

THE UNIVERSITY OF MICHIGAN

7030-9-T

NEAR CAUSTIC SURFACE FIELD

by

R. F. Goodrich

May 1966

Contract A F 04(694)-683

Prepared for

BALLISTIC SYSTEMS DIVISION
AIR FORCE SYSTEMS COMMAND
UNITED STATES AIR FORCE
NORTON AIR FORCE BASE, CALIFORNIA

Engu

44R

1639

TABLE OF CONTENTS

	Page
ABSTRACT	iv
I. INTRODUCTION	1
II. SCALAR DIFFRACTION BY A PROLATE SPHEROID	2
2.1 The Integral Representation	2
2.2 The Asymptotic Analysis	6
III. REFERENCES	20

ABSTRACT

At high frequency the acoustic surface fields for plane wave illumination of a prolate spheroid are found for near symmetric illumination. The surface caustic, in contrast to the symmetric case, is found to be diffuse. The values of the surface fields are used to find the modification of the creeping wave contribution to back scattering.

I

INTRODUCTION

We consider the use of the creeping wave formalism (Keller, 1953; Fock, 1946) for the prediction of surface fields induced by a plane wave on smooth convex scatterers. The application is straightforward away from regions of the surface in which the creeping waves converge due to the geometry of the body. Here the local geometry is taken to be cylindrical. If the creeping waves converge to a point, we speak of this point as a caustic and the creeping wave formalism can be modified in order to predict the fields in the region of a caustic. However, if the creeping waves do not quite converge to a point and yet cannot be treated in the cylinder approximation of the bodies in question by cylinders, a more subtle modification of the formalism is required. We shall consider this problem and designate the near-caustic region as a diffuse caustic.

We attack the problem of describing the field in the region of the diffuse caustic through a canonical problem. We will study the surface fields on a prolate spheroid for a plane wave which is near axially incident and then attempt a generalization to other shapes. In analyzing the prolate spheroid we shall extend slightly the work of Kazarinoff and Ritt (1959) using the asymptotic analysis of Langer (1935, 1949). The generalization of these results to general convex bodies will then follow from a consideration of the creeping wave paths, the geodesics, on a prolate spheroid.

II

SCALAR DIFFRACTION BY A PROLATE SPHEROID

2.1 The Integral Representation

We suppose a scalar plane wave be incident on a prolate spheroid and study the solutions of the Helmholtz equation satisfying either the Neumann or Dirichlet boundary conditions. We use the prolate spheroidal coordinates (ξ, η, ϕ) where

$$\begin{cases} x = c \sqrt{\xi^2 - 1} \sqrt{1 - \eta^2} \cos \phi , \\ y = c \sqrt{\xi^2 - 1} \sqrt{1 - \eta^2} \sin \phi , \\ z = c \xi \eta , \end{cases} \quad (2.1)$$

where c is the semifocal distance. The equation of the spheroid is $\xi = \xi_0$ so the major and minor axes are given by

$$\begin{cases} a = c \xi_0 , \\ b = c \sqrt{\xi_0^2 - 1} . \end{cases} \quad (2.2)$$

The Helmholtz equation

$$(\nabla^2 + k^2)\psi = 0 \quad (2.3)$$

becomes, in the prolate spheroidal coordinates,

$$\frac{\partial}{\partial \xi} \left[(\xi^2 - 1) \frac{\partial \bar{\Psi}}{\partial \xi} \right] + \frac{\partial}{\partial \eta} \left[(1 - \eta^2) \frac{\partial \bar{\Psi}}{\partial \eta} \right] + \left[\frac{1}{\xi^2 - 1} + \frac{1}{1 - \eta^2} \right] \frac{\partial^2 \bar{\Psi}}{\partial \phi^2} + \gamma^2 \left[(\xi^2 - 1) + (1 - \eta^2) \right] \bar{\Psi} = 0, \quad (2.4)$$

where $\gamma = kc$. We require $\bar{\Psi}$ to be of the form

$$\bar{\Psi} = e^{i\vec{k} \cdot \vec{r}} + \bar{\Psi}_s \quad (2.5)$$

where $\bar{\Psi}_s$ satisfies the radiation condition and $\bar{\Psi}$ is to satisfy either of the boundary conditions

$$\bar{\Psi}(\xi_0, \eta, \phi) = 0,$$

or

$$\left. \frac{\partial \bar{\Psi}}{\partial \xi}(\xi, \eta, \phi) \right|_{\xi_0} = 0, \quad (2.6)$$

and when $e^{i\vec{k} \cdot \vec{r}}$ is the incident wave with

$$\vec{k} = k(\sin \theta_0, 0, \cos \theta_0). \quad (2.7)$$

We make the expansion

$$\bar{\Psi} = \sum_{m=-\infty}^{\infty} \bar{\Psi}_m e^{im\phi} \quad (2.8)$$

and consider the component equations

$$\frac{\partial}{\partial \xi} \left[(\xi^2 - 1) \frac{\partial \psi}{\partial \xi} \right] - \frac{m^2 \psi}{\xi^2 - 1} + \gamma^2 (\xi^2 - 1) \psi + \frac{\partial}{\partial \eta} \left[(1 - \eta^2) \frac{\partial \psi}{\partial \eta} \right] - \frac{m^2 \psi}{1 - \eta^2} + \gamma^2 (1 - \eta^2) \psi = 0. \quad (2.9)$$

With λ denoting a separation constant, (2.9) is seen to be equivalent to the separated equations

$$\left[\frac{\partial}{\partial \xi} (\xi^2 - 1) \frac{\partial}{\partial \xi} - \frac{m^2}{\xi^2 - 1} + \gamma^2 (\xi^2 - 1) - \lambda \right] u = 0 \quad (2.10a)$$

$$\left[\frac{\partial}{\partial \eta} (1 - \eta^2) \frac{\partial}{\partial \eta} - \frac{m^2}{1 - \eta^2} + \gamma^2 (1 - \eta^2) + \lambda \right] \omega = 0 \quad (2.10b)$$

From the solutions of (2.10a) which are asymptotically in ξ of the form

$$y_2(\xi, \lambda) \sim \frac{e^{-i\gamma\xi}}{\xi} \quad (2.11)$$

and

$$y_1(\xi, \lambda) \sim \frac{e^{i\gamma\xi}}{\xi}$$

we form either

$$\phi_2^D(\xi, \lambda) = y_1(\xi, \lambda) y_2(\xi_0, \lambda) - y_2(\xi, \lambda) y_1(\xi_0, \lambda) \quad (2.12a)$$

or

$$\phi_2^N(\xi, \lambda) = y_1(\xi, \lambda) y_2'(\xi_0, \lambda) - y_2(\xi, \lambda) y_1'(\xi_0, \lambda)$$

and

$$\phi_1(\xi, \lambda) = y_1(\xi, \lambda) \quad (2.13)$$

With the solutions ϕ_1 and ϕ_2 we then form the resolvent Green's function

$$G = \frac{\phi_2(\xi <) \phi_1(\xi >)}{(\xi^2 - 1)W(\phi_1, \phi_2)} \quad (2.14)$$

where $W(\phi_1, \phi_2)$ is the Wronskian of the solutions ϕ_1 and ϕ_2 . This becomes for the Dirichlet and Neuman boundary conditions

$$G^D = \frac{1}{2i\gamma\phi_1(\xi_0, \lambda)} \phi_2^D(\xi <, \lambda) \phi_1^D(\xi >, \lambda) \quad (2.15a)$$

$$G^N = \frac{1}{2i\gamma\phi_1'(\xi_0, \lambda)} \phi_2^N(\xi <, \lambda) \phi_1^N(\xi >, \lambda) \quad (2.15b)$$

Similarly, we take the solutions of (2.10b) which are regular at $\eta=1, \psi_1(\eta, -\lambda)$ and at $\eta=-1, \psi_{-1}(\eta, -\lambda)$, where

$$\psi_{-1}(\eta, -\lambda) = \psi_1(-\eta, -\lambda) \quad (2.16)$$

and form the resolvent Green's function

$$\tilde{G} = \frac{1}{(1-\eta^2)W(\psi_{-1}, \psi_1)} \psi_{-1}(\eta <, -\lambda) \psi_1(\eta >, -\lambda) \quad (2.17)$$

The solution ψ_m can then be represented by the plane wave limit of

$$\psi_m = \frac{1}{2\pi i} \int_{\Gamma} \tilde{G}(\eta, \eta', -\lambda) G(\xi, \xi', \lambda) d\lambda \quad (2.18)$$

2.2 The Asymptotic Analysis

We wish to evaluate (2.18) for γ large. We will parallel the work of Kazarinoff and Ritt (1959) making a turning point analysis of (2.6a) (Langer, 1949) and a Stokes phenomenon analysis of (2.6b) (Langer, 1935).

On putting

$$u = \frac{1}{\sqrt{\xi^2 - 1}} v, \quad (2.19)$$

Eq. (2.6a) becomes

$$v'' + \left[\gamma^2 - \frac{\lambda}{\xi^2 - 1} + \frac{1 - m^2}{(\xi^2 - 1)^2} \right] v = 0 \quad (2.20)$$

We define ξ_r by

$$\lambda = (\xi_r^2 - 1) \left(\gamma^2 + \frac{1 - m^2}{(\xi_r^2 - 1)^2} \right), \quad (2.21)$$

and rewrite (2.20),

$$v'' + \gamma^2 \frac{\xi^2 - \xi_r^2}{\xi^2 - 1} \left\{ 1 + \frac{m^2 - 1}{\gamma^2} \frac{1}{(\xi^2 - 1)(\xi_r^2 - 1)} \right\} v = 0 \quad (2.22)$$

Now for $m=0$ or for $m \ll \gamma$ the asymptotic forms of two solutions of (2.22) for $\gamma \rightarrow \infty$ with $\xi > 1$ are, after Kazarinoff and Ritt

$$v^{(j)} = \gamma^{1/6} e^{\mp i\gamma f(\xi_r)} V^j(\xi) \quad (j=1, 2) \quad (2.23)$$

$$V^j(\xi) = \sqrt{\frac{\pi}{2}} e^{\pm 5\pi i/12} \Psi(\xi) \xi^{1/3} H_{1/3}^{(j)}(\xi)$$

$$\xi = \gamma \int_{\xi_r}^{\xi} u(\tau) d\tau$$

$$u^2(\xi) = \frac{\xi^2 - \xi_r^2}{\xi^2 - 1}$$

$$\Psi = \left(\frac{\xi}{\gamma}\right)^{1/6} u^{-1/2}(\xi)$$

$$f = - \int_0^1 \frac{\sqrt{\frac{\xi_r^2 - t^2}{1 - t^2}}}{\sqrt{1 - t^2}} dt$$

As m grows large, each solution retains the same form with

$$\gamma \rightarrow \gamma_m = \gamma \sqrt{1 + \frac{m^2 - 1}{2\gamma(\xi_r^2 - 1)}} \quad (2.24)$$

provided ξ is near ξ_r . We note that for ξ increasing without bound, the asymptotic solutions have leading terms independent of m .

Since we shall wish to evaluate (2.18) as a residue series (where this is possible) we look for the roots of

$$\phi_1(\xi_0, \lambda) = 0$$

or

$$\phi_2'(\xi_0, \lambda) = 0$$

(2.25)

The zeros of these solutions occur at the zeros of

$$H_{1/3}^{(1)}(h_r) = 0$$

or

$$H_{1/3}^{(1)'}(h_r') = 0$$

(2.26)

From the definition of ζ these are the values of ξ_r such that

$$h_r \text{ or } h_r' = \gamma_m \int_{\xi_1}^{\xi_0} \sqrt{\frac{\xi^2 - \xi_r^2}{\xi^2 - 1}} d\xi$$

(2.27)

Moreover, if ξ_r is near to ξ_0

$$h_r \text{ or } h_r' \cong \gamma_m \frac{2}{3} \left(\frac{2\xi_0}{\xi_0^2 - 1} \right)^{1/2} (\xi_0 - \xi_r)^{3/2}$$

(2.28)

We now rewrite (2.23) using the Airy integral

$$\omega(t) = \sqrt{\frac{\pi}{3}} e^{2\pi i/3} (-t)^{1/2} H_{1/3}^{(1)}\left(\frac{2}{3}(-t)^{3/2}\right)$$

(2.29)

hence, with $\zeta = \frac{2}{3}(-t)^{3/2}$

$$v^{(1)}(\xi) = e^{-\pi i/4} e^{-i\gamma f(-t)} \left(\frac{\xi^2 - 1}{\xi^2 - \xi_r^2} \right)^{1/4} \omega(t) \quad (2.30)$$

We now approximate $v^{(1)}(\xi_0)$ and $v^{(1)'}(\xi_0)$ with ξ_r assumed to be near ξ_0 . From (2.28) we find

$$\xi_r - \xi_0 = \frac{1}{\gamma_m} \left(\frac{\gamma_m (\xi_0^2 - 1)}{2\xi_0} \right)^{1/3} t_{r_1} \quad (2.31)$$

where t_r is a root of

$$\omega(t) = 0, \quad (\text{Dirichlet problem})$$

or

$$\omega'(t) = 0 \quad (\text{Neumann problem}) \quad .$$

Substituting in (2.30)

$$v^{(1)}(\xi_0) \cong e^{-\pi i/4} e^{-i\gamma f(\xi_1)} \left(\frac{\gamma_m (\xi_0^2 - 1)}{2\xi_0} \right)^{1/6} \omega(t) \quad (2.32)$$

where we have made the approximation

$$\xi_r + \xi_0 \cong 2\xi_0 \quad .$$

On noting that

$$\left. \frac{\partial}{\partial \xi} \right|_{\xi_0} = \gamma_m \left(\frac{\gamma_m (\xi_0^2 - 1)}{2\xi_0} \right)^{-1/3} \frac{\partial}{\partial t}$$

we find

$$v^{(1)'}(\xi_0) \cong e^{-\pi i/4} e^{-i\gamma f(\xi_1)} \gamma_m \left(\frac{\gamma_m (\xi_0^2 - 1)}{2\xi_0} \right)^{-1/6} \omega'(t) \quad (2.33)$$

For the case $\gamma \gg m$, we put

$$\gamma_m \cong \gamma,$$

and define

$$M = \left(\frac{\gamma (\xi_0^2 - 1)}{2\xi_0} \right)^{1/3},$$

$$= \left(\frac{kb^2}{2a} \right)^{1/3}. \quad (2.34)$$

Hence (2.32) and (2.33) become

$$v^{(1)}(\xi_0) = e^{-i\pi/4} e^{-i\gamma f(\xi_1)} M^{1/2} \omega(t) \quad (2.35)$$

$$v^{(1)'}(\xi_0) = e^{-i\pi/4} e^{-i\gamma f(\xi_1)} M^{-1/2} \gamma \omega^1(t). \quad (2.36)$$

The angular Eq. (2.10b) is transformed by letting

$$\omega = \frac{1}{\sqrt{1-\eta^2}} z \quad (2.37)$$

and becomes

$$z'' + \left\{ \gamma^2 + \frac{\lambda}{1-\eta^2} + \frac{1-m^2}{(1-\eta^2)^2} \right\} z = 0. \quad (2.38)$$

As before, we put

$$\lambda = \gamma^2 (\xi_r^2 - 1) \left(1 + \frac{1 - m^2}{2} \right) \quad (2.39)$$

$$\gamma^2 (\xi_r^2 - 1)$$

so that (2.26) becomes

$$v'' + \frac{\gamma^2}{1 - \eta^2} \left\{ \xi_r^2 - \eta^2 + \frac{1 - m^2}{2} \right\} v + \frac{1 - m^2}{(1 - \eta^2)^2} v = 0 \quad (2.40)$$

or, by defining

$$\eta_r^2 = \xi_r^2 + \frac{1 - m^2}{2} \quad ,$$

$$v'' + \frac{\gamma^2}{1 - \eta^2} (\eta_r^2 - \eta^2) v + \frac{1 - m^2}{(1 - \eta^2)^2} v = 0 \quad . \quad (2.41)$$

Using the Stokes phenomenon analysis of Langer (1935) we may approximate the solution of (2.41) that is regular at $\eta=1$, as follows:

$$v \cong \sqrt{\frac{\sigma}{P\gamma}} J_m(\sigma) \quad (2.42)$$

where $\sigma = \gamma \int_{\eta}^1 P(t) dt$,

$$P^2(\eta) = \frac{\eta_r^2 - \eta^2}{1 - \eta^2} \quad .$$

The solutions of (2.10b) are

$$\psi_1(\eta, -\lambda) \cong \sqrt{\frac{\sigma}{\gamma}} \left[(1-\eta^2)(\eta_r^2 - \eta^2) \right]^{-1/4} J_m(\sigma) \quad (2.43a)$$

$$\psi_1(\eta, -\lambda) = \psi_1(-\eta, -\lambda) \quad (2.43b)$$

and

$$(1-\eta^2)W(\psi_{-1}, \psi_1) \cong \frac{2}{\pi} \cos(2\sigma(o)) (-)^m \quad (2.44)$$

The angular Green's function is from (2.44) and (2.17)

$$\tilde{G}(\eta, \eta', -\lambda) = \frac{\psi_{-1}(\eta<, -\lambda)\psi_1(\eta>, -\lambda)}{\frac{2}{\pi} \cos(2\sigma(o)) (-)^m} \quad (2.45)$$

We now form the integral representations for the surface fields using Eqs. (2.45) and (2.35) or (2.36). In the case of the Dirichlet boundary condition the normal derivative of the field on the surface is given by

$$\begin{aligned} \left. \frac{\partial \psi}{\partial n} \right|_{\xi_o}^D &= \frac{e^{-\pi i/4}}{M\pi} \sqrt{\frac{\gamma \xi_o}{2}} \frac{1}{\gamma} \left(\frac{1}{(1-\eta^2)(1-\eta_o^2)} \right)^{1/4} \sum_m e^{im(\phi + \pi)} \\ &\cdot \int_{\Gamma'} dt \frac{e^{-i\sigma(o)}}{2 \cos(2\sigma(o))} \left(\frac{1}{(\eta_r^2 - \eta^2)(\eta_r^2 - \eta_o^2)} \right)^{1/4} \frac{J_m(\sigma(\eta))J_m(\sigma(\eta_o))}{\omega(t)} \sqrt{\sigma(\eta)\sigma(\eta_o)} \end{aligned} \quad (2.46)$$

where we have noted that $\gamma f(\xi_r) = -\sigma(o)$ and that $d\lambda = 2\gamma \xi_o M dt$.

If we take the incident direction to be near axial so that θ_0 is small, we can truncate the m series at some $m=m_0$ so that $\gamma\xi_0$ can be chosen so large that $\gamma\xi_0 \gg m_0$. In this case we put

$$\eta_r = \xi_r \gg 1$$

and, except in oscillatory functions, put

$$\xi_r \cong \xi_0 .$$

Equation (2.43) then becomes

$$\begin{aligned} \left. \frac{\partial \psi^D}{\partial n} \right|_{\xi_0} &\cong \frac{e^{-\pi i/4}}{M\pi} \frac{1}{\sqrt{2}} \left(\frac{\xi_0^2}{\xi_0^2 - \eta^2} \right)^{1/4} \int_{\Gamma'} dt \frac{e^{-i\sigma(o)}}{2 \cos(2\sigma(o))} \cdot \sqrt{\sigma(\eta)\sigma(\eta_0)} \left(\frac{1}{(1-\eta^2)(1-\eta_0^2)} \right)^{1/4} \\ &\cdot \frac{1}{\omega(t)} \sum e^{im(\phi+\pi)} J_m(\sigma(\eta)) J_m(\sigma(\eta_0)) . \end{aligned} \quad (2.47)$$

We note that the summation in (2.47) can be done explicitly to give

$$\begin{aligned} \left. \frac{\partial \psi^D}{\partial n} \right|_{\xi_0} &= \frac{e^{-\pi i/4}}{M\pi} \frac{1}{\sqrt{2}} \left(\frac{\xi_0^2}{\xi_0^2 - \eta^2} \right)^{1/4} \cdot \frac{1}{(1-\eta^2)^{1/4}} \int_{\Gamma'} dt \frac{e^{-i\sigma(o)}}{2 \cos(2\sigma(o))} \sqrt{\sigma(\eta)} \\ &\cdot \frac{1}{\omega(t)} J_0 \left(\sqrt{\sigma^2(\eta) + \sigma^2(\eta_0) + 2\sigma(\eta)\sigma(\eta_0) \cos \phi} \right) , \end{aligned} \quad (2.48)$$

(Magnus and Oberhettinger, 1949).

With a similar argument the surface field satisfying the Neumann boundary conditions can be written as

$$\psi^N(\xi_0) = -\frac{e^{-\pi i/4}}{\pi} \frac{1}{\sqrt{2}} \left(\frac{\xi_0^2}{\xi_0^2 - \eta^2} \right)^{1/4} \frac{1}{(1-\eta^2)^{1/4}} \int_{\Gamma'} dt \frac{e^{-i\sigma(o)}}{2 \cos(2\sigma(o))} \sqrt{\sigma(\eta)}$$

$$\frac{1}{\omega'(t)} J_0 \left(\sum \right) \tag{2.49}$$

where we have put

$$\sum^2 = \sigma^2(\eta) + \sigma^2(\eta_0) + 2\sigma(\eta)\sigma(\eta_0) \cos \phi \tag{2.50}$$

From the definition of $\sigma(\eta)$ we write

$$\sigma(\eta) = \sigma(o) - \gamma(\eta) = \gamma \int_0^1 \sqrt{\frac{\xi_r^2 - x^2}{1-x^2}} dx - \gamma \int_0^\eta \sqrt{\frac{\xi_r^2 - x^2}{1-x^2}} dx \tag{2.51}$$

and expand about $\xi_r = \xi_0$

$$\gamma \int_0^\eta \sqrt{\frac{\xi_r^2 - x^2}{1-x^2}} dx \cong ka \int_0^\eta \sqrt{\frac{1-\epsilon x^2}{1-x^2}} dx + M \int_0^\eta \frac{dx}{\sqrt{(1-\epsilon x^2)(1-x^2)}} t. \tag{2.52}$$

The first term on the right of (2.52) is the wave number k multiplied by the path length measured from $\eta = 0$ to η along a curve of constant ϕ ; the second term is the reduced distance given by Fock (1946) multiplied by t_r . Rewriting

$$\zeta(\eta) = kS(\eta) + \zeta(\eta) t_r \tag{2.53}$$

where

$$S(\eta) = a \int_0^\eta \sqrt{\frac{1-\epsilon^2 x^2}{1-x^2}} dx \tag{2.54}$$

$$\zeta(\eta) = \int_0^{S(\eta)} \left(\frac{kR(s)}{2}\right)^{1/3} \frac{ds}{R(s)} \tag{2.55}$$

$$= M \int_0^\eta \frac{dx}{\sqrt{(1-\epsilon^2 x^2)(1-x^2)}}$$

with $R(s)$ the radius of curvature at $S(\eta)$ along a curve of constant ϕ .

Since the path of integration Γ' is such that $\text{Im}t > 0$ we have from (2.52) that $\text{Im}\sigma(o) > 0$ and we make the convergent expansion

$$\frac{e^{-i\sigma(o)}}{2 \cos(2\sigma(o))} = e^{i\sigma(o)} \sum_{l=0}^{\infty} (-)^l e^{4il\sigma(o)} \tag{2.56}$$

We now consider the forms (2.48) and (2.49) for η near enough zero so that $|\sigma(\eta)| \gg 1$. In this case, we may use the asymptotic form of the Bessel function

and approximate \sum by

$$\begin{aligned} \sum &\cong \sigma(\eta) + \sigma(\eta_0) \cos \phi \\ &= \sigma(o) - \zeta(\eta) + \sigma(\eta_0) \cos \phi \end{aligned} \tag{2.57}$$

in oscillatory functions and

$$\sum \cong \sigma(\eta) \tag{2.58}$$

in non-oscillatory functions. On substituting the asymptotic form of the Bessel function and the expansion (2.56) in (2.48) we have

$$\begin{aligned} \left. \frac{\partial \psi}{\partial n} \right|_{\xi_0}^D &= \frac{1}{2M\pi^{3/2}} \left(\frac{\xi_0^2}{\xi_0^2 - \eta^2} \right)^{1/4} \frac{1}{(1-\eta^2)^{1/4}} \sum_{l=0}^{\infty} (-1)^l \int_{\Gamma} \frac{dt}{\omega(t)} \cdot \\ &\cdot e^{4il\sigma(o)} \left\{ e^{i(\sigma(\eta) - \sigma(\eta_0) \cos \phi)} \quad e^{-i(2\sigma(o) - \sigma(\eta) + \sigma(\eta_0) \cos \phi)} \right\}. \end{aligned} \tag{2.59}$$

Using the forms (2.51) and (2.53) and noting that for η_0 near to one

$$\sigma(\eta_0) \cong kb\theta_0 + \frac{a}{b} Mt\theta_0 \tag{2.60}$$

and rewriting

$$\sigma(o) = k\frac{L}{4} + \frac{\Xi}{4} t,$$

where

$$\frac{L}{4} = a \int_0^1 \frac{\sqrt{1 - \epsilon x^2}}{\sqrt{1-x^2}} dx$$

is one quarter of the distance around, the spheroid for $\phi = \text{constant mod } \pi$ and

$$\Xi = M \int_0^1 \frac{dx}{\sqrt{(1-\epsilon^2 x^2)(1-x^2)}}$$

is the corresponding reduced distance, we have

$$\begin{aligned} \left. \frac{\partial \psi^D}{\partial n} \right|_{\xi_0} &= \frac{1}{2M\pi^{3/2}} \left(\frac{\xi_0^2}{\xi_0^2 - \eta^2} \right)^{1/4} \frac{1}{(1-\eta^2)^{1/4}} \sum_{l=0}^{\infty} (-)^l \int_{\Gamma} \frac{dt}{\omega(t)} e^{i\ell kL + 4i\ell \Xi t} \\ &\cdot \begin{cases} e^{i[kS(\eta) - kb\theta_0 \cos\phi]} e^{i[\zeta(\eta) - \frac{a}{b} M\theta_0 \sin\phi]t} e^{-i\left[k\frac{L}{2} - kS(\eta) + kb\theta_0 \cos\phi\right]t} \\ e^{i\left[\frac{\Xi}{4} - \zeta(\eta) + \frac{a}{b} M\theta_0 \sin\phi\right]t} \end{cases} \end{aligned} \quad (2.61)$$

If we now evaluate (2.61) on the shadow boundary and include only the first term in the back scattered direction we have an expression of the form

$$\begin{aligned} I_B(\eta_1, \phi_1) &= \frac{1}{2M\pi^{3/2}} \left(\frac{\xi_0^2}{\xi_0^2 - \eta_1^2} \right)^{1/4} \frac{1}{(1-\eta_1^2)^{1/4}} (-i)e^{i\left[k\frac{L}{2} - kS(\eta_1) + kb\theta_0 \cos\phi_1\right]t} \\ &\cdot \int_{\Gamma} \frac{dt}{\omega(t)} e^{i\left[\frac{\Xi}{4} - \zeta(\eta_1) + \frac{a}{b} M\theta_0 \sin\phi_1\right]t} \end{aligned} \quad (2.62)$$

where (η_1, ϕ_1) are the coordinates of the shadow boundary and

$$\eta_1 \cong \frac{a}{b} \theta_o \cos \phi_1 . \quad (2.63)$$

Since η_1 is small we make the approximation

$$\begin{aligned} S(\eta_1) &\cong a\eta_1 \\ &= \frac{a}{b} \theta_o \cos \phi_1 \end{aligned} \quad (2.64)$$

We will neglect the terms of order θ_o in the t-integration and include terms of this order only in the phase. This gives the approximation

$$I_B(\eta_1, \phi_1) \cong I_B(o) e^{ik \frac{c}{b} \theta_o \cos \phi_1} \quad (2.65)$$

where $I_B(o)$ is the value taken on the shadow boundary for symmetric illumination.

The back scattered field will be proportional to the integral of (2.65) over the azimuthal angle ϕ_1 from 0 to 2π , that is

$$\psi_B(\theta_o) \sim I_B(o) \int_0^{2\pi} e^{ik \frac{c}{b} \theta_o \cos \phi_1} d\phi_1 . \quad (2.66)$$

But the zeroth order Bessel function has the integral representation

$$J_0(z) = \frac{1}{2\pi} \int_0^{2\pi} e^{iz \cos t} dt$$

so that the leading creeping wave term in the back scattered field is given

$$\psi_{B_0}(\theta) \cong \psi_B(o) J_0\left(k \frac{c}{b} \theta\right)^2 .$$

There is an analogous expression for the Neumann boundary condition.

We have then, that for near axial illumination of the spheroid that the leading creeping wave term in the back scattered field is given by the field arising from symmetric illumination multiplied by the shape factor $J_0\left(k \frac{c}{b} \theta\right)^2$. We note that this factor takes the value of one for either symmetric illumination, $\theta = 0$, or for the sphere limit, $c = 0$.

REFERENCES

Fock, V. A. (1946), J. Phys. USSR, 10, 1.

Kazarinoff, N. D. and R. K. Ritt (1959), Ann. of Phys., 6, 277.

Keller, J. B. (1953), Symposium on Microwave Optics, McGill University.

Langer, R. E. (1935), Trans. Amer. Math. Soc., 37, 397.

Langer, R. E. (1949), Trans. Amer. Math. Soc., 67, 461.

Magnus, W. and F. Oberhettinger (1949), Special Functions of Mathematical Physics, Chelsea, New York.

DOCUMENT CONTROL DATA - R&D

(Security classification of title, body of abstract and indexing annotation must be entered when the overall report is classified)

1. ORIGINATING ACTIVITY (Corporate author) The University of Michigan College of Engineering, Department of Electrical Engineering Radiation Laboratory, Ann Arbor, Michigan		2a. REPORT SECURITY CLASSIFICATION Unclassified	
3. REPORT TITLE Near Caustic Surface Field		2b. GROUP	
4. DESCRIPTIVE NOTES (Type of report and inclusive dates) Technical Report			
5. AUTHOR(S) (Last name, first name, initial) R. F. Goodrich			
6. REPORT DATE May 1966		7a. TOTAL NO. OF PAGES 20	7b. NO. OF REFS 6
8a. CONTRACT OR GRANT NO. AF 04(694)-683		8a. ORIGINATOR'S REPORT NUMBER(S) 7030-9-T	
b. PROJECT NO.		8b. OTHER REPORT NO(S) (Any other numbers that may be assigned this report)	
c.			
d.			
10. AVAILABILITY/LIMITATION NOTICES Qualified Requestors May Obtain Copies of This Report From DDC			
11. SUPPLEMENTARY NOTES		12. SPONSORING MILITARY ACTIVITY Ballistic Systems Division Air Force Systems Command United States Air Force, Norton Air Force Base, California	
13. ABSTRACT At high frequency the acoustic surface fields for plane wave illumination of a prolate spheroid are found for near symmetric illumination. The surface caustic, in contrast to the symmetric case, is found to be diffuse. The values of the surface fields are used to find the modification of the creeping wave contribution to back scattering.			

14. KEY WORDS	LINK A		LINK B		LINK C	
	ROLE	WT	ROLE	WT	ROLE	WT
Surface Field Caustic						

INSTRUCTIONS

1. ORIGINATING ACTIVITY: Enter the name and address of the contractor, subcontractor, grantee, Department of Defense activity or other organization (*corporate author*) issuing the report.

2a. REPORT SECURITY CLASSIFICATION: Enter the overall security classification of the report. Indicate whether "Restricted Data" is included. Marking is to be in accordance with appropriate security regulations.

2b. GROUP: Automatic downgrading is specified in DoD Directive 5200.10 and Armed Forces Industrial Manual. Enter the group number. Also, when applicable, show that optional markings have been used for Group 3 and Group 4 as authorized.

3. REPORT TITLE: Enter the complete report title in all capital letters. Titles in all cases should be unclassified. If a meaningful title cannot be selected without classification, show title classification in all capitals in parenthesis immediately following the title.

4. DESCRIPTIVE NOTES: If appropriate, enter the type of report, e.g., interim, progress, summary, annual, or final. Give the inclusive dates when a specific reporting period is covered.

5. AUTHOR(S): Enter the name(s) of author(s) as shown on or in the report. Enter last name, first name, middle initial. If military, show rank and branch of service. The name of the principal author is an absolute minimum requirement.

6. REPORT DATE: Enter the date of the report as day, month, year; or month, year. If more than one date appears on the report, use date of publication.

7a. TOTAL NUMBER OF PAGES: The total page count should follow normal pagination procedures, i.e., enter the number of pages containing information.

7b. NUMBER OF REFERENCES: Enter the total number of references cited in the report.

8a. CONTRACT OR GRANT NUMBER: If appropriate, enter the applicable number of the contract or grant under which the report was written.

8b, 8c, & 8d. PROJECT NUMBER: Enter the appropriate military department identification, such as project number, subproject number, system numbers, task number, etc.

9a. ORIGINATOR'S REPORT NUMBER(S): Enter the official report number by which the document will be identified and controlled by the originating activity. This number must be unique to this report.

9b. OTHER REPORT NUMBER(S): If the report has been assigned any other report numbers (*either by the originator or by the sponsor*), also enter this number(s).

10. AVAILABILITY/LIMITATION NOTICES: Enter any limitations on further dissemination of the report, other than those

imposed by security classification, using standard statements such as:

- (1) "Qualified requesters may obtain copies of this report from DDC."
- (2) "Foreign announcement and dissemination of this report by DDC is not authorized."
- (3) "U. S. Government agencies may obtain copies of this report directly from DDC. Other qualified DDC users shall request through _____."
- (4) "U. S. military agencies may obtain copies of this report directly from DDC. Other qualified users shall request through _____."
- (5) "All distribution of this report is controlled. Qualified DDC users shall request through _____."

If the report has been furnished to the Office of Technical Services, Department of Commerce, for sale to the public, indicate this fact and enter the price, if known.

11. SUPPLEMENTARY NOTES: Use for additional explanatory notes.

12. SPONSORING MILITARY ACTIVITY: Enter the name of the departmental project office or laboratory sponsoring (*paying for*) the research and development. Include address.

13. ABSTRACT: Enter an abstract giving a brief and factual summary of the document indicative of the report, even though it may also appear elsewhere in the body of the technical report. If additional space is required, a continuation sheet shall be attached.

It is highly desirable that the abstract of classified reports be unclassified. Each paragraph of the abstract shall end with an indication of the military security classification of the information in the paragraph, represented as (TS), (S), (C), or (U).

There is no limitation on the length of the abstract. However, the suggested length is from 150 to 225 words.

14. KEY WORDS: Key words are technically meaningful terms or short phrases that characterize a report and may be used as index entries for cataloging the report. Key words must be selected so that no security classification is required. Identifiers, such as equipment model designation, trade name, military project code name, geographic location, may be used as key words but will be followed by an indication of technical context. The assignment of links, rules, and weights is optional.

