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16. Abstract <p>This document is a User's Manual for the computer-based mathematical simulation program entitled "Truck and Tractor-Trailer Dynamic Response Simulation - T3DRS:V1" developed in 1979 by the Highway Safety Research Institute/University of Michigan. This manual provides an introduction to the simulation program with a description of its external characteristics sufficient for a user to submit a run and interpret the output obtained. A separate Programmer's Manual (FHWA-RD-79-126) describes the internal function of the program in terms of its flow and the various subroutines used.</p> <p>Final reports for this contract are available under the titles: "Simulation of Effects of Increased Truck Size and Weight," Summary Report FHWA-RD-79-123, Technical Report FHWA-RD-79-124.</p>					
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The computer simulation program described in this manual is derived from computer-based mathematical models for trucks and tractor-trailers developed since 1971 at the Highway Safety Research Institute, The University of Michigan. The models were developed in conjunction with earlier computer simulation programs originated in the Motor Truck Braking and Handling Research Program sponsored by the Motor Vehicle Manufacturers Association. The opportunity to consolidate the earlier programs into a single program capable of representing vehicles from trucks to triples combinations was provided by the Federal Highway Administration under the project "Simulation of Effects of Increased Truck Size and Weight." Portions of the program revisions were performed by Dr. James Bernard and Mr. Marty Vanderploeg of Michigan State University.

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## 1.0 GENERAL INFORMATION

### 1.1 Purpose of the Manual

This document is a User's Manual for the computer-based mathematical simulation program entitled "Truck and Tractor-Trailer Dynamic Response Simulation - T3DRS:VI" developed in 1979 by the Highway Safety Research Institute/University of Michigan. This manual provides an introduction to the simulation program with a description of its external characteristics sufficient for a user to submit a run and interpret the output obtained. A separate Programmers Manual describes the internal function of the program in terms of its flow and the various subroutines used.

### 1.2 Background

Since 1971, the HSRI has been conducting research under the sponsorship of the Motor Vehicle Manufacturers Association (MVMA) to develop computer-based methods for analyzing and predicting the directional and braking response of commercial motor vehicles. The initial phase of this research dealt with modeling the braking performance of commercial vehicles and was reported in Reference [1]\* (Phase I). The second phase extended vehicle modeling to allow for directional response and was reported in Reference [2] (Phase II). The continuation of research into braking performance led to additional refinements in the braking simulation which were reported in Reference [3] (Phase III). In total, this research under the auspices of MVMA led to four separate computer simulation models:

- Straight Truck Braking Model (Phase I & III)
- Tractor-Trailer Braking Model (Phase I & III)
- Straight Truck Directional Response Model (Phase II)
- Tractor-Trailer Directional Response Model (Phase II)

Though all programs evolved from the same approach to vehicle modeling, separate programs were prepared and maintained.

In 1977-78, the Federal Highway Administration (FHWA) contracted with the HSRI to obtain braking and directional response simulations of trucks

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\*Cited References are listed in Section 6.0 of this Manual.

and tractor-trailers of the form of the Phase I, II, and III models. Requirements to add one or two full trailers (doubles and triples) to the tractor-semitrailer model were cause for reformulating the computer simulation model for the purposes of:

- Consolidating all vehicle combinations into one program
- Improving the input/output format
- Simplifying the model to include only the most relevant aspects as determined from the intervening research

That work led to the new simulation program using the same model. The program, described here, is designated as "The Truck and Tractor-Trailer Dynamic Response Simulation - T3DRS:V1." Any subsequent changes to this program will be designated by a change in Version number.

### 1.3 Engineering Units

Throughout the T3DRS:V1 program, the English system of units is used. With the exceptions listed below, all input data are given in units of pounds, inches, degrees and seconds. Masses and weights are in units of pounds, with a gravitational constant of 386 in/sec/sec assumed. The units for input data parameters are defined in the input data echo.

Exceptions:

- 1) Input for the initial velocity is given in units of ft/sec.
- 2) Input describing trajectory points for the path-follower steering mode are defined in terms of feet lateral versus feet longitudinal.
- 3) Longitudinal and lateral road slope is defined in percent grade (Rise/Run).
- 4) Certain tandem-axle parameters are described in units of percent.

Output data units are defined on the printed output pages. In general, the same units are used throughout, although the vehicle position, velocity and acceleration variables use the length dimensional unit of "ft."

#### 1.4 Computer Requirements

The T3DRS:V1 program is written for use on any large-scale computer system, and requires only one input and one output device. The source code is in level-G Fortran IV language, with 600,000 bytes of memory required for loading. Support software must include the IBM Scientific Subroutine Package (HPCG, SMPY, LOC, GMPRD and GMADD).

Copies of the program are available to the public by contacting the Physical Factors Division, Highway Safety Research Institute, The University of Michigan, Huron Parkway and Baxter Road, Ann Arbor, Michigan 48109.



## 2.0 APPLICATION

### 2.1 Description of the Program

The T3DRS:V1 program is a time domain mathematical simulation of a truck/tractor, a semitrailer and up to two full trailers. The vehicles are represented by differential equations derived from Newtonian mechanics that are solved for successive time increments by digital integration.

The program is written in a generalized fashion to allow simulation of a large number of vehicle configurations. The first vehicle is the power unit and may be a truck or tractor, both of which may carry payload. As a single unit with no payload, it is equivalent to an empty truck or bobtail tractor. With payload, it is a truck, which, with a semitrailer as well, simulates a car hauler, dromedary tractor, etc. The second unit is always a semitrailer (i.e., current models do not include a truck with full trailer). The third and fourth units are full trailers consisting of semitrailers on either a fixed or converter dolly. Separate payload may be specified for each trailer.

The truck/tractor unit is distinguished by the fact that it can have only a single front axle with single tires, and can be arbitrarily steered. All other axles on the vehicle combination can be represented as single or tandem axles with single or dual wheel sets.

The mathematical model (see Appendix E) incorporates up to 71 degrees of freedom. The number of degrees of freedom are dependent on the vehicle configuration and derive from the following:

- Six degrees of freedom (three translational and three rotational) for the truck/tractor sprung mass
- Three degrees of freedom for the semitrailer (the three other degrees of freedom of the semitrailer are effectively eliminated by dynamic constraints at the hitch)
- Five degrees of freedom for each of the two full trailers allowed.



- Two degrees of freedom (vertical and roll) for each of the 13 axles allowed
- A wheel rotational degree of freedom for each of the 26 wheels allowed

The motion of each of the sprung masses is determined from the summation of forces and moments upon it arising from the tires (acting through the unsprung mass of the axle and suspension), gravity and the hitch point constraints. Small angle assumptions are made in the derivation of the mathematical equations so that the simulation can be validly applied only up to a maneuver limit at which wheel lift-off occurs.

## 2.2 Uses of the Program

The great versatility of the T3DRS:VI program in representing commercial vehicle types and components in steering and braking maneuvers gives it great utility. As indicated previously, it can be used to simulate the following vehicle configurations:

Straight truck, empty and loaded

Bobtail tractor

Tractor-semitrailer (3 to 5 axles), empty and loaded

Tractor-semitrailer-full trailer (5 to 9 axles), empty and loaded

Tractor-semitrailer-full trailer-full trailer (7 to 13 axles), empty and loaded

For simulation of braking performance, the program incorporates state-of-the-art representation of truck air brake systems, antilock wheel control systems and tire-road friction models. Typical examples of braking studies for which it can be or has been used are:

- 1) Stopping distance performance
- 2) Effects of brake timing



- 3) Dynamic behavior in braking
- 4) Comparisons of antilock wheel control logic
- 5) Influence of tire-road friction coupling
- 6) Split friction surfaces
- 7) Brake proportioning
- 8) Tandem-axle effects on braking limits

For simulation of cornering performance behavior, the program incorporates state-of-the-art representations of truck tire lateral force characteristics (with roll-off effects during combined braking), and vehicle suspension properties of significance to cornering behavior. Typical examples of studies involving cornering are as follows:

- 1) Understeer/oversteer properties of commercial vehicles
- 2) Determining cornering limits
- 3) Assessing tandem-axle effects on cornering
- 4) Jackknife prediction
- 5) Effects of suspension properties on cornering and cornering limits
- 6) Accident simulation

In addition to the above, the program can be operated open-loop (defined steer angle inputs) or closed-loop (defined path input), and on roads of specified grade or cross-slope.

### 2.3 Operation

Operation of the T3DRS:V1 program is accomplished by submission of the necessary job control instructions followed by a list of input parameters. The specific job control instructions required are dependent on the user's computer system and whether batch or remote job entry is being used. However, the input parameter list is common to all and is described in Section 3.0 of this Manual.

The program commences by reading the input list containing parametric data describing the vehicle configuration, initial conditions, steering and braking inputs, the output desired, and the road conditions. As input data is read, the data is normally "echoed" as the first pages of output. At the completion of the input read process, the program calculates necessary properties of the total vehicle combination and prints a page of output containing a summary of those vehicle properties. The program then "runs," solving the differential equations of motion for the vehicle until the vehicle reaches a full stop, a default stop (such as rollover), or until the designated maximum simulation time is reached. At various points during the run, simulation output is printed, which (at the option of the user) may include time-based values for the vehicle motion variables, tire forces at each axle, braking conditions on each axle, tire cornering conditions, and the suspension motions and forces.

#### 2.4 Validity

The validity of T3DRS:V1, like any computer program, is dependent on the accuracy and execution of program statements, the capabilities of the simulation models, and the quality of the vehicle and maneuver descriptions defined by the input data.

Every effort, of course, is made to ensure that the program statements are correct and result in solution of the problem to a reasonable level of precision. The time steps have been selected so that round-off and truncation errors do not substantially influence the precision of the calculated results. Nevertheless, if programming errors are discovered, the user should contact the Physical Factors Division, Highway Safety Research Institute, The University of Michigan, Ann Arbor, Michigan.

The modeling used in the simulation is effectively state-of-the-art, reflecting the most practical approaches to mathematical representation of commercial vehicles for braking and handling studies. Over the years, modeling has grown more in sophistication than in detail. For example, early models for truck brake systems extending to mechanical details within the individual brakes have proven no more capable of predicting braking performance than the "black box" representation as a pressure-input, torque-output device. Hence, the latter approach is used in T3DRS:V1, with a

substantial saving in the complexity associated with understanding and using the simulation. With nearly every component model used in the simulation, there are instances where more modeling details would be appropriate for the study at hand; yet, provision for every instance would result in a simulation for which the input data requirements would be untenable. To some extent, these needs are provided for in T3DRS:V1 by allowing optional use of lookup tables, in lieu of a single numerical parameter, as means to describe component characteristics in more detail when needed.

Finally, the ultimate determinant of validity is the user-supplied input data and the interpretation applied to the results. Properly used, the program is capable of validly predicting most aspects of braking performance and directional response in maneuvers up to the limits of wheel lift-off. In the special case where a direct comparison between a vehicle and simulation (i.e., validation) is intended, an iterative process is often involved as the first comparisons of simulation and test reveal unexpected differences, which, when examined, are traced to inaccuracies or errors in the experimental measurements or program input. Fortunately, the usefulness of these simulation programs are not dependent on every user going through the same process. In most applications, the user can assume, for example, a given tire characteristic and investigate vehicle performance with that tire, knowing that it is typical, but yet, not precisely equivalent to any specific tire on hand. Much of the utility of computer simulation programs derives not from absolute prediction of a certain vehicle/test maneuver situation (as required for validation), but as a tool for studying generalized performance and sensitivity of performance to the vehicle parameters.

In this general sense, the T3DRS:V1 program can be expected to yield valid measures of the braking and handling performance comparison when specific vehicle parameters are changed. The T3DRS:V1 program has been tested against other simulations, including its predecessors, which in turn have proven capable of reasonably duplicating actual vehicle performance. The user is referred to the following references for examples of the use and validation of those programs:

	<u>References*</u>
Straight Truck Braking	1, 2, 4, 8, 9, 11
Straight Truck Cornering and Braking	2, 10
Straight Truck Cornering	5
Tractor-Trailer Braking	1, 2
Tractor-Trailer Cornering and Braking	2, 10
Tractor-Trailer Cornering	6
Tractor-Trailer-Full Trailer Cornering	7

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\*Section 6.0



## 3.0 PROGRAM INPUT

### 3.1 General

Program operation is effectively accomplished by input of a parametric data list, along with the necessary job control instructions. This section provides a detailed description of the input data required. Appendix C provides a ready reference list of input parameters. Sample input lists covering the various options are provided in the text and in Appendices A and B.

Depending on the vehicle configuration, the input data list will contain the following elements:

- Title Line (up to 80 characters)
- Simulation Operation Parameters
- Truck/Tractor Parameters
- Truck/Tractor Front Suspension and Axle
- Truck/Tractor Front Tires and Wheels
- Truck/Tractor Rear Suspension and Axle
- Truck/Tractor Rear Tires and Wheels
- Truck/Tractor Front and Rear Brake Parameters (Optional - used only when braking is called)
- First Trailer Parameters (Optional)
- First Trailer Rear Suspension and Axles (Optional)
- First Trailer Rear Tires and Wheels (Optional)
- First Trailer Rear Brake Parameters (Optional)
- Second Trailer Parameters (Optional)
- Second Trailer Dolly, Suspension and Axles (Optional)
- Second Trailer Dolly Tires and Wheels (Optional)
- Second Trailer Rear Suspension and Axles (Optional)
- Second Trailer Rear Tires and Wheels (Optional)
- Second Trailer Front and Rear Brake Parameters (Optional)
- Third Trailer Parameters (Optional)  
(Same as Second Trailer)

The input data is identified only by its position in the input list and hence must be ordered exactly to match the vehicles and options used in the simulation. Errors in the input list will result either in a read fault (with possible system interrupt and abort of the program), or in simulation of the wrong conditions. Every effort has been made to define the input sequence and its alteration with various options in this section. Example input lists are shown throughout the Manual for reference by the user in compiling an input data list.

3.1.1 Tandem-Axle Option. To suit the simulation to the great variety of commercial vehicles, either single or tandem axles may be specified for any suspension in the total vehicle configuration, except on the front (steering) axle of the truck/tractor. Details on use of the tandem suspension are provided in Section 3.3.4.

3.1.2 Table Lookup Option. It is often desirable to include non-linear characteristics of vehicle components (particularly for tires, springs, and brakes) in the model simulated. For such parameters a table lookup option can be used, allowing the parameter to be described by a multiple point approximation over the range of interest rather than assigning to it a single valued linear characteristic. The program thence interprets the dependent variable's value when needed using linear interpolation methods. In the event the program exceeds the range of the table, the dependent variable is limited to the last entry in the table.

The table lookup option may be used with the following input parameters:

- Suspension spring rate
- Tire cornering stiffness
- Tire longitudinal stiffness
- Brake torque

The table lookup option is called by entry of a negative whole number value for the parameter. The negative sign identifies it as a table lookup and the numerical value identifies that table and distinguishes it from other tables in the input list. The table is then entered in the input list immediately following the calling point. For the two-dimensional tables (spring rates and brakes), the first line entry in the table is an integer

value equal to the number of data sets to follow, each being a separate line entry of independent versus dependent variable values. Tire parameter tables are more complicated and are explained in Section 3.3.3.

The same table can be used at subsequent points in the input list by entry of the negative whole number identifying that table. The table values should not be re-entered at these subsequent calling points.

More detailed instruction for entering lookup tables are provided in Sections 3.3.2, 3.3.3 and 3.3.6.

3.1.3 Side-to-Side Option. In most simulation studies, a vehicle has symmetric properties left and right. Nevertheless, it is occasionally of interest to investigate the influence of side-to-side differences in springs, tires, brakes, etc. While vehicle mass properties are modeled as symmetric about the vehicle centerline, most components that are paired, one to each side of the vehicle, may be assigned different parametric values. Different values side-to-side may be assigned for the following parameters:

- Steer angle inputs
- Suspension spring rate
  - viscous damping
  - coulomb friction
- Tire cornering stiffness
  - longitudinal stiffness
  - camber stiffness
  - aligning moment
  - spring rate
  - loaded radius
  - polar moment of inertia
- Brake time lag
  - rise time
  - torque
  - antilock systems

In normal input of those parameters, one entry causes the program to assign that value to both sides of the vehicle. The side-to-side option is exercised by making a double entry on the line, in which case the first value is assigned to the left side of the vehicle and the second to the right. A zero

value cannot be assigned to the right-hand side with a nonzero left-hand side value due to the way this option operates, but zero values can be effectively obtained by entry of very small nonzero values. The side-to-side option can also be combined with the table lookup option. By entry of two negative values, tables are assigned to both the left and right sides. The tables for the left and right sides are entered in sequence immediately after the calling line. More detailed instruction for side-to-side entry options are provided in Sections 3.2, 3.3.2, 3.3.3, and 3.3.6.

### 3.2 Simulation Operation Parameters

The first line entry in the input list is always a user-supplied title line consisting of up to 80 alphanumeric characters. Thereafter, the Simulation Operation Parameters are entered and subsequently echoed as the first page of output, as shown in Figure 1.

The first line of the Simulation Operation Parameters is VEHICLE CONFIGURATION defined by the number of trailers, entered in I2 format, which indicates to the program the extent of input to be expected. Zero trailers indicates a single unit straight truck, which is also equivalent to a bobtail tractor. An "01" entry indicates a tractor/semitrailer. An "02" entry indicates a tractor/semitrailer/full trailer (doubles) configuration. An "03" indicates tractor/semitrailer/full trailer/full trailer (triples) configuration, the maximum number of vehicles allowed.

The second line is INITIAL VELOCITY in units of ft/sec (F15.3 format). At the initiation of the simulation run, all vehicles are in a straight-line configuration, moving forward at the indicated velocity.

The next entries define the steering input to the simulation. Either front-axle steering inputs (open-loop) or a path-following (closed-loop) mode are selected by the respective entry of a positive or negative integer value for STEER TABLE (NUMBER OF LINES) (I3 format). The numerical value of the entry specifies the number of lines appearing in the subsequent table. A "000" entry indicates no steering is involved in the maneuver, hence, no table entries are made and the vehicle performs as if the steering wheel were held fixed in the straight-ahead position (i.e., no steering action occurs except as a result of front suspension roll steer). When a nonzero number of lines is given, a table of the prescribed length must follow according to the following instruction.

-----  
 SIMULATION OPERATIONS PARAMETERS:  
 -----

VEHICLE CONFIGURATION (NUMBER OF TRAILERS - ENTER 0 FOR A STRAIGHT TRUCK) 1  
 INITIAL VELOCITY (FT/SEC) 66.00  
 STEER TABLE (NUMBER OF LINES): POSITIVE - STEER ANGLE TABLE, NEGATIVE - PATH FOLLOWER TABLE 3  
 TABLE OPTIONS:  
 TIME (SEC) LEFT WHEEL (DEG) RIGHT WHEEL (DEG)  
 0.0 0.0 0.0  
 0.10 1.00 1.00  
 1.00 1.00 1.00

TREADLE RESPONSE TABLE (NUMBER OF LINES) 2  
 TABLE OPTIONS:  
 TIME (SEC) PRESSURE (PSI)  
 0.0 0.0  
 1.00 0.0

MAXIMUM SIMULATION TIME (SEC) 0.0  
 TIME INCREMENT OF OUTPUT (SEC) 0.10  
 ROAD KEY = 0 : FLAT ROAD.

OUTPUT PAGE OPTION KEYS: 0 DELETES PAGES  
 -----  
 SPRING MASS POSITION 0 SPRING MASS VELOCITY 0 SPRING MASS ACCELERATION 0  
 TIRE FORCES PAGES 0 BRAKE SUMMARY PAGES 0 LATERAL PAGES 0  
 UNSPRUNG MASS PAGES C

Figure 1. Example of simulation operation parameters.

Steer Table (positive numerical entry) - Each line is a set of time (sec) versus left-wheel steer angle (deg) and right-wheel steer (deg) in 3F10.3 format as shown in Figure 1. If both wheels are to be steered identically, only the time and left-wheel angles are required; the absence of the right-wheel steer angle entry causes it to be assigned the same value as left-wheel steer angle. Up to 25 lines of table are allowed. Steer angles are obtained from the table at each time increment by linear interpolation. The table should always start off with an entry for zero time to assure definition of steer angles throughout the simulation run and be listed in ascending order with time. If simulation time exceeds the last time entry in the table, the last steer angle values are retained.

Path-Follower Table (negative numerical entry) - Each line is a pair of X (inertial forward) and Y (inertial lateral) path coordinates (in units of ft, 2F10.2 format) defining the desired path to be followed by the vehicle during closed-loop operation as shown in Figure 2. Linear interpolation is used by the program to determine path coordinates between entered points.

Following the last line of the closed-loop path-follower table, two additional parameters are entered which permit the program user to exert influence over the manner in which the closed-loop driver model functions. The first of these parameters, DRIVER TRANSPORT LAG (F10.4 format) generates a transport time lag (sec) within the controller to provide a simple means for representing human operator lag characteristics when desired. Values for this parameter should range between 0.0 and 0.5 (sec). Values larger than about 0.5 sec will generally produce an unrealistic and potentially unstable vehicle/driver system, and are hence not allowed. A zero entry inactivates the transport lag feature.

The remaining closed-loop parameter, END OF PREVIEW INTERVAL, (F10.4 format) indicates the distance ahead in time (sec) that the driver model looks during closed-loop steering operation. Hence, a value of 1.0 sec for this parameter would cause the driver model to look ahead over a 1 sec interval, or an equivalent maximum distance of 88 ft at a forward speed of 60 mph. Larger values for this parameter will produce a less responsive, more heavily damped system behavior during closed-loop operation. Likewise, smaller values will provide more responsive system behavior exhibiting less

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 INPUT PAGE 01, 1

VEHICLE CONFIGURATION (NUMBER OF TRAILERS - ENTER 0 FOR A STRAIGHT TRUCK)  
 INITIAL VELOCITY (FT/SEC)  
 STEER TABLE (NUMBER OF LINES): POSITIVE - STEER ANGLE TABLE, NEGATIVE - PATH FOLLOWER TABLE  
 CLOSED-LOOP PATH FOLLOWING MODE  
 X-Y PATH COORDINATES :

X (FEET)	Y (FEET)
0.0	0.0
100.00	-10.10
200.00	-41.70
300.00	-100.00
350.00	-143.00
375.00	-160.00
400.00	-200.00
425.00	-217.00
450.00	-282.00
460.00	-304.00
480.00	-160.00
490.00	-400.00
500.00	-500.00
505.00	-900.00

DRIVER TRANSPORT LAG (SEC) : 0.0  
 END OF PREVIEW INTERVAL (SEC) : 3.00

TREADLE PRESSURE TABLE (NUMBER OF LINES)  
 TABLE ENTRIES:

TIME (SEC)	PRESSURE (PSI)
0.0	0.0
1.00	0.0

MAXIMUM SIMULATION TIME (SEC)  
 TIME INTERVAL OF OUTPUT (SEC)  
 ROAD KEY = -1 : USER-DEFINED ROAD SURFACE (SUBROUTINE ROAD).  
 OUTPUT PAGE OPTION KEYS: 0 DELETES PAGES

SPRING MASS POSITION	SPRING MASS VELOCITY	SPRING MASS ACCELERATION	TIRE FORCES	WHAKE SUMMARY	UNSPRING MASS
1	1	1	1	PAGES	PAGES

Figure 2. Example of simulation operation parameters with path-follower option.





damping. Recommended values for this parameter are 1.0 to 3.0 sec. A more detailed description of the operation of the path-follower model is provided in Appendix G of this Manual.

Treadle Pressure Table - The next entry following the last steer table parameter is the integer (I2 format) for the TREADLE PRESSURE TABLE (NUMBER OF LINES) which is to follow. The treadle pressure is the line pressure demanded by the driver during braking and controlled by the driver-actuated pedal valve. Each line of the treadle pressure table is entered as a pair of time (sec) versus pressure (psi) numbers (2F10.2 format). The complete table defines the desired treadle pressure time history used by the program during a braking maneuver and may be varied with time to simulate the pressure depletion caused by antilock cycling, or to simulate fade in the brakes due to heating effects. The table should begin at zero time and be listed in ascending order with time. Intermediate points in the treadle pressure table are obtained by linear interpolation. The number of lines in the table must equal the integer number of lines indicated and may not exceed 10. If the treadle pressure table is given zero lines, the program will not execute any braking, and brake parameters (Section 3.3.6) are deleted from the input data list. On the other hand, entry of a table with one or more lines (even if all are zero pressure values) keys the program to look for entry of brake data.

Immediately following are two lines of program instruction. The first is MAXIMUM SIMULATION TIME (sec, F15.3 format) which defines the time duration of the maneuver to be simulated. The program will run for this simulated time period unless the vehicle reaches a stop within the period or a fault (such as vehicle rollover) occurs. To ensure printout of the last time increment desired, it is helpful to specify the MAXIMUM SIMULATION TIME as 0.001 seconds longer than the desired time. Typical simulation times are 4-8 sec. The second line is TIME INCREMENT OF OUTPUT (sec, F15.3 format) which selects the intervals of simulation time at which the instantaneous values of output parameters are printed. Since the normal integration interval is 0.0025 sec, the time increment should be a multiple of this value. Section 4.4 gives some hints on selection of this input parameter.

ROAD KEY - A key for defining one of three road options is the next entry. ROAD KEY is an integer entry and provides the following three road options:



	> 0	:	Planar road with a fixed down-slope and cross-slope
ROAD KEY	= 0	:	Flat horizontal road
	< 0	:	User-defined road surface programmed in SUBROUTINE ROAD

ROAD KEY should be entered in I2 format when the flat road or user-defined road surface options are selected.

When the planar road option (IROAD > 0) is selected, two additional numbers need to be entered on the same line as the ROAD KEY (I2, 2F10.2 format). These two additional entries represent the percentage of down-slope (forward) and cross-slope (lateral, positive slopes down to the right) of the road plane at time zero and fixed with respect to the inertial coordinate system. The planar road option is not currently available for down-slopes when simulating vehicle configurations requiring two or more trailers. (Truck and tractor-semitrailer configurations only.) The initial conditions of the truck or tractor-trailer sprung and unsprung masses in pitch and roll are selected by the program under this option as equal to the specified down-slope and cross-slope of the road. A small initial transient will occur at the beginning of the simulation run using this option, since the lateral and fore/aft suspension forces are not initially in equilibrium.

Selection of the third road option, User-Defined Road (IROAD < 0) allows the program user to define an arbitrary road surface (e.g., road roughness, parabolic bowl, cone, etc.) by providing a SUBROUTINE ROAD containing code which defines road elevation as a function of X-Y inertial coordinates. Appendix H discusses this option in greater detail and provides an example user-written subroutine and required format.

OUTPUT PAGE OPTION KEYS - The last line entered for simulation operation parameters requires seven integer keys (7I1 format) that specify which output pages will be printed during program execution. Entry of 1 for any key will cause that page to be printed; entry of 0 will cause its deletion during output printing. The seven output page types corresponding in order from left to right in the 7I1 field are:

- Truck, Tractor, Trailer Sprung Mass Position
- Truck, Tractor, Trailer Sprung Mass Velocity
- Truck, Tractor, Trailer Sprung Mass Acceleration

Longitudinal, Lateral, and Vertical Tire Forces  
Brake Summary  
Lateral Tire Forces and Moments  
Unsprung Mass Summary

### 3.3 Truck/Tractor Description

The first vehicle is the truck or tractor that is modeled as the sprung mass associated with the cab, chassis, body, payload, etc., supported by suspension systems linking it to the unsprung masses of the axles, supported on the ground in turn by the tire/wheel assemblies. Reference [2], Section 2, provides a comprehensive discussion of the type of mathematical formulation used in the simulation model. Parametric data are needed to describe each of the vehicle components. Figure 3 shows the first portion of that input corresponding to input page 2 "echoed" by the program.

3.3.1 Truck/Tractor Parameters. The basic properties of the truck or tractor are described by its sprung mass parameters included in the first group of entries shown in Figure 3. The sprung mass is modeled as a rigid body shown in Figure 4. The characteristic length of the vehicle is its WHEELBASE, defined as the longitudinal distance in inches (F15.3 format) between the geometric center of the front and rear suspensions. For two-axle vehicles, this is the same as the distance between the front and rear axle centerlines, but for three-axle vehicles it is the distance between the front axle and the geometric center of the rear axles.

The rigid-body sprung mass is represented by mass properties concentrated at its center of gravity (c.g.) at the lateral center of the vehicle. Its mass and fore/aft location are determined by the BASE VEHICLE CURB WEIGHT values in pounds for the FRONT and REAR AXLES (the next two line entries, F15.3 format). This approach is used because the curb weight data is more readily available to users than the properties of sprung mass weight and fore/aft position. Internally, the program determines these parameters by calculations that subtract out the unsprung weight of the axles entered later in the input. The base vehicle curb weight is defined as the weight without payload or a trailer. The rear suspension curb weight with tandem axles is the total ground load for both axles.

TRACTOR PARAMETERS

WHEELBASE - DISTANCE FROM FRONT AXLE TO CENTER OF REAR SUSPENSION (IN) 142.00  
 BASE VEHICLE CURB WEIGHT ON FRONT SUSPENSION (LB) 8900.00  
 BASE VEHICLE CURB WEIGHT ON REAR SUSPENSION (LB) 7116.00  
 SPRING MASS CG HEIGHT (IN, ABOVE GROUND) 39.70  
 SPRING MASS ROLL MOMENT OF INERTIA (IN-LP-SEC\*\*2) 18166.00  
 SPRING MASS PITCH MOMENT OF INERTIA (IN-LF-SEC\*\*2) 69555.00  
 SPRING MASS YAW MOMENT OF INERTIA (IN-LA-SEC\*\*2) 40600.00  
 PAYLOAD WEIGHT (LB) 50.00  
 PAYLOAD DISTANCE AHEAD OF REAR SUSPENSION, CENTER (IN) 64.50  
 PAYLOAD CG HEIGHT (IN, ABOVE GROUND) 37500.00  
 PAYLOAD ROLL MOMENT OF INERTIA (IN-LP-SEC\*\*2) 1727000.00  
 PAYLOAD PITCH MOMENT OF INERTIA (IN-LF-SEC\*\*2) 1727000.00  
 PAYLOAD YAW MOMENT OF INERTIA (IN-LA-SEC\*\*2) 0.0  
 FIFTH WHEEL LOCATION (IN, AHEAD OF REAR SUSP, CENTER) 47.50  
 FIFTH WHEEL HEIGHT ABOVE GROUND (IN) 250000.00  
 SIX WHEEL STIFFNESS (IN-LP/DEC)

TRACTOR FRONT SUSPENSION AND AXLE PARAMETERS

SUSPENSION SPRING RATE (LB/IN/SIDE/AXLE) 1012.50  
 SUSPENSION VISCOUS DAMPING (LB-SEC/IN/SIDE/AXLE) 15.00  
 COLUMBER FRICTION (LB/SIDE/AXLE) 500.00

AXLE ROLL MOMENT OF INERTIA (IN-LP-SEC\*\*2) 3719.00  
 ROLL CENTER HEIGHT (IN, ABOVE GROUND) 24.55  
 ROLL STEER COEFFICIENT (DEG, STEER/DEG, ROLL) 0.0  
 AUXILIARY ROLL STIFFNESS (IN-LE/DEG/AXLE) 4000.00  
 LATERAL DISTANCE BETWEEN SUSPENSION SPRINGS (IN) 32.60  
 TRACK WIDTH (IN) 80.50  
 UNSPRUNG WEIGHT (LB) 1190.00

TRACTOR FRONT TIRCS AND WHEELS

CORNERING STIFFNESS (LB/DEG/TIRE) 722.50  
 LONGITUDINAL STIFFNESS (LB/SIIP/TIRE) 28000.00  
 CAMBER STIFFNESS (LB/DEG/TIRE) 0.0  
 ALIGNING MOMENT (LB-LP/DEG/LIFE) 0.0  
 TIRE SPRING RATE (LB/IN/TIRE) 5700.00  
 TIRE LOAD CAPACITY (LB) 20.30  
 REAR MOMENT OF INERTIA (IN-LP-SEC\*\*2/4-FIELD) 103.00

Figure 3. Example of first page of truck/tractor parameters.

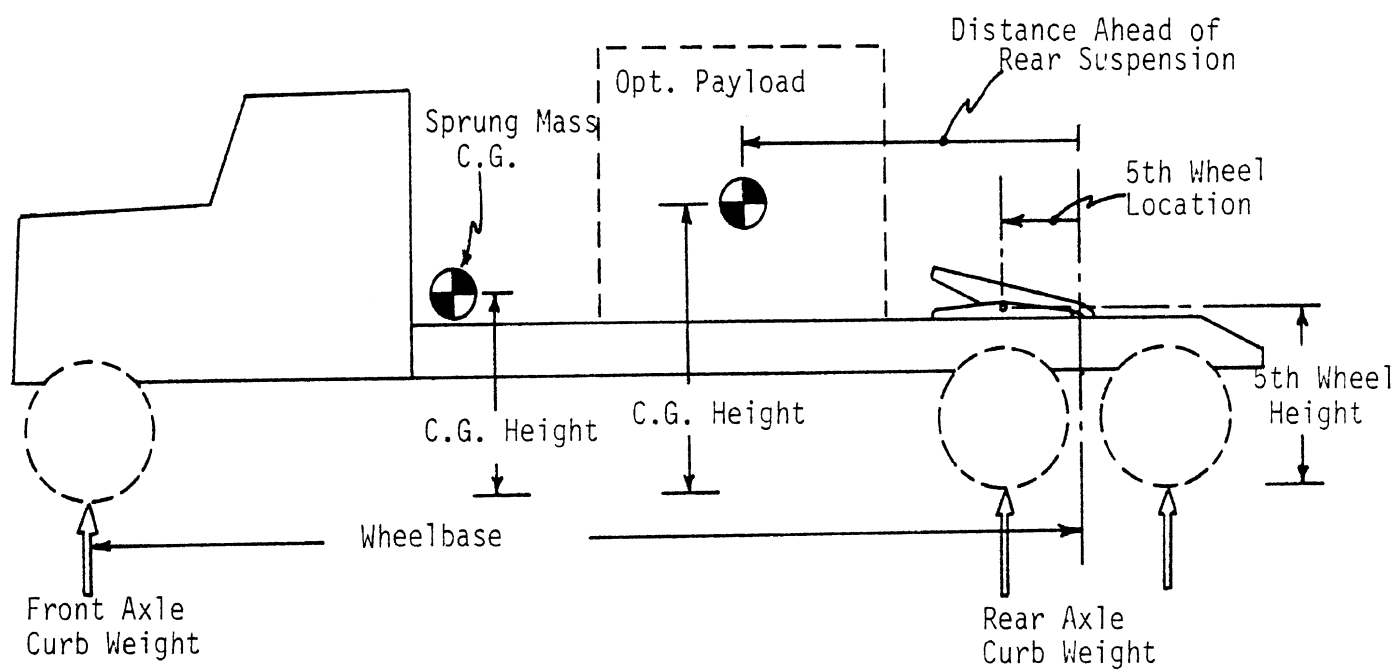


Figure 4. Modeling elements of the truck/tractor sprung mass.

The vertical location of the c.g. is defined by the next entry, SPRUNG MASS CG HEIGHT, which is measured in inches above the ground (F15.3 format). As specified, this is the c.g. of only the sprung mass in the base vehicle configuration corresponding to the curb weight values given above. The height should be given with the vehicle in its fully deflected position as results from loading by a payload or trailer. The sprung mass c.g. height is not readily available to most program users; however, in the absence of such data reasonable estimates can be made. For heavy vehicle cab-chassis configurations, the sprung mass c.g. is usually close to the top of the frame rails (typically 38-40 in above the ground). Such an estimate is reasonable for a tractor or for a truck with a low, light platform bed. However, if the truck includes a substantial body, the c.g. must be measured or estimated from the combined properties of the cab-chassis and vocational body.

The rotational inertia properties of the sprung mass are given by the next three entries for SPRUNG MASS ROLL MOMENT OF INERTIA, PITCH MOMENT OF INERTIA, and YAW MOMENT OF INERTIA. The inertias are given in units of in-lb-sec<sup>2</sup> in F15.3 format. It is normally recommended that these parameters are measured for a vehicle to be simulated, though methods for estimating them have been developed [12]. Appendix F provides a short method for estimating these properties.

As a convenience in using the program to investigate performance of heavy vehicles with variations in payload, the payload parameters are entered separately. The first parameter is PAYLOAD WEIGHT, in lbs (F15.3 format). Thereafter, it is necessary to describe its location by DISTANCE AHEAD OF REAR SUSPENSION CENTER (in, F15.3 format) and CG HEIGHT (inches above the ground in its loaded position, F15.3 format). The payload is always assumed to be located laterally in the center of the vehicle. Likewise, ROLL, PITCH and YAW MOMENTS OF INERTIA are required, in units of in-lb-sec<sup>2</sup> (F15.3 format). If the simulated vehicle is to have no payload, the payload weight is entered as zero, and no entry is required for the subsequent payload parameters. Payload can be specified for both trucks and tractors. If payload is not to be varied, the payload may be lumped in with the vehicle sprung mass properties by entering loaded vehicle axle weights for the BASE VEHICLE CURB WEIGHTS. In that case, the c.g. height and sprung mass moments of inertia must be for the same combination of masses.

Finally, the connection point for a fifth wheel is also located on the sprung mass. If a tractor is being simulated (as indicated by one or more trailers in the VEHICLE CONFIGURATION input), fifth wheel parameters are included at this point in the input list. (The entries are deleted if no trailers are entered.) Three parameters are required: FIFTH WHEEL LOCATION (inches ahead of the rear suspension), HEIGHT ABOVE GROUND (in), and STIFFNESS (in-lb/deg, in the roll direction). All three entries are F15.3 format. The fifth wheel location is arbitrary, typically from 0 to 12 in, and determines the distribution of trailer load on the tractor axles. The height above the ground is the height to the pitch plane hinge point on the fifth wheel for the fully-loaded tractor (typically 45 in). The fifth wheel stiffness parameter is included to allow representation of typical compliances between the payload on the trailer and the frame of the tractor. With a zero entry, the tractor and trailer are completely decoupled in roll. On typical tractor-van trailer combinations, a value of 250,000 in-lb/deg is reasonable. This parameter has significant influence on limit cornering behavior.

The user should be aware that the fifth wheel coupling (as well as pintle hitch couplings, described later) are all represented by spring connections. Thus represented, the equations of motion for different vehicles are coupled by force inputs rather than displacement constraints and may be solved separately and more economically. With the exception of roll stiffness, which may be of interest to some users, all fifth wheel spring rates are selected within the program for optimum operation of the simulation. The resulting rates are high enough to appear effectively rigid.

3.3.2 Truck/Tractor Front Suspension and Axle Parameters. The T3DRS:V1 program models the I-beam type front axle commonly used on medium and heavy trucks. The suspension serves as a compliant link between the sprung and unsprung masses, and is characterized by the forces and moments it produces. All suspensions are modeled in the generalized fashion shown in Figure 5. The parameter entries for the truck or tractor front suspension are shown in Figure 3. The primary compliance of the suspension is in the vertical direction and is defined by SUSPENSION SPRING RATE in lb/in per side of the vehicle. Since these are paired components on an axle, the side-to-side option is available. The rates for the left and right



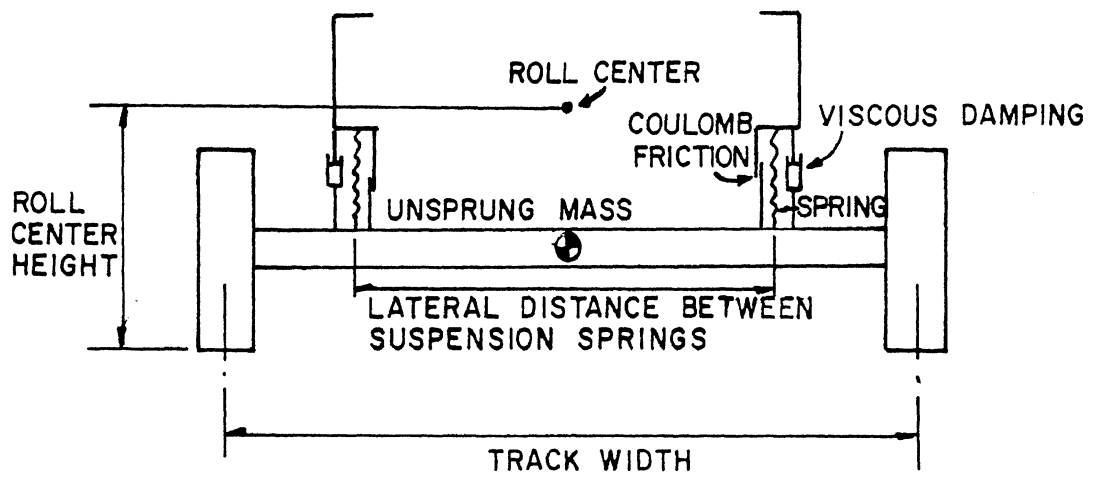


Figure 5. Model of suspension systems.

springs are entered on one line in 2F10.2 format. If left and right are the same, only the first (left) entry needs to be made, and the zero or blank read for the right side causes it to be assigned the same value as for the left. Nonlinear springs can be simulated by defining the force deflection characteristics in a table lookup as follows:

- 1) Enter a negative whole number for spring rate (the negative sign keys the program for a table lookup, and the numerical value identifies the table).
- 2) A single (left spring) entry results in use of the table for both left and right springs.
- 3) Entry of a separate negative number for each spring keys the program to look for two tables.
- 4) Enter the left spring table immediately in the form as follows:

Line #1 - Number of lines to follow, maximum of 10 (I2 format)

Line #2 - Spring force (lb) vs. deflection (in) (2F10.2 format)

. .  
. .  
. .

Line #n - Spring force (lb) vs. deflection (in) (2F10.2 format)

- 5) If a separate right spring table was called for, it is entered next in the same format.

The tables are entered in the positive sense; i.e., positive deflection (spring compression) corresponding to positive force (load) on the axle. The reference point for deflection is arbitrary, since the program simply identifies the initial deflection from the static load, and calculates changes thereafter. It should be noted that even with side-to-side differences in spring characteristics, the program always assumes equal loads on both sides of the axle, adjusting the initial (or static) spring deflection for the fully loaded vehicle to achieve this condition. When using the lookup table, the range of the table should always exceed the expected range of operation of the spring. Typically, it should extend from zero load to

the maximum dynamic load expected. Excursions beyond the range of the table causes it to limit at the last load condition in the table in the direction of the excursion. If tension loads are expected due to the maneuver, the spring force characteristics should be defined in the tension (negative force) range.

The damping characteristics within the suspension are characterized by viscous damping and coulomb friction. SUSPENSION VISCOUS DAMPING is entered in units of lb-sec/in for each side of the suspension (2F10.2 format). The side-to-side option is available. Viscous damping effectively represents the shock absorber damping in the vertical direction, and is applied to motions in both directions. If the shock absorbers to be simulated are at an angle to the vertical, their damping coefficient should be multiplied by the square of the cosine of the angle between the shock absorber centerline and the vertical. Typical front-axle shock absorber damping coefficients should be in the range of 10-20 lb-sec/in.

For heavy vehicles the more common, and sometimes only, damping is coulomb friction derived from interleaf friction of the leaf spring suspensions [18]. COULOMB FRICTION is entered in units of lb/side (2F10.2 format) with the side-to-side option available. The coulomb friction is defined here as one-half the width of the hysteresis loop of the spring force-deflection curve as illustrated in Figure 6. When possible, the coulomb friction magnitude should be selected at the static load condition. In the absence of specific data, the coulomb friction can be estimated at 10% of the static load value. The coulomb friction is neglected during the initial static spring deflection calculations. During the dynamic calculations thereafter, the coulomb friction force is added to or subtracted from the calculated spring force, depending on the direction of relative motion.

The front axle components of the vehicle, including the axle, springs, spindles, hubs, brakes, and wheels, are lumped into one unsprung mass, as shown in Figure 5. The mass has a center of gravity located on the axis of the wheels at the lateral center of the axle. The mass is characterized by a ROLL MOMENT OF INERTIA (units of in-lb-sec<sup>2</sup>, F15.3 format), and its UNSPRUNG WEIGHT (in lbs, F15.3 format, last entry in this group). The yaw moment of inertia is assumed equal to the roll moment of inertia, and since

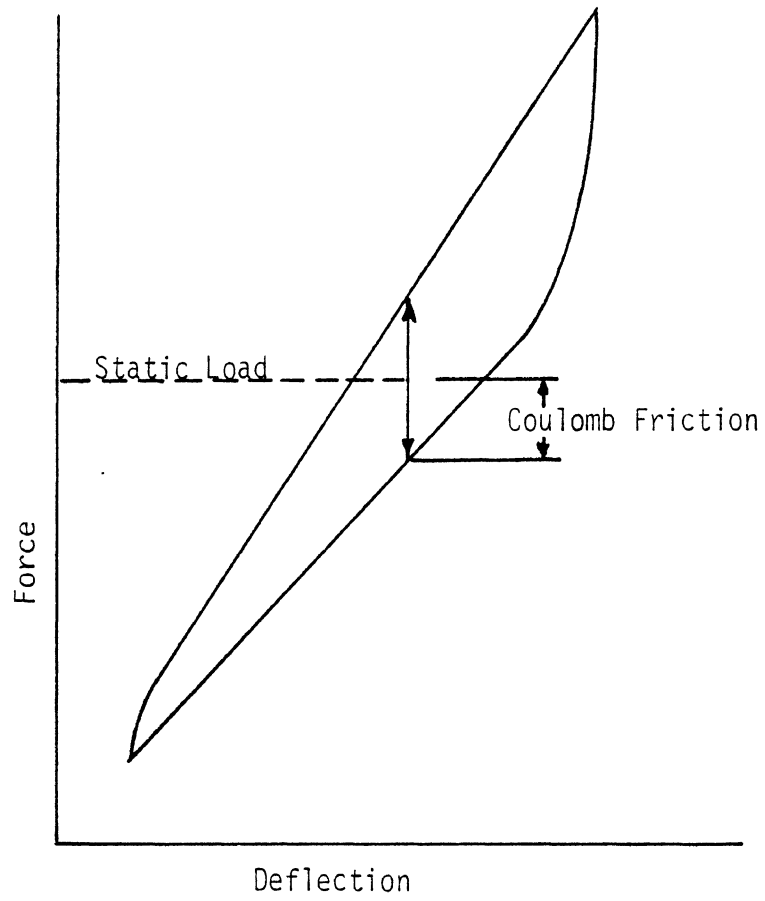


Figure 6. Coulomb friction in a suspension leaf spring assembly.

the axles are constrained to yaw with the sprung mass, the yaw moments of inertia of this and all other axles are added to that of the sprung mass by the program. The pitch moment of inertia for axles is negligible in effect and is not included in the modeling.

While the suspension is primarily a vertical compliance, it also serves to transmit horizontal forces to the sprung mass. The mechanism for transmission of lateral forces through the suspension is important and significant to the overall directional response of the vehicle. When a vehicle is caused to roll on its suspension, it tends to roll about a point designated as the roll center, as shown in Figure 5. Conceptually, the roll center is the point at which lateral forces are transmitted between the sprung and unsprung masses. This parameter is significant to vehicle response because lateral forces present at the roll center cause lateral load transfer on the axle (and hence, tires) and thereby influence the lateral forces developed by the tires. This effect is significant in transient maneuvers due to load transfer effects before the sprung mass has time to roll, and in steady-state maneuvers due to the distribution of roll moment between front and rear axles determined, in part, by the relative height of the front and rear suspension roll centers. The effects of roll center height are included in the modeling and a ROLL CENTER HEIGHT parameter (in. above the ground, F15.3 format) is included in the input list. The suspension and axle system is considered constrained with the sprung mass in the pitch degree of freedom so a similar concept in the pitch plane is not needed to characterize transmission of longitudinal forces and pitch moments.

For various reasons, a suspension system may not always maintain the wheels in alignment with the longitudinal axis of the vehicle throughout all suspension motions. Most suspensions are subject to a small amount of steer effect when the vehicle rolls. Such factors can play an important role in vehicle directional response and overall stability. The input list includes a ROLL STEER COEFFICIENT (in units of degrees steer per degree roll, F15.3 format) to simulate this effect. A positive entry implies an incremental steer to the right when the sprung mass rolls to the right. Hence, a positive front axle roll steer coefficient has an understeer influence.

The vertical force developed within the suspension is the sum of spring deflection, coulomb friction, and viscous damping forces. Roll of the axle relative to the sprung mass produces a roll moment within the suspension due to the lateral spacing between the springs and shock absorbers. The LATERAL DISTANCE BETWEEN SUSPENSION SPRINGS (in., F15.3 format) is included as an input parameter, as a basis for calculating the roll moment effect. At times, the suspension may exhibit a roll stiffness in excess of that accountable by the springs and their separation, because of the additional effects of linkages, spring twist, antisway bars, etc. An AUXILIARY ROLL STIFFNESS input parameter (in-lb per deg., F15.3 format) is provided to allow modeling these effects.

The last remaining parameter to be specified for the suspension-axle system is the TRACK WIDTH (in., F15.3 format), defined as the distance between the wheel planes (center of the wheels) of the right and left tires.

3.3.3 Truck/Tractor Front Tires and Wheels. Tire forces within the T3DRS:V1 program are calculated from models that, in effect, determine the forces from the operating conditions. For example, tire vertical load is a result of its instantaneous vertical height (rolling radius) above the road. The cornering and longitudinal force behavior can be represented by either of two models in the simulation:

- 1) A linear model of cornering and longitudinal stiffness characteristics
- 2) A nonlinear table lookup model for cornering and longitudinal characteristics with variations due to load and speed conditions.

The first line entry for front tires and wheels, as shown in Figure 3, is the left and right CORNERING STIFFNESS lbs/deg/tire, 2F15.3 format). If the right-side value is left blank or entered as zero, it is assumed equal to the left-side value. The cornering stiffness is the slope of the lateral force versus slip angle behavior of the tire in the vicinity of zero slip angle, as illustrated in Figure 7. It is entered as a positive number and is typically numerically equivalent to approximately 10 percent of the static load (i.e., a tire at 5000 lbs load has a cornering stiffness of approximately 500 lb/deg). Since the stiffness is dependent on the tire load, it should be

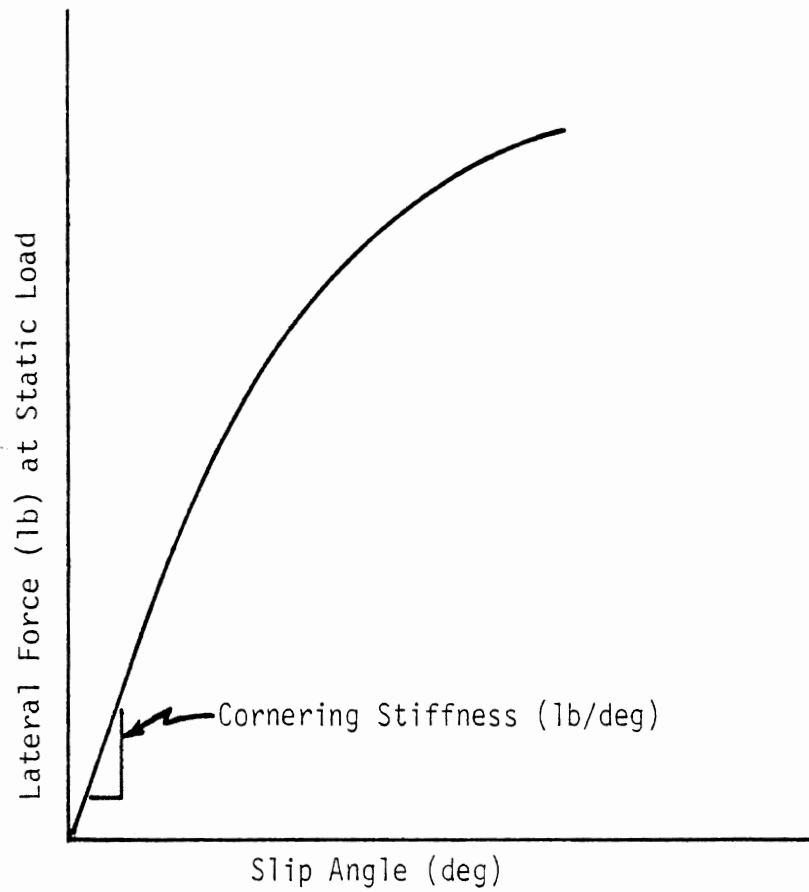


Figure 7. Definition of cornering stiffness parameter.

entered for the condition equivalent to the full static load on that tire in the simulation. Internally, the program continuously adjusts the cornering stiffness in proportion to the changing dynamic load conditions. The linear cornering stiffness model should only be used with moderate cornering maneuvers, where the tire cornering forces generated are less than 50 percent of the vertical load. Beyond this point, the cornering force becomes nonlinear and saturates (no saturation or limit on lateral traction occurs with the linear model). In such cases, the nonlinear table lookup model can be used by entry of a negative whole number to key the model. The numerical value of this entry identifies the table number for the tabular lateral tire force data which is to follow. (The format for the tabular tire data is discussed in the following section, 3.3.3.1.)

The next line entered for front tires and wheels is the left- and right-tire LONGITUDINAL STIFFNESS in lbs/slip (2F15.3 format). The LONGITUDINAL STIFFNESS is equivalent to the initial slope of the brake force versus longitudinal slip curve for a tire, as illustrated in Figure 8, and typically has a numerical value equivalent to about four times the tire static load. The longitudinal stiffness is proportioned inside the program to change with the tire dynamic load. Like the cornering stiffness entry, positive values specify the linear tire model for longitudinal tire force calculations with zero right-side entries, causing the program to assume a right-side value equal to the left. Since it is a linear model, it should only be used with braking maneuvers for which the friction level on each tire is well below the peak (the braking is well below the wheel lockup condition). For high level braking or when antilock braking is used, the tire longitudinal force characteristics are best represented by a table lookup. A negative entry for longitudinal stiffness keys the nonlinear tire force table lookup option. As above, the numerical value of this entry identifies the longitudinal tire force table of data which needs to follow. (Section 3.3.3.1)

Mixtures of linear and nonlinear tire options for longitudinal and lateral tire force representations are permitted for the same tire. Linear and nonlinear mixtures side-to-side are also allowed.

The remaining parameters to be entered for front tires and wheels should be positive or zero. Negative table entry options are not allowed. Two values per line are entered representing left- and right-side values



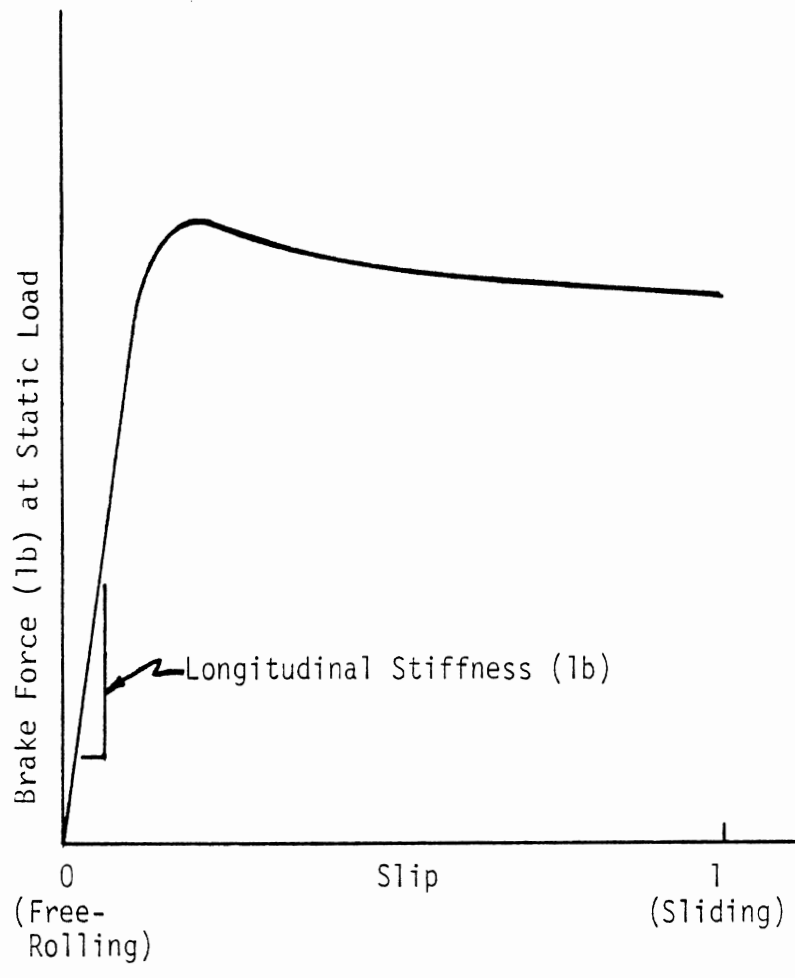


Figure 8. Definition of longitudinal stiffness parameter.

(2F15.3 format). Zero right-side values will equate right with left. The first of these, CAMBER STIFFNESS, defines the lateral force per degree of camber at static load conditions and is entered in lbs/deg. ALIGNING MOMENT at the static load condition is entered next in units of in-lb/deg. TIRE SPRING RATE (lb/in), TIRE LOADED RADIUS (in), and POLAR MOMENT OF INERTIA (in-lb-sec<sup>2</sup>) then follow as the last three lines of the tire/wheel parameters. The polar moment of inertia for all rotating wheel components is defined about the spin axis of the wheel. This parameter can be of importance in antilock braking maneuvers.

3.3.3.1 Nonlinear lateral and longitudinal tire table formats. Negative values for CORNERING STIFFNESS or LONGITUDINAL STIFFNESS parameters trigger the nonlinear tire model table lookup option. Tire data conforming to a specific format needs to be entered immediately following each of these negative entries.

Cornering Stiffness (MU-Y) Tables:

Tabular cornering (lateral) force tire data called by a negative CORNERING STIFFNESS value is entered in terms of a normalized lateral traction coefficient, MU-Y, as a function of tire sideslip angle, ALPHA, for at least one, and as many as three, different vertical tire loads and velocities. MU-Y is defined as the nondimensional ratio of tire lateral force to the prevailing vertical load at zero longitudinal slip (free rolling). Two-way linear interpolation is used by the program between entered table points. The format required for entering MU-Y tabular data is as follows (see Appendix A for examples):

(Define number of loads and velocities)

- Number of vertical loads, NL (3 max.) (I2 format)
- Vertical load values (3F10.2 format)
- Number of velocities, NV (3 max.) (I2 format)
- Velocity values (3F10.2 format)

(First load/first velocity table)

- Number of tire sideslip angles, N11, in first ALPHA versus MU-Y table (max. of 10) (I2 format)
- N11 lines of ALPHA (deg), MU-Y pairs comprising the first table (2F10.2 format, each line)

(First load/second velocity table)

- Number of tire sideslip angles, N12, in second (I2 format) ALPHA versus MU-Y table (max. of 10)
- N12 lines of ALPHA (deg), MU-Y pairs comprising (2F10.2 format, each line) the second table.

(First load/third velocity table)

- Number of tire sideslip angles, N13, in third (I2 format) ALPHA versus MU-Y table (max. of 10)
- N13 lines of ALPHA (deg), MU-Y pairs comprising (2F10.2 format) the third table.

(Repeat for second load condition)

(Repeat for third load condition)

Note: The total number of ALPHA versus MU-Y tables is equal to the product of  $NV \times NL$ . Hence, a maximum of nine (9) such tables are permitted ( $NV = NL = 3$ ) and a minimum of one (1) table ( $NV = NL = 1$ ) is required.

Immediately following the ALPHA versus MU-Y tables, a "roll-off" tabular function which allows for reduction of the free-rolling tire lateral forces under longitudinal (braking) slip conditions is required. In the event no braking occurs, a simple one-point table may be used. The "roll-off" table is a two-way table of the parameter, ROLLY, as a function of longitudinal slip (SLIP) and sideslip (ALPHA) of the tire. ROLLY is simply a multiplication factor for MU-Y defined at the selected SLIP and ALPHA values in the table and interpolated elsewhere. ROLLY values of 1.0 simply return the free-rolling MU-Y value. Likewise, a ROLLY value of 0.75 would diminish the value of MU-Y by 25 percent at the specified longitudinal/sideslip point in the "roll-off" table.

The following format is used for entering lateral "roll-off" function tabular data:

(Define arguments of the table)

- Number of longitudinal slip (SLIP) points, (I2 format) NS, in the "roll-off" table (10 max.)
- NS lines of longitudinal slip (SLIP) values (F10.2 format, each line)
- Number of sideslip (ALPHA) points, NSS, (I2 format) in the "roll-off" table (10 max.)

NSS lines of sideslip (ALPHA) values (F10.2 format, each line)

NSS × NS matrix of ROLLY values defining the "roll-off" tabular function. NSS lines containing NS ROLLY values/line as shown below. (10F8.2 format)

	Slip <sub>1</sub>	Slip <sub>2</sub>	etc.
Alpha <sub>1</sub>	ROLLY <sub>11</sub>	ROLLY <sub>12</sub>	.....
Alpha <sub>2</sub>	ROLLY <sub>21</sub>	ROLLY <sub>22</sub>	.....
etc.	.	.	
	.	.	
	.	.	
	.	.	
	.	.	
	.	.	

-----ROLLY TABLE-----

Note: The maximum size of the ROLLY table is 10 × 10 (NSS = NS = 10). Minimum size is 1 × 1 (NSS = NS = 1).

Longitudinal Stiffness (MU-X) Tables:

Tabular braking (longitudinal) force tire data is entered in exactly the same format as used for cornering data. This data must follow immediately after the negative LONGITUIDNAL STIFFNESS entry. MU-X, a normalized longitudinal traction coefficient, now replaces MU-Y as the dependent table variable and longitudinal slip, SLIP, replaces ALPHA as the independent table variable. MU-X is defined as the nondimensional ratio of longitudinal tire force to the prevailing vertical load at a zero tire sideslip angle. Like the lateral force table data, up to three vertical loads and speeds may be specified.

A longitudinal "roll-off" function is likewise required in the case of MU-X tabular data. ROLLX, a multiplicative factor analogous to ROLLY for cornering data, is specified in a two-way table of longitudinal slip (SLIP) versus sideslip (ALPHA) identical to that format used for the lateral "roll-off" table.

Sources of lateral and longitudinal tire force data for heavy trucks, that are largely compatible with the T3DRS:V1 program, are contained in References [2, 13, 14, 15, 16, 17].

3.3.4 Truck/Tractor Rear Suspension and Axle Parameters. Medium and heavy trucks all use one or more solid rear axles. Since a large percentage of such vehicles use two (tandem) rear axles, an optional tandem axle is provided in the program models. The rear suspension and axle parameters are the next group of input parameters, as shown in Figure 9. The first parameter is a SUSPENSION KEY (I2 format) for which "00" indicates a single axle is to be used, and "01" indicates a tandem axle set.

3.3.4.1 Single axles. When a single axle has been specified, its characteristics are described by the same set of parameters used to describe the front suspension and axle (see Section 3.3.2 for detailed discussion). Hence, following a "00" suspension key, the following parameters are entered:

- SUSPENSION SPRING RATE (lbs/in/side/axle); 2F10.2 format; table lookup and side-to-side options allowed
- SUSPENSION VISCOUS DAMPING (lbs-sec/in/side); 2F10.2 format; side-to-side option allowed
- COULOMB FRICTION (lbs); 2F10.2 format; side-to-side option allowed
- AXLE ROLL MOMENT OF INERTIA (in-lb-sec<sup>2</sup>); F15.3 format
- ROLL CENTER HEIGHT (in above ground); F15.3 format
- ROLL STEER COEFFICIENT (deg steer/deg roll); F15.3 format
- AUXILIARY ROLL STIFFNESS (in-lb/deg); F15.13 format
- LATERAL DISTANCE BETWEEN SUSPENSION SPRINGS (in); F15.3 format
- TRACK WIDTH (in); F15.3 format
- UNSPRUNG WEIGHT (lbs); F15.3 format

Because of the dual tires commonly used on rear axles, the TRACK WIDTH must be carefully defined. As used here, track width is the lateral distance between the centers of the dual tires, as shown in Figure 10. The dual tire separation parameter is included in the Tires and Wheels data and defines the wheel locations relative to the track width.

TRACTOR REAR SUSPENSION AND AXLE PARAMETERS

SUSPENSION KEY - 0 INDICATES SINGLE AXLE, 1 INDICATES TANDEM AXLES  
 TANDEM AXLE SEPARATION (IN BETWEEN LEADING AND TRAILING AXLES) 50.00  
 STATIC LEAD TRANSFER (PERCENT LEAD ON LEAD AXLE) 50.00  
 DYNAMIC LEAD TRANSFER (PERCENT OF BRAKE TORQUE TRANSFERRED ONTC LEADING AXLE) 0.0  
 SUSPENSION SPRING RATE (LB/IN/SIDE/AXLE) 1500.00 1500.00 1500.00  
 SUSPENSION VISCOUS DAMPING (LB-SEC/IN/SIDE/AXLE) 15.00 15.00 15.00  
 COULOMB FRICTION (LB/SIDE/AXLE) 250.00 250.00 250.00

AXLE ROLL MOMENT OF INERTIA (IN-UP-SEC\*\*2) 445R-00 445R-00  
 ROLL CENTER HEIGHT (IN ABOVE GROUND) 22-00 22-00  
 ROLL STIFF COEFFICIENT (DEG. STEER/DEG. ROLL) 0.0 0.0  
 AUXILIARY ROLL STIFFNESS (IN-LE/DEG/AXLE) 35-00 78000.00  
 LATERAL DISTANCE BETWEEN SUSPENSION SPRINGS (IN) 72-00 72-00  
 TRACK WIDTH (IN) 2340-00 2170.00  
 UNSPRUNG WEIGHT (LB)

LEADING TANDEM AXLE		TRAILING TANDEM AXLE	
LEFT SIDE	RIGHT SIDE	LEFT SIDE	RIGHT SIDE
1500.00	1500.00	1500.00	1500.00
15.00	15.00	15.00	15.00
250.00	250.00	250.00	250.00

TRACTOR REAR TIRES AND OFFSETS

DUAL TIRE SEPARATION (IN) 13.00 13.00  
 SPRING STIFFNESS (LB/DEG/TIRE) 690.00 690.00  
 LONGITUDINAL STIFFNESS (LB/SLIP/TIRE) 28000.00 28000.00  
 CAMBER STIFFNESS (LB/DEG/TIRE) 0.0 0.0  
 ALIGNING MOMENT (IN-LP/DEG/TIRE) 0.0 0.0  
 TIRE SPRING RATE (LP/IN/TIRE) 5700.00 5700.00  
 TIRE UNLOADED RADIUS (IN) 20.30 20.30  
 POLAR MOMENT OF INERTIA (IN-UP-SEC\*\*2/WHEEL) 115.00 115.00

LEADING TANDEM AXLE		TRAILING TANDEM AXLE	
LEFT SIDE	RIGHT SIDE	LEFT SIDE	RIGHT SIDE
13.00	13.00	13.00	13.00
690.00	690.00	690.00	690.00
28000.00	28000.00	28000.00	28000.00
0.0	0.0	0.0	0.0
0.0	0.0	0.0	0.0
5700.00	5700.00	5700.00	5700.00
20.30	20.30	20.30	20.30
115.00	115.00	115.00	115.00

TRACTOR FRONT BEAMS

TIME LAG (SEC) 0.0200 0.0200  
 RISE TIME (SEC) 0.1700 0.1700  
 BRAKE TORQUE (IN-LP/PS/BEAK) 100.0000 100.0000

LEADING TANDEM AXLE		TRAILING TANDEM AXLE	
LEFT SIDE	RIGHT SIDE	LEFT SIDE	RIGHT SIDE
0.0200	0.0200	0.0200	0.0200
0.1700	0.1700	0.1700	0.1700
100.0000	100.0000	100.0000	100.0000

TRACTOR REAR BEAMS

TIME LAG (SEC) 0.0500 0.0500  
 RISE TIME (SEC) 0.4000 0.4000  
 BRAKE TORQUE (IN-LP/PS/BEAK) 200.0000 200.0000

LEADING TANDEM AXLE		TRAILING TANDEM AXLE	
LEFT SIDE	RIGHT SIDE	LEFT SIDE	RIGHT SIDE
0.0500	0.0500	0.0500	0.0500
0.4000	0.4000	0.4000	0.4000
200.0000	200.0000	200.0000	200.0000

Figure 9. Example of second page of truck/tractor parameters.

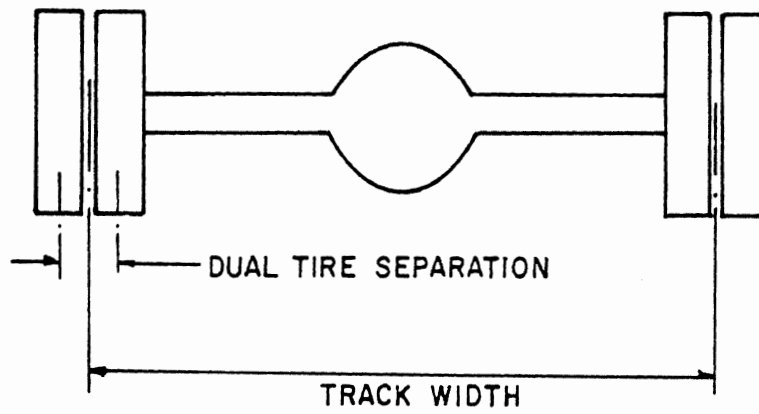


Figure 10. Definition of track width and dual tire separation.

3.3.4.2 Tandem axles option. The tandem axle model has been reformulated for the T3DRS:V1 program. Previously, seven different tandem options have been variously available among the predecessor programs. These included:

- 1) Walking-beam suspension
- 2) Basic four-spring suspension
- 3) Four-spring with spring-type torque rods
- 4) Four-spring with long load leveler
- 5) Multiple torque rod four-spring
- 6) Multiple torque rod four-spring with spring-type lower torque rod
- 7) Air suspension

Reference [3] provides a detailed discussion of these seven types of tandem suspensions. Each axle/suspension system was defined by a detailed list of geometric parameters that served to establish three basic characteristics:

- 1) The tandem axle separation
- 2) The static load distribution among the axles
- 3) The dynamic load transfer between axles during braking.

That approach to modeling was taken under the philosophy that tandem axle geometric characteristics were more readily available to users than such parameters as dynamic load transfer characteristics. However, the limitations of each geometric formulation has resulted in a proliferation of models, each required to handle particular details associated with the many varieties of tandem systems in use.

In T3DRS:V1, tandem axle systems are modeled as two single axles with the additional specification of the three parameters listed above. Hence, the entry of a tandem-axle system is accomplished by entry of a data list as described below.

The tandem-axle option is indicated by entry of "01" value (I2 format) as the first parameter, SUSPENSION KEY. The next entry is TANDEM AXLE SEPARATION (in. between the centers of the leading and trailing axles, in F15.3 format). Tandem-axle separation is typically 48-52 in. for closely spaced tandem sets. Next is the STATIC LOAD TRANSFER (F15.3 format) which is the percent of the total tandem load carried on the lead axle under static



conditions. On the most common tandem suspensions, this is intended to be 50 percent (50.0 entry), although minor variations may occur due to inaccuracies in the equalizing system or due to differences in the unsprung weights of the axles. The value entered here establishes the final static distribution of the loaded vehicle used in the simulation. Internally, the program works back from the load distribution specified, compensates for the unsprung weights of the axles, and selects the necessary static spring deflection on each axle to achieve this static load distribution. If different side-to-side spring characteristics are also specified, the static deflections of the springs on the right and left are selected to achieve equal load on both sides of the axle under static conditions.

Next, the DYNAMIC LOAD TRANSFER parameter is entered (F15.3 format). This parameter, in units of percent, describes the fraction of the total brake torque (generated on the rear axles) applied to transferring load from the trailing to the leading axle of the tandem set. That is, the brake torque generated by the rear axles results in a pitch plane moment on the vehicle that must be counteracted by a moment generated either by a dynamic load transfer to the front axle of the vehicle, or by dynamic load transfers to the leading tandem axle. For example, if the total brake torque on a tandem axle set with a 50-in. TANDEM AXLE SEPARATION is 100,000 in-lb, a DYNAMIC LOAD TRANSFER value of +10.0 (percent) would result in an increase/decrease of 200 lbs of vertical load on the leading/trailing axles. The load transfer characteristics are determined by the inherent geometry of the suspension and torque rod systems. With ideal torque rod designs, all brake torque reaction transfers to the vehicle frame, resulting in load transfer to the front axle. In practice, less than that ideal is achieved. Walking-beam and air suspensions are reasonably effective and a zero entry may be appropriate to those cases. However, some four-spring suspensions by the nature of their load equalization systems may transfer load from the leading to the trailing axle, in which case a negative value for the parameter is required.

After entry of these three special tandem parameters, the remainder of the rear suspension and axle parameters are entered as two serial sets of single axles. That is, a single axle data set of 10 parameters, from SUSPENSION SPRING RATE through UNSPRUNG WEIGHT, is entered to describe the

leading axle; followed by a similar data set to describe the trailing axle. Different parametric values, along with the table lookup and side-to-side options, can be used as desired with each axle. More detailed discussion of the 10 parameters is contained in Sections 3.3.2 and 3.3.4.1. These data are echoed, as shown in Figure 9, in a side-by-side format rather than the serial format actually used in the input list.

3.3.5 Truck/Tractor Rear Tires and Wheels. The rear tires and wheels (see Fig. 9) are generally described by the same parametric information needed for the front wheels, that is described in detail in Section 3.3.3. The primary difference arises from the fact that rear axles commonly employ a dual tire arrangement. Hence, the first parameter to be entered is DUAL TIRE SEPARATION (F15.3 format) which is the distance in inches between the center-plane of the two tires in a dual wheel set (see Fig. 10). Thence the parametric data on a per tire basis is entered. If the dual tire separation is input as zero, a single wheel is assumed at that position defined by the track width entered previously. Different values can be assigned for tires on the left and right side of the axle by side-to-side entry format, but both tires in the dual set are assigned the same parameter values. The last entry, the POLAR MOMENT OF INERTIA, is likewise entered on a per tire basis, and hence, with dual wheels should be entered as half the value for the dual wheel set. If tandem axles have been specified, two complete sets of tire data from DUAL TIRE SEPARATION to POLAR MOMENT OF INERTIA should be entered in series, the first set for the leading axle and the second set for the trailing axle.

3.3.6 Truck/Tractor Front and Rear Brakes. The brake systems on the axles of the simulated vehicles are represented by the timing characteristics of the pneumatic system and the pressure torque characteristics of the brakes. Brake system data are entered as the last category of information about each vehicle and are entered only if a Treadle Pressure Table was entered in the Simulation Operation Parameters. Zero lines in that table signals the program to skip over brake data read instructions. One or more lines in the Treadle Pressure Table, even if all values are zero, is considered a table entry.

Brake data are entered for each axle of the vehicle in sequence from front to rear, the number of brake data sets being equal to the number of axles on the vehicle. The brake data sets consist of three entries.

The first entry is the BRAKE LAG in seconds for the left and right brake (2F10.4 format). This parameter describes the time for a pressure signal to proceed from the treadle valve to the brake chamber and is equivalent to the time from the first motion of the treadle valve to the beginning of the pressure rise at the brake chamber. Typical values are in the range of 0.02 to 0.10 sec for truck/tractor air brake systems.

The second entry is brake RISE TIME in seconds for the left and right brakes (2F10.4 format). The rise time is the effective time constant when the chamber pressure rise is characterized by a first-order lag (i.e., time required to reach 63% of the steady-state step response). Typical values are in the range of 0.2 to 0.5 sec.

The last entry in the brake set is the left and right BRAKE TORQUE coefficient in units of in-lb of brake torque/psi (2F10.4 format). The brake torque coefficient characterizes the brake in a linear fashion and, as with the first two entries, can be given a side-to-side difference. (One entry with any of the above parameters, as with any side-to-side parameter, causes the right side to be given the same value as the left side.) In the event it is desired to model the brake with nonlinear characteristics, as, for example, having a nonzero pushout pressure before the brake is actuated, a brake lookup table can be called by entry of a negative whole number for the BRAKE TORQUE coefficient. Immediately thereafter, a brake table should be entered in the following format:

Line #1	Number of Lines, n (max. of 10)	(I2 format)
Line #2, etc.	'n' lines of the table of pressure (psi) versus torque (in-lb)	(2F10.2 format)

If left and right brakes are given separate tables, the left brake table is entered first, followed immediately by the right brake table. The side-to-side and lookup table options may be mixed as desired on each axle or on different axles.

The performance of hydraulic brake systems can be represented as well by the brake models. In that case, the BRAKE LAG and RISE TIME parameters are negligible and may be entered as zero. Effects of proportioning valves are taken into account by assigning nonlinear brake torque characteristics duplicating slopes and break points in the proportioning.

### 3.4 First Trailer Description

The first trailer is always a semitrailer which is modeled as a rigid body sprung mass supported at the front by the tractor fifth wheel coupling and at the rear by its own suspension and axles. Parametric data for the trailer is shown in Figures 11 and 12.

3.4.1 Trailer Parameters. The basic properties of the trailer are described by sprung mass parameters that constitute the first group of entries. The sprung mass is modeled as a rigid body, shown in Figure 13. The first entry is WHEELBASE, the characteristic length of the trailer defined as the longitudinal distance in inches (F15.3 format) from the kingpin to the center of the rear suspension. For a single-axle trailer, this is the same as the distance to the rear axle centerline, but for a tandem-axle trailer it is the distance to the geometric center of the rear axles.

The rigid body sprung mass is represented by mass properties concentrated at its center of gravity (c.g.). Its mass and fore/aft location are established by input of the BASE VEHICLE KINGPIN STATIC LOAD (lbs., F15.3 format) and CURB WEIGHT ON REAR AXLES (lbs., F15.3 format). The base vehicle weight data defines the mass of the semitrailer only and should exclude loads imposed from other trailers. Rear axle curb weight with tandem axles is the total for both axles.

Thereafter, the sprung mass and payload properties consisting of the following entries are made:

- SPRUNG MASS C.G. HEIGHT
- SPRUNG MASS ROLL MOMENT OF INERTIA
- SPRUNG MASS PITCH MOMENT OF INERTIA

TRAILER NO. 1 PARAMETERS

WHEEL BASE - DISTANCE FROM KINGPIN TO CENTER OF REAR SUSPENSION (IN) 383.00  
 BASE VEHICLE KINGPIN STATIC LOAD (LB) 2815.00  
 BASE VEHICLE CURB WEIGHT ON REAR SUSPENSION (LB) 8650.00  
 SPRUNG MASS CG HEIGHT (IN. ABOVE GROUND) 74.80  
 SPRUNG MASS ROLL MOMENT OF INERTIA (IN-LB-SEC\*\*2) 66224.00  
 SPRUNG MASS PITCH MOMENT OF INERTIA (IN-LB-SFC\*\*2) 547486.00  
 SPRUNG MASS YAW MOMENT OF INERTIA (IN-LB-SEC\*\*2) 644483.00  
 PAYLOAD WEIGHT (LB) 46800.00  
 PAYLOAD CG HEIGHT (IN. ABOVE GROUND) 183.00  
 PAYLOAD ROLL MOMENT OF INERTIA(IN-LB-SEC\*\*2) 60.00  
 PAYLOAD PITCH MOMENT OF INERTIA(IN-LB-SFC\*\*2) 13000.00  
 PAYLOAD YAW MOMENT OF INERTIA(IN-LB-SEC\*\*2) 240000.00  
 LOCATION OF PINTLE HOOK (IN BEHIND REAR SUSP. CENTER) 240000.00  
 HEIGHT OF PINTLE HOOK (IN ABOVE GROUND) 49.00  
 40.00

TRAILER NO. 1 REAR SUSPENSION AND AXLE PARAMETERS

LEADING TANDEM AXLE		TRAILING TANDEM AXLE	
LEFT SIDE	RIGHT SIDE	LEFT SIDE	RIGHT SIDE
4746.00	7818.00	7818.00	7818.00
29.60	50.00	50.00	50.00
-0.00	2600.00	2600.00	2600.00
35490.00			
38.00			
71.25			
1530.00			

SUSPENSION KEY - 0 INDICATES SINGLE AXLE, 1 INDICATES TANDEM AXLES

TANDEM AXLE SEPARATION (IN BETWEEN LEADING AND TRAILING AXLES) 48.00

STATIC LOAD TRANSFER (PERCENT LOAD ON LEAD AXLE) 40.00

DYNAMIC LOAD TRANSFER (PERCENT OF BRAKE TORQUE TRANSFERRED ONTO LEADING AXLE) 10.00

SUSPENSION SPRING RATE (LB/IN/SIDE/AXLE) 7818.00

SUSPENSION VISCOUS DAMPING (LB-SEC/IN/SIDE/AXLE) 50.00

COULOMB FRICTION (LB/SIDE/AXLE) 2600.00

AXLE ROLL MOMENT OF INERTIA (IN-LB-SEC\*\*2) 4746.00

ROLL CENTER HEIGHT (IN. ABOVE GROUND) 29.60

ROLL STEER COEFFICIENT (DEG. STIFER/DEG. ROLL) -0.00

AUXILIARY ROLL STIFFNESS (IN-LB/DEG/AXLE) 35490.00

LATERAL DISTANCE BETWEEN SUSPENSION SPRINGS (IN) 38.00

TRACK WIDTH (IN) 71.25

UNSPRUNG WEIGHT (LB) 1530.00

TRAILER NO. 1 REAR TIRES AND WHEELS

LEADING TANDEM AXLE		TRAILING TANDEM AXLE	
LEFT SIDE	RIGHT SIDE	LEFT SIDE	RIGHT SIDE
12.40	12.40	12.40	12.40
600.00	600.00	600.00	600.00
21000.00	21000.00	21000.00	21000.00
0.0	0.0	0.0	0.0
0.0	0.0	0.0	0.0
4500.00	4500.00	4500.00	4500.00
20.20	20.20	20.20	20.20
212.00	212.00	212.00	212.00

Figure 11. Example of first page of semitrailer parameters.

HSRI TRUCK AND TRACTOR-TRAILER DYNAMIC RESPONSE SIMULATION - T3DRS, VI  
 SAMPLE RUN - TRIPLES BRAKING IN A TURN, ALL OPTIONS EXERCISED

TRAILER NO. 1 REAR BRAKES  
 -----

LEADING TANDEM AXLE  
 -----  
 LEFT SIDE      RIGHT SIDE  
 -----

TRAILING TANDEM AXLE  
 -----  
 LEFT SIDE      RIGHT SIDE  
 -----

TIME LAG (SEC)  
 RISE TIME (SEC)  
 BRAKE TORQUE (IN-LB/PST/BRAKE)

0.1400      0.1400      0.1400  
 0.1700      0.1700      0.1700  
 1000.0000      1000.0000      1000.0000

Figure 12. Example of second page of semitrailer parameters.

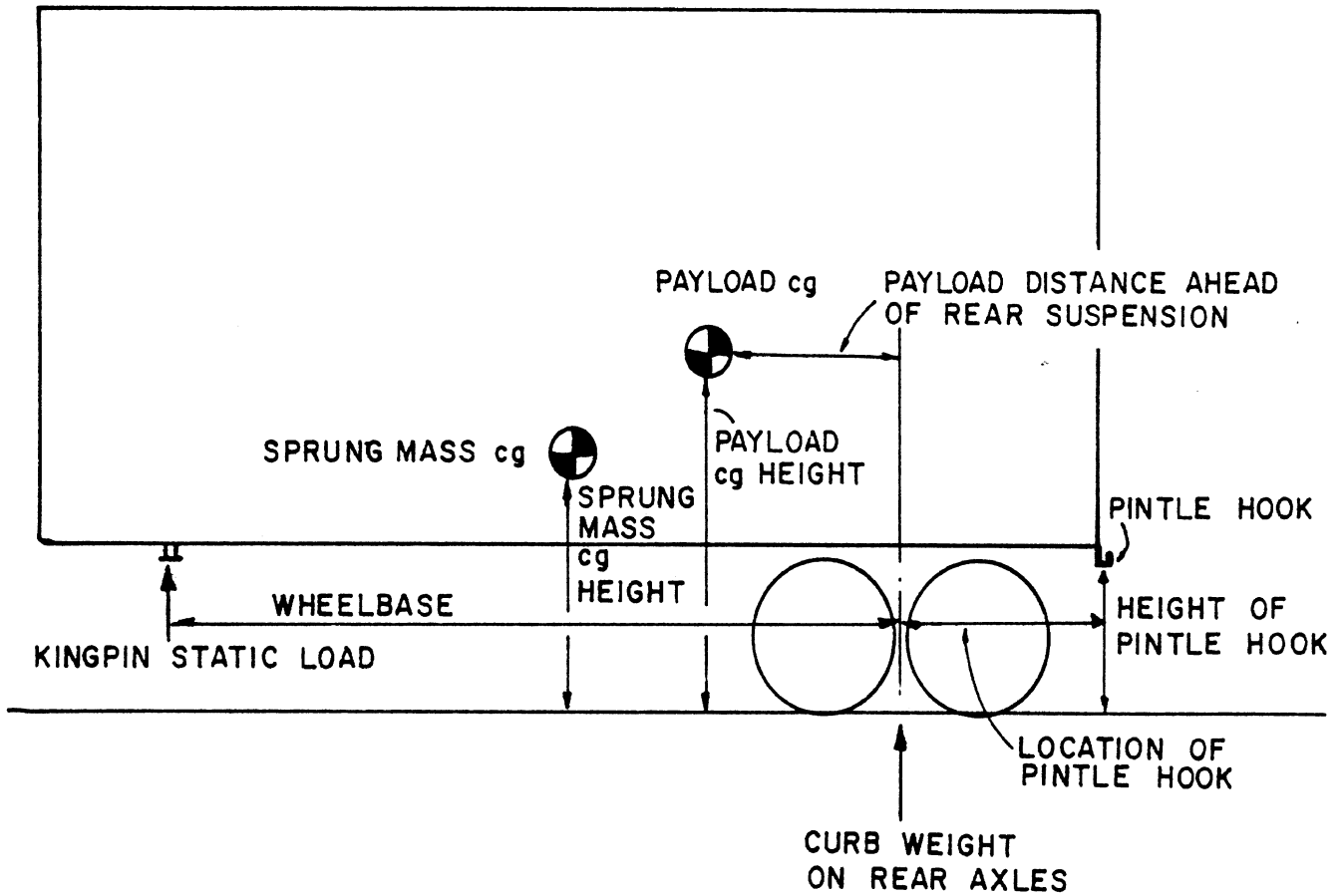


Figure 13. Modeling elements of a semitrailer.

- SPRUNG MASS YAW MOMENT OF INERTIA
- PAYLOAD WEIGHT
  - PAYLOAD DISTANCE AHEAD OF REAR SUSPENSION - Optional
  - PAYLOAD C.G. HEIGHT - Optional
  - PAYLOAD ROLL MOMENT OF INERTIA - Optional
  - PAYLOAD PITCH MOMENT OF INERTIA - Optional
  - PAYLOAD YAW MOMENT OF INERTIA - Optional

Section 3.3.1 gives a detailed description of these parameters for the truck/tractor that is equally applicable here.

If only a tractor-trailer is being simulated, this completes the parameter entries describing the trailer sprung mass. However, if a doubles or triples are to be simulated (i.e., another trailer follows), two more parameters must be entered at this point to locate the pintle hook. The entries required are LOCATION OF PINTLE HOOK (distance in inches behind the rear suspension, F15.3 format), and HEIGHT OF PINTLE HOOK (inches above ground, F15.3 format). The height is taken to be the value when the semitrailer is in its fully loaded static position.

3.4.2 Trailer Suspension, Axle, Tires, Wheels, and Brakes. The parameters to describe these components of the semitrailer follow as shown in Figures 11 and 12. These component entries are identical in format and function to the Truck/Tractor Rear Suspension and Axle Parameters (Section 3.3.4), Truck/Tractor Rear Tires and Wheels (Section 3.3.5), and Truck/Tractor Rear Brakes (Section 3.3.6). The user should refer to these sections to answer questions relating to definitions or format.

### 3.5 Second and Third (Full) Trailer Descriptions

The second and third trailers are always full trailers consisting of a rigid body sprung mass supported at the front on either a fixed or converter dolly, and at the rear by its own suspension and axles. Parametric data for the second trailer is shown in Figures 14 and 15 and is the same for the third trailer. When a third trailer (triples) is simulated, the complete data set as shown in Figures 14 and 15 (with the exception of the two pintle hook parameters) is entered for the third trailer immediately following the second trailer.



TRAILER NO. 2 PARAMETERS

DOLLY KEY: 1 = CONVERTER DOLLY, 2 = FIXED DOLLY  
 DISTANCE FROM TURNABLE CENTER TO PINTLE HOOK (IN)  
 TURNABLE LOCATION (IN AHEAD OF SUSP. CENTER)  
 TURNABLE HEIGHT ABOVE GROUND (IN)  
 WHEELBASE - DISTANCE FROM CENTER OF FRONT SUSP. TO CENTER OF REAR SUSP. (IN)  
 BASE VEHICLE CURB WEIGHT ON FRONT SUSPENSION (LB)  
 BASE VEHICLE CURB WEIGHT ON REAR SUSPENSION (LB)  
 SPRING MASS CG HEIGHT (IN, ABOVE GROUND)  
 SPRING MASS ROLL MOMENT OF INERTIA (IN-LB-SEC\*\*2)  
 SPRING MASS PITCH MOMENT OF INERTIA (IN-LB-SEC\*\*2)  
 SPRING MASS YAW MOMENT OF INERTIA (IN-LB-SEC\*\*2)  
 PAYLOAD WEIGHT (LB)

1  
 60.00  
 0.0  
 52.00  
 300.00  
 8650.00  
 8650.00  
 74.80  
 66274.00  
 542486.00  
 644483.00  
 0.0

\*\*\* ZERO ENTRY INDICATES NO PAYLOAD \*\*\*  
 \*\*\* FIVE PAYLOAD DESCRIPTION PARAMETERS ARE NOT ENTERED \*\*\*  
 LOCATION OF PINTLE HOOK (IN BEHIND REAR SUSP. CENTER)  
 HEIGHT OF PINTLE HOOK (IN ABOVE GROUND)

48.00  
 40.00

TRAILER NO. 2 FRONT SUSPENSION AND AXLE PARAMETERS

SUSPENSION KEY - 0 INDICATES SINGLE AXLE, 1 INDICATES TANDEM AXLES  
 SUSPENSION SPRING RATE (LB/IN/SIDE/AXLE)  
 SUSPENSION VISCOUS DAMPING (LB-SEC/IN/SIDE/AXLE)  
 COULOMB FRICTION (LB/SIDE/AXLE)

0  
 7818.00  
 50.00  
 2600.00

1  
 7818.00  
 50.00  
 2600.00

AXLE ROLL MOMENT OF INERTIA (IN-LB-SEC\*\*2)  
 ROLL CENTER HEIGHT (IN, ABOVE GROUND)  
 ROLL STEER COEFFICIENT (DEG. STEER/DEG. ROLL)  
 AUXILIARY ROLL STIFFNESS (IN-LB/DEG/AXLE)  
 LATERAL DISTANCE BETWEEN SUSPENSION SPRINGS (IN)  
 TRACK WIDTH (IN)  
 UNSPRUNG WEIGHT (LB)

4746.00  
 29.60  
 -0.00  
 35490.00  
 38.00  
 71.25  
 1530.00

TRAILER NO. 2 FRONT TIRES AND WHEELS

DUAL TIRE SEPARATION (IN)  
 CORNERING STIFFNESS (LB/DEG/TIRE)  
 LONGITUDINAL STIFFNESS (LB/SLIP/TIRE)  
 CAMBER STIFFNESS (LB/DEG/TIRE)  
 ALIGNING MOMENT (IN-LB/DEG/TIRE)  
 TIRE SPRING RATE (LB/IN/TIRE)  
 TIRE LOADED RADIUS (IN)  
 POLAR MOMENT OF INERTIA (IN-LB-SEC\*\*2/WHFLL)

12.40  
 600.00  
 21000.00  
 0.0  
 0.0  
 4500.00  
 20.20  
 212.00

12.40  
 600.00  
 21000.00  
 0.0  
 0.0  
 4500.00  
 20.20  
 212.00

Figure 14. Example of first page of full trailer parameters.

TRAILER NO. 2 REAR SUSPENSION AND AXLE PARAMETERS

LEADING TANDEM AXLE		TRAILING TANDEM AXLE	
LEFT SIDE	RIGHT SIDE	LEFT SIDE	RIGHT SIDE
-3.00	-3.00	-3.00	-3.00
50.00	50.00	50.00	50.00
2600.00	2600.00	2500.00	2600.00

SUSPENSION KEY - 0 INDICATES SINGLE AXLE, 1 INDICATES TANDEM AXLES  
 TANDEM AXLE SEPARATION (IN BETWEEN LEADING AND TRAILING AXLES) 1  
 STATIC LOAD TRANSFER (PERCENT LOAD ON LEAD AXLE) 48.00  
 DYNAMIC LOAD TRANSFER (PERCENT OF BRAKE TORQUE TRANSFERRED ONTO LEADING AXLE) 50.00  
 10.00

SUSPENSION SPRING RATE (LR/IN/SIDE/AXLE) -3.00

\*\*\* NEGATIVE ENTRY INDICATES TABLE ENTERED \*\*\*

\*\*\* ECHO WILL APPEAR ON TABLE INDEX PAGE \*\*\*

SUSPENSION VISCOUS DAMPING (LB-SEC/IN/SIDE/AXLE)

COULOMB FRICTION (LR/SIDE/AXLE)

AXLE ROLL MOMENT OF INERTIA (IN-LB-SEC\*\*2)

POUL CENTER HEIGHT (IN. ABOVE GROUND) 4746.00  
 29.60

ROLL STIFF COEFFICIENT (DEG. STEER/DEG. ROLL) -0.00

AUXILIARY ROLL STIFFNESS (IN-LB/DEG/AXLE) 35490.00

LATERAL DISTANCE BETWEEN SUSPENSION SPRINGS (IN) 38.00

TRACK WIDTH (IN) 71.25

UNSPRUNG WEIGHT (LB) 1530.00

4746.00

29.60

-0.00

35490.00

38.00

71.25

1530.00

4746.00

29.60

-0.00

35490.00

38.00

71.25

1530.00

TRAILER NO. 2 REAR TIRES AND WHEELS

LEADING TANDEM AXLE		TRAILING TANDEM AXLE	
LEFT SIDE	RIGHT SIDE	LEFT SIDE	RIGHT SIDE
12.40	12.40	12.40	12.40
600.00	600.00	600.00	600.00
21000.00	21000.00	21000.00	21000.00
0.0	0.0	0.0	0.0
0.0	0.0	0.0	0.0
4500.00	4500.00	4500.00	4500.00
20.20	20.20	20.20	20.20
212.00	212.00	212.00	212.00

DUAL TIRE SEPARATION (IN)

CORNERING STIFFNESS (LB/DEG/TIRE)

LONGITUDINAL STIFFNESS (LR/SLIP/TIRE)

CAMBER STIFFNESS (LB/DEG/TIRE)

ALIGNING MOMENT (IN-LB/DEG/TIRE)

TIRE SPRING RATE (LR/IN/TIRE)

TIRE LOADED RADIUS (IN)

POLAR MOMENT OF INERTIA (IN-LB-SEC\*\*2/WHEEL)

TRAILER NO. 2 FRONT BRAKES

LEFT SIDE RIGHT SIDE

0.1400 0.1400

0.1700 0.1700

21000.00 21000.00

0.0 0.0

0.0 0.0

4500.00 4500.00

20.20 20.20

212.00 212.00

TIME LAG (SEC)

RISE TIME (SEC)

BRAKE TORQUE (IN-LB/PSI/BRAKE)

0.1400 0.1400

0.1700 0.1700

1000.0000 1000.0000

-5.0000 -5.0000

0.1400 0.1400

0.1700 0.1700

1000.0000 1000.0000

-5.0000 -5.0000

TRAILER NO. 2 REAR BRAKES

LEADING TANDEM AXLE		TRAILING TANDEM AXLE	
LEFT SIDE	RIGHT SIDE	LEFT SIDE	RIGHT SIDE
0.1400	0.1400	0.1400	0.1400
0.1700	0.1700	0.1700	0.1700
1000.0000	1000.0000	1000.0000	1000.0000
-5.0000	-5.0000	-5.0000	-5.0000

TIME LAG (SEC)

RISE TIME (SEC)

BRAKE TORQUE (IN-LB/PSI/BRAKE)

0.1400 0.1400

0.1700 0.1700

1000.0000 1000.0000

-5.0000 -5.0000

Figure 15. Example of second page of full trailer parameters.

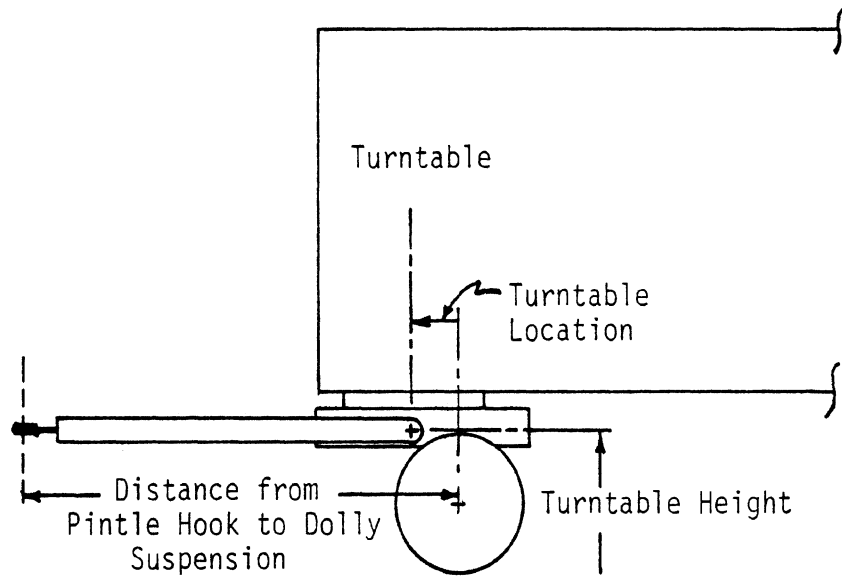
3.5.1 Full Trailer Parameters. A full trailer is modeled by a semitrailer setting on a fixed or converter dolly. The two types of dollies are functionally different, as illustrated in Figure 16. The fixed dolly is attached directly to the trailer and is constrained to move with the trailer in all but the yaw direction. Hence, a pitch direction hinge in the dolly tongue is used to decouple pitch motions from the towing vehicle. The converter dolly incorporates a conventional fifth wheel as a coupling to the trailer. This type of dolly has a rigid tongue and is decoupled from the trailer in yaw and pitch.

Kinematically, the dollies are modeled as shown. The assumptions in the models are as follows:

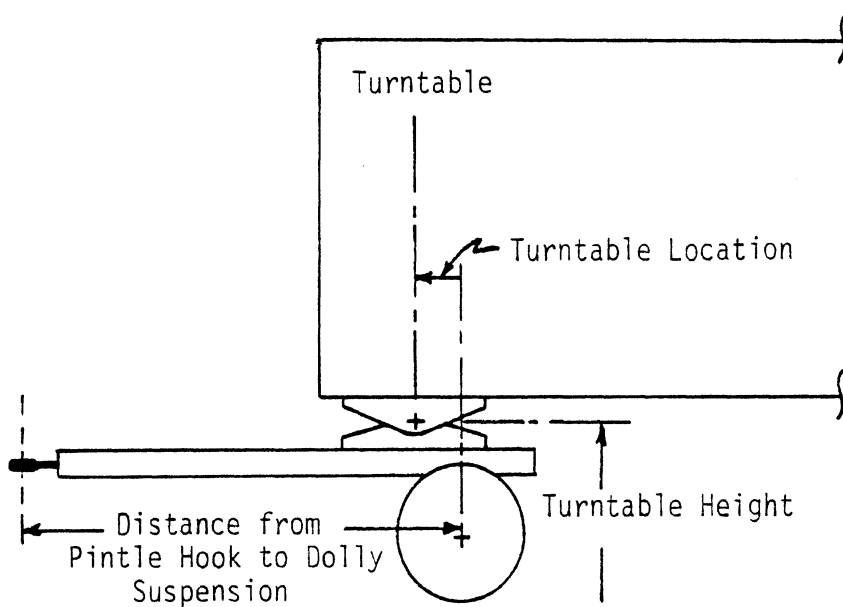
- 1) The yaw inertia of the dolly is assumed negligible.
- 2) The effective sprung mass properties of the dolly are lumped in with that of the trailer.
- 3) Tire longitudinal velocity due to dolly yaw is neglected.

The primary functional difference between the two types of dollies in the simulation is that the converter dolly can exert static load on the rear of the towing trailer, whereas the fixed dolly does not. Like the tractor fifth wheel, the pintle connection is modeled by springs of suitably high stiffness such that they are realistic, yet allow the equations to be coupled by forces rather than displacements. The pintle hitch transmits only longitudinal, lateral and vertical forces, but no moments.

The first parameter entry with a full trailer is the DOLLY KEY (I2 format) for which "01" indicates a converter dolly and "02" a fixed dolly. The next three entries define the geometry for both types of dollies as shown in Figure 16. The first is DISTANCE FROM PINTLE HOOK TO DOLLY SUSPENSION (in., F15.3 format), which defines the effective tongue length of the dolly. For the single-axle dolly this is the distance to the center of the axle, whereas for the tandem axles it is to the midpoint between the two axles. Second is TURNTABLE LOCATION (inches ahead of the suspension center, F15.3 format), which defines the offset between the kingpin or turntable center and suspension system. Last is TURNTABLE HEIGHT (inches above the ground, F15.3 format). By this simplified representation, it is implicitly assumed that the longitudinal tongue forces are applied to the



Fixed Dolly



Converter Dolly

Figure 16. Modeling elements of the fixed and converter dollies.

full trailer at the longitudinal location of the kingpin and at the vertical location defined by the turntable height. Hence, the height should be taken as that of the pitch pivot on the fifth wheel of a converter dolly, and as that of the pitch direction hinge on the tongue of a fixed dolly.

The WHEELBASE (in., F15.3 format) for the full trailer is defined as the distance between the centers of the dolly and the trailer rear suspension systems. The base vehicle sprung mass and longitudinal center of gravity location is then defined by entry of BASE VEHICLE CURB WEIGHT ON FRONT AXLES (lbs., F15.3 format) and BASE VEHICLE CURB WEIGHT ON REAR AXLES (lbs., F15.3 format). In the case of a converter dolly, some weight may be carried on the tongue due to kingpin offset. The front axle curb weight for the converter dolly should include the weight carried on the tongue (i.e., vertical load on the pintle hook). From these static loads, less the unsprung weights that are entered later, sprung mass properties of the trailer are calculated, which include sprung mass contributions from the dolly.

Thereafter, SPRUNG MASS CG HEIGHT, MOMENTS OF INERTIA, and PAYLOAD data, shown in Figure 14, are entered as for a truck/tractor, described in Section 3.3.1.

If the trailer is the second of a three-trailer (triples) combination, pintle hook location data, as follows, appears next.

- LOCATION OF PINTLE HOOK (distance in inches behind the rear suspension, F15.3 format)
- HEIGHT OF PINTLE HOOK (inches above the ground, F15.3 format)

This concludes the trailer parameters.

3.5.2 Full Trailer Suspension, Axles, Tires, Wheels, and Brakes. Input data for these parameters are shown in Figures 14 and 15. The component entries for both the dolly and trailer rear suspensions and axles are identical in format and function to the Truck/Tractor Rear Suspension and Axle Parameters (Section 3.3.4). The tires, wheels and brake component entries are identical to Truck/Tractor Rear Tires and Wheels (Section 3.3.5) and Truck/Tractor Rear Brakes (Section 3.3.6). The user should refer to these sections for definitions and format.

### 3.6 Antilock Brake Description

After the last entries of parametric data (normally the brake data) for the last vehicle in the combination, the user has the option to enter antilock brake control system data for any wheel on the vehicle train. If no antilock data is to be entered for the vehicle, a "00" entry (I2 format) should be entered for the VEHICLE ANTILOCK KEY at this point in the input stream. If antilock data is to be entered, the VEHICLE ANTILOCK KEY entry should be "01" (I2 format). The "01" entry will activate the antilock sub-program to read and echo antilock data according to the format documented in Appendix D, Antilock Simulation. All antilock data must be entered following the "01" entry for the VEHICLE ANTILOCK KEY.

The antilock simulation is a general-purpose program which requires the user to specify operating characteristics of each antilock system simulated. Because of the program's built-in flexibility, permitting simulation of a wide variety of antilock system characteristics, entry and selection of numerical values defining the desired features may be challenging tasks for some first-time users. Examples appearing in Appendix D should prove helpful in understanding the basic program usage.

### 3.7 End of Input

The last line entered in the input stream is the RERUN parameter (I2 format). Note that this parameter is never echoed as an element of the input data list. A "00" entry for RERUN will terminate the program following the simulation run by a CALL EXIT system return. A "01" entry for RERUN is used to perform multiple runs. In this case, a second data set beginning with a Title Line should follow immediately in the same input stream. The "01" RERUN parameter will cause the program to read the second data set and execute the simulation. Following execution for the second data set, its RERUN parameter will be read and the program terminated (RERUN = 00) or a third data set read (RERUN = 01). In the event a data set is not entered following an "01" RERUN entry, a system I/O interrupt will occur and the program generally terminated by the specific system executive.

Job Control Language cards, when required at a specific computer installation to terminate/unload the program, should follow the RERUN parameter.

## 4.0 PROGRAM OUTPUT

### 4.1 General

Operation of the T3DRS:V1 program generates output in a format compatible with line printer systems with 132 or more characters per line. The output falls in three categories—echo of input data, a Summary Page describing the load conditions of the simulation vehicle(s), and time-based listing of simulation output variables.

Fixed and separate page numbering systems are used with the input echo and simulation output pages. The numbering systems are described in Sections 4.2 and 4.4 where those outputs are discussed. All pages have a two-line heading with the title of the T3DRS:V1 program and the one-line title supplied by the user.

4.1.1 Output Options. Only the simulation output pages can be optionally selected by the user. The Input Echo pages and simulation vehicle Summary Page are always printed if the input data is successfully read. The output page options are specified by a seven-digit key read in the Simulation Operation Parameter input group (see Section 3.2). If a simulation input is submitted with zero SIMULATION TIME and no output options, only the Input Echo pages and simulation vehicle Summary Page are obtained. This technique can be used to check an input list prior to making a simulation run.

4.1.2 Coordinate Systems. In order to interpret the vehicle motion parameters given in the simulation output, it is necessary to define the coordinate systems used. Two coordinate systems are necessary to describe the simulated motion of each vehicle; an inertial coordinate system and a body fixed coordinate system, as shown in Figure 17.

The inertial coordinate system is a right-hand orthogonal system fixed in space that serves as the reference point from which vehicle motions and attitudes are defined. The origin is placed at the truck/tractor sprung mass center of gravity at the beginning of the simulation (time=0). The inertial coordinate system is aligned with the gravity vector and the

horizontal projection of the truck/tractor longitudinal axis. The axes are defined according to SAE convention as follows:

X - horizontal out the front of the vehicle

Y - horizontal out the right side of the vehicle

Z - vertically downward in the direction of gravity

The body fixed coordinate system is located and fixed in the vehicle and defines the vehicle location and attitude. Its origin is at the sprung mass center of gravity and is oriented as follows:

x - longitudinally out the front of the vehicle

y - laterally out the right side of the vehicle

z - vertically in the plane of the vehicle sprung mass

Each vehicle in the simulated combination has a separate body fixed coordinate system.

At the beginning of a simulation run, the origin of the truck/tractor body fixed coordinate system is at the origin of the inertial coordinate system. Furthermore, if the vehicle is on a level surface, the axes of the body fixed system are coincident with those of the inertial system.

Since all vehicles in a combination are aligned on the inertial X axis at the beginning of a simulation, all trailers start off with a negative X coordinate and a zero Y coordinate. Since all vehicles may have a different sprung mass center of gravity height as well as different elevations due to road grade, the height of each vehicle in the inertial system is referenced from its initial height (i.e., the Z coordinate for each vehicle is defined by the change from its initial elevation).

During a simulation, the position and attitude of each vehicle is defined by the position and attitude of its body fixed coordinate system in the inertial coordinate system. The vehicle position is given by the X, Y, and Z coordinates locating the origin of the body fixed system. The attitude is defined by Euler angles which orient the body fixed coordinate system with respect to the inertial coordinate system. That is, at any instant of time, the vehicle attitude is defined by the following three rotations going from the orientation of a translated inertial coordinate system to the orientation of the body fixed system.



- 1) Heading angle - rotation in the X-Y inertial plane about the Z axis; positive clockwise when viewed from above.
- 2) Pitch angle - rotation about the y body axis, out of the X-Y inertial plane; positive clockwise looking from left to right on the vehicle.
- 3) Roll angle - rotation about the x body axis; positive clockwise looking forward on the vehicle.

#### 4.2 Input Echo

The first series of pages in the program output is an echo of the input data used to define the vehicles and simulation to be made. The echo pages are labeled as "Input Page No.\_\_\_\_" and are numbered sequentially as follows:

<u>Input Page No.</u>	<u>Content</u>
1	Simulation Operation Parameters
2-3	Truck/Tractor Parameters
4-5	First (Semi-) Trailer Parameters
6-7	Second (Full-) Trailer Parameters
8-9	Third (Full-) Trailer Parameters

As a minimum, pages 1-3 are always printed, while pages 4-9 appear only if a tractor-trailer, doubles, or triples are being simulated.

The input echo is designed to match line for line as much as possible with the input data list so that a copy of the echo can be used as a model for assembling a new input data list. Every line showing a numerical value corresponds to an input line. Blank lines on the echo pages are there only for ease of reading and should not be included in an input list, lest they be read as zero entries. Where multiple numbers are entered on one input line (see discussions in Section 3.0 for format), they appear on one line of echo. Where the side-to-side option is available (see Section 3.1.3) left- and right-side values are shown on a line. Two exceptions to the above rules must be observed:

- 1) When a table lookup option is used, the tabular data entered beginning on the next line in the input is printed on the Table Pages of the output (see example in Appendix A).
- 2) When the tandem-axle option is used, data in each group (suspensions and axles; tires and wheels; brakes) which were entered first for the leading axle then for the trailing axle are printed side by side in the echo for ease of reading.

The input echo is produced during the input data reading process, printing after every few lines of read. An error in the input list will at times halt the reading process and prevent the program from running. In those cases, output of the echo up to the point of the reading fault will be produced, serving as an aid in diagnosing the input error.

At the end of the echo on the last vehicle, the various lookup tables that have been entered are printed in an unnumbered series of pages as required. The tables are printed by categories as follows, in the order in which they were entered:

- 1) Suspension Spring Rate
- 2) Tire Data
- 3) Brake Torque

The tables are identified by the number assigned in the call statement.

If antilock brake control systems were used at any wheel in the vehicle configuration, a series of output pages follows at this point to describe the antilock system(s) used. The format and meaning of the antilock echo pages are given in Appendix D.

#### 4.3 Summary Page

At the completion of a successful input data read, the program calculates the necessary composite characteristics of the vehicle combination. These data are printed on the Summary Page, as shown in Figure 18.

The program first calculates the composite center of gravity location and moments of inertia for the vehicle sprung mass with payload, the

HSR1 TRUCK AND TRACTOR-TRAILER DYNAMIC RESPONSE SIMULATION - T3DRS.VI  
 SAMPLE RUN - TRIPLES BRAKING IN A TURN, ALL OPTIONS EXERCISED

TRAILER NO. 3      PAYLOAD = 0.0 LBS.  
 DISTANCE FROM TRAILER SPRUNG MASS CENTER TO REAR SUSPENSION (IN)      150.000      LOADED  
 DISTANCE FROM TRAILER SPRUNG MASS CENTER TO GROUND (IN)      74.800      74.800  
 ROLL MOMENT OF INERTIA OF TRAILER SPRUNG MASS (IN-LB-SEC\*\*2)      66223.938  
 YAW MOMENT OF INERTIA OF TRAILER SPRUNG MASS (IN-LB-SEC\*\*2)      542485.938  
 YAW MOMENT OF INERTIA OF TRAILER SPRUNG MASS (IN-LB-SEC\*\*2)      644482.938

TRAILER NO. 2      PAYLOAD = 0.0 LBS.  
 DISTANCE FROM TRAILER SPRUNG MASS CENTER TO REAR SUSPENSION (IN)      168.057      LOADED  
 DISTANCE FROM TRAILER SPRUNG MASS CENTER TO GROUND (IN)      74.800      74.800  
 ROLL MOMENT OF INERTIA OF TRAILER SPRUNG MASS (IN-LB-SEC\*\*2)      66223.938  
 YAW MOMENT OF INERTIA OF TRAILER SPRUNG MASS (IN-LB-SEC\*\*2)      542485.938  
 YAW MOMENT OF INERTIA OF TRAILER SPRUNG MASS (IN-LB-SEC\*\*2)      644482.938

TRAILER NO. 1      PAYLOAD = 46800.000 LBS.  
 DISTANCE FROM TRAILER SPRUNG MASS CENTER TO REAR SUSPENSION (IN)      174.182      LOADED  
 DISTANCE FROM TRAILER SPRUNG MASS CENTER TO GROUND (IN)      62.253      62.253  
 ROLL MOMENT OF INERTIA OF TRAILER SPRUNG MASS (IN-LB-SEC\*\*2)      83267.250  
 YAW MOMENT OF INERTIA OF TRAILER SPRUNG MASS (IN-LB-SEC\*\*2)      848450.250  
 YAW MOMENT OF INERTIA OF TRAILER SPRUNG MASS (IN-LB-SEC\*\*2)      946404.000

TRACTOR      PAYLOAD = 0.0 LBS.  
 DISTANCE FROM TRACTOR SPRUNG MASS CENTER TO REAR SUSPENSION (IN)      108.519      LOADED  
 DISTANCE FROM TRACTOR SPRUNG MASS CENTER TO GROUND (IN)      40.130      40.130  
 ROLL MOMENT OF INERTIA OF TRACTOR SPRUNG MASS (IN-LB-SEC\*\*2)      36756.996  
 YAW MOMENT OF INERTIA OF TRACTOR SPRUNG MASS (IN-LB-SEC\*\*2)      105492.938  
 YAW MOMENT OF INERTIA OF TRACTOR SPRUNG MASS (IN-LB-SEC\*\*2)      241479.000

THE STATIC LOADS ON THE AXLES ARE:

AXLE NUMBER	LOAD
NS(1,1,1)	9604.379
NS(1,2,1)	16445.969
NS(1,2,2)	16445.969
NS(2,2,1)	13263.669
NS(2,2,2)	10995.207
NS(3,1,1)	9650.000
NS(3,2,1)	4325.000
NS(3,2,2)	4325.000
NS(4,1,1)	4325.000
NS(4,1,2)	4325.000
NS(4,2,1)	4325.000
NS(4,2,2)	4325.000
TOTAL	110254.938

THE TRACTOR TOTAL MASS CENTER IS 68.600 INCHES BEHIND THE FRONT AXLE  
 THE TOTAL YAW MOMENT OF INERTIA IS 401381.875 IN-LB-SEC\*\*2

THE FIRST TRAILER TOTAL MASS CENTER IS 217.966 INCHES BEHIND THE KINGPIN  
 THE TOTAL YAW MOMENT OF INERTIA IS 1188344.000 IN-LB-SEC\*\*2  
 THE SECOND TRAILER TOTAL MASS CENTER IS 150.000 INCHES BEHIND THE TURNABLE CENTER  
 THE TOTAL YAW MOMENT OF INERTIA IS 941574.000 IN-LB-SEC\*\*2

THE THIRD TRAILER TOTAL MASS CENTER IS 150.000 INCHES BEHIND THE TURNABLE CENTER  
 THE TOTAL YAW MOMENT OF INERTIA IS 1046017.500 IN-LB-SEC\*\*2

Figure 18. Example of summary page output.

resultant data being listed on the Summary Page by vehicle for the empty and loaded condition. To minimize the program memory requirements, these data are printed in the order by which they are calculated, which is from the last to the first vehicle.

Second, the static loads on each of the axles of the assembled vehicle combination is printed, front to rear, along with the total (gross combination) weight. The axles are identified by the number NS(i,j,k) where i is the number of the vehicle (numbered consecutively front to rear), j indicates front (1) or rear (2) suspension, and K indicates the axle number on that suspension. These data serve as a good check to ensure that the desired vehicle has been produced by the input data list.

Last, the longitudinal center of gravity location and yaw moment of inertia for the total mass of each vehicle is printed. The longitudinal c.g. location determines the overall axle loads resulting from the vehicle with payload. The total vehicle yaw moment of inertia is the overall resultant from contributions of the sprung mass, payload and axles.

#### 4.4 Simulation Output

The simulation output pages are the product of the simulation run, providing a description of what happens to the vehicle combination in the course of the simulated maneuver. The output pages present lists of the selected vehicle motion variables and operating conditions at specified intervals of time throughout the maneuver. The variables and conditions are presented in columns with each line representing a point in time, measured in seconds, from the beginning of the simulation.

The output is identified by the "Output Page Number" appearing in the upper right-hand corner of each page. The numbering code is as follows:

x.yy.z

where

x = time block

yy = variable page number

z = vehicle number (1 - truck or tractor, 2 - semitrailer,  
3 - first full trailer, 4 - second full trailer)

The time block code arises from the need to minimize computer memory requirements. Each page of output contains up to 41 time increments of output. If the duration of the maneuver and selected time interval for printing results in more than 41 lines of output; to minimize the number of output devices, output for the first 41 time increments (time block 1), is printed; then it continues with the second block of 41 (time block 2), etc. In order to minimize the number of time blocks and hence the bulk of the output pages, the user may want to choose carefully the TIME INCREMENT OF OUTPUT specified in the Simulation Operation Parameters (Section 3.2), using the following information for guidance:

<u>Manuever Duration</u>	<u>Time Increment of Output</u>	<u>No. of Time Blocks</u>
2 sec.	.05 sec.	1
4	.10	1
4	.05	2
6	.15	1
6	.10	2
6	.05	3
8	.20	1
8	.15	2
8	.10	3
8	.05	4

Up to nineteen output variable pages can be requested for each vehicle. The page numbering system and contents of each page are shown in Table I. All pages are printed for each vehicle, with the vehicles taken in sequence. Variable pages are printed in ascending order by page number, but are not necessarily consecutive since output printing can be suppressed by choice of the OUTPUT PAGE OPTION KEYS. In addition, the numbering system allows for four pages in the last four groups since one page is required per axle and some vehicles can have up to four axles. If the vehicle has less than four axles, certain output page numbers will not appear.

4.4.1 Sprung Mass Position Page. Variable page 01, Sprung Mass Position, shown in Figure 19, describes the simulated vehicle motion by its position and rotational attitude in the inertial coordinate system. The



Table I. Simulation Output Page Contents.

Page No.	Title	Variables
01	Sprung Mass Position (Inertial Coordinate System)	Forward, Lateral and Vertical Translation Roll, Pitch and Heading Angles Turn Radius Body Sideslip Angle Articulation Angle
02	Sprung Mass Velocity (Inertial Coordinate System)	Forward, Lateral and Vertical Roll, Pitch, Heading and Articulation Rate
03	Sprung Mass Accelerations (Inertial & Body Fixed Coordinate Systems)	Forward, Lateral and Vertical Roll, Pitch and Heading Vehicle Longitudinal and Lateral
04- 07	Tire Forces* (Tire Axis System)	Vertical, Longitudinal and Lateral Longitudinal and Lateral Coefficient of Friction Steer Angle (First Vehicle Front Axle Only)
08- 11	Brake Data Summary* (Tire Axis System)	Treadle Pressure, Brake Pressure and Brake Torque Wheel Slip and Brake Force Wheel Angular Velocity and Acceleration
12- 15	Lateral Tire Forces and Moment Summary* (Tire Axis System)	Tire Sideslip Angle Lateral Force and Coefficient of Friction Aligning Torque
16- 19	Unsprung Mass Summary* (Inertial Coordinate System)	Axle Position and Velocity (Vertical and Roll) Auxiliary Roll Torque Spring Deflection, Velocity and Force

\*One page per axle, up to four axles per vehicle.





HSRI TRUCK AND TRACTOR-TRAILER DYNAMIC RESPONSE SIMULATION - FDRS, VI  
 SAMPLE RUN - TRIPLES BRAKING IN A TURN, ALL OPTIONS EXERCISED  
 TRAILER NO. 1 SPRUNG MASS POSITION

TIME (SEC)	FORWARD (FT)	LATERAL (FT)	VERTICAL (FT)	ROLL (DEG)	PITCH (DEG)	HEADING (DEG)	TURN RADIUS (FT)	SIDE SLIP (DEG)	ARTICULATION ANGLE (DEG)
0.0	-26.3614	0.0	0.0	0.0	0.0	0.0	*****	0.0	0.0
0.05	-24.0514	0.0000	-0.0000	-0.0001	-0.0000	0.0000	*****	0.0001	0.0305
0.10	-21.9518	0.0000	-0.0000	-0.0021	-0.0000	0.0002	*****	-0.0001	0.2301
0.15	-19.6534	0.0000	-0.0001	-0.0070	-0.0002	0.0007	*****	-0.0006	0.7638
0.20	-17.4573	0.0000	-0.0003	-0.0137	-0.0010	0.0017	115360.	-0.0010	1.7002
0.25	-15.2643	0.0001	-0.0007	-0.0229	-0.0026	0.0034	45376.5859	-0.0008	3.1998
0.30	-13.0763	0.0002	-0.0011	-0.0342	-0.0029	0.0062	23647.0859	0.0004	5.2750
0.35	-10.8971	0.0006	-0.0012	-0.0479	0.0016	0.0107	14629.0703	0.0028	7.9971
0.40	-8.7305	0.0013	-0.0009	-0.0643	0.0078	0.0173	9802.0938	0.0067	11.3604
0.45	-6.5790	0.0024	-0.0003	-0.0836	0.0095	0.0266	6999.1914	0.0124	15.3872
0.50	-4.4442	0.0042	0.0003	-0.1059	0.0098	0.0393	5222.6172	0.0202	20.0705
0.55	-2.3269	0.0069	0.0011	-0.1311	0.0102	0.0558	4024.0713	0.0304	25.4032
0.60	-0.2280	0.0106	0.0018	-0.1590	0.0106	0.0766	3192.2398	0.0433	31.3764
0.65	1.8518	0.0156	0.0024	-0.1894	0.0110	0.1023	2588.1990	0.0593	37.9776
0.70	3.9114	0.0223	0.0029	-0.2219	0.0121	0.1335	2149.2341	0.0785	45.1949
0.75	5.9506	0.0308	0.0037	-0.2561	0.0134	0.1704	1799.2827	0.1014	53.0143
0.80	7.9689	0.0415	0.0038	-0.2915	0.0146	0.2137	1534.7943	0.1280	61.4235
0.85	9.9663	0.0547	0.0043	-0.3279	0.0155	0.2636	1326.0334	0.1586	70.3961
0.90	11.9476	0.0707	0.0049	-0.3649	0.0164	0.3206	1157.7603	0.1933	79.9233
0.95	13.8975	0.0899	0.0055	-0.4023	0.0172	0.3850	1020.8491	0.2322	89.9836
1.00	15.8310	0.1125	0.0062	-0.4398	0.0177	0.4572	908.1868	0.2754	100.5552
1.05	17.7428	0.1390	0.0068	-0.4771	0.0182	0.5374	815.3914	0.3227	111.5750
1.10	19.6328	0.1695	0.0074	-0.5117	0.0189	0.6258	733.5667	0.3747	122.8550
1.15	21.5008	0.2045	0.0081	-0.5424	0.0197	0.7223	668.8652	0.4315	134.2190
1.20	23.3468	0.2441	0.0086	-0.5703	0.0204	0.8270	615.9939	0.4919	145.5311
1.25	25.1706	0.2888	0.0092	-0.5947	0.0212	0.9398	571.7632	0.5557	156.6915
1.30	26.9722	0.3386	0.0098	-0.6163	0.0221	1.0605	535.7036	0.6218	167.6282
1.35	28.7516	0.3937	0.0105	-0.6351	0.0228	1.1890	504.2910	0.6898	178.2852
1.40	30.5085	0.4543	0.0111	-0.6509	0.0234	1.3249	478.0874	0.7592	188.6298
1.45	32.2431	0.5205	0.0117	-0.6640	0.0241	1.4679	455.2134	0.8297	198.6395
1.50	33.9552	0.5923	0.0124	-0.6740	0.0248	1.6176	435.8127	0.9006	208.2916
1.55	35.6445	0.6698	0.0130	-0.6810	0.0254	1.7736	418.1902	0.9719	217.5818
1.60	37.3115	0.7529	0.0137	-0.6851	0.0260	1.9354	403.0615	1.0431	226.5048
1.65	38.9556	0.8417	0.0143	-0.6864	0.0267	2.1028	390.3754	1.1138	235.0562
1.70	40.5771	0.9361	0.0150	-0.6852	0.0274	2.2752	378.6699	1.1838	243.2332
1.75	42.1760	1.0360	0.0156	-0.6820	0.0280	2.4522	368.1350	1.2528	251.0339
1.80	43.7520	1.1413	0.0162	-0.6768	0.0287	2.6335	359.5647	1.3204	258.4602
1.85	45.3053	1.2519	0.0169	-0.6699	0.0293	2.8186	351.7068	1.3865	265.5134
1.90	46.8359	1.3677	0.0175	-0.6616	0.0299	3.0071	344.5557	1.4510	272.2046
1.95	48.3433	1.4884	0.0182	-0.6519	0.0305	3.1986	338.0251	1.5137	278.5354
2.00	49.8281	1.6139	0.0189	-0.6411	0.0312	3.3927	331.9617	1.5748	284.5134

Figure 19. Example of sprung mass position page.

inertial coordinate system is located at the truck/tractor sprung mass center of gravity at time zero in the simulation (see Section 4.1.2). The vehicle position is defined by X (forward), Y (lateral), and Z (vertical) inertial coordinates of the vehicle sprung mass center of gravity during the simulation. For the truck/tractor, the initial coordinates are always zero. Trailers are always aligned behind the tractor so that they start from a negative forward position and zero lateral. Positive lateral is to the right of the vehicle. To avoid confusion from the differing sprung mass heights and road slopes, the vertical position always begins at zero and indicates relative change in elevation. Note that, by SAE convention, positive values of vertical position are downward, in the direction of gravity.

The attitude of the vehicle is given in the next three columns as defined by the Euler angle rotations (roll, pitch and heading) of the body fixed coordinate system (see Section 4.1.2) in the inertial coordinate system.

In addition, the position page contains lists of the instantaneous radius of turn (positive is right turn); the body sideslip angle (arc-tangent of the lateral over forward velocity at the center of gravity); and with articulated combinations, the articulation angle which is the difference between the heading angles of the leading and trailing vehicles (leading minus trailing).

4.4.2 Sprung Mass Velocity Page. Variable page 02, Sprung Mass Velocity, shown in Figure 20, describes the velocity of the sprung mass in the body fixed coordinate system. Forward velocity is along the longitudinal axis of the vehicle (x), Lateral velocity is positive to the right along the y-axis, and Vertical velocity is positive through the bottom of the vehicle. The velocity components given are the time rate of change of the vehicle position vector resolved into components along the body axis system. The forward velocity is the component along the vehicle longitudinal axis which may be interpreted as vehicle speed.

The Roll, Pitch, and Heading rates are obtained by resolving the vehicle rotation vector into components in the body fixed axis system. The user may note that the frequently used term "yaw rate" is the same as heading rate.

TIME (SEC)	FORWARD (FT/SEC)	LATERAL (FT/SEC)	VERTICAL (FT/SEC)	ROLL (DEG/SEC)	PITCH (DEG/SEC)	HEADING (DEG/SEC)	ARTICULATION RATE (DEG/SEC)
0.0	44.00	0.0	0.0	0.0	0.0	0.0	0.0
0.05	44.00	0.00	-0.00	-0.01	-0.00	0.00	1.78
0.10	44.00	-0.00	-0.00	-0.07	-0.00	0.01	6.67
0.15	43.98	-0.00	-0.00	-0.12	-0.01	0.01	14.32
0.20	43.94	-0.00	-0.01	-0.16	-0.03	0.03	24.24
0.25	43.85	-0.00	-0.01	-0.21	-0.03	0.04	35.58
0.30	43.70	0.00	-0.01	-0.25	0.03	0.07	47.92
0.35	43.48	0.00	0.00	-0.30	0.14	0.11	60.82
0.40	43.20	0.01	0.02	-0.36	0.08	0.16	73.94
0.45	42.88	0.01	0.02	-0.41	0.01	0.22	87.12
0.50	42.54	0.01	0.02	-0.48	0.01	0.29	100.19
0.55	42.18	0.02	0.02	-0.53	0.01	0.37	113.11
0.60	41.80	0.03	0.02	-0.59	0.01	0.46	125.80
0.65	41.41	0.04	0.02	-0.63	0.02	0.57	138.24
0.70	41.01	0.06	0.02	-0.67	0.02	0.68	150.43
0.75	40.60	0.07	0.02	-0.70	0.02	0.80	162.33
0.80	40.19	0.09	0.02	-0.72	0.02	0.93	173.89
0.85	39.77	0.11	0.02	-0.74	0.01	1.07	185.10
0.90	39.34	0.13	0.02	-0.75	0.01	1.21	195.96
0.95	38.91	0.16	0.03	-0.75	0.00	1.37	206.40
1.00	38.48	0.18	0.03	-0.75	-0.00	1.52	216.40
1.05	38.05	0.21	0.03	-0.73	-0.00	1.69	223.65
1.10	37.61	0.25	0.03	-0.65	-0.00	1.85	226.94
1.15	37.17	0.28	0.03	-0.59	-0.00	2.01	227.16
1.20	36.73	0.32	0.03	-0.52	-0.01	2.18	224.99
1.25	36.29	0.35	0.03	-0.46	-0.01	2.34	221.21
1.30	35.85	0.39	0.03	-0.41	-0.01	2.49	216.11
1.35	35.40	0.43	0.03	-0.35	-0.02	2.65	210.14
1.40	34.96	0.46	0.03	-0.29	-0.02	2.79	203.64
1.45	34.51	0.50	0.03	-0.23	-0.02	2.93	196.72
1.50	34.07	0.54	0.03	-0.17	-0.02	3.06	189.49
1.55	33.62	0.57	0.03	-0.11	-0.03	3.18	182.19
1.60	33.17	0.60	0.04	-0.06	-0.02	3.29	174.78
1.65	32.73	0.64	0.04	-0.00	-0.03	3.40	167.34
1.70	32.28	0.67	0.04	0.04	-0.03	3.50	159.89
1.75	31.83	0.70	0.04	0.08	-0.01	3.58	152.43
1.80	31.38	0.72	0.04	0.12	-0.03	3.67	144.95
1.85	30.93	0.75	0.04	0.15	-0.03	3.74	137.66
1.90	30.49	0.77	0.04	0.18	-0.03	3.80	130.43
1.95	30.04	0.79	0.04	0.20	-0.03	3.86	123.32
2.00	29.59	0.81	0.04	0.22	-0.03	3.90	116.42

Figure 20. Example of sprung mass velocity page.

With articulated vehicles, the rate of change of the articulation angle is also shown.

4.4.3 Sprung Mass Acceleration Page. Variable page 03, Sprung Mass Acceleration, shown in Figure 21, describes the acceleration of the sprung mass in the body fixed coordinate system. The accelerations in a moving, rotating coordinate system referenced to an inertial system are given by the expressions

$$\dot{u} = \Sigma F_x / M + r \cdot v - q \cdot w$$

$$\dot{v} = \Sigma F_y / M + p \cdot w - r \cdot u$$

$$\dot{w} = \Sigma F_z / M - q \cdot u + p \cdot v$$

where

$F_x, F_y, F_z$  = forces in the longitudinal, lateral, and vertical directions

$M$  = vehicle mass

$u$  = velocity along the x (forward) axis

$v$  = velocity along the y (lateral) axis

$w$  = velocity along the z (vertical) axis

$p, q, r$  = rotation rates about the x, y, z axes

The dot denotes differentiation with respect to time.

The Forward, Lateral and Vertical accelerations on the left side of the page are the time derivatives of the velocities shown on the preceding page, and hence represent the velocity derivatives ( $\dot{u}, \dot{v}, \dot{w}$ ) defined by the above equations. Most users, however, are interested in the total or inertial acceleration of the simulated vehicle (i.e., the first term on the right-hand side in the above equations). Therefore, a set of Longitudinal and Lateral inertial accelerations resolved into the body axis coordinate system are given on the right side of the page. In effect, these are equivalent to those accelerations felt while in the vehicle. The Longitudinal and Forward accelerations are effectively equivalent because of the small velocities and rotation rates normally involved in the longitudinal equation. (The same would be true for vertical acceleration if it were shown.) The lateral accelerations will differ in turning maneuvers, however, because of the " $r \cdot u$ " term, which is the centripetal acceleration.

HSRI TRUCK AND TRACTOR-TRAILER DYNAMIC RESPONSE SIMULATION - T3DRS.VI  
 SAMPLE RUN - TRIPLES BRAKING IN A TURN, ALL OPTIONS EXERCISED

INERTIAL ACCEL. ALONG BODY AXES

TIME (SEC)	FORWARD (FT/SEC**2)	LATERAL (FT/SEC**2)	VERTICAL (FT/SEC**2)	ROLL (DEG/SEC**2)	PITCH (DEG/SEC**2)	HEADING (DEG/SEC**2)	LONGITUDINAL (FT/SEC**2)	LATERAL (FT/SEC**2)
0.0	0.0	0.0	0.0	0.0	0.0	0.0	-0.0	0.0
0.05	-0.0753	0.0014	-0.0014	-0.7340	-0.0048	0.0628	-0.0053	0.0026
0.10	-0.1170	-0.0065	-0.0205	-1.2932	-0.0571	0.1348	-0.1170	-0.0016
0.15	-0.4767	-0.0083	-0.0642	-0.6240	-0.2060	0.1730	-0.4767	0.0027
0.20	-1.2013	-0.0073	-1.0644	-1.0644	-0.5222	0.2867	-1.2013	0.0169
0.25	-2.3833	0.0092	-0.0398	-0.7832	0.4662	0.4621	-2.3833	0.0428
0.30	-3.7605	0.0268	0.1531	-0.9514	2.2635	0.6434	-3.7605	0.0912
0.35	-5.0349	0.0467	0.3026	-1.1605	0.8304	0.8694	-5.0349	0.1295
0.40	-5.9390	0.0713	0.1165	-1.0603	-2.3535	1.0838	-5.9390	0.1905
0.45	-6.5658	0.0991	0.0649	-1.2705	-0.4939	1.3142	-6.5658	0.2623
0.50	-7.0437	0.1302	0.0401	-1.1464	0.1038	1.5391	-7.0437	0.3451
0.55	-7.4167	0.1657	-0.0237	-1.1035	-0.0877	1.7511	-7.4169	0.4394
0.60	-7.6551	0.2039	-0.0399	-1.0041	0.1658	1.9587	-7.6554	0.5429
0.65	-7.8874	0.2457	-0.0235	-0.9078	0.1750	2.1536	-7.8878	0.6559
0.70	-8.0774	0.2898	-0.0011	-0.6934	0.0743	2.3367	-8.0781	0.7764
0.75	-8.2367	0.3355	0.0170	-0.5114	-0.1496	2.5106	-8.2377	0.9031
0.80	-8.3271	0.3825	0.0366	-0.3736	-0.1477	2.6780	-8.3285	1.0353
0.85	-8.4204	0.4295	0.0455	-0.2529	-0.0404	2.8318	-8.4225	1.1711
0.90	-8.5275	0.4766	0.0366	-0.1461	-0.0153	2.9718	-8.5253	1.3099
0.95	-8.5909	0.5225	0.0173	-0.0532	-0.1734	3.1103	-8.5946	1.4501
1.00	-8.6004	0.5669	0.0069	0.0391	-0.1176	3.2365	-8.6053	1.5908
1.05	-8.6830	0.6083	0.0102	1.0449	0.0560	3.2593	-8.6893	1.7286
1.10	-8.7364	0.6594	0.0065	1.7376	-0.0365	3.2368	-8.7443	1.8733
1.15	-8.7907	0.6961	0.0078	0.9782	-0.0895	3.2831	-8.8001	2.0015
1.20	-8.7965	0.7213	0.0179	1.5118	0.0596	3.2405	-8.8085	2.1163
1.25	-8.8675	0.7397	0.0262	1.0488	0.0423	3.1745	-8.8818	2.2189
1.30	-8.8145	0.7431	0.0179	1.0950	-0.2424	3.1079	-8.8315	2.3032
1.35	-8.8587	0.7442	0.0214	1.2356	-0.0822	2.9801	-8.8783	2.3789
1.40	-8.8979	0.7362	0.0220	1.0467	-0.0138	2.8414	-8.9204	2.4189
1.45	-8.9023	0.7241	0.0166	1.2358	-0.0934	2.6904	-8.9279	2.4884
1.50	-8.8932	0.7064	0.0112	1.2367	-0.0904	2.5105	-8.9218	2.5249
1.55	-8.9517	0.6852	0.0114	1.1343	0.0200	2.3554	-8.9834	2.5512
1.60	-8.9227	0.6599	0.0168	1.0970	0.0405	2.1948	-8.9574	2.5668
1.65	-8.9240	0.6300	0.0096	0.9942	-0.0858	2.0205	-8.9618	2.5712
1.70	-8.9704	0.5992	0.0114	0.9222	0.0487	1.8746	-9.0111	2.5684
1.75	-8.9871	0.5661	0.0136	0.7052	0.0227	1.7276	-9.0306	2.5574
1.80	-8.9377	0.5263	0.0090	0.6867	-0.0206	1.5213	-8.9840	2.5338
1.85	-8.9814	0.4896	0.0072	0.5499	0.0111	1.3734	-9.0303	2.5072
1.90	-8.9134	0.4504	0.0081	0.5195	-0.0045	1.2121	-8.9647	2.4726
1.95	-8.9524	0.4108	0.0044	0.5078	0.0570	1.0063	-9.0059	2.4327
2.00	-8.9501	0.3717	0.0002	0.4372	-0.0390	0.8514	-9.0055	2.3980

Figure 21. Example of sprung mass acceleration page.

The Roll, Pitch and Heading accelerations are the resolution of the total rotational acceleration vector into the body fixed coordinate system. (The time derivatives of the rotational velocities appearing on the preceding page.)

4.4.4 Tire Forces Page. Variable pages 04-07, Tire Forces, shown in Figure 22, provide a summary of the vertical, longitudinal and lateral forces exerted on the tires at the tire/road interface. The forces are presented for tires on both the left and right sides of the axle, with each axle on a separate page. The forces are defined in the axis system of the wheel according to SAE convention (see Figure 23). All forces and moments acting on the tire are measured relative to the center of the tire/road contact patch which may be defined as the point of intersection of the road plane, wheel plane and a perpendicular plane through the wheel spin axis.

The Vertical force is the instantaneous force in the center of tire/road contact patch normal to the road. Vertical force on the tire in the upward direction is defined by SAE convention as positive. The Longitudinal force is the force in the road plane in the direction of the wheel heading. Negative values correspond to a braking force. Lateral force is the force in the road plane perpendicular to the wheel heading with positive values corresponding to a force on the tire to the right, when looking in the direction of wheel heading. A positive Lateral force results when the tire is steered to the right.

Two variables, "MU-X" and "MU-Y" are also printed. These variables are the respective ratios of the longitudinal and lateral forces to the vertical force, and represent the normalized friction levels being utilized in each direction.

4.4.5 Brake Data Summary Page. Variable pages 08-11, Brake Summary, provide detailed information on the brake function on the left and right wheels of each axle. The page, shown in Figure 24, lists the treadle pressure being applied by interpolation of the Treadle Pressure Table input for the simulation, and the brake pressure in the chamber that results from action of the time lags and rise times for each brake. Next is listed the actual brake torque produced at the wheel. If the wheel is moving,



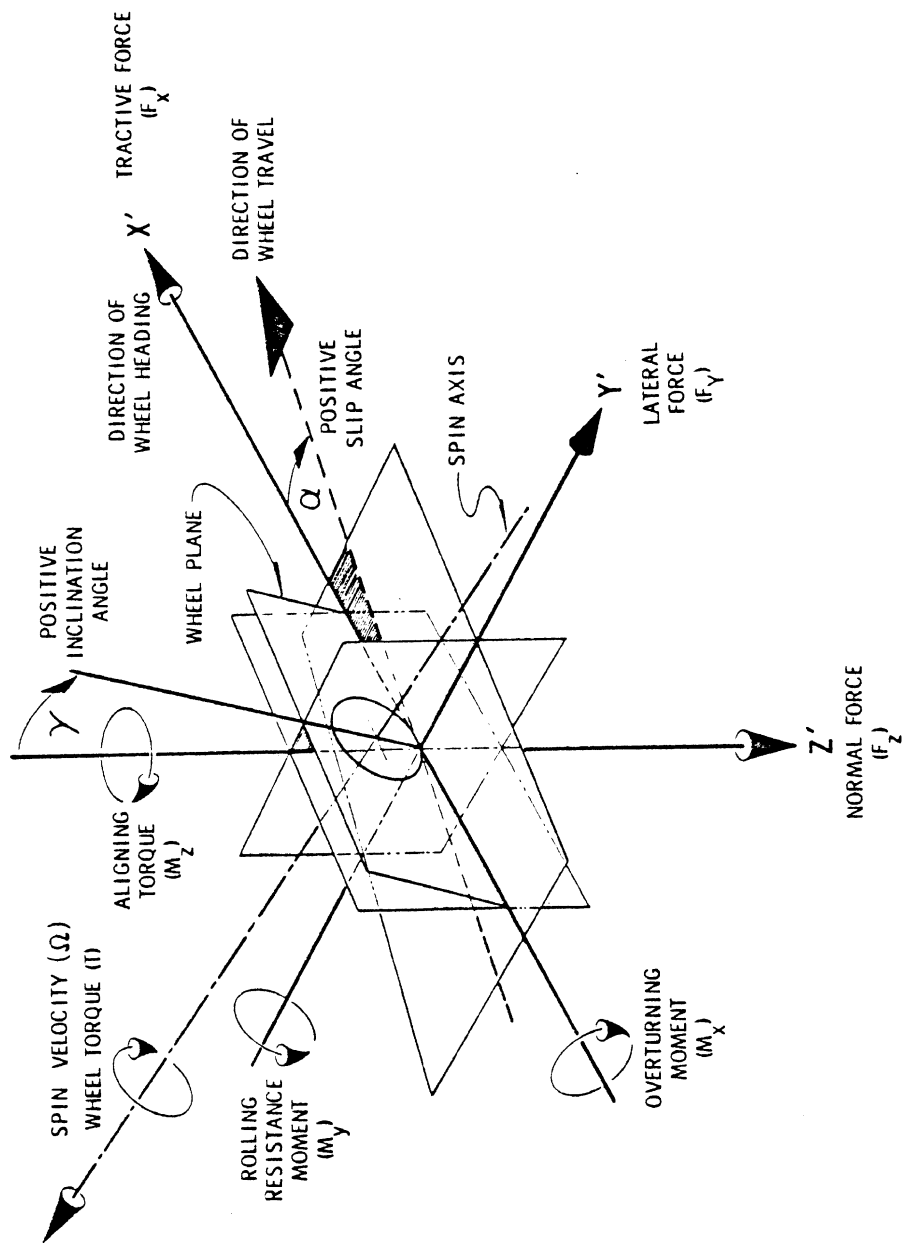


Figure 23. SAE Tire Axis System





the torque corresponds to that of the brake torque coefficient or table value input at the applied pressure. However, if the wheel reaches lock-up, the actual torque is limited by the tire friction and may be less than the attempted value. In addition to brake torque, the tire brake force is listed which, in effect, is an indication of the portion of the brake torque applied to decelerating the vehicle. In the simulation, the torque is actually applied to the wheel causing it to decelerate, with the tire brake force resulting from longitudinal slip in the tire model. Hence, at any instant of time a portion of the brake torque may be devoted to decelerating the wheel rather than to developing actual braking force. The wheel slip, angular wheel velocity and angular wheel acceleration are also listed for their utility in investigating antilock braking system performance.

4.4.6 Lateral Pages. Variable pages 12-15, Lateral Tire Force and Moment Summary, shown in Figure 25, provide detailed information on the cornering performance of each tire on the vehicle combination. Each page lists the left and right side cornering parameters for an axle on the vehicle. The first parameter is tire sideslip angle, which by SAE convention is positive when the tire is sideslipping to the right of its heading direction (see Fig. 23). Next is listed the tire lateral force, which is the force on the tire in the road plane perpendicular to the wheel heading, positive force being to the right. The parameter "MU-Y" is the lateral force value normalized by the instantaneous vertical load. Finally, the aligning torque developed on the tire is listed. The aligning torque is perpendicular to the road plane and is positive clockwise looking down on the tire.

On axles with dual wheel assemblies, the values listed on this page are the total for the two tires.

4.4.7 Unsprung Mass Summary Page. Variable pages 16-19, Unsprung Mass Summary, provide detailed information as to what is happening to each of the axles and suspensions on the simulated vehicle. On the left side of the page, shown in Figure 26, are given axle motion parameters; specifically, the position and velocity for the axle's two degrees of freedom (vertical and roll). The axle vertical and roll positions are measured relative to the inertial coordinate system. Positive vertical is down and is the

SAMPLE RUN - TRIPLES BRAKING IN A TURN, ALL OPTIONS EXERCISED  
 TRAILER NO. 1 REAR SUSPENSION - LATERAL TIRE FORCE AND MOMENT SUMMARY  
 LEADING TANDEM AXLE

TIME (SEC)	LEFT SIDE				RIGHT SIDE			
	TIRE SIDESLIP ANGLE (DEG)	TIRE LATERAL FORCE (LR)	MU-Y	ALIGNING TORQUE (IN-LB)	TIRE SIDESLIP ANGLE (DEG)	TIRE LATERAL FORCE (LR)	MU-Y	ALIGNING TORQUE (IN-LB)
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.05	0.0004	-0.4723	-0.0001	0.0	0.0	-0.4723	0.0	0.0
0.10	0.0025	-3.0457	-0.0005	0.0	0.0025	-3.0444	-0.0005	0.0
0.15	0.0025	-3.0589	-0.0005	0.0	0.0025	-3.0507	-0.0005	0.0
0.20	0.0016	-1.9208	-0.0003	0.0	0.0016	-1.9096	-0.0003	0.0
0.25	-0.0006	0.6778	0.0001	0.0	-0.0006	0.6708	0.0001	0.0
0.30	-0.0044	5.8730	0.0009	0.0	-0.0048	5.7792	0.0009	0.0
0.35	-0.0099	12.1543	0.0014	0.0	-0.0099	11.8951	0.0018	0.0
0.40	-0.0168	21.2247	0.0030	0.0	-0.0169	20.5830	0.0030	0.0
0.45	-0.0251	32.3371	0.0045	0.0	-0.0251	31.0767	0.0045	0.0
0.50	-0.0347	45.8300	0.0063	0.0	-0.0348	43.5923	0.0063	0.0
0.55	-0.0459	61.9841	0.0083	0.0	-0.0459	58.2870	0.0083	0.0
0.60	-0.0580	80.2044	0.0105	0.0	-0.0581	74.4966	0.0105	0.0
0.65	-0.0712	100.8151	0.0129	0.0	-0.0713	92.4183	0.0129	0.0
0.70	-0.0950	123.2435	0.0154	0.0	-0.0952	111.4496	0.0154	0.0
0.75	-0.0922	147.1950	0.0180	0.0	-0.0994	131.2674	0.0180	0.0
0.80	-0.1136	172.4881	0.0206	0.0	-0.1139	151.1675	0.0206	0.0
0.85	-0.1279	198.6342	0.0231	0.0	-0.1283	172.2474	0.0232	0.0
0.90	-0.1419	225.2343	0.0257	0.0	-0.1423	192.6528	0.0258	0.0
0.95	-0.1552	251.9317	0.0281	0.0	-0.1558	212.6296	0.0282	0.0
1.00	-0.1630	278.5791	0.0304	0.0	-0.1687	232.1034	0.0305	0.0
1.05	-0.1806	305.7227	0.0327	0.0	-0.1814	251.5879	0.0328	0.0
1.10	-0.1943	335.6958	0.0352	0.0	-0.1953	273.0833	0.0353	0.0
1.15	-0.2037	358.6191	0.0369	0.0	-0.2049	289.1694	0.0371	0.0
1.20	-0.2113	378.5803	0.0382	0.0	-0.2126	303.0171	0.0385	0.0
1.25	-0.2164	394.4719	0.0392	0.0	-0.2179	313.9775	0.0394	0.0
1.30	-0.2195	404.6030	0.0395	0.0	-0.2201	320.8179	0.0398	0.0
1.35	-0.2195	412.7163	0.0397	0.0	-0.2212	326.3584	0.0400	0.0
1.40	-0.2179	415.6582	0.0394	0.0	-0.2197	328.3271	0.0398	0.0
1.45	-0.2148	415.1943	0.0389	0.0	-0.2166	327.9983	0.0392	0.0
1.50	-0.2101	411.4404	0.0380	0.0	-0.2120	325.4766	0.0384	0.0
1.55	-0.2036	403.6021	0.0368	0.0	-0.2056	320.1328	0.0372	0.0
1.60	-0.1957	392.4668	0.0354	0.0	-0.1977	312.4790	0.0358	0.0
1.65	-0.1865	378.1211	0.0338	0.0	-0.1885	302.5024	0.0341	0.0
1.70	-0.1761	360.6746	0.0319	0.0	-0.1781	290.1882	0.0322	0.0
1.75	-0.1647	340.6843	0.0298	0.0	-0.1667	275.8623	0.0302	0.0
1.80	-0.1527	318.7136	0.0276	0.0	-0.1545	259.8665	0.0280	0.0
1.85	-0.1398	294.4583	0.0253	0.0	-0.1415	241.8901	0.0256	0.0
1.90	-0.1264	268.5969	0.0229	0.0	-0.1280	222.3804	0.0232	0.0
1.95	-0.1128	241.7359	0.0204	0.0	-0.1143	201.7634	0.0207	0.0
2.00	-0.0986	212.9695	0.0174	0.0	-0.0999	179.2546	0.0181	0.0

Figure 25. Example of tire lateral force and moment summary page.



elevation relative to its starting position. Roll is positive in the clockwise direction facing forward on the vehicle. Roll angle is always measured relative to the horizontal X-Y plane in the inertial coordinate system.

Suspension motions and forces are given on a side-to-side basis (at the suspension spring locations). The auxiliary roll torque arising from the auxiliary roll stiffness is listed first since it is associated with both sides of the suspension. A positive torque corresponds to a positive roll moment exerted on the vehicle sprung mass.

Thence the relative suspension deflection, velocity and force is listed for each side of the suspension. The deflection is indicated in terms of its change from the static loaded deflection, with positive values equivalent to extension of the suspension. The suspension force is actually the change in force from its static value. Positive force is a downward force on the sprung mass. The suspension force is the total of contributions from the springs, coulomb and viscous friction and braking load transfer effects.

## 5.0 PROGRAM DIAGNOSTICS

Errors in operation of T3DRS:V1 occur basically in two categories—Input Errors and Simulation Run Errors. Only a few error messages are contained within the program so that the user needs to be aware of some of the pitfalls that may be experienced in order to identify the proper corrective action. In the normal batch running mode, the user will find the error only by the fact that the program fails to run properly and a correction and resubmission is required.

### 5.1 Input Errors

The most critical operation and most likely source of errors in using the program occurs in the process of reading input data describing the vehicle and maneuver desired. Since the data type is only identified by its location in a sequence of input lines, one data line missing, out of place, or with incorrect format can confound the entire data reading process. For this reason, the users should consult Section 3 of this Manual and the numerous examples of input provided when preparing an input list. The severity of any error depends on its meaning to the program when read, and the type of computer system on which the simulation is operating. The most common error is a simple format error. Systems that allow a free read format can significantly reduce this type of problem.

Two error messages are incorporated in the input subroutine of the program. Tables in the table lookup option are identified by the whole number value following the negative sign keying the table lookup. Unique numbers must be used for each table, unless the table is to be used at multiple points on the vehicle. If the number identifying a table for one type of parameter (e.g., suspension spring rate) is inadvertently assigned for a second type of parameter (e.g., brake torque), an error message to this effect is printed and execution terminates.

The second error message relates to the value for the DRIVER TRANSPORT LAG parameter, included in the path-follower model. If the value assigned is greater than one second, the simulated vehicle is certain to be unstable and unable to run. Hence, an error message is printed indicating that the value is too large and program execution is terminated.

Recognizing that errors will occur, several scenarios of possible consequences are given below.

- 1) Non-Fatal Errors - In simple cases where a parametric value is misread (due to a forgivable format error) or values are interchanged (due to lines being out of order), the program may not recognize that an error has occurred. In that case, the program may successfully complete the read process and execute the simulation even though with an erroneous vehicle description. To discover such errors, the user should continually review the input echo pages and vehicle summary page to ensure that the proper vehicle conditions have been obtained.
- 2) Fatal Errors - The more common case is an error that is incompatible with the input reading process resulting in a system interrupt and termination of the program execution. Since the input echo is printed after every few lines of reading, the major portion of the input successfully read is reflected in the output obtained. For diagnosis of the problem, the user should review the echoed portion of the input, then the lines immediately following the termination point as the likely locations of the error.

## 5.2 Simulation Run Errors

Once the calculation process constituting the vehicle simulation has begun, only one type of error will occur that will halt the execution. Normal job termination occurs by either the vehicle reaching a full stop, or simulation to the MAXIMUM SIMULATION TIME limit specified in the input. Otherwise, the simulation may terminate with the message "IHLF=11." The message derives from the inability of the integration process (the IBM Scientific Subroutine Package HPCG) to converge on a solution at a particular point in time. Integration is normally carried out at 0.0025-second time steps with the option of halving the time step when necessary to meet an error criteria. The integration algorithm is allowed to halve the time step eleven times in an effort to achieve a satisfactory integration, and





if unsuccessful, the execution is terminated with the above error message. As a general rule to prevent this error, the user should ensure that all dynamic systems being simulated have a natural frequency of less than 20 Hz. In particular, this error most commonly occurs when inertia values are inordinately low or stiffness values (especially spring and tire rates) are too high. In general, a simple check for this is to ensure that the smallest mass connected to any spring has a mass (in pounds) to spring rate (pounds/inch) ratio greater than 0.025 inches.

Finally, the simulation is only expected to be valid in maneuvers up to the severity point where a wheel lifts off the ground. The above error will often occur after a prolonged period of wheel lift-off or when the vehicle has reached a divergent rollover condition. The accuracy of the calculations up to this point is limited by the small angle assumptions used in the programming. However, it should be found that the wheel lift-off condition occurs at body roll angles of 8-10 degrees with most heavy vehicles simulated, whereas the small angle assumptions should not create significant error until angles approach 20 degrees.



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## APPENDIX A

### SAMPLE RUN OF A TRUCK

The following pages are copies of the complete computer output package obtained from a four-second simulation of a straight truck in a step-steer maneuver. The first four pages are an echo of the input with a summary of composite vehicle characteristics. These pages are normally reviewed to ensure that the desired vehicle and maneuver is being simulated. The remaining 12 pages are all the output pages (excluding the Brake Data Summary Page, since no braking is applied) indicating the vehicle's response in the maneuver.

The maneuver is a right-hand step-steer of 8 degrees at the front wheels, applied at 0.1 seconds into the run. The vehicle responds by turning to the right with some initial transients that effectively settle out after a few seconds into the run. The vehicle is stable and assumes a steady-state turn at about 0.25 g's (8 ft/sec<sup>2</sup>) lateral acceleration.



SIMULATION OPERATION PARAMETERS:  
-----

VEHICLE CONFIGURATION (NUMBER OF TRAILERS - ENTER 0 FOR A STRAIGHT TRUCK) 0  
INITIAL VELOCITY (FT/SEC) 30.00  
STEER TABLE (NUMBER OF LINES): POSITIVE -STEER ANGLE TABLE, NEGATIVE - PATH FOLLOWER TABLE 3  
TABLE ENTRIES: TIME (SEC) LEFT WHEEL (DEG) RIGHT WHEEL (DEG)  
-----  
0.0 0.0 0.0  
0.10 8.00 8.00  
0.00 8.00 8.00

TREADLE PRESSURE TABLE (NUMBER OF LINES) 0  
\* ZERO ENTRY INDICATES NO FURTHER TABLE DATA IS NECESSARY - THE FOLLOWING TABLE IS ASSIGNED INTERNALLY \*  
TABLE ENTRIES: TIME (SEC) PRESSURE (PSI)  
-----  
0.0 0.0

MAXIMUM SIMULATION TIME (SEC) 3.90  
TIME INCREMENT OF OUTPUT (SEC) 0.10

ROAD KEY = 0 : FLAT ROAD.

OUTPUT PAGE OPTION KEYS: 0 DELETES PAGES  
-----

POSITION	1	SPRUNG MASS VELOCITY	1	SPRUNG MASS ACCELERATION	1	TIRE FORCES	1	BRAKE SUMMARY	0	LATERAL PAGES	1	UNSPRUNG MASS PAGES	1
----------	---	----------------------	---	--------------------------	---	-------------	---	---------------	---	---------------	---	---------------------	---

TRUCK PARAMETERS

WHEELBASE - DISTANCE FROM FRONT AXLE TO CENTER OF REAR SUSPENSION (IN)	142.00
BASE VEHICLE CURB WEIGHT ON FRONT SUSPENSION (LB)	9073.80
BASE VEHICLE CURB WEIGHT ON REAR SUSPENSION (LB)	10519.20
SPRUNG MASS CG HEIGHT (IN, ABOVE GROUND)	47.90
SPRUNG MASS ROLL MOMENT OF INERTIA (IN-LB-SEC**2)	33852.00
SPRUNG MASS PITCH MOMENT OF INERTIA (IN-LB-SEC**2)	120000.00
SPRUNG MASS YAW MOMENT OF INERTIA (IN-LB-SEC**2)	120000.00
PAYLOAD WEIGHT (LB)	24907.00
PAYLOAD DISTANCE AHEAD OF REAR SUSPENSION CENTER(IN)	6.00
PAYLOAD CG HEIGHT (IN, ABOVE GROUND)	70.25
PAYLOAD ROLL MOMENT OF INERTIA(IN-LB-SEC**2)	7485.00
PAYLOAD PITCH MOMENT OF INERTIA(IN-LB-SEC**2)	50896.00
PAYLOAD YAW MOMENT OF INERTIA(IN-LB-SEC**2)	54422.00

TRUCK FRONT SUSPENSION AND AXLE PARAMETERS

SUSPENSION SPRING RATE (LB/IN/SIDE/AXLE)	1012.50	1012.50
SUSPENSION VISCOUS DAMPING (LB-SEC/IN/SIDE/AXLE)	15.00	15.00
COULOMB FRICTION (LB/SIDE/AXLE)	500.00	500.00

LEFT SIDE	RIGHT SIDE
-----	-----
1012.50	1012.50
15.00	15.00
500.00	500.00
-----	-----

AXLE ROLL MOMENT OF INERTIA (IN-LB-SEC**2)	5307.00
ROLL CENTER HEIGHT (IN, ABOVE GROUND)	24.55
ROLL STEER COEFFICIENT (DEG, STEER/DEG, ROLL)	0.0
AUXILIARY ROLL STIFFNESS (IN-LB/DEG/AXLE)	4000.00
LATERAL DISTANCE BETWEEN SUSPENSION SPRINGS (IN)	32.00
TRACK WIDTH (IN)	80.50
UNSPRUNG WEIGHT (LB)	1190.00

5307.00
24.55
0.0
4000.00
32.00
80.50
1190.00

TRUCK FRONT TIRES AND WHEELS

CORNERING STIFFNESS (LB/DEG/TIRE)	612.00	612.00
LONGITUDINAL STIFFNESS (LB/SLIP/TIRE)	40000.00	40000.00
CAMBER STIFFNESS (LB/DEG/TIRE)	0.0	0.0
ALIGNING MOMENT (IN-LB/DEG/TIRE)	1200.00	1200.00
TIRE SPRING RATE (LB/IN/TIRE)	5700.00	5700.00
TIRE LOADED RADIUS (IN)	20.30	20.30
POLAR MOMENT OF INERTIA (IN-LB-SEC**2/WHEEL)	244.60	244.60

LEFT SIDE	RIGHT SIDE
-----	-----
612.00	612.00
40000.00	40000.00
0.0	0.0
1200.00	1200.00
5700.00	5700.00
20.30	20.30
244.60	244.60

TRUCK REAR SUSPENSION AND AXLE PARAMETERS

	LEADING TANDEM AXLE		TRAILING TANDEM AXLE	
	LEFT SIDE	RIGHT SIDE	LEFT SIDE	RIGHT SIDE
SUSPENSION KEY - 0 INDICATES SINGLE AXLE, 1 INDICATES TANDEM AXLES				1
TANDEM AXLE SEPARATION (IN BETWEEN LEADING AND TRAILING AXLES)				50.00
STATIC LOAD TRANSFER (PERCENT LOAD ON LEAD AXLE)				50.00
DYNAMIC LOAD TRANSFER (PERCENT OF BRAKE TORQUE TRANSFERRED ONTO LEADING AXLE)				0.0
SUSPENSION SPRING RATE (LB/IN/SIDE/AXLE)	3000.00	3000.00	3000.00	3000.00
SUSPENSION VISCOUS DAMPING (LB-SEC/IN/SIDE/AXLE)	15.00	15.00	15.00	15.00
COULOMB FRICTION (LB/SIDE/AXLE)	100.00	100.00	100.00	100.00
AXLE ROLL MOMENT OF INERTIA (IN-LB-SEC**2)	11088.00			11088.00
ROLL CENTER HEIGHT (IN. ABOVE GROUND)	22.00			22.00
ROLL STEER COEFFICIENT (DEG. STEER/DEG. ROLL)	0.0			0.0
AUXILIARY ROLL STIFFNESS (IN-LB/DEG/AXLE)	0.0			70000.00
LATERAL DISTANCE BETWEEN SUSPENSION SPRINGS (IN)	35.00			35.00
TRACK WIDTH (IN)	72.00			72.00
UNSPRUNG WEIGHT (LB)	2340.00			2170.00

TRUCK REAR TIRES AND WHEELS

	LEADING TANDEM AXLE		TRAILING TANDEM AXLE	
	LEFT SIDE	RIGHT SIDE	LEFT SIDE	RIGHT SIDE
DUAL TIRE SEPARATION (IN)	13.00	13.00	13.00	13.00
CORNERING STIFFNESS (LB/DEG/TIRE)	565.00	565.00	565.00	565.00
LONGITUDINAL STIFFNESS (LB/SLIP/TIRE)	40000.00	40000.00	40000.00	40000.00
CAMBER STIFFNESS (LB/DEG/TIRE)	0.0	0.0	0.0	0.0
ALIGNING MOMENT (IN-LB/DEG/TIRE)	900.00	900.00	900.00	900.00
TIRE SPRING RATE (LB/IN/TIRE)	5700.00	5700.00	5700.00	5700.00
TIRE LOADED RADIUS (IN)	20.30	20.30	20.30	20.30
POLAR MOMENT OF INERTIA (IN-LB-SEC**2/WHEEL)	196.60	196.60	196.60	196.60

\*\*\* ZERO LINES IN TREADLE PRESSURE TABLE INDICATES NO BRAKING \*\*\*  
 \*\*\* THREE BRAKE PARAMETERS PER AXLE ARE DELETED AT THIS POINT \*\*\*

ANTILOCK KEY: 1 INDICATES ANTILOCK WILL BE USED

HSRI TRUCK AND TRACTOR-TRAILER DYNAMIC RESPONSE SIMULATION - T3DRS,V1  
 STRAIGHT TRUCK TEST FILE 30 FT/SEC 8 DEG STEP STEER.

SUMMARY PAGE

TRUCK	PAYLOAD = 24907.000 LBS	EMPTY	LOADED
DISTANCE FROM TRUCK	SPRUNG MASS CENTER TO REAR SUSPENSION (IN)	80.580	32.705
DISTANCE FROM TRUCK	SPRUNG MASS CENTER TO GROUND (IN)	47.900	62.247
ROLL MOMENT OF INERTIA OF TRUCK	SPRUNG MASS (IN-LB-SEC**2)	33852.000	52878.234
PITCH MOMENT OF INERTIA OF TRUCK	SPRUNG MASS (IN-LB-SEC**2)	120000.000	310949.438
YAW MOMENT OF INERTIA OF TRUCK	SPRUNG MASS (IN-LB-SEC**2)	120000.000	302934.375

THE STATIC LOADS ON THE AXLES ARE:

AXLE NUMBER	LOAD
NS(1,1,1)	10126.215
NS(1,2,1)	17186.891
NS(1,2,2)	17186.891
-----	
TOTAL	44499.996

THE TRUCK TOTAL MASS CENTER IS 109.687 INCHES BEHIND THE FRONT AXLE  
 THE TOTAL YAW MOMENT OF INERTIA IS 386314.313 IN-LB-SEC\*\*2

TIME (SEC)	FORWARD (FT)	LATERAL (FT)	VERTICAL (FT)	ROLL (DEG)	PITCH (DEG)	HEADING (DEG)	TURN RADIUS (FT)	SIDE SLIP (DEG)
0.0	0.0	0.0	0.0	0.0	0.0	0.0	*****	0.0
0.10	3.0743	0.0068	-0.0000	-0.3121	-0.0043	0.2251	279.0068	0.1345
0.20	6.0691	0.0382	-0.0000	-1.3414	-0.0286	1.2489	255.0396	-0.3333
0.30	9.0590	0.1050	0.0003	-2.5608	-0.0422	2.7127	159.2781	-0.9215
0.40	12.0426	0.2277	0.0012	-3.7494	-0.0354	4.3331	116.6549	-1.2599
0.50	15.0165	0.4262	0.0020	-4.6925	-0.0261	5.9992	95.6426	-1.2812
0.60	17.9763	0.7165	0.0017	-5.2365	-0.0291	7.6701	86.0439	-1.0438
0.70	20.9178	1.1083	0.0007	-5.3560	-0.0387	9.3356	83.5666	-0.6741
0.80	23.8377	1.6034	-0.0008	-5.1513	-0.0489	10.9953	85.5666	-0.3155
0.90	26.7335	2.1986	-0.0009	-4.7393	-0.0387	12.6517	90.3943	-0.0309
1.00	29.6040	2.8876	0.0002	-4.2842	-0.0216	14.3013	97.3436	0.1313
1.10	32.4478	3.6627	0.0009	-3.9060	-0.0159	15.9455	104.7338	0.1655
1.20	35.2643	4.5168	0.0005	-3.6669	-0.0241	17.5898	110.2085	0.0942
1.30	38.0533	5.4452	-0.0001	-3.5784	-0.0324	19.2386	112.2409	-0.0369
1.40	40.8134	6.4456	0.0000	-3.6221	-0.0315	20.8909	111.1061	-0.1788
1.50	43.5422	7.5176	0.0006	-3.7539	-0.0256	22.5429	108.0340	-0.2914
1.60	46.2368	8.6620	0.0011	-3.9166	-0.0230	24.1919	104.4773	-0.3530
1.70	48.8943	9.8799	0.0006	-4.0581	-0.0260	25.8374	101.4768	-0.3286
1.80	51.5115	11.1723	0.0010	-4.1457	-0.0303	27.4801	99.5214	-0.2111
1.90	54.0855	12.5391	0.0003	-4.1708	-0.0316	29.1200	98.7027	-0.2727
2.00	56.6139	13.9796	0.0003	-4.1431	-0.0296	30.7565	98.8731	-0.1579
2.10	59.0950	15.4919	0.0004	-4.0815	-0.0274	32.3892	99.7476	-0.1222
2.20	61.5274	17.0738	0.0004	-4.0063	-0.0269	34.0187	100.9610	-0.1068
2.30	63.9097	18.7229	0.0003	-3.9356	-0.0277	35.6460	102.1451	-0.1092
2.40	66.2408	20.4369	0.0003	-3.8823	-0.0282	37.2719	103.0144	-0.1226
2.50	68.5193	22.2135	0.0004	-3.8523	-0.0279	38.8964	103.4031	-0.1395
2.60	70.7440	24.0509	0.0004	-3.8444	-0.0271	40.5191	103.0576	-0.1534
2.70	72.9133	25.9473	0.0005	-3.8520	-0.0268	42.1400	102.5605	-0.1607
2.80	75.0256	27.9013	0.0005	-3.8664	-0.0272	43.7588	102.0676	-0.1602
2.90	77.0792	29.9107	0.0005	-3.8799	-0.0276	45.3755	101.6925	-0.1407
3.00	79.0723	31.9742	0.0004	-3.8870	-0.0277	46.9901	101.4900	-0.1268
3.10	81.0035	34.0896	0.0004	-3.8854	-0.0275	48.6022	101.4598	-0.1135
3.20	82.8710	36.2560	0.0004	-3.8753	-0.0273	50.2120	101.5624	-0.1026
3.30	84.6737	38.4712	0.0004	-3.8589	-0.0273	51.8195	101.7427	-0.0909
3.40	86.4108	40.7335	0.0004	-3.8393	-0.0273	53.4247	101.9312	-0.0902
3.50	88.0813	43.0407	0.0004	-3.8194	-0.0272	55.0278	102.0796	-0.0875
3.60	89.6841	45.3908	0.0004	-3.8017	-0.0270	56.6289	102.1637	-0.0857
3.70	91.2184	47.7814	0.0004	-3.7876	-0.0269	58.2275	102.1772	-0.0838
3.80	92.6832	50.2106	0.0004	-3.7769	-0.0269	59.8238	102.1361	
3.90	94.0777	52.6765	0.0004	-3.7690	-0.0269	61.4182		

TIME (SEC)	FORWARD (FT/SEC)	LATERAL (FT/SEC)	VERTICAL (FT/SEC)	ROLL (DEG/SEC)	PITCH (DEG/SEC)	HEADING (DEG/SEC)
0.0	30.00	0.0	0.0	0.0	0.0	0.0
0.10	29.98	0.07	-0.00	-7.71	-0.19	6.24
0.20	29.93	-0.17	-0.02	-11.67	-0.55	13.13
0.30	29.88	-0.48	-0.04	-12.39	-0.72	15.67
0.40	29.83	-0.66	-0.05	-10.98	-0.96	16.48
0.50	29.77	-0.67	-0.06	-7.59	-1.32	16.61
0.60	29.71	-0.54	-0.07	-3.21	-1.59	16.55
0.70	29.65	-0.35	-0.07	0.60	-1.66	16.46
0.80	29.59	-0.16	-0.05	3.40	-1.48	16.47
0.90	29.55	-0.02	-0.01	4.57	-1.19	16.44
1.00	29.51	0.07	0.01	4.32	-1.09	16.39
1.10	29.47	0.09	-0.00	3.14	-1.14	16.36
1.20	29.43	0.05	-0.02	1.63	-1.16	16.39
1.30	29.40	-0.02	-0.02	0.18	-1.07	16.45
1.40	29.36	-0.09	-0.02	-0.96	-0.99	16.47
1.50	29.32	-0.15	-0.02	-1.56	-1.02	16.45
1.60	29.27	-0.18	-0.02	-1.59	-1.13	16.40
1.70	29.23	-0.18	-0.03	-1.17	-1.20	16.36
1.80	29.18	-0.17	-0.03	-0.55	-1.21	16.33
1.90	29.14	-0.14	-0.03	0.05	-1.18	16.30
2.00	29.10	-0.11	-0.02	0.49	-1.15	16.27
2.10	29.05	-0.08	-0.02	0.72	-1.14	16.23
2.20	29.01	-0.06	-0.02	0.76	-1.14	16.21
2.30	28.97	-0.05	-0.02	0.64	-1.12	16.19
2.40	28.93	-0.06	-0.02	0.43	-1.10	16.18
2.50	28.89	-0.06	-0.02	0.19	-1.08	16.17
2.60	28.85	-0.07	-0.02	-0.01	-1.08	16.15
2.70	28.81	-0.08	-0.02	-0.12	-1.08	16.13
2.80	28.77	-0.08	-0.02	-0.14	-1.09	16.11
2.90	28.73	-0.08	-0.02	-0.10	-1.09	16.09
3.00	28.69	-0.08	-0.02	-0.08	-1.09	16.06
3.10	28.65	-0.07	-0.02	0.07	-1.08	16.04
3.20	28.61	-0.06	-0.02	0.14	-1.08	16.02
3.30	28.57	-0.06	-0.02	0.19	-1.08	16.00
3.40	28.53	-0.05	-0.02	0.21	-1.07	15.97
3.50	28.49	-0.05	-0.02	0.20	-1.06	15.95
3.60	28.45	-0.04	-0.02	0.17	-1.06	15.94
3.70	28.42	-0.04	-0.02	0.13	-1.05	15.92
3.80	28.38	-0.04	-0.02	0.10	-1.05	15.90
3.90	28.34	-0.04	-0.02	0.08	-1.04	15.88



TIME (SEC)	FORWARD (FT/SEC**2)	LATERAL (FT/SEC**2)	VERTICAL (FT/SEC**2)	ROLL (DEG/SEC**2)	PITCH (DEG/SEC**2)	HEADING (DEG/SEC**2)	LONGITUDINAL (FT/SEC**2)	LATERAL (FT/SEC**2)
0.0	0.0	0.0	0.0	0.0	0.0	0.0	-0.0	0.0
0.10	-0.6090	-0.0840	-0.0787	-105.8050	-5.3286	106.6932	-0.6166	3.1818
0.20	-0.4171	-3.3477	-0.1991	-17.8276	-2.1635	40.5839	-0.3770	3.50A2
0.30	-0.4788	-2.5385	-0.1566	1.8220	-1.7272	14.17A7	-0.3469	5.6242
0.40	-0.5632	-0.9160	-0.1403	24.6765	-3.1832	3.6591	-0.3737	7.6534
0.50	-0.6072	0.6681	-0.1369	40.7966	-3.6409	-0.2217	-0.4127	9.2906
0.60	-0.6021	1.6986	0.0286	44.4034	-1.3044	-0.6312	-0.4438	10.2740
0.70	-0.5536	2.0054	0.0352	31.4345	-0.3888	-0.8052	-0.4515	10.5254
0.80	-0.4848	1.7320	0.4039	21.4505	4.3661	-0.0195	-0.4367	10.2421
0.90	-0.4183	1.1734	0.3133	3.8798	2.1565	-0.6351	-0.4135	9.6535
1.00	-0.3766	0.4965	0.0648	-8.4139	-0.0290	-0.5585	-0.3960	8.9354
1.10	-0.3539	-0.1298	-0.1535	-14.5039	-0.6451	0.0232	-0.3782	8.2846
1.20	-0.3527	-0.5649	-0.1115	-15.3238	0.5058	0.5712	-0.3663	7.8570
1.30	-0.3665	-0.7405	0.0105	-13.4971	1.0608	0.4531	-0.3607	7.6909
1.40	-0.3878	-0.6785	0.0389	-8.9799	0.2647	-0.0343	-0.3612	7.7603
1.50	-0.4098	-0.4533	-0.0249	3.0839	-0.8140	-0.4072	-0.3667	7.9608
1.60	-0.4267	-0.1701	-0.0770	2.2985	-1.0496	-0.4531	-0.3747	8.2000
1.70	-0.4352	0.0791	-0.0549	5.6121	-0.4472	-0.3250	-0.3819	8.4243
1.80	-0.4347	0.2441	0.0104	6.4175	0.2124	-0.2626	-0.3863	8.5623
1.90	-0.4273	0.3147	0.0535	5.3489	0.3825	-0.3168	-0.3873	8.6059
2.00	-0.4167	0.3029	0.0484	3.4036	0.1824	-0.3612	-0.3858	8.5642
2.10	-0.4058	0.2316	0.0196	1.3239	0.0242	-0.3025	-0.3828	8.4635
2.20	-0.3970	0.1300	0.0008	-0.4942	0.0875	-0.1854	-0.3791	8.3376
2.30	-0.3911	0.0292	0.0005	-1.7946	0.2230	-0.1069	-0.3755	8.2180
2.40	-0.3885	-0.0455	0.0051	-2.3922	0.2318	-0.1101	-0.3726	8.1265
2.50	-0.3885	-0.0817	0.0024	-2.2540	0.0975	-0.1569	-0.3707	8.0720
2.60	-0.3901	-0.0810	-0.0057	-1.5733	-0.0444	-0.1950	-0.3700	8.0521
2.70	-0.3922	-0.0545	-0.0099	-0.6764	-0.0852	-0.2067	-0.3701	8.0568
2.80	-0.3937	-0.0159	-0.0062	0.1264	-0.0382	-0.2081	-0.3707	8.0735
2.90	-0.3940	0.0225	0.0009	0.6606	0.0189	-0.2163	-0.3711	8.0897
3.00	-0.3931	0.0521	0.0056	0.8902	0.0384	-0.2287	-0.3713	8.0966
3.10	-0.3911	0.0684	0.0062	0.8590	0.0343	-0.2334	-0.3710	8.0899
3.20	-0.3884	0.0708	0.0050	0.6430	0.0385	-0.2257	-0.3704	8.0694
3.30	-0.3855	0.0622	0.0044	0.3309	0.0584	-0.2100	-0.3694	8.0385
3.40	-0.3828	0.0470	0.0042	0.0132	0.0753	-0.1954	-0.3683	8.0021
3.50	-0.3806	0.0310	0.0042	-0.2329	0.0747	-0.1899	-0.3671	7.9654
3.60	-0.3788	0.0183	0.0028	-0.3572	0.0580	-0.1899	-0.3660	7.9321
3.70	-0.3775	0.0108	0.0013	-0.3607	0.0400	-0.1898	-0.3651	7.9041
3.80	-0.3765	0.0088	0.0004	-0.2788	0.0313	-0.1902	-0.3644	7.8817
3.90	-0.3756	0.0111	0.0006	-0.1561	0.0308	-0.1899	-0.3639	7.8639



MSRI TRUCK AND TRACTOR-TRAILER DYNAMIC RESPONSE SIMULATION - T3DRS,V1 OUTPUT PAGE NO. 1.05.1  
 STRAIGHT TRUCK TEST FILE 30 FT/SEC 8 DEG STEP STEER.  
 TRUCK REAR SUSPENSION TIRE FORCES  
 LEADING TANDEM AXLE

TIME (SEC)	LEFT SIDE				RIGHT SIDE					
	VERTICAL (LB)	LONG. (LB)	LATERAL (LB)	MU-X	MU-Y	VERTICAL (LB)	LONG. (LB)	LATERAL (LB)	MU-X	MU-Y
0.0	8593.45	-0.0	0.0	0.0	0.0	8593.45	-0.0	0.0	0.0	0.0
0.10	8143.41	-55.16	-915.37	-0.0068	-0.1124	9040.35	68.49	-1038.61	0.0076	-0.1149
0.20	8608.45	-21.46	-704.76	-0.0024	-0.0891	8352.36	30.07	-779.16	0.0036	-0.0933
0.30	9657.69	-5.08	-163.64	-0.0005	-0.0169	7510.63	13.01	-134.45	0.0017	-0.0179
0.40	10481.05	1.87	510.46	0.0002	0.0487	6745.59	6.67	348.14	0.0010	0.0516
0.50	11149.36	4.79	1120.01	0.0004	0.1005	6129.00	4.63	652.85	0.0008	0.1065
0.60	11518.35	5.46	1533.90	0.0005	0.1332	5722.21	4.65	807.95	0.0008	0.1412
0.70	11526.95	5.68	1623.25	0.0005	0.1408	5655.47	4.65	844.27	0.0008	0.1493
0.80	11343.26	4.87	1538.62	0.0004	0.1356	5777.20	5.30	830.81	0.0009	0.1438
0.90	11068.38	5.08	1285.85	0.0005	0.1162	6054.97	4.45	745.74	0.0007	0.1232
1.00	10798.98	4.87	990.16	0.0005	0.0917	6403.65	4.24	622.40	0.0007	0.0972
1.10	10562.97	4.34	741.17	0.0004	0.0702	6690.57	4.34	497.63	0.0006	0.0744
1.20	10391.94	3.86	598.41	0.0004	0.0576	6807.33	4.54	415.60	0.0007	0.0611
1.30	10329.58	3.85	550.62	0.0004	0.0533	6824.19	4.42	385.77	0.0006	0.0565
1.40	10378.98	4.14	570.52	0.0004	0.0550	6786.99	4.13	395.70	0.0006	0.0583
1.50	10492.08	4.43	634.99	0.0004	0.0605	6713.26	3.96	430.94	0.0006	0.0642
1.60	10608.74	4.56	720.68	0.0004	0.0679	6615.36	4.01	476.62	0.0006	0.0720
1.70	10691.84	4.57	802.53	0.0004	0.0751	6519.16	4.17	518.95	0.0006	0.0796
1.80	10733.33	4.58	858.34	0.0004	0.0800	6456.12	4.26	547.54	0.0007	0.0848
1.90	10739.59	4.62	876.50	0.0004	0.0816	6442.63	4.25	557.62	0.0007	0.0866
2.00	10718.12	4.63	859.65	0.0004	0.0802	6471.53	4.20	550.43	0.0006	0.0851
2.10	10675.95	4.57	820.54	0.0004	0.0769	6521.94	4.20	531.55	0.0006	0.0815
2.20	10623.45	4.46	774.02	0.0004	0.0729	6574.49	4.23	507.95	0.0006	0.0773
2.30	10574.13	4.37	731.29	0.0004	0.0692	6619.83	4.24	485.41	0.0006	0.0733
2.40	10539.10	4.33	698.72	0.0004	0.0663	6651.29	4.20	467.63	0.0006	0.0703
2.50	10522.19	4.34	678.79	0.0004	0.0645	6670.47	4.15	456.35	0.0006	0.0684
2.60	10520.09	4.35	671.06	0.0004	0.0638	6676.26	4.12	451.65	0.0006	0.0676
2.70	10526.21	4.36	672.65	0.0004	0.0639	6671.25	4.11	452.12	0.0006	0.0678
2.80	10534.82	4.37	679.04	0.0004	0.0645	6661.13	4.12	455.34	0.0006	0.0680
2.90	10541.83	4.38	685.16	0.0004	0.0650	6652.27	4.12	458.69	0.0006	0.0690
3.00	10544.80	4.39	688.19	0.0004	0.0653	6649.00	4.11	460.19	0.0006	0.0692
3.10	10542.18	4.39	685.77	0.0004	0.0651	6652.34	4.11	458.93	0.0006	0.0690
3.20	10533.23	4.38	678.44	0.0004	0.0644	6661.17	4.11	454.99	0.0006	0.0683
3.30	10521.28	4.36	667.50	0.0004	0.0634	6673.44	4.10	449.01	0.0006	0.0661
3.40	10506.66	4.33	654.69	0.0004	0.0623	6687.34	4.10	441.93	0.0006	0.0649
3.50	10492.54	4.32	641.71	0.0004	0.0612	6701.20	4.09	434.65	0.0006	0.0649
3.60	10480.41	4.31	629.85	0.0004	0.0601	6713.66	4.08	427.91	0.0006	0.0637
3.70	10470.77	4.30	619.90	0.0004	0.0592	6723.81	4.07	422.18	0.0006	0.0628
3.80	10463.30	4.29	612.02	0.0004	0.0585	6731.43	4.06	417.58	0.0006	0.0620
3.90	10457.46	4.28	605.81	0.0004	0.0579	6737.14	4.05	413.93	0.0006	0.0614

TIME (SEC)	LEFT SIDE				RIGHT SIDE					
	VERTICAL (LB)	LONG. (LB)	LATERAL (LB)	MU-X	MU-Y	VERTICAL (LB)	LONG. (LB)	LATERAL (LB)	MU-X	MU-Y
0.0	8593.45	-0.0	0.0	0.0	0.0	8593.45	-0.0	0.0	0.0	0.0
0.10	8959.23	-55.63	4.46	-0.0062	0.0005	8209.97	37.85	4.18	0.0083	0.0005
0.20	10921.88	-21.28	1596.29	-0.0019	0.1462	6118.62	30.11	936.36	0.0049	0.1530
0.30	12931.56	-4.97	3399.70	-0.0004	0.2629	4060.36	13.01	1127.76	0.0032	0.2777
0.40	14812.13	1.91	5083.36	0.0001	0.3432	2268.54	6.45	824.94	0.0028	0.3636
0.50	16271.43	4.80	6474.88	0.0003	0.3979	900.07	3.67	379.74	0.0041	0.4219
0.60	17017.88	5.46	7320.86	0.0003	0.4302	74.03	0.75	33.76	0.0101	0.4561
0.70	17156.33	5.68	7496.97	0.0003	0.4370	0.00	0.00	0.00	0.0232	0.4632
0.80	16662.51	4.90	7203.86	0.0003	0.4323	268.60	9.57	123.10	0.0356	0.4583
0.90	16175.23	5.09	6675.48	0.0003	0.4127	851.71	12.77	372.60	0.0150	0.4375
1.00	15600.29	4.87	6047.72	0.0003	0.3877	1554.41	5.49	638.70	0.0035	0.4109
1.10	15065.39	4.33	5515.62	0.0003	0.3661	2133.07	4.52	827.73	0.0021	0.3880
1.20	14663.53	3.86	5198.57	0.0003	0.3545	2424.73	4.57	911.31	0.0019	0.3758
1.30	14508.48	3.85	5100.30	0.0003	0.3515	2505.84	4.44	934.11	0.0018	0.3728
1.40	14600.29	4.14	5167.25	0.0003	0.3539	2440.26	4.13	915.94	0.0017	0.3753
1.50	14835.45	4.44	5332.43	0.0003	0.3594	2270.84	3.92	865.65	0.0017	0.3812
1.60	15085.42	4.56	5528.95	0.0003	0.3665	2044.64	3.93	794.70	0.0019	0.3887
1.70	15270.42	4.57	5702.10	0.0003	0.3734	1829.18	4.07	724.31	0.0022	0.3960
1.80	15371.09	4.58	5814.06	0.0003	0.3782	1689.80	4.21	677.77	0.0025	0.4011
1.90	15397.17	4.62	5847.77	0.0003	0.3798	1655.33	4.25	666.65	0.0026	0.4027
2.00	15360.75	4.63	5809.18	0.0003	0.3782	1709.45	4.24	685.50	0.0025	0.4010
2.10	15274.92	4.57	5722.73	0.0003	0.3746	1811.64	4.25	719.66	0.0023	0.3972
2.20	15162.48	4.46	5619.59	0.0003	0.3706	1923.92	4.27	756.05	0.0022	0.3930
2.30	15054.32	4.37	5525.96	0.0003	0.3671	2022.98	4.27	787.38	0.0021	0.3892
2.40	14976.16	4.33	5457.47	0.0003	0.3644	2097.25	4.23	810.40	0.0020	0.3864
2.50	14937.34	4.34	5418.89	0.0003	0.3628	2141.02	4.17	823.63	0.0019	0.3847
2.60	14931.12	4.35	5407.01	0.0003	0.3621	2154.00	4.12	827.17	0.0019	0.3840
2.70	14943.79	4.36	5413.86	0.0003	0.3623	2142.93	4.11	823.26	0.0019	0.3842
2.80	14963.01	4.37	5429.51	0.0003	0.3629	2120.43	4.11	815.93	0.0019	0.3848
2.90	14979.98	4.38	5444.32	0.0003	0.3634	2100.01	4.12	809.36	0.0020	0.3854
3.00	14988.86	4.39	5451.13	0.0003	0.3637	2090.70	4.11	806.30	0.0020	0.3857
3.10	14985.83	4.39	5446.53	0.0003	0.3634	2095.31	4.11	807.56	0.0020	0.3854
3.20	14970.28	4.38	5430.97	0.0003	0.3628	2112.08	4.11	812.54	0.0019	0.3847
3.30	14944.87	4.36	5407.01	0.0003	0.3618	2137.22	4.11	820.04	0.0019	0.3837
3.40	14914.78	4.33	5379.99	0.0003	0.3607	2166.56	4.11	828.75	0.0019	0.3825
3.50	14885.25	4.32	5352.73	0.0003	0.3596	2196.16	4.10	837.48	0.0019	0.3813
3.60	14859.67	4.31	5328.39	0.0003	0.3586	2222.67	4.09	845.19	0.0018	0.3803
3.70	14839.29	4.30	5308.34	0.0003	0.3577	2244.09	4.09	851.30	0.0018	0.3794
3.80	14823.72	4.29	5292.75	0.0003	0.3570	2260.05	4.06	855.74	0.0018	0.3786
3.90	14811.81	4.28	5280.64	0.0003	0.3565	2271.84	4.06	858.93	0.0018	0.3781

HSRI TRUCK AND TRACTOR-TRAILER DYNAMIC RESPONSE SIMULATION - T3DRS.V1      OUTPUT PAGE NO. 1.11.1  
 STRAIGHT TRUCK TEST FILE 30 FT/SEC 8 DEG STEP STEER,  
 TRUCK FRONT SUSPENSION - LATERAL TIRE FORCE AND MOMENT SUMMARY

LEFT SIDE				RIGHT SIDE				
TIME (SEC)	TIRE SIDESLIP ANGLE (DEG)	TIRE LATERAL FORCE (LB)	MU-Y	ALIGNING TORQUE (IN-LB)	TIRE SIDESLIP ANGLE (DEG)	TIRE LATERAL FORCE (LB)	MU-Y	ALIGNING TORQUE (IN-LB)
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.10	-5.1957	4409.3125	0.6280	-8645.6953	-5.1266	1943.1987	0.6197	-3810.1875
0.20	-3.2404	2550.9424	0.3917	-5001.8390	-2.9904	1350.8638	0.3615	-2648.7488
0.30	-3.0037	2400.4546	0.3631	-4706.7656	-2.6886	1181.9329	0.3250	-2317.5125
0.40	-3.2288	2674.4824	0.3903	-5244.0742	-2.9109	1140.0342	0.3518	-2313.7893
0.50	-3.5407	3036.3818	0.4280	-5953.6758	-3.2400	1215.6481	0.3916	-2384.0127
0.60	-3.7636	3302.3086	0.4549	-6475.1016	-3.4782	1251.3606	0.4204	-2453.6400
0.70	-3.8097	3358.2886	0.4605	-6584.8633	-3.5283	1270.3933	0.4265	-2490.9639
0.80	-3.7420	3268.0862	0.4523	-6408.0000	-3.4554	1277.5789	0.4177	-2505.0532
0.90	-3.5911	3067.8645	0.4341	-6015.4102	-3.2940	1263.0408	0.3983	-2476.5471
1.00	-3.4192	2858.6238	0.4133	-5605.1367	-3.1120	1238.8923	0.3762	-2429.1973
1.10	-3.2667	2690.6479	0.3949	-5275.7695	-2.9496	1213.3936	0.3565	-2379.2000
1.20	-3.1654	2586.6438	0.3826	-4985.2969	-2.8404	1193.0220	0.3433	-2339.2559
1.30	-3.1207	2542.5049	0.3772	-4871.8398	-2.7913	1179.3928	0.3374	-2312.5320
1.40	-3.1286	2552.2349	0.3782	-5004.3750	-2.7988	1174.7446	0.3383	-2303.4177
1.50	-3.1749	2603.9280	0.3838	-5105.7305	-2.8482	1179.7319	0.3443	-2313.1970
1.60	-3.2366	2674.8948	0.3912	-5244.8828	-2.9144	1190.7664	0.3523	-2334.8328
1.70	-3.2911	2738.7290	0.3978	-5370.0469	-2.9728	1202.1255	0.3593	-2357.1057
1.80	-3.3247	2777.1245	0.4019	-5445.3320	-3.0088	1209.5593	0.3637	-2371.6819
1.90	-3.3345	2785.8479	0.4031	-5462.4375	-3.0193	1212.0664	0.3650	-2376.5977
2.00	-3.3245	2771.3826	0.4018	-5434.0742	-3.0084	1210.9756	0.3637	-2374.4587
2.10	-3.3011	2743.3000	0.3990	-5379.0117	-2.9841	1207.8513	0.3607	-2368.3330
2.20	-3.2712	2709.8281	0.3954	-5313.3789	-2.9523	1203.4773	0.3569	-2359.7563
2.30	-3.2414	2677.6536	0.3919	-5250.2930	-2.9208	1198.3704	0.3530	-2349.7427
2.40	-3.2184	2652.0723	0.3890	-5200.1328	-2.8955	1193.3853	0.3500	-2339.9678
2.50	-3.2040	2636.4456	0.3873	-5169.4922	-2.8800	1189.6069	0.3481	-2332.5593
2.60	-3.1986	2630.9392	0.3866	-5158.6953	-2.8744	1187.6384	0.3474	-2328.6995
2.70	-3.1996	2632.7292	0.3868	-5162.2031	-2.8752	1187.2612	0.3475	-2327.9600
2.80	-3.2035	2637.6670	0.3872	-5171.8867	-2.8793	1187.7302	0.3480	-2328.8796
2.90	-3.2071	2642.0137	0.3877	-5180.4102	-2.8831	1188.2795	0.3485	-2329.9570
3.00	-3.2084	2643.5149	0.3878	-5183.3555	-2.8846	1188.4722	0.3487	-2330.3342
3.10	-3.2066	2641.3123	0.3876	-5179.0352	-2.8826	1188.1392	0.3484	-2329.6814
3.20	-3.2015	2635.5513	0.3870	-5167.7383	-2.8773	1187.2520	0.3478	-2327.9419
3.30	-3.1939	2627.0474	0.3861	-5151.0625	-2.8691	1185.8660	0.3468	-2325.2244
3.40	-3.1849	2617.1467	0.3850	-5131.6523	-2.8595	1184.1370	0.3456	-2321.8337
3.50	-3.1757	2607.0139	0.3839	-5111.7813	-2.8496	1182.2185	0.3444	-2318.0725
3.60	-3.1673	2597.8101	0.3828	-5093.7344	-2.8406	1180.3477	0.3434	-2314.4041
3.70	-3.1602	2590.1863	0.3820	-5078.7891	-2.8330	1178.7100	0.3424	-2311.1929
3.80	-3.1545	2584.1125	0.3813	-5066.8789	-2.8269	1177.3459	0.3417	-2308.5183
3.90	-3.1499	2579.2949	0.3807	-5057.4336	-2.8219	1176.2322	0.3411	-2306.3342

HSRI TRUCK AND TRACTOR-TRAILER DYNAMIC RESPONSE SIMULATION - T3DRS,V1 OUTPUT PAGE NO. 1.13.1  
 STRAIGHT TRUCK TEST FILE 30 FT/SEC 8 DEG STEP STEER.  
 TRUCK REAR SUSPENSION - LATERAL TIRE FORCE AND MOMENT SUMMARY  
 LEADING TANDEM AXLE

TIME (SEC)	LEFT SIDE				RIGHT SIDE			
	TIRE SIDESLIP ANGLE (DEG)	TIRE LATERAL FORCE (LB)	MU-Y	ALIGNING TORQUE (IN-LR)	TIRE SIDESLIP ANGLE (DEG)	TIRE LATERAL FORCE (LB)	MU-Y	ALIGNING TORQUE (IN-LR)
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.10	0.8548	-915.3735	-0.1124	1458.1157	0.8737	-1038.6055	-0.1149	1654.4143
0.20	0.6775	-784.7565	-0.0891	1250.0566	0.7094	-779.1567	-0.0933	1241.1331
0.30	0.1289	-163.6390	-0.0169	260.6636	0.1361	-134.4535	-0.0179	214.1735
0.40	-0.3704	510.4553	0.0487	-813.1138	-0.3925	348.1379	0.0516	-554.5554
0.50	-0.7639	1120.0051	0.1005	-1784.0771	-0.8100	652.8462	0.1065	-1039.9307
0.60	-1.0127	1533.9011	0.1332	-2443.3799	-1.0738	807.9539	0.1412	-1287.0046
0.70	-1.0709	1623.2510	0.1408	-2585.7070	-1.1353	844.2710	0.1493	-1344.8550
0.80	-1.0315	1538.6208	0.1356	-2450.8982	-1.0936	830.8066	0.1438	-1323.4072
0.90	-0.8835	1285.8496	0.1162	-2048.2539	-0.9366	745.7407	0.1232	-1187.9041
1.00	-0.6973	990.1602	0.0917	-1577.2449	-0.7391	622.3987	0.0972	-991.4299
1.10	-0.5336	741.1736	0.0702	-1180.6292	-0.5656	497.6313	0.0744	-792.6863
1.20	-0.4379	598.4077	0.0576	-953.2148	-0.4643	415.5991	0.0611	-662.0156
1.30	-0.4054	550.6174	0.0533	-877.0886	-0.4299	385.7703	0.0565	-614.5005
1.40	-0.4180	570.5200	0.0550	-908.7920	-0.4434	395.7009	0.0583	-630.3188
1.50	-0.4603	634.9941	0.0605	-1011.4937	-0.4882	430.9365	0.0642	-686.4465
1.60	-0.5166	720.6770	0.0679	-1147.9797	-0.5479	476.6208	0.0720	-759.2183
1.70	-0.5708	802.5295	0.0751	-1278.3640	-0.6054	518.9485	0.0796	-826.6483
1.80	-0.6082	858.3403	0.0800	-1367.2661	-0.6450	547.5391	0.0848	-872.1848
1.90	-0.6207	876.5022	0.0816	-1396.1968	-0.6582	557.6201	0.0866	-888.2432
2.00	-0.6099	859.6519	0.0802	-1369.3552	-0.6468	550.4314	0.0851	-876.7920
2.10	-0.5845	820.5439	0.0769	-1307.0596	-0.6198	531.5537	0.0815	-846.7214
2.20	-0.5541	774.0173	0.0729	-1232.9465	-0.5876	507.9478	0.0773	-809.1191
2.30	-0.5259	731.2852	0.0692	-1164.8774	-0.5577	485.4092	0.0733	-773.2170
2.40	-0.5042	698.7151	0.0663	-1112.9963	-0.5347	467.6321	0.0703	-744.8997
2.50	-0.4906	678.7871	0.0645	-1081.2527	-0.5203	456.3506	0.0684	-726.9290
2.60	-0.4851	671.0637	0.0638	-1068.9500	-0.5145	451.6472	0.0676	-719.4370
2.70	-0.4860	672.6533	0.0639	-1071.4819	-0.5154	452.1174	0.0678	-725.3271
2.80	-0.4902	679.0354	0.0645	-1081.6482	-0.5199	455.3450	0.0684	-730.6592
2.90	-0.4944	685.3923	0.0650	-1091.7744	-0.5244	458.6924	0.0690	-733.0404
3.00	-0.4963	688.1621	0.0653	-1096.1866	-0.5266	460.1897	0.0692	-731.0435
3.10	-0.4947	685.7698	0.0651	-1092.3752	-0.5246	458.9333	0.0690	-724.7556
3.20	-0.4998	678.4402	0.0644	-1080.6997	-0.5194	454.9861	0.0683	-715.2422
3.30	-0.4825	667.5000	0.0634	-1063.2729	-0.5117	449.0137	0.0673	-703.9548
3.40	-0.4739	654.6912	0.0623	-1022.8694	-0.5026	441.6200	0.0669	-692.3621
3.50	-0.4651	641.7987	0.0612	-1022.1895	-0.4933	434.6501	0.0664	-681.6243
3.60	-0.4570	629.8499	0.0601	-1003.2993	-0.4847	427.9092	0.0657	-672.4929
3.70	-0.4502	619.0989	0.0592	-987.4485	-0.4775	422.1768	0.0628	-665.1741
3.80	-0.4440	612.0171	0.0585	-974.8933	-0.4718	417.5820	0.0620	-659.3579
3.90	-0.4406	605.0098	0.0579	-965.0056	-0.4672	413.9309	0.0614	-659.3579

MSRI TRUCK AND TRAILER DYNAMIC RESPONSE SIMULATION - T3DRS.V1 OUTPUT PAGE NO. 1.14.1  
 STRAIGHT TRUCK TEST FILE 30 FT/SEC 8 DEG STEP STEER.  
 TRUCK REAR SUSPENSION - LATERAL TIRE FORCE AND MOMENT SUMMARY  
 TRAILING TANDEM AXLE

LEFT SIDE				RIGHT SIDE				
TIME (SEC)	TIRE SIDESLIP ANGLE (DEG)	TIRE LATERAL FORCE (LB)	MU-Y	ALIGNING TORQUE (IN-LB)	TIRE SIDESLIP ANGLE (DEG)	TIRE LATERAL FORCE (LB)	MU-Y	ALIGNING TORQUE (IN-LR)
0.00	0.00038	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.10	-1.1115	1596.2927	0.0005	-7.1079	-0.0039	4.1792	0.0005	-6.6571
0.20	-1.9993	3399.6960	0.1462	-2542.7646	-1.1638	936.3650	0.1530	-1491.5532
0.30	-2.6099	5083.3594	0.2629	-5415.4375	-2.1122	1127.7571	0.2777	-1796.4253
0.40	-3.0262	6474.8789	0.3432	-8097.3750	-2.7654	824.9417	0.3636	-1314.0647
0.50	-3.2715	7320.8555	0.3979	-10313.9531	-3.2085	379.7397	0.4219	-604.8940
0.60	-3.3232	7496.9727	0.4302	-11661.5273	-3.4682	33.7605	0.4561	-53.7778
0.70	-3.2879	7203.0633	0.4370	-11942.0625	-3.5224	0.0000	0.4632	-0.0000
0.80	-3.1385	6675.4766	0.4323	-11475.1641	-3.4054	123.1000	0.4583	-196.0897
0.90	-2.9481	6047.7188	0.4127	-10633.4883	-3.3269	372.6021	0.4375	-593.5242
1.00	-2.7842	5515.6172	0.3877	-9633.5195	-3.1248	638.7004	0.4109	-1017.3977
1.10	-2.6961	5198.5742	0.3661	-8785.9219	-2.9510	827.7312	0.3880	-1318.5083
1.20	-2.6734	5100.3008	0.3545	-8280.9023	-2.8582	911.3127	0.3758	-1451.6470
1.30	-2.6915	5167.2461	0.3515	-8124.3555	-2.8349	934.1138	0.3728	-1487.9670
1.40	-2.7335	5332.4297	0.3539	-8230.9961	-2.8544	915.9443	0.3753	-1459.0249
1.50	-2.7872	5528.9492	0.3594	-8494.1250	-2.8990	865.6521	0.3812	-1378.9133
1.60	-2.8397	5702.1016	0.3665	-8807.1602	-2.9558	794.6997	0.3887	-1265.8918
1.70	-2.8765	5814.0625	0.3734	-9082.9805	-3.0113	724.3059	0.3960	-1153.7603
1.80	-2.8883	5847.7656	0.3782	-9261.3281	-3.0627	677.7739	0.4011	-1079.6384
1.90	-2.8491	5722.7266	0.3798	-9315.0117	-3.0496	666.6519	0.4027	-1061.9219
2.00	-2.7915	5619.5938	0.3746	-9115.8398	-3.0210	719.6616	0.4010	-1091.9460
2.10	-2.7713	5457.4727	0.3706	-8951.5547	-2.9885	756.0549	0.3972	-1146.3625
2.20	-2.7588	5418.8906	0.3671	-8802.3906	-2.9599	787.3765	0.3930	-1204.3337
2.30	-2.7539	5407.0078	0.3644	-8693.3008	-2.9386	810.4038	0.3892	-1254.2266
2.40	-2.7551	5413.8594	0.3628	-8631.8477	-2.9255	823.6311	0.3864	-1290.9070
2.50	-2.7595	5429.5078	0.3623	-8612.9219	-2.9204	823.1660	0.3847	-1311.9771
2.60	-2.7639	5444.3203	0.3629	-8623.8320	-2.9216	823.2615	0.3840	-1317.6082
2.70	-2.7657	5451.1289	0.3634	-8648.7578	-2.9263	815.9285	0.3848	-1299.7078
2.80	-2.7639	5446.5313	0.3637	-8672.3555	-2.9310	809.3688	0.3854	-1289.2456
2.90	-2.7589	5430.9688	0.3634	-8683.1992	-2.9329	806.3032	0.3857	-1284.3752
3.00	-2.7432	5379.9922	0.3634	-8675.8750	-2.9310	807.5593	0.3854	-1286.3762
3.10	-2.7347	5352.7314	0.3628	-8651.0859	-2.9256	812.5354	0.3847	-1294.3025
3.20	-2.7269	5328.3867	0.3618	-8613.5977	-2.9179	820.0366	0.3837	-1306.2512
3.30	-2.7204	5308.3359	0.3607	-8569.8867	-2.9090	828.7478	0.3825	-1320.1277
3.40	-2.7153	5292.7461	0.3596	-8526.4609	-2.9000	837.4792	0.3813	-1334.0361
3.50	-2.7112	5280.6367	0.3586	-8487.6797	-2.8918	845.1914	0.3803	-1346.3210
3.60	-2.7078	5270.4336	0.3577	-8455.7383	-2.8849	851.3000	0.3800	-1356.0515
3.70	-2.7044	5261.9922	0.3570	-8430.9063	-2.8795	855.7424	0.3786	-1363.1279
3.80	-2.7012	5254.8567	0.3565	-8411.6250	-2.8752	858.9331	0.3781	-1368.2104









## APPENDIX B

### SAMPLE RUN OF A TRIPLES COMBINATION

The following pages are copies of the complete computer output package obtained from a two-second simulation of a triples combination in a braking-in-a-turn maneuver. The example illustrates use of optional spring tables, tire tables and brake torque tables. Antilock brake control systems are used on the tractor tandem rear axles, and cycling of the trailing axle can be observed on output page numbers 1.06.1, 1.10.1, and 1.14.1.

The first 20 pages are echo of the input data illustrating parameters for a triples combination; tables for suspensions, tires and brakes; an antilock system; and the vehicle summary page. These pages are normally reviewed to ensure that the desired vehicle and maneuver is being simulated.

The 60 remaining pages are the output indicating the response of each vehicle in the maneuver. In the process of exercising all options, however, the vehicle obtained is not representative and the performance indicated here should not be viewed as typical.



-----  
 SIMULATION OPERATION PARAMETERS  
 -----

VEHICLE CONFIGURATION (NUMBER OF TRAILERS - ENTER 0 FOR A STRAIGHT TRUCK) - 3  
 INITIAL VELOCITY (FT/SEC) 44.00  
 STEER TABLE (NUMBER OF LINES): POSITIVE - STEER ANGLE TABLE, NEGATIVE - PATH FOLLOWER TABLE  
 TABLE ENTRIES:                    TIME (SEC)   LEFT WHEEL (DEG)   RIGHT WHEEL (DEG)  
                                   0.0           0.0               0.0  
                                   1.00          2.00            2.00

TREADLE PRESSURE TABLE (NUMBER OF LINES)  
 TABLE ENTRIES:

TIME (SEC)	PRESSURE (PSI)
0.0	0.0
0.10	50.00
2.00	2.00
	0.05

MAXIMUM SIMULATION TIME (SEC)  
 TIME INCREMENT OF OUTPUT (SEC)

ROAD KEY = 0 : FLAT ROAD.

OUTPUT PAGE OPTION KEYS: 0 DELETES PAGES  
 -----

OPTION KEY	DESCRIPTION	PAGES
1	SPRUNG MASS POSITION	1
1	SPRUNG MASS VELOCITY	1
1	SPRUNG MASS ACCELERATION	1
1	TIRE FORCES	1
1	BRAKE SUMMARY	1
1	LATERAL PAGES	1
1	UNSPRUNG MASS PAGES	1



TRACTOR PARAMETERS

WFFELPASE - DISTANCE FROM FRONT AXLE TO CENTER OF REAR SUSPENSION (IN)  
 BASE VEHICLE CURB WEIGHT (IN FRONT SUSPENSION (LB))  
 BASE VEHICLE CURB WEIGHT (IN REAR SUSPENSION (LB))  
 SPRUNG MASS CG HEIGHT (IN, ABOVE GROUND)  
 SPRUNG MASS ROLL MOMENT OF INERTIA (IN-LB-SEC\*\*2)  
 SPRUNG MASS PITCH MOMENT OF INERTIA (IN-LB-SEC\*\*2)  
 SPRUNG MASS YAW MOMENT OF INERTIA (IN-LB-SEC\*\*2)  
 PAYLOAD WEIGHT (LB)

15C.0C  
 9437.00  
 7552.00  
 4C.13  
 36757.00  
 1C5453.00  
 241475.00  
 0.0

\*\*\* ZEPD ENTRY INDICATES NO PAYLOAD \*\*\*  
 \*\*\* FIVE PAYLOAD DESCRIPTION PARAMETERS ARE NOT ENTERED \*\*\*

FIFTH WHEEL LOCATION (IN, AHEAD OF REAR SUSP. CENTER)  
 FIFTH WHEEL HEIGHT ABOVE GROUND (IN)  
 5TH WHEEL STIFFNESS (IN-LB/DEG)

1.00  
 47.50  
 250000C.00

TRACTOR FRONT SUSPENSION AND AXLE PARAMETERS

SUSPENSION SPRING RATE (LB/IN/SIDE/AXLE)  
 SUSPENSION VISCOUS DAMPING (LB-SEC/IN/SIDE/AXLE)  
 CULCUMB FRICTION (LB/SIDE/AXLE)

LEFT SIDE      RIGHT SIDE  
 -----  
 1380.00      1500.00  
 50.00      50.00  
 670.00      670.00  
 -----

AXLE ROLL MOMENT OF INERTIA (IN-LB-SEC\*\*2)  
 ROLL CENTER HEIGHT (IN, ABOVE GROUND)  
 ROLL STEER COEFFICIENT (DEG. STEER/DEG. ROLL)  
 AUXILIARY ROLL STIFFNESS (IN-LB/DEG/AXLE)  
 LATERAL DISTANCE BETWEEN SUSPENSION SPRINGS (IN)  
 TRACK WIDTH (IN)  
 UNSPRUNG WEIGHT (LB)

5307.00  
 20.00  
 0.17  
 9900.00  
 36.00  
 79.50  
 1450.00

TRACTOR FRONT TIRES AND WHEELS

CORNERING STIFFNESS (LB/DEG/TIRE)  
 LONGITUDINAL STIFFNESS (LB/SLIP/TIRE)  
 CAMBER STIFFNESS (LB/DEG/TIRE)  
 ALIGNING MOMENT (IN-LB/DEG/TIRE)  
 TIRE SPRING RATE (LB/IN/TIRE)  
 TIRE LEADED RADIUS (IN)  
 FLAR MOMENT OF INERTIA (IN-LB-SEC\*\*2/WHEEL)

LEFT SIDE      RIGHT SIDE  
 -----  
 600.0C      600.00  
 21000.0C      21000.00  
 100.00      100.00  
 500.0C      500.00  
 4700.00      4700.00  
 20.0C      20.00  
 245.0C      245.00  
 -----

FSP1 TRUCK AND TRACTOR-TRAILER DYNAMIC RESPONSE SIMULATION - T3DRS.V1  
 SAMPLE RUN - TRIFLES BRAKING IN A TURN, ALL OPTICNS EXERCISED

TRACTOR REAR SUSPENSION AND AXLE PARAMETERS

LEADING TANDEM AXLE		TRAILING TANDEM AXLE	
LEFT SIDE	RIGHT SIDE	LEFT SIDE	RIGHT SIDE
3880.00	3880.00	3880.00	3880.00
50.00	50.00	50.00	50.00
1741.00	1741.00	1741.00	1741.00

SUSPENSION KEY - 0 INDICATES SINGLE AXLE, 1 INDICATES TANDEM AXLES  
 TANDEM AXLE SEPARATION (IN BETWEEN LEADING AND TRAILING AXLES) 1  
 48.00  
 50.00  
 10.00  
 STATIC LOAD TRANSFER (PERCENT LOAD ON LEAD AXLE)  
 DYNAMIC LOAD TRANSFER (PERCENT OF BRAKE TORQUE TRANSFERRED) (IN-LEADING AXLE)  
 3880.00 3880.00  
 50.00 50.00  
 1741.00 1741.00  
 SUSPENSION SPRING RATE (LB/IN/SIDE/AXLE)  
 SUSPENSION VISCOUS DAMPING (LB-SEC/IN/SIDE/AXLE)  
 CULCUMB FRICTION (LB/SIDE/AXLE)

AXLE ROLL MOMENT OF INERTIA (IN-LB-SEC\*\*2)  
 12230.00 12230.00  
 29.60 29.60  
 0.01 0.01  
 30000.00 30000.00  
 40.75 40.75  
 72.00 72.00  
 2450.00 2450.00  
 ROLL CENTER HEIGHT (IN. ABOVE GROUND)  
 ROLL STIFF COEFFICIENT (FEG. STIFF/DEG. ROLL)  
 AUXILIARY ROLL STIFFNESS (IN-LB/DEG/AXLE)  
 LATERAL DISTANCE BETWEEN SUSPENSION SPRINGS (IN)  
 TRACK WIDTH (IN)  
 UNSPRUNG WEIGHT (LB)

TRACTOR REAR TIRES AND WHEELS

LEADING TANDEM AXLE		TRAILING TANDEM AXLE	
LEFT SIDE	RIGHT SIDE	LEFT SIDE	RIGHT SIDE
12.80	12.80	12.80	12.80
-1.00	-1.00	-1.00	-1.00
-2.00	-2.00	-2.00	-2.00

DUAL TIRE SEPARATION (IN)  
 CORNERING STIFFNESS (LB/DEG/TIRE)  
 \*\*\* NEGATIVE ENTRY INDICATES TABLE ENTERED \*\*\*  
 \*\*\* ECHO WILL APPEAR ON TABLE INDEX PAGE \*\*\*  
 LENGTHWISE STIFFNESS (LB/SLIP/TIRE)  
 \*\*\* NEGATIVE ENTRY INDICATES TABLE ENTERED \*\*\*  
 \*\*\* ECHO WILL APPEAR ON TABLE INDEX PAGE \*\*\*  
 CAMBER STIFFNESS (LB/DEG/TIRE)  
 ALIGNING MOMENT (IN-LB/DEG/TIRE)  
 TIRE SPRING RATE (LB/IN/TIRE)  
 TIRE LOAD RADIUS (IN)  
 PCLAR MOMENT OF INERTIA (IN-LB-SEC\*\*2/WHEEL)

TRACTOR FRONT BRAKES

LEADING TANDEM AXLE		TRAILING TANDEM AXLE	
LEFT SIDE	RIGHT SIDE	LEFT SIDE	RIGHT SIDE
0.0200	0.0200	0.0200	0.0200
0.1700	0.1700	0.1700	0.1700
1000.0000	1000.0000	1200.0000	1200.0000

TIME LAG (SEC)  
 RISE TIME (SEC)  
 BRAKE TORQUE (IN-LB/PST/PRAKE)

TRACTOR REAR BRAKES

LEADING TANDEM AXLE		TRAILING TANDEM AXLE	
LEFT SIDE	RIGHT SIDE	LEFT SIDE	RIGHT SIDE
0.0500	0.0500	0.0500	0.0500
0.4000	0.4000	0.4000	0.4000
2000.0000	2000.0000	1500.0000	1500.0000

TIME LAG (SEC)  
 RISE TIME (SEC)  
 BRAKE TORQUE (IN-LB/PST/PRAKE)



HSRI TRUCK AND TRACTOR-TRAILER DYNAMIC RESPONSE SIMULATION - T3DRS.VI  
 SAMPLE RUN - TRIPLES BRAKING IN A TURN, ALL OPTICNS EXERCISED

TRAILER NO. 1 PARAMETERS

WHEELBASE - DISTANCE FROM KINGPIN TO CENTER OF REAR SUSPENSION (IN) 382.00  
 BASE VEHICLE KINGPIN STATIC LOAD (LB) 2815.00  
 REAR VEHICLE CURB WEIGHT ON REAR SUSPENSION (LB) 8650.00  
 SPRUNG MASS CG HEIGHT (IN, ABOVE GROUND) 74.80  
 UNSPRUNG MASS ROLL MOMENT OF INERTIA (IN-LB-SEC\*\*2) 66224.00  
 SPRUNG MASS PITCH MOMENT OF INERTIA (IN-LB-SEC\*\*2) 542466.00  
 UNSPRUNG MASS YAW MOMENT OF INERTIA (IN-LB-SEC\*\*2) 644482.00  
 PAYLOAD WEIGHT (LB) 46800.00  
 PAYLOAD CENTER OF GRAVITY (IN, ABOVE GROUND) 182.00  
 PAYLOAD CG HEIGHT (IN, ABOVE GROUND) 60.00  
 PAYLOAD ROLL MOMENT OF INERTIA (IN-LB-SEC\*\*2) 130000.00  
 PAYLOAD PITCH MOMENT OF INERTIA (IN-LB-SEC\*\*2) 240000.00  
 PAYLOAD YAW MOMENT OF INERTIA (IN-LB-SEC\*\*2) 240000.00  
 LOCATION OF PINTLE HOOK (IN, ABOVE GROUND) 48.00  
 HEIGHT OF PINTLE HOOK (IN, ABOVE GROUND) 40.00

TRAILER NO. 1 REAR SUSPENSION AND AXLE PARAMETERS

SUSPENSION KEY - 0 INDICATES SINGLE AXLE, 1 INDICATES TANDEM AXLES  
 TANDEM AXLE SEPARATION (IN BETWEEN LEADING AND TRAILING AXLES) 48.00  
 STATIC LOAD TRANSFER (PERCENT LOAD ON LEAD AXLE) 40.00  
 DYNAMIC LOAD TRANSFER (PERCENT OF BRAKE TORQUE TRANSFERRED ONTO LEADING AXLE) 10.00  
 SUSPENSION SPRING RATE (LB/IN/SIDE/AXLE) 7818.00 7818.00  
 SUSPENSION VISCOUS DAMPING (LB-SFC/IN/SIDE/AXLE) 50.00 50.00  
 COULOMB FRICTION (LB/SIDE/AXLE) 2600.00 2600.00  
 AXLE ROLL MOMENT OF INERTIA (IN-LB-SEC\*\*2) 4746.00 4746.00  
 ROLL CENTER HEIGHT (IN, ABOVE GROUND) 29.60 29.60  
 ROLL STEER COEFFICIENT (DEG. STEER/DEG. ROLL) -0.00 -0.00  
 AUXILIARY ROLL STIFFNESS (IN-LB/DEG/AXLE) 35490.00 35490.00  
 LATERAL DISTANCE BETWEEN SUSPENSION SPRINGS (IN) 38.00 38.00  
 TRACK WIDTH (IN) 71.25 71.25  
 UNSPRUNG WEIGHT (LB) 1530.00 1530.00

TRAILER NO. 1 REAR TIRFS AND WHEELS

DUAL TIRE SEPARATION (IN) 12.40 12.40  
 CORNERING STIFFNESS (LP/DLC/TIRF) 600.00 600.00  
 LONGITUDINAL STIFFNESS (LP/SLIP/TIRE) 21000.00 21000.00  
 CAMBER STIFFNESS (LB/DEG/TIRF) 0.00 0.00  
 ALIGNING MOMENT (IN-LP/FFC/TIRE) 0.00 0.00  
 TIRE SPRING RATE (LB/IN/TIRE) 4500.00 4500.00  
 TIRE LOADED RADIUS (IN) 20.20 20.20  
 PEARL MOMENT OF INERTIA (IN-LB-SEC\*\*2/WHEEL) 212.00 212.00

HSKI TRUCK AND TRACTOR-TRAILER DYNAMIC RESPONSE SIMULATION - TRSRS, VI  
SAMPLE RUN - TRIPLES BRAKING IN A TURN, ALL OPTICS EXERCISED

TRAILER NO. 1 REAR BRAKES

LEADING TANDEM AXLF		TRAILING TANDEM AXLF	
LEFT SIDE	RIGHT SIDE	LEFT SIDE	RIGHT SIDE
C.14CC	C.140C	C.1400	C.1400
0.17CC	0.170C	C.1700	C.1700
100C.00CC	100C.000C	1000.0000	100C.0000

TIME LAG (SEC)  
RISE TIME (SFC)  
BRAKE TCRGUL (IN-LB/PSI/BRAKE)

TRAILER NO. 2 PARAMETERS

DCLLY KEY: 1 = CONVERTER DCLLY, 2 = FIXED DCLLY  
 DISTANCE FROM TURNABLE CENTER TO PINTLE HOOK (IN)  
 TURNABLE LOCATION (IN AHEAD OF SUSP. CENTER)  
 TURNABLE HEIGHT ABOVE GROUND (IN)  
 WHEELBASE - DISTANCE FROM CENTER OF FRONT SUSP. TO CENTER OF REAR SUSP. (IN)  
 BASE VEHICLE CURB WEIGHT ON FRONT SUSPENSION (LB)  
 BASE VEHICLE CURB WEIGHT ON REAR SUSPENSION (LB)  
 SPRUNG MASS CG HEIGHT (IN. ABOVE GROUND)  
 SPRUNG MASS ROLL MOMENT OF INERTIA (IN-LB-SEC\*\*2)  
 SPRUNG MASS PITCH MOMENT OF INERTIA (IN-LB-SEC\*\*2)  
 SPRUNG MASS YAW MOMENT OF INERTIA (IN-LB-SEC\*\*2)  
 PAYLOAD WEIGHT (LB)

\*\*\* ZERO ENTRY INDICATES NO PAYLOAD \*\*\*  
 \*\*\* FIVE PAYLOAD DESCRIPTION PARAMETERS ARE NOT ENTERED \*\*\*  
 LOCATION OF PINTLE HOOK (IN BEHIND REAR SUSP. CENTER)  
 HEIGHT OF PINTLE HOOK (IN ABOVE GROUND)

TRAILER NO. 2 FRONT SUSPENSION AND AXLE PARAMETERS

SUSPENSION KEY - 0 INDICATES SINGLE AXLE, 1 INDICATES TANDEM AXLES  
 SUSPENSION SPRING RATE (LR/IN/SIDE/AXLE)  
 SUSPENSION VISCOUS DAMPING (LR-SEC/IN/SIDE/AXLE)  
 CULCUMB FRICTION (LR/SIDE/AXLE)  
 AXLE ROLL MOMENT OF INERTIA (IN-LB-SEC\*\*2)  
 ROLL CENTER HEIGHT (IN. ABOVE GROUND)  
 ROLL STEER COEFFICIENT (DEG. STEER/DEG. ROLL)  
 AUXILIARY ROLL STIFFNESS (IN-LB/DEG/AXLE)  
 LATERAL DISTANCE BETWEEN SUSPENSION SPRINGS (IN)  
 TRACK WIDTH (IN)  
 UNSPRUNG WEIGHT (LB)

LEFT SIDE	RIGHT SIDE
7818.00	7818.00
50.00	50.00
2600.00	2600.00
-----	
0	0
4746.00	4746.00
29.60	29.60
-0.00	-0.00
35490.00	35490.00
38.00	38.00
71.25	71.25
1530.00	1530.00

TRAILER NO. 2 FRONT TIRES AND WHEELS

DUAL TIRE SEPARATION (IN)  
 CORNERING STIFFNESS (LB/DEG/TIRE)  
 LONGITUDINAL STIFFNESS (LR/SLIP/TIRE)  
 CAMBER STIFFNESS (LR/DEG/TIRE)  
 ALIGNING MOMENT (IN-LB/DIG/TIRE)  
 TIRE SPRING RATE (LR/IN/TIRE)  
 TIRE LOADFC RADIUS (IN)  
 PCLAR MOMENT OF INERTIA (IN-LB-SEC\*\*2/WHEEL)

LEFT SIDE	RIGHT SIDE
12.40	12.40
600.00	600.00
21000.00	21000.00
0.0	0.0
0.0	0.0
4500.00	4500.00
20.20	20.20
212.00	212.00

TRAILER NO. 2 REAR SUSPENSION AND AXLE PARAMETERS

LEADING TANDEM AXLE		TRAILING TANDEM AXLE	
LEFT SIDE	RIGHT SIDE	LEFT SIDE	RIGHT SIDE

SUSPENSION KEY - 0 INDICATES SINGLE AXLE, 1 INDICATES TANDEM AXLES  
 TANDEM AXLE SEPARATION (IN BETWEEN LEADING AND TRAILING AXLES) 1  
 STATIC LOAD TRANSFER (PERCENT LOAD ON LEAD AXLE) 48.00  
 DYNAMIC LOAD TRANSFER (PERCENT OF BRAKE TORQUE TRANSFERRED ONTO LEADING AXLE) 50.00  
 SUSPENSION SPRING RATE (LB/IN/SIDE/AXLE) -3.00 -3.00 -3.00  
 \*\*\* NEGATIVE ENTRY INDICATES TABLE ENTERED \*\*\*  
 \*\*\* ECHO WILL APPEAR ON TABLE INDEX PAGE \*\*\*  
 SUSPENSION VISCOUS DAMPING (LB-SEC/IN/SIDE/AXLE) 50.00 50.00 50.00  
 CULOMB FRICTION (LB/SIDE/AXLE) 2600.00 2600.00 2600.00

AXLE ROLL MOMENT OF INERTIA (IN-LB-SEC\*\*2) 4746.00 4746.00  
 ROLL CENTER HEIGHT (IN. ABOVE GROUND) 25.60 29.60  
 ROLL STEER COEFFICIENT (DEG. STEER/DEG. ROLL) -0.00 -0.00  
 AUXILIARY ROLL STIFFNESS (IN-LF/DEG/AXLE) 35450.00 35490.00  
 LATERAL DISTANCE BETWEEN SUSPENSION SPRINGS (IN) 38.00 38.00  
 TRACK WIDTH (IN) 71.25 71.25  
 UNSPRUNG WEIGHT (LB) 1530.00 1530.00

TRAILER NO. 2 REAR TIRES AND WHEELS

LEADING TANDEM AXLE		TRAILING TANDEM AXLE	
LEFT SIDE	RIGHT SIDE	LEFT SIDE	RIGHT SIDE

DUAL TIRE SEPARATION (IN) 12.40 12.40 12.40  
 CCRNERING STIFFNESS (LB/DEG/TIRE) 600.00 600.00 600.00  
 LONGITUDINAL STIFFNESS (LB/SLIP/TIRE) 21000.00 21000.00 21000.00  
 CAMBER STIFFNESS (LB/DEG/TIRE) 0.0 0.0 0.0  
 ALIGNING MOMENT (IN-LB/DEG/TIRE) 0.0 0.0 0.0  
 TIRE SPRING RATE (LB/IN/TIRE) 4500.00 4500.00 4500.00  
 TIRE LOAD RADIUS (IN) 20.20 20.20 20.20  
 PCLAR MOMENT OF INERTIA (IN-LP-SEC\*\*2/WHEEL) 212.00 212.00 212.00

TRAILER NO. 2 FRONT BRAKES

LEADING TANDEM AXLE		TRAILING TANDEM AXLE	
LEFT SIDE	RIGHT SIDE	LEFT SIDE	RIGHT SIDE

TIME LAG (SEC) 0.1400 0.1400  
 RISE TIME (SEC) 0.1700 0.1700  
 BRAKE TORQUE (IN-LB/PST/BRAKE) -5.0000 -5.0000  
 \*\*\* NEGATIVE ENTRY INDICATES TABLE ENTERED \*\*\*  
 \*\*\* ECHO WILL APPEAR ON TABLE INDEX PAGE \*\*\*

TRAILER NO. 2 REAR BRAKES

LEADING TANDEM AXLE		TRAILING TANDEM AXLE	
LEFT SIDE	RIGHT SIDE	LEFT SIDE	RIGHT SIDE

TIME LAG (SEC) 0.1400 0.1400 C.1400  
 RISE TIME (SEC) 0.1700 0.1700 C.1700  
 BRAKE TORQUE (IN-LB/PST/BRAKE) 1000.0000 1000.0000 1000.0000

TRAILER NO. 2 PARAMETERS

DCLLY KEY: 1 = CONVERTER DCLLY, 2 = FIXED DCLLY  
 DISTANCE FROM TURNABLE CENTER TO FINITE P-CK (IN)  
 TURNABLE LOCATION (IN AHEAD OF SUSP. CENTER)  
 TURNABLE HEIGHT ABOVE GROUND (IN)  
 WHEELBASE - DISTANCE FROM CENTER OF FRONT SUSP. TO CENTER OF REAR SUSP. (IN)  
 BASE VEHICLE CURB WEIGHT ON FRONT SUSPENSION (LB)  
 BASE VEHICLE CURB WEIGHT ON REAR SUSPENSION (LB)  
 SPRUNG MASS CG HEIGHT (IN. ABOVE GROUND)  
 SPRUNG MASS ROLL MOMENT OF INERTIA (IN-LB-SEC\*\*2)  
 SPRUNG MASS PITCH MOMENT OF INERTIA (IN-LB-SEC\*\*2)  
 SPRUNG MASS YAW MOMENT OF INERTIA (IN-LB-SEC\*\*2)  
 PAYLOAD WEIGHT (LB)

\*\*\* ZERO ENTRY INDICATES NO PAYLOAD \*\*\*  
 \*\*\* FIVE PAYLOAD DESCRIPTION PARAMETERS ARE NOT ENTERED \*\*\*

TRAILER NO. 3 FRONT SUSPENSION AND AXLE PARAMETERS

SUSPENSION KEY - 0 INDICATES SINGLE AXLE, 1 INDICATES TANDEM AXLES

	LEADING TANDEM AXLE		TRAILING TANDEM AXLE	
	LEFT SIDE	RIGHT SIDE	LEFT SIDE	RIGHT SIDE
TANDEM AXLE SEPARATION (IN BETWEEN LEADING AND TRAILING AXLES)				
STATIC LOAD TRANSFER (PERCENT LOAD ON LEAD AXLE)	4P.00			
DYNAMIC LOAD TRANSFER (PERCENT OF BRAKE TORQUE TRANSFERRED INTO LEADING AXLE)	50.00			
SUSPENSION SPRING RATE (LB/IN/SIDE/AXLE)	7818.00	7818.00	7818.00	7818.00
SUSPENSION VISCOUS DAMPING (LB-SEC/IN/SIDE/AXLE)	50.00	50.00	50.00	50.00
CCULOMB FRICTION (LB/SIDE/AXLE)	2600.00	2600.00	2600.00	2600.00
AXLE ROLL MOMENT OF INERTIA (IN-LB-SEC**2)	4746.00		4746.00	
ROLL CENTER HEIGHT (IN. ABOVE GROUND)	25.60		29.60	
ROLL STIFFER COEFFICIENT (DEG. STEER/DEG. ROLL)	-0.00		-0.00	
AUXILIARY ROLL STIFFNESS (IN-LB/DEG/AXLE)	35450.00		35490.00	
LATERAL DISTANCE BETWEEN SUSPENSION SPRINGS (IN)	3P.00		38.00	
TRACK WIDTH (IN)	71.25		71.25	
UNSPRUNG WEIGHT (LB)	1530.00		1530.00	

TRAILER NO. 3 FRONT TIRES AND WHEELS

	LEADING TANDEM AXLE		TRAILING TANDEM AXLE	
	LEFT SIDE	RIGHT SIDE	LEFT SIDE	RIGHT SIDE
DUAL TIRE SEPARATION (IN)	12.40	12.40	12.40	12.40
CORNERING STIFFNESS (LB/DEG/TIRE)	600.00	600.00	600.00	600.00
LONGITUDINAL STIFFNESS (LP/SIIP/TIRE)	21000.00	21000.00	21000.00	21000.00
CAMBER STIFFNESS (LP/DEG/TIRE)	0.0	0.0	0.0	0.0
ALIGNING MOMENT (IN-LB/DEG/TIRE)	0.0	0.0	0.0	0.0
TIRE SPRING RATE (LB/IN/TIRE)	4500.00	4500.00	4500.00	4500.00
TIRE LOADED RADIUS (IN)	20.20	20.20	20.20	20.20
PCLAR MOMENT OF INERTIA (IN-LB-SEC**2/WHEEL)	212.00	212.00	212.00	212.00

TRAILER NO. 3 REAR SUSPENSION AND AXLE PARAMETERS

SUSPENSION KEY - 0 INDICATES SINGLE AXLE, 1 INDICATES TANDEM AXLES  
 TANDEM AXLE SEPARATION (IN BETWEEN LEADING AND TRAILING AXLES)  
 STATIC LOAD TRANSFER (PERCENT LOAD ON LEAF AXLE)  
 DYNAMIC LOAD TRANSFER (PERCENT OF BRAKE TORQUE TRANSFERRED (INTC LEADING AXLE)  
 SUSPENSION SPRING RATE (LB/IN/SIDE/AXLE)  
 SUSPENSION VISCOUS DAMPING (LB-SEC/IN/SIDE/AXLE)  
 C-CULOMB FRICTION (LB/SIDE/AXLE)  
 AXLE ROLL MOMENT OF INERTIA (IN-LP-SEC\*\*2)  
 ROLL CENTER HEIGHT (IN - ARCVE GROUND)  
 ROLL STEEF COEFFICIENT (DEG. STEER/DEG. ROLL)  
 AUXILIARY ROLL STIFFNESS (IN-LP/DEG/AXLE)  
 LATERAL DISTANCE BETWEEN SUSPENSION SPRINGS (IN)  
 TRACK WIDTH (IN)  
 UNSPRUNG WEIGHT (LB)

LEADING TANDEM AXLE		TRAILING TANDEM AXLE	
LEFT SIDE	RIGHT SIDE	LEFT SIDE	RIGHT SIDE
7818.00	7818.00	7818.00	7818.00
50.00	50.00	50.00	50.00
2600.00	2600.00	2600.00	2600.00
4746.00	4746.00	4746.00	4746.00
29.60	29.60	29.60	29.60
-0.00	-0.00	-0.00	-0.00
35450.00	35450.00	35490.00	35490.00
38.00	38.00	38.00	38.00
71.25	71.25	71.25	71.25
1530.00	1530.00	1530.00	1530.00

TRAILER NO. 3 REAR TIRES AND WHEELS

DUAL TIRE SEPARATION (IN)  
 CORNERING STIFFNESS (LB/DEG/TIRE)  
 LONGITUDINAL STIFFNESS (LB/SLIP/TIRE)  
 CAMBER STIFFNESS (LB/DEG/TIRE)  
 ALIGNING MOMENT (IN-LP/DEG/TIRE)  
 TIRE SPRING RATE (LB/IN/TIRE)  
 TIRE LOADED RADIUS (IN)  
 PCLAR MOMENT OF INERTIA (IN-LP-SEC\*\*2/WHEEL)

LEADING TANDEM AXLE		TRAILING TANDEM AXLE	
LEFT SIDE	RIGHT SIDE	LEFT SIDE	RIGHT SIDE
12.40	12.40	12.40	12.40
600.00	600.00	600.00	600.00
21000.00	21000.00	21000.00	21000.00
0.0	0.0	0.0	0.0
0.0	0.0	0.0	0.0
4500.00	4500.00	4500.00	4500.00
20.20	20.20	20.20	20.20
212.00	212.00	212.00	212.00

TRAILER NO. 3 FRONT BRAKES

TIME LAG (SEC)  
 RISE TIME (SEC)  
 BRAKE TORQUE (IN-LP/PSI/PRAKF)

LEADING TANDEM AXLE		TRAILING TANDEM AXLE	
LEFT SIDE	RIGHT SIDE	LEFT SIDE	RIGHT SIDE
0.1400	0.1400	0.1400	0.1400
0.1700	0.1700	0.1700	0.1700
1000.0000	1000.0000	1000.0000	1000.0000

TRAILER NO. 3 REAR BRAKES

TIME LAG (SEC)  
 RISE TIME (SEC)  
 BRAKE TORQUE (IN-LP/PSI/PRAKE)

LEADING TANDEM AXLE		TRAILING TANDEM AXLE	
LEFT SIDE	RIGHT SIDE	LEFT SIDE	RIGHT SIDE
0.1400	0.1400	0.1400	0.1400
0.1700	0.1700	0.1700	0.1700
1000.0000	1000.0000	1000.0000	1000.0000

ANTILOCK KEY: 1 INDICATES ANTILOCK WILL BE USED

HSPI TRUCK AND TRACTOR-TRAILER DYNAMIC RESPONSE SIMULATION - TDRS, VI  
 SAMPLE RUN - TRIPLES BRAKING IN A TURN, ALL OPTIONS EXERCISED

SPRING TABLES

-----  
 NG. OF LINES  
 -----

5

TABLE NO.

-----  
 -3  
 -----

DEFLECTION (IN)	FORCE (LB)
-5.00	-4000.00
0.0	0.0
0.50	3000.00
1.00	9000.00
4.00	32000.00

HSRT TRUCK AND TRACTOR-TRAILER DYNAMIC RESPONSE SIMULATION - T3DRS.V1  
 SAMPLE RUN - TRIPLES BRAKING IN A TURN, ALL OPTICS EXERCISED

---  
 MU-Y VS ALPHA TABLES  
 ---

TABLE AC.

- 1 -

NC. OF LEADS	NC. OF VELOCITIES	LEAD =
3	3	3000.00 LB
VELOCITY = 25.00 FT/SEC		
ALPHA (DEG)		
0.0	0.0	
5.00	0.50	
10.00	0.80	
VELOCITY = 25.00 FT/SEC		
ALPHA (DEG)		
0.0	0.0	
5.00	0.40	
10.00	0.70	
VELOCITY = 25.00 FT/SEC		
ALPHA (DEG)		
0.0	0.0	
5.00	0.30	
10.00	0.60	
VELOCITY = 50.00 FT/SEC		
ALPHA (DEG)		
0.0	0.0	
5.00	0.50	
10.00	0.80	
VELOCITY = 50.00 FT/SEC		
ALPHA (DEG)		
0.0	0.0	
5.00	0.40	
10.00	0.70	
VELOCITY = 50.00 FT/SEC		
ALPHA (DEG)		
0.0	0.0	
5.00	0.30	
10.00	0.60	



HSRI TRUCK AND TRACTOR-TRAILER DYNAMIC RESPONSE SIMULATION - TRDRS, VI  
 SAMPLE RUN - TRIPLES BRAKING IN A TURN, ALL OPTICNS EXERCISED

VELOCITY = 75.00 FT/SEC  
 ALPHA (DEG) -----  
 MC - Y

0.0  
 5.00  
 10.00

VELOCITY = 75.00 FT/SEC  
 ALPHA (DEG) -----  
 MC - Y

0.0  
 5.00  
 10.00

VELOCITY = 75.00 FT/SEC  
 ALPHA (DEG) -----  
 MC - Y

0.0  
 5.00  
 10.00

RCLL-CFF TABLE  
 -----

SLIP	ALPHA
0.0	1.00
0.0	0.35
20.00	0.35

FSRI TRUCK AND TRACTOR-TRAILER DYNAMIC RESPONSE SIMULATION - T30RS, VI  
 SAMPLE RUN - TRIPLES BRAKING IN A TURN, ALL OPTIONS EXERCISED

MC-X VS. SLIP TABLES

TABLE NC.

-2-

NC. OF LEADS      NC. OF VELOCITIES

VELOCITY = 30.00 FT/SEC      LCAD = 2000.00 LB  
 SLIP      MU - X

0.0      C.0  
 0.20      1.00  
 1.00      C.00

VELOCITY = 30.00 FT/SEC      LCAD = 5000.00 LB  
 SLIP      MU - X

0.0      0.0  
 0.20      C.00  
 1.00      0.40

VELOCITY = 30.00 FT/SEC      LCAD = 8000.00 LB  
 SLIP      MU - X

0.0      C.C  
 0.20      0.60  
 1.00      0.20

VELOCITY = 45.00 FT/SEC      LCAD = 2000.00 LB  
 SLIP      MU - X

0.0      0.0  
 0.20      C.50  
 1.00      0.50

VELOCITY = 45.00 FT/SEC      LCAD = 5000.00 LB  
 SLIP      MU - X

0.0      0.0  
 0.20      0.70  
 1.00      0.30

VELOCITY = 45.00 FT/SEC      LCAD = 8000.00 LB  
 SLIP      MU - X

0.0      0.0  
 0.20      0.50  
 1.00      0.10

HSRI TRUCK AND TRACTOR-TRAILER DYNAMIC RESPONSE SIMULATION - T3DRS.V1  
 SAMPLE RUN - TRIPLE BRAKING IN A TURN, ALL OPTIONS EXERCISED  
 2000.00 LP

VELOCITY = 60.00 FT/SEC  
 SLIP -----  
 0.0  
 0.20  
 1.00

VELOCITY = 60.00 FT/SEC  
 SLIP -----  
 0.0  
 0.20  
 1.00

VELOCITY = 60.00 FT/SEC  
 SLIP -----  
 0.0  
 0.20  
 1.00

PULL-OFF TABLE  
 -----

SLIP	0.0	0.20	0.40	0.50	1.00
ALPHA	1.00	1.00	1.00	1.00	1.00

FSR1 TRUCK AND TRACTOR-TRAILER DYNAMIC RESPONSE SIMULATION - T3DRS, VI  
 SAMPLE RUN - TRIPLES BRAKING IN A TURN, ALL OPTICS EXERCISED

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 PRESSURE VS TORQUE TABLES  
 -----

NO. OF LINES  
 -----

5

-----  
 TABLE NO  
 -----

-5

-----  
 TORQUE (IA-1P)  
 -----

-----  
 PRESSURE (PSI)  
 -----

0.0	0.0
10.00	0.0
20.00	20000.00
30.00	25000.00
100.00	150000.00

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**          D I C T I O N A R Y   O F   A N T I - L O C K   V A R I A B L E S / P A R A M E T E R S   A V A I L A B L E   T O   U S E R .
**
**
**  V A R I A B L E   I . D .      D E S C R I P T I O N      V A R I A B L E   I . D .      D E S C R I P T I O N
**  -----      -----      -----      -----
**
**  1 .....      I . 0 .....      45 .....      W M A X 1 .....
**  2 .....      T I M E .....      46 .....      W M A X 2 .....
**  3 .....      C M E G A .....      47 .....      T M A X 1 .....
**  4 .....      C M E G A C O T .....      48 .....      T M A X 2 .....
**  5 .....      X C C T .....      49 .....      W M I N .....
**  6 .....      X C C O T .....      50 .....      T M I N .....
**  7 .....      P C F F 1 .....      51 .....      T F M A X 2 .....
**  8 .....      P C F F 2 .....      52 .....      T F M I N 2 .....
**  9 .....      P C N 1 .....      53 .....      G P V 1 .....
** 10 .....      P C N 2 .....      54 .....      G P V 2 .....
** 11 .....      T C F F 1 .....      55 .....      G P V 3 .....
** 12 .....      T C N 1 .....      56 .....      G P V 4 .....
** 13 .....      X C C F F .....      57 .....      G P V 5 .....
** 14 .....      X D C N .....      58 .....      F C S 4 .....
** 15 .....      W C F F .....      59 .....      F C S 5 .....
** 16 .....      W C N .....      60 .....      O M E G C I F .....
** 17 .....      W C O F F .....
** 18 .....      W C G N .....
** 19 .....      W C M A X .....
** 20 .....      W C M I N .....
** 21 .....      T P M A X 1 .....
** 22 .....      T P M I N 1 .....
** 23 .....      W L O C K .....
** 24 .....      T L O C K .....
** 25 .....      S L C N .....
** 26 .....      S L O F F .....
** 27 .....      P M A X 1 .....
** 28 .....      P M A X 2 .....
** 29 .....      P M I N 1 .....
** 30 .....      P M I N 2 .....
** 31 .....      P C .....
** 32 .....      C N .....
** 33 .....      T M O D .....
** 34 .....      S L I P .....
** 35 .....      P .....
** 36 .....      C Y C N T .....
** 37 .....      S Q U A R E .....
** 38 .....      S Q U A R N .....
** 39 .....      T C F F 2 .....
** 40 .....      T C N 2 .....
** 41 .....      F C S 1 .....
** 42 .....      F C S 2 .....
** 43 .....      F C S 3 .....
** 44 .....      G P C N T .....
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*** UNIT 1 SUSPENSION 1 AXLE 1 LEFT SIDE WILL HAVE NO ANTI-LOCK SYSTEM
*** UNIT 1 SUSPENSION 1 AXLE 1 RIGHT SIDE WILL HAVE NO ANTI-LOCK SYSTEM

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\*\*\* ANTI-LOCK SUBROUTINE INPUT PARAMETER TABLE 6 --- UNIT 1 SUSPENSION 2 AXLF 1 LEFT 1 SIDE \*\*\*

SYMBOL	DESCRIPTION	INITIAL VALUE	FIRST ADAPTIVE VALUE	SECOND ADAPTIVE VALUE	UNIT 1	SUSPENSION 2	AXLF 1	LEFT 1	SIDE	FIRST BREAK-PT	SECOND BREAK-PT
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INEQUALITY EXPRESSION: 1

C(1)	COEFFICIENT(1)	-1.0000									
C(2)	COEFFICIENT(2)	-30.0000									

INEQUALITY EXPRESSION: 2

C(1)	COEFFICIENT(1)	0.5000									
C(2)	COEFFICIENT(2)	-1.0000									
C(3)	COEFFICIENT(3)	-20.0000									
C(4)	COEFFICIENT(4)	20.0000									

INEQUALITY EXPRESSION: 3

C(1)	COEFFICIENT(1)	1.0000									
C(2)	COEFFICIENT(2)	-0.1000									

INEQUALITY EXPRESSION: 5

C(1)	COEFFICIENT(1)	1.0000									
C(2)	COEFFICIENT(2)	-1.0000									
C(3)	COEFFICIENT(3)	12.0000									
C(4)	COEFFICIENT(4)	-12.0000									
C(5)	COEFFICIENT(5)	0.1000									

INEQUALITY EXPRESSION: 6

C(1)	COEFFICIENT(1)	1.0000									
C(2)	COEFFICIENT(2)	-1.0000									

EPSILON 1:

H(1)	COEFFICIENT(1)	1.0000									
H(2)	COEFFICIENT(2)	-1.0000									
H(3)	COEFFICIENT(3)	0.0									

EPSILON 2:

G(1)	COEFFICIENT(1)	0.0									
G(2)	COEFFICIENT(2)	-1.0000									

G(3)	COEFFICIENT(3)	1.0000		2	
G(4)	COEFFICIENT(4)	-1.0000		21	1

EPSILON 3:

R(1)	COEFFICIENT(1)	5.0000		1	
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EPSILON 4:

S(1)	COEFFICIENT(1)	0.0	1.0000	25	41	0.500
S(2)	COEFFICIENT(2)	-1.0000		27		
S(3)	COEFFICIENT(3)	1.0000		2		
S(4)	COEFFICIENT(4)	-1.0000		21	1	

CME-SHOT 1:

CS1(1)	COEFFICIENT(1)	1.0000		12	
CS1(2)	COEFFICIENT(2)	-1.0000		11	
CS1(3)	COEFFICIENT(3)	-0.1000		1	

CS1(1)	COEFFICIENT(1)	0.5000		1	
CS1(2)	COEFFICIENT(2)	-1.0000		32	

CEN. PUPP. VARIB. 3:

CPV(1)	COEFFICIENT(1)	0.6200		27	
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\*\* NON-ADAPTIVE ANTI-LOCK PARAMETERS. \*\*

TAU1	LOGIC TIME DELAY	0.0
TAU2	"	0.0
TAU3	"	0.0
TAU4	"	0.0
X1	EPSILON 1 BREAK-PT	0.0
X2	"	0.1000
X3	EPSILON 2 BREAK-PT	-5.0000
X4	"	2.0000
FFE1	EXP. PRESSURE FALL RATE	18.0000
FFE2	"	6.5000
FFE3	"	6.5000
PRE1	EXP. PRESSURE RISE RATE	11.5000
PRE2	"	11.5000
PRE3	"	0.0
X5	EPSILON 3 BREAK-PT	0.0
X6	"	50.0000
X7	EPSILON 4 BREAK-PT	-5.0000
X8	"	2.5000
FFL1	LIN. PRESSURE FALL RATE	0.0
FFL2	"	0.0
FFL3	"	0.0
FRL1	LIN. PRESSURE RISE RATE	0.0
FRL2	"	0.0
FRL3	"	15.0000
TAUON	PRESSURE-ON TIME DELAY	0.0000

TAUOFF	PRESSURE-OFF TIME DELAY	C.0200	
TAUW	TIME CONSTANT-WHEEL RATE	C.0100	
TAUWD	TIME CONSTANT-WHEEL ACCEL.	C.0100	
CP12	LOGICAL OPERATOR SWITCH	1	
CP23	"	C	
CP34	"	O	
CP56	LOGICAL OPERATOR SWITCH	1	
CP67	"	C	
CP78	"	C	
IGS1	CNE-SHOT TIME DURATION	2.0000	
ISAMPLE	ANTI-LOCK SAMPLING RATE	C.0200	
OPTICN	SIDE-TO-SIDE	1	
CMEGDIF	SIDE-TO-SIDE TOLERANCE	100.0000	
*** UNIT 1	SUSPENSION 2 AXLE 1 RIGHT SIDE	WILL HAVE THE SAME ANTI-LOCK SYSTEM AS	
UNIT 1	SUSPENSION 2 AXLE 1 LEFT SIDE		
*** UNIT 1	SUSPENSION 2 AXLE 2 LEFT SIDE	WILL HAVE THE SAME ANTI-LOCK SYSTEM AS	
UNIT 1	SUSPENSION 2 AXLE 1 LEFT SIDE		
*** UNIT 1	SUSPENSION 2 AXLE 1 LEFT SIDE	WILL HAVE NO ANTI-LOCK SYSTEM	
*** UNIT 2	SUSPENSION 2 AXLE 1 RIGHT SIDE	WILL HAVE NO ANTI-LOCK SYSTEM	
*** UNIT 2	SUSPENSION 2 AXLE 2 LEFT SIDE	WILL HAVE NO ANTI-LOCK SYSTEM	
*** UNIT 2	SUSPENSION 2 AXLE 2 LEFT SIDE	WILL HAVE NO ANTI-LOCK SYSTEM	
*** UNIT 2	SUSPENSION 2 AXLE 2 RIGHT SIDE	WILL HAVE NO ANTI-LOCK SYSTEM	
*** UNIT 3	SUSPENSION 1 AXLE 1 LEFT SIDE	WILL HAVE NO ANTI-LOCK SYSTEM	
*** UNIT 3	SUSPENSION 1 AXLE 1 RIGHT SIDE	WILL HAVE NO ANTI-LOCK SYSTEM	
*** UNIT 3	SUSPENSION 2 AXLE 1 LEFT SIDE	WILL HAVE NO ANTI-LOCK SYSTEM	
*** UNIT 3	SUSPENSION 2 AXLE 1 RIGHT SIDE	WILL HAVE NO ANTI-LOCK SYSTEM	
*** UNIT 3	SUSPENSION 2 AXLE 2 LEFT SIDE	WILL HAVE NO ANTI-LOCK SYSTEM	
*** UNIT 3	SUSPENSION 2 AXLE 2 RIGHT SIDE	WILL HAVE NO ANTI-LOCK SYSTEM	
*** UNIT 4	SUSPENSION 1 AXLE 1 LEFT SIDE	WILL HAVE NO ANTI-LOCK SYSTEM	
*** UNIT 4	SUSPENSION 1 AXLE 1 RIGHT SIDE	WILL HAVE NO ANTI-LOCK SYSTEM	
*** UNIT 4	SUSPENSION 1 AXLE 2 LEFT SIDE	WILL HAVE NO ANTI-LOCK SYSTEM	
*** UNIT 4	SUSPENSION 1 AXLE 2 RIGHT SIDE	WILL HAVE NO ANTI-LOCK SYSTEM	
*** UNIT 4	SUSPENSION 2 AXLE 1 LEFT SIDE	WILL HAVE NO ANTI-LOCK SYSTEM	
*** UNIT 4	SUSPENSION 2 AXLE 1 RIGHT SIDE	WILL HAVE NO ANTI-LOCK SYSTEM	
*** UNIT 4	SUSPENSION 2 AXLE 2 LEFT SIDE	WILL HAVE NO ANTI-LOCK SYSTEM	
*** UNIT 4	SUSPENSION 2 AXLE 2 RIGHT SIDE	WILL HAVE NO ANTI-LOCK SYSTEM	



F-35M TUCK AND TRACTR-TRAILER DYNAMIC RESPONSE SIMULATION - TPOPS.VI  
 SAMPLE RUN - TRIFLES BRAKING IN A TURN, ALL OPTICS EXERCISED

TRAILER NO. 3	PAYLOAD =	C.0	LBS.	EMPTY	LOADED
DISTANCE FROM TRAILER SPRUNG MASS CENTER TO REAR SUSPENSION (IN)				150.000	150.000
DISTANCE FROM TRAILER SPRUNG MASS CENTER TO GROUND (IN)				74.800	74.800
ROLL MOMENT OF INERTIA OF TRAILER SPRUNG MASS (IN-LB-SEC**2)				66223.938	66223.938
PITCH MOMENT OF INERTIA OF TRAILER SPRUNG MASS (IN-LB-SEC**2)				542485.938	542485.938
YAW MOMENT OF INERTIA OF TRAILER SPRUNG MASS (IN-LB-SEC**2)				644482.938	644482.938
TRAILER NO. 2	PAYLOAD =	C.0	LBS.	EMPTY	LOADED
DISTANCE FROM TRAILER SPRUNG MASS CENTER TO REAR SUSPENSION (IN)				168.057	168.057
DISTANCE FROM TRAILER SPRUNG MASS CENTER TO GROUND (IN)				74.800	74.800
ROLL MOMENT OF INERTIA OF TRAILER SPRUNG MASS (IN-LB-SEC**2)				66223.938	66223.938
PITCH MOMENT OF INERTIA OF TRAILER SPRUNG MASS (IN-LB-SEC**2)				542485.938	542485.938
YAW MOMENT OF INERTIA OF TRAILER SPRUNG MASS (IN-LB-SEC**2)				644482.938	644482.938
TRAILER NO. 1	PAYLOAD =	46800.000	LBS.	EMPTY	LOADED
DISTANCE FROM TRAILER SPRUNG MASS CENTER TO REAR SUSPENSION (IN)				125.082	174.182
DISTANCE FROM TRAILER SPRUNG MASS CENTER TO GROUND (IN)				74.800	62.253
ROLL MOMENT OF INERTIA OF TRAILER SPRUNG MASS (IN-LB-SEC**2)				66223.938	83267.250
PITCH MOMENT OF INERTIA OF TRAILER SPRUNG MASS (IN-LB-SEC**2)				542485.938	648450.250
YAW MOMENT OF INERTIA OF TRAILER SPRUNG MASS (IN-LB-SEC**2)				644482.938	546404.000
TRACTOR	PAYLOAD =	0.0	LBS.	EMPTY	LOADED
DISTANCE FROM TRACTOR SPRUNG MASS CENTER TO REAR SUSPENSION (IN)				108.519	108.519
DISTANCE FROM TRACTOR SPRUNG MASS CENTER TO GROUND (IN)				40.130	40.130
ROLL MOMENT OF INERTIA OF TRACTOR SPRUNG MASS (IN-LB-SEC**2)				36756.996	36756.996
PITCH MOMENT OF INERTIA OF TRACTOR SPRUNG MASS (IN-LB-SEC**2)				105492.938	105492.938
YAW MOMENT OF INERTIA OF TRACTOR SPRUNG MASS (IN-LB-SEC**2)				241479.000	241479.000

THE STATIC LOADS ON THE AXLES ARE:

AXLE NUMBER	LOAD
NS(1,1,1)	9604.379
NS(1,2,1)	16445.969
NS(1,2,2)	16445.969
NS(2,1,1)	13263.469
NS(2,2,2)	19855.203
NS(3,1,1)	8650.000
NS(3,2,1)	4325.000
NS(3,2,2)	4325.000
NS(4,1,1)	4325.000
NS(4,1,2)	4325.000
NS(4,2,1)	4325.000
NS(4,2,2)	4325.000
TOTAL	110254.938

THE TRACTOR TOTAL MASS CENTER IS 68.690 INCHES BEHIND THE FRONT AXLE  
 THE TOTAL YAW MOMENT OF INERTIA IS 401281.875 IN-LB-SEC\*\*2

THE FIRST TRAILER TOTAL MASS CENTER IS 217.966 INCHES BEHIND THE KINGPIN  
 THE TOTAL YAW MOMENT OF INERTIA IS 1168344.000 IN-LB-SEC\*\*2

THE SECOND TRAILER TOTAL MASS CENTER IS 150.000 INCHES BEHIND THE TURNABLE CENTER  
 THE TOTAL YAW MOMENT OF INERTIA IS 541574.000 IN-LB-SEC\*\*2

THE THIRD TRAILER TOTAL MASS CENTER IS 150.000 INCHES BEHIND THE TURNABLE CENTER  
 THE TOTAL YAW MOMENT OF INERTIA IS 1046017.500 IN-LB-SEC\*\*2

TIME (SEC)	FORWARD (FT)	LATERAL (FT)	VERTICAL (FT)	PCLL (DEG)	PITCH (DEG)	HEADING (DEG)	TURN RADIS (FT)	SIDE SLIP (DEG)
0.0	0.0	0.0	0.0	0.0	0.0	0.0	*****	0.0
0.05	2.3100	C.C001	C.0000	-0.0010	-0.0002	0.0005	8696.0586	0.0072
0.10	4.5052	C.0008	C.0004	-0.0042	-0.0077	0.0043	4445.2305	0.0251
0.15	6.7044	C.0025	C.0020	-0.0087	-0.0420	0.0143	2581.2686	C.0505
0.20	8.8903	C.0058	C.0107	-0.0162	-0.0199	0.0334	2213.1108	C.0807
0.25	11.0641	C.0113	C.0251	-0.0250	-0.02356	0.0641	1740.3245	0.1139
0.30	13.2265	C.0154	C.0443	-0.0363	-0.03852	0.1087	1427.2600	0.1484
0.35	15.3777	C.0306	C.0642	-0.0505	-0.0552	0.1690	1198.1235	0.1827
0.40	17.5141	C.0456	C.0815	-0.0675	-0.07152	0.2466	1028.3337	0.2158
0.45	19.6283	C.0647	C.0920	-0.0877	-0.08257	0.3425	855.4089	0.2462
0.50	21.7110	C.0884	C.0973	-0.1095	-0.09001	0.4569	757.4507	0.2729
0.55	23.7544	C.1169	C.0555	-0.1327	-0.05288	0.5859	712.7769	0.2953
0.60	25.7530	C.1503	C.0504	-0.1563	-0.09288	0.7409	638.4070	0.3139
0.65	27.7046	C.1885	C.0852	-0.1801	-0.09170	0.9056	570.6362	C.3305
0.70	29.6093	C.2330	C.0827	-0.2043	-0.09105	1.0955	508.8486	C.3472
0.75	31.4689	C.2830	C.0828	-0.2292	-0.09205	1.2986	452.9731	C.3661
0.80	33.2853	C.3391	C.0882	-0.2556	-0.09477	1.5191	406.0881	C.3886
0.85	35.0603	C.4018	C.0950	-0.2834	-0.09852	1.7570	365.8088	0.4154
0.90	36.7948	C.4714	C.1022	-0.3122	-1.0242	2.0123	332.4077	0.4460
0.95	38.4884	C.5481	C.1081	-0.3413	-1.0580	2.2844	304.8418	C.4796
1.00	40.1402	C.6315	C.1116	-0.3695	-1.0821	2.5727	281.3193	C.5154
1.05	41.7486	C.7227	C.1131	-0.3944	-1.0945	2.8753	280.4375	C.5406
1.10	43.3118	C.8158	C.1122	-0.4138	-1.0973	3.1876	274.6852	C.5511
1.15	44.8280	C.9226	C.1103	-0.4282	-1.0920	3.5057	264.4082	0.5558
1.20	46.2962	C.1035	C.1081	-0.4356	-1.0872	3.8262	252.9919	0.5617
1.25	47.7162	C.1425	C.1065	-0.4388	-1.0941	4.1468	242.5656	C.5707
1.30	49.0882	C.1856	C.1055	-0.4377	-1.0855	4.4652	234.6504	C.5834
1.35	50.4134	C.2300	C.1025	-0.4333	-1.0915	4.7751	228.4512	C.5992
1.40	51.6929	C.2780	C.1001	-0.4268	-1.1005	5.0869	222.7903	0.6181
1.45	52.9275	C.3301	C.1100	-0.4179	-1.1106	5.3872	218.1857	C.6408
1.50	54.1178	C.3848	C.1115	-0.4067	-1.1191	5.6789	215.0329	C.6663
1.55	55.2637	C.4400	C.1122	-0.3925	-1.1239	5.9607	212.9410	0.6937
1.60	56.3652	C.5021	C.1126	-0.3747	-1.1221	6.2318	194.5854	C.7266
1.65	57.4236	C.5682	C.1120	-0.3536	-1.0929	6.4982	148.5358	0.8228
1.70	58.4404	C.6380	C.1022	-0.3278	-1.0414	6.7630	193.5673	C.9293
1.75	59.4152	C.7108	C.0988	-0.2986	-0.9960	7.0055	205.3100	0.9584
1.80	60.3387	C.7848	C.0526	-0.2773	-0.9687	7.2289	202.2103	C.9955
1.85	61.2080	C.8583	C.0930	-0.2557	-0.9705	7.4342	195.7654	1.0436
1.90	62.0265	C.9320	C.0565	-0.2206	-1.0042	7.6248	207.1635	1.0906
1.95	62.7991	C.1001	C.1041	-0.1813	-1.0594	7.8047	212.0431	1.1211

SAMPLE RUN - TRIPLES BRAKING IN A TURN, ALL OPTICAS EXERCISED  
TRACTOR SPRUNG MASS VELOCITY (BODY AXES)

TIME (SEC)	FORWARD (FT/SEC)	LATERAL (FT/SEC)	VERTICAL (FT/SEC)	ROLL (DEG/SEC)	PITCH (DEG/SEC)	HEADING (DEG/SEC)
0.0	44.00	0.0	0.0	0.0	0.0	0.0
0.05	44.00	0.01	0.00	-0.05	-0.03	0.03
0.10	43.57	0.02	0.01	-0.07	-0.34	0.13
0.15	43.83	0.04	0.06	-0.12	-1.09	0.28
0.20	43.00	0.06	0.13	-0.17	-1.97	0.45
0.25	43.26	0.09	0.18	-0.19	-2.66	0.75
0.30	43.14	0.11	0.12	-0.25	-3.33	1.04
0.35	42.50	0.14	-0.03	-0.30	-3.45	1.37
0.40	42.54	0.16	-0.23	-0.35	-2.72	1.73
0.45	42.00	0.19	-0.45	-0.39	-1.86	2.10
0.50	41.25	0.20	-0.63	-0.41	-0.97	2.47
0.55	40.43	0.21	-0.73	-0.43	-0.24	2.84
0.60	39.51	0.22	-0.75	-0.42	0.17	3.20
0.65	38.57	0.22	-0.70	-0.42	0.22	3.55
0.70	37.65	0.23	-0.61	-0.43	-0.03	3.89
0.75	36.78	0.24	-0.53	-0.44	-0.40	4.23
0.80	35.95	0.24	-0.47	-0.47	-0.70	4.58
0.85	35.14	0.25	-0.46	-0.48	-0.82	4.93
0.90	34.33	0.27	-0.48	-0.49	-0.77	5.27
0.95	33.51	0.29	-0.52	-0.47	-0.62	5.60
1.00	32.67	0.29	-0.57	-0.44	-0.41	5.92
1.05	31.79	0.30	-0.60	-0.32	-0.19	6.16
1.10	30.88	0.30	-0.62	-0.23	-0.01	6.32
1.15	29.93	0.29	-0.61	-0.09	0.07	6.40
1.20	28.98	0.28	-0.59	0.02	0.05	6.42
1.25	28.02	0.28	-0.55	0.09	-0.03	6.40
1.30	27.05	0.28	-0.51	0.18	-0.13	6.33
1.35	26.17	0.27	-0.47	0.23	-0.20	6.22
1.40	25.28	0.27	-0.45	0.27	-0.25	6.08
1.45	24.40	0.27	-0.43	0.32	-0.24	5.92
1.50	23.52	0.27	-0.42	0.36	-0.18	5.74
1.55	22.64	0.27	-0.42	0.43	-0.09	5.53
1.60	21.76	0.28	-0.43	0.50	0.23	5.34
1.65	20.93	0.30	-0.47	0.56	0.85	5.36
1.70	20.14	0.33	-0.51	0.67	1.01	5.09
1.75	19.20	0.32	-0.47	0.62	0.73	4.66
1.80	18.12	0.31	-0.37	0.42	0.27	4.29
1.85	17.06	0.31	-0.25	0.65	-0.39	3.95
1.90	16.10	0.31	-0.16	0.83	-0.54	3.70
1.95	15.22	0.30	-0.12	0.89	-1.25	3.51

TIME (SEC)	FORWARD (FT/SEC**2)	LATRAL (FT/SEC**2)	VERTICAL (FT/SEC**2)	ROLL (DEG/SEC**2)	PITCH (DEG/SEC**2)	HEADING (DEG/SEC**2)	LONGITUDINAL (FT/SEC**2)	LATERAL (FT/SEC**2)
0.0	0.0	0.0	0.0	0.0	0.0	0.0	-0.0	0.0
0.05	-0.1623	0.2026	0.0682	-1.0966	-2.2435	1.2780	-0.1423	0.2274
0.10	-1.4993	0.2413	0.5861	-0.2851	-10.0560	2.5144	-1.4994	0.4387
0.15	-3.8306	0.4265	1.3205	-1.5213	-17.8964	3.6803	-3.8410	0.6444
0.20	-4.5166	0.4812	1.2775	-0.2377	-16.3858	4.6457	-4.9217	0.8549
0.25	-4.5039	0.5087	0.1118	-1.0788	-12.3982	5.5252	-4.5131	1.0731
0.30	-4.3165	0.5085	-2.2746	-1.0482	-12.0466	6.2876	-4.3256	1.2931
0.35	-5.7172	0.4878	-3.5738	-0.5058	8.6745	6.9237	-5.7187	1.5150
0.40	-8.9593	0.4364	-4.3060	-1.1210	17.0752	7.2919	-8.8493	1.7191
0.45	-12.6052	0.3581	-4.2147	-0.3630	17.6075	7.4235	-12.5973	1.8943
0.50	-15.8619	0.2658	-2.9611	-0.2415	17.1385	7.3871	-15.8598	2.0435
0.55	-17.5769	0.1782	-1.2414	0.1204	11.4885	7.1864	-17.9841	2.1780
0.60	-18.8105	0.1150	0.4400	0.3304	4.7312	6.9622	-18.8248	2.3157
0.65	-18.6327	0.0877	1.5202	0.1352	-2.4175	6.7769	-18.6492	2.4709
0.70	-17.9032	0.0950	1.8002	0.1347	-7.0344	6.6567	-17.9184	2.6465
0.75	-16.5811	0.1228	1.4580	-0.0830	-7.2414	6.7518	-16.9947	2.8371
0.80	-16.3649	0.1550	0.7495	-0.0549	-4.2392	6.7477	-16.3786	3.0320
0.85	-16.6698	0.2130	-0.0355	0.2273	-0.6288	6.7472	-16.0852	3.2137
0.90	-16.1621	0.2130	-0.6610	0.5907	2.1528	6.5482	-16.1802	3.3684
0.95	-16.5635	0.2135	-0.9680	1.1239	3.8259	6.1855	-16.5853	3.4876
1.00	-17.1750	0.2061	-0.9057	1.6324	4.5348	5.7353	-17.2013	3.5755
1.05	-17.5189	-0.0555	-0.5676	2.2994	4.2280	3.5931	-17.9492	3.3611
1.10	-18.5762	-0.1854	-0.1061	2.4755	2.6362	1.9140	-16.6088	3.2161
1.15	-18.5991	-0.2124	0.3324	4.0703	0.5611	0.5901	-15.0322	3.1284
1.20	-19.1417	-0.1517	0.6514	2.1669	-1.1284	-0.3479	-19.1740	3.0557
1.25	-18.5802	-0.1593	0.8158	2.7385	-1.8949	-1.2878	-15.0171	2.9714
1.30	-18.5249	-0.1321	0.8057	2.1580	-1.7631	-2.2192	-18.5542	2.8614
1.35	-18.0806	-0.1108	0.6500	1.5944	-1.1725	-2.8562	-18.1086	2.7327
1.40	-17.6958	-0.0865	0.4208	1.8844	-0.3871	-3.3845	-17.7228	2.5998
1.45	-17.5258	-0.0682	0.2001	1.6430	0.6751	-3.8492	-17.5522	2.4561
1.50	-17.5430	-0.0029	0.0504	1.3690	1.6157	-4.2922	-17.5741	2.2953
1.55	-17.6675	-0.0682	-0.0035	2.2244	2.0344	-4.7236	-17.6933	2.1207
1.60	-16.8571	0.1385	-0.3705	1.9600	15.8746	-1.7891	-16.8845	2.1687
1.65	-16.8030	0.6561	-1.1181	2.5015	5.9488	1.3846	-16.8380	2.6580
1.70	-16.0025	-0.0348	-0.1757	2.4578	-4.0648	-11.3122	-16.1006	1.7613
1.75	-20.7633	-0.1591	1.6875	-2.7453	-6.6377	-7.6146	-20.7954	1.3664
1.80	-21.9388	-0.1050	2.2942	0.2443	-12.3145	-7.6606	-21.8640	1.1943
1.85	-20.3397	-0.1101	2.1488	7.3367	-12.7475	-6.2143	-20.3593	1.0680
1.90	-18.2830	-0.1836	1.3944	1.0967	-0.7750	-4.4558	-18.3001	0.8573
1.95	-16.5781	-0.2022	0.2712	3.1568	-3.0456	-3.7001	-16.9937	0.7251



TIME (SEC)	LEFT SIDE					RIGHT SIDE				
	VERTICAL (LP)	LUNG. (LP)	LATERAL (LP)	MU-X	MU-Y	VERTICAL (LP)	LUNG. (LP)	LATERAL (LP)	MU-X	MU-Y
0.0	8222.98	-0.0	C.C	C.C	C.C	8222.98	-0.0	C.C	C.C	C.C
0.05	8221.55	-0.05	-2.21	-C.C003	-C.C003	8222.30	1.10	-2.21	C.C001	-0.0003
0.10	8213.76	-86.28	-4.45	-C.C015	-C.C005	8211.78	-83.39	-4.49	-0.0102	-0.0005
0.15	8226.02	-610.53	-5.55	-C.C500	-C.C007	8217.37	-406.33	-5.55	-0.0694	-0.0007
0.20	8301.02	-858.68	-3.49	-C.C1083	-C.C004	8274.72	-897.34	-3.45	-0.1078	-0.0004
0.25	8455.06	-1378.85	2.25	-C.C1631	C.C003	8404.03	-1370.91	2.25	-0.1631	0.0003
0.30	8606.77	-1306.80	11.71	-C.C2095	C.C014	8523.38	-1797.19	11.69	-0.2109	0.0014
0.35	8600.96	-2164.57	25.59	-C.C2517	C.C030	8469.13	-2152.93	25.86	-0.2542	0.0031
0.40	8629.14	-2463.55	44.86	-C.C2855	C.C052	8440.12	-2450.50	44.53	-0.2904	0.0053
0.45	8619.35	-2706.14	68.82	-0.3140	C.C080	8359.03	-2691.35	68.05	-0.3220	0.0081
0.50	8518.81	-2915.18	77.75	-C.C3422	C.C115	8177.32	-2898.80	56.20	-0.3545	0.0118
0.55	8412.24	-3109.51	131.27	-0.3697	C.C156	7983.35	-3092.34	128.34	-0.3873	0.0161
0.60	8335.10	-3296.55	168.75	-C.C3955	C.0202	7811.91	-3778.24	163.83	-0.4196	0.0210
0.65	8328.50	-3476.67	205.38	-C.C4174	C.C251	7708.57	-3458.75	201.87	-0.4487	0.0262
0.70	8389.80	-3644.10	252.25	-C.C4343	C.C301	7668.82	-3626.83	241.63	-0.4729	0.0315
0.75	8477.79	-3795.16	256.74	-0.4666	C.C349	7671.93	-3778.72	282.55	-0.4925	0.0368
0.80	8642.52	-3926.50	342.46	-0.4544	C.C396	7707.74	-3911.39	324.34	-0.5075	0.0421
0.85	8807.50	-4038.44	389.01	-0.4585	C.C486	7759.01	-4023.80	366.62	-0.5186	0.0473
0.90	8963.27	-4130.39	435.66	-C.C4608	C.C486	7799.59	-4116.48	408.63	-0.5278	0.0524
0.95	9082.43	-4205.83	481.80	-C.C4631	C.C530	7804.48	-4192.23	449.57	-0.5372	0.0576
1.00	9152.72	-4268.25	527.04	-0.4663	C.C576	7764.39	-4254.58	488.90	-0.5480	0.0630
1.05	9184.49	-4320.38	574.56	-C.C4704	C.C626	7691.35	-4309.30	529.83	-0.5603	0.0689
1.10	9192.11	-4366.13	621.78	-C.C4750	C.C676	7605.76	-4358.33	565.13	-0.5730	0.0748
1.15	9186.96	-4408.41	665.52	-0.4799	C.C724	7521.84	-4396.75	605.31	-0.5845	0.0805
1.20	9174.19	-4441.04	701.73	-C.C4841	C.C765	7454.86	-4439.75	635.10	-0.5956	0.0852
1.25	9165.33	-4480.58	729.49	-0.4889	C.C796	7409.55	-4482.46	658.18	-0.6050	0.0888
1.30	9170.42	-4520.39	748.43	-C.C4529	C.C816	7392.93	-4525.79	674.25	-0.6122	0.0912
1.35	9187.03	-4556.55	758.66	-0.4960	C.C826	7408.60	-4564.73	684.01	-0.6161	0.0923
1.40	9214.08	-4587.96	762.06	-C.C4979	C.C827	7441.50	-4597.66	688.23	-C.6178	0.0925
1.45	9237.34	-4613.48	758.23	-0.4994	C.C821	7485.62	-4624.84	686.69	-0.6178	0.0917
1.50	9250.46	-4633.87	747.57	-0.5009	C.C804	7533.21	-4646.09	679.81	-0.6167	0.0902
1.55	9250.82	-4650.00	732.45	-0.5027	C.C792	7578.37	-4663.03	668.32	-0.6153	0.0882
1.60	9197.11	-4666.56	713.38	-C.C5074	C.C776	7584.67	-4675.46	653.28	-0.6164	0.0861
1.65	9033.46	-4691.01	654.27	-0.5193	C.C769	7484.86	-4694.19	636.81	-0.6272	0.0851
1.70	8932.79	-4717.15	605.72	-0.5281	C.C678	7520.13	-4744.75	560.16	-C.6309	0.0745
1.75	8863.45	-4670.88	533.01	-C.C601	C.C601	7669.95	-4692.11	501.08	-0.6117	0.0653
1.80	8857.36	-4662.57	474.35	-0.5264	C.C0536	7714.65	-4678.11	447.60	-0.6064	0.0580
1.85	8830.20	-4684.44	424.44	-C.5305	C.C481	7807.57	-4701.16	403.88	-0.0518	0.0518
1.90	8798.29	-4719.11	351.62	-0.5364	C.C445	7908.20	-4731.11	376.56	-0.5983	0.0476
1.95	8800.27	-4743.67	318.70	-0.5390	C.C430	7984.85	-4752.59	366.35	-0.5952	0.0459













SAMPLE RUN - TRIPLES BRAKING IN A TURN, ALL OPTICS EXERCISED  
 TRACTOR REAR SUSPENSION - LATERAL TIRE FORCE FAC MOMENT SUMMARY

LEADING TANDEM AXLE

LEFT SIDE				RIGHT SIDE				
TIME (SEC)	TIRE SIDESLIP ANGLE (DEG)	TIRE LATERAL FORCE (LB)	MJ-Y	ALIGNING TORQUE (IN-LB)	TIRE SIDESLIP ANGLE (DEG)	TIRE LATERAL FORCE (LB)	MU-Y	ALIGNING TORQUE (IN-LB)
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.05	0.0030	-2.2077	-0.0002	0.0	0.0	-2.2079	-0.0003	0.0
0.10	0.0062	-4.4855	-0.0005	0.0	0.0030	-4.4905	-0.0005	0.0
0.15	0.0077	-5.5506	-0.0007	0.0	0.0062	-5.5519	-0.0007	0.0
0.20	0.0048	-3.4893	-0.0004	0.0	0.0077	-3.4878	-0.0004	0.0
0.25	-0.0031	2.2533	0.0002	0.0	0.0048	2.2506	0.0003	0.0
0.30	-0.0152	11.7131	0.0014	0.0	-0.0031	11.6853	0.0014	0.0
0.35	-0.0363	25.5771	0.0020	0.0	-0.0152	25.8565	0.0031	0.0
0.40	-0.0629	44.8627	0.0052	0.0	-0.0363	44.5321	0.0053	0.0
0.45	-0.0971	66.8176	0.0080	0.0	-0.0629	68.0458	0.0081	0.0
0.50	-0.1394	57.7922	0.0115	0.0	-0.0971	96.2009	0.0118	0.0
0.55	-0.1891	131.2715	0.0156	0.0	-0.1394	128.3401	0.0161	0.0
0.60	-0.2453	168.7515	0.0202	0.0	-0.1891	163.8287	0.0210	0.0
0.65	-0.3055	209.3765	0.0251	0.0	-0.2473	201.8727	0.0262	0.0
0.70	-0.3676	252.2480	0.0301	0.0	-0.3084	241.6325	0.0315	0.0
0.75	-0.4304	296.7354	0.0345	0.0	-0.3716	282.5510	0.0368	0.0
0.80	-0.4932	342.4553	0.0396	0.0	-0.4357	324.3381	0.0421	0.0
0.85	-0.5555	389.0117	0.0442	0.0	-0.4998	366.6169	0.0473	0.0
0.90	-0.6172	425.6628	0.0486	0.0	-0.5628	408.6252	0.0524	0.0
0.95	-0.6786	481.7951	0.0530	0.0	-0.6272	449.5659	0.0576	0.0
1.00	-0.7400	527.0400	0.0576	0.0	-0.6907	488.9048	0.0630	0.0
1.05	-0.8063	574.9583	0.0626	0.0	-0.7542	529.8320	0.0689	0.0
1.10	-0.8719	621.7765	0.0676	0.0	-0.8225	569.1313	0.0748	0.0
1.15	-0.9338	665.5225	0.0724	0.0	-0.8908	605.3137	0.0805	0.0
1.20	-0.9858	701.7332	0.0765	0.0	-0.9550	635.0991	0.0852	0.0
1.25	-1.0262	725.4854	0.0796	0.0	-1.0090	658.1760	0.0888	0.0
1.30	-1.0534	748.4348	0.0816	0.0	-1.0510	674.2896	0.0912	0.0
1.35	-1.0675	758.6552	0.0826	0.0	-1.0795	684.0129	0.0923	0.0
1.40	-1.0714	762.0613	0.0827	0.0	-1.0945	688.2280	0.0925	0.0
1.50	-1.0504	747.5744	0.0809	0.0	-1.0988	686.6858	0.0917	0.0
1.55	-1.0288	732.4541	0.0752	0.0	-1.0776	679.8053	0.0902	0.0
1.60	-1.0053	713.3840	0.0776	0.0	-1.0555	668.3191	0.0882	0.0
1.65	-0.9879	694.2715	0.0765	0.0	-1.0314	653.2837	0.0861	0.0
1.70	-0.9672	665.7178	0.0678	0.0	-1.0147	636.8135	0.0851	0.0
1.75	-0.9455	632.0110	0.0601	0.0	-0.8905	560.1577	0.0745	0.0
1.80	-0.9213	474.3528	0.0526	0.0	-0.7852	501.0803	0.0653	0.0
1.85	-0.9108	424.4377	0.0481	0.0	-0.6984	447.6030	0.0580	0.0
1.90	-0.9350	351.6155	0.0445	0.0	-0.6258	403.8777	0.0518	0.0
1.95	-0.9465	378.7017	0.0420	0.0	-0.5788	376.5591	0.0476	0.0
					-0.5555	366.3513	0.0459	0.0

F5R1 TRUCK AND TRACTOR-TRAILER DYNAMIC RESPONSE SIMULATION - T3DRS, V1  
 SAMPLE RUN - TRIPLES BRAKING IN A TURN, ALL OPTICS EXERCISED  
 TRACTOR REAR SUSPENSION - LATERAL TIRF FORCE AND MOMENT SUMMARY  
 TRAILING TANDEM AXLE

LEFT SIDE				RIGHT SIDE				
TIRE (SFC)	TIRE SIDESLIP ANGLE (DEG)	TIRE LATERAL FORCE (LB)	MU-Y	ALIGNING TORQUE ((IN-LB))	TIRE SIDESLIP ANGLE (DEG)	TIRE LATERAL FORCE (LB)	MU-Y	ALIGNING TORQUE ((IN-LB))
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.05	0.001	-0.0644	-0.0000	0.0	0.0001	-0.0646	-0.0000	0.0
0.10	0.0054	3.5280	0.0005	0.0	-0.0054	3.9250	0.0005	0.0
0.15	-0.0181	12.5148	0.0010	0.0	-0.0181	12.8852	0.0016	0.0
0.20	-0.0402	27.8235	0.0036	0.0	-0.0403	27.6834	0.0037	0.0
0.25	-0.0720	48.2303	0.0066	0.0	-0.0721	47.8054	0.0066	0.0
0.30	-0.1129	72.8846	0.0104	0.0	-0.1122	71.8529	0.0105	0.0
0.35	-0.1644	95.5843	0.0154	0.0	-0.1645	97.6591	0.0157	0.0
0.40	-0.2256	130.5586	0.0214	0.0	-0.2266	124.7709	0.0216	0.0
0.45	-0.2968	163.1400	0.0282	0.0	-0.2984	152.4036	0.0282	0.0
0.50	-0.3785	196.6088	0.0357	0.0	-0.3805	179.9155	0.0357	0.0
0.55	-0.4693	224.0632	0.0440	0.0	-0.4728	209.4877	0.0440	0.0
0.60	-0.5678	276.2550	0.0520	0.0	-0.5727	241.3779	0.0525	0.0
0.65	-0.6717	324.1305	0.0624	0.0	-0.6782	276.6487	0.0623	0.0
0.70	-0.7787	376.1659	0.0721	0.0	-0.7872	313.3486	0.0715	0.0
0.75	-0.8882	429.8130	0.0820	0.0	-0.8990	349.1216	0.0817	0.0
0.80	-0.9998	485.0430	0.0921	0.0	-1.0122	383.8792	0.0916	0.0
0.85	-1.1129	542.7771	0.1023	0.0	-1.1294	417.9946	0.1016	0.0
0.90	-1.2270	602.1104	0.1126	0.0	-1.2465	450.8584	0.1219	0.0
0.95	-1.3420	661.0732	0.1230	0.0	-1.3657	480.8352	0.1320	0.0
1.00	-1.4578	719.0735	0.1335	0.0	-1.4857	506.9102	0.1420	0.0
1.05	-1.5739	773.7800	0.1440	0.0	-1.6062	530.6030	0.1512	0.0
1.10	-1.6812	824.4827	0.1537	0.0	-1.7178	551.4966	0.1594	0.0
1.15	-1.7785	870.1838	0.1625	0.0	-1.8188	569.4436	0.1663	0.0
1.20	-1.8613	906.8755	0.1700	0.0	-1.9050	583.9041	0.1717	0.0
1.25	-1.9282	934.3352	0.1758	0.0	-1.9745	594.5520	0.1742	0.0
1.30	-1.9762	952.5365	0.1800	0.0	-2.0252	597.7102	0.1731	0.0
1.35	-2.0063	963.1925	0.1825	0.0	-2.0568	592.7139	0.1685	0.0
1.40	-2.0218	967.6780	0.1837	0.0	-2.0734	578.0002	0.1600	0.0
1.45	-2.0236	964.8021	0.1827	0.0	-2.0757	552.3408	0.1473	0.0
1.50	-2.0134	955.5515	0.1827	0.0	-2.0655	513.5801	0.1320	0.0
1.55	-1.9932	940.6404	0.1807	0.0	-2.0445	457.5376	0.1295	0.0
1.60	-1.9725	915.5437	0.1826	0.0	-2.0238	416.2891	0.1146	0.0
1.65	-1.9566	878.0754	0.1834	0.0	-2.0058	392.6440	0.1528	0.0
1.70	-1.9641	851.2813	0.1803	0.0	-1.9141	707.0442	0.1812	0.0
1.75	-1.7217	855.2205	0.1622	0.0	-1.7660	650.1375	0.1629	0.0
1.80	-1.6156	814.5258	0.1455	0.0	-1.6561	602.1196	0.1499	0.0
1.85	-1.5254	750.4255	0.1401	0.0	-1.5628	552.3381	0.1396	0.0
1.90	-1.4739	688.7124	0.1342	0.0	-1.5095	530.5383	0.1339	0.0
1.95	-1.4590	656.1321	0.1320	0.0	-1.4947	509.8438	0.1316	0.0









FIRST TRUCK AND TRAILER DYNAMIC RESPONSE SIMULATION - TRIP 5, VI  
 SAMPLE RUN - TRIPLES BRAKING IN A TURN, ALL OPTICS EXERCISED  
 TRAILER NO. 1 SPRUNG MASS POSITION

TIME (SEC)	FORWARD (FT)	LATERAL (FT)	VERTICAL (FT)	ROLL (DEG)	PITCH (DEG)	HEADING (DEG)	TURN RADIUS (FT)	SIDE SLIP (DEG)	ARTICULATION ANGLE (DEG)
0.0	-26.7614	0.0	0.0	0.0	0.0	0.0	*****	0.0	0.0
0.05	-24.0514	0.0000	-0.0000	-0.0001	0.0000	0.0000	*****	0.0000	0.0005
0.10	-21.8522	0.0000	-0.0000	-0.0020	0.0002	0.0002	*****	-0.0001	0.0041
0.15	-19.6570	0.0000	-0.0004	-0.0067	0.0014	0.0006	*****	-0.0008	0.0136
0.20	-17.4711	-0.0000	-0.0014	-0.0130	0.0036	0.0013	*****	-0.0015	0.0321
0.25	-15.2973	-0.0000	-0.0033	-0.0214	0.0017	0.0025	75191.0000	-0.0018	0.0616
0.30	-13.1349	0.0001	-0.0065	-0.0318	0.0061	0.0046	30994.5938	-0.0011	0.1041
0.35	-10.9836	0.0003	-0.0113	-0.0452	0.0260	0.0081	17681.0703	0.0008	0.1605
0.40	-8.8472	0.0007	-0.0173	-0.0621	0.0471	0.0137	11280.0625	0.0041	0.2329
0.45	-6.7330	0.0016	-0.0240	-0.0819	0.0671	0.0215	7669.6523	0.0091	0.3206
0.50	-4.6501	0.0030	-0.0305	-0.1042	0.0883	0.0320	5475.6563	0.0164	0.4239
0.55	-2.6065	0.0052	-0.0360	-0.1277	0.1093	0.0476	4060.4783	0.0268	0.5423
0.60	-0.6077	0.0083	-0.0430	-0.1516	0.1251	0.0655	3124.3364	0.0409	0.6750
0.65	1.3444	0.0120	-0.0423	-0.1756	0.1329	0.0884	2479.1394	0.0589	0.8212
0.70	3.2496	0.0182	-0.0430	-0.1597	0.1348	0.1155	2017.1440	0.0811	0.9801
0.75	5.1098	0.0255	-0.0423	-0.2245	0.1342	0.1476	1674.5898	0.1075	1.1511
0.80	6.9271	0.0347	-0.0408	-0.2507	0.1324	0.1851	1412.0679	0.1383	1.3340
0.85	8.7032	0.0455	-0.0392	-0.2784	0.1290	0.2284	1202.9475	0.1736	1.5285
0.90	10.4391	0.0594	-0.0390	-0.3073	0.1245	0.2778	1031.3032	0.2140	1.7344
0.95	12.1344	0.0754	-0.0375	-0.3367	0.1211	0.3336	887.8547	0.2602	1.9505
1.00	13.7882	0.0941	-0.0378	-0.3654	0.1208	0.3957	768.5828	0.3132	2.1770
1.05	15.3990	0.1157	-0.0386	-0.3519	0.1230	0.4643	671.0388	0.3735	2.4110
1.10	16.9650	0.1404	-0.0398	-0.4129	0.1266	0.5385	588.3108	0.4420	2.6488
1.15	18.4844	0.1684	-0.0411	-0.4267	0.1303	0.6192	523.2026	0.5190	2.8865
1.20	19.9561	0.1997	-0.0423	-0.4348	0.1341	0.7051	471.7708	0.6032	3.1211
1.25	21.3799	0.2344	-0.0430	-0.4374	0.1376	0.7965	431.9783	0.6933	3.3504
1.30	22.7561	0.2724	-0.0434	-0.4358	0.1400	0.8928	399.4634	0.7874	3.5724
1.35	24.0899	0.3137	-0.0433	-0.4310	0.1407	0.9938	371.4270	0.8849	3.7853
1.40	25.3699	0.3591	-0.0430	-0.4236	0.1399	1.0951	347.9719	0.9850	3.9877
1.45	26.6095	0.4055	-0.0425	-0.4143	0.1383	1.2082	327.1606	1.0870	4.1789
1.50	27.8050	0.4556	-0.0420	-0.4026	0.1366	1.3205	308.1414	1.1910	4.3583
1.55	28.9562	0.5082	-0.0416	-0.3880	0.1349	1.4352	291.0168	1.2970	4.5255
1.60	30.0631	0.5631	-0.0413	-0.3698	0.1333	1.5514	276.5706	1.4048	4.6804
1.65	31.1272	0.6198	-0.0410	-0.3470	0.1314	1.6682	270.1460	1.5107	4.8300
1.70	32.1497	0.6781	-0.0403	-0.3200	0.1283	1.7846	240.7737	1.6187	4.9784
1.75	33.1302	0.7378	-0.0393	-0.2858	0.1261	1.9036	211.8769	1.7500	5.1019
1.80	34.0594	0.7990	-0.0387	-0.2537	0.1255	2.0254	212.5477	1.8808	5.2033
1.85	34.9341	0.8610	-0.0398	-0.2476	0.1244	2.1455	222.8593	1.9929	5.2883
1.90	35.7579	0.9231	-0.0395	-0.2125	0.1233	2.2616	222.6418	2.0919	5.3633
1.95	36.5356	0.9844	-0.0407	-0.1665	0.1257	2.3716	221.5917	2.1864	5.4331

F-81 TRUCK AND TRACTOR-TRAILER DYNAMIC RESPONSE SIMULATION - T3CRS,V1 OUTPUT PAGE NO. 1.01.2  
 SAMPLE RUN - TRIPLES BRAKING IN A TURN, ALL OPTICS EXERCISED  
 TRAILER NO. 1 SPRUNG MASS VELOCITY (PCY FXFS)

TIME (SEC)	FORWARD (FT/SEC)	LATERAL (FT/SEC)	VERTICAL (FT/SEC)	ROLL (DEG/SEC)	PITCH (DEG/SEC)	HEADING (DEG/SEC)	ARTICULATION RATE (DEG/SEC)
0.0	44.00	0.00	0.00	0.00	0.00	0.00	0.00
0.05	44.00	0.00	-0.00	-0.01	0.00	0.00	0.03
0.10	44.00	-0.00	-0.00	-0.07	0.01	0.01	0.12
0.15	43.58	-0.00	-0.01	-0.11	0.04	0.01	0.27
0.20	43.02	-0.00	-0.03	-0.14	-0.02	0.02	0.47
0.25	43.77	-0.00	-0.05	-0.19	-0.07	0.03	0.72
0.30	43.48	-0.00	-0.08	-0.23	0.28	0.05	0.99
0.35	43.05	0.00	-0.09	-0.30	0.44	0.05	1.25
0.40	42.51	0.00	-0.10	-0.37	0.40	0.14	1.60
0.45	41.88	0.01	-0.09	-0.42	0.41	0.15	1.91
0.50	41.17	0.01	-0.06	-0.46	0.44	0.26	2.22
0.55	40.38	0.02	-0.02	-0.48	0.38	0.33	2.51
0.60	39.55	0.03	0.02	-0.48	0.23	0.41	2.79
0.65	38.65	0.04	0.06	-0.48	0.08	0.49	3.05
0.70	37.81	0.05	0.05	-0.49	0.00	0.59	3.30
0.75	36.94	0.07	0.11	-0.51	-0.03	0.70	3.54
0.80	36.09	0.09	0.12	-0.54	-0.05	0.81	3.78
0.85	35.24	0.11	0.11	-0.57	-0.09	0.93	4.01
0.90	34.35	0.13	0.05	-0.59	-0.09	1.05	4.23
0.95	33.54	0.15	0.07	-0.59	-0.05	1.18	4.43
1.00	32.67	0.18	0.06	-0.56	0.01	1.31	4.61
1.05	31.77	0.21	0.05	-0.49	0.05	1.43	4.73
1.10	30.85	0.24	0.04	-0.35	0.06	1.55	4.77
1.15	29.92	0.27	0.04	-0.22	0.06	1.66	4.73
1.20	28.99	0.31	0.05	-0.11	0.06	1.77	4.65
1.25	28.06	0.34	0.06	-0.01	0.05	1.88	4.52
1.30	27.13	0.37	0.07	0.06	0.02	1.97	4.35
1.35	26.22	0.40	0.07	0.12	-0.02	2.07	4.16
1.40	25.31	0.44	0.07	0.16	-0.04	2.15	3.94
1.45	24.40	0.46	0.07	0.20	-0.05	2.22	3.71
1.50	23.50	0.49	0.07	0.26	-0.05	2.27	3.47
1.55	22.60	0.51	0.06	0.32	-0.05	2.31	3.22
1.60	21.65	0.53	0.06	0.40	-0.05	2.33	3.00
1.65	20.78	0.55	0.06	0.50	-0.07	2.33	3.02
1.70	19.85	0.56	0.07	0.54	-0.08	2.34	2.75
1.75	19.02	0.58	0.06	0.43	-0.04	2.42	2.23
1.80	18.15	0.60	0.05	0.47	-0.02	2.44	1.85
1.85	17.24	0.60	0.03	0.58	-0.04	2.37	1.58
1.90	16.29	0.59	0.02	0.83	-0.01	2.26	1.44
1.95	15.33	0.59	0.01	0.96	0.00	2.15	1.36

HISRI TRUCK AND TRACTOR-TRAILER DYNAMIC RESPONSE SIMULATION - T3DRS.V1  
 SAMPLE RUN - TRIPLES BRAKING IN A TURN, ALL OPTICS EXERCISED

TIME (SEC)	TRAILER AC. 1 SPLUNC MASS ACCELERATION (BODY AXES)				INFRIAL ACCEL. ALCNG BODY AXES			
	FORWARD (FT/SEC**2)	LATERAL (FT/SEC**2)	VERTICAL (FT/SEC**2)	ROLL (DEG/SEC**2)	HEADING (DFG/SEC**2)	PITCH (DEG/SEC**2)	LCAGITUDINAL (FT/SEC**2)	LATERAL (FT/SEC**2)
0.0	0.0	0.0	0.0	0.0	0.0	0.0	-0.0	0.0
0.05	-0.0035	0.0008	-0.0002	-0.0002	0.0519	0.0412	-0.0035	0.0015
0.10	-0.0091	-0.0067	-0.0055	-1.2735	0.1284	0.4108	-0.0981	-0.0023
0.15	-0.0548	-0.0123	-0.0252	-0.5039	0.1041	0.6865	-0.5649	-0.0033
0.20	-1.9488	-0.0094	-0.3572	-0.8942	0.1662	-1.9305	-1.9488	0.0041
0.25	-4.3052	0.0026	-0.5752	-0.7744	0.3609	2.5005	-4.3051	0.0259
0.30	-7.1841	0.0203	-0.4278	-1.1832	0.5915	7.1076	-7.1845	0.0613
0.35	-9.7799	0.0376	-0.0376	-1.4559	0.8278	-0.5155	-9.7806	0.1047
0.40	-11.7845	0.0585	-0.0034	-1.1631	1.0158	-0.5484	-11.7852	0.1594
0.45	-13.4678	0.0869	0.3723	-1.0361	1.2163	0.6720	-13.4664	0.2267
0.50	-14.5671	0.1215	0.7117	-0.4707	1.3720	0.0492	-14.5676	0.3058
0.55	-16.2020	0.1636	0.8558	-0.01370	1.4968	-2.2212	-16.2022	0.3952
0.60	-17.0277	0.2087	0.8053	-0.0193	1.6450	-3.3746	-17.0278	0.4901
0.65	-17.4235	0.2536	0.6847	-0.0123	1.8239	-2.4345	-17.4237	0.5877
0.70	-17.4435	0.2561	0.5182	-0.3342	2.0166	-0.8821	-17.4440	0.6862
0.75	-17.2723	0.3357	0.2725	-0.5495	2.1808	-0.4587	-17.2732	0.7849
0.80	-16.9996	0.3740	-0.0224	-0.6307	2.3080	-0.7282	-17.0009	0.8837
0.85	-16.8682	0.4132	-0.2673	-0.5308	2.4311	-0.5159	-16.8701	0.9838
0.90	-16.5442	0.4551	-0.3755	-0.3755	2.5351	0.4752	-16.5467	1.0865
0.95	-17.2401	0.5007	-0.3518	0.2714	2.5865	1.2402	-17.2432	1.1913
1.00	-17.6717	0.5482	-0.2605	0.8122	2.5705	1.0658	-17.6757	1.2943
1.05	-18.1058	0.5935	-0.1505	2.2202	2.4372	0.4500	-18.1109	1.3887
1.10	-18.4689	0.6430	-0.0356	3.0613	2.2664	0.0400	-18.4752	1.4783
1.15	-18.6630	0.6757	0.0745	2.1074	2.2629	-0.0067	-18.6708	1.5446
1.20	-18.6920	0.6875	0.1505	2.3356	2.1627	-0.1146	-18.6914	1.5861
1.25	-18.5854	0.6786	0.1666	1.6097	1.9827	-0.4685	-18.5964	1.5985
1.30	-18.4274	0.6553	0.1302	1.2735	1.8784	-0.7335	-18.4402	1.5905
1.35	-18.2349	0.6242	0.0718	1.0345	1.7232	-0.6018	-18.2455	1.5690
1.40	-18.1073	0.5817	0.0112	0.7099	1.5245	-0.2972	-18.1237	1.5297
1.45	-18.0353	0.5346	-0.0444	0.9757	1.2523	-0.0565	-18.0532	1.4783
1.50	-18.0436	0.4860	-0.0500	1.1694	0.9481	0.0330	-18.0630	1.4174
1.55	-18.1147	0.4338	-0.1186	1.4226	0.6430	0.0710	-18.1354	1.3450
1.60	-18.1714	0.3713	-0.0472	1.8256	0.2446	-0.1253	-18.1931	1.2547
1.65	-18.0093	0.2782	0.1281	1.9573	-0.3094	-0.5441	-18.0316	1.1232
1.70	-17.5342	0.3403	0.0381	-1.6265	1.2578	0.4040	-17.6072	1.1517
1.75	-17.3054	0.3744	-0.1568	-0.9474	1.3445	0.8517	-17.3300	1.1786
1.80	-17.7695	0.1520	-0.3203	1.6581	-0.7770	-0.3238	-17.7939	0.9633
1.85	-19.5704	-0.0256	-0.3489	3.5385	-1.8886	-0.0557	-19.5951	0.6860
1.90	-19.1259	-0.1476	-0.2204	5.1222	-2.3479	1.5416	-19.1453	0.4941
1.95	-19.1709	-0.2461	-0.0444	-0.1811	-1.9205	2.0886	-19.1928	0.3265

F501 TRUCK AND TRACTOR-TRAILER DYNAMIC RESPONSE SIMULATION - F30RS, VI CLIPUT PAGE NO. 1.05.2  
 SAMPLE RUN - TRIPLES BRAKING IN A TURN, ALL OPTIIONS EXERCISED  
 TRAILER NO. 1 REAR SUSPENSION TIRE FORCES  
 LEADING TANDEM AXLE

TIME (SEC)	LEFT SIDE				RIGHT SIDE				
	VERTICAL (LBS)	LATERAL (LBS)	LCNG. (LBS)	MU-X	VERTICAL (LBS)	LATERAL (LBS)	LCNG. (LBS)	MU-X	MU-Y
0.0	6631.73	C-C	-0.0	C-C	6631.73	0.0	-0.0	0-C	0-C
0.05	6631.74	-0.53	-0.00	-C.C000	6631.72	-0.53	0.04	0.0000	-0.0001
0.10	6632.85	-3.05	0.61	C.C001	6630.24	-3.08	0.76	C.C001	-0.0005
0.15	6636.60	-3.30	0.22	C.C000	6619.72	-3.25	0.37	C.C001	-0.0005
0.20	6651.62	-2.82	-1.68	-C.C254	6615.91	-2.80	-168.41	-0.0255	-0.0004
0.25	6615.04	-1.28	-583.18	-0.C082	6553.20	-1.27	-581.30	-0.C087	-0.C002
0.30	6604.04	2.63	-1016.56	-C.C159	6506.91	2.55	-1013.31	-0.1557	0.0004
0.35	6677.68	7.54	-1339.57	-C.C206	6536.02	7.38	-1335.12	-0.2043	0.0011
0.40	6666.44	15.24	-1573.00	-C.C230	6466.67	14.79	-1566.97	-0.2423	0.C023
0.45	6609.59	25.10	-1746.68	-C.C263	6341.36	24.09	-1739.23	-0.2743	0.C038
0.50	6585.59	37.40	-1877.24	-C.C285	6240.50	35.45	-1869.87	-0.2995	0.0057
0.55	6612.52	51.75	-1973.36	-C.C284	6183.23	49.46	-1964.91	-0.3178	0.0078
0.60	6647.00	66.55	-2043.35	-C.C074	6133.71	61.48	-2034.97	-0.3318	0.0100
0.65	6672.21	81.61	-2097.52	-C.C144	6074.68	74.40	-2089.03	-0.3439	0.0122
0.70	6715.46	96.67	-2143.17	-C.C191	6033.64	87.00	-2135.03	-0.3539	0.0144
0.75	6802.00	111.85	-2180.85	-C.C206	6033.43	95.41	-2173.38	-0.3602	0.0165
0.80	6911.13	127.04	-2209.17	-0.2197	6051.95	111.50	-2202.05	-0.3639	0.0184
0.85	7001.50	141.66	-2227.77	-C.C182	6048.43	122.71	-2220.35	-0.3671	0.C203
0.90	7055.79	156.06	-2239.20	-0.2174	6006.00	133.26	-2231.26	-0.3715	0.0222
0.95	7089.29	170.10	-2245.49	-C.C167	5942.61	143.10	-2237.67	-0.3765	0.0241
1.00	7118.89	182.78	-2248.03	-C.C158	5879.50	151.58	-2241.02	-0.3812	0.0258
1.05	7143.23	193.61	-2247.75	-0.2147	5820.50	158.45	-2241.51	-0.3852	0.C272
1.10	7153.65	203.41	-2246.45	-C.C140	5764.15	164.75	-2242.25	-0.3890	0.C286
1.15	7146.57	203.42	-2246.21	-C.C143	5722.63	163.83	-2244.16	-0.3922	0.C286
1.20	7140.73	198.19	-2248.14	-C.C148	5702.35	155.27	-2247.52	-0.3941	0.0279
1.25	7135.88	186.65	-2250.81	-0.2152	5709.05	150.31	-2252.16	-0.3945	0.C263
1.30	7137.64	168.34	-2253.70	-C.C157	5733.55	136.24	-2255.96	-0.3935	0.0238
1.35	7129.16	147.43	-2256.45	-0.2165	5762.33	120.13	-2259.23	-0.3921	0.0208
1.40	7111.87	121.50	-2258.22	-C.C176	5795.09	100.15	-2261.87	-0.3903	0.0173
1.45	7090.29	93.74	-2259.80	-C.C187	5831.65	77.82	-2263.57	-0.3882	0.0133
1.50	7062.77	62.52	-2255.74	-C.C200	5872.51	52.83	-2264.12	-0.3855	0.0090
1.55	7023.68	28.80	-2258.80	-C.C216	5914.45	24.50	-2263.67	-0.3827	0.0041
1.60	6971.98	-7.77	-2257.71	-0.2238	5957.07	-6.73	-2263.16	-0.3799	-0.0011
1.65	6909.43	-50.05	-2258.87	-C.C269	6009.45	-44.05	-2265.50	-0.3770	-0.0073
1.70	6851.65	-89.40	-2265.01	-C.C306	6078.36	-80.29	-2269.50	-0.3734	-0.0132
1.75	6832.76	-114.33	-2270.75	-0.2323	6150.25	-104.25	-2273.31	-0.3696	-0.0170
1.80	6798.43	-156.06	-2263.59	-C.C330	6231.58	-146.92	-2270.03	-0.3643	-0.0236
1.85	6656.99	-219.85	-2252.39	-C.C363	6288.29	-209.40	-2259.37	-0.3594	-0.0333
1.90	6566.95	-255.04	-2244.82	-C.C348	6307.57	-252.42	-2252.42	-0.3571	-0.0400
1.95	6441.89	-304.06	-2244.68	-C.C405	6274.37	-305.28	-2252.65	-0.3534	-0.0479







TIME (SEC)	LEFT SIDE				RIGHT SIDE			
	TIRE SIDESLIP ANGLE (DEG)	TIRE LATERAL FORCE (LB)	MU-Y	ALIGNING TORQUE (IN-LB)	TIRE SIDESLIP ANGLE (DEG)	TIRE LATERAL FORCE (LB)	MU-Y	ALIGNING TORQUE (IN-LB)
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.05	0.0004	-0.5345	-0.0001	0.0	0.0004	-0.5349	0.0	0.0
0.10	0.0026	-3.0851	-0.0005	0.0	0.0026	-3.0839	-0.0005	0.0
0.15	0.0027	-2.3006	-0.0005	0.0	0.0027	-3.2923	-0.0005	0.0
0.20	0.0023	-2.8182	-0.0004	0.0	0.0022	-2.8022	-0.0004	0.0
0.25	0.0011	-1.2778	-0.0002	0.0	0.0011	-1.2659	-0.0002	0.0
0.30	-0.0022	2.6282	0.0004	0.0	-0.0022	2.5399	0.0004	0.0
0.35	-0.0067	7.5403	0.0011	0.0	-0.0062	7.3819	0.0011	0.0
0.40	-0.0126	15.2387	0.0022	0.0	-0.0126	14.7869	0.0023	0.0
0.45	-0.0210	25.0954	0.0038	0.0	-0.0210	24.0883	0.0038	0.0
0.50	-0.0314	37.3550	0.0057	0.0	-0.0314	35.4528	0.0057	0.0
0.55	-0.0433	51.7859	0.0078	0.0	-0.0433	48.4644	0.0078	0.0
0.60	-0.0553	66.5505	0.0100	0.0	-0.0554	61.4765	0.0100	0.0
0.65	-0.0676	81.6146	0.0122	0.0	-0.0677	74.4033	0.0122	0.0
0.70	-0.0796	96.6722	0.0144	0.0	-0.0797	86.9566	0.0144	0.0
0.75	-0.0909	111.8522	0.0164	0.0	-0.0911	99.4060	0.0165	0.0
0.80	-0.1016	127.0308	0.0184	0.0	-0.1018	111.5010	0.0184	0.0
0.85	-0.1118	141.6637	0.0202	0.0	-0.1121	122.7115	0.0203	0.0
0.90	-0.1222	156.0573	0.0221	0.0	-0.1226	133.2566	0.0222	0.0
0.95	-0.1326	170.0974	0.0240	0.0	-0.1331	143.1009	0.0241	0.0
1.00	-0.1419	182.7751	0.0257	0.0	-0.1425	151.5772	0.0258	0.0
1.05	-0.1498	193.6103	0.0271	0.0	-0.1505	158.4928	0.0272	0.0
1.10	-0.1571	203.4124	0.0284	0.0	-0.1580	164.7518	0.0286	0.0
1.15	-0.1573	203.4287	0.0285	0.0	-0.1582	163.8297	0.0286	0.0
1.20	-0.1534	198.1914	0.0278	0.0	-0.1544	159.2683	0.0279	0.0
1.25	-0.1445	186.6917	0.0261	0.0	-0.1455	150.3092	0.0263	0.0
1.30	-0.1303	168.3423	0.0236	0.0	-0.1313	136.2419	0.0238	0.0
1.35	-0.1143	147.4328	0.0207	0.0	-0.1152	120.1328	0.0208	0.0
1.40	-0.0947	121.8974	0.0171	0.0	-0.0955	100.1926	0.0173	0.0
1.45	-0.0731	93.7430	0.0132	0.0	-0.0737	77.8199	0.0133	0.0
1.50	-0.0492	62.5164	0.0089	0.0	-0.0497	52.8273	0.0090	0.0
1.55	-0.0227	28.7954	0.0041	0.0	-0.0229	24.4965	0.0041	0.0
1.60	0.0062	-7.7718	-0.0011	0.0	0.0062	-6.7284	-0.0011	0.0
1.65	0.0400	-50.0463	-0.0072	0.0	0.0405	-44.0500	-0.0073	0.0
1.70	0.0721	-85.3583	-0.0130	0.0	0.0730	-80.2946	-0.0132	0.0
1.75	0.0925	-114.3253	-0.0167	0.0	0.0937	-104.2913	-0.0170	0.0
1.80	0.1285	-158.0550	-0.0222	0.0	0.1302	-146.9209	-0.0236	0.0
1.85	0.1814	-219.8487	-0.0328	0.0	0.1840	-209.4027	-0.0333	0.0
1.90	0.2180	-259.0144	-0.0354	0.0	0.2212	-252.4229	-0.0400	0.0
1.95	0.2609	-304.0605	-0.0472	0.0	0.2647	-305.2808	-0.0479	0.0



F-SPI TRUCK AND TRACTOR-TRAILER DYNAMIC RESPONSE SIMULATION - TOURS, VI      CUTPUT PAGE NO. 1.14-2  
 SAMPLE RUN - TRIPLES BRAKING IN A TURN, ALL OPTICSAS EXERCISED  
 TRAILER NO. 1 REAR SUSPENSION - LATERAL TIRE FORCE AND MOMENT SUMMARY  
 TRAILING TANDEM AXLE

LEFT SIDE				RIGHT SIDE				
TIME (SECG)	TIRE SIDESLIP ANGLE (DEG)	TIRE LATERAL FORCE (LB)	MU-Y	ALIGNING TORQUE (IN-LB)	TIRE SIDESLIP ANGLE (DEG)	TIRE LATERAL FORCE (LB)	MU-Y	ALIGNING TORQUE (IN-LB)
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.05	0.0004	-0.4332	-0.0000	0.0	0.0004	-0.4331	-0.0000	0.0
0.10	0.0021	-2.4625	-0.0002	0.0	0.0021	-2.4617	-0.0002	0.0
0.15	0.0017	-2.0156	-0.0002	0.0	0.0017	-2.0119	-0.0002	0.0
0.20	0.0007	-0.8717	-0.0001	0.0	0.0007	-0.8684	-0.0001	0.0
0.25	-0.0017	2.0410	0.0002	0.0	-0.0017	2.0273	0.0002	0.0
0.30	-0.0072	8.3637	0.0009	0.0	-0.0072	8.2742	0.0009	0.0
0.35	-0.0146	17.0719	0.0018	0.0	-0.0146	16.8050	0.0018	0.0
0.40	-0.0254	29.7555	0.0031	0.0	-0.0254	29.0960	0.0031	0.0
0.45	-0.0393	45.8220	0.0047	0.0	-0.0393	44.4480	0.0047	0.0
0.50	-0.0563	65.7810	0.0068	0.0	-0.0564	63.2301	0.0068	0.0
0.55	-0.0750	85.2245	0.0091	0.0	-0.0759	84.9485	0.0092	0.0
0.60	-0.0965	114.3952	0.0116	0.0	-0.0966	107.8528	0.0116	0.0
0.65	-0.1186	141.2355	0.0143	0.0	-0.1188	131.8101	0.0143	0.0
0.70	-0.1419	165.6953	0.0171	0.0	-0.1421	156.7478	0.0171	0.0
0.75	-0.1660	200.2617	0.0200	0.0	-0.1664	183.0675	0.0201	0.0
0.80	-0.1909	232.7447	0.0230	0.0	-0.1914	210.4942	0.0231	0.0
0.85	-0.2167	266.3716	0.0261	0.0	-0.2173	238.1761	0.0262	0.0
0.90	-0.2441	301.4023	0.0295	0.0	-0.2449	266.2068	0.0295	0.0
0.95	-0.2720	337.9057	0.0325	0.0	-0.2738	294.6790	0.0330	0.0
1.00	-0.3016	375.0505	0.0364	0.0	-0.3025	323.0400	0.0365	0.0
1.05	-0.3297	411.8914	0.0398	0.0	-0.3313	350.7297	0.0400	0.0
1.10	-0.3575	448.1672	0.0431	0.0	-0.3554	377.8999	0.0434	0.0
1.15	-0.3789	475.8777	0.0457	0.0	-0.3810	398.6541	0.0460	0.0
1.20	-0.3974	500.2205	0.0479	0.0	-0.3995	417.2000	0.0482	0.0
1.25	-0.4112	519.0027	0.0496	0.0	-0.4140	432.0618	0.0499	0.0
1.30	-0.4202	531.5728	0.0507	0.0	-0.4234	442.5994	0.0511	0.0
1.35	-0.4280	541.8538	0.0516	0.0	-0.4315	451.6807	0.0521	0.0
1.40	-0.4324	547.2988	0.0522	0.0	-0.4362	457.2329	0.0526	0.0
1.45	-0.4345	545.4573	0.0524	0.0	-0.4366	460.4729	0.0529	0.0
1.50	-0.4337	547.5952	0.0523	0.0	-0.4381	460.8708	0.0528	0.0
1.55	-0.4295	540.6846	0.0518	0.0	-0.4340	457.6121	0.0524	0.0
1.60	-0.4219	529.0083	0.0505	0.0	-0.4266	450.9036	0.0515	0.0
1.65	-0.4059	506.1804	0.0490	0.0	-0.4106	435.6272	0.0495	0.0
1.70	-0.3953	490.3075	0.0477	0.0	-0.4001	426.5752	0.0483	0.0
1.75	-0.4137	512.3826	0.0495	0.0	-0.4151	448.5115	0.0506	0.0
1.80	-0.4046	501.4556	0.0488	0.0	-0.4102	441.9832	0.0495	0.0
1.85	-0.3635	446.1531	0.0438	0.0	-0.3687	399.1226	0.0445	0.0
1.90	-0.3319	402.0455	0.0400	0.0	-0.3367	365.0747	0.0406	0.0
1.95	-0.2948	353.1343	0.0356	0.0	-0.2991	327.0264	0.0361	0.0





HSRI TRUCK AND TRACTOR-TRAILER DYNAMIC RESPONSE SIMULATION - TRCRS.VI  
SAMPLE RUN - TRIPLES BRAKING IN A TURN, ALL OPTIONS EXERCISED  
TRAILER NO. 2 SPRUNG MASS POSITION

TIME (SEC)	FORWARD (FT)	LATERAL (FT)	VERTICAL (FT)	RCLL (DFG)	PITCH (DEG)	HEADING (DEG)	TURN RADIUS (FT)	SIDE SLIP (DEG)	ARTICULATION ANGLE (DEG)
0.0	-60.8718	0.0	0.0	0.0	0.0	0.0	*****	0.0	0.0
0.05	-58.5619	0.0000	0.0000	-0.0000	0.0000	0.0000	*****	0.0000	0.0000
0.10	-56.3626	0.0000	0.0000	-0.0000	-0.0000	0.0000	*****	0.0000	0.0002
0.15	-54.1674	0.0000	0.0000	-0.0000	-0.0000	0.0000	*****	0.0000	0.0006
0.20	-51.9815	0.0000	0.0000	-0.0000	-0.0017	0.0000	*****	0.0000	0.0013
0.25	-49.8077	0.0000	0.0000	0.0000	-0.0133	0.0000	*****	-0.0001	0.0025
0.30	-47.6453	0.0000	0.0015	0.0002	-0.0340	-0.0001	198.633	0.0005	0.0046
0.35	-45.4841	0.0000	0.0054	0.0008	-0.0546	-0.0002	94.731	-0.0012	0.0084
0.40	-43.3276	0.0001	0.0078	0.0019	-0.0691	-0.0000	54.914	-0.0024	0.0145
0.45	-41.1734	0.0003	0.0085	0.0035	-0.0717	-0.0017	35.852	-0.0043	0.0236
0.50	-39.0206	0.0006	0.0087	0.0056	-0.0689	-0.0031	25.545	-0.0068	0.0362
0.55	-37.1169	0.0010	0.0098	0.0081	-0.0681	-0.0051	19.698	-0.0100	0.0527
0.60	-35.1180	0.0016	0.0120	0.0105	-0.0703	-0.0077	16.619	-0.0138	0.0737
0.65	-33.1660	0.0025	0.0143	0.0124	-0.0719	-0.0100	15.265	-0.0178	0.0952
0.70	-31.2607	0.0036	0.0155	0.0133	-0.0693	-0.0142	15.176	-0.0216	0.1297
0.75	-29.4005	0.0048	0.0154	0.0128	-0.0629	-0.0178	16.443	-0.0249	0.1654
0.80	-27.5832	0.0063	0.0151	0.0108	-0.0568	-0.0213	20.133	-0.0273	0.2064
0.85	-25.8070	0.0079	0.0154	0.0074	-0.0542	-0.0245	21.476	-0.0283	0.2529
0.90	-24.0711	0.0095	0.0165	0.0029	-0.0545	-0.0272	14.719	-0.0275	0.3050
0.95	-22.3757	0.0111	0.0175	-0.0023	-0.0549	-0.0293	39.933	-0.0245	0.3629
1.00	-20.7218	0.0126	0.0180	-0.0078	-0.0537	-0.0306	15.689	-0.0190	0.4263
1.05	-19.1108	0.0135	0.0180	-0.0132	-0.0519	-0.0310	91.43	-0.0107	0.4952
1.10	-17.5446	0.0145	0.0175	-0.0182	-0.0509	-0.0302	62.11	0.0006	0.5690
1.15	-16.0250	0.0155	0.0181	-0.0226	-0.0516	-0.0280	45.59	0.0150	0.6472
1.20	-14.5529	0.0155	0.0134	-0.0263	-0.0529	-0.0242	35.50	0.0325	0.7254
1.25	-13.1237	0.0150	0.0186	-0.0295	-0.0533	-0.0188	28.85	0.0527	0.8153
1.30	-11.7520	0.0139	0.0185	-0.0321	-0.0524	-0.0114	24.05	0.0755	0.9041
1.35	-10.4218	0.0120	0.0182	-0.0343	-0.0508	-0.0019	20.49	0.1006	0.9957
1.40	-9.1370	0.0094	0.0180	-0.0362	-0.0498	0.0058	17.67	0.1280	1.0854
1.45	-7.8967	0.0059	0.0181	-0.0376	-0.0499	0.0235	15.35	0.1576	1.1848
1.50	-6.7004	0.0017	0.0184	-0.0387	-0.0504	0.0354	13.41	0.1997	1.2812
1.55	-5.5482	0.0034	0.0185	-0.0392	-0.0506	0.0574	11.79	0.2242	1.3778
1.60	-4.4403	0.0094	0.0185	-0.0391	-0.0503	0.0773	10.47	0.2614	1.4741
1.65	-3.3751	0.0162	0.0185	-0.0381	-0.0500	0.0953	9.29	0.3012	1.5689
1.70	-2.3513	0.0238	0.0185	-0.0362	-0.0501	0.1230	8.36	0.3435	1.6616
1.75	-1.3654	0.0323	0.0186	-0.0331	-0.0503	0.1464	7.87	0.3866	1.7552
1.80	-0.4288	0.0414	0.0187	-0.0283	-0.0503	0.1751	7.46	0.4291	1.8505
1.85	0.4375	0.0513	0.0188	-0.0218	-0.0502	0.2028	7.00	0.4715	1.9431
1.90	1.2629	0.0617	0.0188	-0.0144	-0.0504	0.2312	6.72	0.5133	2.0303
1.95	2.0422	0.0724	0.0187	-0.0067	-0.0511	0.2603	6.58	0.5528	2.1113

FSRT TRUCK AND TRACTOR-TRAILER DYNAMIC RESPONSE SIMULATION - TRERS, VI  
 SAMPLE RUN - TRIPLES BRAKING IN A TURN, ALL OPTICS EXERCISED  
 TRAILER NO. 2 SPRUNG MASS VELOCITY (BODY AXES)

TIME (SEC)	FORWARD (FT/SEC)	LATERAL (FT/SEC)	VERTICAL (FT/SEC)	ROLL (DEG/SEC)	PITCH (DEG/SEC)	HEADING (DEG/SEC)	ARTICULATION RATE (DEG/SEC)
0.0	44.00	0.0	0.0	C.0	0.0	0.0	0.0
0.05	44.00	0.00	-0.00	-C.00	-0.00	0.00	0.00
0.10	44.00	0.00	-0.00	-C.00	-0.00	0.00	0.01
0.15	43.55	0.00	-0.00	-C.00	-0.00	0.00	0.01
0.20	43.55	0.00	-0.00	C.00	-0.10	0.00	0.02
0.25	43.77	-0.00	-0.01	C.00	-0.37	-0.00	0.02
0.30	43.31	-0.00	0.04	C.01	-0.43	-0.00	0.06
0.35	42.75	-0.00	0.03	C.02	-0.38	-0.01	0.10
0.40	42.13	-0.00	-0.02	C.03	-0.17	-0.01	0.15
0.45	41.45	-0.00	-0.05	C.04	0.04	-0.02	0.21
0.50	40.77	-0.00	-0.04	C.05	0.05	-0.03	0.29
0.55	40.11	-0.01	-0.01	C.05	-0.02	-0.05	0.37
0.60	39.44	-0.01	0.00	C.04	-0.05	-0.06	0.46
0.65	38.73	-0.01	-0.01	C.03	0.00	-0.07	0.56
0.70	37.97	-0.01	-0.04	C.00	0.10	-0.07	0.66
0.75	37.14	-0.02	-0.05	-0.03	0.14	-0.07	0.77
0.80	36.27	-0.02	-0.04	-C.05	0.09	-0.07	0.87
0.85	35.35	-0.02	-0.02	-C.08	0.02	-0.06	0.99
0.90	34.42	-0.02	-0.01	-C.10	-0.02	-0.05	1.10
0.95	33.48	-0.01	-0.02	-C.11	0.01	-0.03	1.21
1.00	32.55	-0.01	-0.03	-0.11	0.04	-0.02	1.32
1.05	31.64	-0.01	-0.03	-C.10	0.03	0.00	1.43
1.10	30.75	0.00	-0.03	-C.05	0.00	0.03	1.52
1.15	29.87	0.01	-0.02	-C.08	-0.03	0.06	1.60
1.20	29.00	C.02	-0.02	-C.07	-0.02	0.05	1.68
1.25	28.11	0.03	-0.03	-C.06	0.01	0.13	1.75
1.30	27.21	C.04	-0.03	-C.05	0.03	0.17	1.81
1.35	26.30	C.05	-0.03	-C.04	0.03	0.21	1.85
1.40	25.37	0.06	-0.02	-C.03	0.01	0.25	1.89
1.45	24.43	C.07	-0.02	-C.03	-0.01	0.30	1.92
1.50	23.49	C.08	-0.02	-C.02	-0.01	0.34	1.93
1.55	22.56	0.09	-0.02	-C.00	0.00	0.38	1.93
1.60	21.63	C.10	-0.02	C.01	0.01	0.42	1.92
1.65	20.72	0.11	-0.02	C.02	0.00	0.46	1.87
1.70	19.82	0.12	-0.02	C.05	-0.00	0.49	1.85
1.75	18.95	0.13	-0.01	C.08	-0.00	0.52	1.90
1.80	18.05	0.14	-0.01	C.11	0.00	0.54	1.89
1.85	17.24	C.14	-0.01	C.14	-0.00	0.56	1.81
1.90	16.36	0.15	-0.02	C.15	-0.01	0.58	1.68
1.95	15.45	0.15	-0.02	C.15	-0.01	0.55	1.56

HSKI TRUCK AND TRACTOR-TRAILER DYNAMIC RESPONSE SIMULATION - TBCPS.VI  
 SAMPLE RUN - TRIPLES BRAKING IN A TURN, ALL OPTICS EXERCISED  
 TRAILER NO. 2 SPRING MASS ACCELERATION (PCDY AXES)

OUTPUT PAGE NO. 1.02.3

INERTIAL ACCEL. ALONG BODY AXES

TIME (SEC)	FORWARD (FT/SEC**2)	LATERAL (FT/SEC**2)	VERTICAL (FT/SEC**2)	ROLL (DEG/SEC**2)	PITCH (DEG/SEC**2)	HEADING (DEG/SEC**2)	LONGITUDINAL (FT/SEC**2)	LATERAL (FT/SEC**2)
0.0	0.0	0.0	0.0000	0.0	0.0001	0.0	-0.0	0.0
0.05	-0.0012	0.0000	-0.0000	-0.0004	-0.0002	0.0001	-0.0012	0.0000
0.10	-0.0140	0.0005	-0.0006	-0.0087	-0.0080	0.0031	-0.0140	0.0005
0.15	-0.1642	0.0000	-0.0151	0.0006	-0.2772	0.0018	-0.1642	0.0002
0.20	-1.8346	-0.0012	-0.1845	0.0273	-4.1241	-0.0084	-1.8346	-0.0012
0.25	-6.4135	-0.0031	0.6072	0.0597	-4.1522	-0.0237	-6.4134	-0.0036
0.30	-10.7117	-0.0075	0.6580	0.1304	0.2622	-0.0583	-10.7120	-0.0095
0.35	-11.6458	-0.0142	-1.0507	0.2066	2.0740	-0.1105	-11.6460	-0.0192
0.40	-13.1349	-0.0219	-0.8566	0.2449	5.3720	-0.1645	-13.1348	-0.0320
0.45	-13.7104	-0.0304	-0.1804	0.2181	2.1458	-0.2086	-13.7104	-0.0471
0.50	-13.4090	-0.0354	0.4625	0.1260	-1.1075	-0.2340	-13.4090	-0.0637
0.55	-13.1912	-0.0473	0.5224	-0.0191	-1.3819	-0.2364	-13.1912	-0.0795
0.60	-13.6612	-0.0510	-0.0045	-0.2153	0.2654	-0.2026	-13.6612	-0.0904
0.65	-14.6744	-0.0452	-0.4782	-0.4164	1.8462	-0.1344	-14.6744	-0.0937
0.70	-15.8739	-0.0422	-0.4388	-0.5584	1.6218	-0.0500	-15.8740	-0.0888
0.75	-17.0052	-0.0303	0.0008	-0.6040	-0.1501	0.0333	-17.0053	-0.0762
0.80	-17.5667	-0.0138	0.3674	-0.5564	-1.5420	0.1094	-17.5668	-0.0564
0.85	-18.5511	0.0070	0.3392	-0.4441	-1.2657	0.1814	-18.5511	-0.0300
0.90	-18.7456	0.0311	0.0172	-0.2903	0.0011	0.2513	-18.7456	0.0016
0.95	-18.0317	0.0572	-0.2337	-0.1154	0.7535	0.3178	-18.6317	0.0368
1.00	-18.4046	0.0643	-0.1568	0.0485	0.3256	0.3847	-18.4046	0.0744
1.05	-18.0082	0.1116	0.0216	0.1709	-0.4047	0.4592	-18.0082	0.1136
1.10	-17.6234	0.1374	0.1524	0.2458	-0.6881	0.5400	-17.6234	0.1528
1.15	-17.4676	0.1617	0.0841	0.2494	-0.2704	0.6313	-17.4676	0.1919
1.20	-17.5712	0.1811	-0.0650	0.2332	0.3720	0.7150	-17.5712	0.2275
1.25	-17.8289	0.1948	-0.1289	0.2123	0.6151	0.7761	-17.8289	0.2581
1.30	-18.1090	0.2043	-0.0406	0.1735	0.3055	0.8237	-18.1091	0.2846
1.35	-18.4591	0.2087	0.0902	0.1547	-0.2822	0.8476	-18.4593	0.3055
1.40	-18.7045	0.2106	0.1355	0.1470	-0.4792	0.8559	-18.7047	0.3225
1.45	-18.8061	0.2110	0.0732	0.1603	-0.2021	0.8521	-18.8064	0.3374
1.50	-18.7667	0.2108	-0.0240	0.2026	0.1478	0.8364	-18.7671	0.3496
1.55	-18.5933	0.2056	-0.0566	0.2672	0.2272	0.8101	-18.5938	0.3592
1.60	-18.3868	0.2065	-0.0107	0.3454	-0.0034	0.7713	-18.3875	0.3648
1.65	-18.0882	0.2015	0.0506	0.3893	-0.1481	0.7322	-18.0850	0.3672
1.70	-17.7015	0.1920	0.0620	0.4313	-0.0690	0.6843	-17.7025	0.3635
1.75	-17.2594	0.1665	0.0288	0.6918	0.1045	0.5117	-17.2605	0.3395
1.80	-16.9690	0.1355	-0.0116	0.7133	0.0891	0.3621	-16.9703	0.3118
1.85	-17.2311	0.1125	-0.0255	0.4043	-0.1910	0.3190	-17.2325	0.2823
1.90	-17.9199	0.0731	-0.0255	0.0629	-0.2124	0.2534	-17.9213	0.2375
1.95	-18.5862	0.0248	-0.0162	-0.2679	0.1557	0.1518	-18.5876	0.1826

LEFT SIDE

RIGHT SIDE

LEFT SIDE		RIGHT SIDE						
TIME (SEC)	VERTICAL (LB)	LONG. (LB)	LATERAL (LB)	VERTICAL (LB)	LONG. (LB)	LATERAL (LB)	MU-X	MU-Y
0.0	4325.00	-0.0	C.C	4325.00	-0.0	C.C	0.0	0.0
0.05	4325.00	0.01	C.C	4325.00	0.01	C.C	0.0000	0.0000
0.10	4325.08	0.09	C.C	4324.91	0.09	0.14	C.C	0.0000
0.15	4325.33	1.05	C.C	4325.10	1.09	C.C	0.0003	0.0000
0.20	4335.14	14.55	C.C	4339.42	14.55	-0.35	0.0034	-0.0001
0.25	4445.52	-244.73	-1.06	4450.70	-244.79	-1.06	-0.0050	-0.0002
0.30	4773.63	-918.53	-2.72	4777.30	-918.75	-2.72	-0.1923	-0.0006
0.35	5181.02	-1112.89	-5.15	5189.15	-1113.23	-5.20	-0.2145	-0.0010
0.40	5412.52	-1511.76	-7.54	5426.88	-1512.41	-7.96	-0.2787	-0.0015
0.45	5436.43	-1838.42	-10.42	5458.32	-1839.31	-10.46	-0.3370	-0.0019
0.50	5405.73	-2057.07	-12.32	5435.82	-2098.10	-12.39	-0.3860	-0.0023
0.55	5463.68	-2259.50	-13.46	5501.89	-2300.42	-13.56	-0.4181	-0.0025
0.60	5610.05	-2442.65	-13.36	5654.65	-2443.22	-13.48	-0.4321	-0.0024
0.65	5735.59	-2533.27	-12.02	5783.47	-2533.52	-12.13	-0.4381	-0.0021
0.70	5750.54	-2589.57	-9.77	5797.71	-2589.53	-9.86	-0.4466	-0.0017
0.75	5674.21	-2630.27	-6.82	5716.00	-2629.86	-6.85	-0.4601	-0.0012
0.80	5605.07	-2664.72	-3.10	5636.48	-2663.80	-3.13	-0.4726	-0.0006
0.85	5615.88	-2695.23	1.61	5632.04	-2693.87	1.60	-0.4783	0.0003
0.90	5690.02	-2718.70	7.16	5687.03	-2717.13	7.15	-0.4778	0.0013
0.95	5756.70	-2735.37	13.15	5732.32	-2733.72	13.09	-0.4769	0.0023
1.00	5772.51	-2747.90	19.25	5726.11	-2746.21	15.14	-0.4796	0.0033
1.05	5757.04	-2761.74	25.44	5689.28	-2760.05	25.14	-0.4851	0.0044
1.10	5754.43	-2775.39	31.26	5667.22	-2773.83	30.78	-0.4895	0.0054
1.15	5784.08	-2784.82	36.95	5679.58	-2783.41	36.27	-0.4901	0.0064
1.20	5824.34	-2788.07	41.91	5705.27	-2786.80	41.01	-0.4885	0.0072
1.25	5840.91	-2786.53	45.50	5710.40	-2785.31	44.75	-0.4878	0.0078
1.30	5824.13	-2783.79	49.37	5684.30	-2782.58	48.04	-0.4895	0.0085
1.35	5795.09	-2781.66	51.52	5648.38	-2780.57	50.36	-0.4923	0.0089
1.40	5782.37	-2781.10	53.59	5631.05	-2780.18	51.79	-0.4937	0.0092
1.45	5753.43	-2781.41	54.16	5639.93	-2780.67	52.15	-0.4930	0.0092
1.50	5812.02	-2782.35	53.27	5659.40	-2781.75	51.04	-0.4915	0.0090
1.55	5818.29	-2783.82	50.74	5670.11	-2783.35	48.32	-0.4909	0.0085
1.60	5838.93	-2786.25	46.49	5669.34	-2785.93	43.88	-0.4914	0.0077
1.65	5795.88	-2790.04	41.02	5669.07	-2789.86	38.19	-0.4921	0.0067
1.70	5789.29	-2794.77	33.82	5679.56	-2794.78	30.71	-0.4921	0.0054
1.75	5784.38	-2800.25	20.65	5702.64	-2800.79	17.30	-0.4911	0.0030
1.80	5775.37	-2804.00	8.16	5725.95	-2804.54	4.45	-0.4899	0.0008
1.85	5761.84	-2801.58	C.27	5743.38	-2802.07	-4.02	-0.4879	-0.0007
1.90	5746.95	-2794.07	-6.48	5761.01	-2794.55	-11.53	-0.4851	-0.0020
1.95	5731.94	-2785.70	-12.24	5777.41	-2786.10	-16.22	-0.4822	-0.0032

FSPI TRUCK AND TRAILER-TRAILER DYNAMIC RESPONSE SIMULATION - TBCRS, VI  
 TRAILER NO. 2 REAR SUSPENSION TIRE FORCES  
 LEADING TANDEM AXLE

TIME (SEC)	LEFT SIDE				RIGHT SIDE					
	VERTICAL (LB)	LONG. (LB)	LATERAL (LB)	MU-X	MU-Y	VERTICAL (LB)	LONG. (LB)	LATERAL (LB)	MU-X	MU-Y
0.0	2162.50	-0.0	C.C	C.C	C.C	2162.50	-0.0	0.0	C.C	0.0
0.05	2162.50	C.01	-C.00	0.0030	-C.0000	2162.50	0.01	-0.00	C.C000	-0.0000
0.10	2162.49	0.08	-C.C2	C.C000	-C.0000	2162.50	0.09	-0.02	C.C000	-0.0000
0.15	2162.52	-3.48	-C.C3	-C.C016	-C.0000	2162.52	-3.48	0.03	-0.0000	-0.0000
0.20	2196.48	-173.40	C.05	-0.0000	C.C000	2196.38	-173.40	0.05	-0.0000	0.0000
0.25	2754.38	-576.32	C.17	-C.0000	C.C001	2754.22	-576.32	C.17	-0.0000	0.0000
0.30	2420.88	-997.88	C.45	-0.0000	C.C002	2420.72	-997.94	C.45	-0.0000	0.0002
0.35	2577.20	-1330.37	C.50	-0.0000	C.C003	2577.15	-1330.52	C.90	-0.0000	0.0003
0.40	2636.73	-1572.34	1.35	-0.0000	C.C005	2637.52	-1572.65	1.35	-0.0000	0.0005
0.45	2723.02	-1758.49	1.65	-C.0000	C.C006	2725.45	-1758.96	1.66	-0.0000	0.0006
0.50	2784.17	-1901.83	1.65	-C.0000	C.C006	2789.11	-1902.43	1.69	-0.0000	0.0006
0.55	2837.02	-2017.41	1.46	-C.0000	C.C005	2844.97	-2013.05	1.46	-0.0000	0.0005
0.60	2886.17	-2087.09	C.96	-0.0000	C.C005	2897.18	-2087.66	C.96	-0.0000	0.0003
0.65	2915.26	-2133.09	0.24	-C.0000	C.C001	2932.79	-2133.48	C.24	-0.0000	0.0001
0.70	2936.62	-2161.09	-0.48	-C.0000	C.C002	2951.30	-2161.20	-0.48	-0.0000	-0.0002
0.75	2946.09	-2179.43	-C.56	-0.0000	C.C003	2960.00	-2179.42	-C.97	-0.0000	-0.0003
0.80	2955.57	-2192.07	-C.59	-C.0004	C.C004	2966.62	-2191.57	-1.12	-0.0004	-0.0004
0.85	2964.87	-2202.72	-C.59	-C.0003	C.C003	2976.31	-2201.99	-1.00	-0.0004	-0.0004
0.90	2986.98	-2212.57	-C.65	-C.0002	C.C002	2987.55	-2212.10	-0.65	-0.0002	-0.0002
0.95	2994.60	-2223.27	-0.36	-C.0001	C.C001	2993.83	-2222.32	-C.36	-0.0001	-0.0001
1.00	3002.87	-2232.20	-0.21	-C.0001	C.C001	2990.96	-2231.25	-C.20	-0.0001	-0.0001
1.05	3006.14	-2242.40	-0.51	-C.0002	C.C002	2983.12	-2241.49	-C.51	-0.0002	-0.0002
1.10	2999.51	-2251.63	-1.43	-C.0005	C.C005	2978.92	-2250.78	-1.42	-C.0005	-0.0005
1.15	3001.93	-2257.28	-3.13	-C.0010	C.C010	2979.63	-2256.50	-3.11	-C.0010	-0.0010
1.20	3004.54	-2258.57	-5.62	-C.0019	C.C019	2982.43	-2258.21	-5.55	-C.0019	-0.0019
1.25	3004.95	-2257.51	-8.67	-0.0029	C.C029	2984.42	-2256.77	-8.62	-0.0029	-0.0029
1.30	3003.08	-2254.58	-12.34	-C.0041	C.C041	2985.59	-2254.27	-12.27	-C.0041	-0.0041
1.35	3000.58	-2251.55	-16.48	-C.0055	C.C055	2987.31	-2251.25	-16.42	-0.0055	-0.0055
1.40	2998.86	-2245.82	-21.06	-C.0070	C.C070	2990.82	-2245.15	-21.02	-0.0070	-0.0070
1.45	2994.10	-2248.52	-26.10	-C.0087	C.C087	2996.45	-2248.28	-26.12	-0.0087	-0.0087
1.50	2996.34	-2249.59	-31.61	-C.0105	C.C105	3002.25	-2249.00	-31.72	-0.0105	-0.0105
1.55	2992.48	-2251.42	-37.57	-C.0126	C.C126	3007.34	-2250.90	-37.83	-0.0126	-0.0126
1.60	2985.75	-2254.01	-43.58	-C.0147	C.C147	3011.05	-2253.57	-44.45	-0.0147	-0.0147
1.65	2978.05	-2257.65	-50.94	-C.0171	C.C171	3015.71	-2257.29	-51.71	-0.0171	-0.0171
1.70	2971.29	-2262.15	-58.58	-C.0197	C.C197	3023.63	-2261.88	-59.77	-0.0197	-0.0197
1.75	2966.26	-2267.87	-65.47	-C.0221	C.C221	3033.86	-2267.69	-67.15	-0.0221	-0.0221
1.80	2960.92	-2271.54	-72.33	-C.0244	C.C244	3045.16	-2271.64	-74.62	-0.0244	-0.0244
1.85	2949.23	-2268.84	-80.50	-C.0274	C.C274	3054.96	-2269.04	-84.09	-0.0274	-0.0274
1.90	2931.80	-2261.12	-90.00	-C.0307	C.C307	3060.45	-2261.25	-94.25	-0.0307	-0.0307
1.95	2915.35	-2252.86	-98.86	-C.0339	C.C339	3066.07	-2252.53	-104.38	-0.0339	-0.0339



HSRI TRUCK AND TRACTOR-TRAILER DYNAMIC RESPONSE SIMULATION - TBCRS.VI  
 SAMPLE RUN - TRIPLES BRAKING IN A TURN, ALL OPTIONS EXERCISED  
 TRAILER NO. 2 REAR SUSPENSION TIRE FORCES  
 TRAILING TANDEM AXLE

OUTPUT PAGE NO. 1.06.3

TIME (SEC)	LEFT SIDE					RIGHT SIDE				
	VERTICAL (LB)	LONG. (LB)	LATERAL (LB)	MU-X	MU-Y	VERTICAL (LB)	LONG. (LB)	LATERAL (LB)	MU-X	MU-Y
0.0	2162.50	-0.0	0.0	0.0	0.0	2162.50	-0.0	0.0	0.0	0.0
0.05	2162.50	0.01	-0.00	0.0000	-0.0000	2162.50	0.01	-0.00	0.0000	-0.0000
0.10	2162.49	0.08	-0.01	0.0000	-0.0000	2162.49	0.09	-0.01	0.0000	-0.0000
0.15	2161.99	-3.48	-0.00	-0.0016	-0.0000	2161.96	-3.48	-0.00	-0.0016	-0.0000
0.20	2116.74	-170.19	0.05	-0.0804	0.0000	2116.62	-170.19	0.05	-0.0804	0.0000
0.25	1935.98	-547.77	0.08	-0.2830	0.0000	1935.86	-547.79	0.08	-0.2830	0.0000
0.30	1848.23	-953.85	0.09	-0.5161	0.0000	1848.58	-953.97	0.09	-0.5161	0.0000
0.35	1833.77	-1287.67	-0.01	-0.7027	-0.0000	1835.17	-1288.05	-0.01	-0.7019	-0.0000
0.40	1774.23	-1536.20	-0.37	-0.8658	-0.0002	1777.62	-1537.03	-0.37	-0.8647	-0.0002
0.45	1797.16	-1737.54	-1.12	-0.9725	-0.0006	1793.80	-1739.21	-1.13	-0.9696	-0.0006
0.50	1785.27	-1982.73	-2.24	-1.0546	-0.0013	1796.19	-1884.41	-2.26	-1.0491	-0.0013
0.55	1780.93	-1998.35	-3.63	-1.1221	-0.0020	1796.51	-2000.22	-3.66	-1.1134	-0.0020
0.60	1785.68	-2080.18	-5.16	-1.1649	-0.0029	1806.02	-2081.86	-5.22	-1.1527	-0.0029
0.65	1792.06	-2131.65	-6.61	-1.1895	-0.0037	1816.01	-2132.77	-6.69	-1.1744	-0.0037
0.70	1797.30	-2162.89	-7.69	-1.2034	-0.0043	1822.93	-2163.21	-7.80	-1.1867	-0.0043
0.75	1799.41	-2182.43	-8.20	-1.2129	-0.0046	1824.25	-2181.89	-8.31	-1.1960	-0.0046
0.80	1799.15	-2194.84	-8.08	-1.2206	-0.0045	1819.68	-2193.51	-8.17	-1.2054	-0.0045
0.85	1798.99	-2206.54	-7.37	-1.2265	-0.0041	1814.99	-2204.56	-7.43	-1.2146	-0.0041
0.90	1806.14	-2218.60	-6.14	-1.2284	-0.0034	1814.89	-2216.14	-6.17	-1.2211	-0.0034
0.95	1815.83	-2229.67	-4.41	-1.2279	-0.0024	1816.10	-2226.98	-4.41	-1.2262	-0.0024
1.00	1820.46	-2237.64	-2.27	-1.2292	-0.0012	1811.62	-2234.98	-2.26	-1.2336	-0.0012
1.05	1818.56	-2246.63	0.17	-1.2355	0.0001	1800.54	-2244.07	0.17	-1.2463	0.0001
1.10	1816.93	-2256.16	2.90	-1.2417	0.0016	1789.94	-2253.47	2.86	-1.2590	0.0016
1.15	1818.38	-2262.75	5.93	-1.2444	0.0033	1782.71	-2260.17	5.81	-1.2678	0.0033
1.20	1823.15	-2265.55	9.38	-1.2427	0.0051	1778.86	-2263.03	9.15	-1.2722	0.0051
1.25	1829.64	-2264.64	13.35	-1.2377	0.0073	1776.58	-2262.19	12.97	-1.2733	0.0073
1.30	1835.92	-2262.15	17.76	-1.2322	0.0097	1774.02	-2259.91	17.17	-1.2738	0.0097
1.35	1840.91	-2258.78	22.64	-1.2270	0.0123	1769.92	-2256.45	21.78	-1.2749	0.0123
1.40	1845.08	-2256.53	27.95	-1.2230	0.0151	1764.82	-2254.31	26.76	-1.2774	0.0152
1.45	1850.25	-2255.65	33.66	-1.2191	0.0182	1760.59	-2253.57	32.07	-1.2800	0.0182
1.50	1856.11	-2256.28	39.74	-1.2156	0.0214	1757.02	-2254.39	37.67	-1.2831	0.0214
1.55	1861.98	-2257.95	46.17	-1.2127	0.0248	1753.68	-2256.28	43.51	-1.2866	0.0248
1.60	1865.52	-2260.02	52.68	-1.2115	0.0282	1748.62	-2258.58	49.48	-1.2916	0.0283
1.65	1867.65	-2263.44	59.32	-1.2119	0.0318	1743.05	-2262.31	55.49	-1.2979	0.0318
1.70	1870.89	-2267.85	66.11	-1.2122	0.0353	1739.55	-2267.03	61.63	-1.3032	0.0354
1.75	1876.13	-2273.54	73.29	-1.2118	0.0391	1738.92	-2273.20	68.11	-1.3072	0.0392
1.80	1880.93	-2276.55	79.34	-1.2106	0.0422	1741.22	-2277.56	73.68	-1.3080	0.0423
1.85	1879.28	-2273.56	83.86	-1.2100	0.0446	1741.13	-2274.87	77.96	-1.3065	0.0448
1.90	1871.23	-2266.23	88.30	-1.2111	0.0472	1735.06	-2267.11	82.17	-1.3066	0.0474
1.95	1864.53	-2258.44	93.29	-1.2113	0.0500	1729.17	-2259.36	86.86	-1.3066	0.0502







HSRI TRUCK AND TRACTOR-TRAILER DYNAMIC RESPONSE SIMULATION - TDRS.VI

SAMPLE RUN - TRIPLES BRAKING IN A TURN, ALL OPTIONS EXERCISED  
 TRAILER NO. 2 FRONT SUSPENSION - LATERAL TIRE FORCE AND MOMENT SUMMARY  
 LEFT SIDE

TIME (SEC)	TIRE SICESLIP ANGLE (DEG)	TIRE LATERAL FORCE (LB)	MU-Y	ALIGNING TORQUE (IN-LB)	TIRE SICESLIP ANGLE (DEG)	TIRE LATERAL FORCE (LB)	MU-Y	ALIGNING TORQUE (IN-LB)
0.0	0.0	0.0	C.0	0.0	0.0	0.0	0.0	0.0
0.05	-0.0000	0.0069	C.0000	0.0	-0.0000	0.0069	C.0000	0.0
0.10	-0.0001	0.1465	C.0000	0.0	-0.0001	0.1465	C.0000	0.0
0.15	-0.0001	0.0739	0.0000	0.0	-0.0001	0.0739	0.0000	0.0
0.20	0.0003	-0.3527	-0.0001	0.0	0.0003	-0.3527	-0.0001	0.0
0.25	0.0009	-1.0575	-0.0002	0.0	0.0009	-1.0575	-0.0002	0.0
0.30	0.0021	-2.7204	-0.0006	0.0	0.0021	-2.7204	-0.0006	0.0
0.35	0.0036	-5.1944	-0.0010	0.0	0.0036	-5.2027	-0.0010	0.0
0.40	0.0053	-7.9378	-0.0015	0.0	0.0053	-7.9592	-0.0015	0.0
0.45	0.0069	-10.4174	-0.0019	0.0	0.0069	-10.4606	-0.0019	0.0
0.50	0.0082	-12.3150	-0.0023	0.0	0.0082	-12.3863	-0.0023	0.0
0.55	0.0089	-13.4568	-0.0025	0.0	0.0085	-13.5559	-0.0025	0.0
0.60	0.0086	-13.3633	-0.0024	0.0	0.0086	-13.4775	-0.0024	0.0
0.65	0.0076	-12.0155	-0.0021	0.0	0.0076	-12.1269	-0.0021	0.0
0.70	0.0061	-9.7668	-0.0017	0.0	0.0061	-9.8600	-0.0017	0.0
0.75	0.0043	-6.8232	-0.0012	0.0	0.0043	-6.8871	-0.0012	0.0
0.80	0.0020	-3.1015	-0.0006	0.0	0.0020	-3.1319	-0.0006	0.0
0.85	-0.0010	1.6075	0.0002	0.0	-0.0010	1.6020	0.0003	0.0
0.90	-0.0045	7.1644	0.0013	0.0	-0.0045	7.1531	0.0013	0.0
0.95	-0.0082	13.1531	0.0022	0.0	-0.0082	13.0934	0.0023	0.0
1.00	-0.0120	19.2927	0.0032	0.0	-0.0120	19.1366	0.0033	0.0
1.05	-0.0159	25.4351	0.0044	0.0	-0.0155	25.1396	0.0044	0.0
1.10	-0.0196	31.2612	0.0054	0.0	-0.0196	30.7840	0.0054	0.0
1.15	-0.0230	36.9525	0.0064	0.0	-0.0230	36.2706	0.0064	0.0
1.20	-0.0259	41.5113	0.0072	0.0	-0.0259	41.0148	0.0072	0.0
1.25	-0.0283	45.5008	0.0075	0.0	-0.0283	44.7915	0.0078	0.0
1.30	-0.0306	49.3741	0.0085	0.0	-0.0305	48.0354	0.0085	0.0
1.35	-0.0323	51.9225	0.0090	0.0	-0.0321	50.3554	0.0089	0.0
1.40	-0.0334	53.5857	0.0092	0.0	-0.0332	51.7944	0.0092	0.0
1.45	-0.0337	54.1622	0.0093	0.0	-0.0333	52.1466	0.0092	0.0
1.50	-0.0330	52.2655	0.0092	0.0	-0.0325	51.0437	0.0090	0.0
1.55	-0.0314	50.7363	0.0087	0.0	-0.0307	49.3182	0.0085	0.0
1.60	-0.0288	46.4866	0.0080	0.0	-0.0275	43.8755	0.0077	0.0
1.65	-0.0255	41.0177	0.0071	0.0	-0.0242	38.1855	0.0067	0.0
1.70	-0.0211	33.8182	0.0058	0.0	-0.0195	30.7135	0.0054	0.0
1.75	-0.0129	20.6474	0.0036	0.0	-0.0109	17.3029	0.0030	0.0
1.80	-0.0051	8.1583	0.0014	0.0	-0.0028	4.4456	0.0008	0.0
1.85	-0.0002	0.2726	0.0000	0.0	0.0025	-4.0025	-0.0007	0.0
1.90	0.0041	-6.4818	-0.0011	0.0	0.0072	-11.5341	-0.0020	0.0
1.95	0.0077	-12.2417	-0.0021	0.0	0.0114	-18.2169	-0.0032	0.0

TIME (SEC)	LEFT SIDE					RIGHT SIDE				
	TIRE SIDESLIP ANGLE (DEG)	TIRE LATERAL FORCE (LB)	MU-Y	ALIGNING TORQUE (IN-LB)	TIRE SIDESLIP ANGLE (DEG)	TIRE LATERAL FORCE (LB)	MU-Y	ALIGNING TORQUE (IN-LB)		
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		
0.05	0.000	-0.0000	-0.0000	0.0000	0.0000	-0.0000	0.0000	0.0000		
0.10	0.000	-0.0102	-0.0000	0.0000	0.0000	-0.0102	0.0000	0.0000		
0.15	0.000	-0.0205	-0.0000	0.0000	0.0000	-0.0205	0.0000	0.0000		
0.20	-0.0000	0.0456	0.0000	-0.0000	0.0456	0.0000	0.0000	0.0000		
0.25	-0.0001	0.1709	0.0001	-0.0001	0.1709	0.0001	0.0001	0.0001		
0.30	-0.0003	0.4463	0.0002	-0.0002	0.4463	0.0002	0.0002	0.0002		
0.35	-0.0006	0.8585	0.0003	-0.0003	0.8585	0.0003	0.0003	0.0003		
0.40	-0.0009	1.3487	0.0005	-0.0005	1.3487	0.0005	0.0005	0.0005		
0.45	-0.0011	1.6543	0.0006	-0.0006	1.6543	0.0006	0.0006	0.0006		
0.50	-0.0011	1.6876	0.0006	-0.0006	1.6876	0.0006	0.0006	0.0006		
0.55	-0.0009	1.4604	0.0005	-0.0005	1.4604	0.0005	0.0005	0.0005		
0.60	-0.0006	0.5556	0.0003	-0.0003	0.5556	0.0003	0.0003	0.0003		
0.65	-0.0001	0.2402	0.0001	-0.0001	0.2402	0.0001	0.0001	0.0001		
0.70	0.0003	-0.4765	-0.0002	0.0002	-0.4765	-0.0002	0.0002	0.0002		
0.75	0.0006	-0.5640	-0.0003	0.0003	-0.5640	-0.0003	0.0003	0.0003		
0.80	0.0007	-1.1200	-0.0004	0.0004	-1.1200	-0.0004	0.0004	0.0004		
0.85	0.0006	-0.5575	-0.0003	0.0003	-0.5575	-0.0003	0.0003	0.0003		
0.90	0.0004	-0.6935	-0.0002	0.0002	-0.6935	-0.0002	0.0002	0.0002		
0.95	0.0002	-0.3560	-0.0001	0.0001	-0.3560	-0.0001	0.0001	0.0001		
1.00	0.0001	-0.2054	-0.0001	0.0001	-0.2054	-0.0001	0.0001	0.0001		
1.05	0.0003	-0.5059	-0.0002	0.0002	-0.5059	-0.0002	0.0002	0.0002		
1.10	0.0009	-1.4278	-0.0005	0.0005	-1.4278	-0.0005	0.0005	0.0005		
1.15	0.0019	-3.1331	-0.0010	0.0010	-3.1331	-0.0010	0.0010	0.0010		
1.20	0.0034	-5.6248	-0.0019	0.0019	-5.6248	-0.0019	0.0019	0.0019		
1.25	0.0052	-8.6735	-0.0029	0.0029	-8.6735	-0.0029	0.0029	0.0029		
1.30	0.0074	-12.3374	-0.0041	0.0041	-12.3374	-0.0041	0.0041	0.0041		
1.35	0.0099	-16.4808	-0.0055	0.0055	-16.4808	-0.0055	0.0055	0.0055		
1.40	0.0127	-21.0554	-0.0070	0.0070	-21.0554	-0.0070	0.0070	0.0070		
1.45	0.0157	-26.1028	-0.0087	0.0087	-26.1028	-0.0087	0.0087	0.0087		
1.50	0.0190	-31.6063	-0.0105	0.0105	-31.6063	-0.0105	0.0105	0.0105		
1.55	0.0226	-37.5737	-0.0126	0.0126	-37.5737	-0.0126	0.0126	0.0126		
1.60	0.0265	-43.9832	-0.0147	0.0147	-43.9832	-0.0147	0.0147	0.0147		
1.65	0.0308	-50.5421	-0.0171	0.0171	-50.5421	-0.0171	0.0171	0.0171		
1.70	0.0355	-58.5848	-0.0197	0.0197	-58.5848	-0.0197	0.0197	0.0197		
1.75	0.0398	-65.4674	-0.0221	0.0221	-65.4674	-0.0221	0.0221	0.0221		
1.80	0.0440	-72.3281	-0.0244	0.0244	-72.3281	-0.0244	0.0244	0.0244		
1.85	0.0494	-80.5025	-0.0274	0.0274	-80.5025	-0.0274	0.0274	0.0274		
1.90	0.0553	-89.9558	-0.0307	0.0307	-89.9558	-0.0307	0.0307	0.0307		
1.95	0.0611	-98.8557	-0.0335	0.0335	-98.8557	-0.0335	0.0335	0.0335		

HEMT TRUCK AND TRACTOR-TRAILER DYNAMIC RESPONSE SIMULATION - TERS.VI  
 SAMPLE RUN - TRIPLES BRAKING IN A TURN, ALL OPTICNS EXERCISED  
 TRAILER NO. 2 REAR SUSPENSION - LATERAL TIRE FORCE AND MOMENT SUMMARY  
 TRAILING TANDEM AXLE

TIME (SEC)	LEFT SIDE					RIGHT SIDE					ALIGNING TORQUE (IN-LB)
	TIRE SIDESLIP ANGLE (DEG)	TIRE LATERAL FORCE (LB)	MU-Y	ALIGNING TORQUE (IN-LB)	TIRE SIDESLIP ANGLE (DEG)	TIRE LATERAL FORCE (LB)	MU-Y	ALIGNING TORQUE (IN-LB)			
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.05	0.0000	-0.0002	-0.0000	0.0	0.0000	-0.0002	-0.0000	0.0	0.0000	-0.0000	0.0
0.10	0.0000	-0.0055	-0.0000	0.0	0.0000	-0.0055	-0.0000	0.0	0.0000	-0.0000	0.0
0.15	0.0000	-0.0011	-0.0000	0.0	0.0000	-0.0011	-0.0000	0.0	0.0000	-0.0000	0.0
0.20	-0.0000	0.0531	0.0000	0.0	-0.0000	0.0531	0.0000	0.0	0.0000	0.0000	0.0
0.25	-0.0001	0.0807	0.0000	0.0	-0.0001	0.0807	0.0000	0.0	0.0000	0.0000	0.0
0.30	-0.0001	0.0924	0.0000	0.0	-0.0001	0.0924	0.0000	0.0	0.0000	0.0000	0.0
0.35	0.0000	-0.0004	-0.0000	0.0	0.0000	-0.0004	-0.0000	0.0	0.0000	-0.0000	0.0
0.40	0.0004	-0.3718	-0.0002	0.0	0.0004	-0.3718	-0.0002	0.0	0.0004	-0.0002	0.0
0.45	0.0011	-1.1223	-0.0006	0.0	0.0011	-1.1223	-0.0006	0.0	0.0011	-0.0006	0.0
0.50	0.0023	-2.2428	-0.0013	0.0	0.0023	-2.2428	-0.0013	0.0	0.0023	-0.0013	0.0
0.55	0.0037	-3.6261	-0.0020	0.0	0.0037	-3.6261	-0.0020	0.0	0.0037	-0.0020	0.0
0.60	0.0052	-5.1585	-0.0029	0.0	0.0052	-5.1585	-0.0029	0.0	0.0052	-0.0029	0.0
0.65	0.0066	-6.6064	-0.0037	0.0	0.0066	-6.6064	-0.0037	0.0	0.0066	-0.0037	0.0
0.70	0.0077	-7.6871	-0.0043	0.0	0.0077	-7.6871	-0.0043	0.0	0.0077	-0.0043	0.0
0.75	0.0082	-8.1585	-0.0046	0.0	0.0082	-8.1585	-0.0046	0.0	0.0082	-0.0046	0.0
0.80	0.0081	-8.0750	-0.0045	0.0	0.0081	-8.0750	-0.0045	0.0	0.0081	-0.0045	0.0
0.85	0.0074	-7.3702	-0.0041	0.0	0.0074	-7.3702	-0.0041	0.0	0.0074	-0.0041	0.0
0.90	0.0061	-6.1383	-0.0034	0.0	0.0061	-6.1383	-0.0034	0.0	0.0061	-0.0034	0.0
0.95	0.0044	-4.4115	-0.0024	0.0	0.0044	-4.4115	-0.0024	0.0	0.0044	-0.0024	0.0
1.00	0.0023	-2.2730	-0.0012	0.0	0.0023	-2.2730	-0.0012	0.0	0.0023	-0.0012	0.0
1.05	-0.0002	0.1689	0.0001	0.0	-0.0002	0.1689	0.0001	0.0	-0.0002	0.0001	0.0
1.10	-0.0029	2.8983	0.0010	0.0	-0.0029	2.8983	0.0010	0.0	-0.0029	0.0010	0.0
1.15	-0.0059	5.9281	0.0022	0.0	-0.0059	5.9281	0.0022	0.0	-0.0059	0.0022	0.0
1.20	-0.0093	9.3754	0.0051	0.0	-0.0093	9.3754	0.0051	0.0	-0.0093	0.0051	0.0
1.25	-0.0131	13.3488	0.0073	0.0	-0.0131	13.3488	0.0073	0.0	-0.0131	0.0073	0.0
1.30	-0.0174	17.7595	0.0097	0.0	-0.0174	17.7595	0.0097	0.0	-0.0174	0.0097	0.0
1.35	-0.0222	22.6386	0.0123	0.0	-0.0222	22.6386	0.0123	0.0	-0.0222	0.0123	0.0
1.40	-0.0273	27.9453	0.0151	0.0	-0.0273	27.9453	0.0151	0.0	-0.0273	0.0151	0.0
1.45	-0.0328	33.6567	0.0182	0.0	-0.0328	33.6567	0.0182	0.0	-0.0328	0.0182	0.0
1.50	-0.0396	39.7382	0.0214	0.0	-0.0396	39.7382	0.0214	0.0	-0.0396	0.0214	0.0
1.55	-0.0466	46.1200	0.0248	0.0	-0.0466	46.1200	0.0248	0.0	-0.0466	0.0248	0.0
1.60	-0.0509	52.6790	0.0282	0.0	-0.0509	52.6790	0.0282	0.0	-0.0509	0.0282	0.0
1.65	-0.0572	59.3214	0.0316	0.0	-0.0572	59.3214	0.0316	0.0	-0.0572	0.0316	0.0
1.70	-0.0637	66.1098	0.0353	0.0	-0.0637	66.1098	0.0353	0.0	-0.0637	0.0353	0.0
1.75	-0.0704	73.2758	0.0391	0.0	-0.0704	73.2758	0.0391	0.0	-0.0704	0.0391	0.0
1.80	-0.0760	79.3406	0.0422	0.0	-0.0760	79.3406	0.0422	0.0	-0.0760	0.0422	0.0
1.85	-0.0804	83.8646	0.0446	0.0	-0.0804	83.8646	0.0446	0.0	-0.0804	0.0446	0.0
1.90	-0.0850	88.2958	0.0472	0.0	-0.0850	88.2958	0.0472	0.0	-0.0850	0.0472	0.0
1.95	-0.0902	93.2505	0.0500	0.0	-0.0902	93.2505	0.0500	0.0	-0.0902	0.0500	0.0







HSPI TRUCK AND TRAILER-TRAILER DYNAMIC RESPONSE SIMULATION - TRDRS.V1  
 SAMPLE RUN - TRIPLES BRAKING IN A TURN, ALL OPTIONS EXERCISED  
 TRAILER NO. 2 REAR SUSPENSION - UNSPRUNG MASS SUMMARY  
 TRAILING TANDEM AXLE

OUTPUT PAGE NO. 1.18.3

TIME (SEC)	AXLE POSITION			VELOCITY			LEFT SIDE			RIGHT SIDE		
	VERTICAL (FT)	ROLL (DEG)	VERTICAL (FT/SEC)	RCLL (DEG/SEC)	AUXILIARY ROLL TORQUE (IN-LB)	SUSP. DEFLECT. (IN)	SUSP. VELOCITY (IN/SEC)	SUSP. FORCE (LB)	SUSP. DEFLECT. (IN)	SUSP. VELOCITY (IN/SEC)	SUSP. FORCE (LB)	
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.00	0.0	0.0	0.00	
0.05	0.0	-0.0000	0.0	0.0000	0.0	-0.0000	0.0000	0.00	-0.0000	0.0000	0.00	
0.10	-0.0000	0.0000	-0.0000	-0.0000	0.12	0.0000	0.0002	0.03	0.0000	0.0004	0.05	
0.15	-0.0000	0.0000	-0.0000	-0.0001	0.75	0.0001	0.0042	2.74	0.0001	0.0044	2.78	
0.20	-0.0004	0.0000	-0.0004	-0.0001	1.03	0.0012	0.1411	60.55	0.0013	0.1410	60.54	
0.25	-0.0020	0.0000	-0.0035	0.0004	-0.60	0.0212	0.7328	220.97	0.0212	0.7315	220.83	
0.30	-0.0025	0.0000	-0.0031	0.0010	-0.97	0.0580	0.6260	306.67	0.0575	0.6221	306.16	
0.35	-0.0030	0.0001	-0.0125	0.0026	-23.00	0.0793	0.2911	338.30	0.0789	0.2826	337.10	
0.40	-0.0036	0.0003	-0.0031	0.0046	-53.75	0.0938	0.1992	378.47	0.0928	0.1844	376.21	
0.45	-0.0035	0.0006	-0.0025	0.0082	-101.87	0.0980	-0.1151	376.53	0.0962	-0.1363	373.40	
0.50	-0.0034	0.0010	-0.0012	0.0082	-165.45	0.0873	-0.2799	374.61	0.0842	-0.3061	369.77	
0.55	-0.0035	0.0014	0.0000	0.0087	-238.16	0.0714	-0.3293	376.03	0.0670	-0.3571	370.14	
0.60	-0.0034	0.0018	0.0016	0.0078	-305.03	0.0531	-0.3922	370.02	0.0474	-0.4168	363.64	
0.65	-0.0033	0.0021	0.0014	0.0052	-362.96	0.0328	-0.4344	361.80	0.0260	-0.4501	355.71	
0.70	-0.0033	0.0023	0.0000	0.0012	-388.54	0.0117	-0.4344	355.36	0.0044	-0.4364	350.48	
0.75	-0.0032	0.0022	-0.0001	-0.0034	-372.29	-0.0087	-0.3882	352.71	-0.0157	-0.3737	349.82	
0.80	-0.0033	0.0019	-0.0007	-0.0078	-311.40	-0.0266	-0.3108	353.78	-0.0325	-0.2797	353.43	
0.85	-0.0033	0.0015	0.0001	-0.0114	-208.89	-0.0411	-0.2530	353.82	-0.0452	-0.2075	356.27	
0.90	-0.0033	0.0008	0.0010	-0.0141	-73.01	-0.0536	-0.2420	349.22	-0.0552	-0.1861	354.43	
0.95	-0.0032	0.0001	0.0000	-0.0158	84.36	-0.0656	-0.2421	343.16	-0.0642	-0.1806	350.88	
1.00	-0.0032	-0.0007	-0.0000	-0.0165	245.90	-0.0766	-0.1968	342.38	-0.0721	-0.1347	352.15	
1.05	-0.0033	-0.0016	-0.0013	-0.0163	411.18	-0.0845	-0.1156	347.25	-0.0769	-0.0571	358.56	
1.10	-0.0033	-0.0024	-0.0000	-0.0158	558.36	-0.0887	-0.0492	352.58	-0.0784	0.0025	364.92	
1.15	-0.0034	-0.0031	-0.0000	-0.0152	685.34	-0.0905	-0.0197	355.19	-0.0778	0.0239	368.17	
1.20	-0.0033	-0.0039	0.0000	-0.0155	790.76	-0.0915	-0.0224	354.66	-0.0767	0.0132	368.02	
1.25	-0.0032	-0.0047	0.0004	-0.0157	875.16	-0.0927	-0.0357	352.67	-0.0764	-0.0077	366.21	
1.30	-0.0033	-0.0055	0.0000	-0.0160	940.83	-0.0945	-0.0431	350.88	-0.0765	-0.0216	364.51	
1.35	-0.0033	-0.0063	-0.0001	-0.0164	990.28	-0.0966	-0.0369	350.40	-0.0781	-0.0210	364.00	
1.40	-0.0033	-0.0071	-0.0000	-0.0167	1025.49	-0.0983	-0.0247	350.77	-0.0791	-0.0140	364.23	
1.45	-0.0033	-0.0080	0.0002	-0.0169	1047.16	-0.0996	-0.0211	350.45	-0.0800	-0.0155	363.60	
1.50	-0.0033	-0.0088	0.0000	-0.0168	1054.44	-0.1007	-0.0234	349.55	-0.0805	-0.0236	362.16	
1.55	-0.0033	-0.0096	0.0000	-0.0161	1044.46	-0.1018	-0.0225	349.01	-0.0822	-0.0300	360.70	
1.60	-0.0033	-0.0104	-0.0000	-0.0147	1012.72	-0.1025	-0.0065	350.33	-0.0835	-0.0232	360.64	
1.65	-0.0033	-0.0111	-0.0000	-0.0129	952.68	-0.1024	0.0139	352.74	-0.0844	-0.0140	361.12	
1.70	-0.0033	-0.0117	0.0000	-0.0115	862.47	-0.1015	0.0208	354.08	-0.0852	-0.0194	360.04	
1.75	-0.0033	-0.0122	0.0000	-0.0090	735.51	-0.1007	0.0108	353.52	-0.0867	-0.0461	356.11	
1.80	-0.0033	-0.0125	0.0000	-0.0073	555.07	-0.1004	0.0011	352.61	-0.0897	-0.0745	351.06	
1.85	-0.0033	-0.0124	-0.0000	0.0038	335.02	-0.0999	0.0284	355.96	-0.0934	-0.0634	349.94	
1.90	-0.0033	-0.0122	-0.0000	0.0029	77.56	-0.0971	0.0875	364.29	-0.0954	-0.0125	354.29	
1.95	-0.0034	-0.0121	-0.0000	0.0000	-186.76	-0.0917	0.1215	371.55	-0.0950	0.0231	358.53	

TIME (SEC)	FORWARD (FT)	LATERAL (FT)	VERTICAL (FT)	ROLL (DEG)	PITCH (DEG)	HEADING (DEG)	TURN RADIUS (FT)	SIDE SLIP (DEG)	ARTICULATION ANGLE (DEG)
0.0	-96.3765	0.0	C.C	0.0	0.0	0.0	*****	0.0	0.0
0.05	-94.0666	-0.0000	-C.CC00	0.0000	-0.0000	-0.0000	*****	0.0000	0.0000
0.10	-91.8673	C.CC00	-C.CC00	0.0000	-0.0000	0.0000	*****	0.0000	0.0000
0.15	-89.6721	C.CC00	-C.CC00	0.0000	0.0000	0.0000	*****	0.0000	0.0000
0.20	-87.4863	-C.CC00	-C.CC00	C.CC00	-0.0018	-0.0000	*****	-0.0000	0.0000
0.25	-85.3124	-C.CC00	-C.CC00	0.0000	-0.0130	-0.0000	*****	-0.0000	0.0000
0.30	-83.1500	-C.CC00	-C.CC00	C.CC00	-0.0311	-0.0000	*****	-0.0000	-0.0001
0.35	-80.9988	-0.0000	-C.CC14	-0.0000	-0.0403	-0.0000	*****	0.0000	-0.0003
0.40	-78.8624	C.CC00	-C.CC15	-C.CC00	-0.0417	0.0000	*****	0.0000	-0.0008
0.45	-76.7481	0.0000	-C.CC17	-0.0000	-0.0472	0.0000	*****	0.0001	-0.0017
0.50	-74.6652	C.CC00	-C.CC19	-C.CC01	-0.0536	0.0001	*****	0.0002	-0.0032
0.55	-72.6216	0.0000	-0.0020	-C.CC02	-0.0545	0.0001	*****	0.0004	-0.0053
0.60	-70.6228	C.CC00	-C.CC20	-C.CC02	-0.0550	0.0002	*****	0.0005	-0.0080
0.65	-68.6707	C.CC01	-C.CC20	-C.CC01	-0.0583	0.0001	*****	0.0005	-0.0111
0.70	-66.7655	C.CC01	-C.CC21	C.CC00	-0.0600	0.0004	*****	0.0004	-0.0146
0.75	-64.9053	0.0001	-0.0021	C.CC03	-0.0599	0.0004	*****	-0.0001	-0.0182
0.80	-63.0879	C.CC01	-C.CC21	C.CC06	-0.0609	0.0002	*****	-0.0009	-0.0215
0.85	-61.3117	0.0001	-C.CC22	0.0010	-0.0623	-0.0001	*****	-0.0020	-0.0244
0.90	-59.5758	-C.CC00	-C.CC22	C.CC13	-0.0623	-0.0006	*****	-0.0035	-0.0266
0.95	-57.8804	-0.0002	-C.CC22	0.0014	-0.0621	-0.0014	*****	-0.0053	-0.0279
1.00	-56.2265	-C.CC04	-C.CC22	0.0014	-0.0625	-0.0023	*****	-0.0071	-0.0283
1.05	-54.6154	-C.CC07	-C.CC22	C.CC12	-0.0626	-0.0035	*****	-0.0089	-0.0275
1.10	-53.0493	-0.0011	-C.CC22	C.CC08	-0.0623	-0.0048	*****	-0.0104	-0.0254
1.15	-51.5296	-0.0015	-C.CC22	0.0004	-0.0624	-0.0062	*****	-0.0115	-0.0218
1.20	-50.0576	-C.CC20	-C.CC22	C.CC01	-0.0626	-0.0077	*****	-0.0122	-0.0166
1.25	-48.6334	-C.CC25	-C.CC22	-C.CC02	-0.0627	-0.0093	*****	-0.0125	-0.0095
1.30	-47.2567	-C.CC31	-C.CC22	-C.CC04	-0.0627	-0.0108	*****	-0.0125	-0.0006
1.35	-45.9265	-0.0036	-C.CC22	-C.CC05	-0.0629	-0.0122	*****	-0.0122	0.0104
1.40	-44.6417	-0.0042	-0.0022	-0.0005	-0.0630	-0.0136	*****	-0.0117	0.0234
1.45	-43.4014	-0.0047	-C.CC22	-C.CC06	-0.0630	-0.0145	*****	-0.0110	0.0384
1.50	-42.2050	-0.0053	-C.CC22	-0.0007	-0.0630	-0.0160	*****	-0.0100	0.0554
1.55	-41.0529	-C.CC58	-C.CC22	-C.CC08	-0.0630	-0.0170	*****	-0.0087	0.0743
1.60	-39.9449	-0.0063	-C.CC22	-0.0010	-0.0629	-0.0177	*****	-0.0068	0.0950
1.65	-38.8797	-0.0067	-C.CC22	-0.0012	-0.0628	-0.0181	*****	-0.0043	0.1174
1.70	-37.8559	-0.0071	-C.CC22	-0.0014	-0.0628	-0.0184	*****	-0.0012	0.1414
1.75	-36.8743	-0.0074	-C.CC22	-C.CC14	-0.0628	-0.0183	*****	0.0025	0.1667
1.80	-35.9434	-0.0076	-C.CC22	-0.0013	-0.0627	-0.0175	*****	0.0068	0.1931
1.85	-35.0671	-0.0077	-C.CC22	-0.0011	-0.0627	-0.0173	*****	0.0116	0.2201
1.90	-34.2417	-0.0078	-0.0022	-C.CC08	-0.0627	-0.0164	*****	0.0167	0.2476
1.95	-33.4623	-0.0077	-0.0022	-C.CC05	-0.0628	-0.0152	*****	0.0221	0.2754

TIME (SEC)	FORWARD (FT/SEC)	LATERAL (FT/SEC)	VERTICAL (FT/SEC)	ROLL (DEG/SEC)	PITCH (DEG/SEC)	FEADING (DEG/SEC)	ARTICULATION RATE (DEG/SEC)
0.0	44.00	0.0	0.0	0.0	0.0	0.0	0.0
0.05	44.00	0.00	-0.00	0.00	-0.00	-0.00	0.00
0.10	44.00	0.00	-0.00	-0.00	-0.00	0.00	0.00
0.15	44.00	0.00	-0.00	0.00	-0.00	0.00	0.00
0.20	43.55	-0.00	-0.00	0.00	-0.11	-0.00	0.00
0.25	43.70	-0.00	-0.02	0.00	-0.34	-0.00	-0.00
0.30	42.20	-0.00	-0.03	-0.00	-0.32	-0.00	-0.00
0.35	42.53	0.00	-0.03	-0.00	-0.06	0.00	-0.01
0.40	41.81	0.00	-0.03	-0.00	-0.05	0.00	-0.01
0.45	41.12	0.00	-0.04	-0.00	-0.15	0.00	-0.02
0.50	40.50	0.00	-0.04	-0.00	-0.07	0.00	-0.04
0.55	39.52	0.00	-0.04	-0.00	0.01	0.00	-0.05
0.60	39.25	0.00	-0.04	0.00	-0.05	0.00	-0.06
0.65	38.75	0.00	-0.04	0.00	-0.06	0.00	-0.07
0.70	38.08	0.00	-0.04	0.00	-0.01	0.00	-0.07
0.75	37.21	-0.00	-0.04	0.01	-0.00	-0.00	-0.06
0.80	36.42	-0.00	-0.04	0.01	-0.03	-0.00	-0.06
0.85	35.46	-0.00	-0.04	0.01	-0.01	-0.01	-0.04
0.90	34.45	-0.00	-0.04	0.00	0.01	-0.01	-0.04
0.95	33.43	-0.00	-0.04	0.00	-0.00	-0.02	-0.02
1.00	32.46	-0.00	-0.04	-0.00	-0.01	-0.02	0.00
1.05	31.54	-0.00	-0.03	-0.01	0.00	-0.03	0.03
1.10	30.67	-0.01	-0.03	-0.01	0.00	-0.03	0.06
1.15	29.82	-0.01	-0.03	-0.01	-0.00	-0.03	0.09
1.20	29.00	-0.01	-0.03	-0.01	-0.00	-0.03	0.12
1.25	28.15	-0.01	-0.03	-0.00	0.00	-0.03	0.16
1.30	27.28	-0.01	-0.03	-0.00	-0.00	-0.03	0.20
1.35	26.37	-0.01	-0.03	-0.00	-0.00	-0.03	0.24
1.40	25.42	-0.01	-0.03	-0.00	-0.00	-0.03	0.28
1.45	24.46	-0.00	-0.03	-0.00	0.00	-0.02	0.32
1.50	23.49	-0.00	-0.03	-0.00	-0.00	-0.02	0.36
1.55	22.53	-0.00	-0.02	-0.00	0.00	-0.02	0.40
1.60	21.55	-0.00	-0.02	-0.00	0.00	-0.01	0.43
1.65	20.67	-0.00	-0.02	-0.00	0.00	-0.01	0.46
1.70	19.78	-0.00	-0.02	-0.00	0.00	-0.00	0.49
1.75	18.51	0.00	-0.02	0.00	0.00	0.00	0.52
1.80	18.06	0.00	-0.02	0.00	0.00	0.01	0.52
1.85	17.22	0.00	-0.02	0.00	0.00	0.02	0.55
1.90	16.35	0.00	-0.02	0.01	-0.00	0.02	0.55
1.95	15.52	0.01	-0.02	0.01	-0.00	0.03	0.56

TIME (SEC)	FORWARD (FT/SEC**2)	LATERAL (FT/SEC**2)	VERTICAL (FT/SEC**2)	ROLL (DEG/SEC**2)	PITCH (DEG/SEC**2)	HEADING (DEG/SEC**2)	INERTIAL ACCEL. ALONG BODY AXES	LATERAL (FT/SEC**2)
0.0	0.0	0.0	0.0	0.0	0.0	0.0	-0.0	0.0
0.05	-0.0009	0.0000	-0.0000	-0.0000	-0.0002	0.0000	-0.0009	0.0000
0.10	-0.0024	0.0000	-0.0000	-0.0000	0.0003	0.0000	-0.0024	0.0000
0.15	-0.0019	-0.0000	-0.0000	-0.0000	-0.0015	-0.0000	-0.0019	-0.0000
0.20	-2.4733	-0.0000	-0.2062	-0.0005	-4.1154	-0.0003	-2.4733	-0.0000
0.25	-7.4991	-0.0000	-0.3862	-0.0001	-3.5421	-0.0002	-7.4990	-0.0000
0.30	-12.1243	-0.0001	-0.1605	-0.0017	4.4365	0.0004	-12.1241	-0.0000
0.35	-14.3444	0.0003	0.0924	-0.0042	3.6651	0.0020	-14.3444	0.0003
0.40	-14.2678	0.0007	-0.0515	-0.0073	-2.4347	0.0050	-14.2678	0.0008
0.45	-12.9990	0.0013	-0.1456	-0.0081	-0.4038	0.0089	-12.9989	0.0017
0.50	-11.8599	0.0018	0.0024	-0.0018	2.7767	0.0115	-11.8598	0.0026
0.55	-11.4090	0.0015	0.0572	0.0119	-0.0151	0.0102	-11.4091	0.0030
0.60	-11.5041	0.0012	-0.0356	0.0279	-1.4004	0.0031	-11.5041	0.0025
0.65	-12.4580	-0.0007	-0.0441	0.0412	0.8121	-0.0107	-12.4579	0.0005
0.70	-14.3943	-0.0038	0.0258	0.0446	0.8814	-0.0304	-14.3943	-0.0032
0.75	-16.6287	-0.0078	0.0265	0.0333	-0.6277	-0.0527	-16.6287	-0.0086
0.80	-18.5624	-0.0121	-0.0096	-0.0091	-0.1586	-0.0727	-18.5624	-0.0145
0.85	-19.8805	-0.0158	0.0084	-0.0264	0.6675	-0.0861	-19.8805	-0.0210
0.90	-20.3837	-0.0185	0.0340	-0.0573	0.0534	-0.0908	-20.3837	-0.0262
0.95	-19.5849	-0.0155	0.0237	-0.0733	-0.3155	-0.0874	-19.5849	-0.0296
1.00	-18.9474	-0.0185	0.0125	-0.0715	0.1587	-0.0775	-18.9474	-0.0307
1.05	-17.8904	-0.0156	0.0157	-0.0526	0.1797	-0.0623	-17.8904	-0.0294
1.10	-17.0477	-0.0113	0.0234	-0.0217	-0.1651	-0.0446	-17.0477	-0.0261
1.15	-16.6092	-0.0063	0.0175	0.0105	-0.0915	-0.0270	-16.6092	-0.0216
1.20	-16.6479	-0.0014	0.0148	0.0350	0.1126	-0.0104	-16.6475	-0.0168
1.25	-17.1143	0.0026	0.0179	0.0446	0.0000	0.0046	-17.1143	-0.0124
1.30	-17.8569	0.0056	0.0157	0.0365	-0.0357	0.0189	-17.8569	-0.0086
1.35	-18.5937	0.0077	0.0154	0.0166	0.0148	0.0327	-18.5937	-0.0055
1.40	-19.1436	0.0052	0.0158	-0.0060	0.0750	0.0467	-19.1436	-0.0027
1.45	-19.4146	0.0107	0.0212	-0.0221	-0.0105	0.0606	-19.4146	0.0005
1.50	-19.3331	0.0127	0.0220	-0.0258	-0.0088	0.0741	-19.3331	0.0042
1.55	-19.0102	0.0153	0.0215	-0.0157	0.0336	0.0864	-19.0102	0.0088
1.60	-18.5244	0.0164	0.0204	0.0043	0.0072	0.0969	-18.5244	0.0135
1.65	-18.0494	0.0216	0.0200	0.0266	-0.0254	0.1051	-18.0494	0.0191
1.70	-17.6175	0.0242	0.0155	0.0448	-0.0015	0.1105	-17.6175	0.0237
1.75	-17.2153	0.0258	0.0152	0.0526	0.0182	0.1129	-17.2153	0.0272
1.80	-16.8562	0.0267	0.0186	0.0418	-0.0086	0.1106	-16.8562	0.0298
1.85	-16.6434	0.0267	0.0182	0.0263	-0.0304	0.1199	-16.6434	0.0314
1.90	-16.8931	0.0253	0.0164	0.0204	-0.0305	0.1157	-16.8931	0.0314
1.95	-17.7074	0.0225	0.0187	0.0208	-0.0180	0.1022	-17.7074	0.0298

TIME (SEC)	LEFT SIDE				RIGHT SIDE				
	VERTICAL (LB)	LUNG. (LB)	LATERAL (LP)	MU-Y	VERTICAL (LR)	LUNG. (LB)	LATERAL (LR)	MU-X	MU-Y
0.0	2162.50	-0.00	0.00	C.C	2162.50	-0.00	0.00	0.00	0.00
0.05	2162.50	0.00	0.00	C.C000	2162.50	0.00	0.00	0.0000	0.0000
0.10	2162.50	0.00	0.00	C.C000	2162.50	0.00	0.00	0.0000	0.0000
0.15	2162.89	-4.23	-C.CC	-C.C000	2162.89	-4.23	-C.CC	-C.C020	-0.0000
0.20	2220.85	-169.83	-0.01	-C.C000	2220.86	-169.83	-C.C01	-0.0765	-0.0000
0.25	2446.23	-576.76	-0.00	-C.C000	2446.24	-576.76	-C.C0C	-0.2358	-0.0000
0.30	2741.04	-554.77	0.01	C.C000	2741.03	-994.77	0.01	-0.2625	0.0000
0.35	2891.29	-1302.00	0.05	C.C000	2891.24	-1301.99	C.C05	-0.4519	0.0000
0.40	2928.48	-1555.36	0.13	C.C000	2528.30	-1555.34	0.13	-0.5311	0.0000
0.45	3036.62	-1768.19	0.24	C.C001	3036.23	-1768.16	0.24	-0.5824	0.0001
0.50	3131.22	-1921.35	0.29	C.C001	3130.63	-1921.32	0.29	-0.6137	0.0001
0.55	3145.38	-2028.53	0.24	C.C001	3144.70	-2028.91	0.24	-0.6452	0.0001
0.60	3167.73	-2111.48	0.03	C.C000	3167.24	-2111.51	0.03	-0.6667	0.0000
0.65	3221.32	-2161.77	-0.37	-C.C001	3221.41	-2161.84	-0.37	-0.6711	-0.0001
0.70	3242.90	-2180.07	-0.93	-C.C003	3244.02	-2180.21	-C.C93	-0.6721	-0.0003
0.75	3242.85	-2185.33	-1.54	-C.C005	3245.34	-2185.51	-1.54	-0.6734	-0.0005
0.80	3262.26	-2186.37	-2.06	-C.C006	3266.21	-2187.11	-2.06	-0.6696	-0.0006
0.85	3280.98	-2190.63	-2.33	-C.C007	3286.10	-2186.54	-2.33	-0.6654	-0.0007
0.90	3279.24	-2190.63	-2.26	-C.C007	3284.89	-2190.75	-2.26	-0.6669	-0.0007
0.95	3278.71	-2204.61	-1.82	-C.C006	3284.06	-2204.66	-1.82	-0.6713	-0.0006
1.00	3287.04	-2224.19	-1.04	-C.C003	3291.16	-2224.17	-1.04	-0.6758	-0.0003
1.05	3285.18	-2241.59	C.CC	C.C000	3291.31	-2241.91	-C.CC	-0.6812	-0.0000
1.10	3286.70	-2256.87	1.14	C.C003	3286.41	-2256.77	1.13	-0.6867	0.0003
1.15	3289.86	-2266.53	2.24	C.C007	3287.10	-2266.41	2.23	-0.6895	0.0007
1.20	3294.87	-2268.55	3.19	C.C010	3289.94	-2268.85	3.18	-0.6896	0.0010
1.25	3295.91	-2265.40	3.52	C.C012	3289.36	-2265.33	3.91	-0.6887	0.0012
1.30	3297.00	-2258.28	4.47	C.C014	3289.38	-2258.23	4.46	-0.6865	0.0014
1.35	3300.29	-2250.16	4.86	-C.C6850	3292.06	-2250.12	4.84	-0.6835	0.0015
1.40	3302.06	-2243.50	5.14	-C.C6794	3293.48	-2243.45	5.12	-0.6812	0.0016
1.45	3301.65	-2240.21	5.34	C.C016	3292.79	-2240.15	5.32	-C.C803	0.0016
1.50	3301.69	-2241.14	5.46	C.C017	3292.51	-2241.06	5.44	-C.C807	0.0017
1.55	3302.02	-2245.15	5.47	-C.C6799	3292.51	-2245.06	5.45	-0.6819	0.0017
1.60	3301.20	-2251.04	5.32	C.C016	3291.50	-2250.94	5.30	-0.6839	0.0016
1.65	3300.03	-2257.08	4.52	-C.C6840	3250.50	-2256.98	4.92	-0.6859	0.0015
1.70	3295.40	-2262.54	4.27	-C.C6857	3290.61	-2262.46	4.25	-0.6876	0.0013
1.75	3298.38	-2267.43	3.25	-C.C6874	3291.07	-2267.37	3.28	-0.6889	0.0010
1.80	3296.54	-2271.54	2.05	-C.C6902	3291.37	-2271.88	2.09	-C.C6903	0.0006
1.85	3294.66	-2274.93	C.f1	C.C002	3292.27	-2274.88	C.61	-0.6910	0.0002
1.90	3293.39	-2272.47	-1.25	-C.C6900	3294.47	-2272.43	-1.26	-C.C6898	-0.0004
1.95	3292.94	-2263.20	-3.41	-C.C6873	3297.97	-2263.26	-3.43	-0.6863	-0.0010

TIME (SEC)	LEFT SIDE				RIGHT SIDE			
	VERTICAL (LB)	LATERAL (LB)	MU-X	MU-Y	VERTICAL (LB)	LATERAL (LB)	MU-X	MU-Y
0.0	2162.50	C.C	C.C	C.C	2162.50	0.0	C.C	0.0
0.05	2162.50	C.C	C.C	C.C	2162.50	0.00	C.C	0.0000
0.10	2162.50	C.C	C.C	C.C	2162.50	0.03	C.C	0.0000
0.15	2162.34	-4.23	-C.C020	-C.C000	2162.34	-C.00	-0.0020	-0.0000
0.20	2158.09	-167.47	-0.001	-C.C000	2158.10	-0.01	-0.00776	-0.0000
0.25	2211.04	-560.02	-0.001	-C.C000	2211.05	-C.01	-0.2533	-0.0000
0.30	2312.94	-973.25	0.001	C.C000	2312.94	0.01	-0.4208	0.0000
0.35	2335.07	-1283.24	-0.001	-C.C000	2335.02	C.05	-0.5496	0.0000
0.40	2312.90	-1538.72	C.C031	C.C001	2312.72	C.13	-0.6653	0.0001
0.45	2347.65	-1755.95	C.C021	C.C001	2347.24	C.25	-0.7481	0.0001
0.50	2382.19	-1912.61	-C.002	C.C002	2381.50	C.36	-0.8031	0.0002
0.55	2368.31	-2021.75	C.C002	C.C002	2367.44	0.40	-0.8540	0.0002
0.60	2367.32	-2107.56	-C.001	-C.C001	2366.50	C.25	-C.8906	0.0001
0.65	2392.47	-2161.08	-0.002	-C.C000	2392.13	-0.03	-C.5034	-0.0000
0.70	2397.39	-2180.45	-C.002	-C.C002	2398.07	-0.57	-0.5092	-0.0002
0.75	2389.73	-2186.60	-0.005	-C.C005	2391.94	-1.31	-C.5143	-0.0005
0.80	2398.10	-2185.65	-C.009	-C.C009	2402.18	-2.16	-0.5117	-0.0009
0.85	2406.91	-2185.15	-C.012	-C.C012	2412.84	-2.98	-0.9074	-0.0012
0.90	2401.83	-2152.80	-C.015	-C.C015	2409.22	-3.66	-C.5103	-0.0015
0.95	2398.69	-2206.76	-C.017	-C.C017	2406.87	-4.11	-0.5169	-0.0017
1.00	2402.67	-2226.33	-C.018	-C.C018	2410.85	-4.30	-C.5235	-0.0018
1.05	2402.58	-2243.90	-C.018	-C.C018	2409.57	-4.24	-C.5311	-0.0018
1.10	2399.54	-2258.50	-C.015	-C.C015	2405.60	-3.98	-0.9390	-0.0015
1.15	2401.00	-2269.02	-C.015	-C.C015	2405.54	-3.64	-0.9432	-0.0015
1.20	2404.09	-2271.72	-C.044	-C.C014	2407.18	-3.27	-C.5437	-0.0014
1.25	2404.42	-2268.37	-2.92	-C.5434	2406.37	-2.92	-0.9426	-0.0012
1.30	2404.88	-2261.52	-2.59	-C.9404	2406.04	-2.59	-0.5399	-0.0011
1.35	2407.11	-2253.56	-2.25	-C.5362	2407.72	-2.25	-0.5359	-0.0009
1.40	2408.39	-2246.81	-1.85	-C.9329	2409.45	-1.85	-0.5328	-0.0008
1.45	2408.19	-2243.42	-1.34	-0.5316	2407.62	-1.34	-0.5317	-0.0006
1.50	2408.47	-2244.24	-C.70	-C.5318	2406.94	-0.70	-C.5323	-0.0003
1.55	2405.16	-2248.14	C.66	-0.5332	2406.37	0.06	-C.5342	0.0000
1.60	2409.18	-2253.52	C.91	-C.5356	2404.96	C.91	-0.5371	0.0004
1.65	2409.05	-2259.89	1.81	-C.5381	2403.42	1.81	-C.9402	0.0008
1.70	2409.42	-2265.34	2.70	-C.9402	2402.60	2.69	-0.9428	0.0011
1.75	2409.59	-2270.17	3.55	-C.5421	2402.00	3.53	-C.5451	0.0015
1.80	2409.24	-2274.63	4.42	-C.5441	2401.24	4.40	-0.9472	0.0018
1.85	2408.93	-2277.67	5.31	-C.5455	2400.78	5.29	-C.5487	0.0022
1.90	2405.18	-2275.40	6.12	-C.5445	2401.17	6.10	-0.5476	0.0025
1.95	2410.08	-2266.47	6.82	-C.5404	2402.48	6.75	-C.5434	0.0028

TIME (SECC)	LEFT SIDE				RIGHT SIDE					
	VERTICAL (LB)	LCNG. (LB)	LATERAL (LB)	MU-X	MU-Y	VERTICAL (LB)	LCNG. (LB)	LATERAL (LB)	MU-X	MU-Y
0.0	2162.50	-C.C	C.C	0.C	C.C	2162.50	-0.0	0.0	0.C	0.C
0.05	2162.50	0.00	-0.00	0.0000	-C.C000	2162.50	0.00	-0.00	0.0000	-0.0000
0.10	2162.50	0.C3	-C.C0	C.C000	-C.C000	2162.50	0.03	-0.00	C.C000	-0.C0C0
0.15	2162.83	-4.23	-C.C0	-C.C020	-C.C000	2162.83	-4.23	-0.00	0.0020	-0.0000
0.20	2177.63	-168.64	C.C0	-0.C772	C.C000	2177.62	-168.04	0.00	-0.C772	0.0000
0.25	2126.51	-545.56	C.C0	-0.2586	C.C000	2126.52	-549.96	0.00	-0.2586	0.C0C0
0.30	2022.77	-941.82	-C.C0	-C.4703	-C.C000	2022.78	-941.82	-0.00	-C.4703	-0.0000
0.35	1976.40	-1273.09	-0.C1	-0.6441	-C.C000	1976.41	-1273.09	-0.01	-0.6441	-0.0000
0.40	2015.55	-1537.48	-0.C3	-C.7628	-C.C000	2015.54	-1537.47	-0.03	-0.7628	-0.0000
0.45	1982.46	-1732.15	-C.C5	-0.8737	-C.C000	1982.37	-1732.13	-0.05	-0.8738	-0.0000
0.50	1938.06	-1896.81	-0.C5	-0.5787	-C.C000	1937.83	-1896.76	-0.05	-C.5788	-0.0000
0.55	1953.07	-2026.78	-0.C1	-1.C377	-C.C000	1952.65	-2026.72	-0.01	-1.C379	-0.0000
0.60	1960.68	-2102.85	0.C7	-1.C725	C.C000	1960.12	-2102.81	0.07	-1.C728	0.0000
0.65	1934.35	-2149.45	C.18	-1.1112	C.C001	1933.81	-2149.47	C.18	-1.1115	0.0001
0.70	1925.13	-2181.53	C.29	-1.1332	C.C001	1924.90	-2181.66	C.29	-1.1334	0.0001
0.75	1932.73	-2190.81	C.35	-1.1335	C.C002	1933.15	-2191.06	C.35	-1.1334	0.0002
0.80	1925.19	-2187.41	C.34	-1.1362	C.C002	1926.57	-2187.75	C.34	-1.1356	0.0002
0.85	1914.32	-2189.50	0.24	-1.1438	C.C001	1916.75	-2189.86	C.24	-1.1425	0.C001
0.90	1916.92	-2157.73	0.08	-1.1465	C.C000	1920.34	-2198.02	0.08	-1.1446	0.C000
0.95	1915.82	-2209.21	-0.C7	-1.1507	-C.C000	1923.76	-2209.38	-0.07	-1.1485	-0.C000
1.00	1916.71	-2227.09	-0.15	-1.1619	-C.C001	1920.58	-2227.11	-0.15	-1.1596	-0.0001
1.05	1917.32	-2246.74	-C.14	-1.1718	-C.C001	1920.53	-2246.62	-C.14	-1.1698	-0.0001
1.10	1921.05	-2261.52	-C.C2	-1.1774	-C.C000	1923.13	-2261.70	-C.02	-1.1761	-0.0000
1.15	1921.16	-2270.65	C.17	-1.1819	C.C001	1921.85	-2270.40	0.17	-1.1813	0.C001
1.20	1915.82	-2273.78	0.38	-1.1844	C.C002	1919.30	-2273.56	C.38	-1.1846	0.0002
1.25	1920.46	-2271.38	C.56	-1.1827	C.C003	1919.98	-2271.23	0.56	-1.1836	0.0003
1.30	1920.39	-2264.20	C.66	-1.1790	C.C003	1918.35	-2264.17	C.66	-1.1802	0.0003
1.35	1918.61	-2256.10	C.66	-1.1759	C.C003	1916.37	-2256.06	C.66	-1.1773	0.C0C3
1.40	1917.80	-2245.84	C.58	-1.1731	C.C003	1915.56	-2249.81	0.58	-1.1745	0.0003
1.45	1918.28	-2246.58	C.48	-1.1711	C.C002	1916.02	-2246.51	0.48	-1.1725	0.0002
1.50	1918.43	-2247.10	C.38	-1.1713	C.C002	1915.98	-2246.98	0.38	-1.1728	0.0002
1.55	1918.61	-2250.96	0.31	-1.1732	C.C002	1915.77	-2250.81	0.31	-1.1749	0.0002
1.60	1915.68	-2256.81	C.26	-1.1756	C.C001	1916.32	-2256.65	0.26	-1.1776	0.C0C1
1.65	1920.69	-2262.61	0.21	-1.1780	C.C001	1916.88	-2262.46	0.21	-1.1803	0.0001
1.70	1920.94	-2267.52	0.10	-1.1806	C.C001	1916.94	-2267.81	0.10	-1.1830	0.C0C1
1.75	1921.06	-2272.75	-0.11	-1.1831	-C.C001	1917.33	-2272.69	-0.11	-1.1853	-0.C001
1.80	1921.27	-2277.19	-0.47	-1.1853	-C.C002	1918.34	-2277.19	-0.47	-1.1871	-0.0002
1.85	1920.96	-2280.15	-1.00	-1.1870	-C.C005	1919.34	-2280.17	-1.00	-1.1880	-0.0005
1.90	1915.83	-2277.94	-1.58	-1.1865	-C.C008	1919.75	-2277.97	-1.58	-1.1866	-0.0008
1.95	1917.91	-2269.17	-2.17	-1.1831	-C.C011	1919.51	-2269.20	-2.17	-1.1822	-0.0011



ESPT TRUCK AND TRACTOR-TRAILER DYNAMIC RESPONSE SIMULATION - TORSION VI CLIPUT PACE NO.  
 SAMPLE RUN - TRIPLES BRAKING IN A TURN, ALL OPTICNS EXERCISED  
 TRAILER NO. 3 REAR SUSPENSION TIRE FORCES  
 TRAILING TANDEM AXLE

TIME (SEC)	LEFT SIDE				RIGHT SIDE					
	VERTICAL (LR)	LCNG. (LR)	LATERAL (LR)	MU-X	MU-Y	VERTICAL (LR)	LCNG. (LR)	LATERAL (LR)	MU-X	MU-Y
0.0	2162.50	-C.C	0.0	0.0	C.C	2162.50	-0.0	0.0	0.0	0.0
0.05	2162.50	0.00	-0.00	0.0000	-C.C000	2162.50	0.00	-0.00	0.0000	-0.0000
0.10	2162.50	C.C3	-C.CC	C.C000	-C.C0000	2162.50	0.03	-0.00	C.C000	-0.0000
0.15	2162.27	-4.23	0.00	-0.0020	C.C000	2162.27	-4.23	0.00	-0.0020	0.0000
0.20	2114.86	-165.62	C.CC	-C.C783	C.C000	2114.86	-165.62	0.00	-0.0783	0.0000
0.25	1891.32	-527.74	-C.CC	-0.2790	-C.C000	1891.32	-527.74	-0.00	-0.2790	-0.0000
0.30	1574.67	-888.53	-C.CC	-C.5643	-C.C000	1574.68	-888.53	-0.00	-0.5643	-0.0000
0.35	1430.19	-1216.71	-0.01	-C.8507	-C.C000	1430.15	-1216.71	-0.01	-0.8507	-0.0000
0.40	1395.93	-1452.54	-C.C1	-1.0661	-C.C000	1399.94	-1492.51	-0.01	-1.0661	-0.0000
0.45	1293.51	-1666.64	0.01	-1.2835	C.C000	1293.35	-1666.56	C.01	-1.2886	0.0000
0.50	1185.04	-1821.05	C.C4	-1.5399	C.C000	1188.69	-1830.89	C.04	-1.5403	0.0000
0.55	1175.98	-1955.11	0.10	-1.6599	C.C001	1175.42	-1998.92	0.10	-1.7006	0.0001
0.60	1160.18	-2077.45	0.17	-1.7906	C.C001	1159.48	-2077.23	0.17	-1.7916	0.0001
0.65	1105.30	-2112.10	C.22	-1.5109	C.C002	1104.71	-2112.17	C.22	-1.5120	0.0002
0.70	1079.35	-2166.52	0.21	-2.0072	C.C002	1079.22	-2166.93	C.21	-2.0079	0.0002
0.75	1079.31	-2194.06	0.12	-2.0328	C.C001	1080.05	-2194.87	0.12	-2.0322	0.0001
0.80	1060.81	-2183.26	-0.10	-2.0581	-C.C001	1062.77	-2184.40	-0.10	-2.0554	-0.0001
0.85	1040.22	-2187.51	-0.42	-2.1029	-C.C004	1043.55	-2188.80	-0.42	-2.0974	-0.0004
0.90	1039.80	-2208.06	-0.82	-2.1235	-C.C008	1044.39	-2209.13	-0.82	-2.1152	-0.0008
0.95	1040.46	-2218.29	-1.24	-2.1320	-C.C012	1045.90	-2218.97	-1.24	-2.1216	-0.0012
1.00	1033.45	-2231.23	-1.60	-2.1590	-C.C015	1039.16	-2231.45	-1.61	-2.1474	-0.0015
1.05	1032.25	-2254.75	-1.89	-2.1843	-C.C018	1037.66	-2254.46	-1.90	-2.1726	-0.0018
1.10	1035.77	-2272.30	-2.05	-2.1538	-C.C020	1040.44	-2271.63	-2.10	-2.1833	-0.0020
1.15	1034.48	-2278.78	-2.18	-2.2028	-C.C021	1038.15	-2277.98	-2.18	-2.1943	-0.0021
1.20	1031.45	-2282.63	-2.15	-2.2130	-C.C021	1034.13	-2281.68	-2.20	-2.2066	-0.0021
1.25	1031.52	-2283.17	-2.18	-2.2134	-C.C021	1033.44	-2282.59	-2.18	-2.2087	-0.0021
1.30	1030.92	-2276.27	-2.15	-2.2080	-C.C021	1032.37	-2275.51	-2.16	-2.2045	-0.0021
1.35	1028.12	-2267.88	-2.12	-2.2059	-C.C021	1029.33	-2267.67	-2.13	-2.2030	-0.0021
1.40	1026.82	-2262.79	-2.07	-2.2037	-C.C020	1028.87	-2262.59	-2.08	-2.2013	-0.0020
1.45	1027.45	-2260.05	-1.98	-2.1997	-C.C019	1028.22	-2259.76	-1.98	-2.1577	-0.0019
1.50	1027.69	-2259.76	-1.80	-2.1999	-C.C017	1027.92	-2259.30	-1.80	-2.1979	-0.0017
1.55	1029.55	-2263.25	-1.51	-2.2016	-C.C015	1027.35	-2262.64	-1.51	-2.2023	-0.0015
1.60	1029.55	-2265.18	-1.13	-2.2041	-C.C011	1027.88	-2263.51	-1.13	-2.2070	-0.0011
1.65	1031.14	-2274.53	-0.66	-2.2058	-C.C006	1028.37	-2273.90	-0.65	-2.2112	-0.0006
1.70	1031.81	-2275.30	-0.12	-2.2090	-C.C001	1028.07	-2278.80	-0.12	-2.2166	-0.0001
1.75	1032.48	-2294.01	C.43	-2.2122	C.C004	1028.05	-2283.69	0.43	-2.2214	0.0004
1.80	1033.45	-2288.35	C.99	-2.2143	C.C010	1028.71	-2288.22	C.98	-2.2244	0.0010
1.85	1033.94	-2291.13	1.55	-2.2159	C.C015	1029.14	-2291.09	1.54	-2.2262	0.0015
1.90	1033.42	-2285.24	2.17	-2.2152	C.C021	1028.66	-2289.24	2.16	-2.2255	0.0021
1.95	1031.84	-2291.17	2.82	-2.2108	C.C027	1027.24	-2281.23	2.81	-2.2207	0.0027

TRAILER NO. 3 FFCT SUSPENSION - BRAKE SUMMARY

LEADING TANDEM AXLE

TIME (SEC)	LEFT SIDE								RIGHT SIDE							
	TREADLE PRESSURE (PST)	BRAKE PRESSURE (PST)	BRAKE TORQUE (IN-LB)	TIRE FORCE (LB)	WHEEL SLIP	ANGULAR VELOCITY (RAD/SEC)	WHEEL ACCEL. (RAD/SEC)	WHEEL ACCEL. (RAD/SEC)	TREADLE PRESSURE (PST)	BRAKE PRESSURE (PST)	BRAKE TORQUE (IN-LB)	TIRE FORCE (LB)	WHEEL SLIP	ANGULAR VELOCITY (RAD/SEC)	WHEEL ACCEL. (RAD/SEC)	WHEEL ACCEL. (RAD/SEC)
0.0	0.0	0.0	0.0	-0.0	C.0	26.14	-0.0	0.0	0.0	0.0	-0.0	0.0	0.0	26.14	-0.0	0.0
0.05	26.25	0.0	0.0	0.00	-0.000	26.14	-0.0	0.0	0.0	0.0	0.00	0.0	-0.000	26.14	-0.0	0.00
0.10	50.00	0.0	0.0	0.03	-0.000	26.14	-0.0	0.0	0.0	0.0	-0.000	0.0	-0.000	26.14	-0.0	0.00
0.15	50.00	0.27	268.45	-4.23	C.0001	26.13	-0.42	0.27	268.45	-4.23	C.0001	0.0039	C.0001	26.13	-0.43	0.27
0.20	50.00	5.29	5292.59	-165.83	C.0039	26.00	-4.35	5.29	5292.59	-165.83	C.0039	0.0039	0.0039	26.00	-4.39	5.29
0.25	50.00	15.14	15138.39	-576.76	C.0121	25.65	-8.22	15.14	15138.39	-576.76	C.0121	0.0121	0.0121	25.65	-8.23	15.14
0.30	50.00	24.02	24021.62	-594.77	C.0187	25.19	-9.22	24.02	24021.62	-594.77	C.0187	0.0187	0.0187	25.19	-9.26	24.02
0.35	50.00	30.64	30641.29	-1302.00	C.0233	24.68	-10.24	30.64	30641.29	-1302.00	C.0233	0.0233	0.0233	24.68	-10.24	30.64
0.40	50.00	35.57	35574.09	-1555.36	C.0273	24.16	-9.80	35.57	35574.09	-1555.36	C.0273	0.0273	0.0273	24.16	-9.80	35.57
0.45	50.00	39.25	39249.84	-1768.19	C.0300	23.70	-8.23	39.25	39249.84	-1768.19	C.0300	0.0300	0.0300	23.70	-8.33	39.25
0.50	50.00	41.99	41588.98	-1921.35	C.0316	23.30	-7.49	41.99	41588.98	-1921.35	C.0316	0.0316	0.0316	23.30	-7.50	41.99
0.55	50.00	44.03	44030.18	-2028.93	C.0322	22.93	-7.18	44.03	44030.18	-2028.93	C.0322	0.0322	0.0322	22.93	-7.18	44.03
0.60	50.00	45.55	45551.23	-2111.48	C.0333	22.57	-6.84	45.55	45551.23	-2111.48	C.0333	0.0333	0.0333	22.57	-6.84	45.55
0.65	50.00	46.68	46684.67	-2161.77	C.0346	22.23	-6.12	46.68	46684.67	-2161.77	C.0346	0.0346	0.0346	22.23	-7.11	46.68
0.70	50.00	47.53	47529.34	-2193.07	C.0346	21.84	-8.24	47.53	47529.34	-2193.07	C.0346	0.0346	0.0346	21.84	-8.23	47.53
0.75	50.00	48.16	48158.78	-2185.33	C.0347	21.39	-9.47	48.16	48158.78	-2185.33	C.0347	0.0347	0.0347	21.39	-9.46	48.16
0.80	50.00	48.63	48627.82	-2186.92	C.0345	20.89	-10.50	48.63	48627.82	-2186.92	C.0345	0.0345	0.0345	20.89	-10.49	48.63
0.85	50.00	48.98	48971.23	-2186.37	C.0343	20.34	-11.25	48.98	48971.23	-2186.37	C.0343	0.0343	0.0343	20.34	-11.34	48.98
0.90	50.00	49.24	49237.78	-2190.63	C.0344	19.76	-11.72	49.24	49237.78	-2190.63	C.0344	0.0344	0.0344	19.76	-11.76	49.24
0.95	50.00	49.43	49431.89	-2204.61	C.0346	15.17	-11.55	49.43	49431.89	-2204.61	C.0346	0.0346	0.0346	15.18	-11.55	49.43
1.00	50.00	49.58	49576.55	-2224.19	C.0348	16.61	-10.50	49.58	49576.55	-2224.19	C.0348	0.0348	0.0348	16.61	-10.96	49.58
1.05	50.00	49.68	49684.31	-2241.99	C.0351	18.08	-10.27	49.68	49684.31	-2241.99	C.0351	0.0351	0.0351	18.08	-10.37	49.68
1.10	50.00	49.76	49764.61	-2256.87	C.0354	17.57	-9.85	49.76	49764.61	-2256.87	C.0354	0.0354	0.0354	17.57	-9.85	49.76
1.15	50.00	49.82	49824.47	-2266.53	C.0355	17.09	-9.52	49.82	49824.47	-2266.53	C.0355	0.0355	0.0355	17.09	-9.54	49.82
1.20	50.00	49.87	49865.05	-2268.95	C.0355	16.61	-9.52	49.87	49865.05	-2268.95	C.0355	0.0355	0.0355	16.61	-9.52	49.87
1.25	50.00	49.90	49902.28	-2265.40	C.0354	16.13	-9.77	49.90	49902.28	-2265.40	C.0354	0.0354	0.0354	16.13	-9.77	49.90
1.30	50.00	49.93	49927.03	-2258.28	C.0353	15.63	-10.16	49.93	49927.03	-2258.28	C.0353	0.0353	0.0353	15.63	-10.17	49.93
1.35	50.00	49.95	49945.90	-2250.16	C.0351	15.11	-10.55	49.95	49945.90	-2250.16	C.0351	0.0351	0.0351	15.11	-10.60	49.95
1.40	50.00	49.96	49955.23	-2243.50	C.0350	14.57	-10.54	49.96	49955.23	-2243.50	C.0350	0.0350	0.0350	14.57	-10.95	49.96
1.45	50.00	49.97	49969.50	-2240.21	C.0349	14.02	-11.12	49.97	49969.50	-2240.21	C.0349	0.0349	0.0349	14.02	-11.13	49.97
1.50	50.00	49.98	49977.14	-2241.14	C.0349	13.46	-11.10	49.98	49977.14	-2241.14	C.0349	0.0349	0.0349	13.46	-11.10	49.98
1.55	50.00	49.98	49982.81	-2245.15	C.0350	12.91	-10.52	49.98	49982.81	-2245.15	C.0350	0.0350	0.0350	12.91	-10.93	49.98
1.60	50.00	49.95	49987.08	-2251.04	C.0351	12.37	-10.65	49.95	49987.08	-2251.04	C.0351	0.0351	0.0351	12.37	-10.66	49.95
1.65	50.00	49.99	49990.27	-2251.09	C.0352	11.85	-10.27	49.99	49990.27	-2251.09	C.0352	0.0352	0.0352	11.85	-10.38	49.99
1.70	50.00	49.99	49992.61	-2262.54	C.0353	11.34	-10.12	49.99	49992.61	-2262.54	C.0353	0.0353	0.0353	11.34	-10.12	49.99
1.75	50.00	49.99	49994.34	-2267.43	C.0354	10.84	-9.85	49.99	49994.34	-2267.43	C.0354	0.0354	0.0354	10.84	-9.89	49.99
1.80	50.00	50.00	49995.66	-2271.94	C.0355	10.35	-9.68	50.00	49995.66	-2271.94	C.0355	0.0355	0.0355	10.35	-9.68	50.00
1.85	50.00	50.00	49996.64	-2274.93	C.0356	5.87	-9.54	50.00	49996.64	-2274.93	C.0356	0.0356	0.0356	5.87	-9.54	50.00
1.90	50.00	50.00	49997.34	-2272.47	C.0355	5.39	-9.65	50.00	49997.34	-2272.47	C.0355	0.0355	0.0355	5.39	-9.66	50.00
1.95	50.00	50.00	49997.95	-2263.29	C.0354	8.90	-10.00	50.00	49997.95	-2263.29	C.0354	0.0354	0.0354	8.90	-10.09	50.00

TRAILER NO. 3 FRONT SUSPENSION - BRAKE SUMMARY

TRAILING TANDEM AXLE

TIME (SEC)	LEFT SIDE										RIGHT SIDE									
	TREADLF PRESSURE (PSI)	BRAKE PRESSURE (PSI)	BRAKE TORQUE (IN-LP)	TIRE FORCE (LB)	WHEEL SLIP	ANGULAR WFL. (RAD/SEC)	ANGULAR WHEEL ACCEL. (RAD/SEC)	WHEEL ACCEL. (RAD/SEC)	BRAKE PRESSURE (PSI)	PRAKE TORQUE (IN-LB)	TIRE FORCE (LB)	WHEEL SLIP	ANGULAR WHEEL VEL (RAD/SEC)	ANGULAR WHEEL ACCEL. (RAD/SEC)						
0.0	0.0	0.0	C.C	-0.0	C.0	26.14	-0.0	0.0	0.0	-0.0	0.0	0.0	26.14	-0.0						
0.05	26.25	0.0	C.C	0.00	-0.000	26.14	-0.00	0.0	0.0	0.00	-0.000	26.14	-0.00	-0.00						
0.10	50.00	0.0	C.0	0.03	-0.000	26.14	-0.00	0.0	0.0	0.03	-0.000	26.14	-0.00	-0.00						
0.15	50.00	0.27	268.45	-4.23	C.0001	26.13	-0.42	0.27	268.45	-4.23	C.0001	26.13	-0.43	-0.43						
0.20	50.00	5.29	5292.59	-167.47	C.0040	26.00	-4.50	5.29	5292.59	-167.47	C.0040	26.00	-4.50	-4.50						
0.25	50.00	15.14	15138.39	-560.02	C.0130	25.62	-9.02	15.14	15138.39	-560.02	C.0130	25.62	-9.02	-9.02						
0.30	50.00	24.02	24021.62	-573.25	C.0217	25.11	-10.25	24.02	24021.62	-573.25	C.0217	25.11	-10.29	-10.29						
0.35	50.00	30.64	30641.25	-1283.25	C.0283	24.55	-11.12	30.64	30641.25	-1283.25	C.0283	24.55	-11.13	-11.13						
0.40	50.00	35.57	35574.09	-1538.75	C.0343	23.98	-10.55	35.57	35574.09	-1538.75	C.0343	23.98	-10.59	-10.59						
0.45	50.00	39.25	39245.84	-1756.01	C.0385	23.49	-8.51	39.25	39245.84	-1756.01	C.0385	23.49	-8.91	-8.91						
0.50	50.00	41.99	41988.98	-1912.61	C.0413	23.07	-7.51	41.99	41988.98	-1912.61	C.0413	23.07	-7.91	-7.91						
0.55	50.00	44.03	44030.18	-2021.75	C.0440	22.67	-7.52	44.03	44030.18	-2021.75	C.0440	22.67	-7.53	-7.53						
0.60	50.00	45.55	45551.23	-2107.56	C.0458	22.30	-7.02	45.55	45551.23	-2107.56	C.0458	22.30	-7.02	-7.02						
0.65	50.00	46.68	46684.67	-2160.97	C.0465	21.95	-7.15	46.68	46684.67	-2160.97	C.0465	21.95	-7.15	-7.15						
0.70	50.00	47.53	47525.34	-2180.22	C.0468	21.57	-8.22	47.53	47525.34	-2180.22	C.0468	21.57	-8.22	-8.22						
0.75	50.00	48.16	48158.78	-2186.60	C.0471	21.12	-9.41	48.16	48158.78	-2186.60	C.0471	21.12	-9.39	-9.39						
0.80	50.00	48.63	48627.82	-2189.69	C.0470	20.62	-10.27	48.63	48627.82	-2189.69	C.0470	20.62	-10.35	-10.35						
0.85	50.00	48.58	48577.33	-2189.15	C.0468	20.08	-11.22	48.58	48577.33	-2189.15	C.0468	20.08	-11.20	-11.20						
0.90	50.00	49.24	49237.78	-2192.80	C.0470	19.50	-11.66	49.24	49237.78	-2192.80	C.0470	19.50	-11.65	-11.65						
0.95	50.00	49.43	49431.85	-2206.76	C.0474	18.92	-11.45	49.43	49431.85	-2206.76	C.0474	18.92	-11.44	-11.44						
1.00	50.00	49.58	49576.55	-2226.33	C.0477	18.36	-10.80	49.58	49576.55	-2226.33	C.0477	18.92	-11.44	-11.44						
1.05	50.00	49.68	49694.31	-2243.90	C.0481	17.83	-10.28	49.68	49694.31	-2243.90	C.0475	18.37	-10.86	-10.86						
1.10	50.00	49.76	49764.61	-2258.90	C.0485	17.33	-9.75	49.76	49764.61	-2258.90	C.0479	17.84	-10.28	-10.28						
1.15	50.00	49.82	49824.47	-2265.02	C.0487	16.86	-9.41	49.82	49824.47	-2265.02	C.0486	16.86	-9.42	-9.42						
1.20	50.00	49.87	49865.05	-2271.72	C.0487	16.39	-9.35	49.87	49865.05	-2271.72	C.0486	16.39	-9.40	-9.40						
1.25	50.00	49.50	49502.28	-2268.37	C.0486	15.91	-9.62	49.50	49502.28	-2268.37	C.0485	15.91	-9.63	-9.63						
1.30	50.00	49.93	49927.03	-2261.52	C.0484	15.47	-10.01	49.93	49927.03	-2261.52	C.0484	15.91	-10.02	-10.02						
1.35	50.00	49.95	49945.50	-2253.56	C.0482	14.91	-10.42	49.95	49945.50	-2253.56	C.0482	14.91	-10.44	-10.44						
1.40	50.00	49.56	49555.22	-2246.91	C.0480	14.38	-10.75	49.56	49555.22	-2246.91	C.0480	14.38	-10.79	-10.79						
1.45	50.00	49.97	49965.50	-2243.42	C.0480	13.83	-10.57	49.97	49965.50	-2243.42	C.0480	13.83	-10.98	-10.98						
1.50	50.00	49.98	49977.14	-2244.24	C.0480	13.28	-10.55	49.98	49977.14	-2244.24	C.0480	13.83	-10.96	-10.96						
1.55	50.00	49.98	49982.81	-2248.14	C.0480	12.74	-10.78	49.98	49982.81	-2248.14	C.0481	12.74	-10.79	-10.79						
1.60	50.00	49.99	49987.08	-2253.92	C.0482	12.21	-10.51	49.99	49987.08	-2253.92	C.0482	12.21	-10.52	-10.52						
1.65	50.00	49.65	49560.27	-2255.85	C.0483	11.69	-10.24	49.65	49560.27	-2255.85	C.0482	12.21	-10.52	-10.52						
1.70	50.00	49.99	49992.61	-2265.34	C.0484	11.18	-9.58	49.99	49992.61	-2265.34	C.0485	11.69	-9.99	-9.99						
1.75	50.00	49.59	49554.34	-2270.17	C.0485	10.69	-9.76	49.59	49554.34	-2270.17	C.0487	10.69	-9.76	-9.76						
1.80	50.00	50.00	49995.66	-2274.63	C.0486	10.21	-9.55	50.00	49995.66	-2274.63	C.0487	10.69	-9.76	-9.76						
1.85	50.00	50.00	49966.64	-2277.67	C.0487	9.73	-9.41	50.00	49966.64	-2277.67	C.0488	10.21	-9.55	-9.55						
1.90	50.00	50.00	49997.34	-2275.00	C.0486	9.26	-9.51	50.00	49997.34	-2275.00	C.0488	10.21	-9.55	-9.55						
1.95	50.00	50.00	49997.95	-2266.47	C.0484	8.78	-9.54	50.00	49997.95	-2266.47	C.0486	9.26	-9.52	-9.52						

LEFT SIDE

RIGHT SIDE

TIME (SEC)	TREADLF PRESSURE (PSI)	BRAKE PRESSURE (PSI)	BRAKE TORQUE (IN-LB)	TIRE FORCE (LB)	WHEEL SLIP	WHEEL VELOCITY (RAD/SEC)	WHEEL ACCEL. (RAD/SEC)	BRAKE PRESSURE (PSI)	TORQUE (IN-LB)	TIRE FORCE (LB)	WHEEL SLIP	WHEEL VELOCITY (RAD/SEC)	WHEEL ACCEL. (RAD/SEC)
0.0	0.0	0.0	C.0	-0.0	C.0	26.14	-0.0	0.0	0.0	-0.0	C.0	26.14	-0.0
0.05	26.25	0.0	C.0	0.00	-0.000	26.14	-0.00	0.0	0.0	0.00	-0.000	26.14	-0.00
0.10	50.00	0.0	C.0	0.03	-0.000	26.14	-0.00	0.0	0.0	0.03	-0.000	26.14	-0.00
0.15	50.00	0.27	268.45	-4.23	0.000	26.13	-0.42	0.27	268.45	-4.23	0.000	26.13	-0.42
0.20	50.00	5.29	5252.55	-168.04	0.000	26.00	-4.48	5.29	5252.55	-168.04	0.000	26.00	-4.48
0.25	50.00	15.14	15138.35	-549.96	0.0133	25.62	-9.50	15.14	15138.35	-549.96	0.0133	25.62	-9.50
0.30	50.00	24.02	24021.62	-541.82	0.0242	25.04	-11.78	24.02	24021.62	-541.82	0.0242	25.04	-11.78
0.35	50.00	30.64	30641.25	-1273.09	0.0332	24.43	-11.62	30.64	30641.25	-1273.09	0.0332	24.43	-11.62
0.40	50.00	35.57	35574.05	-1537.48	0.0353	23.86	-10.65	35.57	35574.05	-1537.48	0.0353	23.86	-10.65
0.45	50.00	39.25	39245.64	-1732.15	0.0450	23.33	-10.05	39.25	39245.64	-1732.15	0.0450	23.33	-10.05
0.50	50.00	41.99	41588.98	-1896.81	0.0504	22.85	-8.67	41.99	41588.98	-1896.81	0.0504	22.85	-8.67
0.55	50.00	44.03	44030.16	-2026.78	0.0534	22.45	-7.29	44.03	44030.16	-2026.78	0.0534	22.45	-7.29
0.60	50.00	45.55	45551.23	-2102.81	0.0552	22.08	-7.25	45.55	45551.23	-2102.81	0.0552	22.08	-7.25
0.65	50.00	46.68	46684.67	-2149.45	0.0572	21.70	-7.70	46.68	46684.67	-2149.45	0.0572	21.70	-7.70
0.70	50.00	47.53	47525.34	-2181.53	0.0583	21.30	-8.17	47.53	47525.34	-2181.53	0.0583	21.30	-8.17
0.75	50.00	48.16	48158.78	-2190.81	0.0584	20.87	-9.21	48.16	48158.78	-2190.81	0.0584	20.87	-9.21
0.80	50.00	48.63	48627.82	-2187.41	0.0585	20.37	-10.48	48.63	48627.82	-2187.41	0.0585	20.37	-10.48
0.85	50.00	48.98	48577.33	-2189.50	0.0589	19.82	-11.20	48.98	48577.33	-2189.50	0.0589	19.82	-11.20
0.90	50.00	49.24	49237.76	-2197.73	0.0550	19.26	-11.42	49.24	49237.76	-2197.73	0.0550	19.26	-11.42
0.95	50.00	49.43	49431.85	-2209.21	0.0552	18.68	-11.32	49.43	49431.85	-2209.21	0.0552	18.68	-11.32
1.00	50.00	49.58	49576.55	-2227.09	0.0558	18.13	-10.82	49.58	49576.55	-2227.09	0.0558	18.13	-10.82
1.05	50.00	49.68	49684.31	-2246.74	0.0603	17.60	-10.14	49.68	49684.31	-2246.62	0.0602	17.61	-10.15
1.10	50.00	49.76	49764.61	-2261.92	0.0606	17.11	-9.61	49.76	49764.61	-2261.70	0.0606	17.11	-9.62
1.15	50.00	49.82	49824.47	-2270.65	0.0609	16.64	-9.32	49.82	49824.47	-2270.40	0.0608	16.64	-9.35
1.20	50.00	49.87	49865.05	-2273.78	0.0610	16.17	-9.25	49.87	49865.05	-2273.56	0.0610	16.17	-9.30
1.25	50.00	49.90	49902.28	-2271.38	0.0609	15.71	-9.48	49.90	49902.28	-2271.23	0.0609	15.71	-9.49
1.30	50.00	49.93	49927.03	-2264.20	0.0607	15.22	-9.88	49.93	49927.03	-2264.12	0.0608	15.22	-9.89
1.35	50.00	49.95	49945.50	-2256.10	0.0605	14.77	-10.21	49.95	49945.50	-2256.06	0.0606	14.71	-10.31
1.40	50.00	49.96	49955.23	-2245.84	0.0604	14.19	-10.64	49.96	49955.23	-2245.81	0.0605	14.19	-10.64
1.45	50.00	49.97	49965.50	-2246.53	0.0603	13.65	-10.82	49.97	49965.50	-2246.51	0.0604	13.65	-10.83
1.50	50.00	49.98	49977.14	-2247.10	0.0603	13.11	-10.82	49.98	49977.14	-2246.98	0.0604	13.11	-10.82
1.55	50.00	49.98	49982.81	-2250.96	0.0604	12.57	-10.64	49.98	49982.81	-2250.81	0.0605	12.57	-10.65
1.60	50.00	49.99	49987.08	-2256.81	0.0605	12.05	-10.21	49.99	49987.08	-2256.65	0.0606	12.05	-10.38
1.65	50.00	49.99	49990.27	-2262.61	0.0607	11.54	-10.11	49.99	49990.27	-2262.46	0.0608	11.53	-10.11
1.70	50.00	49.99	49992.61	-2267.92	0.0608	11.04	-9.61	49.99	49992.61	-2267.81	0.0609	11.04	-9.87
1.75	50.00	49.99	49994.34	-2272.75	0.0609	10.55	-9.62	49.99	49994.34	-2272.69	0.0610	10.55	-9.64
1.80	50.00	50.00	49995.66	-2277.19	0.0610	10.07	-9.42	50.00	49995.66	-2277.15	0.0611	10.07	-9.43
1.85	50.00	50.00	49996.64	-2280.15	0.0611	9.61	-9.25	50.00	49996.64	-2280.17	0.0612	9.61	-9.29
1.90	50.00	50.00	49997.34	-2277.94	0.0611	9.14	-9.25	50.00	49997.34	-2277.97	0.0611	9.14	-9.39
1.95	50.00	50.00	49997.95	-2269.17	0.0609	8.66	-9.81	50.00	49997.95	-2269.20	0.0609	8.66	-9.81

PSRI TRUCK AND TRACTOR-TRAILER DYNAMIC RESPONSE SIMULATION - TORSION VI TRAILER NO. 3 REAR SUSPENSION - BRAKE SUMMARY

Table with columns: TIME (SEC), TREADLF PRESSURE (PSI), BRAKE PRESSURE (PSI), BRAKE TORQUE (IN-LB), TIRE BRAKE FORCE (LB), WHEEL SLIP, ANGULAR WHEEL VEL. (RAD/SEC), BRAKE PRESSURE (PSI), BRAKE TORQUE (IN-LB), TIRE BRAKE FORCE (LB), WHEEL SLIP, ANGULAR WHEEL VEL. (RAD/SEC), WHEEL ACCEL. (RAD/SEC), ANGULAR WHEEL ACCEL. (RAD/SEC).

TIME (SFC)	LEFT SIDE				RIGHT SIDE			
	TIRE SIDE SLIP ANGLE (DEG)	TIRE LATERAL FORCE (LB)	MU-Y	ALIGNING TORQUE (IN-LB)	TIRE SIDE SLIP ANGLE (DEG)	TIRE LATERAL FORCE (LB)	MU-Y	ALIGNING TORQUE (IN-LB)
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.05	-0.0000	0.0000	0.0000	0.0	-0.0000	0.0000	0.0000	0.0
0.10	0.0000	0.0000	0.0000	0.0	-0.0000	0.0004	0.0000	0.0
0.15	0.0000	-0.0000	-0.0000	0.0	0.0000	-0.0008	-0.0000	0.0
0.20	0.0000	-0.0062	-0.0000	0.0	0.0000	-0.0062	-0.0000	0.0
0.25	0.0000	-0.0037	-0.0000	0.0	0.0000	-0.0037	-0.0000	0.0
0.30	-0.0122	0.0000	0.0000	0.0	-0.0000	0.0122	0.0000	0.0
0.35	-0.0000	0.0535	0.0000	0.0	-0.0000	0.0535	0.0000	0.0
0.40	-0.0001	0.1345	0.0000	0.0	-0.0001	0.1345	0.0000	0.0
0.45	-0.0001	0.2360	0.0001	0.0	-0.0001	0.2359	0.0001	0.0
0.50	-0.0002	0.2944	0.0001	0.0	-0.0002	0.2944	0.0001	0.0
0.55	-0.0001	0.2354	0.0001	0.0	-0.0001	0.2394	0.0001	0.0
0.60	-0.0000	0.0270	0.0000	0.0	-0.0000	0.0270	0.0000	0.0
0.65	0.0002	-0.3712	-0.0001	0.0	0.0002	-0.3713	-0.0001	0.0
0.70	0.0005	-0.5262	-0.0003	0.0	0.0005	-0.5265	-0.0003	0.0
0.75	0.0009	-1.5372	-0.0005	0.0	0.0005	-1.5364	-0.0005	0.0
0.80	0.0011	-2.0500	-0.0006	0.0	0.0011	-2.0606	-0.0006	0.0
0.85	0.0013	-2.3205	-0.0007	0.0	0.0012	-2.3328	-0.0007	0.0
0.90	0.0012	-2.2563	-0.0007	0.0	0.0012	-2.2608	-0.0007	0.0
0.95	0.0010	-1.8158	-0.0006	0.0	0.0010	-1.8240	-0.0006	0.0
1.00	0.0006	-1.0353	-0.0003	0.0	0.0006	-1.0387	-0.0003	0.0
1.05	-0.0000	0.0026	0.0000	0.0	-0.0000	0.0003	0.0000	0.0
1.10	-0.0006	1.1385	0.0003	0.0	-0.0006	1.1345	0.0003	0.0
1.15	-0.0012	2.2358	0.0007	0.0	-0.0012	2.2253	0.0007	0.0
1.20	-0.0017	3.1697	0.0010	0.0	-0.0017	3.1756	0.0010	0.0
1.25	-0.0021	3.9255	0.0012	0.0	-0.0021	3.9121	0.0012	0.0
1.30	-0.0024	4.4721	0.0014	0.0	-0.0024	4.4560	0.0014	0.0
1.35	-0.0027	4.8623	0.0015	0.0	-0.0027	4.8445	0.0015	0.0
1.40	-0.0028	5.1405	0.0016	0.0	-0.0028	5.1222	0.0016	0.0
1.45	-0.0029	5.3378	0.0017	0.0	-0.0029	5.3189	0.0017	0.0
1.50	-0.0030	5.4505	0.0017	0.0	-0.0030	5.4400	0.0017	0.0
1.55	-0.0030	5.4701	0.0017	0.0	-0.0030	5.4517	0.0017	0.0
1.60	-0.0029	5.3154	0.0016	0.0	-0.0029	5.2903	0.0016	0.0
1.65	-0.0027	4.9341	0.0015	0.0	-0.0027	4.9193	0.0015	0.0
1.70	-0.0023	4.2655	0.0013	0.0	-0.0022	4.2545	0.0012	0.0
1.75	-0.0018	3.2873	0.0010	0.0	-0.0018	3.2798	0.0010	0.0
1.80	-0.0011	2.0921	0.0006	0.0	-0.0011	2.0874	0.0006	0.0
1.85	-0.0003	0.6130	0.0002	0.0	-0.0003	0.6085	0.0002	0.0
1.90	0.0007	-1.2520	-0.0004	0.0	0.0007	-1.2620	-0.0004	0.0
1.95	0.0010	-3.4064	-0.0010	0.0	0.0010	-3.4267	-0.0010	0.0

TIME (SEC)	LEFT SIDE				RIGHT SIDE			
	TIRE SIDESLIP ANGLE (DEG)	TIRE LATERAL FORCE (LB)	MU-Y	ALIGNING TORQUE (IN-LB)	TIRE SIDESLIP ANGLE (DEG)	TIRE LATERAL FORCE (LB)	MU-Y	ALIGNING TORQUE (IN-LB)
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.05	-0.0000	0.0000	0.0000	0.0	-0.0000	0.0000	0.0000	0.0
0.10	-0.0000	0.0005	0.0000	0.0	-0.0000	0.0005	0.0000	0.0
0.15	0.0000	0.0007	-0.0000	0.0	0.0000	-0.0007	-0.0000	0.0
0.20	0.0000	-0.0007	-0.0000	0.0	0.0000	0.0007	-0.0000	0.0
0.25	0.0000	-0.0056	-0.0000	0.0	0.0000	-0.0056	-0.0000	0.0
0.30	-0.0000	0.0004	0.0000	0.0	-0.0000	0.0004	0.0000	0.0
0.35	-0.0000	0.0481	0.0000	0.0	-0.0000	0.0481	0.0000	0.0
0.40	-0.0001	0.1316	0.0000	0.0	-0.0001	0.1316	0.0000	0.0
0.45	-0.0002	0.2525	0.0000	0.0	-0.0002	0.2525	0.0000	0.0
0.50	-0.0003	0.3643	0.0000	0.0	-0.0003	0.3643	0.0000	0.0
0.55	-0.0003	0.3960	0.0000	0.0	-0.0003	0.3960	0.0000	0.0
0.60	-0.0002	0.2864	0.0000	0.0	-0.0002	0.2864	0.0000	0.0
0.65	0.0000	-0.0250	-0.0000	0.0	0.0000	-0.0250	-0.0000	0.0
0.70	0.0004	-0.5700	-0.0000	0.0	0.0004	-0.5700	-0.0000	0.0
0.75	0.0010	-1.3114	-0.0000	0.0	0.0010	-1.3114	-0.0000	0.0
0.80	0.0016	-2.1574	-0.0000	0.0	0.0016	-2.1574	-0.0000	0.0
0.85	0.0022	-2.9761	-0.0000	0.0	0.0022	-2.9761	-0.0000	0.0
0.90	0.0027	-3.6441	-0.0000	0.0	0.0027	-3.6441	-0.0000	0.0
0.95	0.0031	-4.0936	-0.0000	0.0	0.0031	-4.0936	-0.0000	0.0
1.00	0.0032	-4.2868	-0.0000	0.0	0.0032	-4.2868	-0.0000	0.0
1.05	0.0032	-4.2233	-0.0000	0.0	0.0032	-4.2233	-0.0000	0.0
1.10	0.0030	-3.5722	-0.0000	0.0	0.0030	-3.5722	-0.0000	0.0
1.15	0.0027	-3.6278	-0.0000	0.0	0.0027	-3.6278	-0.0000	0.0
1.20	0.0024	-3.2621	-0.0000	0.0	0.0024	-3.2621	-0.0000	0.0
1.25	0.0022	-2.5165	-0.0000	0.0	0.0022	-2.5165	-0.0000	0.0
1.30	0.0019	-2.5887	-0.0000	0.0	0.0019	-2.5887	-0.0000	0.0
1.35	0.0017	-2.2505	-0.0000	0.0	0.0017	-2.2505	-0.0000	0.0
1.40	0.0014	-1.8466	-0.0000	0.0	0.0014	-1.8466	-0.0000	0.0
1.45	0.0010	-1.3389	-0.0000	0.0	0.0010	-1.3389	-0.0000	0.0
1.50	0.0005	-0.7601	-0.0000	0.0	0.0005	-0.7601	-0.0000	0.0
1.55	-0.0000	0.0605	0.0000	0.0	-0.0000	0.0605	0.0000	0.0
1.60	-0.0007	0.5129	0.0000	0.0	-0.0007	0.5129	0.0000	0.0
1.65	-0.0014	1.8110	0.0000	0.0	-0.0014	1.8110	0.0000	0.0
1.70	-0.0020	2.7011	0.0000	0.0	-0.0020	2.7011	0.0000	0.0
1.75	-0.0027	3.5450	0.0000	0.0	-0.0027	3.5450	0.0000	0.0
1.80	-0.0033	4.4181	0.0000	0.0	-0.0033	4.4181	0.0000	0.0
1.85	-0.0040	5.3125	0.0000	0.0	-0.0040	5.3125	0.0000	0.0
1.90	-0.0046	6.1245	0.0000	0.0	-0.0046	6.1245	0.0000	0.0
1.95	-0.0051	6.8227	0.0000	0.0	-0.0051	6.8227	0.0000	0.0

TIME (SEC)	LEFT SIDE				RIGHT SIDE				ALIGNING TORQUE (IN-LB)
	TIRE SIDESLIP ANGLE (DEG)	TIRE LATERAL FORCE (LR)	MU-Y	ALIGNING TORQUE (IN-LB)	TIRE SIDESLIP ANGLE (DEG)	TIRE LATERAL FORCE (LR)	MU-Y	ALIGNING TORQUE (IN-LB)	
0.0	0.0	0.0	C.0	0.0	0.0	0.0	C.0	0.0	0.0
0.05	0.0000	-C.0000	-C.0000	0.0	0.0000	-C.0000	-C.0000	0.0	0.0
0.10	0.0000	-C.0001	-C.0000	0.0	0.0000	-C.0000	-C.0000	0.0	0.0
0.15	0.0000	-C.0000	-C.0000	0.0	0.0000	-C.0000	-C.0000	0.0	0.0
0.20	-0.0000	0.0015	C.0000	0.0	-0.0000	0.0015	C.0000	0.0	0.0
0.25	-0.0000	C.0017	C.0000	0.0	-C.0000	0.0017	0.0000	0.0	0.0
0.30	0.0000	-0.0027	-C.0000	0.0	0.0000	-0.0027	0.0000	0.0	0.0
0.35	0.0000	-0.0125	-C.0000	0.0	0.0000	-0.0125	-C.0000	0.0	0.0
0.40	C.0000	-0.0307	-C.0000	0.0	C.0000	-0.0307	-C.0000	0.0	0.0
0.45	0.0000	-C.0455	-C.0000	0.0	0.0000	-0.0455	-C.0000	0.0	0.0
0.50	0.0000	-0.0515	-C.0000	0.0	0.0000	-0.0515	-C.0000	0.0	0.0
0.55	C.0000	-0.0142	-C.0000	0.0	0.0000	-0.0142	-C.0000	0.0	0.0
0.60	-0.0001	0.0666	C.0000	0.0	-0.0001	0.0665	0.0000	0.0	0.0
0.65	-0.0002	0.1756	C.0001	0.0	-C.0002	0.1756	C.0001	0.0	0.0
0.70	-0.0003	C.2863	0.0001	0.0	-0.0003	0.2862	C.0001	0.0	0.0
0.75	-0.0003	0.3547	C.0002	0.0	-0.0003	0.3543	C.0002	0.0	0.0
0.80	-0.0003	0.3437	C.0002	0.0	-0.0002	0.3439	C.0002	0.0	0.0
0.85	-0.0002	0.2442	C.0001	0.0	-0.0002	0.2445	C.0001	0.0	0.0
0.90	-0.0001	0.0843	C.0000	0.0	-0.0001	0.0845	0.0000	0.0	0.0
0.95	0.0001	-C.0681	-0.0000	0.0	0.0001	-0.0682	-0.0000	0.0	0.0
1.00	0.0001	-0.1527	-C.0001	0.0	0.0001	-0.1540	-0.0001	0.0	0.0
1.05	0.0001	-C.1425	-C.0001	0.0	0.0001	-0.1427	-C.0001	0.0	0.0
1.10	C.0000	-0.0239	-C.0000	0.0	0.0000	-0.0239	-C.0000	0.0	0.0
1.15	-0.0002	C.1705	0.0001	0.0	-0.0002	0.1705	0.0001	0.0	0.0
1.20	-0.0004	0.3815	0.0002	0.0	-0.0004	0.3813	0.0002	0.0	0.0
1.25	-C.0005	0.5611	C.0003	0.0	-C.0005	0.5606	C.0003	0.0	0.0
1.30	-0.0006	C.6600	C.0003	0.0	-0.0006	0.6593	C.0003	0.0	0.0
1.35	-0.0006	C.6600	C.0003	0.0	-0.0006	0.6591	C.0003	0.0	0.0
1.40	-C.0005	C.5845	C.0003	0.0	-C.0005	0.5838	C.0003	0.0	0.0
1.45	-C.0004	0.4765	0.0002	0.0	-C.0004	0.4759	0.0002	0.0	0.0
1.50	-C.0004	C.3755	0.0002	0.0	-C.0004	0.3753	0.0002	0.0	0.0
1.55	-C.0003	0.3055	0.0002	0.0	-0.0003	0.3054	0.0002	0.0	0.0
1.60	-0.0002	C.2615	C.0001	0.0	-C.0002	0.2610	C.0001	0.0	0.0
1.65	-0.0002	0.2084	C.0001	0.0	-0.0002	0.2080	C.0001	0.0	0.0
1.70	-0.0001	C.0591	C.0001	0.0	-0.0001	0.0989	C.0001	0.0	0.0
1.75	0.0001	-C.1064	-0.0001	0.0	0.0001	-0.1062	-0.0001	0.0	0.0
1.80	0.0004	-C.4718	-C.0002	0.0	0.0004	-0.4711	-C.0002	0.0	0.0
1.85	0.0009	-C.5557	-C.0005	0.0	0.0009	-0.5550	-C.0005	0.0	0.0
1.90	0.0015	-1.5845	-0.0008	0.0	0.0015	-1.5846	-0.0008	0.0	0.0
1.95	C.0020	-2.1666	-C.0011	0.0	C.0020	-2.1710	-C.0011	0.0	0.0



TIME (SEC)	LEFT SIDE				RIGHT SIDE			
	TIRE SIDESLIP ANGLE (DEG)	TIRE LATERAL FORCE (LB)	MU-Y	ALIGNING TORQUE (IN-LB)	TIRE SIDESLIP ANGLE (DEG)	TIRE LATERAL FORCE (LB)	MU-Y	ALIGNING TORQUE (IN-LB)
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.05	0.0000	-0.0000	-0.0000	0.0	0.0000	-0.0000	-0.0000	0.0
0.10	0.0000	-0.0000	-0.0000	0.0	0.0000	-0.0000	-0.0000	0.0
0.15	-0.0000	0.0000	0.0000	0.0	-0.0000	0.0000	0.0000	0.0
0.20	-0.0000	0.0000	0.0000	0.0	-0.0000	0.0000	0.0000	0.0
0.25	0.0000	-0.0000	-0.0000	0.0	0.0000	-0.0000	-0.0000	0.0
0.30	0.0000	-0.0000	-0.0000	0.0	0.0000	-0.0000	-0.0000	0.0
0.35	0.0000	-0.0000	-0.0000	0.0	0.0000	-0.0000	-0.0000	0.0
0.40	0.0000	-0.0000	-0.0000	0.0	0.0000	-0.0000	-0.0000	0.0
0.45	-0.0000	0.0000	0.0000	0.0	-0.0000	0.0000	0.0000	0.0
0.50	-0.0001	0.0000	0.0000	0.0	-0.0001	0.0000	0.0000	0.0
0.55	-0.0002	0.0000	0.0000	0.0	-0.0002	0.0000	0.0000	0.0
0.60	-0.0003	0.0000	0.0000	0.0	-0.0003	0.0000	0.0000	0.0
0.65	-0.0004	0.0000	0.0000	0.0	-0.0004	0.0000	0.0000	0.0
0.70	-0.0004	0.0000	0.0000	0.0	-0.0004	0.0000	0.0000	0.0
0.75	-0.0002	0.0000	0.0000	0.0	-0.0002	0.0000	0.0000	0.0
0.80	0.0002	-0.0000	-0.0000	0.0	0.0002	-0.0000	-0.0000	0.0
0.85	0.0007	-0.0000	-0.0000	0.0	0.0007	-0.0000	-0.0000	0.0
0.90	0.0014	-0.0000	-0.0000	0.0	0.0014	-0.0000	-0.0000	0.0
0.95	0.0021	-0.0000	-0.0000	0.0	0.0021	-0.0000	-0.0000	0.0
1.00	0.0028	-0.0000	-0.0000	0.0	0.0028	-0.0000	-0.0000	0.0
1.05	0.0033	-0.0000	-0.0000	0.0	0.0033	-0.0000	-0.0000	0.0
1.10	0.0036	-0.0000	-0.0000	0.0	0.0036	-0.0000	-0.0000	0.0
1.15	0.0038	-0.0000	-0.0000	0.0	0.0038	-0.0000	-0.0000	0.0
1.20	0.0038	-0.0000	-0.0000	0.0	0.0038	-0.0000	-0.0000	0.0
1.25	0.0038	-0.0000	-0.0000	0.0	0.0038	-0.0000	-0.0000	0.0
1.30	0.0038	-0.0000	-0.0000	0.0	0.0038	-0.0000	-0.0000	0.0
1.35	0.0037	-0.0000	-0.0000	0.0	0.0037	-0.0000	-0.0000	0.0
1.40	0.0036	-0.0000	-0.0000	0.0	0.0036	-0.0000	-0.0000	0.0
1.45	0.0035	-0.0000	-0.0000	0.0	0.0035	-0.0000	-0.0000	0.0
1.50	0.0032	-0.0000	-0.0000	0.0	0.0032	-0.0000	-0.0000	0.0
1.55	0.0027	-0.0000	-0.0000	0.0	0.0027	-0.0000	-0.0000	0.0
1.60	0.0020	-0.0000	-0.0000	0.0	0.0020	-0.0000	-0.0000	0.0
1.65	0.0011	-0.0000	-0.0000	0.0	0.0011	-0.0000	-0.0000	0.0
1.70	0.0002	-0.0000	-0.0000	0.0	0.0002	-0.0000	-0.0000	0.0
1.75	-0.0008	0.0000	0.0000	0.0	-0.0008	0.0000	0.0000	0.0
1.80	-0.0017	0.0000	0.0000	0.0	-0.0017	0.0000	0.0000	0.0
1.85	-0.0027	0.0000	0.0000	0.0	-0.0027	0.0000	0.0000	0.0
1.90	-0.0038	0.0000	0.0000	0.0	-0.0038	0.0000	0.0000	0.0
1.95	-0.0049	0.0000	0.0000	0.0	-0.0049	0.0000	0.0000	0.0

TRUCK AND TRACTOR-TRAILER DYNAMIC RESPONSE SIMULATION - T3DRS.VL  
 SAMPLE RUN - TRIPLES BRAKING IN A TURN, ALL OPTIONS EXERCISED  
 TRAILER NO. 3 FRONT SUSPENSION - UNSPRUNG MASS SUMMARY  
 LEADING TANDEM AXLE

AXLE MOTION

DYNAMIC SUSPENSION MOTIONS AND FORCES

TIME (SEC)	POSITION		VELOCITY		LEFT SIDE				RIGHT SIDE		
	VERTICAL (FT)	ROLL (DEG)	VERTICAL (FT/SEC)	ROLL (DEG/SEC)	AUXILIARY ROLL TORQUE (IN-LB)	SUSP. DEFLECT. (IN)	SUSP. VELOCITY (IN/SEC)	SUSP. FORCE (LB)	SUSP. DEFLECT. (IN)	SUSP. VELOCITY (IN/SEC)	SUSP. FORCE (LB)
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-0.0	0.0	0.0	-0.0
0.05	0.0	0.0000	0.0	-0.0000	0.00	-0.0000	-0.0000	-0.00	-0.0000	-0.0000	-0.00
0.10	0.0	-0.0000	0.0	-0.0000	-0.00	-0.0000	-0.0000	-0.01	-0.0000	-0.0000	-0.01
0.15	0.0000	-0.0000	0.0000	0.0000	0.00	0.0000	0.0037	-3.91	0.0000	0.0037	-3.91
0.20	0.0005	0.0000	0.0000	0.0000	0.02	0.0017	-0.0098	-76.18	0.0017	-0.0098	-76.18
0.25	0.0025	0.0000	0.0000	-0.0000	-0.02	-0.0024	-0.0289	-256.59	-0.0024	-0.0289	-256.59
0.30	0.0052	-0.0000	0.0052	-0.0000	-0.10	-0.0172	-0.2752	-565.27	-0.0172	-0.2752	-565.27
0.35	0.0066	-0.0000	0.0120	-0.0001	-0.13	-0.0256	-0.4109	-709.99	-0.0256	-0.4109	-710.01
0.40	0.0071	-0.0000	0.0121	-0.0003	-0.01	-0.0235	-0.6160	-774.75	-0.0235	-0.6161	-774.74
0.45	0.0080	-0.0000	0.0235	-0.0004	0.50	-0.0262	-0.8372	-874.37	-0.0262	-0.8365	-874.27
0.50	0.0085	-0.0001	0.0100	-0.0003	1.63	-0.0325	-1.0543	-960.26	-0.0325	-1.0536	-959.97
0.55	0.0091	-0.0001	0.0001	0.0000	3.24	-0.0327	-1.2456	-984.27	-0.0326	-1.2462	-983.74
0.60	0.0093	-0.0000	0.0000	0.0000	4.59	-0.0316	-1.4034	-1009.69	-0.0315	-1.4038	-1008.97
0.65	0.0098	0.0000	0.0000	0.0014	4.73	-0.0346	-1.5678	-1056.10	-0.0345	-1.5681	-1055.41
0.70	0.0100	0.0001	0.0000	0.0022	2.73	-0.0367	-1.7031	-1078.83	-0.0367	-1.7038	-1078.51
0.75	0.0100	0.0002	0.0010	0.0026	-2.01	-0.0361	-1.8066	-1083.83	-0.0361	-1.8043	-1084.31
0.80	0.0102	0.0003	0.0040	0.0025	-5.27	-0.0367	-1.9352	-1101.16	-0.0368	-1.9383	-1102.77
0.85	0.0104	0.0005	0.0017	0.0017	-18.00	-0.0383	-2.1040	-1117.34	-0.0386	-2.1073	-1120.27
0.90	0.0104	0.0005	-0.0010	0.0003	-26.37	-0.0382	-2.2169	-1117.66	-0.0387	-2.2141	-1121.79
0.95	0.0104	0.0005	0.0005	-0.0013	-32.45	-0.0376	-2.3010	-1117.51	-0.0382	-2.3007	-1122.44
1.00	0.0104	0.0004	0.0013	-0.0029	-35.08	-0.0379	-2.3687	-1123.31	-0.0385	-2.3650	-1128.52
1.05	0.0104	0.0002	-0.0000	-0.0040	-34.02	-0.0380	-2.4065	-1124.71	-0.0387	-2.4076	-1129.66
1.10	0.0104	-0.0000	-0.0004	-0.0045	-25.83	-0.0376	-2.4068	-1122.57	-0.0382	-2.4088	-1126.83
1.15	0.0104	-0.0002	0.0000	-0.0043	-23.94	-0.0375	-2.4063	-1124.55	-0.0380	-2.4040	-1127.91
1.20	0.0105	-0.0004	0.0004	-0.0035	-18.03	-0.0379	-2.4057	-1128.23	-0.0383	-2.4037	-1130.73
1.25	0.0105	-0.0006	-0.0001	-0.0024	-13.42	-0.0381	-2.4003	-1129.22	-0.0383	-2.4016	-1131.10
1.30	0.0105	-0.0007	0.0004	-0.0015	-10.81	-0.0381	-2.4003	-1130.20	-0.0383	-2.4027	-1131.75
1.35	0.0105	-0.0007	0.0000	-0.0008	-9.87	-0.0383	-2.4006	-1132.82	-0.0385	-2.4059	-1134.27
1.40	0.0105	-0.0008	0.0001	-0.0005	-9.52	-0.0386	-2.4014	-1134.34	-0.0387	-2.4012	-1135.73
1.45	0.0105	-0.0008	-0.0001	-0.0005	-8.44	-0.0386	-2.4011	-1134.19	-0.0387	-2.4018	-1135.37
1.50	0.0105	-0.0008	0.0001	-0.0006	-5.61	-0.0385	-2.4006	-1134.30	-0.0386	-2.4009	-1134.99
1.55	0.0105	-0.0008	-0.0000	-0.0005	-6.64	-0.0396	-2.4003	-1134.70	-0.0386	-2.4019	-1134.60
1.60	0.0105	-0.0009	-0.0002	-0.0001	6.06	-0.0386	-2.4015	-1134.40	-0.0385	-2.4042	-1133.26
1.65	0.0105	-0.0009	-0.0001	0.0007	13.46	-0.0385	-2.4007	-1133.98	-0.0382	-2.4035	-1131.75
1.70	0.0105	-0.0008	-0.0000	0.0019	20.33	-0.0385	-2.4005	-1134.13	-0.0381	-2.4019	-1130.90
1.75	0.0105	-0.0007	-0.0001	0.0032	25.63	-0.0385	-2.4005	-1134.14	-0.0380	-2.4021	-1130.19
1.80	0.0105	-0.0005	-0.0001	0.0043	28.54	-0.0384	-2.4015	-1133.63	-0.0375	-2.4021	-1129.33
1.85	0.0105	-0.0002	-0.0000	0.0055	29.81	-0.0384	-2.4004	-1133.29	-0.0378	-2.4007	-1128.81
1.90	0.0105	0.0001	0.0002	0.0066	30.84	-0.0384	-2.4023	-1133.86	-0.0378	-2.4019	-1129.21
1.95	0.0105	0.0004	0.0004	0.0073	31.60	-0.0386	-2.4044	-1135.38	-0.0380	-2.4043	-1130.63

AXLE MOTION

DYNAMIC SUSPENSION MOTIONS AND FORCES

TIME (SEC)	POSITION			VELOCITY			LEFT SIDE			RIGHT SIDE		
	VERTICAL (FT)	ROLL (DEG)	ROLL (DEG/SEC)	VERTICAL (FT/SEC)	ROLL (DEG/SEC)	AUXILIARY ROLL TORQUE (IN-LB)	SUSP. DEFLECT. (IN)	SUSP. VELFCY (IN/SEC)	SUSP. FORCE (LB)	SUSP. DEFLECT. (IN)	SUSP. VELFCY (IN/SEC)	SUSP. FORCE (LB)
0.0	0.0	0.0000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.05	0.0	0.0000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.10	0.0	0.0000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.15	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.20	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
0.25	0.0004	0.0000	0.0000	0.0015	0.0000	0.0000	0.0017	0.0000	0.0000	0.0000	0.0000	0.0000
0.30	0.0013	0.0000	0.0000	0.0035	0.0000	0.0000	0.0016	0.0000	0.0000	0.0000	0.0000	0.0000
0.35	0.0016	0.0000	0.0000	0.0035	0.0000	0.0000	0.0016	0.0000	0.0000	0.0000	0.0000	0.0000
0.40	0.0014	0.0000	0.0000	0.0034	0.0000	0.0000	0.0016	0.0000	0.0000	0.0000	0.0000	0.0000
0.45	0.0017	0.0000	0.0000	0.0037	0.0000	0.0000	0.0017	0.0000	0.0000	0.0000	0.0000	0.0000
0.50	0.0020	0.0000	0.0000	0.0041	0.0000	0.0000	0.0018	0.0000	0.0000	0.0000	0.0000	0.0000
0.55	0.0019	0.0000	0.0000	0.0037	0.0000	0.0000	0.0017	0.0000	0.0000	0.0000	0.0000	0.0000
0.60	0.0019	0.0000	0.0000	0.0037	0.0000	0.0000	0.0017	0.0000	0.0000	0.0000	0.0000	0.0000
0.65	0.0021	0.0000	0.0000	0.0041	0.0000	0.0000	0.0018	0.0000	0.0000	0.0000	0.0000	0.0000
0.70	0.0022	0.0000	0.0000	0.0042	0.0000	0.0000	0.0018	0.0000	0.0000	0.0000	0.0000	0.0000
0.75	0.0021	0.0000	0.0000	0.0041	0.0000	0.0000	0.0018	0.0000	0.0000	0.0000	0.0000	0.0000
0.80	0.0022	0.0000	0.0000	0.0042	0.0000	0.0000	0.0018	0.0000	0.0000	0.0000	0.0000	0.0000
0.85	0.0023	0.0000	0.0000	0.0043	0.0000	0.0000	0.0018	0.0000	0.0000	0.0000	0.0000	0.0000
0.90	0.0023	0.0000	0.0000	0.0043	0.0000	0.0000	0.0018	0.0000	0.0000	0.0000	0.0000	0.0000
0.95	0.0023	0.0000	0.0000	0.0043	0.0000	0.0000	0.0018	0.0000	0.0000	0.0000	0.0000	0.0000
1.00	0.0023	0.0000	0.0000	0.0043	0.0000	0.0000	0.0018	0.0000	0.0000	0.0000	0.0000	0.0000
1.05	0.0023	0.0000	0.0000	0.0043	0.0000	0.0000	0.0018	0.0000	0.0000	0.0000	0.0000	0.0000
1.10	0.0022	0.0000	0.0000	0.0042	0.0000	0.0000	0.0018	0.0000	0.0000	0.0000	0.0000	0.0000
1.15	0.0022	0.0000	0.0000	0.0042	0.0000	0.0000	0.0018	0.0000	0.0000	0.0000	0.0000	0.0000
1.20	0.0023	0.0000	0.0000	0.0043	0.0000	0.0000	0.0018	0.0000	0.0000	0.0000	0.0000	0.0000
1.25	0.0022	0.0000	0.0000	0.0042	0.0000	0.0000	0.0018	0.0000	0.0000	0.0000	0.0000	0.0000
1.30	0.0022	0.0000	0.0000	0.0042	0.0000	0.0000	0.0018	0.0000	0.0000	0.0000	0.0000	0.0000
1.35	0.0023	0.0000	0.0000	0.0043	0.0000	0.0000	0.0018	0.0000	0.0000	0.0000	0.0000	0.0000
1.40	0.0023	0.0000	0.0000	0.0043	0.0000	0.0000	0.0018	0.0000	0.0000	0.0000	0.0000	0.0000
1.45	0.0023	0.0000	0.0000	0.0043	0.0000	0.0000	0.0018	0.0000	0.0000	0.0000	0.0000	0.0000
1.50	0.0023	0.0000	0.0000	0.0043	0.0000	0.0000	0.0018	0.0000	0.0000	0.0000	0.0000	0.0000
1.55	0.0023	0.0000	0.0000	0.0043	0.0000	0.0000	0.0018	0.0000	0.0000	0.0000	0.0000	0.0000
1.60	0.0023	0.0000	0.0000	0.0043	0.0000	0.0000	0.0018	0.0000	0.0000	0.0000	0.0000	0.0000
1.65	0.0023	0.0000	0.0000	0.0043	0.0000	0.0000	0.0018	0.0000	0.0000	0.0000	0.0000	0.0000
1.70	0.0023	0.0000	0.0000	0.0043	0.0000	0.0000	0.0018	0.0000	0.0000	0.0000	0.0000	0.0000
1.75	0.0023	0.0000	0.0000	0.0043	0.0000	0.0000	0.0018	0.0000	0.0000	0.0000	0.0000	0.0000
1.80	0.0022	0.0000	0.0000	0.0042	0.0000	0.0000	0.0018	0.0000	0.0000	0.0000	0.0000	0.0000
1.85	0.0022	0.0000	0.0000	0.0042	0.0000	0.0000	0.0018	0.0000	0.0000	0.0000	0.0000	0.0000
1.90	0.0022	0.0000	0.0000	0.0042	0.0000	0.0000	0.0018	0.0000	0.0000	0.0000	0.0000	0.0000
1.95	0.0023	0.0000	0.0000	0.0043	0.0000	0.0000	0.0018	0.0000	0.0000	0.0000	0.0000	0.0000

TIME (SEC)	POSITION			VELOCITY			LEFT SIDE			RIGHT SIDE		
	VERTICAL (FT)	ROLL (DEG)	REAR (FT)	VERTICAL (FT/SEC)	ROLL (DEG/SEC)	AUXILIARY ROLL TORQUE (IN-LB)	SUSP. DEFLECT. (IN)	SUSP. VELOCITY (IN/SEC)	SUSP. FORCE (LB)	SUSP. DEFLECT. (IN)	SUSP. VELOCITY (IN/SEC)	SUSP. FORCE (LB)
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.05	0.0	-0.0000	0.0	-0.0000	-0.0000	-0.00	0.0000	0.0000	0.00	0.0000	0.0000	0.00
0.10	0.0	0.0000	0.0	0.0000	0.0000	0.00	0.0000	0.0000	0.00	0.0000	0.0000	0.00
0.15	0.0000	-0.0000	0.0000	0.0000	-0.0000	0.00	0.0000	0.0000	-3.23	0.0000	0.0000	-3.23
0.20	0.0001	-0.0000	0.0000	0.0000	-0.0000	-0.01	0.0059	0.2850	-10.41	0.0059	0.2850	-10.42
0.25	0.0003	0.0000	0.0000	-0.0177	0.0000	-0.05	0.0283	0.6550	41.70	0.0283	0.6550	41.69
0.30	0.0014	0.0000	0.0000	-0.0201	0.0000	-0.06	0.0616	0.5912	146.71	0.0616	0.5912	146.71
0.35	0.0017	0.0000	0.0000	0.0055	-0.0000	0.07	0.0843	0.2562	176.76	0.0843	0.2562	176.78
0.40	0.0014	-0.0000	0.0000	0.0000	0.0001	0.51	0.0932	0.1611	153.95	0.0932	0.1613	154.04
0.45	0.0016	-0.0000	0.0000	-0.0112	-0.0002	1.44	0.1032	0.2525	180.80	0.1032	0.2525	181.05
0.50	0.0021	-0.0000	0.0000	-0.0031	-0.0003	2.80	0.1149	0.1650	216.84	0.1150	0.1655	217.29
0.55	0.0020	-0.0000	0.0000	0.0045	-0.0003	4.10	0.1200	0.0435	209.49	0.1201	0.0435	210.12
0.60	0.0019	-0.0000	0.0000	-0.0024	-0.0002	4.45	0.1223	0.0768	205.40	0.1224	0.0766	206.04
0.65	0.0021	-0.0000	0.0000	-0.0045	0.0002	2.86	0.1270	0.0596	226.10	0.1271	0.0586	226.42
0.70	0.0022	-0.0000	0.0000	0.0000	0.0008	-1.40	0.1309	0.0386	235.45	0.1309	0.0364	235.06
0.75	0.0021	0.0000	0.0000	0.0007	0.0014	-6.41	0.1320	0.0201	231.88	0.1315	0.0170	230.38
0.80	0.0022	0.0001	0.0001	-0.0025	0.0019	-17.29	0.1335	0.0443	238.40	0.1332	0.0408	235.56
0.85	0.0023	0.0002	0.0002	-0.0000	0.0015	-26.36	0.1356	0.0289	247.41	0.1352	0.0257	243.27
0.90	0.0023	0.0003	0.0003	0.0012	0.0014	-33.53	0.1364	0.0021	246.33	0.1358	0.0000	241.23
0.95	0.0022	0.0004	0.0004	-0.0001	0.0005	-37.06	0.1365	0.0069	244.16	0.1358	0.0064	238.68
1.00	0.0023	0.0003	0.0003	-0.0000	-0.0006	-36.11	0.1370	0.0105	246.03	0.1363	0.0117	240.83
1.05	0.0023	0.0003	0.0003	0.0000	-0.0016	-30.87	0.1373	-0.0014	245.34	0.1367	0.0013	241.03
1.10	0.0022	0.0002	0.0002	0.0004	-0.0023	-22.58	0.1371	-0.0033	242.32	0.1367	0.0022	239.29
1.15	0.0022	0.0001	0.0001	-0.0004	-0.0024	-13.11	0.1371	0.0040	241.94	0.1368	0.0075	240.31
1.20	0.0022	-0.0000	0.0000	-0.0002	-0.0021	-4.29	0.1373	0.0032	242.86	0.1372	0.0062	242.48
1.25	0.0022	-0.0001	0.0001	0.0001	-0.0014	7.46	0.1374	-0.0000	242.55	0.1374	0.0020	243.08
1.30	0.0023	-0.0002	0.0002	-0.0002	-0.0007	6.69	0.1374	0.0030	242.77	0.1376	0.0042	243.84
1.35	0.0023	-0.0002	0.0002	-0.0003	-0.0001	8.95	0.1376	0.0046	244.22	0.1378	0.0052	245.58
1.40	0.0023	-0.0002	0.0002	0.0000	0.0000	10.40	0.1378	0.0010	244.88	0.1380	0.0015	246.46
1.45	0.0023	-0.0002	0.0002	0.0001	-0.0001	12.32	0.1378	-0.0004	244.46	0.1380	0.0001	246.35
1.50	0.0023	-0.0003	0.0003	-0.0000	0.0005	15.61	0.1378	0.0003	244.10	0.1381	0.0012	246.52
1.55	0.0023	-0.0003	0.0003	0.0001	-0.0008	20.43	0.1377	-0.0015	243.63	0.1381	0.0006	246.80
1.60	0.0023	-0.0003	0.0003	0.0002	-0.0005	26.15	0.1376	-0.0031	242.48	0.1381	-0.0005	246.51
1.65	0.0023	-0.0003	0.0003	0.0001	-0.0007	31.65	0.1375	-0.0021	241.39	0.1381	-0.0003	246.20
1.70	0.0023	-0.0004	0.0004	-0.0000	-0.0000	35.66	0.1374	-0.0008	240.90	0.1381	-0.0003	246.23
1.75	0.0023	-0.0003	0.0003	0.0001	0.0009	37.15	0.1374	-0.0009	240.53	0.1381	-0.0009	246.00
1.80	0.0022	-0.0003	0.0003	0.0001	0.0015	35.87	0.1373	-0.0008	240.11	0.1380	-0.0017	245.32
1.85	0.0022	-0.0002	0.0002	0.0000	0.0026	32.52	0.1373	0.0005	240.08	0.1379	-0.0010	244.75
1.90	0.0022	-0.0000	0.0000	-0.0001	0.0025	27.57	0.1374	0.0027	240.83	0.1375	0.0006	244.72
1.95	0.0023	0.0001	0.0001	-0.0002	0.0031	21.20	0.1375	0.0045	242.36	0.1379	0.0018	245.28

AXLE ACTION DYNAMIC SUSPENSION ACTIONS AND FORCES TRAILING TANDEM AXLE

TIME (SEC)	POSITION			VELOCITY			LEFT SIDE			RIGHT SIDE		
	VERTICAL (FT)	ROLL (DEG)	RCLL (IN)	VERTICAL (FT/SEC)	RCLL (DEG/SEC)	AUXILIARY ROLL TORQUE (IN-LB)	SUSP. DEFLECT. (IN)	SUSP. VELOCITY (IN/SEC)	SUSP. FORCE (LB)	SUSP. DEFLECT. (IN)	SUSP. VELOCITY (IN/SEC)	SUSP. FORCE (LB)
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.05	0.0	-0.0000	-0.0000	0.0	-0.0000	-0.0000	0.0	0.0000	0.00	0.0000	0.0000	0.00
0.10	0.0	0.0000	0.0000	0.0	-0.0000	0.0000	0.0	0.0000	0.01	0.0000	0.0000	0.01
0.15	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	0.0000	-0.0000	0.0000	2.30	-0.0000	0.0000	2.30
0.20	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	0.0000	0.0000	65.32	0.0000	0.0000	65.32
0.25	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	0.0000	0.0000	285.21	0.0010	0.0010	285.21
0.30	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	0.0000	0.0000	571.48	0.0138	0.0138	571.48
0.35	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	0.0000	0.0000	720.31	0.0404	0.0404	720.31
0.40	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	0.0000	0.0000	772.48	0.0578	0.0578	772.48
0.45	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	0.0000	0.0000	870.44	0.0601	0.0601	870.44
0.50	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	0.0000	0.0000	963.58	0.0664	0.0664	963.58
0.55	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	0.0000	0.0000	987.07	0.0767	0.0767	987.07
0.60	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	0.0000	0.0000	1007.94	0.0795	0.0795	1007.94
0.65	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	0.0000	0.0000	1054.71	0.0837	0.0837	1054.71
0.70	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	0.0000	0.0000	1080.15	0.0872	0.0872	1080.15
0.75	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	0.0000	0.0000	1084.41	0.0875	0.0875	1084.41
0.80	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	0.0000	0.0000	1055.52	0.0886	0.0886	1055.52
0.85	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	0.0000	0.0000	1116.56	0.0907	0.0907	1116.56
0.90	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	0.0000	0.0000	1118.05	0.0912	0.0912	1118.05
1.00	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	0.0000	0.0000	1117.90	0.0913	0.0913	1117.90
1.05	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	0.0000	0.0000	1123.45	0.0915	0.0915	1123.45
1.10	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	0.0000	0.0000	1125.39	0.0915	0.0915	1125.39
1.15	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	0.0000	0.0000	1124.07	0.0911	0.0911	1124.07
1.20	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	0.0000	0.0000	1126.28	0.0909	0.0909	1126.28
1.25	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	0.0000	0.0000	1129.90	0.0912	0.0912	1129.90
1.30	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	0.0000	0.0000	1132.46	0.0912	0.0912	1132.46
1.35	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	0.0000	0.0000	1135.10	0.0915	0.0915	1135.10
1.40	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	0.0000	0.0000	1136.48	0.0917	0.0917	1136.48
1.45	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	0.0000	0.0000	1136.37	0.0917	0.0917	1136.37
1.50	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	0.0000	0.0000	1136.53	0.0915	0.0915	1136.53
1.55	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	0.0000	0.0000	1136.15	0.0916	0.0916	1136.15
1.60	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	0.0000	0.0000	1135.46	0.0915	0.0915	1135.46
1.65	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	0.0000	0.0000	1135.23	0.0913	0.0913	1135.23
1.70	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	0.0000	0.0000	1134.70	0.0912	0.0912	1134.70
1.75	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	0.0000	0.0000	1133.51	0.0912	0.0912	1133.51
1.80	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	0.0000	0.0000	1132.57	0.0912	0.0912	1132.57
1.85	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	0.0000	0.0000	1132.34	0.0913	0.0913	1132.34
1.90	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	0.0000	0.0000	1132.95	0.0913	0.0913	1132.95
1.95	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	-0.0000	0.0000	0.0000	1131.07	0.0915	0.0915	1131.07



APPENDIX C  
INPUT PARAMETER REFERENCE LIST  
TRUCK AND TRACTOR/TRAILER DYNAMIC RESPONSE SIMULATION PROGRAM - T3DRS:VI

Parameter Name	Description	Engineering Units	Format*	Program Symbol	Options Available	User Manual Section	Comments
Title Line	User Identification of Run		20A4	HEAD		3.1, 3.2	First line of input list
Simulation Operation	Parameters						
Vehicle Configuration	Number of trailers		I2	NVEH		3.2	Zero=Truck or bobtail tractor; 3 max.
Initial Velocity	Vehicle speed at beginning of simulation	ft/sec	F15.3	VEL		3.2	
Steer Input Table	Number of lines in table Pos. - Path-Follower Table Neg. - Steer Angle Table		I3 2F10.2	ISTEER XP,YP		3.2 3.2, App. G.	Zero lines=Straight ahead Max. of 25 lines
End of Preview Interval	Driver's view distance ahead (in time)	sec	F10.4	TURNX, TURNY	side-to side	3.2	Typ. 11-3 sec } Appear only with 1 sec. max. } path-follower mode
Driver Transport Lag	Pure time lag in driver model	sec	F10.4	TFF		3.2, App. G	Maximum of 10 lines
Treadle Pressure Table	Number of lines in table Time-pressure table entries	sec, psi	I2 2F10.2	TAUMEM NTP XTP,YTP		3.2, App. G 3.2	
Max. Simulation Time	Length of time of simulation run	sec	F15.3	TIMF		3.2	
Time Increment of Output	Simulation time interval of print-out lines	sec	F15.3	TINC		3.2	
Road Key	Choice of following road options Neg. - User written road sub-routine call Zero - Flat, horizontal road Pos. - Planar road w/downgrade & cross-slope	- , % , %	I2	ROAD		3.2 App. H	May be used for rough roads, etc.
Output Page Option Keys	Seven digits key for seven page types (0=no print, 1=print) as follows -Sprung Mass Position Page -Sprung Mass Velocity Page -Sprung Mass Acceleration Page -Tire Forces Page -Brake Summary Page -Lateral Pages -Unsprung Mass Page		I2 I2 I2, 2F10.2	ROAD ROAD ROAD, OZDXO, OZDYO			
Truck/Tractor/Trailer Parameters							
Wheelbase	Center-to-center distance, front-to-rear suspensions on trucks/tractors/full trailers; kingpin to center of rear suspension on semitrailers	in.	F15.3	WHBS		3.3.1, 3.4.1, 3.5.1	

\*All formats begin in Column 1, additional columns may be used for users' comments, labels, etc.





Base Vehicle Curb Mt. on FA	Front axle curb weight on trucks/tractors/full trailers w/o payload or hitch load	lb	F15.3	SNL(,1)	3.3.1, 3.5.1	Payload may be included in base vehicle
Base Vehicle Kingpin Static Load	Weight at kingpin of semitrailer w/o payload or hitch loads	lb	F15.3	SNL(,1)	3.4.1	Payload may be included in base vehicle
Base Vehicle Curb Mt. on RA	Rear axle curb weight w/o payload or hitch loads	lb	F15.3	SNL(,2)	3.3.1, 3.4.1, 3.5.1	Payload may be included in base vehicle
Sprung Mass CG Height	Distance above ground (at final load conditions)	in.	F15.3	DELTA	3.3.1	
Sprung Mass	Moment of inertia properties of sprung mass only				3.3.1	
-Roll Moment of Inertia		in-lb-sec <sup>2</sup>	F15.3	VJ(,1)	3.3.1, 3.4.1 3.3.1, 3.4.1	May be lumped in with base vehicle
-Pitch Moment of Inertia		in-lb-sec <sup>2</sup>	F15.3	VJ(,2)		
-Yaw Moment of Inertia		in-lb-sec <sup>2</sup>	F15.3	VJ(,3)		
Payload Weight	Long. location ahead of rear susp.	lb	F15.3	PW	3.3.1, 3.4.1	
-Dist. Ahead of Rear Susp.	Height above ground (at full load condition)	in.	F15.3	PX		
-CG Height	Height above ground (at full load condition)	in.	F15.3	PZ	3.3.1, 3.4.1	
-Roll Moment of Inertia	Payload moment of inertia properties	in-lb-sec <sup>2</sup>	F15.3	PJ(,1)	3.3.1, 3.4.1	Entries only when payload is not zero
-Pitch Moment of Inertia	" " " "	in-lb-sec <sup>2</sup>	F15.3	PJ(,2)	3.3.1, 3.4.1	
-Yaw Moment of Inertia	" " " "	in-lb-sec <sup>2</sup>	F15.3	PJ(,3)	3.3.1, 3.4.1	
Fifth Wheel Location	Long. distance ahead of rear susp.	in.	F15.3	BB1	3.3.1	Entries in tractor parameters only when trailers are specified in configuration
Fifth Wheel Height	Height above ground at pitch articulation	in.	F15.3	D		
Fifth Wheel Stiffness	Roll stiffness (Typ. = 250,000)	in-lb/deg	F15.3	MC5	3.3.1	
Dolly Key	Choice of converter (1) or fixed (2) dolly		I2	KDOLLY	3.5.1	
Dist. from Turntable Center to Pintle Hook	Length of dolly tongue	in.	F15.3	APHI	3.5.1	Entries only with a full trailer (enter preceding full trailer wheelbase)
Turntable Location	Dist. ahead of dolly susp. center	in.	F15.3	BB1	3.5.1	
Turntable Height Above Ground	Height of pitch articulation on dolly	in.	F15.3	D		
Location of Pintle Hook	Dist. behind rear susp. of towing vehicle	in.	F15.3	A3	3.4.1, 3.5.1	Entries for trailer towing a full trailer
Height of Pintle Hook	Dist. above ground on towing veh.	in.	F15.3	PH	3.4.1, 3.5.1	



Suspension and Axle Parameters

Suspension Key	(Choice of single (0) or tandem (1) axles)	Units	I2	KEY		
Tandem Separation	Center-to-center dist. between tandem axles	in.	F15.3	TD	3.3.4.2	Entries only if tandem axles are specified
Static Load Transfer	Percent load on leading tandem axle	%	F15.3	FSPLIT	3.3.4.2	
Dynamic Load Transfer	Percent of tandem axle brake torque acting to transfer load onto leading tandem axle	%	F15.3	FSHIFT	3.3.4.2	
Suspension Spring Rate	Stiffness of each susp. spring (L&R)	lb/in	F15.3	K( <sub>1</sub> , <sub>2</sub> )	3.3.2	
Suspension Viscous Damping	Shock absorber damping coefficients (L&R)	lb-sec <sup>2</sup> /in	F15.3	C( <sub>1</sub> , <sub>2</sub> )	3.3.2	Serial entry of this data set when tandem axles are specified (leading tandem, trailing tandem)
Coulomb Friction	One-half the force hysteresis in each spring (L&R)	lb	F15.3	CF( <sub>1</sub> , <sub>2</sub> )	3.3.2	
Axle Roll Moment of Inertia	Roll inertia properties of total unsprung mass	in-lb-sec <sup>2</sup>	F15.3	IA	3.3.2	
Roll Center Height	Height of roll center above ground	in.	F15.3	RCI	3.3.2	
Roll Steer Coeff.	Axle roll steer effects	deg steer/deg roll	F15.3	RST	3.3.2	
Auxiliary Roll Stiffness	Roll stiffness not due to spring forces	in-lb/deg	F15.3	KRS	3.3.2	
Lat. Dist. between Susp. Springs	Suspension lateral spacing	in.	F15.3	SYI	3.3.2	
Truck Width	Center-to-center dist. between wheel sets	in.	F15.3	TRA	3.3.2, 3.3.4.1	
Unsprung Weight	Total weight of axle, brakes, wheels, etc.	lb	F15.3	ASW	3.3.2	
Dual Tire Separation	Center-to-center dist. between tires in a dual set	in.	F15.3	DTS	3.3.5	
Cornering Stiffness	Initial slope of tire lateral force-slip angle curve at loaded cond.	lb/deg	F15.3	CALF	3.3.3, 3.3.5	Deleted on truck/tractor front axle
Long. Stiffness	Initial slope of tire brake force-slip curve at loaded condition	lb/slip	F15.3	CS	3.3.3, 3.3.5	Data on per tire basis
Camber Stiffness	Initial slope of tire lateral force-camber angle curve at loaded cond.	lb/deg	F15.3	CAM	3.3.3, 3.3.5	Data on per tire basis
Aligning Moment	Initial slope of tire aligning moment-slip angle curve at loaded condition	in-lb/deg	F15.3	CAT	3.3.3, 3.3.5	Data on per tire basis
Tire Spring Rate	Force-deflection rate at loaded cond	lb/in	F15.3	KT	3.3.3, 3.3.5	Data on per tire basis



Tire Loaded Radius	Tire radius at loaded condition	in.	F15.3	SRAD	Side-to side	3.3.3, 3.3.5	Use one-half of total for a dual wheel set
Polar Moment of Inertia	Spin inertia of wheel assembly	in-lb-sec <sup>2</sup>	F15.3	WHEELI	Side-to side	3.3.3, 3.3.5	
Brake Parameters							
Time Lag	Time from treadle valve motion to beginning of pressure rise at brake	sec.	F15.3	TQ(,1)	Side-to side	3.3.6	Entries deleted if no lines in treadle pressure table
Rise Time	First-order time constant of pressure rise at brake	sec.	F15.3	TQ(,2)	Side-to side	3.3.6	
Brake Torque	Torque-pressure coefficient of brake	in-lb/psi	F15.3	BTQ	Side-to side, table lookup	3.3.6	Max. of 10 lines
Antilock Parameters							
Vehicle Antilock Key	Vehicle antilock key, 0-no antilock, 01-indicates antilocks used	—	I2	ILOCK		3.6, App. D	
Antilock Parameters	See Appendix D						
Rerun Parameter	Key at end of data input list						
Rerun	00 - ends simulation runs 01 - indicates another run follows	—	I2	RERUN		3.7	Last line of input list

## APPENDIX D

### ANTILOCK SIMULATION

The documentation presented in this appendix represents the most recent version of the HSRI antilock program. The simulation concentrates on the three areas common to most antilock systems: (1) wheel speed sensor, (2) control logic module, and (3) pressure modulator. Axle-by-axle systems are allowed for, as well as four side-to-side options: (1) worst wheel, (2) best wheel, (3) average wheel, and (4) independent wheel.

A block diagram showing the relationship between the antilock elements and the main program is shown in Figure D-1. The wheel speed signal,  $\omega$ , is received from the main program and processed by the wheel sensor wherein an effective time delay occurs resulting in delayed wheel speed and acceleration signals  $\omega_d$  and  $\dot{\omega}_d$ . These signals, along with vehicle velocity,  $\dot{x}$ , vehicle acceleration,  $\ddot{x}$ , and feedback from the pressure modulator, are input to the control logic module. The control logic module outputs an ON/OFF solenoid command signal to the pressure modulator which in turn generates the brake pressure, P, returned to the main program.

A complete description of the antilock simulation and explanation of its use is presented in the following sections.

---

D.1. User Dictionary of Variables/Parameters. In order to offer much greater flexibility to the program user as regards variable and parameter programming choices, a table or dictionary of such variables/parameters has been added. This dictionary, as shown in Figure D-2, is simply a listing of various variables and parameters which might be considered to be of some importance or interest to an antilock system. A user selects, for programming purposes, a particular variable/parameter by referring to its variable I.D. numeral shown in Figure D-2. Each of these variables/parameters are defined in Table D-1 and Figure D-3. If a user has need for additional variables or parameters not included in the dictionary, they can be added by rather simple additions to the FORTRAN code.

The purpose of the dictionary is to allow the program user to select, from a wide variety of possible antilock variables/parameters, only those which are of interest to the particular

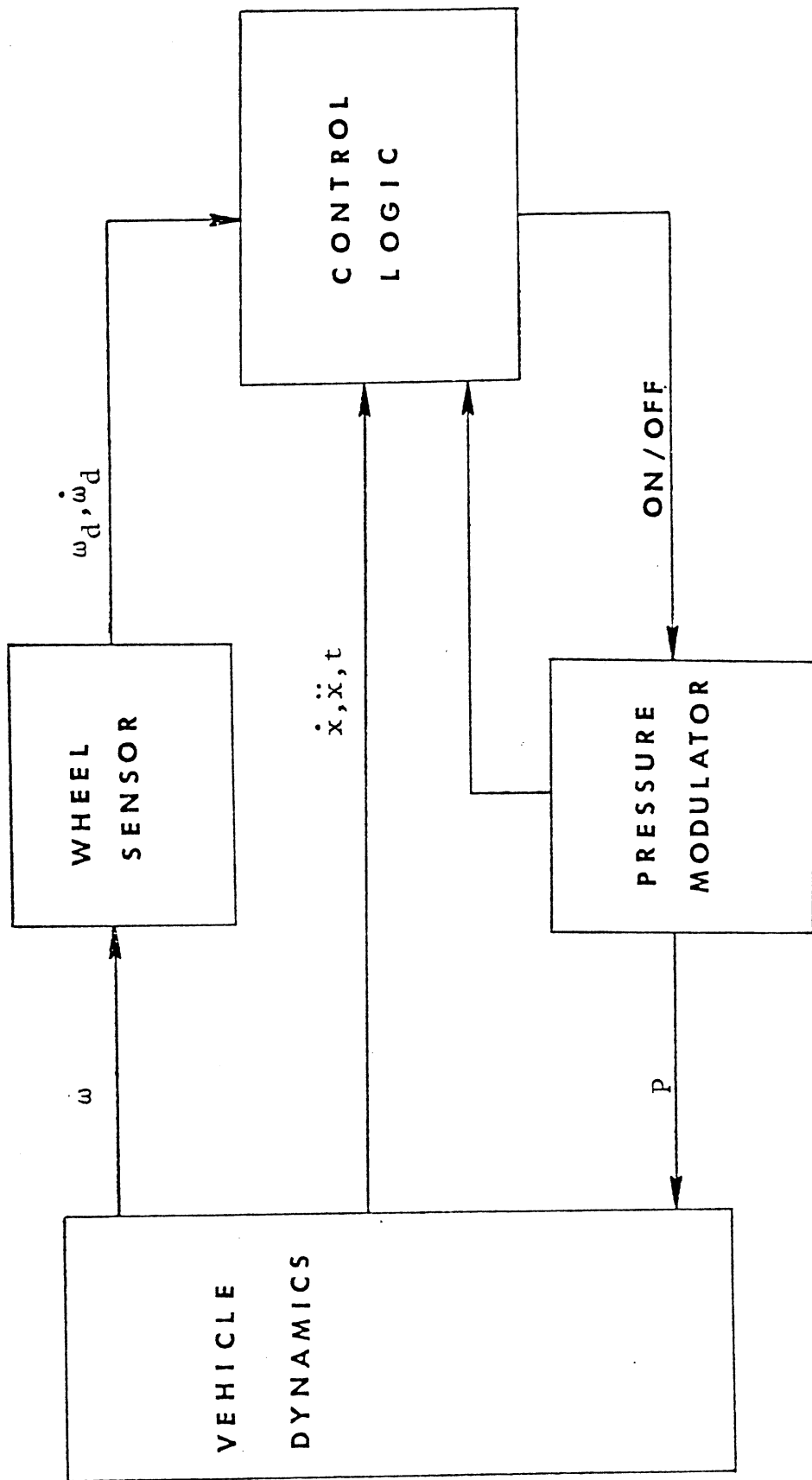


Figure D-1. Anti-lock block diagram.



\*\*\*\*\*  
 DICT ONARY OF ANTI-LOCK VARIABLES/PARAMETERS AVAILABLE TO USER.  
 \*\*\*\*\*

VARIABLE I.D.	DESCRIPTION	VARIABLE I.D.	DESCRIPTION
1	1.0	45	WMAX1
2	TIME	46	WMAX2
3	OMEGA	47	TWMAX1
4	OMEGADOT	48	TWMAX2
5	XDOT	49	WMIN
6	XDDOT	50	TMIN
7	POFF1	51	TPMAX2
8	POFF2	52	TPMIN2
9	PONI	53	GPV1
10	PON2	54	GPV2
11	TOFF1	55	GPV3
12	TON1	56	GPV4
13	XDOFF	57	GPV5
14	XDON	58	FDS4
15	WOFF	59	FDS5
16	WON	60	OMEGDIF
17	WDOFF		
18	WDON		
19	WDMAX		
20	WDMIN		
21	TPMAX1		
22	TPMIN1		
23	WLOCK		
24	TLOCK		
25	SLOIN		
26	SLOFF		
27	PMAX1		
28	PMAX2		
29	PHINI		
30	PMIN?		
31	PD		
32	ON		
33	TMOD		
34	SLIP		
35	P		
36	CYCNT		
37	SQUARF		
38	SQUARN		
39	TOFF2		
40	TON2		
41	FDS1		
42	FDS2		
43	FDS3		
44	GCNT		

Figure D-2

Table D-1. Variable/Parameter Definitions

<u>Symbol</u>	<u>I.D. Code</u>	<u>Definition</u>	<u>Units</u>
1.0	1	Constant; Unity Parameter	
TIMF	2	Time in simulation	(sec)
OMEGA	3	Wheel speed at tire-road interface (expressed as an equivalent translational velocity)	(ft/sec)
OMEGADOT	4	Wheel acceleration at tire-road interface (expressed as an equivalent translational acceleration)	(ft/sec <sup>2</sup> )
XDOT	5	Vehicle velocity	(ft/sec)
XDDOT	6	Vehicle acceleration	(ft/sec <sup>2</sup> )
POFF1	7	Brake pressure at last "OFF" signal	(psi)
POFF2	8	Brake pressure at "OFF" signal in next to last cycle	(psi)
PON1	9	Brake pressure at last "ON" signal	(psi)
PON2	10	Brake pressure at "ON" signal in next to last cycle	(psi)
TOFF1	11	Time at last "OFF" signal	(sec)
TON1	12	Time at last "ON" signal	(sec)
XDOFF	13	Vehicle velocity at last "OFF" signal	(ft/sec)
XDON	14	Vehicle velocity at last "ON" signal	(ft/sec)
WOFF	15	Wheel speed at last "OFF" signal	(ft/sec)
WON	16	Wheel speed at last "ON" signal	(ft/sec)
WDOFF	17	Wheel acceleration at last "OFF" signal	(ft/sec <sup>2</sup> )
WDON	18	Wheel acceleration at last "ON" signal	(ft/sec <sup>2</sup> )
WDMAX	19	Maximum wheel acceleration in last cycle	(ft/sec <sup>2</sup> )
WDMIN	20	Minimum wheel acceleration in last cycle	(ft/sec <sup>2</sup> )

Table D-1 (Cont.)

<u>Symbol</u>	<u>I.D. Code</u>	<u>Definition</u>	<u>Units</u>
TPMAX1	21	Time of maximum pressure in last cycle	(sec)
TPMIN1	22	Time of minimum pressure in last cycle	(sec)
WLOCK	23	Parameter having value 1.0 if wheel is locked; otherwise having value of 0.0	
TLOCK	24	Time ramp beginning at start of any wheel lock	(sec)
SLON	25	Wheel slip at last "ON" signal	
SLOFF	26	Wheel slip at last "OFF" signal	
PMAX1	27	Maximum pressure from last cycle	(psi)
PMAX2	28	Maximum pressure from cycle before last	(psi)
PMIN1	29	Minimum pressure from last cycle	(psi)
PMIN2	30	Minimum pressure from cycle before last	(psi)
PD	31	Treadle pressure	(psi)
ON	32	Parameter having value of 1.0 during "ON" signal; otherwise 0.0	
TMOD	33	Time of modulation for the pulse-width modulated square wave	(sec)
SLIP	34	Wheel slip	
P	35	Brake pressure	(psi)
CYCNT	36	Cycle counter beginning at 0 and incrementing its count by 1 every "OFF" signal	
SQUARE	37	Pulse-width modulated square wave having value 1.0 or 0.0	
SQUARN	38	SQUARE - 1.0	
TOFF2	39	Time of "OFF" signal in cycle before last	(sec)
TON2	40	Time of "ON" signal in cycle before last	(sec)
FOS1	41	First one-shot variable having value 1.0 during one-shot firing; otherwise having value of 0.0	

Table D-1 (Cont.)

<u>Symbol</u>	<u>I.D. Code</u>	<u>Definition</u>	<u>Units</u>
FOS2	42	Second one-shot variable	
FOS3	43	Third one-shot variable	
GPCNT	44	General purpose counter	
WMAX1	45	Maximum wheel speed in last cycle	(ft/sec)
WMAX2	46	Maximum wheel speed in cycle before last	(ft/sec)
TWMAX1	47	Time of maximum wheel speed in last cycle	(sec)
TWMAX2	48	Time of maximum wheel speed in cycle before last	(sec)
WMIN	49	Minimum wheel speed in last cycle	(ft/sec)
TWMIN	50	Time of minimum wheel speed in last cycle	(sec)
TPMAX2	51	Time of maximum brake pressure in cycle before last	(sec)
TPMIN2	52	Time of minimum brake pressure in cycle before last	(sec)
GPV1	53	First general purpose variable	
GPV2	54	Second general purpose variable	
GPV3	55	Third general purpose variable	
GPV4	56	Fourth general purpose variable	
GPV5	57	Fifth general purpose variable	
FOS4	58	Fourth one-shot variable	
FOS5	59	Fifth one-shot variable	
IMEGDIF	60	Side-to-side wheel speed difference indicator having the value 1.0 (otherwise 0.0) when the same axle side-to-side wheel speed difference (ft/sec) is greater than the input parameter, WWDIF.	

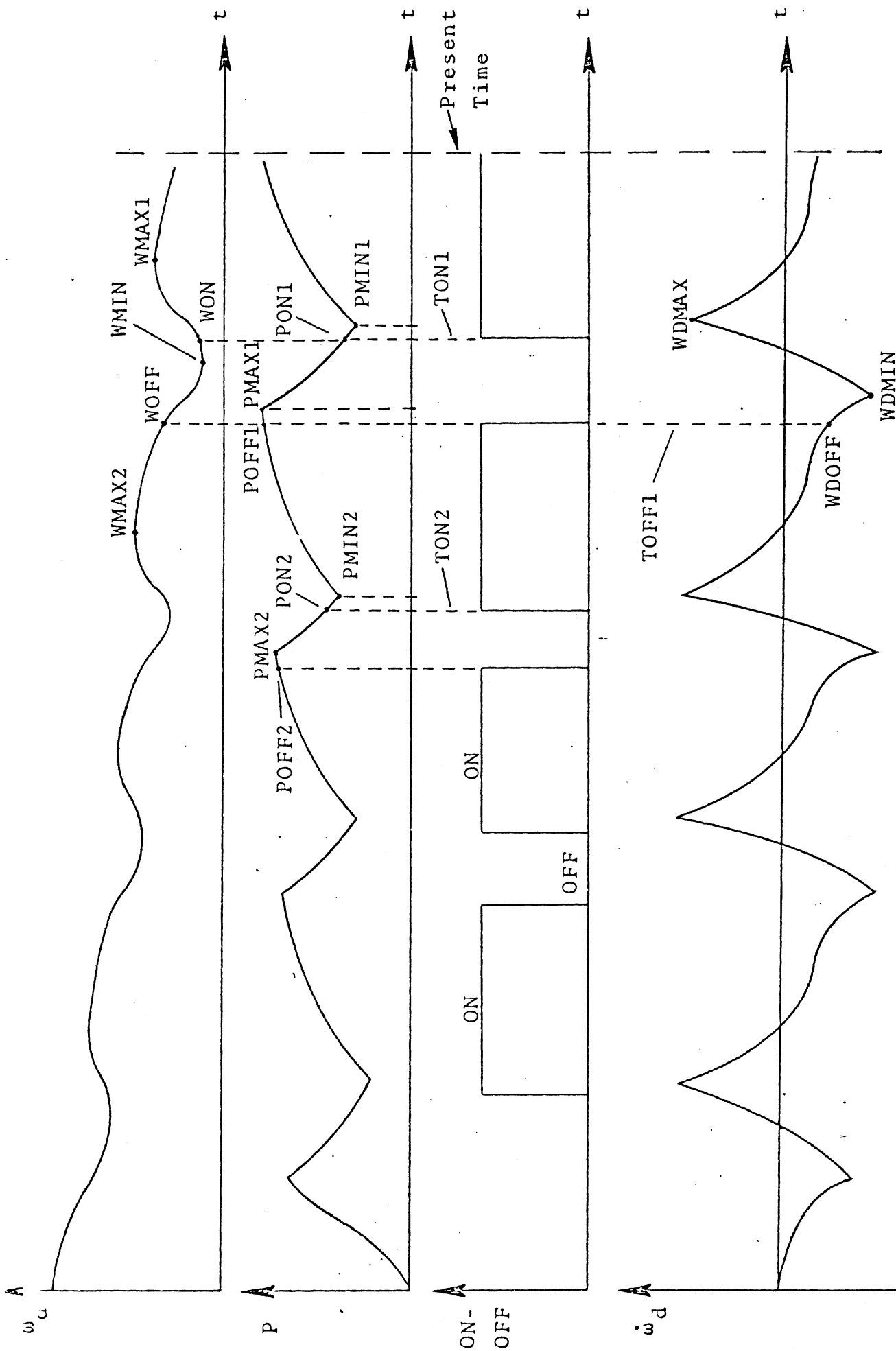


Figure D-3

system he is attempting to simulate. Those familiar with the previous antilock simulation may recall that such variable/parameter choices were fixed and limited to wheel speed, acceleration, and four or five other variables. Thus, the present approach should eliminate most problems where the user was handicapped with the previous program because a particular variable or parameter was not available.

Within the antilock variables/parameters are stored in an array of dimension 60 called VARIB(J), J=1,60. Therefore, VARIB(1) contains the constant 1.0, VARIB(2) contains the present value of the time, t, and so on as defined in Table D-1.

D.2. General Expression Form. Throughout the remainder of this discussion a particular algebraic expression will be encountered repeatedly. It would therefore be helpful beforehand to define each term in the expression and then discuss its purpose. The expression referred to is of the general form:

$$C_1x_1 + C_2x_2 + C_3x_3 + C_4x_4y_4 + C_5x_5y_5 \quad (D-1)$$

The  $C_i$  ( $i=1, \dots, 5$ ) are constant coefficients for each term. Any of these coefficients may be adaptive to as many as two different variables. This adaptive feature will be discussed in detail in Section D-4. The  $x_i$ , ( $i=1, \dots, 5$ ) and  $y_i$ , ( $i=4, 5$ ) are variables or parameters available in the user dictionary. Note that the fourth and fifth terms are quadratic in form. During execution of the program the  $x_i$  and  $y_i$ , which the user has selected from the dictionary to form some relationship, are actually assigned values from the array VARIB(J).

The purpose of these expressions is to allow the user to form various algebraic relationships between the variables and parameters available in the dictionary, subject to the form of the general expression (D-1). A form of this general expression appears in almost every section of the program from control logic inequality expressions to evaluation of one-shot conditions. Only those terms necessary to form a desired expression are required. Some simple examples illustrating the use of these general expressions are presented in the following sections.

D.3. Wheel Sensor Module. The primary effect of a wheel sensor is a phase shift and/or time delay between the actual wheel rate and the derived wheel rate. This input-output relationship can often be described adequately by transfer functions of various order and/or transport time delay expressions. The present version assumes a general first-order filter of the form  $1/\tau_{\omega}p + 1$  relating actual wheel rate to derived wheel rate, where  $\tau_{\omega}$  is the time constant of the filter and  $p$  is an operator denoting differentiation with respect to time.

Many antilock systems make use of wheel acceleration derived from the output of the wheel sensor. This normally involves additional delays along with a differentiation process. The assumed transfer function here was taken as  $p/\tau_{\omega d}p + 1$  relating derived wheel rate to derived wheel acceleration. The derived wheel acceleration calculation normally takes place within the electronic control unit. However, since it, along with wheel rate, is a primary input to the control unit logic, it is included here within the wheel sensor module so that the control unit can be characterized by logical or decision-making processes only. The wheel sensor module can then be described by the input-output relationships shown in Figure D-4.

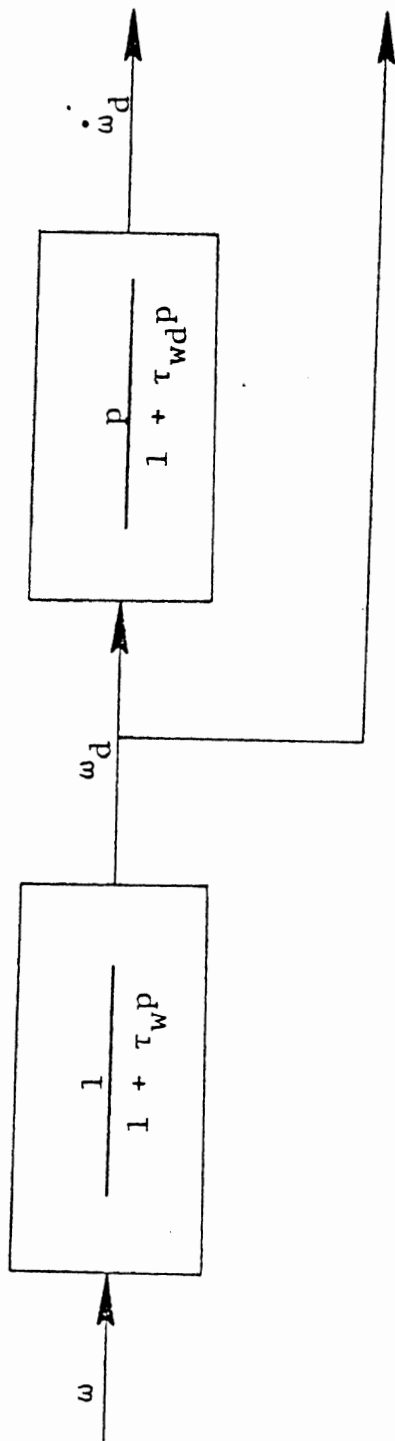


Figure D-4. Wheel sensor module.



The delayed wheel speed and acceleration signals,  $\omega_d$  and  $\dot{\omega}_d$ , are used as the primary inputs to the control logic module. The assumed wheel sensor and derivative circuit input-output relationships are therefore described by two input parameters,  $\tau_\omega$  and  $\tau_{\dot{\omega}_d}$ , which represent the first-order filter time constants of the wheel sensor and its derivative circuit. The variables,  $\omega_d$  and  $\dot{\omega}_d$ , appear in the user dictionary as OMEGA and OMEGADOT, I.D. codes 3 and 4. (The symbols  $\omega$  and  $\dot{\omega}$  are used interchangeably throughout this section for  $\omega_d$  and  $\dot{\omega}_d$ .)

Other variables are provided as possible inputs to the control logic module, however, no similar operations are attempted on these other input variables.

D.4. Control Logic Module. The control logic is characterized by a set of eight inequality expressions which the user forms as conditions for generating "ON" and "OFF" signals. Associated with each arithmetic inequality expression is a logical variable. These logical variables, reflecting the state or polarity of the inequality expressions, are logically combined to generate the "ON" and "OFF" signals. "ON" is defined here as air being applied to, or "ON," the brake air chambers. Figure D-5 summarizes the overall structure of the control logic module.

#### Inequality Expressions.

Each of the eight arithmetic inequalities has the general form:

$$F_i \triangleq c_{i1}v_{i1} + c_{i2}v_{i2} + c_{i3}v_{i3} + c_{i4}v_{i4}w_{i4} + c_{i5}v_{i5}w_{i5} \geq 0, \quad i=1,8 \quad (D-2)$$

where

Inequality Expression	Logical Variable	Logical Operator	Solenoid Command
$F_1 \geq 0$	$L_1$	}	}
$F_2 \geq 0$	$L_2$		
$F_3 \geq 0$	$L_3$	}	}
$F_4 \geq 0$	$L_4$		
$\cdot$	$\cdot$	$\cdot$	$\cdot$
$\cdot$	$\cdot$	$\cdot$	$\cdot$
$\cdot$	$\cdot$	$\cdot$	$\cdot$
$\cdot$	$\cdot$	$\cdot$	$\cdot$
$\cdot$	$\cdot$	$\cdot$	$\cdot$
$F_8 \geq 0$	$L_8$		
		OP <sub>12</sub>	}
		OP <sub>23</sub>	
		OP <sub>34</sub>	}
		$\cdot$	
		$\cdot$	}
		$\cdot$	
		$\cdot$	}
		$\cdot$	
		OP <sub>78</sub>	ON

Figure D-5. Control logic module.

$c_{ij}$ , ( $j=1,5$ ) are the constant coefficients of each term.

$v_{ij}$ ,  $w_{ik}$ , ( $j=1,5; k=4,5$ ) are the variables/parameters selected from the user dictionary.

The first four inequalities,  $F_1$  through  $F_4$ , are used for generating the "OFF" signal; the last four inequalities for the "ON" signal.

As an example, suppose the condition

$$\dot{\omega} \leq -100 \text{ ft/sec}^2*$$

or

$$-\dot{\omega} - 100 \geq 0$$

was used as the first "OFF" condition. Then  $F_1$  would become

$$F_1 \triangleq (-1.0)\dot{\omega} + (-100.)1.0 \geq 0 ,$$

with -1.0 and -100. required as  $c_{11}$  and  $c_{12}$ . OMEGADOT, ( $\dot{\omega}$ ), would be selected from the user dictionary for  $v_{11}$  and the unity parameter, 1.0, would be selected as  $v_{12}$ . As will be described in detail in Section D.7, five numbers would be required as program input for forming this expression: (a) the number of terms involved in the expression, (2); (b) two coefficients, (-1.0) and (-100.); and (c) two variable I.D. codes from the user dictionary, '4' and '1' for OMEGADOT and the unity parameter, respectively.

---

\*See definition of OMEGADOT in Table D-1.

A simple description of the sequence of operations taking place within the antilock control logic module is as follows:

During a braking maneuver, the variables/parameters selected by the user are substituted in the user-defined inequality expressions. These expressions are evaluated, and based upon their polarity, OFF signals or ON signals are sent to the pressure modulator. At the beginning of the braking maneuver, evaluation of the inequalities associated with generating the "OFF" signal takes place until an "OFF" signal is generated. Attention then is focused on the inequalities associated with generating an "ON" signal until an "ON" signal is generated. This sequence continues until either the treadle valve pressure demanded by the driver falls to near zero, or until the vehicle velocity decreases to below some cut-off velocity.

#### Logical Variables

Each of the eight inequalities has assigned to it a logical variable that is defined as TRUE if the inequality is satisfied as shown; FALSE if not. In other words, if  $F_i \geq 0$ , then the logical variable  $L_i$  associated with  $F_i$  assumes the value TRUE. If  $F_i < 0$ , then  $L_i$  assumes the value FALSE. Since there are four inequalities for the generation of the "OFF" signal, there are four logical variables associated with the "OFF" signal. The purpose of these logical variables is to facilitate the generation of an "OFF" signal by allowing them to be "AND"-ed and "OR"-ed together by the program user. If, for example, the user had decided that  $F_1$  and  $F_2$  must be satisfied or else  $F_3$  or  $F_4$  be satisfied ( $F_1$ ,  $F_2$ ,  $F_3$ , and  $F_4$  having been previously defined by the data set selected by the user), the proper "OFF" signal would be defined by the following expression:

$$\text{OFF} = (L_1 \text{ AND } L_2) \text{ OR } (L_3 \text{ OR } L_4) .$$

The same discussion applies to the "ON" signal and associated logical variables  $L_5$ ,  $L_6$ ,  $L_7$ , and  $L_8$ .

The user specifies the logical operations between  $L_1$  and  $L_2$ ,  $L_3$ , and  $L_4$ , and between the bracketed expressions by means of three logical operator switches,  $OP_{12}$ ,  $OP_{34}$ , and  $OP_{23}$ , respectively. Input values of 0 imply logical "OR" operations; values of 1 imply logical "AND" operations. The same rules apply to logical variables  $L_5$ ,  $L_6$ ,  $L_7$ ,  $L_8$  and their logical operator switches  $OP_{56}$ ,  $OP_{78}$ , and  $OP_{67}$ . The general forms of these logical equations are:

$$\text{OFF} = (L_1 \text{ } OP_{12} \text{ } L_2) \text{ } OP_{23} \text{ } (L_3 \text{ } OP_{34} \text{ } L_4) \quad (\text{D-3 } )$$

and

$$\text{ON} = (L_5 \text{ } OP_{56} \text{ } L_6) \text{ } OP_{67} \text{ } (L_7 \text{ } OP_{78} \text{ } L_8) \quad (\text{D-4 } )$$

The user is required to input data only for the number of inequality expressions needed. The details relating to data input for the inequality expressions and logical operators are explained in Section D.7 .

### Time Delays

Four programmable time delays are available in the control logic. The first time delay,  $\tau_1$ , is the delay between the evaluations of  $F_1$  and the evaluations of either  $F_2$ ,  $F_3$ , or  $F_4$ . The second time delay,  $\tau_2$ , is the delay between the time of generation of the "OFF" signal and the time that  $F_5$  may be evaluated in the generation of the next "ON" signal.  $\tau_3$  is the delay between the time of evaluation of  $F_5$  and the time of evaluation of either  $F_6$ ,  $F_7$ , or  $F_8$ .  $\tau_4$  is the delay between the time of generation of the "ON" signal and the time that  $F_1$  may be evaluated in the generation of the next "OFF" signal. For time delay effects other than those described here, the one-shot variables (Section D.6) may be employed.

### Example

A brief example covering the above outlined features should prove helpful. Consider an antilock system which generates an "OFF" signal subject to the following laws:

- 1)  $\dot{\omega} \leq -50 \text{ ft/sec}^2$
- and 2) at a time .05 second after (1) is satisfied,  
 $\omega \leq .9 \dot{x}$  must also be satisfied.

Suppose the corresponding "ON" signal must satisfy the following requirements

- 3)  $\dot{\omega} \geq -1.5 \text{ ft/sec}^2$
- and 4) at a time .02 second after (3) is satisfied,  
 $\omega \geq .8 \dot{x}$  must also be satisfied.

Suppose also that once the "ON" signal is generated during any cycle, the test for the next "OFF" signal must not take place for at least 0.1 second, guaranteeing a certain amount of brake on-time.

Rewriting (1) as

$$F_1 = -\dot{\omega} - 50 \geq 0$$

$$c_{11} = -1.0$$

$$c_{12} = -50.$$

The variable I.D. codes for  $v_{11}$  and  $v_{12}$  would be "4" and "1," corresponding to OMEGADOT and the unity parameter from the user dictionary.

Similarly, for (2),

$$F_2 = -\omega + .9 \dot{x} \geq 0$$

$$c_{21} = -1.0$$

$$c_{22} = .90$$

The variable I.D. codes for  $v_{21}$  and  $v_{11}$  would be "3" and "5".

Since  $F_3$  and  $F_4$  are not required, no input for these expressions would be needed.  $OP_{12}$  should be entered as 1 since  $OFF = L_1 \text{ AND } L_2$ .  $OP_{23}$  and  $OP_{24}$  have no meaning here and can therefore be either 0 or 1. The time delay between  $F_1$  and  $F_2$  implies  $\tau_1 = 0.05$ . Since there is no time delay specified between the generation of the "OFF" signal and the evaluation for the next "ON" signal,  $\tau_2 = 0.0$ .

Similarly, for the "ON" criteria, (3) may be rewritten as

$$F_5 = \dot{\omega} + 5 \geq 0$$

$$c_{51} = 1.0$$

$$c_{52} = 5.0$$

With variable I.D. codes for  $v_{51}$  and  $v_{52}$  of "4" and "1".

Likewise

$$F_6 = \omega - .8 \dot{x} \geq 0$$

$$c_{61} = 1.0$$

$$c_{62} = -.8$$

With variable I.D. codes for  $v_{61}$  and  $v_{62}$  of "3" and "5".

Since  $F_7$  and  $F_8$  are not required, no input for these expressions would be needed.  $OP_{56}$  should be entered as 1 for the required "AND" operation, while  $OP_{67}$  and  $OP_{78}$  are meaningless here and can be either 0 or 1. The time delay between  $F_5$  and  $F_6$  requires  $\tau_3 = 0.02$ . The time delay between the "ON" signal and the test for the next "OFF" signal requires  $\tau_4 = 0.10$ .

### Adaptive Coefficients

Many antilock systems possess adaptive capabilities for changing coefficients involved in their control logic. For this reason, and increased programming flexibility, an adaptive coefficient feature is provided for in this program. Each coefficient,  $C_{ij}$ , involved in the inequality expressions may be altered to change its value as a function of one or two dictionary variables in the manner shown in Figures D-6 and D-7.

In Figure D-6, the value of  $C_{ij}$  is  $A_0$  (its initial value), if  $u_{ij} < b_1$ . If  $u_{ij}$ , the adaptive variable, is greater than its breakpoint value of  $b_1$ ,  $C_{ij}$  is equal to  $A_1$ .

If two adaptive variables are involved, as illustrated in Figure D-7,

$$C_{ij} = \begin{cases} A_0 & \text{if } u_{ij} \leq b_1 \text{ and } z_{ij} \leq b_2 \\ A_1 & \text{if } u_{ij} > b_1 \text{ and } z_{ij} \leq b_2 \\ A_2 & \text{if } z_{ij} > b_2 \end{cases} \quad (\text{D-5})$$

By including an additional numerical switch in the input, the two adaptive variable case may be altered to:

$$C_{ij} = \begin{cases} A_0 & \text{if } u_{ij} \leq b_1 \\ A_1 & \text{if } u_{ij} > b_1 \text{ and } z_{ij} \leq b_2 \\ A_2 & \text{if } u_{ij} > b_1 \text{ and } z_{ij} > b_2 \end{cases} \quad (\text{D-6})$$

as illustrated in Figure D-8.

The details of the numerical input format are explained in Section D.7.



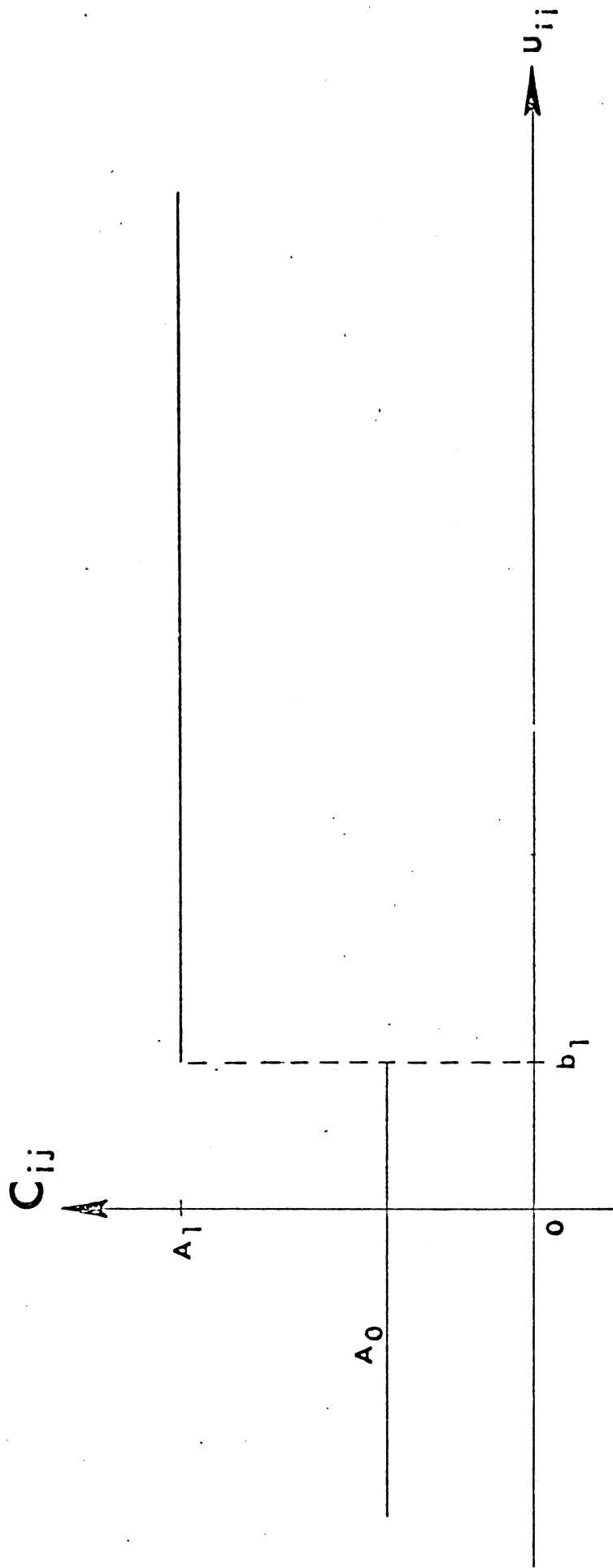


Figure D-6.

$$C_{ij} = \begin{cases} A_0, & \text{if } u_{ij} \leq b_1 \text{ and } z_{ij} \leq b_2 \\ A_1, & \text{if } u_{ij} > b_1 \text{ and } z_{ij} \leq b_2 \\ A_2, & \text{if } z_{ij} > b_2 \end{cases}$$

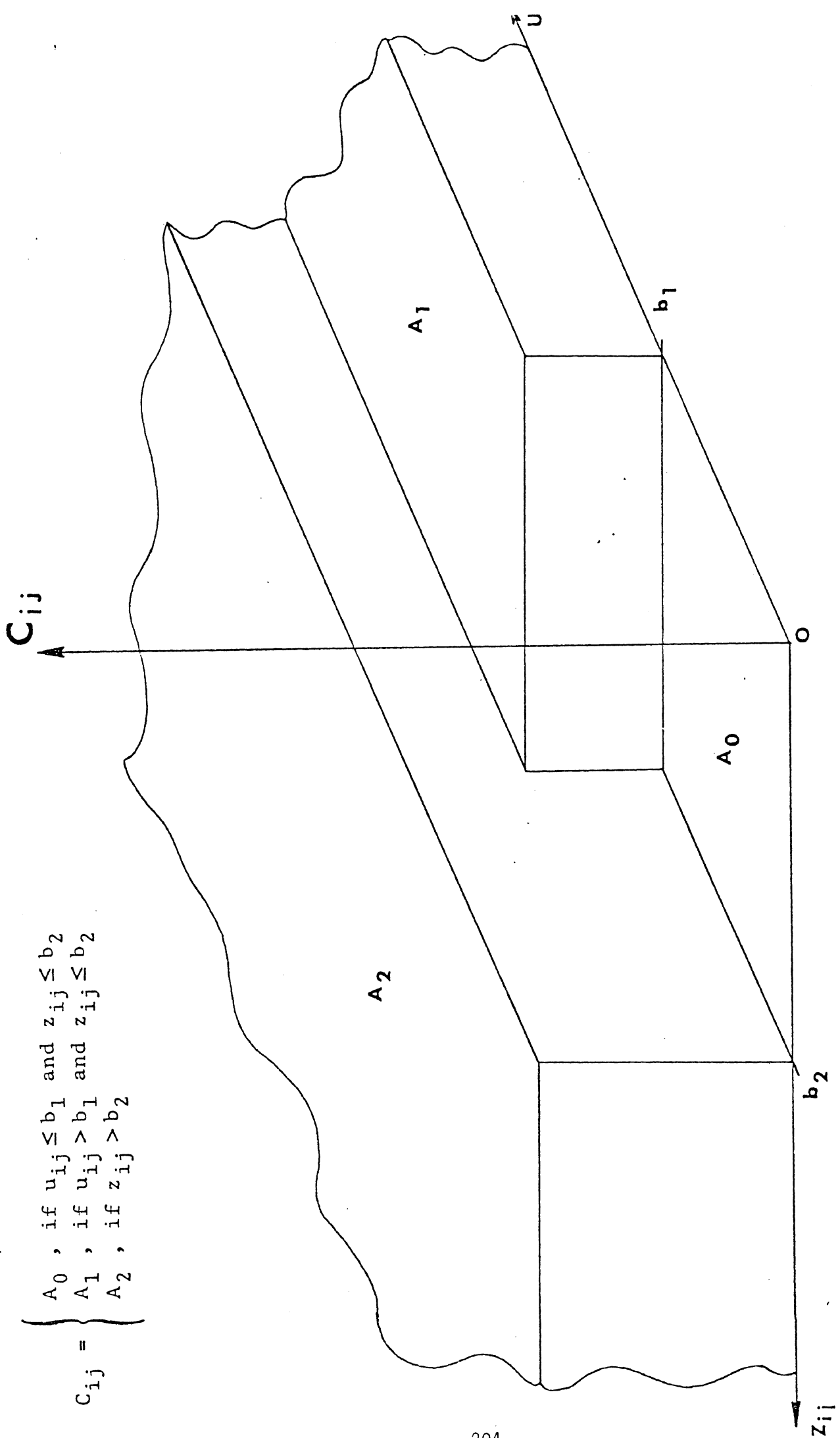


Figure D-7. Adaptive coefficient feature.

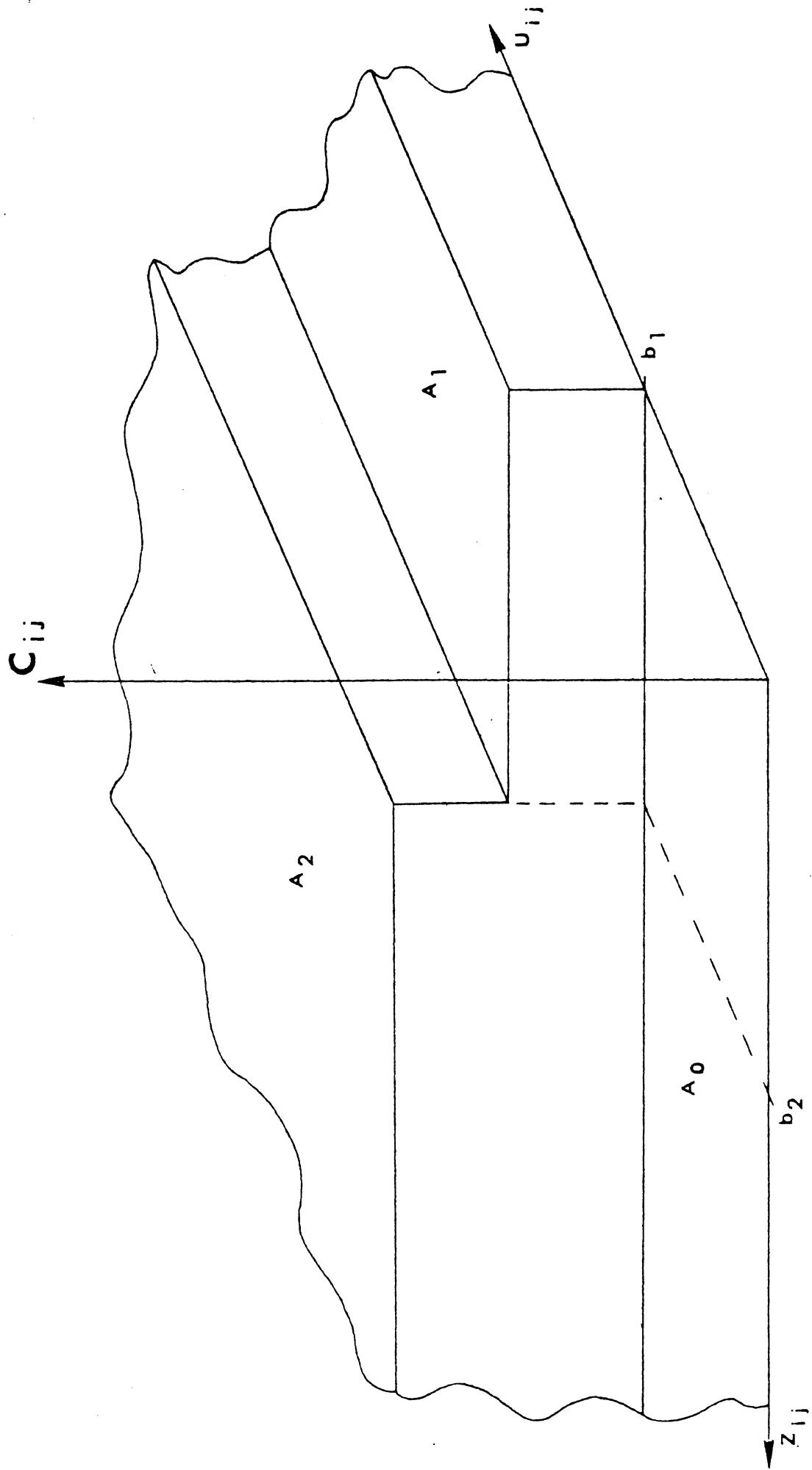


Figure D-8.

### Side-to-Side Options

Three different side-to-side options per axle are available. One antilock system is allowed for each axle with the same pressure being returned to both sides for each of the available options. These are summarized below:

OPTION 1 - Worst Wheel. The wheel having the lowest rotational rate ( $\omega$ ) for a given axle is selected by the control logic as its input. The same pressure is returned to both sides based on this input.

OPTION 2 - Best Wheel. Same as Option 1 except that the wheel with the highest rotational rate is selected as input.

OPTION 3 - Average Wheel. Both wheel rates are averaged by the control logic module and used as input. The same pressure is returned to both sides.

See Section D.7 for the numerical input and format required for each option.

### Logic Sampling Rate Control

The program user is asked to specify a logic sampling period, TSMPL, which controls the rate at which the antilock logic is interrogated. If TSMPL is specified to be less than or equal to the digital simulation time step, then no sampling rate control is in effect. If, however, a logic sampling period greater than the digital simulation time step is called for, all control logic and special option features pertaining to the control logic module are interrogated at time intervals set by the logic sampling period, TSMPL. Wheel sensor computations and pressure modulator activities are not affected.

For vehicle velocities less than 7 ft/sec, the antilock simulation is inactivated and line pressures will follow the treadle pressure.

D.5. Pressure Modulator. The pressure modulator valve is simulated by two time delays and several programmable rise and fall rates for both exponential and linear characteristics. The programmable rise and fall rates make possible the simulation of relatively complex pressure modulator activity including designs involving pneumatic logic or pulse-width modulators.

#### Time Delays

The input received by the pressure modulator is simply the "ON" and "OFF" signals generated in the control logic module. Once a control signal is received there is normally a time delay before actual pressure reduction or increase takes place. These time lags are denoted in the simulation as  $\tau_{ON}$  and  $\tau_{OFF}$  and are program inputs specified by the user.

#### Exponential Fall and Rise Rates

The pressure rise is defined to be exponential in time with the upper pressure limit set by the treadle valve output or by a programmable limit PDRSE offered as a special option and explained in Section D.6. Likewise, the pressure fall is exponential in time with its lower limit as zero pressure or by a programmable lower limit, PDFALL, offered as a special option and defined in Section D.6. As many as three pressure fall rates and three rise rates can be programmed. The fall and rise rates referred to are defined as the inverse of the time constants associated with the exponential pressure rise and fall.

The three exponential fall rates are denoted as  $PFE_i$ , ( $i=1,3$ ); the three exponential rise rates are defined as  $PRE_i$ , ( $i=1,3$ ). For reasons of flexibility these fall and rise rates are defined to be functions of variables denoted as  $\epsilon_1$  and  $\epsilon_2$ , respectively.  $\epsilon_1$  and  $\epsilon_2$  are defined by the general form expressions:

$$\epsilon_1 \triangleq H_1 v_1 + H_2 v_2 + H_3 v_3 + H_4 v_4 w_4 + H_5 v_5 w_5$$

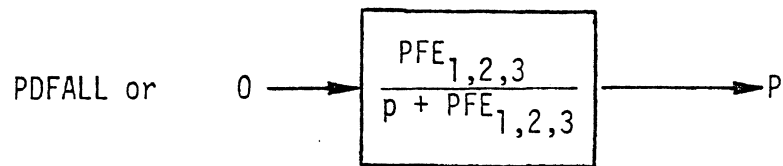
$$\epsilon_2 \triangleq G_1 v_1 + G_2 v_2 + G_3 v_3 + G_4 v_4 w_4 + G_5 v_5 w_5$$

where  $H_i$  and  $G_i$ , ( $i=1,5$ ) are the constant coefficients of each term, and  $v_j$  and  $w_k$ , ( $j=1,5$ ;  $k=4,5$ ) are variables/parameters available in the user dictionary.

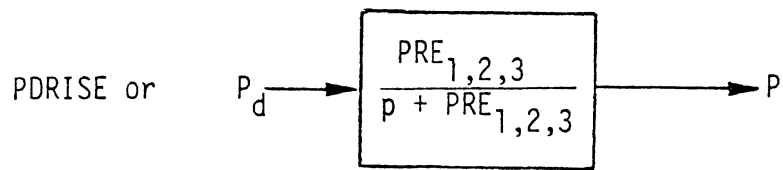
These relationships are shown in Figures D-9 and D-10. The break-points  $X_1$ ,  $X_2$ ,  $X_3$ , and  $X_4$  along the  $\epsilon_1$  and  $\epsilon_2$  axes separate the fall and rise rate regions.

In terms of transfer function notation, the above relationships can be expressed as:

Pressure Fall:



Pressure Rise:



where  $PFE_{1,2,3}$  and  $PRE_{1,2,3}$  defined above are functions of  $\epsilon_1$  and  $\epsilon_2$ , respectively, and  $p$  is an operator denoting differentiation with respect to time.

### Exponential Pressure Fall Rate

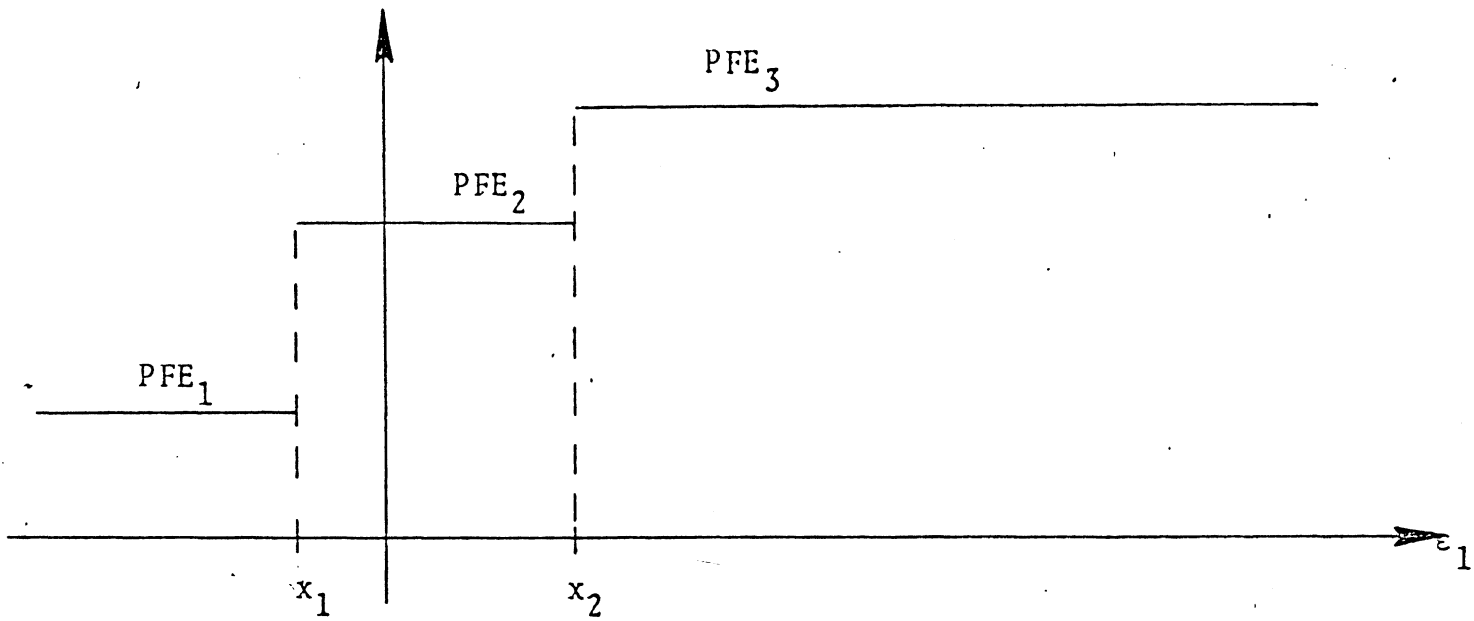


Figure D-9.

### Exponential Pressure Rise Rate

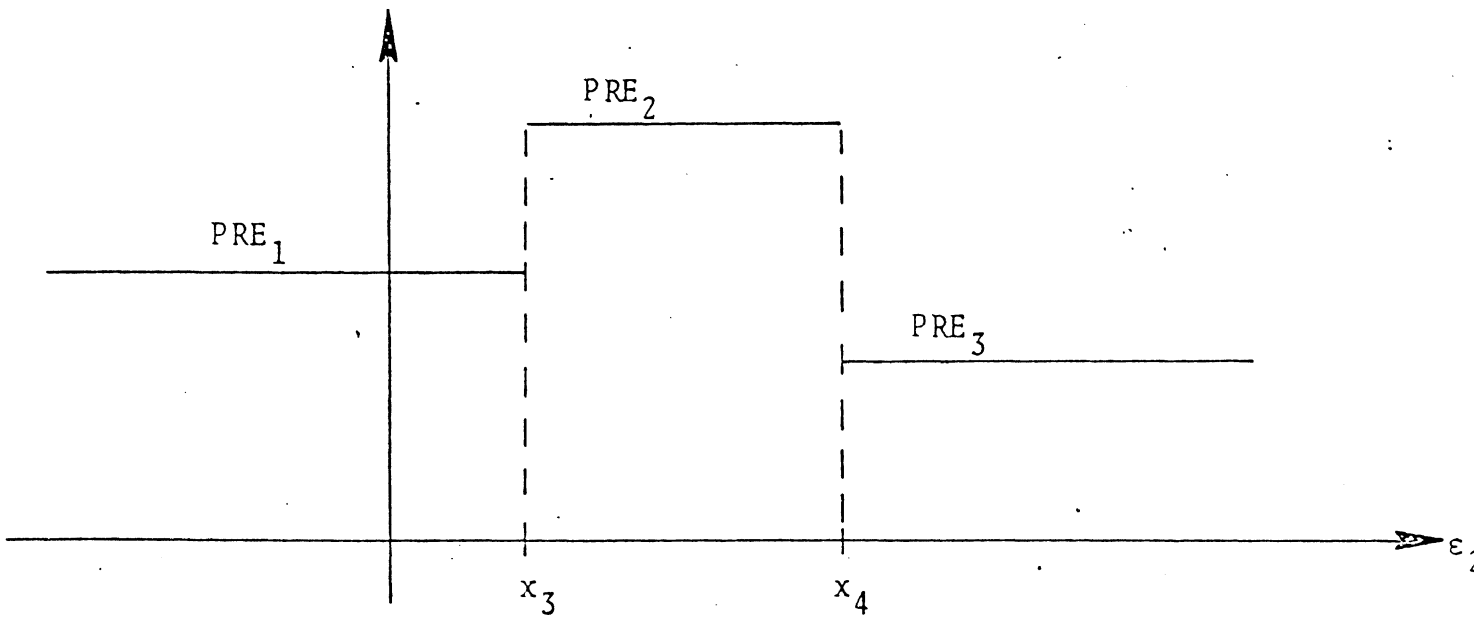


Figure D-10.

### Linear Fall and Rise Rates

The pressure fall and rise, under this option, is linear in time with an upper limit as treadle pressure,  $P_d$ , and a lower limit as zero pressure. Three fall rates and three rise rates may be specified as in the exponential case. The linear fall and rise rates are denoted as  $PFL_i$  and  $PRL_i$ , ( $i=1,3$ ), respectively. Again, for programming flexibility, the linear fall and rise rates are defined as functions of variables denoted as  $\epsilon_3$  and  $\epsilon_4$ , respectively.  $\epsilon_3$  and  $\epsilon_4$  are defined by the general form expressions:

$$\epsilon_3 \triangleq R_1 v_1 + R_2 v_2 + R_3 v_3 + R_4 v_4 w_4 + R_5 v_5 w_5$$

$$\epsilon_4 \triangleq S_1 v_1 + S_2 v_2 + S_3 v_3 + S_4 v_4 w_4 + S_5 v_5 w_5$$

where  $R_j$  and  $S_j$ , ( $j=1,5$ ) are the constant coefficients of each term, and  $v_j w_k$ , ( $j=1,5; k=4,5$ ) are variables/parameters available in the user dictionary. These relationships are illustrated in Figures D-11 and D-12. The pressure returned is given simply by the following two equations:

$$P(t-t_0) = [PFL_i(\epsilon_3)] \cdot (t-t_0) + P(t_0) \quad ; \quad (\text{fall})$$

$$P(t-t_0) = [PRL_i(\epsilon_4)] \cdot (t-t_0) + P(t_0) \quad ; \quad (\text{rise})$$

$X_5$ ,  $X_6$ ,  $X_7$ , and  $X_8$  are the associated break-points similar to the exponential case.



Linear Pressure Fall Rate

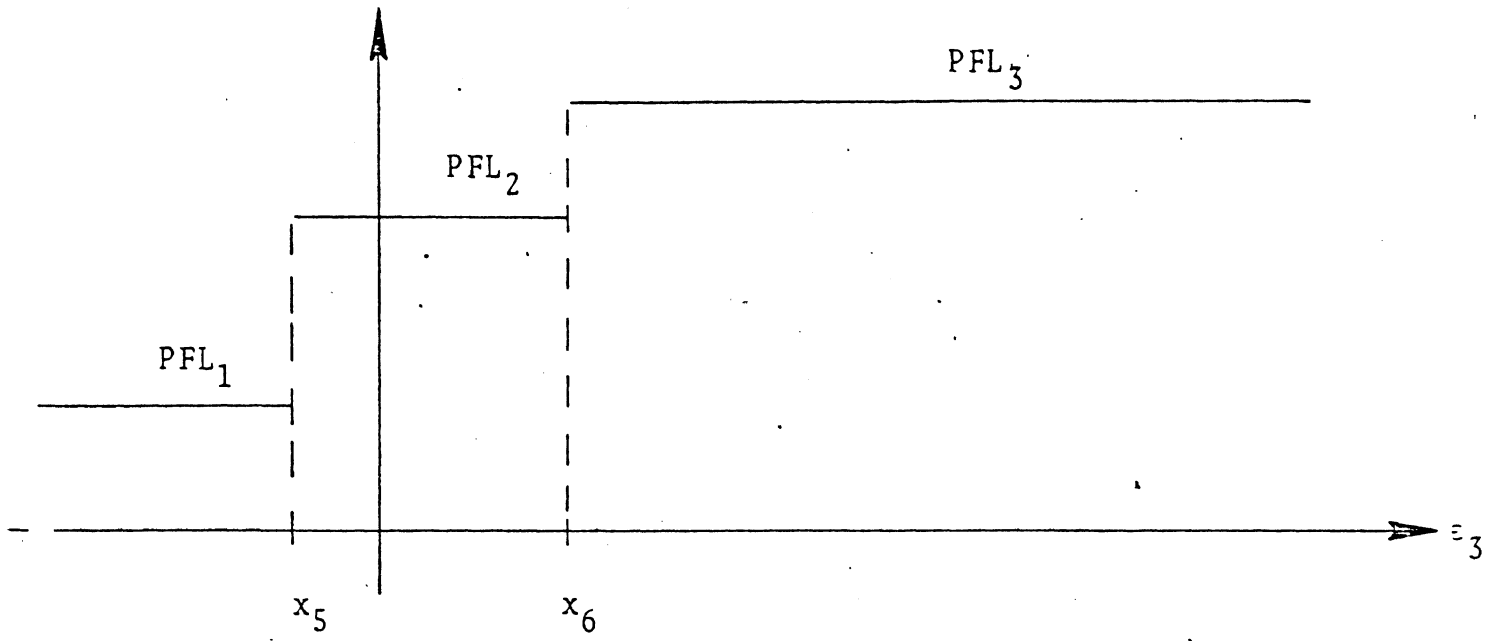


Figure D-11

Linear Pressure Rise Rate

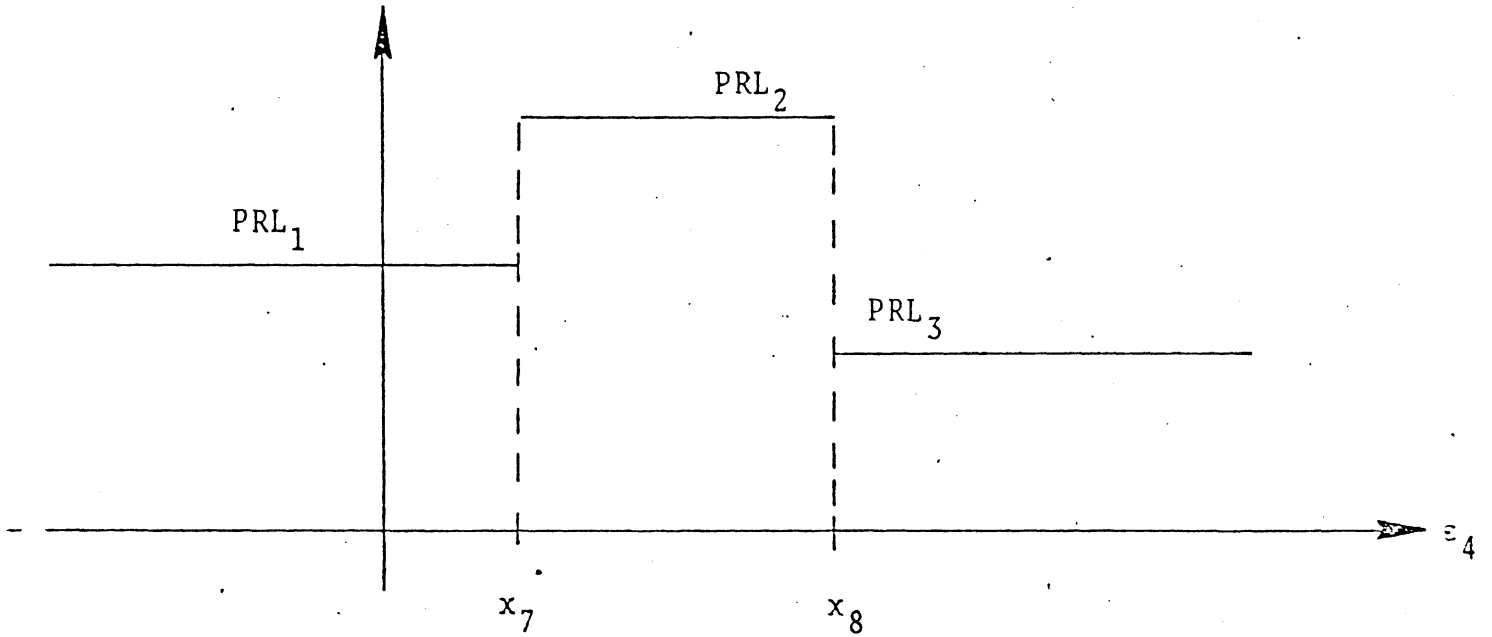


Figure D-12

### Pressure Modulator Key

A pressure modulator key, IPKEY, is read during input just prior to any data related to the pressure modulator. The value of this key distinguishes for the program whether exponential, linear, or both exponential and linear characteristics will be computed. The following key defines the IPKEY values required for each case:

$$\text{IPKEY} = \left\{ \begin{array}{ll} 0 & , \quad \text{exponential} \\ 1 & , \quad \text{linear} \\ 2 & , \quad \text{exponential and linear} \end{array} \right.$$

The exponential and linear option (IPKEY=2) returns a pressure representing the summation of the exponential and linear pressure computations.

Finally, all coefficients appearing in the general form expressions for the pressure modulator possess the adaptive coefficient feature.

### Example

Consider the following example of a certain pressure modulator having only exponential pressure fall and rise characteristics:

- 1) "ON" delay = "OFF" delay = 0.05 seconds.
- 2) The exponential pressure rise rate assumes an approximate value of  $(0.2)^{-1} = 5.0$  for differences between treadle valve output pressure and line pressure of 50 psi or more, and an approximate exponential rise rate of  $(0.33)^{-1} = 3.0$  for pressure differences of less than 50 psi.
- 3) The exponential pressure fall rate is approximately constant for all line pressure values with a fall rate equal to  $(0.25)^{-1} = 4.0$ .

This could be simulated by the following choice of input parameters:

IPKEY = 0  
 $\tau_{ON}$  = 0.05  
 $\tau_{OFF}$  = 0.05  
 $H_1$  = 1.0 } =>  $\epsilon_1 = 1.0$   
 $G_1$  = -1.0 ,  $G_2 = 1.0$  } =>  $\epsilon_2 = P_d - P$

Variable I.D. code for  $P_d = 31$ .

See User Dictionary

Variable I.D. code for  $P = 35$ .

$X_1 = X_2 = 0.0$   
 $PFE_1 = PFE_2 = PFE_3 = 4.0$   
 $X_3 = 0.0$  ,  $X_4 = 50.0$   
 $PRE_1 = PRE_2 = 3.0$  ,  $PRE_3 = 5.0$

The number of terms required for  $\epsilon_1$ , (1 term) and  $\epsilon_2$  (2 terms) would also be required as input as explained in Section D.7.

D.6. Special Options. Five special options have been included in the model in order to facilitate simulation of certain features displayed in some actual antilock systems while also providing increased programming flexibility. The five options referred to are: (1) treadle pressure modulation/programming, (2) pulse-width modulated square wave, (3) five programmable one-shots, (4) general purpose counter, and (5) general purpose variables. Each of these options will be explained in the following sections.

#### Treadle Pressure Modulation/Programming

Most pressure valves operating without antilock interruption, and many under antilock cycling, follow or are limited above by the treadle pressure application; while similarly, the output pressure of these valves fall to treadle pressure or zero

pressure when treadle pressure is decreased or removed. However, in some valves, during antilock cycling, pressure may rise to some limiting pressure less than treadle and/or fall to some pressure greater than zero. Such treadle modulation or programming of demanded pressure is a feature which is allowed for under this option.

Prior to any input for this option, a key, IPDKEY, for treadle pressure modulation, is read. A value of -1 or less negates the use of this option, while values greater than or equal to 0 activate the option. Variables PDFALL and PDRISE become the demanded pressure during pressure fall and rise periods, respectively. These variables are defined by the following general form expressions:

$$\text{PDFALL} \triangleq V_1v_1 + V_2v_2 + V_3v_3 + V_4v_4w_4 + V_5v_5w_5$$

$$\text{PDRISE} \triangleq W_1v_1 + W_2v_2 + W_3v_3 + W_4v_4w_4 + W_5v_5w_5$$

where,

$V_j$  and  $W_j$ , ( $j=1,5$ ) are constant coefficients for each term. The adaptive coefficient feature is provided for these coefficients.

$v_j$ ,  $w_k$ , ( $j=1,5; k=4,5$ ) are variables/parameters selected from the user dictionary.

As an example, suppose an antilock system operated so as to always rise to the maximum pressure attained in the previous cycle rather than to treadle pressure. PDRSE would then be defined as simply

$$\text{PDRSE} = (1.0) \text{POFF1}$$

where 1.0 is  $W_1$  and POFF1, the maximum pressure from the last cycle, is selected from the user dictionary for  $v_1$ . In this case, the coefficient, 1.0, and the variable I.D. code for POFF1, 7, would be required as input for the option.

### Pulse-Width Modulated Square Wave

A time, or pulse-width, modulated square wave is provided as an option for general use. This option was motivated by a particular antilock system known to possess such a feature for purposes of treadle pressure modulation. The square wave generated under this option can be used in any portion of the program and is available in the user dictionary under the name SQUARE. Figure D-13 illustrates the parameter and variable relationships which define the square wave. The period of the square wave, PERIOD, is constant. The amount of time modulation, represented by TMOD, may be variable and programmable. This is accomplished in the program by allowing the ratio, TMOD/PERIOD, to be a tabular function of a variable,  $\epsilon_5$ , as shown in Figure D-14.  $\epsilon_5$  is defined as a general form expression:

$$\epsilon_5 = PW_1 v_1 + PW_2 v_2 + PW_3 v_3 + PW_4 v_4 w_4 + PW_5 v_5 w_5$$

where

$PW_i$ , ( $i=1,5$ ) are constant coefficients for each term. The adaptive coefficient feature is provided for these coefficients.

$v_i, w_k$ , ( $i=1,5; k=4,5$ ) are variables/parameters selected from the user dictionary.

Note that the  $FZ_i$  values in the TMOD/PERIOD table should not be greater than 1.0 or less than 0.0. Values of 1.0 ideally signify 100% modulation; values of 0.0, no modulation. (In

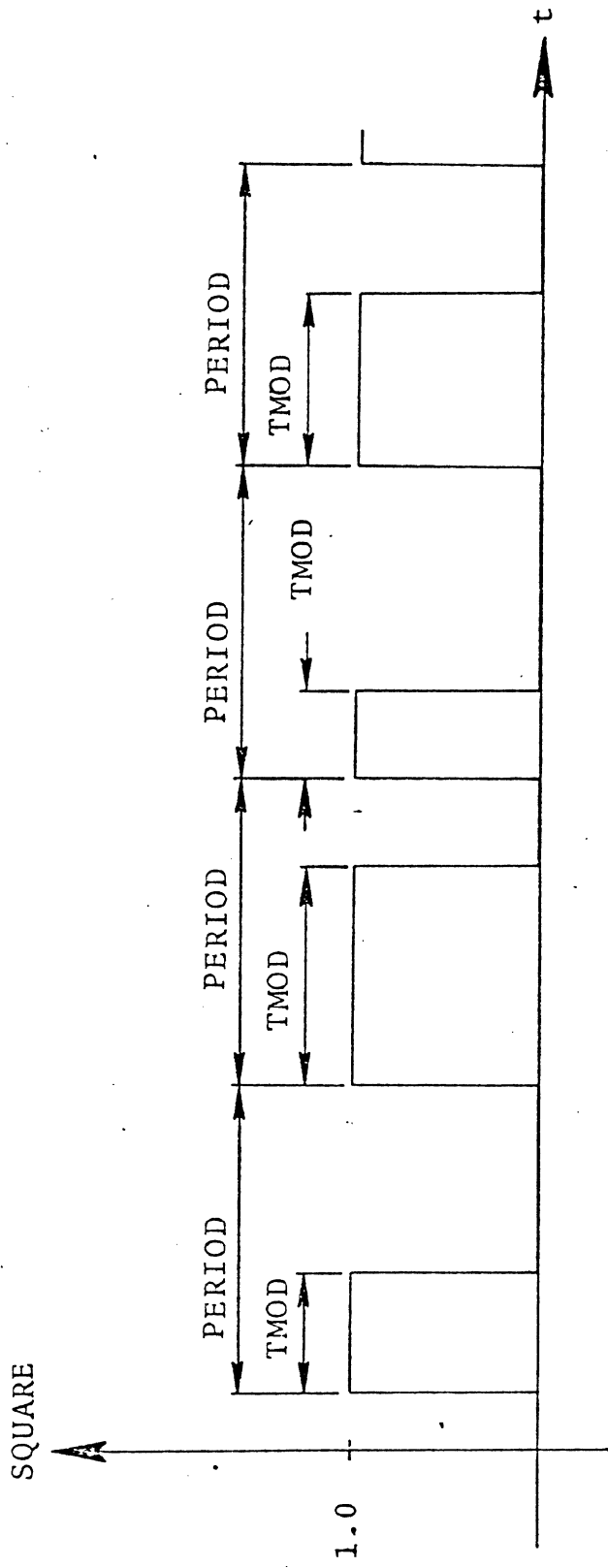


Figure D-13. Pulse-width modulated square wave.

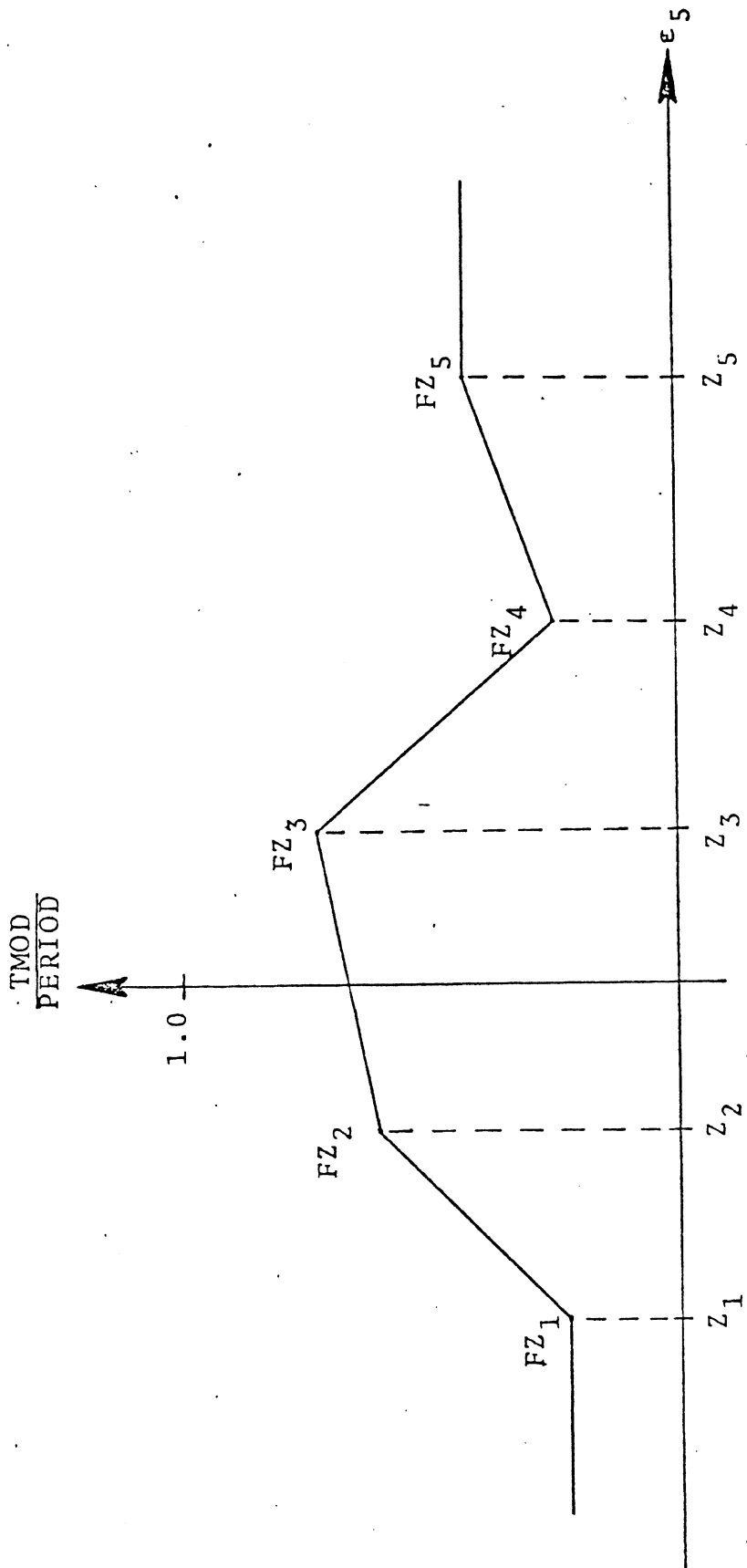


Figure D-14. Pulse-width table.

actuality, the degree of modulation attainable depends on the simulation time step used and the period chosen for the square wave.)

Input data required for this option includes: (a) five pairs of  $FZ_i$  and  $Z_i$ , (b) PERIOD, and (c) coefficient values and variable I.D. codes used in the general form expression for  $\epsilon_5$ . As before, a key for the pulse-width modulation option, IPWMKY, is read prior to any input for this option. IPWMKY values greater than or equal to 0 enable the option.

If desired, two additional sets of  $FZ_i$  values may be input. Each set is associated with a specific variable/parameter chosen by the user from the dictionary and a break-point for that variable/parameter. If the specified variable exceeds the break-point value for the given  $FZ_i$  set, that  $FZ_i$  set replaces the original or previous set used by the program. The purpose of this is to allow for some adaptive capability within the  $FZ_i$  table, if desired. The details of the numerical input for this adaptive option are explained in Section D.7.

### One-Shots

Three programmable one-shots are provided under this option and can be used for several different purposes. Two common uses are: (1) simulating time delay effects and (2) as auxiliary binary variables for use in any general purpose expressions. The three one-shots, as defined in this document, are binary variables having the numerical value of 1.0 or 0.0. These are available in the user dictionary under the names FOS1, FOS2, and FOS3.

The one-shots used in the program operate according to the following rule: If a trigger or input condition (inequality) changes from negative to positive, the one-shot will change its value from 0.0 to 1.0 for a fixed length of time, specified by the user, then return to 0.0. During a one-shot firing (1.0



value), the trigger input is disabled and cannot effect recurrent firings from this state. The one-shot is reset for another firing by two necessary occurrences: (1) the time duration of the present one-shot firing has been exceeded, followed by or concurrent with, (2) the trigger condition being negative. A trigger condition value of 0.0 is interpreted by the program as positive. See Figure D-15.

The one-shot can also be reset by a clear command which is programmed similarly as the trigger condition. It may be used to override any current trigger command to clear or reset the one-shot. The one-shot is reset whenever the clear condition is positive or zero. The clear condition is always evaluated after the trigger condition at each program time step.

The trigger condition is defined by the general form expression:

$$OS_1v_1 + OS_2v_2 + OS_3v_3 + OS_4v_4w_4 + OS_5v_5w_5 \geq 0$$

where

$OS_i$  ( $i=1,5$ ) are constant coefficients for each term and possess the adaptive coefficient feature.

$v_i, w_k$  ( $i=1,5; k=4,5$ ) are variables/parameters from the user dictionary.

The clear condition is defined by the general form expression:

$$RIDCL_1v_1 + RIDCL_2v_2 + RIDCL_3v_3 + RIDCL_4v_4w_4 + RIDCL_5v_5w_5 \geq 0$$

where

$RIDCL_i$  ( $i=1,5$ ) are constant coefficients for each term and possess the adaptive coefficient feature.

$v_i, w_k$  ( $i=1,5; k=4,5$ ) are variables/parameters from the user dictionary.

Each one-shot trigger and clear command is programmable by a general form expression as shown above. The one-shot time durations are denoted as  $TOS_1, \dots, TOS_5$  and are required as input for each one-shot used.

#### General Purpose Counter

This option allows the user to generate a count sequence by incrementing a counter by 1 every digital time step, if a particular inequality expression is greater than or equal to 0. The variable

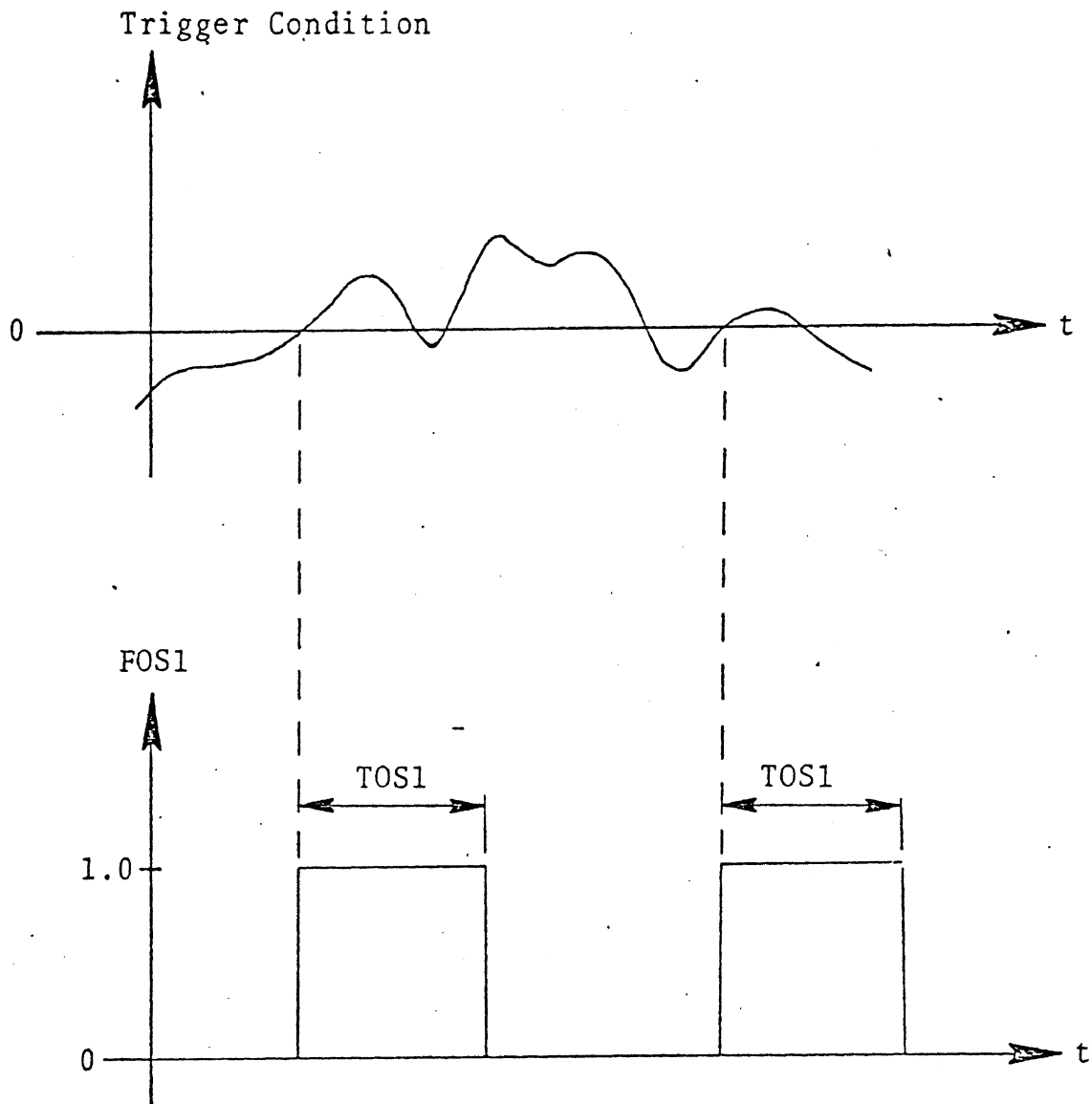


Figure D-15. One-shot operation. (Clear condition < 0)

containing the count is called GPCNT and is in the user dictionary with the I.D. code 44. The general form expression is given by

$$GP_1 v_1 + GP_2 v_2 + GP_3 v_3 + GP_4 v_4 w_4 + GP_5 v_5 w_5 > 0$$

where

$GP_i$  ( $i=1,5$ ) are constant coefficients for each term and can be adaptive.

$v_i, w_k$  ( $i=1,5; k=4,5$ ) are variables/parameters from the user dictionary.

If the above inequality is satisfied, the GPCNT count is incremented each time step. If only a one count increment is desired whenever a particular condition is satisfied, then a one-shot could be fired for a time period equal to or less than the digital time step, with the general purpose counter incrementing itself every one-shot firing.

The above discussion applies whenever the logic sampling period is specified as less than or equal to the digital simulation time step. If the user specifies a larger logic sampling period (slower sampling rate), then the general purpose counter will be incremented only each logic sampling period.

The counter can be reset to zero by allowing the inequality expression to become less than or equal to -10,000.

#### General Purpose Variables

This option allows the program user to define new dictionary variables as linear combinations and products of any other variables available in the dictionary. Each general purpose variable is defined by a general form expression:

$$GPV = GPVV_1 v_1 + GPVV_2 v_2 + GPVV_3 v_3 + GPVV_4 v_4 w_4 + GPVV_5 v_5 w_5$$

where

GPV is the general purpose variable

$GPVV_i$  ( $i=1,5$ ) are constant coefficients for each term and possess the adaptive coefficient feature.

D.7. Input Data Format - General Form Expressions. The most frequently occurring form encountered by the program user is the general form expression which appears in almost every program segment and special

option. As discussed in Section D.2, it has the form

$$C_1x_1 + C_2x_2 + C_3x_3 + C_4x_4y_4 + C_5x_5y_5$$

where

$C_i$  ( $i=1,5$ ) are the constant coefficients of each term.

$x_i, y_k$  ( $i=1,5; k=4,5$ ) are variables/parameters available in the user dictionary.

The user defines a given general form expression for the program by inputting three different pieces of information: (1) the number of terms in the expression required (1 to 5), (2) the variable I.D. codes corresponding to the  $x_i, y_k$  from the user dictionary for each variable/parameter used in constructing the expression, and (3) the coefficients of each term,  $C_i$ , used in the expression. The following data input sequence is what would be required for defining a general form expression:

NT	, number of terms	; I1 format
(I.D. code of $x_1$ )		; F10.4 format
(I.D. code of $x_2$ )		; F10.4 format
(I.D. code of $x_3$ )		; F10.4 format
(I.D. code of $x_4$ ), (I.D. code of $y_4$ )		; 2F10.4 format
(I.D. code of $x_5$ ), (I.D. code of $y_5$ )		; 2F10.4 format
Coefficient of $x_1$		; F10.4 format
Coefficient of $x_2$		; F10.4 format
Coefficient of $x_3$		; F10.4 format
Coefficient of $x_4y_4$		; F10.4 format
Coefficient of $x_5y_5$		; F10.4 format

If NT is 5, the above format is used. If  $NT = M < 5$ , only M I.D. code cards and M coefficient cards are required. Note that the second fields of the I.D. code cards are used only for the 4th and 5th terms. The 4th and 5th terms allow for quadratic representations, but can be linear if one of the two variable I.D. codes is selected as 1.0 (unity parameter).

Constant terms are represented by the unity parameter, 1.0, and the desired constant coefficient.

As an example, consider the general form expression,  $\dot{x} - \omega - 10$ . The required input for this would be:

3	number of terms required; I1 format
5.	variable I.D. codes from the user
3.	dictionary corresponding to $\dot{x}$ , $\omega$ ,
1.	and the constant; F10.4 format
1.	the $C_j$ coefficients for each of
-1.	the terms; F10.4 format
-10.	

#### Adaptive Coefficient Input Format

As explained in Section D.4, an adaptive coefficient feature exists to allow the coefficients appearing in the general form expressions to change value as a function of one or two variables from the user dictionary and their associated break-points. The third and fourth fields (columns 21-30, 31-40) of each variable I.D. input card are used to identify the variable(s) to which the corresponding term's coefficient is adaptive. Similarly, the fourth and fifth fields (columns 31-40, 41-50) of each coefficient card are used for specifying their associated break-points. The alternate coefficients are specified in the second and third fields (columns 11-20, 21-30) of each coefficient card. Consider the example from the previous section and suppose it was desired to alter the coefficient of  $\dot{x}$ , i.e., 1., to values of .5, and .2 according to the following rule:

$$\text{Coefficient of } \dot{x} = \begin{cases} 1.0 & \text{initial or nominal value} \\ 0.5 & \text{whenever } \dot{\omega} > 25 \text{ and} \\ & t \leq 2.0 \\ 0.2 & \text{if } t > 2.0 \end{cases}$$

The input required would now become:

3  
 5.           ,           ;           4.           ,           2.           ,  
 3.  
 1.  
 1.           , 0.5   , 0.2           , 25.           ,           2.0           ,  
 -1.  
 -10.

where the numbers 4. and 2. are the I.D. codes for  $\dot{\omega}$  and  $t$ , respectively, and occur on the I.D. card for  $\dot{x}$  in fields 3 and 4.

If only one adaptive variable is required, then field 4 of the I.D. code card and fields 3 and 5 of the coefficient card should not be used. Negative I.D. codes are permitted for the adaptive variables. This will cause the program to invert the sign of the adaptive variable. It would be used if one found it more convenient to have the adaptive condition,  $u_{ij} > b_1$ , interpreted as

$$-u_{ij} > -b_1 \quad , \quad (u_{ij} < b_1).$$

Reference was made in Section D.4 to a numerical switch which allows the adaptive coefficient feature to be defined by Equation (D-6) rather than by Equation (D-5). If this optional

definition is desired, any negative number should be entered in field 2 (columns 11-20) of the variable I.D. card. Normally, this field is not used except when 4 or 5 terms are needed in a general form expression. In the case of a 4th or 5th term and the optional definition, the negative of the variable I.D. code should be used in field 2.

#### Pulse-Width Modulation Table - Adaptive Capability

The adaptive capability for the  $FZ_i$  table is implemented by the following numerical input procedure: If field 6 (column 51-60) of the first  $FZ_i$  card is non-zero, two more  $FZ_i$  cards are read. Each of these cards maintain the same five fields for the alternate  $FZ_i$  input. However, two additional fields are included (columns 51-60, 61-70) and are used to specify the adaptive variable I.D. code and its associated break-point for that card (alternate table). The second alternate card takes precedence over the first alternate in the event both break-points are exceeded. The following sample input is an example:

$Z_i$ card:	-30.	-10.	0.	10.	50.		
1st $FZ_i$ card:	0.	.10	.20	.50	.90	99.	
1st alternate $FZ_i$ card:	0.	.05	.10	.25	.45	5.	50.
2nd alternate $FZ_i$ card:	0.	.025	.05	.12	.22	5.	70.

The number 99. in field 6 for the 1st  $FZ_i$  card simply causes the next two cards to be read. Both alternate cards are adaptive in this case to the same variable, vehicle velocity (I.D. code 5; field 6). The respective break-points are 50. ft/sec and 70. ft/sec. The effect of this input is to cause the program to use table 3 for speeds above 70 ft/sec, table 2 for speeds between 70 ft/sec and 50 ft/sec, and table 1 for speeds less than 50 ft/sec. The adaptive variables do not have to be the same, as in the example.

### Antilock Input Stream

Before any input data for the antilock subroutine is read, a key parameter (ILOCK) is read to indicate whether or not any wheel of the vehicle possesses an antilock system (see Section 3.6 of the Users Manual). If any or all wheels do, the key parameter (ILOCK) in the input stream should be set to 01 (I2 format). If no antilock system at all is desired, ILOCK should be set to 0. No antilock data should follow ILOCK if ILOCK is 0. For ILOCK set to 01, the following table number and input parameter discussion applies for each wheel on the vehicle train.

A table number not currently in use for a tire, spring, or other antilock table, causes the program to read antilock data for the specified table number. Subsequent wheels on the vehicle train requiring the same antilock data as one previously read, need only enter the same table number. An entry of 0 for any antilock table number implies no antilock system for that wheel.

The following example illustrates the antilock table number usage for a tractor-trailer with tandem rear suspensions on the tractor and trailer. Following an 01 ILOCK entry indicating antilock systems on the vehicle train:



0	}	No antilock on the tractor front axle	
0		(left and right wheels)	
05	}	New table number of tractor rear suspension,	
		front tandem axle, left side	
.	}	Antilock data for front tandem axle,	
.			left side
.			
.			
.			
05	}	Same antilock data requested for front	
		tandem, right side	
05	}	Same antilock data requested for rear tandem,	
05		left and right sides	
06	}	New table number for trailer rear suspensions,	
		front tandem, left side	
.	}	Antilock data for trailer front tandem,	
.			left side
.			
.			
.			
06	}	Same antilock data requested for trailer front	
		tandem, right side	
0	}	No antilock data for trailer rear tandem	
0		axle, left and right wheels	

The numerical inputs for OPTION, the side-to-side option key, are as follows:

OPTION

- 01 => Worst Wheel
- 02 => Best Wheel
- 03 => Average Wheel
- 04 => Independent Wheel  
(I2 format)

The following list defines all the input parameters available for each antilock system used. The parameters required should be entered in the order given below.

It should be noted that this complete listing is presented to define the order and format of any required input data. The program, however, requires only that amount of input data needed to define a particular system.

<u>Input</u>	<u>Description</u>	<u>Format</u>		
ILOCK	global antilock key	I2		
TN <sub>1</sub>	Table number entry for 1st wheel (front axle, left side)	I2		
OPTION <sub>1</sub>	side-to-side option, 1st wheel	I2		
WWDIF	side-to-side wheel speed difference operator (see variable I.D. 60 definition)	F10.2		
NOFF <sub>1</sub>	No. of 'OFF' <u>inequalities</u> to follow	I1		
M1	No. of terms in 1st inequality	I1		
ID <sub>1</sub> · · · ID <sub>M1</sub>	M1 variable I.D. code cards for logic inequality 1	4F10.4		
C <sub>1,1</sub> · · · C <sub>1,M1</sub>				
M <sub>2</sub>			No. of terms in 2nd inequality	I1
ID <sub>1</sub> · · · ID <sub>M2</sub>			M2 variable I.D. code cards for logic inequality 2	4F10.4
C <sub>2,1</sub> · · · C <sub>2,M2</sub>				
M <sub>3</sub>	No. of terms in 3rd inequality	I1		
· · · ·	· · · ·			

For NOFF<sub>1</sub> inequality expressions, NOFF<sub>1</sub> ≤ 4.

$NON_1$	No. of 'ON' inequalities to follow	I1
M5	No. of terms in 5th inequality	I1
$ID_1$ · · · $ID_{M5}$	M5 variable I.D. code cards for logic inequality 5	4F10.4
$C_{5,1}$ · · · $C_{5,M5}$		
M6	No. of terms in 6th inequality	I1
·	·	
·	·	
·	·	
·	·	
·	·	

For  $NON_1$  inequality expressions,  $NON_1 \leq 4$ .

---

$\tau_1, \tau_2, \tau_3, \tau_4$	Logic time delays	4F10.4
IPKEY	Pressure modulator key	I1
N1	No. of terms in $\epsilon_1$ expression (IPKEY=0,2)	I1
$ID_1$ · · · $ID_{N1}$	N1 variable I.D. code cards	4F10.4
$H_1$ · · · $H_{N1}$		
	N1 coefficient cards	5F10.4

N2		No. of terms in the $\epsilon_2$ expressions	I1
ID <sub>1</sub>	}	N2 variable I.D. code cards	4F10.4
·			
ID <sub>N2</sub>			
G <sub>1</sub>	}	N2 coefficient cards	5F10.4
·			
G <sub>N2</sub>			
X <sub>1</sub> X <sub>2</sub>		$\epsilon_1$ break-points	2F10.4
X <sub>3</sub> X <sub>4</sub>		$\epsilon_2$ break-points	2F10.4
PFE1 PFE2 PFE3		exponential fall rates	3F10.4
PRE1 PRE2 PRE3		exponential rise rates	3F10.4
N3		No. of terms in $\epsilon_3$ expression (IPKEY=1,2)	I1
ID <sub>1</sub>	}	N3 variable I.D. code cards	4F10.4
·			
ID <sub>N3</sub>			
R <sub>1</sub>	}	N3 coefficient cards	5F10.4
·			
R <sub>N3</sub>			
N4		No. of terms in $\epsilon_4$ expression	I1
ID <sub>1</sub>	}	N4 variable I.D. code cards	4F10.4
·			
ID <sub>N4</sub>			

$S_1$ . . . $S_{N4}$	} N4 coefficient cards	5F10.4
$X_5$ $X_6$	$\epsilon_3$ break-points	2F10.4
$X_7$ $X_8$	$\epsilon_4$ break-points	2F10.4
PFL1 PFL2 PFL3	linear fall rates	3F10.4
PRL1 PRL2 PRL3	linear rise rates	3F10.4
$\tau_{ON}$ , $\tau_{OFF}$	pressure modulator time delays	2F10.4
$\tau_W$ , $\tau_{WD}$	wheel rate, acceleration time constants	2F10.4
$OP_{12}$ , $OP_{23}$ , $OP_{34}$	logical operator switches	3I1
$OP_{56}$ , $OP_{67}$ , $OP_{78}$	logical operator switches	3I1
IPDKEY	treadle pressure modulator key	I2
N5	No. of terms for PDRISE	I1
$ID_1$ . . . $ID_{N5}$	} N5 variable I.D. code cards	4F10.4
$W_1$ . . . $W_{N5}$	} N5 coefficient cards	5F10.4
N6	No. of terms in PDFALL expression	I1
$ID_1$ . . . $ID_{N6}$	} N6 variable I.D. code cards	4F10.4

$V_1$ . . . $V_{N6}$	}    	N6 coefficient cards	5F10.4
IPWMKY		pulse-width modulation key	I2
PERIOD		period of pulse-width modulated square wave	F10.4
N7		No. of terms in $\epsilon_5$ expression	I1
$ID_1$ . . . $ID_{N7}$	}    	N7 variable I.D. code cards	4F10.4
$PW_1$ . . . $PW_{N7}$	}    	N7 coefficient cards	5F10.4
$Z_1, Z_2, Z_3, Z_4, Z_5$		$\frac{TMOD}{PERIOD}$ table break-points	5F10.4
$FZ_1, FZ_2, FZ_3, FZ_4, FZ_5$		$\frac{TMOD}{PERIOD}$ table input	6F10.4
		alternate/adaptive $FZ_i$ input (see Section )	7F10.4 7F10.4
IOSKEY		one-shot option key	I2
N1		No. of terms for 1st one-shot expression	I1
$ID_1$ . . . $ID_{N1}$	}    	N1 variable I.D. code cards	4F10.4

OS <sub>1</sub>	}	N1 coefficient cards	5F10.4
·			
·			
OS <sub>N1</sub>			
NC1		no. of terms for 1st one-shot 'clear' expression	I1
ID <sub>1</sub>	}	N1 variable I.D. code cards	4F10.4
·			
·			
ID <sub>NC1</sub>			
RIDCL <sub>1</sub>	}	N1 coefficient cards	5F10.4
·			
·			
RIDCL <sub>NC1</sub>			
TOS <sub>1</sub>		time duration of 1st one-shot	F10.4
N2		no. of terms in 2nd one-shot expression	I1
ID <sub>1</sub>	}	N2 variable I.D. code cards	4F10.4
·			
·			
ID <sub>N2</sub>			
OS <sub>1</sub>	}	N2 coefficient cards	5F10.4
·			
·			
OS <sub>N2</sub>			
NC2		no. of terms for 2nd one-shot 'clear' expression	I1
ID <sub>1</sub>	}	N2 variable I.D. code cards	4F10.4
·			
·			
ID <sub>N2</sub>			
RIDCL <sub>1</sub>	}	N2 coefficient cards	5F10.4
·			
·			
RIDCL <sub>NC2</sub>			



TOS2		time duration of 2nd one-shot expression	F10.4
N3		no. of terms in 3rd one-shot expression	I1
ID <sub>1</sub>	}	N3 variable I.D. code cards	4F10.4
·			
ID <sub>N3</sub>			
OS <sub>1</sub>	}	N3 coefficient cards	5F10.4
·			
OS <sub>N3</sub>			
NC3		no. of terms for 3rd one-shot 'clear' expression	I1
ID <sub>1</sub>	}	NC3 variable I.D. code cards	4F10.4
·			
ID <sub>NC3</sub>			
RIDCL <sub>1</sub>	}	NC3 coefficient cards	5F10.4
·			
RIDCL <sub>NC3</sub>			
TOS3		time duration of 3rd one-shot	F10.4
N4		no. of terms for 4th one-shot expression	I1
ID <sub>1</sub>	}	N4 variable I.D. code cards	4F10.4
·			
ID <sub>N4</sub>			
OS <sub>1</sub>	}	N4 coefficient cards	5F10.4
·			
OS <sub>N4</sub>			

NC4		no. of terms for 4th one-shot 'clear' expression	I1
ID <sub>1</sub>	}	NC4 variable I.D. code cards	4F10.4
⋮			
ID <sub>NC4</sub>			
RIDCL <sub>1</sub>	}	NC4 coefficient cards	5F10.4
⋮			
RIDCL <sub>NC4</sub>			
TOS4		time duration of 4th one-shot	F10.4
N5		no. of terms for 5th one-shot expression	I1
ID <sub>1</sub>	}	N5 variable I.D. code cards	4F10.4
⋮			
ID <sub>N5</sub>			
OS <sub>1</sub>	}	N5 coefficient cards	5F10.4
⋮			
OS <sub>N5</sub>			
NC5		no. of terms for 5th one-shot 'clear' expression	I1
ID <sub>1</sub>	}	NC5 variable I.D. code cards	4F10.4
⋮			
ID <sub>NC5</sub>			
RIDCL <sub>1</sub>	}	NC5 coefficient cards	5F10.4
⋮			
RIDCL <sub>NC5</sub>			
TOS5		time duration of 5th one-shot	F10.4

IGPKEY		general purpose counter key	I2
NG		no. of terms in general purpose counter expression	I1
ID <sub>1</sub>	}	NG variable I.D. code cards	4F10.4
·			
ID <sub>NG</sub>			
GP <sub>1</sub>	}	NG coefficient cards	5F10.4
·			
GP <sub>NG</sub>			
IGPVKY		general purpose variable option key	I2
NV <sub>1</sub>		no. of terms in first general purpose expression	I1
ID <sub>1</sub>	}	NV1 variable I.D. code cards	4F10.4
·			
ID <sub>NV1</sub>			
GPV <sub>1</sub>	}	NV1 coefficient cards	5F10.4
·			
GPV <sub>NV1</sub>			
NV2		no. of terms in 2nd general purpose expression	I1
ID <sub>2</sub>	}	NV2 variable I.D. code cards	4F10.4
·			
ID <sub>NV2</sub>			
GPV <sub>1</sub>	}	NV2 coefficient cards	5F10.4
·			
GPV <sub>NV2</sub>			
NV3		no. of terms in 3rd general purpose expression	I1

ID <sub>3</sub> ⋮ ID <sub>NV3</sub>	} NV3 variable I.D. code cards	4F10.4
GPV <sub>3</sub> ⋮ GPV <sub>NV3</sub>	} NV3 coefficient cards	5F10.0
NV4	no. of terms in 4th general purpose variable expression	I1
ID <sub>1</sub> ⋮ ID <sub>NV4</sub>	} NV4 variable I.D. code cards	4F10.4
GPV <sub>1</sub> ⋮ GPV <sub>NV4</sub>	} NV4 coefficient cards	5F10.4
NV5	no. of terms in 5th general purpose variable expression	I1
ID <sub>1</sub> ⋮ ID <sub>NV5</sub>	} NV5 variable I.D. code cards	4F10.4
GPV <sub>1</sub> ⋮ GPV <sub>NV5</sub>	} NV5 coefficient cards	5F10.4
TSMPL	control logic sampling period	F10.4
TN <sub>2</sub>	Table number entry for 2nd wheel (front axle, right side)	I2
OPTION <sub>2</sub>	OPTION for 2nd wheel	I2
	{ Same input format as for wheel 1 }	

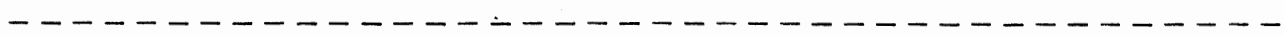
Table number entry for 3rd wheel I2

OPTION<sub>3</sub> OPTION for 3rd wheel I2

{ Same input format as for wheel 1 }

•  
•  
•

End of antilock input



The following section provides two example problems and their associated input lists.

### Example Problems

#### EXAMPLE 1.

Suppose an antilock system possesses the following features: (1) a wheel sensor time delay effect of 10 ms. and another 20 ms. delay in the derivation of wheel acceleration; (2) control logic which generates an "OFF" signal once the wheel acceleration falls below  $-50.0 \text{ ft/sec}^2$  and an "ON" signal for wheel accelerations greater than  $-10.0 \text{ ft/sec}^2$ ; (3) pressure modulator time delays of 40 ms. for "OFF" signals and 60 ms. for "ON" signals. The supposed exponential pressure rates are functions of wheel acceleration defined as follows:

$$\begin{aligned} \text{Pressure Fall Rate} &\equiv (0.1)^{-1} = 10.0 \text{ for } \dot{\omega} \leq -100 \text{ ft/sec}^2 \\ &\quad (0.2)^{-1} = 5.0 \text{ for } \dot{\omega} > -100 \text{ ft/sec}^2 \end{aligned}$$

$$\begin{aligned} \text{Pressure Rise Rate} &\equiv (0.2)^{-1} = 5.0 \text{ for } \dot{\omega} \leq 50 \text{ ft/sec}^2 \\ &\quad (0.1)^{-1} = 10.0 \text{ for } \dot{\omega} > 50 \text{ ft/sec}^2 \end{aligned}$$

The following choice of input parameters would describe the above antilock system:

$$\tau_{\omega} = 0.01$$

$$\tau_{\omega d} = 0.02$$

$$C_{11} = -1.0$$

$$\rightarrow F_1 = -\dot{\omega} - 50.0 \geq 0$$

$$C_{12} = -50.0$$

$$C_{51} = 1.0$$

$$\rightarrow F_5 = \dot{\omega} + 10.0 \geq 0$$

$$C_{52} = 10.0$$

I.D. Code for  $\dot{\omega} = 4$ .

I.D. Code for 1.0 = 1.

$$\tau_1 = \tau_3 = \tau_4 = 0.0$$

$$\tau_2 = 0.2$$

$$H_1 = 1.0$$

$$\rightarrow \epsilon_1 = \dot{\omega} + 100$$

$$H_2 = 100.0$$

$$X_1 = -10000.0$$

$$X_2 = 0.0$$

$$PFE1 = 10.0$$

$$PFE2 = 5.0$$

$$G_1 = 1.0$$

$$\rightarrow \epsilon_2 = \dot{\omega} - 50.0$$

$$G_2 = -50.0$$

$$X_3 = -10000.0$$

$$X_4 = 0.0$$

$$\text{PRE1} = 5.0$$

$$\text{PRE2} = 10.0$$

$$\text{OP}_{12} = \text{OP}_{23} = \text{OP}_{34} = \text{OP}_{56} = \text{OP}_{67} = \text{OP}_{78} = \text{either } 0 \text{ or } 1$$

$$\tau_{\text{ON}} = 0.06$$

$$\tau_{\text{OFF}} = 0.04$$

The following input list would be required:



01			ILOCK	
01			TN <sub>1</sub>	
01			worst-wheel side-to-side option	
0:0			WWDIF	
1			NOFF1	
2			M1	
4.			I.D. code for $\dot{\omega}$	
1.			I.D. code for 1.0	
-1.			1st term coefficient, C <sub>11</sub>	
-50.			2nd term coefficient, C <sub>12</sub>	
1			NON <sub>1</sub>	
2			M5	
4.			I.D. code for $\dot{\omega}$	
1.			I.D. code for 1.0	
1.			1st term coefficient, C <sub>51</sub>	
10.			2nd term coefficient, C <sub>52</sub>	
0.	0.	0.	0.	$\tau_i$
0			IPKEY	
2			N1	
4.			I.D. for $\dot{\omega}$	
1.	}	$\epsilon_1$	I.D. for 1.0	
1.			1st term coefficient for $\epsilon_1$	
100.			2nd term coefficient for $\epsilon_1$	
2			N2	
4.			I.D. for $\dot{\omega}$	
1.	}	$\epsilon_2$	I.D. for 1.0	
1.			1st term coefficient for $\epsilon_2$	
-50.			2nd term coefficient for $\epsilon_2$	
-10000.	0.		X <sub>1</sub> , X <sub>2</sub>	
-10000.	0.		X <sub>3</sub> , X <sub>4</sub>	

10.	10.	5.	PFE1, PFE2, PFE3
5.	5.	10.	PRE1, PRE2, PRE3
.06	.04		$\tau_{ON}$ , $\tau_{OFF}$
.01	.02		$\tau_W$ , $\tau_{WD}$
000			OP <sub>12</sub> , OP <sub>23</sub> , OP <sub>34</sub>
000			OP <sub>56</sub> , OP <sub>67</sub> , OP <sub>78</sub>
-1			IPDKEY
-1			IPWMKY
-1			IOSKEY
-1			IGPKEY
-1			IGPVKY
.0001			TSMPL
01			TN <sub>2</sub>
01			TN <sub>3</sub>
.			.
.			.
.			.

EXAMPLE 2.

Simulation of an antilock system having the following features:

Wheel Sensor:  $\tau_{\omega}, \tau_{\omega d} = .010$  seconds

Control Logic:

OFF signal given by

$$\begin{aligned} F_1 &= \dot{x} - \omega - 14 \geq 0, \text{ for } \dot{x} > 50 \text{ ft/sec} \\ &= \dot{x} - \omega - 11 \geq 0, \text{ for } \dot{x} \leq 50 \end{aligned}$$

AND

$$F_2 = -\dot{\omega} - 12 \geq 0$$

OR

$$F_3 = \text{SLIP} - .50 \geq 0$$

ON signal generated when

$$F_5 = -\dot{x} + \omega + 10 \geq 0$$

AND

$$F_6 = \dot{\omega} - 20. \geq 0$$

OR

$$F_7 = \dot{\omega} - 250. \geq 0$$

Pressure Modulator:

- a)  $\tau_{ON} = .015 \text{ sec.}$  ;  $\tau_{OFF} = .010 \text{ sec.}$
- b) One exponential fall rate of  $14. \text{ sec}^{-1}$ .
- c) One exponential rise rate of  $14. \text{ sec}^{-1}$ .  
and one linear rise rate of  $45. \text{ sec}^{-1}$ .

The exponential and linear pressure rise regions are determined by a decaying time ramp from the maximum pressure in the previous cycle. For pressure below this time ramp, the pressure rise is exponential; for pressure greater than the time ramp, the pressure rise is linear (see Figure D-16). The decaying time ramp can be written as

$$P_{MAX1} - 85. (t - T_{P_{MAX1}})$$

where

$P_{MAX1}$  is the maximum pressure in the last cycle

$t$  is time

$T_{P_{MAX1}}$  is the time of the maximum pressure in  
the last cycle

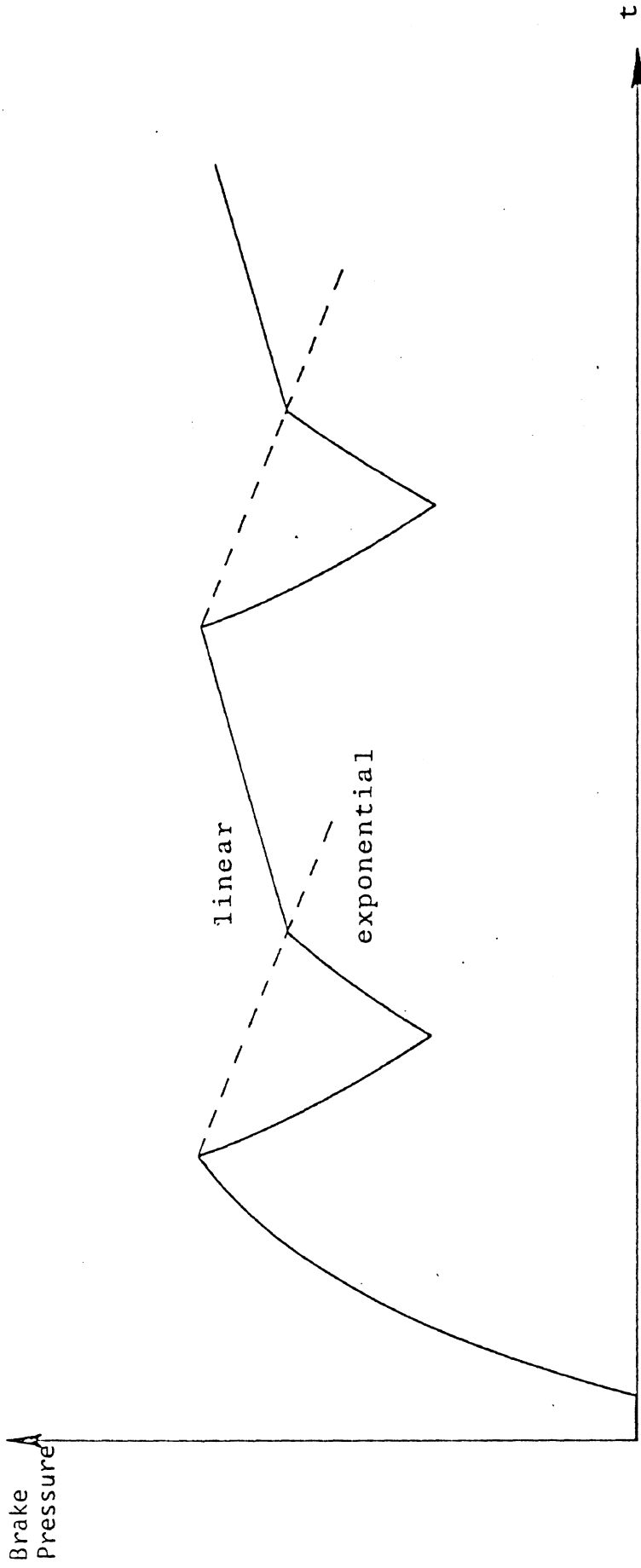
and 85. is the rate of decay. (psi/sec)

By subtracting the above expression from brake pressure,  $P$ , the  $\epsilon_2$  and  $\epsilon_4$  general expressions become:

$$\epsilon_2 = P - P_{MAX1} + 85 T - 85 T_{P_{MAX1}}$$

and

$$\epsilon_4 = P - P_{MAX1} + 85 T - 85 T_{P_{MAX1}},$$



PRESSURE MODULATOR CHARACTERISTIC - - - SYSTEM #2.

Figure D-16.

the switching point occurring at  $\varepsilon_2 = \varepsilon_4 = 0$ . Therefore, the desired rise characteristic can be simulated by the following set of pressure inputs:

$$X_3 = X_4 = X_7 = X_8 = 0$$

$$\text{PRE1} = \text{PRE2} = 14. \quad , \quad \text{PRE3} = 0$$

$$\text{PRL1} = \text{PRL2} = 0. \quad , \quad \text{PRL3} = 45.$$

The following input list would be required:

01		ILOCK
01		TN <sub>1</sub>
01		OPTION <sub>1</sub>
0.0		WWDIF
3		NOFF <sub>1</sub>
3		M1
5.		
3.		
1.	, , 5. , ,	
1.		C <sub>11</sub>
-1.		C <sub>12</sub>
-11. , -14. , , 50. , ,		C <sub>13</sub>
2		M2
4.		
1.		
-1.		C <sub>21</sub>
-120.		C <sub>22</sub>
2		M3
34.		
1.		
1.		C <sub>31</sub>
-.50		C <sub>32</sub>
3		NON <sub>1</sub>
3		M5
5.		
3.		
1.		

-1.						$C_{51}$
1.						$C_{52}$
10.						$C_{53}$
2						M6
4.						
1.						
1.						$C_{61}$
-20.						$C_{62}$
2						M7
4.						
1.						
1.						$C_{71}$
-250.						$C_{72}$
0.	0.	0.	0.			$\tau_i$
2						IPKEY
1						N1
1.						
5.						
						$\epsilon_1$
4						N2
35.						
27.						
2.						
21.	1.					
1.						$\epsilon_2$
-1.						
85.						
85.						



0.	0.		$X_1, X_2$
0.	0.		$X_3, X_4$
14.	14.	14.	PFE1, PFE2, PFE3
14.	14.	0.	PRE1, PRE2, PRE3
1			N3
1.		}	$\epsilon_3$
5.			
4			
35.		}	$\epsilon_4$
27.			
2.			
21.	1.		
1.			
-1.			
85.			
85.			
0.	0.		$X_5, X_6$
0.	0.		$X_7, X_8$
0.	0.	0.	PFL1, PFL2, PFL3
0.	0.	45.	PRL1, PRL2, PRL3
.015	.010		$\tau_{ON}, \tau_{OFF}$
.010	.010		$\tau_{\omega}, \tau_{\omega D}$
100			OP <sub>12</sub> , OP <sub>23</sub> , OP <sub>34</sub>
100			OP <sub>56</sub> , OP <sub>67</sub> , OP <sub>78</sub>
-1			IPDKEY
-1			IPWMKY
-1			IOSKEY

-1

IGPKEY

-1

IGPVKY

.0001

TSMPL

01

TN<sub>2</sub>

01

TN<sub>3</sub>

·  
·  
·  
·

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### Output-Echo Format

Figures D-17 through D-20 show an example of the kind of output-echo produced by the antilock subroutine. The first output page is simply the user dictionary of variables/parameters. The succeeding pages represent a computer echo of the antilock input. The "First" and "Second Adaptive Value" columns refer to the alternate coefficients available with the adaptive coefficient feature. The "First" and "Second Adaptive Variable" columns echo the variable I.D. codes for the two adaptive variables, while the columns labeled "First" and "Second Break-Point" contain their associated break-points. If the secondary adaptive coefficient definition (Figure D-8) is used, the word "AND" appears between the First and Second Adaptive Variable columns in the output echo for that coefficient. Any input not associated with a general form expression is listed under "Non-Adaptive Antilock Parameters."

\*\*\*\*\*  
 \*\*\*\*\* DICTONARY OF ANTILOCK VARIABLES/PARAMETERS AVAILABLE TO USER. \*\*\*\*\*  
 \*\*\*\*\*

VARIABLE I.D.	DESCRIPTION	VARIABLE I.D.	DESCRIPTION
1	I.O	45	WMAX1
2	TIME	46	WMAX2
3	OMEGA	47	TWMAX1
4	OMEGADOT	48	TWMAX2
5	XDOT	49	WMIN
6	XDDOT	50	TMIN
7	POFF1	51	TPMAX2
8	POFF2	52	TPMIN2
9	PON1	53	GPV1
10	PON2	54	GPV2
11	TOFF1	55	GPV3
12	TON1	56	GPV4
13	XDOFF	57	GPV5
14	XDON	58	FOS4
15	WOFF	59	FOS5
16	WON	60	OMEGDIF
17	WDOFF		
18	WONN		
19	WDMAX		
20	WDMIN		
21	TPMAX1		
22	TPMIN1		
23	WLOCK		
24	TLOCK		
25	SLOW		
26	SLOFF		
27	PMAX1		
28	PMAX2		
29	PMIN1		
30	PHIN2		
31	PD		
32	ON		
33	TMOD		
34	SLIP		
35	P		
36	CYCNT		
37	SQUARE		
38	SQJARN		
39	TOFF2		
40	TON2		
41	FOS1		
42	FOS2		
43	FOS3		
44	GPCNT		

Figure D-17. Antilock Output Echo

\*\*\* ANTI-LOCK SUBROUTINE INPUT PARAMETER TABLE --- AXLE 1. \*\*\*

SYMBOL	DESCRIPTION	INITIAL VALUE	FIRST ADAPTIVE VALUE	SECOND ADAPTIVE VALUE	INITIAL VALUE VARIABLE	FIRST ADAPTIVE VARIABLE	SECOND ADAPTIVE VARIABLE	FIRST BREAK-PT	SECOND BREAK-PT
INEQUALITY EXPRESSION: 1									
C (1)	COEFFICIENT (1)	-1.0000			3				
C (2)	COEFFICIENT (2)	1.0000			45				
C (3)	COEFFICIENT (3)	-20.0000	-10.0000		2	6		-16.000	
C (4)	COEFFICIENT (4)	20.0000	10.0000		47, 1	6		-16.000	
C (5)	COEFFICIENT (5)	-4.0000	-7.0000		1, 1	36		0.500	
INEQUALITY EXPRESSION: 2									
C (1)	COEFFICIENT (1)	-1.0000			4				
C (2)	COEFFICIENT (2)	-70.0000			1				
INEQUALITY EXPRESSION: 3									
C (1)	COEFFICIENT (1)	1.0000			42				
C (2)	COEFFICIENT (2)	-0.1000			1				
C (3)	COEFFICIENT (3)	1000.0000			23				
INEQUALITY EXPRESSION: 5									
C (1)	COEFFICIENT (1)	1.0000			3				
C (2)	COEFFICIENT (2)	-1.0000			45				
C (3)	COEFFICIENT (3)	20.0000	10.0000		2	6		-16.000	
C (4)	COEFFICIENT (4)	-20.0000	-10.0000		47, 1	6		-16.000	
C (5)	COEFFICIENT (5)	7.0000			1, 1				
INEQUALITY EXPRESSION: 6									
C (1)	COEFFICIENT (1)	1.0000			4				
C (2)	COEFFICIENT (2)	-20.0000			1				
INEQUALITY EXPRESSION: 7									
C (1)	COEFFICIENT (1)	1.0000			42				
C (2)	COEFFICIENT (2)	-0.1000			1				

EPSILON 1:

Figure D-18. Antilock output echo.

P (1)	COEFFICIENT (1)	5.0000			1			
EPSILON 2:								
G (1)	COEFFICIENT (1)	1.0000			35			
G (2)	COEFFICIENT (2)	-1.0000			27			
G (3)	COEFFICIENT (3)	200.0000	100.0000		2		36	1.500
G (4)	COEFFICIENT (4)	-200.0000	-100.0000		21,	1	36	1.500
EPSILON 3:								
R (1)	COEFFICIENT (1)	5.0000			1			
EPSILON 4:								
S (1)	COEFFICIENT (1)	1.0000			35			
S (2)	COEFFICIENT (2)	-1.0000			27			
S (3)	COEFFICIENT (3)	200.0000	100.0000		2		36	1.500
S (4)	COEFFICIENT (4)	-200.0000	-100.0000		21,	1	36	1.500
ONE-SHOT 1:								
OS1 (1)	COEFFICIENT (1)	-1.0000			3			
OS1 (2)	COEFFICIENT (2)	1.0000			45			
OS1 (3)	COEFFICIENT (3)	-20.0000	-10.0000		2		6	-16.000
OS1 (4)	COEFFICIENT (4)	20.0000	10.0000		47,	1	6	-16.000
OS1 (5)	COEFFICIENT (5)	-6.0000			1,	1		
ONE-SHOT 2:								
OS2 (1)	COEFFICIENT (1)	0.0			1			
OS2 (2)	COEFFICIENT (2)	-0.1000			1			
OS2 (3)	COEFFICIENT (3)	50.0000			41			
OS2 (4)	COEFFICIENT (4)	1.0000			41,	4		
** NON-ADAPTIVE ANTI-LCK PARAMETERS. **								
TAU1	LOGIC TIME DELAY	0.0						
TAU2	"	0.0						
TAU3	"	0.0						
TAU4	"	0.0						
X1	EPSILON 1 BREAK-PT	0.0						
X2	"	50.0000						
X3	EPSILON 2 BREAK-PT	-5.0000						
X4	"	2.5000						
PFE1	EXP. PRESSURE FALL RATE	12.5000						
PFE2	"	12.5000						
PFE3	"	12.5000						
PRE1	EXP. PRESSURE RISE RATE	14.0000						
PRE2	"	14.0000						
PRE3	"	0.0						
X5	EPSILON 3 BREAK-PT	0.0						
X6	"	50.0000						
X7	EPSILON 4 BREAK-PT	-5.0000						

Figure D-19. Antilock output echo.

Y8		2.
PFL1	LIN. PRESSURE FALL RATE	0.0
PFL2	"	0.0
PPL3	"	0.0
PRL1	LIN. PRESSURE RISE RATE	0.0
PRL2	"	0.0
PRL3	"	40.0000
TAUON	PRESSURE-ON TIME DELAY	0.0150
TAUOFF	PRESSURE-OFF TIME DELAY	0.0100
TAUW	TIME CONSTANT-WHEEL RATE	0.0100
TAUWD	TIME CONSTANT-WHEEL ACCEL.	0.0100
OP12	LOGICAL OPERATOR SWITCH	1
OP23	"	0
OP34	"	0
OP56	LOGICAL OPERATOR SWITCH	1
OP67	"	0
OP78	"	0
TOS1	ONE-SHOT TIME DURATION	0.0200
TOS2	ONE-SHOT TIME DURATION	0.0200
TSAMPLE	ANTI-LOCK SAMPLING RATE	0.0010
OPTION	SIDE-TO-SIDE	1

Figure D-20. Antilock output echo.

## APPENDIX E

### THE EQUATIONS OF MOTION

To explain the equations of motion of the system, it is convenient to describe several subsystems and their interconnections. These subsystems are described in an orthogonal coordinate system which will be defined first.

#### E.1 The Coordinate Systems

The coordinate systems used are unchanged from the Phase II HSRI/MVMA program [2],\* and details can be found in Section 4.1.2 of this manual. To briefly summarize:

Each sprung mass has a set of body axes fixed to the sprung mass origin at the sprung mass center designated as  $x, y, z$ , where  $x$  goes toward the front,  $y$  goes to the right, and  $z$  goes down.

A second set of axes is the inertial set designated as  $X, Y, Z$ . These are fixed and never change direction. In the initial condition for any simulation run, the sprung mass c.g. of the truck/tractor is at the origin of  $X, Y, Z$ , facing in the  $X$  direction.

A third set of axes, called the yaw plane system, is required. These are designated as  $\bar{x}, \bar{y}, \bar{z}$ , and have an origin which follows the sprung mass c.g. The direction of  $\bar{z}$  remains normal to the road, and  $\bar{x}$  and  $\bar{y}$  follow the rotation of the vehicle around the  $\bar{z}$  axis. Thus,  $\bar{x}$  faces along the projection of  $x$  in the road plane.

There is frequent need to rotate forces and moments from one coordinate system to another. These are done using the "A" matrix, which rotates vectors between body and inertial, and the "BZ" matrix, which rotates vectors between body and yaw plane. The cosine and sine of the yaw angle,  $\psi$ , is used to go between the yaw plane and inertial systems.

---

\*Numbers in brackets designate references appearing in Section 6.0.



## E.2 General Equations

Each sprung mass has body axes  $x, y, z$ . All forces are rotated into these directions, resulting in  $\Sigma F_x, \Sigma F_y, \Sigma F_z$  which in the computer code are called FSUM(1), FSUM(2), and FSUM(3). As is typical in the vehicle dynamics literature, the velocity in the  $x$  direction is  $u$ , the velocity in the  $y$  direction is  $v$ , and the velocity in the  $z$  direction is  $w$ . The rotation rate about the  $x$  axis is  $p$ , the rotation rate about the  $y$  axis is  $q$ , and the rotation rate about the  $z$  axis is  $r$ .

The translational equations of motion are then:

$$\begin{aligned}M(\dot{u} - vr + wq) &= \Sigma F_x \\M(\dot{v} + ur - wp) &= \Sigma F_y \\M(\dot{w} + uq - vp) &= \Sigma F_z\end{aligned}$$

where  $M$  is the sprung mass and the dot indicates differentiation with respect to time. In the computer program these equations are solved for  $\dot{u}$ ,  $\dot{v}$ , and  $\dot{w}$  at the beginning of each integration time step.

There are also the equations of rotational motion about each body axis. All moments on the sprung mass are rotated into the  $x, y$ , and  $z$  directions, thus resulting in  $\Sigma M_x, \Sigma M_y$ , and  $\Sigma M_z$  which in the computer code are called TSUM(1), TSUM(2), and TSUM(3). The equations of rotational motion are Euler's equations with zero cross-products of inertia, namely:

$$\begin{aligned}I_{xx}\dot{p} + qr(I_{zz} - I_{yy}) &= \Sigma M_x \\I_{yy}\dot{q} + pr(I_{xx} - I_{zz}) &= \Sigma M_y \\I_{zz}\dot{r} + pq(I_{yy} - I_{xx}) &= \Sigma M_z\end{aligned}$$

where  $p$  is the rotation rate about  $x$ ,  $q$  about  $y$ , and  $r$  about  $z$ . The program solves for  $\dot{p}$ ,  $\dot{q}$ , and  $\dot{r}$  at the beginning of each integration time step.

The accelerations of the sprung mass motions depend on the forces FSUM(I) and the moments TSUM(I). Each of those forces and moments will be discussed in the next sections.

### E.3 Forces on the Sprung Mass

There are several forces on the sprung mass. These forces are applied either through the suspensions or the fifth wheel (pintle hook). Consider first the suspension forces.

E.3.1 Suspension Forces. There are suspension forces in the x, y, and z directions. The force in the z direction is the most straightforward. For a single axle, the calculations are unchanged from Phase II [2], i.e., the force, SF, in the z direction is the deflection of the spring times the spring rate plus the force of coulomb and viscous friction. Some notes:

- 1) Tension is positive. Zero force is at static equilibrium. Thus the preload in the spring, which is the weight on that spring at static equilibrium, drops out of the calculations.
- 2) The springs may be made nonlinear by using a table lookup.
- 3) The coulomb friction break-point is set based on the masses, coulomb friction, and integration time step. Details of the theory are presented in [20].
- 4) Suspension force calculations take place in subroutine LINE.

For tandem axles, the SF use the same algorithms as the single axle. But, if braking occurs, suspension force is added to the lead axle and subtracted from the trailing axle according to the rule

$$SF(LEAD) = SF(LEAD) + FSHIFT*BTORQ/TD$$

$$SF(TRAIL) = SF(TRAIL) - FSHIFT*BTORQ/TD$$

where

BTORQ is the total brake torque of all four brakes on the tandem set, FSHIFT comes from the dynamic load transfer and TD is the fore-aft separation distance of the tandem axles.

The load transfer calculations are found in subroutine LINE.

The lateral and longitudinal suspension forces are also calculated using the Phase II [2] procedure. To explain briefly, the lateral forces at the suspensions may be viewed as constraint forces which hold sprung and unsprung masses together. To calculate these forces, the following procedure is used:

- 1) The sprung and unsprung masses are assumed to move as a unit with yawing but no rolling or pitching. Thus an estimated acceleration for the vehicle can be calculated using the entire mass and the known forces at the tire-road interface.
- 2) The unsprung mass acceleration is assumed to be a simple function of the gross acceleration calculated in (1). Then, since the yaw plane forces on the tires are known, the yaw plane constraint forces can be found.
- 3) These yaw plane constraint forces are applied to the sprung mass in the full blown equations of motion.

The user should note that the purpose of the method is to avoid dynamic coupling which requires matrix inversions each  $\Delta t$ . The height of the constraint point is the roll center height given as an input parameter. Finally, the accuracy of the method is quite good. (See [21] for details.)

E.3.2 The Forces at the Fifth Wheel. The T3DRS:V1 simulation, like Phase II [2], uses a spring-dashpot for the fifth wheel and pintle hook connection. Two advantages accrue:

- 1) removal of dynamic coupling
- 2) the ability to simulate roll compliance at the hitch.

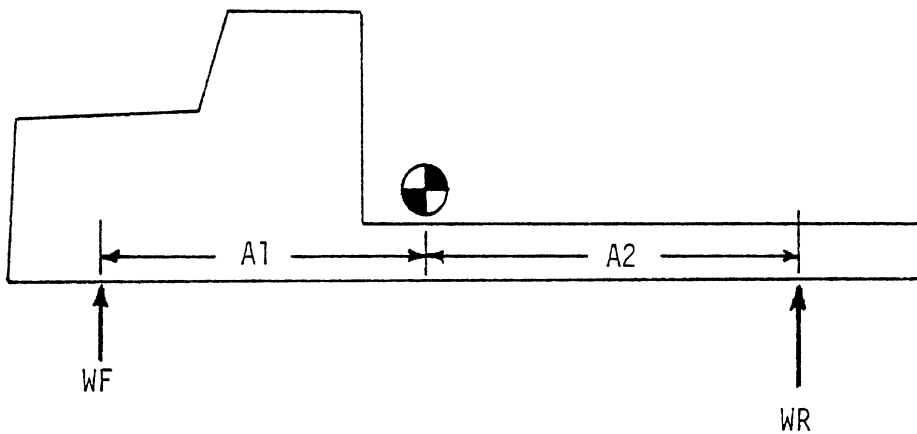
The method works as follows. At each integration time step the position of the tractor fifth wheel, a point located on the tractor, is calculated and the position of the trailer fifth wheel, a point on the trailer, is calculated. A force is assumed to act along the line between these points. The magnitude of the force is assumed to be a spring rate, PIN, times the distance between the points plus a damping rate, CFW, times the relative velocity between the points.

APPENDIX F  
PARAMETER ESTIMATION METHOD

This appendix describes simplified methods for estimating the mass moments of inertia for heavy vehicles with as little user time and energy as possible.

In the simulation program, the static loads on the tires are entered, along with the unsprung weights and the wheelbase. Note that the fore-aft mass center location is implicitly input by the user.

From this same data, one may find the total weight supported by the front and rear suspensions. Referring to these as WF and WR, and locating the mass center leads to the vehicle representation shown in the figure below.



Schematic diagram of sprung mass

It is obvious that for conventional vehicles one must expect the sprung mass pitch moment of inertia,  $I_{yy}$ , to be limited by

$$I_{yy} < \frac{1}{g}(WF \cdot A1^2 + WR \cdot A2^2) \quad (1)$$

Since one expects (at least in the unloaded condition)

$$A2 > A1 \quad (2)$$

we were led to try the formulation

$$I_{yy} = \frac{1}{g}([WF + a \cdot WR]A1^2 + WR(1-a)A2^2) \quad (3)$$

A comparison between empirical data and computed results has led to the conclusion that the value  $a = .4$  leads to reasonable pitch inertia values for unloaded vehicles. Furthermore, even in the case of loaded vehicles, Equation (3) leads to very reasonable results.

Given the pitch inertia from Equation (3), empirical data has shown it reasonable to assume that the sprung mass yaw moment of inertia,  $I_{zz}$ , is equal to the pitch inertia, and the roll inertia may be related to the pitch and yaw inertias by a multiple of the vehicle dimensions. In particular

$$I_{zz} = I_{yy} \quad (4)$$

$$I_{xx} = 2 \left[ \frac{(\text{TRACK})}{(\text{Total Length})} \right]^2 I_{yy} \quad (5)$$

## APPENDIX G

### PATH-FOLLOWER, CLOSED-LOOP DRIVER MODEL

Section 3.2 of the Users Manual explains the input requirements for the closed-loop driver model. This appendix will outline the manner in which the model works and demonstrate its use in simulating a closed-loop double lane-change maneuver with a tractor-trailer.

The driver model is based on a technique, discussed more completely in Reference [19], which selects a steering control at each point in time by minimizing the current preview error (squared error). Referring to Figure G-1, the solid line shows the desired path trajectory input by the program user (table values), and the dashed line the estimated trajectory of the vehicle using the current steering control. The preview interval (user input), over which the path estimates are made, extends from the current vehicle position, time  $t$ , to the end of the interval, time  $t + T$ . This interval is divided into ten equal parts and position errors,  $\epsilon_i$ , between the desired and estimated trajectories are calculated for each. The current steering control is then selected to minimize the sum of the squares,

$$\sum_{i=1}^{10} \epsilon_i^2 .$$

Estimates of the vehicle position over the preview interval ( $t$ ,  $t+T$ ) are obtained from an internal linear model representation of the truck/tractor vehicle.

#### Example Usage

The following discussion demonstrates the use of the driver model in simulating a closed-loop double lane-change maneuver measured on an actual tractor-trailer. The input data describing the experimentally measured vehicle path, and the necessary driver model parameters are shown in Table G-1. The format corresponds to the requirements discussed in the Users Manual, Section 3.2.





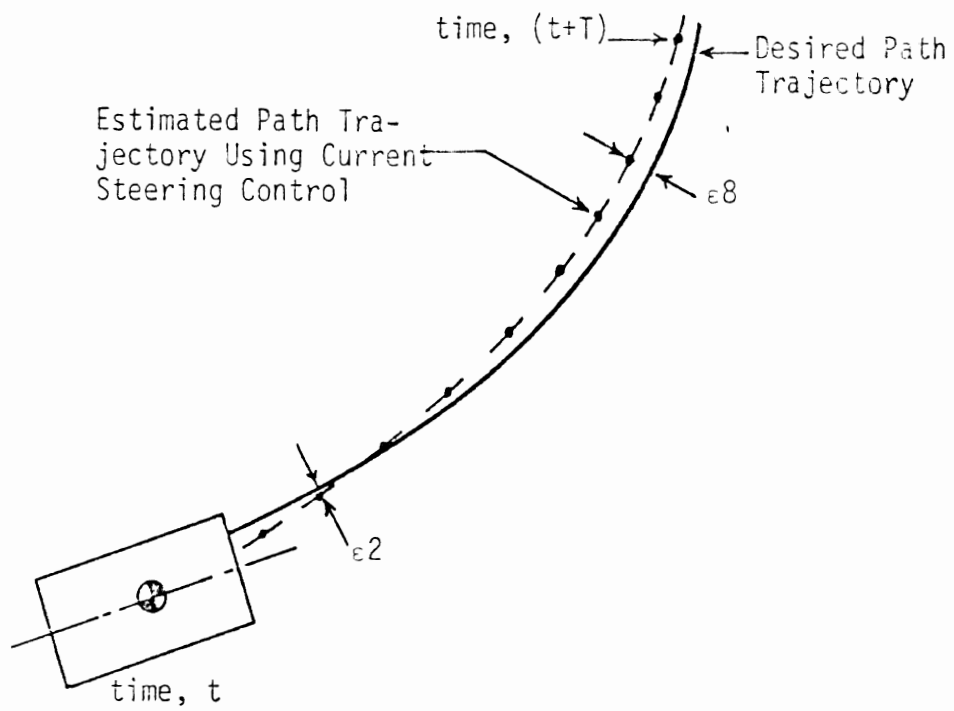


Figure G.1. Closed-loop steering model.



Table G-1

-16		} Closed-loop key (- sign) 16 points in path table.
0.0	0.0	} x-y path table
70.0	0.0	
85.0	-1.0	
100.0	-4.2	
115.0	-6.7	
130.0	-9.0	
145.0	-10.7	
160.0	-11.3	
175.0	-11.3	
190.0	-10.3	
205.0	-8.7	
220.0	-6.2	
235.0	-3.3	
250.0	-1.3	
265.0	0.0	
900.0	0.0	
0.0		} Transport lag
1.10		} Preview interval

The two driver model parameters following the path table input are the driver transport lag and the preview interval parameter,  $T$ , discussed above. In this example, the driver transport lag was selected as zero and the preview interval parameter value varied to find the best match between simulated and measured responses for the maneuver.

Simulation results for this data set are shown in Figure G-2, along with corresponding measured vehicle responses. The first time history is tractor lateral acceleration (simulated and measured), followed by tractor yaw rate and front-wheel steering angle. Excellent agreement between the simulated and measured responses is demonstrated in Figure G-2 even though estimates of tire cornering stiffness had to be used in this case.

Very similar responses can be obtained for non-zero driver transport lags (more accurate representations of human operator limitations) by increasing the value of the preview interval parameter. For example, a transport lag of 0.25 seconds would require an increase of the preview interval parameter value from 1.1 to about 1.5 in order to obtain responses similar to those shown in Figure G-2. The principal effect would be somewhat decreased damping in each of the simulated time histories responses.

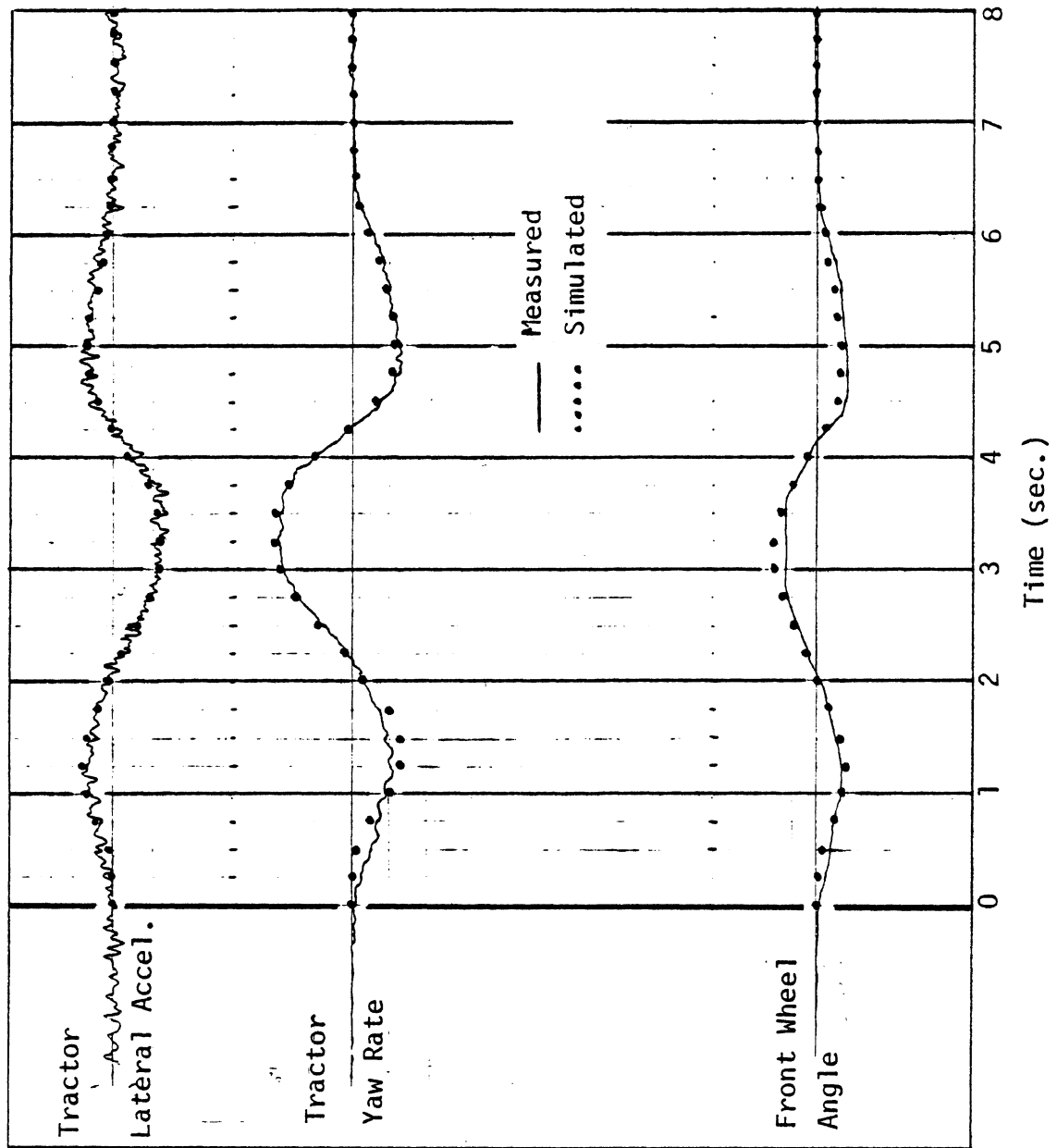


Figure 6.2. Path-follower replication of an actual maneuver.



## APPENDIX H

### USER-WRITTEN ROAD SUBROUTINE

Entry of a negative value for the road key, IROAD, referred to in Section 3.2 of the Users Manual, allows the program user to define an alternate road surface for use in the simulation. By entering code (e.g., FORTRAN) in SUBROUTINE ROAD, which calculates the road elevations, Z, at each wheel as a function of X and Y inertial coordinates, the user is free to define nearly any road surface desired. The only restrictions are that (1) the complete vehicle train starts from a flat or horizontal surface and (2) all gradients (cross-slopes, downgrades) encountered by the vehicle train during the simulation remain less than about 0.10 (rise/run).

The vehicle train is assumed to start at time zero pointing in a straight line along the X inertial coordinate axis as shown in Figure H-1. Since the vehicle train starts from a flat horizontal plane, the code defining the road surface must guarantee that the road surface elevation is zero for negative values of the inertial X-coordinate.

The user-written subroutine (SUBROUTINE ROAD) must use the following FORTRAN format (or alternate equivalent):

```
SUBROUTINE ROAD(X,Y,Z,T)
```

```
Codes for the calculation of road elevation, Z  
(in feet) as a function of X, Y (in feet) inertial  
coordinates—supplied by the main calling program.
```

```
RETURN
```

```
ENTRY ROADDZ(X,Y,DZDX,DZDY)
```

```
Code for the calculation of road gradients  
dz/dx(DZDX) and dz/dy(DZDY) consistent with the  
elevation definition above.
```

```
RETURN
```

```
END
```

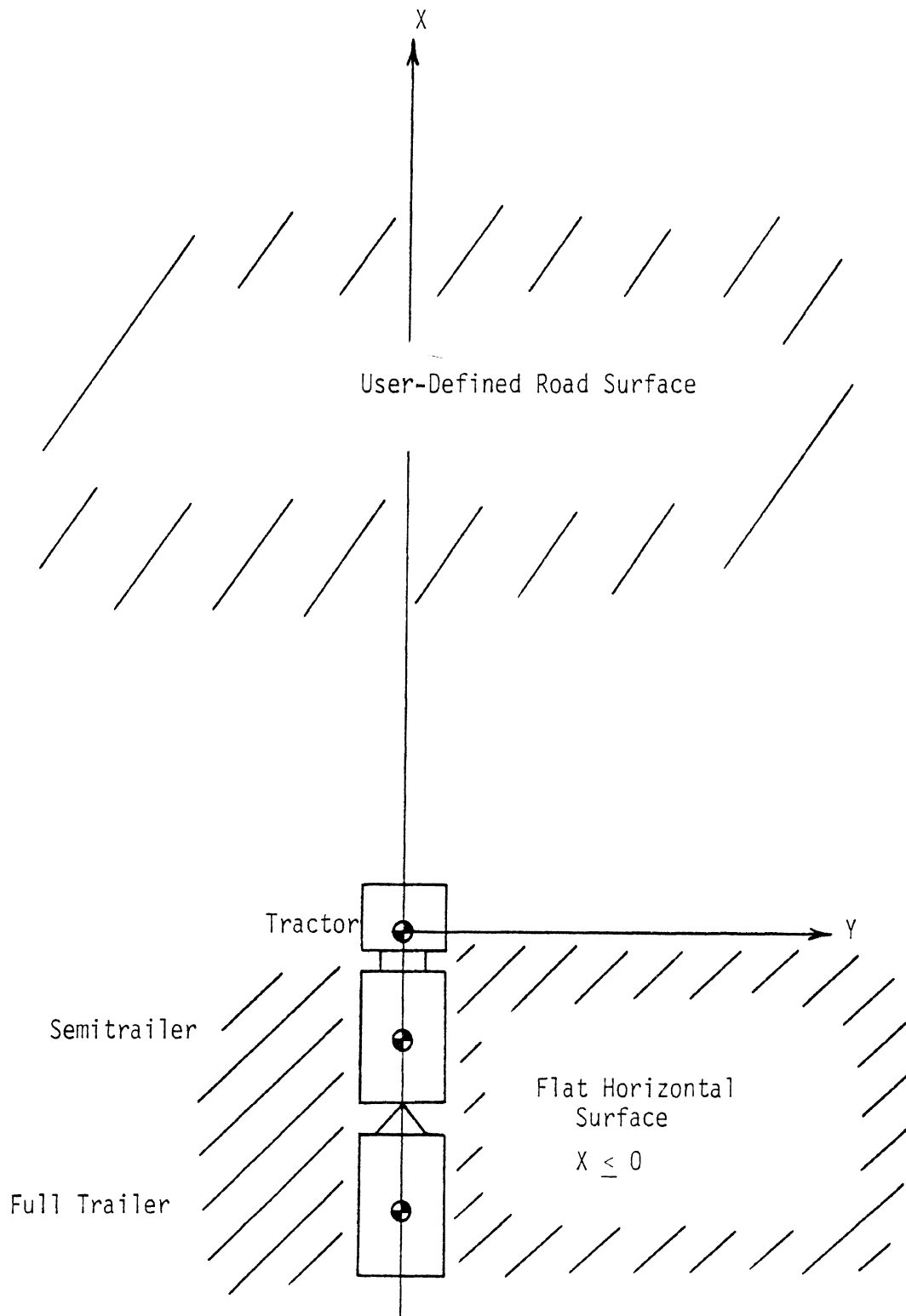


Figure H-1. Vehicle position at zero time.



The argument list for SUBROUTINE ROAD is defined as

- X forward inertial coordinate of the wheel, supplied by the calling program
- Y lateral inertial coordinate of the wheel, supplied by the calling program
- Z vertical road elevation (in feet) calculated by the user code using X and Y—returned to the calling program
- T simulation time supplied by the calling program for possible use in the subroutine calculations.

The argument list for ENTRY ROADDZ is:

- X same as above
- Y same as above
- DZDX user-calculated gradient ( $dz/dx$ ) of the road surface along the X inertial coordinate direction
- DZDY user-calculated gradient ( $dz/dy$ ) of the road surface along the Y inertial coordinate direction.

The DZDX and DZDY calculations should be consistent with the definition of  $Z = f(X,Y)$ . For example, if  $Z = X^2Y + Y^2$  in ROAD,

$$\begin{aligned}DZDX &= 2XY \\DZDY &= X^2 + 2Y\end{aligned}$$

should be calculated in ROADDZ. The derivatives are used to establish the yaw plane coordinate system in the simulation procedure. In the case of a rough, but essentially horizontal road, the derivatives may be arbitrarily set to zero.

#### Example Road

The following code should be used to describe a super-elevated, 500-foot circular roadway (cone): The roadway is horizontal for values of  $X \leq 0$ . The super-elevation, E, is increased linearly between  $X=0$

and  $X=200$  to a maximum value of 0.08. For values of  $X > 200$ , the super-elevation is fixed at 0.08 (Figure H-2).  $R$  is the actual radius (calculated) of the  $(X,Y)$  point supplied by the calling program.

```
SUBROUTINE ROAD(X,Y,Z,T)
R = SQRT(X**2 + (Y+500)**2)
E = 0.08 * X/200.
IF(X.GT. 200.) E = 0.08
IF(X.LT. 0.) E = 0.0
Z = E * (500-R)
RETURN
ENTRY ROADDZ(X,Y,DZDX,DZDY)
DZDX = - E * X/R
DZDY = - E * (Y+500)/R
RETURN
END
```

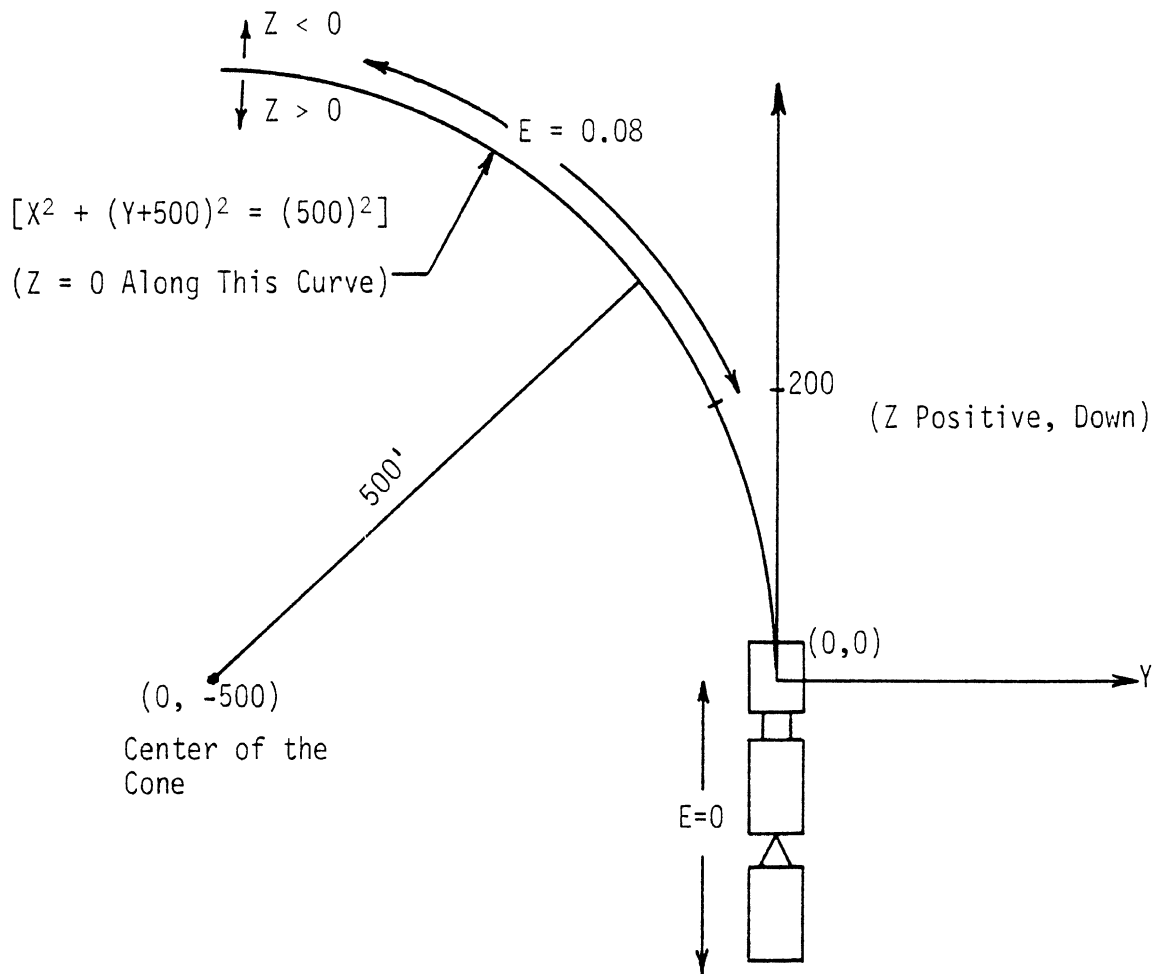


Figure H-2. Circular super-elevated roadway example.

