measured. It was found that for both stainless steels critical voltage (related directly to oscillation amplitude) at incipience and desincidence was  $\sqrt{130}$  volts, whereas for Ta-SW-ZMF  $\sqrt{170}$  volts, and for Ch-1Zr,  $\sqrt{70}$  volts. Hence, there was no hysteresis effect difference between incipience and desincidence points which sometimes occurs in flowing systems<sup>4</sup>. The lower voltages for Ta-SW-ZMF and Ch-1Zr are thought to indicate decreased wetting of these alloys by Pb-Bi.

<sup>2</sup>Mean depth of penetration (assuming weight loss smeared uniformly over surface)

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