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EFFECTS OF TIRE PROPERTIES ON TRUCK AND BUS HANDLING APPENDICES D, E, F, G

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Final Report

June 1976

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Highway Safety Research Institute The University of Michigan

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16. Abstract				
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differences in the qualit	ative perform	ance charact	eristics of tru	uck tires
relative to passenger car	tires, and t	he manner in	which these ur	nique truck
tire properties may affec	t the yaw sta	bility of the	e commercial ve	ehicle.
Potential problems of veh	icle stabilit	y were drama	tically illust	rated by a
rollover incident which o	ccurred durin	g testing of	a heavy truck.	•
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APPENDIX D

VEHICLE TEST PROCEDURES

D.1 Introduction

The following sections of Appendix D provide specific, quantitative descriptions of the test procedures called for in Table D-1. This table indicates the tests which were conducted, indicating the specific vehicles and test conditions. The shaded area indicates those tests which were planned, but which were not completed due to the rollover incident discussed in Appendi¥ F. The specific steer angles indicated were obtained by simplified analyses using vehicle and tire parameters available prior to testing. As a result of test experience, certain of these values were altered. In general, steer angles were chosen to make an orderly approach to maximum lateral accelerations of .5 g on the dry asphalt surface and .3 g on the wet asphalt surface.

D.2 Straight-Line Braking

D.2.1 <u>Effectiveness Testing Procedures</u>. With cold brakes (i.e., less than 200°F) and the vehicle traveling in a straight line at the initial velocity of 40 mph, the clutch was depressed and the brake pedal displaced in a quasi-step manner to a predetermined level. This level of pedal displacement and a steering wheel angle of zero was maintained until the vehicle stopped.

Brake system input for hydraulically-braked vehicles was recorded in terms of brake pedal force. For air-braked vehicles, brake system input was recorded as brake line pressure at the output of the treadle valve.

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Table D-1. Detailed Vehicle Test Matrix

	s	Ext.	• 10 /		Ϋ́	Š	X	X	X				×		
	Bu	üC	710	¥.	X	¥	X	X	×			X	X	<u>H</u>	
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nber o	ck-Up 1	Ext. Var.			×	×	×	×	×	£		×	×	×	
INN	Ρi	OE	;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;	X	Х	×	Х	×	Х		×	Х	Х	Х	
		rface	- Accb - 1 +	y Aspnalt	t Asphalt	t Asphalt	y Asphalt								
		on Su			We	We	Dr	Dr	Dr	Dr	Dr	Dr	Dr)	Dr)	Dr)
	Condition	Load Configuratio	L	Empry	Empty	Empty	Empty	Empty	Empty	Empty	Loaded	Loaded	Loaded	Loaded	Loaded
	Test	Test* Procedure	-	-	2	3	2	'n,	4	S	1	2	£	4	S
		Test No.	-	-	2	м	4	S	9	2	∞	6	10	11	12

*Numbers refer to test procedures as follows:

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Straight-Line Braking
Braking-in-a-Turn

Sinusoidal Steer
Trapezoidal Steer (conducted with increasing severity)
Trapezoidal Steer (conducted with decreasing severity)

Trapezoidal Steer (conducted with decreasing severity)

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Deleted as a result of rollover incident.

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Within the limits of vehicle stability and safe test practice, tests were conducted at a minimum of five levels of brake system input corresponding to 20, 40, 60, 80, and 100% of the input required for the occurrence of first wheel lockup. One repeat test of each input level was conducted.

D.2.2 <u>Front-Only and Rear-Only Braking Tests</u>. For frontonly tests, brakes on the vehicle's rear axle were disabled. For rear-only tests, brakes on the vehicle's front axle were disabled.

Tests were conducted identically to those described in Section D.2.1, save the following exceptions:

- 1) Initial velocity was 28 mph.
- 2) There were only four runs, two with front brakes only and two with rear brakes only. In all runs, brake system input was 50% of the level required for first wheel lockup (as determined by the effectiveness test of the vehicle in its corresponding load configuration).

D.3 Trapezoidal Steer

With the vehicle traveling in a straight line at the designated initial velocity, a trapezoidal (or quasi-step) steer angle, of the form indicated in Figure D-1, was input to the vehicle via the Automatic Vehicle Controller.

Each trapezoidal steer test called for in Table D-1 implied a full series of trapezoidal steer tests conducted at both 30 and 50 mph. Test procedure number 4, Trapezoidal Steer (conducted with increasing severity), also included quasi-step steer tests at both 30 and 50 mph.



Figure D-1

Table D-2 lists the specific parameters describing the input steer angle wave forms used in each vehicle/test surface configuration called for in Table D-1. Tests conducted at the lower steer angle levels were all done with one polarity of turn.

D.4 Braking In A Turn

The braking-in-a-turn test was conducted in a manner similar to the trapezoidal steer test with the addition of constant level braking introduced during the turn. The vehicle input wave forms are illustrated in Figure D-2.

Table D-3 indicates the specific input levels used in testing. Tests were conducted beginning with low levels of braking and progressing to higher levels. Upon the occurrence of first wheel lock, the test series was terminated, i.e., no higher level of braking was employed.

As was the case in trapezoidal steer, successive runs were conducted in one polarity with the highest level test conducted in both directions and with one repeat run in both directions.

Table D-2

÷ .

	T5-T4	1 sec	l sec	l sec	1 sec	
	$T_4 - T_1$	5 sec	5 sec	5 sec	5 sec	
	τ ₁ -τ ₀	min*	min.	l sec	l sec	
	To		>l sec			
Steer Angle, es)	Intercity Bus	Ø	3	6,8,10,12,14	2,3,4,5	
Average Front Wheel δ_{v} (degre	Truck, Van, Pickup	4	1.5	3,4,5,6,7	1,1.5,2,2.5	
	Initial Velocity, mph	30	50	30	50	
	Test Type	Step Steer	Step Steer	Trapezoidal Steer	Trapezoidal Steer	

*For step steer tests, the minimum possible value of T_1 - T_0 , as determined by the maximum $\hat{\delta}_w$ which the AVC can produce, will be used.



Figure D-2

Surface	Initial Velocity, mph	Steer Angle, $\hat{\delta}_w$	Brake Level, $\hat{\delta}_{b}$ (%)*	т _о	^T 1 ^{-T} o	T * * * ² *	T ₃	^T 4 ^{-T} 1	^T 5 ^{-T} 4
Wet Asphalt	30	**	20,30,40,50	<u>></u> 1 sec	l sec	2.5 sec	= T ₅	5 sec	l sec
Dry Asphalt	50	* * *	40,50,60,70						

*Brake input levels are expressed as a percentage of the level required to produce wheel lock during effectiveness testing on the dry surface of the same vehicle in the same load condition.

✓ **Equivalent to a .2 g steady-state turn.

*******Equivalent to a .35 g steady-state turn.

****In the earliest testing, T₂ was set equal to T₁, but was later altered to allow full development of Steady-state turn.

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Table D-3

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D.5 Sinusoidal Steer

With the vehicle traveling in a straight line at the prescribed initial velocity, a steer angle of the form shown in Figure D-3 was input to the vehicle. Table D-4 lists the values of the various input parameters used. As the table indicates, tests were run at 30 mph on the wet surface and 30 and 50 mph on the dry surface. As in the other handling tests described, lower level runs were made with one polarity of turn. The highest level tests were then conducted in both directions and with repeat runs. In the case of the sinusoidal steer tests, the highest level runs for both values of T were conducted in this manner.



Table D-4

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Average Front Wheel

Surface	Initial Velocity	Period T, s	ec.	Steer Angle Truck, Van	δ _w , deg.	
Surrace	mpn	neavy venicie	Light venicie	TICKUP	<u></u>	
Wet Asphalt	30	2,4	2,3	2,3,4	4,6,8	
Dry Asphalt	30	2,4	2,3	2,4,6	4,8,12	
Dry Asphalt	50	2,4	2,3	1,2,3	2,4,6	

1



APPENDIX E

DATA FROM FULL-SCALE VEHICLE TESTS

Data plots are provided covering the steering test results obtained on the three test vehicles: van, pickup, and heavy truck. Tabular data follow, covering all tests conducted on all three vehicles in the program.

E.1 Ford Econoline Van Trapezoidal and Sinusoidal Steer Test

Data labeled "OE" refer to the installation of code L-2 tires at all four wheel positions (where tire codes are identified on the attached copy of Table 3.1 from the Technical Discussion). Data labeled extreme variation, "EV," represent the installation of code L-2 tires on the front axle and code L-11 tires on the rear.

TABLE 3.1. FLAT-BED TEST TIRES

	Tire No. Heavy Truck	Manufacturer	Mode 1	<u>Size</u>
	Tires		• • •	
	H-1	Uniroyal	Triple Tread	10 x 20F
	N-2	Uniroyal	Triple Tread	10 x 20G
•	H-3	Uniroyal	Triple Tread	11 x 22.5F
	· H-4	B.F. Goodrich	Milesaver Radial Steel H.D.R.	10 R 20 G
	H-5	B.F. Goodrich	Milesaver Radial Steel H.D.B.	10 R 20 G
	H-6	Goodyear	Unisteel R-1	10 R 20 G
	H-7	Goodyear	Unisteel L-1	10 R 20 G
	H-8	Firestone	Power Drive	10 x 20F
	H-9	Uniroyal	Unimaster Rib	15 x 22.5H
	H-10	Michelin	Radial	10 R 20 G
	H-11	Uniroyal	Fleetmaster - Superlug	10 x 20F
	Heavy Bus Tires			
	H-12	Firestone	Hiway Mileage	12.5 x 22.5G
	H-13	B.F. Goodrich	Intercity Mileage	12.5 x 22.5G
	H-14	B.F. Goodrich	Intercity Mileage	11.5 x 20G
	H-15	Uniroyal	Intercity	12.5 x 22.5G
· .	H-16	Uniroyal	MaxRoute I	11.00 R 20H
	H-17	Goodyear	Custom Cruiser	12.5 x 22.5G
	H-18	Michelin	Radial XZA	11-R 20 H
	H-19	Michelin	Radial XZA	11 R 22.5 H
	H-20	Michelin	Radial XZA	12 R 22.5H
	Light Truck Tires			۶
	L-1	Firestone	Transport 500	8.00 x 16.5D
	L-2	Goodyear	Custom HiMiler	8.75 x 16.5E
	L-3	Goodyear	Rib HiMiler	8.00 x 16.5D
	L-4	Firestone	Transport 110	7.50 x 16.5C
	L-5	Goodyear	Super Single HiMiler	10.00 x 16.5E
	L-6	Firestone	Town & Country Truck	8.00 x 16.5D
	L-7	Goodyear	Custom Flexsteel	8.00 R 16.5E
	L-8	Goodrich	Milesaver Radial	8.00 R 16.5D
	L-9	Goodyear	Glas Guard XG	8.00 x 16.5D
	L-10	Goodyear	Glas Guard XG	8.75 x 16.5E
	L-11	Firestone	Town & Country Truck	8.75 x 16.5E
	L-12	Goodyear	Custom Flexsteel	8.75 R 16.5E
	L-13	Michelin	Radial XCA	8.00 R 16.5E
	L-14	Wards	Steel Belted Super Wide	9.50 x 16.5D
	L-15	Michelin	Radial XCA	8.75 R 16.5D
	L-16	General	Jumbo Power Jet	8.00 x 16.5D
	L-17	General	Jumbo Power Jet	8.75 x 16.5E
	L-18	Goodycar	Glas Guard	8.00 x 16.5D
	L-19	Goodyear	Glas Guard	8.75 x 16.5E
	L-20	Goodyear	Rib HiMiler	8.75 x 16.5E
			14	

12

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dry concrete, $\tau = 2$ sec.







Figure E.14. Light van: loaded OE, sinusoidal steer runs at 30 mph, dry concrete, $\tau = 3$ sec.





Figure E.16. Light van: loaded OE, sinusoidal steer runs at 50 mph, dry concrete, = 3 sec.















Figure E.20. Light van: loaded EV, sinusoidal steer runs at 50 mph, dry concrete, $\tau = 3$ sec.
E.2	Test Results -	Ford F-250 Pickup	Truck - Trapezoidal and
	Sinusoidal Stee	r Test Results	

Test conditions are identified by the following codes:

	Tire code no.'s ref in the text (pg. 24	fer to Table 3.1 })
Test Code	Front Tires	Rear Tires
OE	Ll (bias-rib)	Ll (bias-rib)
TC 13	L13 (radial-rib)	Ll3 (radial-rib)
TC 14	L16 (bias-rib)	L16 (bias-rib)
TC 15	Ll (bias-rib)	L9 (bias-lug/snow)













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5. Start









dry asphalt.

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E.3 White Road Boss Heavy Truck Trapezoidal Steer Results

1

Data describing the trapezoidal steer numerics for the baseline truck equipped with code H1 tires at all six wheel positions.









E.4 Tabular Presentation of Vehicle Test Data

Tables indicate the following test conditions and response measures:

- 1) Loaded/unloaded state
- 2) Maneuver type, coded as follows

<u>Code No.</u>	Maneuver
1	Straight-line braking
2	Braking in a turn
3	Sinusoidal steer
4a	Trapezoidal steer, step-fronted input
4b	Trapezoidal steer, ramp-fronted input

- 3) Test velocity (mph)
- 4) Steering wheel displacement amplitude (deg)
- 5) Period of sinusoidal steering inputs
- 6) Brake input level (% of input level needed to lock all wheels on any one axle)
- 7) A_x, average value of longitudinal acceleration ave during a braking test (g's).
- A, peak value of lateral acceleration (g's).
 y_{peak} (In sinusoidal steer experiments, the peak values achieved at both polarities of accelerations.)
- 9) r_{peak}, peak value of yaw rate (deg/sec). (In sinusoidal steer, both polarity peaks are listed.)
- 10) T_{inf}, the time (seconds) at which the lateral acceleration time history crosses back through zero-measured with respect to initiation of steering—in a sinusoidal steer maneuver.

Data presented for the light van and heavy truck indicate the installed tires by model and size. Pickup truck tests are identified by a code indicating tire installations as shown below.

Test Code	Front Tires	<u>Rear Tires</u>
TC-12	LI	LI
TC-13	L13	L13
TC-14	L16	L16
TC-15	LI	L9

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		VEF	RUN	NO.		4 - 08	4 - 09	4-10	1 - 1	5-05	5-06	5-27	5-08	5-26	5-10	5-11	5-12	610	5-14	5-15	5-16	5-17	
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· . •	1	NSH-I.	00-1	TVE	HICLE	HAND	DLING	DATA SI	JAMAR		SHEET 4	11 10	
VE	HICLE V	NK		TIRES	SI FRONT	GOODYER	CUSTON	TIRE	S, REAR:	CODYEAR	2,15,70M	- 1E	
RUN	LOADED	MANEU-	>	NSO	STEER	BRAKE	A×	Aγ	5	TINE.		• -	
NO	YES/NO	VER TYRE	HdW	DEG.	PERIOD	INPUT	AVERAGE	PEAK	PEAK	SEC.	•		. :
	• • • • • • •	NO.	 	• • • •	SEC.	%	g's	3'5	°/sec	• •	•	• •	<u> </u>
5-18	NO	ŝ	05	324		• • • • • •	.07	L.10/E.57	13/22	11		4.	1
5-19	0N	m	20	64L	Ũ		, o ,	L.25/K.17	1-1/1/6	1.1	• · ·		
2:20	0N	M	6	796	ୌ		Ö.	52.2/56.7	1 13/210	1.2	,		
5-21	NO	M	\mathcal{E}	796	2		0 U	L.35/R.15	L 12/2 10	/, 3			•
5-22	07	M	50	96 R	2	•	20	R.27/1.55	R10/412	1.1	¥	• •	
5-23	02	M.	50	36 K	ন		-0.	R.25/6.35	210/212	1.2		· ,	
5-24	N N	M	50	375	m		Z0.	21/5/6.08	L 4/22	1.5		• .	
5-25	Ċ.	M	50	709	M			02.3/02.7	29/2G	1.5		•••	
5-26	0N	M	Q	796	m			L42/R.36	L12/29	1.0		ţ,	
5-27	0	<u>N</u>	Q.?	796	M		20.	2,40/1.30	L 12/210	1.8	· •	• •	
5-28	20	M	0 	296	M		-0-	04.30/140	X.10/6.12	1.7	, .	• ;	
5-26	0N	Μ.	2	20 5	M		A. O.	N. 30/1.40	R10/412	1.7			•
6-05	0 Z	4 9	<u>[17]</u>	1281		1	~	cd æ	R		•		
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10-9	0N	5		128	<u> </u>		20.	2.)		• ·		
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0-9	C ~	3	0. Di	787			Ĉ Ŵ	2 2 2	Ø			i i	
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TING	SEC.	•••											I		 \ 	I	<u> </u>		. :	: • • •
۲. ۲.	PEAK	o/sec	0	4	4	0	4	18	61	22	21	21	22	4	-0	-00-	01	0	0	•
ΑΥ	PEAK	9'5	.25	0/2	./5	25	30	.40	45	53	53	.45	48	./5	e E	м О С	, 37	.37	C.E.	
A×	AVERAGE	g's	50.	10.	N.	.05	50.	.07	70,	.06	• 06	.0.	50	0.1	.07	10,	6.0	·	ω O	. 7
BRAKE	INPUT	%	· · · ·		1	ł	N		- 1	1		1		1	1			1	1	
STEER	PERIOD	SEC.]	1	· · · · ·			1	1		1	1	· 1 :	1			I	
Ssw	DEG.	· · · · · ·	484	400	C) (2) (2)	796	7007	1602	16.21	2242	27.11	224R	224K	324	484	644	<u>ا د</u>	<u></u>	N.	
>	HdW		50	Ś	00	<u>.</u>	- <u>C</u> -	0 M	0 M	0 M	00	57 0	\widetilde{O}	- Q . D	5	95	0	Ð	0	
MANEU-	VER TYPE	NO.	4 2	40	4 2	4	4	4.6	46	46	46	46	4.6	46	46	4	\$ ++	2	46	
LOADED	YES/NO	- +	Ň	NO NO	0N	DN.	<u>No</u>	<u>o</u> N	ON	NO	ON	<u>on</u>	NO.	Q Z	NO V	DN	NO	СŅ	0N	
RUN	No.		6 - 10	11-9	2/-9	2-13	6-14	6 -15	91-9	2-17	6 - 18	6-19	6-70	12-9	6-22	6 -23	6-25	6.20	6 - 27	
	RUN LOADED MANEU- V SSW STEER BRAVE Ax AY T TINE	RUN LOADED MANEU- V SEER BRANE Ax AY T TINF. NO. YES/NO VER TYPE MPH DEG. PERIOD INPUT AVERAGE PEAK PEAK SEC.	RUN LOADED MANEU- V SSW STEER BRANE Ax AY T TINE. NO. YES/NO VER TYRE MPH DEG. PERIOD INPUT AVERAGE PEAK PEAK SEC. NO. Ves/NO. VES. 29'S 9'S 9'S 9'S 0'SEC.	RUN LOADED MANEU- V δ sw steer Brake Ax AY Γ Tine. No. Yes/No Vertype MPH deg. Period INPUT Average peak peak sec. No. 48 , 50 48 , -1 -1 05 2 , 25 6 -1	RUNLOADEDMANEU-V6swSteerBRAKEAxAYrTine.NO.YES/NOVER TYPEMPHDEG.PERIODINPUITAVERAGEPEAKSEC.NO.YES/NOVESYPEPERIODINPUITAVERAGEPEAKSEC.6-10NO4a50484052566-11NO4a5048405256-	RUN LOADED MANEU- V δ_{sw} steer BRAVE Ax AY Γ Tine. No. Yes/No ver type MPH deg. Period Input Average peak peak sec. No. 43 50 434	RUN LOADED MANEU- V δ sw steer BRAKE Ax AY Γ Tine. No. Yes/No Ver tyre MPH deg. Period induit Average Peak reak sec. $\delta -10$ No. $4a$ 50 494	RUN LOADED MANEU- V 6sw STEER BRAWE Ax AY Γ Tine. No. Yes/No Ver Type MPH deg. Period Input Average peak peak sec. 6-10 No. $4a$ 50 494 $.05$ 3's 9's 0'sec 6-11 No. $4a$ 50 494 $.05$ 3's 9's 0'sec 6-11 No 4a 50 486 $.05$ 25 6 $.05$ 25 6 $.05$ 25 6 $.05$ 25 6 $.05$ 25 6 $.05$ 25 6 $.05$ 25 6 $.05$ 25 6 $.05$ 25 6 $.05$ 25 6 $.05$ 25 6 $.05$ 25 6 $.05$ 25 6 $.05$ 25 6 $.05$ 25 6 $.05$ 25 6 $.05$ 25 6 $.05$ 25 6 $.05$ 25 6 $.05$ 25 6 $.05$ 25 6 $.05$ 25 6 $.05$ 25 6 $.05$ 25 $ 100$ $.05$ 25 $ 100$ $.05$ 25 $ 100$ $.05$ 25 $ 100$ $.05$ 25 $ 100$ $.05$ 25 $ 100$ $.05$ 25 $ 100$ $.05$ 25 $ 100$ $.05$ 25 $ 100$ $.05$ 25 $ 100$ $ -$	RUN LOADED MANEU- V 65W STEER BRAWE AX AY Γ Tine. NO. YES/NO VER TYRE MPH DEG. PERIOD INPUT AVERAGE PEAK PEAK SEC. 6-10 NO. 42 50 434 $-$ 50 434 $-$ 50 56 6-10 NO. 42 50 436 $-$ 50 436 $-$ 50 436 $-$ 50 44 $-$ 50 45 $-$ 50 7 50 $-$ 50 $-$ 50 7 50 $-$ 5	RUN LOADED MANEW- V δ_{sw} STEER BRAWE Ax AY T TINE NO. YES/NO VER TYPE MPH DEG. PERIOD INDUIT AVERAGE PEAK SEC. No. NO. YES/NO VER MPH DEG. PERIOD INDUIT AVERAGE PEAK SEC. No. SEC. No. SEC. No. SEC. No. SEC. No. SEC. No. SEC. SEC. No. SEC. SEC. No. SEC. No. SEC. No. SEC. No. SEC. No. SEC. No. SEC. SC. No.	RUN Loadded Maneu- V 6sw Steer Brance A T Time NO. Yes/NO VER TYPE MPH Deg. Period INPUIT Average Peak Sec. No NO. Yes/NO VER TYPE MPH Deg. Period INPUIT Average Peak Sec. Sec.	RUN LOADED MANEU: V δ_{sw} STEER BRAME A T TINE. NO. VES/NO VES/NO VER MPH DEG. PERIOD INPUT AVEORGE PEAK SEC. δ_{s} $g's$ $g's$ $g's$ $g's$ $c's$	RUN Loaded manueut V 6sw eteere Brane A T Time NO. Yes/No Vertype MPH De6. Period INDUT MPH Sec. % 9's 9's Sec. % NO. Yes/No Verype MPH De6. Period INDUT A T Time 6-10 NO 4a 50 484 =	RUN LOADED MANEU: V 6 sw steer BRAWE Ax A T Time NO. Yes/NO VER TYRE MPH DE6. PERIOD INPUT AY T Time NO. Yes/NO VER TYRE MPH DE6. PERIOD INPUT AY T Time 6-10 NO 4a 50 484 - .05 484 sec. 25 9's 9's 0'sec 8's 0'sec 1's - .07 1'5 4 - - .07 1'5 4 - - .05 $3'sec$ 1'5 4 - - .07 1'5 4 - - .05 $3'sec$ 1'5 4'5 1'7 1'7 1'5 1'7 - .05 $3'sec$ 1'7 - .07 $1'7$ 1'5 1'7 - - .07 $1'7$ 1'7 1'7 1'7 1'7 1'7 1'7 1'7 1'7 <t< th=""><th>RUN LOADED MANEL: V δ_{SWVE} STEER BRAWE Ax Ay T TINE. NO. VES/NO VER TYRE MPH DEG. PERIOD INPLIT AVERAME Ax Ay T TINE. $6-10$ NO. $4a$ 50 434 $5c$ $3'$ $9'$ $sec.$ $6-10$ NO. $4a$ 50 434 -20 434 $sec.$ $8'$ $9'$ $sec.$ $6-11$ NO $4a$ 50 434 -70 436 -7 $1/5$ 4 -7 $6-13$ NO $4a$ 50 436 -7 $1/5$ 4 -7 $6-13$ NO $4a$ 50 436 -7 $1/5$ 4 -7 $6-14$ NO $4d$ 50 490 18 -7 167 167 167 167 167 167 167 167</th><th>RUN LOADED MANUL: V Saw STERR BRAUE Ar T TINE NO. VES/NO VER TYPE MPH DEG. PERIOD NPUT Av A T TINE NO. VES/NO VER TYPE MPH DEG. PERIOD NPUT Av A T TINE 6-10 NO FEM DEG. % 9'S 0'SEC % 0'SEC SEC. % 9'S 0'SEC SEC. % 0'SEC % 0'SEC 5'S 6'S 1'S <t< th=""><th>RUN Loadded Maneur V δ_{sw} steek Brance A T Time NO. Yes/No Ver TYR MPH Des. PERIOD INDUT Auespace Peak FERIOD INDUT Auespace Peak Sec. δ_{s} $g's$ <t< th=""><th>RUN LUMDED MANELL V 6 sun steeler Ranket A T Tink NO. YES/NO VER TYRE MPH DEG. PERIOD INPUT AVERAGE PEAK PEAK PEAK SEC. X 9's 9's sec. K 1'n $6-10$ NO $4a$ J's $3's$ 9's $3'sec$ Sec. $3's$ $9's$ sec <</th><th>RUN Londed Maneul: V δ_{sw} GTERR BRAUE Ar T Time, NO. YES/NO VER TYRE MPH DEG. PERIOD INDUIT AVERAGE PERIOD INDUIT AVERAGE PERIOD NO. 6-10 NO. 4 SEC. % 9'S 9'S SEC. SEC. % 9'S SEC. SEC. SEC. % 9'S 9'S SEC. SEC.</th><th>RUN LOADED MANEL! V δ_{SW} STEER BRAUE Ay T TINE. NO. YES/NO VER TYRE MPH DEG. PERIOD INPUT Avecage DEAK SEC. χ_{S} $g's$ $g's$</th></t<></th></t<></th></t<>	RUN LOADED MANEL: V δ_{SWVE} STEER BRAWE Ax Ay T TINE. NO. VES/NO VER TYRE MPH DEG. PERIOD INPLIT AVERAME Ax Ay T TINE. $6-10$ NO. $4a$ 50 434 $5c$ $3'$ $9'$ $sec.$ $6-10$ NO. $4a$ 50 434 -20 434 $sec.$ $8'$ $9'$ $sec.$ $6-11$ NO $4a$ 50 434 -70 436 -7 $1/5$ 4 -7 $6-13$ NO $4a$ 50 436 -7 $1/5$ 4 -7 $6-13$ NO $4a$ 50 436 -7 $1/5$ 4 -7 $6-14$ NO $4d$ 50 490 18 -7 167 167 167 167 167 167 167 167	RUN LOADED MANUL: V Saw STERR BRAUE Ar T TINE NO. VES/NO VER TYPE MPH DEG. PERIOD NPUT Av A T TINE NO. VES/NO VER TYPE MPH DEG. PERIOD NPUT Av A T TINE 6-10 NO FEM DEG. % 9'S 0'SEC % 0'SEC SEC. % 9'S 0'SEC SEC. % 0'SEC % 0'SEC 5'S 6'S 1'S 1'S <t< th=""><th>RUN Loadded Maneur V δ_{sw} steek Brance A T Time NO. Yes/No Ver TYR MPH Des. PERIOD INDUT Auespace Peak FERIOD INDUT Auespace Peak Sec. δ_{s} $g's$ <t< th=""><th>RUN LUMDED MANELL V 6 sun steeler Ranket A T Tink NO. YES/NO VER TYRE MPH DEG. PERIOD INPUT AVERAGE PEAK PEAK PEAK SEC. X 9's 9's sec. K 1'n $6-10$ NO $4a$ J's $3's$ 9's $3'sec$ Sec. $3's$ $9's$ sec <</th><th>RUN Londed Maneul: V δ_{sw} GTERR BRAUE Ar T Time, NO. YES/NO VER TYRE MPH DEG. PERIOD INDUIT AVERAGE PERIOD INDUIT AVERAGE PERIOD NO. 6-10 NO. 4 SEC. % 9'S 9'S SEC. SEC. % 9'S SEC. SEC. SEC. % 9'S 9'S SEC. SEC.</th><th>RUN LOADED MANEL! V δ_{SW} STEER BRAUE Ay T TINE. NO. YES/NO VER TYRE MPH DEG. PERIOD INPUT Avecage DEAK SEC. χ_{S} $g's$ $g's$</th></t<></th></t<>	RUN Loadded Maneur V δ_{sw} steek Brance A T Time NO. Yes/No Ver TYR MPH Des. PERIOD INDUT Auespace Peak FERIOD INDUT Auespace Peak Sec. δ_{s} $g's$ <t< th=""><th>RUN LUMDED MANELL V 6 sun steeler Ranket A T Tink NO. YES/NO VER TYRE MPH DEG. PERIOD INPUT AVERAGE PEAK PEAK PEAK SEC. X 9's 9's sec. K 1'n $6-10$ NO $4a$ J's $3's$ 9's $3'sec$ Sec. $3's$ $9's$ sec <</th><th>RUN Londed Maneul: V δ_{sw} GTERR BRAUE Ar T Time, NO. YES/NO VER TYRE MPH DEG. PERIOD INDUIT AVERAGE PERIOD INDUIT AVERAGE PERIOD NO. 6-10 NO. 4 SEC. % 9'S 9'S SEC. SEC. % 9'S SEC. SEC. SEC. % 9'S 9'S SEC. SEC.</th><th>RUN LOADED MANEL! V δ_{SW} STEER BRAUE Ay T TINE. NO. YES/NO VER TYRE MPH DEG. PERIOD INPUT Avecage DEAK SEC. χ_{S} $g's$ $g's$</th></t<>	RUN LUMDED MANELL V 6 sun steeler Ranket A T Tink NO. YES/NO VER TYRE MPH DEG. PERIOD INPUT AVERAGE PEAK PEAK PEAK SEC. X 9's 9's sec. K 1'n $6-10$ NO $4a$ J's $3's$ 9's $3'sec$ Sec. $3's$ $9's$ sec <	RUN Londed Maneul: V δ_{sw} GTERR BRAUE Ar T Time, NO. YES/NO VER TYRE MPH DEG. PERIOD INDUIT AVERAGE PERIOD INDUIT AVERAGE PERIOD NO. 6-10 NO. 4 SEC. % 9'S 9'S SEC. SEC. % 9'S SEC. SEC. SEC. % 9'S 9'S SEC. SEC.	RUN LOADED MANEL! V δ_{SW} STEER BRAUE Ay T TINE. NO. YES/NO VER TYRE MPH DEG. PERIOD INPUT Avecage DEAK SEC. χ_{S} $g's$

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	анеет 6 о	R CUSTO B.75 X10	•	. •		• •			• • •	,, ,, ,,	• • • •	•	• •	•	· · ·	· · · ·	• • • • • •	· · · · · ·		• •	• •	· · ·	• • • • • •
···· ·		GOODYER HI MILEIR	TINE	SEC.	· • •			۰۰۰ ۱		N	1	• • • • • • • • • • • • • • • • • • •			1	1			1	1			· · · · · · · · · · · · · · · · · · ·
	UMMAR	S, REAR:		PEAK	°/sec	21 10 1	22	22		61	15	21	Ø	ດ	0)	0	01	10	\$	Θ	1	1	
-	DATA S	M TIRE	ΑY	PEAK	. 3,2	.45	54.	5	5	.45	35	.30	-Q	0 2).	с. <u>)</u> . "	<u>.</u>	n n	 0	01 01	10.		1	· · · · · · · · · · · · · · · · · · ·
 	DLING	R CUSTO	A× A×	AVERAGE	9's	06	0		.0	ç.	.05	50.	.0 <i>5</i>	¢0.	, o,		0	1.0.	- <u>C</u> -	<u>.</u>			· · · · · · · · · · · · · · · · · · ·
· · · · ·	HAND	: GOODYER	BRAKE	INPUT	??	. I	1	1			1	1	1		1	1		1	1	1	0 01	ļģ.	· · · · · · · · · · · · · · · · · · ·
	HICLE	S, FRONT	GTEER	PERIOD	SEC.	· · · · · ·	1	1		1		1	1	1	1	1	- 1 :	1 					
	DT VE	TIRE	Ssw	DEG.		224 R	224R	7544	2241	1261	1091	1231	796	<u>x</u> -6	XCS	704	7 ℃	614	7 2 2	19 19			
	I-DC	• • • • • • •	>	HdW	· · · · · · · · · · · · · · · · · · ·	0 M	0 m	ŝ	30	30 M	0 M	30	0 E	0	0	0	<u>C</u> -\0	50	$\frac{0}{1_{0}}$	<u>0</u>	40	4	
	NSH-I.	VAN	MANEU-	VER TYPE	NO.	46	4	46	46	46	46	48	46	4	<i>?</i>	8	9	1.21	\$	9	М	Я	
	11	licle	LOADED	YES/NO		NO.	No	Nd	ØN	0N	NO	NO	No	NO	<u>o</u> N	-V	NO.	No	CN N	NON NO	YES	X S	
•••••••	 	VEH	RUN	No.		7-05	7-06	707	7 -03	1-03	ÖJ=L		7-12	7-13	./- 4	7-15	-1-16			61-	81-05	S)- S	
	• •	• • • • •	•••	• •	···• •				• •	•	e		6/ 2	U C	7	••••••	· · • • • •		•	• •	••••		

.•••			A2H-I	I - D0	T VE	HICLE	HAND	L NG	DATA SI	MMAR		SHEET 7 OF 11
	VEH	HCLE V	AN	• • •	TIRES	SI FRONT	GOODYE	AR CUSTON	TIRE	S, REAR:	GOOD YEA	R CUSTOPY B.75 X16.5 IE
•	RUN	LOADED	MANEU-	>	Ssw	GTEER	BRAKE	A×	ΑY	د د	TINE	
	No.	YES/NO	VER TYPE	HdW	DEG.	PERIOD	INPUT	AVERAGE	PEAK	PEAK	SEC.	· ·
, .			NO.	- • • • • • • • • • • • • • • • • • • •	· • • • •	SEC.	%	9's	9'5	°/sec	• •	
•	8-07	YES	. 1	012			40	52.	4. • • • •	· •	· · · · · · · · · · · · · · · · · · ·	
•	8-03	YES	Н	40			40	-12 -12 -				•
•	8-09	YE\$	М	40	1		0	+5-	R.05	K 3	I	
i i	8-10	YES	И	40		I	60	0	R.06	к К К	1	•
· •	<u>भ</u> । ०	YES	M	40		1	0	. 60	R.08	<i>R</i> 4	1	
e	8 - 13	YES	7	40		1	80	0 1	R.10	RG	• • •	· ·
57	6-14	<u>Y</u> =5	× ×	0			001	0/.	R. 30	K 31	1	R.R. LOCK, 45° R
(2)	0-12	YES	7	40			001	10-	R.45	R40+		R.R. LOCK,
17.	6 - 20	<u>Y</u> =5	Z	40			50					FRONT ONLY
	1 1 0	2 5 1 2	И	40			0				↓ ↑	FEONT ENCY
>	8-22	い じ ~~~	Н	4.0	<u> </u>	1	0				•	REAR ONLY
• • •	8-23	- √=S	N	40	t		ß					REAR OILY
• •	70-6	YES	Q	20	208	1	40	0 0		1	1	• • •
•	9 -03	SEY	2	50	10	1	0 O	, M	•	14	• • • • • • • • • • • • • • • • • • •	
	60-16		Q	0 10	7	3	Q		0.0	6	1	
•	<u>c</u>		<u>cu</u>	10	7		0	0 5	09.	(1) (1)		LR LOCK
;		江库	N	<u>را</u> ارا	763	1	0	0	-Ç-	2		LP LOC'
									-		•	•

SHEET 8 OF 11	AR CUSTON	· · ·	•••	•	RR LOCK	RE LOCK		- •		· · ·	• •	•	END DSC, ROLL	• • • • •	· · · · · · · · · · · · · · · · · · ·		• • • • • •	•	• •		· · ·	• • • • • • • • • • • • • • • • • • •
	HI MILEN	TINE	SEC.	• •	· · · · · · · · · · · · · · · · · · ·		1.1	/ /	/*/	1.1	/'/	1.1	1.6	1,5	1.6	1.6	1,6	1,6	0'1	1,2	2.1	••••
NMMAR	S, REAR		PEAK	°/sec	4.4	45	L 15/210	715/610	8/2//8/7	L 17/E12	K17/L17	RIT/18	L 5/RB	L 2/R 4	L18/R17	L 6/87	K 18/213	0/18/13	ES/E1	L 7/R 7	710/810	
DATA SI	IRE TIRE	γÅ	PEAK	9'S	-22	.53	7 1/2 0B	L,25/R.20	06.35/6.30	L. 35/230	R. 30/1.35	R, 30/L.35	L.15/k.08	L.27/r.22	1.40/2.35	L.42/233	R. 35/2.40	P, 35/,37	01.3/0117	1 20/1:15	1 30/1.25	
UNG DLNG	92 CUST 75 X 16.5	A×	AVERAGE	g's	157.	+5+·	tŋ -0-	50,	•0°	65	1.0	.0°	50,	-60.	.06	000	-50.	6	50.	50.	, C,	
HANC	MILER 8	BRAKE	INPUT	%	-20	20	1	1	1			1	1	1					1.			· · · · · · · · · · · · · · · · · · ·
HICLE	SI FRONT	STEER	PERIOD	SEC.	1	1	ល	2	N	ิณ	Q	ચ	m	m	σ	η	m	M	<i>C</i> I	2	<u>N</u>	
DT VE	TIRE	Ssw	DEG.	· · · · · ·	858	848	749	11281	1924	1924	1/3/	1928	641	1287	1251	126	2761	<u>ः</u> ः /	1 1 1 1	74.0	700	
О - - -	• • • • • • •	>	HdW		20	Q Q	0 M	00	30	0 m	<u>,</u>	000	ЭÖ.	98	0 M	Q (1)	0 m	_ <u>``</u>	0	0	0	
H-I	VAN	MANEU-	VER TYRE	NO.	A]	Q	m	R	3	m	3	'n	β	m	M	m	<u>w</u>	i U	<u>Ny</u>	- <u></u>		
	HCLE	LOADED	YES/NO		YES.	Xes S	YES	5775	YES	RES	4CS	YES	VES	VES	Ye's.	VES	YES	YE'S	VĖS		. <u>_Y</u> E\$	
	VEF	RUN	No.		9-12	<u>n</u> <u>n</u>	60-01	01-01	10-11	21-01	10-13	10-14	10-15	91-01	11-01	10-18	51-01	10-20	11-21	11-22	1-2 1-1	
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SHEET 9	R CUSTI	•	•				-	•	•	 	•		•	•				•	•	• • • • •		
~~~>	GOODYEA HI MILER	TINE	SEC.		2.7	2.	1,2	1.5	971	7:00	27	1:7	<u>1</u> ,7	1.	•	1	1			1		· · · · · · · · · · · · · · · · · · ·
NMMAR	S, REAR:	د د د	PEAK	°/sec	- 11/1-	2.10/49	R 9/412	73/27	L.71/RG	~ <i>11/2 11</i>	11/11/1	10/112	117/012	۲) ا	e M	2	2	9	2	4	Ŋ	
DATA SI	M TIRE	AΥ	PEAK	9'5	1.30/4.25	R.25/,30	R.25/.30	201/21.7	6/10/32.7	25/2.32	2,35/1.35	230/135	2t 702 Y	, m	0 m	14	10	8. 2.	ରା ୧୯	41.	<b>0</b>	
LING L	R CUSTO	A×	AVERAGE	9's	-90-		40.	90.	10.	- - - - -	<b>1</b> 90		0	0	.05		-0 -0	00	,00,	9	5 Q	
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DT VE	TIRES	Sew	DEG.	· · · · · · · · · · · · · · · · · · ·	796	96	96R	322	644	795	126	96 K	22	1281	1287	1982	13 20 20 20	484	49	484	200 -+	
	• • • • • •	>	HdW	· · · · ·	8	B	2	-bj	£	3	R	20	5	30	С С	<u>ි</u> ස	<u></u> [6]	5	् २	2	5	
R H-I	Å∕ N	MANEU-	VER TYPE	NO.	m	M	m	_w	M	- M	m	m	m	4.	40	4		40	4 9	4	40	
	IICLE V	LOADED	YES/NO		YES	5.72	465	<u>V</u> <del>C</del> S	Kes.	1		i.	Ks.	10 	YES			Y£5	2	VE:	XE S	-
	VEH	RUN	NO.	• •	11-24	11-25	11-26	11-27	//-23	11-29	08=11	11=31	1[-35	12-05	12-06	12-07	12-03	12-09	12-10	11-12	12-12	
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•	SHEET 10 0	Z CUSTOM	•			• •		• •		• ₩ •	, , ,	• • •		· · ·	· ·			• •	• •	• •	• •	• • • • •••	••••••••••••••••••••••••••••••••••••••
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	<b>N-HSR</b>	VAN	MANEU-	VER TYPE	NO.	4b	40	4 a	4 a	40	4	4a	40	,4a	40	4 9	1 1 1	4	4	1 A	7	G	
· · · · · ·	+	IICLE	LOADED	YES/NO		765	<u>V</u> ES	YE5	VES	YES	Ves	KB	X ES	YES	K K	YES-	7 11 2	22	YES.	Z N	1/1-2	5	
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<b>НЕЕТ // 01</b> CUSTOM 8,757X16.5		•		•	• •	 		•¥ /	• •	• •	•	• •			•	• •	• • • ••	· •	· • •	• - •	• • • •••
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I-HSR VAN	MANEU-	VER TYPE	NO.	49	4a	4a	40	4a	Ap	4a	40	40	4 Q	4 8	4	4a					
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VEH	RUN	ON N		14-07	14-08	14-09	14-10	11-11	74-12	7/4 - 1/4	14-15	14-17	81-14	61-17	14-20	12-21	+	•	3 <b>1</b>		· · · · · · · · · · · · · · · · · · ·
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	· · · · · · · · · · · · · · · · · · ·	ENRESTON COUNTRY	TINE	SEC.	• •	1	1	<b>1</b>		\ \ 	1		1		02 · /	021	1,20	1,20	1,25	11,20	10	170	
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- · · ·	DATA SI	TIRE	AY	PEAK	9'5	.3'/	č.	•	5.5	• 47	.47	•67	68	•75	L.12/R.10	L .25/R.22	L.35/R.32	L. 35/R.30	R. 35/L.33	R. 35/L. 33	L.12/R.10	1,27/9.25	
· · · ·	LING 1	Z CUSTON	Ax Ax	AVERAGE	9's	. 15	-1	10-01-	en M	<u>س</u> 00	64	• #3	- 1 <u>0</u> -	,27	5		6.		-~~	0			
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	5, REAR:	L	PEAK	o/sec	1.1/12 21	2 20 / 8 ZZ	R23/1 20	122/120	14/183	6 2/4 7	L 11/R 13	R13/212	R13/4 12	13/23	13/29	115/214	1 2/517	R15/4 M	L15/4 15	14	5	
	TIRES	Aγ	PEAK	9'5	L.42/R.37	L.40/R.37	R.40/1.38	R.40/L.40	L.12/R.10	L.20/R.18	L.30/R.27	R.30/L.28	R.32/2.24	21.3/6.12	L,25/12.23	1,40/1.37	1.1335	R.4211 .35	R 40/. 38	m m	35	
	LING L	A×	AVERAGE	g's	03	-0-	-0- -0-		2 ()•		-0, -3)	<i>•0</i> ×				0	00	<u>م</u>	- <u>o</u> -'n	10 3	to o	· · · · · · · · · · · · · · · · · · ·
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	VAN	MANEU-	VER TYRE	NO.		m	<del>m</del>	<u>m</u>	m	m	ſ	M	1/1	6	M	m	n	<u>m</u>	-0	÷40	ð	
· · · · · · · · · · · · · · · · · · ·	ICLE TT	LOADED	YES/NO	· · · · · · · · · · · · · · · · · · ·	YES	YES	1 2 2	5	YES	ye s	YES	Yes	10	YE's	- <b>ア</b> - - - - - - - - - - -	С С	S S			400	VES	
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· · · · ·	LING 1	A× A	AVERAGE	Q_s	1.0.	.0.	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	<i>∞</i> .		-4.0	μ <u>c</u> .	9	, , ,	L.()•	œ.	<b>*</b> () <b>+</b>	<u> </u>	÷ Č	~	e C		
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· · · ·	VHN	MANEU-	VER TYRE	NO.	.40	<u>1</u>	4 a	40	40	40	at:	4	4 Q	40	4	0		40.	40	40		
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D NC	· · · ·	A×	g's	NWA4444 6 60000000000000000000000000000000
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+	ICLE PI	LOADED	Yes/NO	>?????????????????????????????????????
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- DC	22	>	HdW	39999695599999777797 198959599
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ASH-I	K-UP	MANEU-	VER TYPE NO.	( , el el
	HICLE PIC	LOADED	Yes/no	
	VEH	RUN	Ö V	82 2 2 20 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2

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	DATA S	TIRE	ΑY	PEAK	g's	winning und not of the mode
	DLING		A×	AVERAGE	g's	5265220 500202N#22000
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dH-HJ	MANEU-	VER TYPE	NO.	NNNNN MMMMMMMMMMMMMMMMMMMMMMMMMMMMMMMM
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TIRE	Aγ	PEAK	9'5	24000000000000000000000000000000000000
	A×	AVERAGE	g's	PC2795053951222355557553
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s TIRES	Ssw	DEG.		202242320000000000000000000000000000000
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T VE	Z TIRE	Ssw	DEG.		60004444 2000000000000000000000000000000
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VE	HICLE	PICK-UP	TCI	3 TIRE	S, FRONT	•		TIRE	SIREAR		· · · · · · · ·
RUN NO.	LOADED YES/NO	MANEU- VER TYPE NO.	V MPH	ర్ sw DEG,	STEER PERIOD SEC.	BRAKE INPUT %	Ax AVERAGE 9's	Ay Peak g's	r PEAK °/sec	TINF. SEC.	
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 	VEh	RUN	No.	• • •	644	4333 1111 1111 1111
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ATA SU	TEE TIRES 20/F	AΥ	PEAK	9'5	53	53	5	.45	48	L.I.: /R. 08	1.18/6.17	L 30/R.27	L 32/R.27	R.21/L.32	R. / .31	7,12/200	L23/R.20	L 37/P.23	123/621	ζ€ 1/c2.1	R.3./1, 35	L.12/R.10
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 	VEH	RUN	No.		23-11	1 1 1 1 1	13-13	23-14	23-15	24 - 05	1 - OC	24-07	24-08	24-09	24-10	1- 42	21-42	14 - 13	24 - 14	24 - 15	24 - IG	24 . 11
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		- - -	NSH-I.	I - D0	T VE	HICLE	HAND	R N L	DATA SI	UMMAR	<u> </u>	SHEET	L OF 7
	VE	HICLE HE	AVV TRUC		TIRE	SI FRONT	TRIPLE TR	FLEETIMA FT 6 EAU 10,00 × 20	D/F TIRE	S, REAR:	UNIROYAL	FLEETMI	\srER Xvo∕F
	RUN	LOADED	MANEU-	>	Ssw	GTEER	BRAKE	Ax	ΑY	۲ ۲	TINE		
	NO.	YES/NO	VER TYPE	HdW	DEG.	PERIOD	INPUT	AVERAGE	PEAK	PEAK	SEC.	•••-	• • •
			NO.			SEC.	%	9's	9'5	o/sec	·····	•	
·• .	24 - 13	0 Z	'n	20	BOL	с <u>і</u>	1	.04	1.22 .15	74/27	1.2	· •	
-	24-19	0 Z	а) Т	6	1201		· · · ·	03	2.28° 2° 24	18/128	11		
< -	02-72	07	6.3	50	7.02			S.	1,34/R,24	L8/R 8	c5 >		
		NO.	€ 	50	120 R			50	R. 22/1. 23	RB/LB	i i i	-	
	24 - 22	NO	n	50	120 12			ر کر	R.23/1.28	R 8/18	1.1	Y	
	25 - 23	O Z	M	20-	40 L			۶ ۲	2.10/2.08	12/22	0.5	j‡ -	
	5-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1	0	m	0	80 F	*		ň	L 22/R/B	L 4/R 5	0.	DATA L	A 76
85	25-25	0 V	m	50	120 L			6	L. 30/R. 28	$L \frac{1}{R} g$	7.7	-	
	25-26	0 7	N	50	1021	· · · · · · · · · · · · · · · · · · ·			L == /R25	L 7/R 6	2.1		
20	25-27	o Z	M.	20.	120 6		;	40.	R. 2/4.30	R6/4 7	2,1		
7	25-28	0 7	ŝ M	ري ري	12012	<u></u>		4	2.5/4.2	R-1/2 7	2,4		
-	26-05	o Z	40	S S	1601	- ···	·····	M C	ý	5		· · · · · · · ·	
	25 - 06	ON	4 2	- 0. - 0.	اردی ا			<u> </u>	<u>, 1</u>				
ana ina 19 Na 1	10-92	0 Z	40	. 0 . 2 . 2	16012			-20-	<u>,</u>	5		· • - · · · · · · · · · · · · · · · · ·	
•	30-92	0 Z	4 0,	 M	160 R	· ·	·· ·	<u>10</u>	ČĮ.	6		-+ }	
•	56-00	0 Z	4	10 0	90 F	 	· · · · · · · · · · · · · · · · · · ·		./.	M			
i.	Ci - 9-	N N	40	Ń	6	· · · · · · · · · · · · · · · · · · ·	: 	5	67-	m			
	26-11	O Z	4	0	200		<u>, , , ,</u>	51	ωţ	44	1-1	• • • •	• • • • • • • • • • •
	10-11) Z	44-1	ດ 2	2 2 0	-		<u>, 1</u>	5	F		•	

			ASH-I	I-D0	T V E	HICLE	HAND	UNG	DATA SI	UMMAR	~	SHEET 5	of 7
	VEN	ICLE HE	AVY TRU		TIRES	S, FRONT	TRIPLE TR	FLEETMAS		S, REAR:	TIGIPLE TRI	FLEETMAS EHD. 10.00)	тес (20/ г .
	RUN	LOADED	MANEU-	>	Ssw	STEER	BRAKE	×	ΑY		TINE	· ·	,
	No.	YES/NO	VER TYRE	HdW	DEG,	PERIOD	INPUT	AVERNGE	PEAK	PEAK	SEC.	· ·	• • • • • • • • • • • • • • • • • • •
			NO.		• • • •	SEC.	%	9's	9'5	°/sec	· · · ·	• •	
	26 - 13	ON	46	30	120 L	-	· · · · · · · · · · · · · · · · · · ·		÷.	μ	· (·	ASCEND	
	26-14	ON	46	-Se Se	1691			N C		00	1	• • •	
4	26 - 15	NO	46	30	2001			N Ç	S.		•		
	91-9	NO	46	30	1 0 F t			ŝ		13			
	71-02	071	4 2	- Ci	190 F		<u> </u>	m.	27	- 76	•		
	26-18	NO	4 6	0 M	280 L			ć. Ŧ	4	9/			
1	26-19	ON	4.6	<u>Q</u>	280 iz			.05	.45	Г	1		
28	26-20	NO	.46	0 M	280 P	}		40.	+ H.	[]	b		
1	26-21	0 N	46	20	40 L	· T		50.	[0]				
	26 - 22	0 Z	48	50	109	1 1 1 1		40.	10-	N	1		
8	26-23	0 V	46	<u>را</u>	90-L 90-L			90.	54	4			
Bassa - 10	26 - 24	0N	4	20	100	· / ·		pd.		2			
		NO	4	<u></u>	1001			•06	୍	9			
	52 - LJ	ON	4 7-0	5	ioo iz	· · · · ·	}-	ľ¢,		٩	+	· · · · · · · · · · · · · · · · · · ·	
		NO.	2 T	<u>.</u>	10/1	· · · ·	1.	10	ų į	9	1	RECORDER	an LATE
	- 8	ON	4	.9. M	28012			رب 10	13 13	5	1	DECSEV	
)(- 8 -	110	4.		24 24 24	· · · · ·		2	40	Ø			
,	10-81	.10	4	<i>R</i>	1	· · ·	1	2	2	2		· · ·	

			SH-I	I - D0	T VE	HICLE	HAND		DATA SI	UMMAR	>	SHEET 6	0F 7
	VEH	HCLE HE	AVY TRI		TIRE	L FRONT	JEANARD TRA	FLIFETMAST EAD, ID.00X	ER TIRE	S, REAR:	UNIROVAL TRIPLE T	FLEETM READ 10.	STER 20x 20/F
	RUN	LOADED	MANEU-	>	Ssw	STEER	BRAKE	Åx	AY	5	TINE		
	No.	YES/NO	VER TYPE	HdW	DEG.	PERIOD	INPUT	AVERACE	PEAK	PEAK	SEC.	• •	
			NO.			SEC.	%	g's	9'5	o/sec	• •	•	
	28-08	ÔN	46	30	-1082	. .	· · · ·	50	5	õ	·	•	
	23-09	ON	46	0 M	2401	1	1	05	5	<u></u>	:- }	· · · ·	• • • • • • • • • • • • • • • • • • •
	23-10	071	46	ŝ	200-	;	- 7	,06	30	9			
_	29-15	ON	46	30	28012			90.	4	16			
· · · · · · · · · · · · · · · · · · ·	29-16	ON	46	QC	2802	•		00	10	16			
*** * ****	L1-62	NO	46	ON N	2.80				04	-17			
	21-62	0N N	4 6	ŝ	285 285			1.0.	с), Ф	//			
87	29 - 12	NO	4 4-	- hi	2401-			-10	34	/4	1		
	29-20	ON	46	ю. 0	7002			501	δĴ,	0			
]	29-21	NO	42	0. 0.	1.091			0	M M	80			
	22-62	NC	4	$\overset{0}{\mathfrak{B}}$	1202			9	<u> </u>	29		-	
	29-23	NO	4 5	<u>Ş</u>	100 2			40'	- <u>c</u> . <u></u> -	<u>.</u>	· · · · · · · · · · · · · · · · · · ·		
·····	29-20	07.	46	-0-0-	10012			- - -	4	9		· · · · · · · · · · · · · · · · · · ·	
	29-25	NO	4.6	Q.	7001		- <u></u>	1.0.	1,7	4	1		
	29-26	ΝÖ	46	S.	1001	····	· · ·	90	M	9			
	29. 24	ON	48	20	804			ζċ	24	4			
	29-28	0.1		\mathcal{B}	60		· · · · ·	<u>0</u> 5	67.	m		∔ ∔ ↓ _ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓	
	5.68	NO	4	50	404	· · · · · ·		50	4		<u> </u>	· · · ·	
				•	•	•	-		•	•		•	

IEET 7 OF 7	LEETMASTER				D. LOCK UP							ALLED TO LEFT			DNT. BEEAK ONLY	3	EAR BREAK ONLY	2				
K SH	UNIROYAL F	TINE	SEC.		· Z						48))							
UMMAR	SI REAR:		PEAK	o/sec		0	0	0				0			0	0	0	0		:		
DATA S	STELTIRE X20/F	AY	PEAK	3'S	20,	5 C	S.	10	C C	8	â	2	Ĩ	, M	0 0	a a	-(0	07				
DLING	FLEETWA	A×	AVERAGE	g's	.13	-13	12	10	32	т С	Ő	.45	15	44	10	Ň	02	02,				· · · · · · · · · · · · · · · · · · ·
HAN	: UNIROYAL	BRAKE	INPUT	??	20	50	40	0 T	60	09	8	0	100	001	-0- -0-	D.	ß	50	······································			······································
HICLE	S, FRONT	GTEER	PERIOD	SEC.		· · ·	· · · ·		· · ·	1	1	· · · · · ·		1		· · · ·	- · · · · · · · · · · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·		· · · · ·	· ···	· · · · · ·
DT VE	TIRE	Ssw	DEG.		1			·	}		·		· · · · ·	•		· · ·	 	· · ·			· ·	· · · · · ·
	UCK	>	HdW		40	40	40	40	4 0	4	4	4	40	40.	40	Å O		40	· ·	· · · · · · · · · · · · · · · · · · ·	••••••••••••••••••••••••••••••••••••••	· · · · · · · · · · · · · · · · · · ·
SH-I.	AVY TR	MANEU-	VER TYRE	NO.	71	Ч	7	Н	А	М	A	7	71	· · ·	H	71			· · · · ·		• • •	· · · ·
T T	ICLE HE	LOADED	YES/NO		YES	YES	YES	YES	YES.	YES	YES	YES	YE S	YES	Υ Ε'ι	YES	YES.	く ビ ン ン				
	VEH	RUN	No.		30-05	30-02	30-04	30-03	30-00	30-10	30-11	30-12	20-13	30-14	61-08	30-20	30-21	30-22				
-								4		,	7) 88	7		.							

APPENDIX F

This appendix presents listings of the condensed metrics []] describing the results of simulated trapezoidal and sinusoidal steer maneuvers conducted on the various test vehicles.

The results from three classes of tests: Trapezoidal steer, Sinusoidal steer 1 and Sinusoidal steer 2, are presented. Trapezoidal steer tests employed a steering wheel angle input of the following form:



For Sinusoidal steer 1, an sine wave steering wheel angle input of a 2-second period is used for all vehicles. Sinusoidal steer 2 employes a 3-second period for the two lighter vehicles and a 4-second period for the two heavy vehicles.

The title for each page of data indicates the vehicle and its loading condition, the initial velocity of the test maneuver, and a tire code, which in combination with Table F.1 indicates the tires used on the vehicle.

A dictionary of metric definitions appears in Table F.2.

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Heavy Bus:

HBO: Tire H12 on all wheelsHB1: Tire H18 on all wheelsHB2: Tire H19 on all wheels

Heavy Truck:

HT1: Tire H1 on all wheels

HT2: Tire H4 on all wheels

HT3: Tire H6 on all wheels

Light Van:

EO: Tire L2 on all wheels (75 psi)

El: Tire L10 on all wheels

E2: Tire L15 on all wheels

E3: Tire L2 on all wheels (45 psi front, 75 psi rear)

E4: Tire L2 on front wheels (45 psi) and L11 on rear wheels

Pickup Truck

- FO: Tire L1 on all wheels
- Fl: Tire L16 on all wheels

F2: Tire L13 on all wheels

F3: Tire Ll on all wheels (45 psi front, 75 psi rear)

*Tires identified as per codings presented in Table 3.1. Recommended inflation pressures except as indicated. Table F.2.Dictionary of Metrics for Simulated
Trapezoidal and Sinusoidal Steer Maneuvers.

Trapezoidal Steer

JINA. Maximum Sceering wheel angle (deg	STR4:	Maximum	steering	wheel	angle	(deq
---	-------	---------	----------	-------	-------	------

BETAMX: Maximum absolute sideslip angle during the 2-second time period (t), beginning at the time of steering input (rad.)

BETDMX: Maximum absolute value of the rate of change of sideslip angle during the time period t (rad/sec).

CUVRAT: Average path curvature ratios = $(1/R)_{av}/(1/R)_{o}$

where

$$\begin{pmatrix} \frac{1}{R} \end{pmatrix}_{av} = \frac{1}{2} \int_{t_4}^{t_4+2} (\frac{1}{R}) dt = \frac{1}{2s_f} \sum_{i=1}^{2s_f} (\frac{1}{R})_i$$

$$\begin{pmatrix} \frac{1}{R} \end{pmatrix}_o = \frac{1}{R} \Big|_{t_4} = (\frac{1}{R})_i, \quad i=0$$

and

 t_4 is the time of the steering input t_4 +1 is the time 2 seconds after the steering input $\left(\frac{1}{R}\right)_{av}$ is the average path curvature over the above defined interval $[t_4, t_4+1]$ $\left(\frac{1}{R}\right)_0$ is the path curvature at t_0 .

Table F.2 (Cont.)

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AYMAX:	Maximum lateral acceleration over the entire maneuver time interval (g's).
RMAX:	Maximum yaw rate over the entire maneuver time interval (rad/sec).
PHIMAX:	Maximum roll angle over the entire maneuver time interval (deg).

Sinusoidal Steer

STR5:	Maximum steering wheel angle (deg).
AYMAX:	Maximum lateral acceleration over the entire maneuver time interval (g's).
DEL:	Lateral deviation of the vehicle position from the "desired" 12-ft lane change at the completion of the maneuver (ft).
BETAMAX:	Maximum absolute value of sideslip angle during the time period t (rad).
DELPSI:	Vehicle heading angle at the completion of the maneuver (rad).
UIN:	Initial velocity (mph).
PHIMAX:	Maximum roll angle over the entire maneuver time interval (deg).

HEAVY BUS SIMULATION RESULTS

		Tra	pezoidal Steer					
TR4. (1) BETAMX(1) BETDMX(1) CUVRATI	1) AYMAX.(1) RMAX.	-) FHIMAX(+
180. 240.	0.108F-	-0Z 0.118E-0 -01 0.181E-0	01 0.275 01 0.358	0.264 0.348	0.10	4 9 U	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	
300.	0.172E-	-01 0.262E-	0.436	0.423	0.3	20	5.27	
360.	0.246E-	-01 0.348E-(01 0.508	0.493	0.3	86	6.14	
420.	0.329E-	-01 0.469E-0	0.573	0.549	0.4	37	6.7 8	
480.	0.400E-	-01 0.575E-(01 0.631	0.637	0.4	94	7.50	
		Sir	usoidal Steer	_				·
STR5(1) AYMAX.(1) DEL(1) BETAMX(1) DELPSI(1) UIN.	-	1 PHTMAX	
120.	0.118	9.76	0.593E	-02 0.47	5E-02 3(0.0	2.12	-
240.	0.219	7.71	0.151E	-01 0.75	0E-02 3(0.0	3.95	
360.	0.307	5.96	0.271E	-01 0.111	3E-01 3(0.0	5.39	
460.	0.370	4.86	0.400E	-01 0.16	5E-01 3(0.0	6.40	
600.	0.413	4.98	0.504E	-01 0.20	1E01 3(0.0	6.95	
720./	0.438	5.13	0.561E	-01 0.21	4E01 3(0.0	7.06	
840.	0.453	in N In	0.596E	-01 0.22	6F-01 30	0.0	7 04	
					-	•		
		Sin	usoidal Steer 2	0				
STR5(1) AYMAX.(1) DEL(1) BETAMX(1) DELPSI(1) UIN.	_	1) FHIMAX(•
120.	0.153	8.79	0.553E	-02 0.66	5E-02 30	0.0	2.04	•
240.	0.285	17.6	0.161E	-01 0.10	0E-01 3(0.0	3.75	
360.	0.394	27.0	0.326E	-01 0.18	7E-01 3(0.0	5.11	
460.	0.481	34.6	0.529E	-01 0.31	1E-01 3(0.0	6.14	
480.	0.481	34.6	0.530E	-01 0.31	1E01 3(0.0	6.15	
550.	0.521	37.8	0.649E	-01 0.383	2E-01 3(0.0	6.74	
L 								
r igure r	.I. UNIOAGEG IN	eavy pus, v _o = Ju	mpn, iire cout	e: HbU.				

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	PHIMAX(2.65 5.21 5.21 7.21 12.3	
	1) RMAX. (1) 0.940E-01 0.143 0.193 0.290 0.335	
	AYMAX.(0.211 0.319 0.319 0.423 0.507 0.607 0.645	
ezoidal Steer	CUVRAT(1) 0.645E-01 0.936E-01 0.120 0.167 0.187	soidal Steer 1
Trap	BETDMX(1) 0.162E-01 0.253E-01 0.351E-01 0.457E-01 0.5876-01 0.687E-01	Sin
	1) BETAMX(1) 0.175E-01 0.284E-01 0.406E-01 0.538E-01 0.679E-01 0.825E-01	
	STR4. (60.0 90.0 120 150 210.	

7		7			۰ ۱				
1) PHIMAX(1.75	3.27	4.54	5.57	6.38	7.01	7.46	7.75	
UIN(50.0	50.0	50.0	50.0	50.0	50.0	0.01	0.01	
DELFSI(1)	0.369E-02	0.382E-02	0.194E-02	-0.284E-02	-0.107E-01	-0.246E-01	-0.464E-01	-0.731E-01	
) BETAMX(1)	0.120E-01	0.256E-01	0.407E-01	0.567E-01	0.729E-01	0.874E-01	0.988E-01	0.108	
1) DEL(5.4.9	7.44	5.50	5.92	6.64	7.25	7.62	2.79	
1 AYMAX (0 105		0.271	0.334	0.383	0.420	0.453	0.476	
CTRS	0.07		.041	240.	300.	360.	420.	480.	

			Sinusoidal Steer 2		·	
STR5(1) AYMAX.(1) DEL(1) BETAMX(1) 0.145F-01	DELFSI(1) 0.696E-02	UIN(50.0	1) PHIMAX(2.06
60.0 100	0110	21.6	0.388E-01	0.795E-02	50.0	3.82
	0 413	33.5	0.675E-01	0.829E-02	0.00	091 1
		44.8	0.102	0.127E-01	0.02	
		54.5	0.141	0.115E-01	50.0	8.82
- C C C C			0.180	0.316E-01	0.02	9.02
	0 458 0 458	65.8	0.209	0.124E-01	50.0	10.3
480.	0.843	67.3	0.231	-0.647E-01	50.0	11.1

Figure F.2. Unloaded heavy bus, $V_0 = 50 \text{ mph}$, tire code: HBO.

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					Trap	ezoidal Stee	٤				
STR4(*	BETAMX (1	BETDMX(1)	CUVRAT (1)	AYMAX. (1) KMAX(1) PHIMAX(•
180.		0.315E-	00	0.642	E-02	0.255		0.230	0.168	3.71	
240.		0.418E-	N ⊙	0.100	E-01	0.333		0.301	0.222	4.84	
300.		0.998E-	0 0	0.175	E-01	0.403		0.364	0.272	5.89	
360.		0.178E-	01	0.2691	E-01	0.468		0.421	0.321	6.81	
420.		0.268E-	01	0.3931	E-01	0.528		0.473	0.367	7.71	
480.		0.346E-	01	0.5091	E-01	0.584		0.531	0.409	₿ . 46	
					Sinu	soidal Steer	_				ł
STR5(Ĵ	AYMAX. (1	a C	EL(1)	BETAMX(1)	DELPSI(1)) UIN	1) FHIMAX(1
120.		0.127		9.98		0.386E-	00	0.371E-02	20.0	2.82	
240.		0.228		6.03		0.561E-	0 0	0.597E-02	20.0	4.96	
360.		0.305		6.32		0.147E-	01	0.784E-02	20.0	6.78	
480.		0.360		4.94		0.260E-	01	0.777E-02	20.0	<u>6,20</u>	
540.		0.387		4.62		0.343E-0	01	0.801E-02	20.0	8.80	

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	1					
	1) FHIMAX(2.46	4.57	6.15	7.63	<u>8.34</u>
	UINI	30.0	30.0	30.0	30.0	30.0
	(1)	42E02	48E-02	08E-01	83E-01	92E-01
	DELFSI	0,5	0.6	0.10	0.11	0.19
teer 2	(()	16E-02	24E-02	39E-01	33E-01	50E01
inusoidal S	1) BETAMX	0.3	0.6	0.1	0.3	0.4
S) DEL(7.98	15.1	23.4	30.6	33.4
	1) AYMAX.(1	0.142	0.271	0.374	0.455	0.485
	STR5(120.	240.	360.	480.	540.

HBO. Loaded heavy bus, V₀ = 30 mph, tire code: Figure F.3.

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	PHIMAX(44 44	3 . 70	4.86	5.91	6.9B	7.85	Ĭ	PHIMAX(
	1)	E-01							-
	RMAX(0.689	0.104	0.139	0.172	0.204	0.235		line
coidal Steer	1)								
	AYMAX.(0.154	0.232	0.304	0.369	0.430	0.483		
	1)	E-01	E-01					r]	~
	CUVRATI	0.551	0.808	0.105	0.127	0.147	0.165	soidal Stee	D RETAMY
Trape	1)	E-01	E-01	E-01	F-01	E-01	Ш-01 Ш-01	Sinus	-
	BETDMX(0.116	0.184	0.261	0.349	0.451	0.564		ncı (
	;	П-01	-01		- 0 - u				
	1) BETAMX(0.1191	0.2001	0.7981	0.4001	0.534	0.6711		
	, ,	0.0		000	- - 		10.		1
	STR4.	9	0	• •	• •		- 01	•	CTD5

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) PHIMAX(1.98	3.86	5.42	6.69	7.73
J [1 50.0	50.0	50.0	50.0	0.0
016	0.201E-02	0.876E-04	-0.717E-02	-0.206E-01
BETAMX(1) 0.AB9F-02	0.200E-01	0.339E-01	0.495E-01	0.651E-01
DEL(1)	6.29	6.54	5.11	5.47
1) AYMAX.(1)] 0 008F-01	0.188	0.261	0.313	0.350
STR5(120.	180.	240.	300.

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Figure F

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4.12 6.07 8.09 9.88 2.21 DELFSI(1) UIN...(0.337E-02 50.0 0.375E-02 50.0 0.112E-02 50.0 -0.714E-02 50.0 -0.475E-01 50.0 FAMX(1) DELFSI(0.111E-01 0.333 0.272E-01 0.493E-01 0.773E-01 0.117 40.45 40.45 40.32 40.33 1) DEL...(8.50 1) AYMAX.(0.133 0.257 0.257 0.363 0.454 0.583 STR5..(60.0 120. 180. 240. 300.

Sinusoidal Steer 2

1) BETAMX(

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1) FHIMAX(

	- 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	4 m m 0 9	
	1) FHIMAX 34. 55. 56. 57.	РНІМАХ И 4 № 2 И 4 № 2) FHIMAX 2.4 5.2 5.2 5.2
	RMAX. (0.193 0.256 0.318 0.318 0.431 0.431 0.543		JIN(30.0 30.0 30.0 30.0 30.0
	AYMAX.(1) 0.265 0.347 0.422 0.491 0.518 0.655 0.655	DELFSI(1) 0.479E-02 0.764E-02 0.127E-01 0.194E-01 0.222E-01	DELPSI(1) 1 0.662E-02 0.995E-02 0.183E-01 0.183E-01
oezoidal Steer	CUVRAT(1) 0.283 0.368 0.448 0.589 0.589 0.589 0.589 0.589	soidal Steer BETAMX(1) 0.476E-02 0.124E-01 0.229E-01 0.349E-01 0.401E-01	Isoidal Steer 2 ETAMX(1) I 0.415E-02 0.123E-01 0.256E-01 0.256E-01
Trap	BETDMX(1) 0.952E-02 0.143E-01 0.212E-01 0.297E-01 0.404E-01 0.599E-01	DEL(Sinu 9.71 7.64 5.84 4.79 4.29 4.29	Sinu DEL(1) B 8.74 17.7 27.1 27.1
	<pre>1) BETAMX(1) 0.416E-02 0.645E-02 0.176E-01 0.251E-01 0.391E-01</pre>) AYMAX.(1) 0.123 0.229 0.319 0.411) AYMAX.(1) 1 0.157 0.294 0.405
	STR4. (180. 240. 360. 420. 550.	STR5(120. 240. 360. 540. 540.	STR5(120. 240. 480.

Figure F.5. Unloaded heavy bus, V₀ = 30 mph, tire code: HBl.

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	PHIMAX(2.63	3.90	5.10	6.24	7.11	12.5	- - - -	1.87	3.48	4.81	5.89	6.74
	F 01						-					
	RMAX. (0.935E	0.140	0.187	0.237	0.276	0.333		50.0	50.0	50.0	50.0	50.0
	AYMAX.(1) 0.211	0.314	0.413	0.510	0.587	0.656	DEL PST (1)	0.335E-02	0.287E-02	0.160E-03	-0.554E-02	-0.140E-01
oidal Steer	CUVRAT(1) 0.676E-01	0.979E-01	0.126	0.151	0.175	0.195	oidal Steer]	0.113E-01	0.240E-01	0.381E-01	0.534E-01	0.691E-01
Trape	BETDMX(1) 0.149E-01	0.234E-01	0.320E-01	0.416E-01	0.520E-01	0.618E-01	Sinus Sinus	9.56	7.33	5.44	5,62	6.59
	1) BETAMX(1) 0.158E-01	0.257E-01	0.368E-01	0.488E-01	0.620E-01	0.758E-01	1 1 AYMAX.(1 1	0.112	0.207	0.268	0.353	0.401
	STR4(60.0	0°0' 60'	120.	150.	180.	210.	STRS	60.0	120.	180.	240.	300.

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1 PHTMAXI	2.14 3.93 7.75 9.48 48 48
	00000 00000 00000
	0.648E-02 0.685E-02 0.608E-02 0.663E-02 0.663E-02 -02 -02
Sinusoidal Steer 2	0.136 0.149 0.347 0.347 0.347 0.347 0.146 0.130
	11 DEL
	1) AYMAX.(0.166 0.307 0.425 0.516 0.591
	STR5(60.0 120. 120. 240. 300.

Figure F.6. Unloaded heavy bus, $V_0 = 50 \text{ mph}$, tire code: HBl.

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	2	÷. Ę	Ę
•	1) PHIMAX(3.65 4.75 5.77 6.67 8.32 8.32	1) PHIMAX(3.13 5.42 6.96 8.36 8.36	1) FHIMAX(2.53 4.67 6.25 7.55 8.17
	RMAX(0.166 0.219 0.256 0.313 0.390 0.390	UIN(30.0 30.0 30.0 30.0 30.0	UIN(30.05 30.05 30.05 30.05
	AYMAX.(AYMAX.(0.226 0.357 0.357 0.412 0.460 0.505	DELPSI(1) 0.442E-02 0.442E-02 0.670E-02 0.677E-02 0.677E-02	DELPSI(1) 0.228E-02 0.381E-02 0.848E-02 0.150E-01 0.156E-01
idal Steer	CUVRAT(0.262 0.340 0.412 0.472 0.533 0.593	dal Steer 1 BETAMX(1) 0.577E-02 0.682E-02 0.107E-01 0.197E-01 0.281E-01	idal Steer 2 BETAMX(1) 0.453E-02 0.790E-02 0.121E-01 0.267E-01 0.315E-01
Trapezo	BETDMX(1) 0.831E-02 0.866E-02 0.141E-01 0.223E-01 0.325E-01 0.418E-01	DEL(Sinusoi 9.99 8.03 6.34 4.99 4.54	Sinuso DEL(1)] 7.78 14.8 22.9 29.7 32.3
	1) BETAMX(1) 0.528E-02 0.574E-02 0.593E-02 0.593E-02 0.164E-01 0.164E-01	1) AYMAX.(1) 0.141 0.236 0.358 0.358	1) AYMAX.(1) 0.145 0.273 0.376 0.458 0.468
	STR4. (160. 240. 300. 360. 420.	STR5(120. 240. 360. 540.	STR5. (120. 240. 360. 540.

Figure F.7. Loaded heavy bus, $V_0 = 30$ mph, tire code: HB1.

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	PHIMAX(14 N I	5.00 	4.80	5.83	6.6B		PHIMAX(2.13	4.10	5.67	6.94	7.97		DHTMAX(2.29	4.21	4.5		200	
	-	0						Ŧ							1 1	-					
	RMAX. (0.684E	0.103	0.137	0.168	0.198		UIN(0.02	50.0	50.0	50.0	50.0		ITN C		0.0r				0.00
	1)							,	M0-	-04	N 0-	-01	-01				10				Ģ
	AYMAX.(0.152	0.229	0.300	0.362	0.415		DELPSI (0.173E	-0.886E	-0.327E	-0.116E	-0.260E		1 1 1 1 1 1 1 1 1	DELFAIN	0 0 4 5 F -		0.137E-		-0,330E-
eer	-	E-01	E-01			_	er 1	(N0 -00	10-	-01	10-	01	0 1				-	- 0-	- - -	0
sezoidal St	CUVRATI	0.572	0.839	0.108	0.131	0.110	usoidal Ste	BETAMX (0.7835	0.1816	0.3146	0.461E	0.606F	Cto Cto		BETAMX(0.437E	0.6725	0.968E
Traf	1)	E-02	E-01	E-01		50	Sin	1)								-					
	BETDMX(0.964	0.156	0.226	002.0			DEL (10.1	8.25	6.53	5.07	5.20	·)EL(8.3/	15.4	24.1	32.0	38.4
	1)	-02	10-	0		50		1)								1)]					
	1) BETAMX(0.9586	0.166F			0.470		1) AYMAX.(0.106	0.199	0.270	0.321	0.362			I) AYMAX.(0.138	0.262	0.371	0.459	0.552
	STR4(6.64				, 00, 1 , 00, 1		STR5(60.0	120.	180.	240.	300.			STR5(60.03	120.	180.	240.	300.

Figure F.8. Loaded heavy bus, V₀ = 50 mph, tire code: HBl.

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		Trape	zoidal Steer				
TR4(1) BETAMX(1)	BETDMX(1)	CUVRAT (1) AYMAX.(1) RMAX(1) PHIMAX(-
180.	0.663E-02	0.124E-01	0.271	0.262	0.193	3.31	
240.	0.116E-01	0.184E-01	0.352	0.343	0.255	4.29	
300.	0.177E-01	0.264E-01	0.427	0.416	0.316	5.18	
360.	0.250E-01	0.344E-01	0.497	0.483	0.377	6.01	
420.	0.331E-01	0.449E-01	0.560	0.539	0.429	6.64	
480.	0.406E-01	0.573E-01	0.617	0.607	0.482	7.25	
540.	0.467E-01	0.641E-01	0.667	0.642	0.530	10.2	

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PHIMAX(C8.2	2.42	6.26	6.84
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UIN(30.0	30.0	30.0	30.0
÷.		N 0 1	0	-0-	-01
DELPSI(100+ · A	0.738E	0.112E	0.162E	0.2005
÷.	N D	-01	-01	-01	-01
BETAMX(0 041E	0.157E-	0.274E	0.397E	0.502E
1)					
1) DEL[61.4	7.78	6.06	4.90	5.00
1) AYMAX.(0.115	0.214	0.298	0.363	0.406
STR5(120.	240.	360.	480.	600.

	,					
	1) FHIMAX(2.00	3.66	4.98	6.01	6.95
)NIU	30.0	30.0	30.0	30.0	30.0
	DELFSI(1) (0.653E-02	0.955E-02	0.171E-01	0.279E-01	0.374E-01
Sinusoidal Steer 2	BETAMX(1)	0.602E-02	0.168E-01	0.326E-01	0.521E-01	0.716E-01
	1) DEL(1	6.77	17.3	26.5	33.9	36.8
	1) AYMAX.(0.150	0.280	0.386	0.471	0.532
	STR5(120.	240.	360.	480.	600.

Figure F.9. Unloaded heavy bus, $V_0 = 30$ mph, tire code: HB2.

		Tra	pezoidal Steer			
STR4. (1) BETAMX(1)	BETDMX(1)	CUVRAT(1)	AYMAX.(1) FMAX(1) F	PHIMAX(
6.02	0.178E-01	0.164E-01	0.632E-01	0.207	0.920E-01	2.59
120.	0.404E-01	0.351E-01	0.117	0.408	0.186	N 0 . 1
180.	0.664E-01	0.563E-01	0.163	0.573	0.276	1.02
240.	0.946E-01	0.801E-01	0.200	0.744	0.384	13.0
300.	0.122	0.115	0.228	0.872	0.438	0.51
360.	0.147	0.140	0.249	0.823	0.454	1.51

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1) PHIMAX(1.69	3.16		4.50	5.40	6.20	6.03	7.29	7.60	7.79
UIN(50.0	0.05		0.02	50.0	50.0	50.0	50.0	50.0	50.0
DELPSI(1)	0.317E-02	0 2815-02		0.292E-03	-0.513E-02	-0.136E-01	-0.260E-01	-0.454E-01	-0.712E-01	-0.971E-01
1) BETAMX(1)	0 122E-01			0.403E-01	0.557E-01	0.712E-01	0.860E-01	0.976E-01	0.107	0.115
11 DFI (5.66	5.81	6.46	7.07	7.47	7.67	7.73
1 DYMAX			9.18Y	0.263	0.325	0.373	0.409	0.441	0.468	0.486
, tos			.021	180.	000	300.	360.	420.	480.	540.

			Sinusoidal Steer 2				
STR5(1) AYMAX.(1) DEL(1) BETAMX(1)	DELFSI(1)	UIN(1) PHIMAX(-
60.0	0.157	10.5	0.168E-01	0.641E-02	50.0	2.02	
120.	0.291	20.9	0.386E-01	0.670E-02	50.0	3.70	
180.	0.402	32.3	0.657E-01	0.510E-02	50.0	5.40	
240.	0.487	43.2	0,998E-01	0.774E-02	50.0	7.07	
300.	0.555	52.5	0.136	-0.667E-02	50.0	8.60	
360.	0.643	60.9	0.186	0.465E-01	50.0	9.34	
420.	0.711	66.2	. 0.227	0.868E-01	50.0	9.78	
480.	0.729	68.5	0.252	0.855E-01	50.0	10.7	

Figure F.10. Unloaded heavy bus, $V_0 = 50$ mph, tire code: HB2.

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1) FHIMAX(3.66 4.76 5.77 6.63 8.22 8.22	1) FHIMAX(2.73 4.81 6.55 8.81	1) FHIMAX(2.40 4.44 7.35 8.42
RMAX(0.166 0.268 0.313 0.313 0.355	UIN(30.0 30.0 30.0 30.0 30.0 30.0	UIN(30.0 30.05 30.0 30.0 30.0 30.0 30.0 30.
AYMAX.[1] 0.227 0.296 0.358 0.410 0.497 0.497	DELFSI(1) 0.354E-02 0.560E-02 0.705E-02 0.690E-02 0.607E-02	DELFSI(1) 0.497E-02 0.615E-02 0.971E-02 0.138E-01 0.122E-01
oidal Steer CUVRAT(1) 0.251 0.326 0.324 0.324 0.564 0.564	idal Steer l BETAMX(1) B.361E-02 0.369E-02 0.158E-01 0.269E-01 0.391E-01	idal Steer 2 BETAMX(1) 0.306E-02 0.735E-02 0.207E-01 0.381E-01 0.500E-01
Trapeze BETDMX(1) BETDMX(1) 0.607E-02 0.195E-01 0.278E-01 0.286E-01 0.504E-01	Sinuso DEL(1) 10.0 8.11 6.47 5.17 4.65	Sinuso DEL(1) 7.97 14.8 22.8 22.8 24.1
 BETAMX(BETAMX(2966E-02 5666E-02 1596E-02 1596E-02 1596E-02 3456-01 	1) AYMAX.(0.124 0.222 0.226 0.394 0.394	1) AYMAX.(1) 0.140 0.264 0.363 0.441 0.495
STR4(180. 240. 360. 420. 480.	STR5(240. 240. 360. 600.	STR5. (120. 240. 360. 480. 600.

Figure F.ll. Loaded heavy bus, V₀ = 30 mph, tire ccde: HB2.

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				Trape	zoidal Steer	e '				
STR4(()	BETAMX(1)	BETDMX(1)	CUVRATI	1)	AYMAX.(1)	RMAX(1) FHIMAX(+
60.0		0.121E-01	0.118	E-01	0.541E-	01	0.152	0.680E	-01 2.4	~
90.0		0.202E-01	0.186	E-01	0.793E-	01	0.227	0.102	3.6	~
120.		0.303E-01	0.264	E-01	0.102		0.297	0.136	4.7	~
150.		0.416E-01	0.357	E-01	0.123		0.359	0.168	5.7	
180.		0.536E-01	0.457	E01	0.142		0.414	0.198	6.6	
219.		0.662E-01	0.561	E-01	0.159		0.460	0.225	7.4	~
•				Sinus	oidal Steer	·)
CTR5	1	AYMAX.(1)) DEL((t	BETAMX(()	DELFSI(1) UIN(1) FHIMAX(-
0.07	•	0.977F-01	10.5	~	0.8986-	20	0.182E-0	2 50.0	1.9	M
					0.202E-	-01	0.182E-0	2 50.0	3.7	រា
		0.055	6.76		0.340E-	-01	-0.112E-0	2 50.0		01
240.		0.302	1.20		0.491E-	-01	-0.885E-0	2 50.0	6.4	Ŋ
300.		0.340	5.34	. +	0.643E-	-01	-0.221E-0	1 50.0	7.4	~ -

Figure F.12. Loaded heavy bus, V_o = 50 mph, tire code: HB2.

3.99 5.91 7.75 9.36 2.15)ELFSI(1) UIN...(0.350E-02 50.0 0.352E-02 50.0 0.221E-03 50.0 -0.940E-02 50.0 0.277E-01 0.499E-01 0.764E-01 0.113E-01 0.114 8.50 15.1 23.6 37.8 1) AYMAX.(0.131 0.250 0.352 0.439 0.574 STR5..(60.0 120. 180. 240. 300.

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1) FHIMAX(

1) DELFSI(

Sinusoidal Steer 2

1) BETAMX(

1) DEL...(

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HEAVY TRUCK SIMULATION RESULTS

SIR4. (1) BETAMX(1)	BETDMX(1)	CUVRAT (1) AYMAX.(1) RMAX(1) FHIMAX(
0.09	0.971E-02	0.126E-01	0.231	0.182	0.133	0.47
120.	0.125E-01	0.159E-01	0.306	0.241	0.177	97.0
150.	0.151E-01	0.1966-01	0.381	0.300	0.221	0.94
180.	0.175E-01	0.231E-01	0.455	0.358	0.265	
210.	0.197E-01	0.271E-01	0.529	0.415	0.309	
240.	0.216E-01	0.305E-01	0.601	0.472	0.354	1.41
270.	0.232E-01	0.342E-01	0.673	0.536	0.469	- ,
300.	0.245E-01	0.380E-01	0.745	0.593	0.459	1.8

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UIN	30.0	30.0	0.00	30.0	30.0
(j	20-03	5E-02	6E-02	2E02	2E02
DELPSI(0.139	0.155	0.166	0.177	0.167
()	E-02	E-01	E-01	E01	E-01
BETAMX (0.703	0.137	0.203	0.267	0.332
ĺ					
) DEL(10.3	8.64	7.02	5.47	4,02
	-m		ି		×
AYMAX.(0.10	0.25	0.31	040	0.48
ĺ					
STR5(60.0	120.	180.	240.	300.

Sinusoidal Steer 2

()					
UIN(30.0	30.0	30.0	30.0	30.0
ELPSIC () (0.230E-02	0.2546-02	0.388E-02	0.7456-02	0.6866-02
1.1 BETANX(() L	0,001E-02	0.126E-01	0.161E-01	0.236E-01	0.2666-01
1)))E	10.6	6.27	/ C. /	10.8	14.1
1.) AYMAX.(0.115	0.224	0.330	0.427	0.512
STR5 (60.0	120.	180.	240.	300.

Figure F.13. Unloaded heavy truck, $V_0 = 30$ mph, tire code: HT1.

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()	I BETAMX(;	BETDMX1	(CUVKAII 1	AYMAX.(1) RMAX	())	FHIMAX(
Ģ	0.518E-	02	0.7046-	00	0 . 468E01	0.112	0	.527E-01	0.368
0	0.832E-	0 0	0.111E-	10.	0.730E-01	0.176	0	.7946-01	0.556
0	0.117E-	01	0.155E-	10.	0.965E-01	0.232	0	.106	0.733
ৃ	0.157E-	01	0.201E-	01	0.120	0.289	0	.133	0.911
0	0.201E-	61	0.251E-	10.	0.143	0.346	0	.159	1.09
4	0.253E-	01	0.306E-	٠O.	0.166	0.404	0	.186	1.27

	2
	9.90.00
	200 200 200 200 200 200 200 200 200 200
	DELPSI(-0.56 -0.55 -0.55
er l	K(1) 584E-02 23E-01 95E-01 79E-01 74E-01
usoidal Stee	1) BETANY 0.5 0.3 0.2 0.2
Sin	DEL(10.5 8.97 7.47 5.99 4.54
	1) AYMAX.(1) 0.892E-01 0.175 0.335 0.335 0.408
	20.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0

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		0	0	0	0	0
	UIN(50.	50.	50.	50.	50.
	DELPSIC ()	-0.401E-03	-0.131E-03	0.186E-03	0.170E-03	-0.910E-03
usoidal Steer 2	1) BETAMX(1)	0.5626-02	0.121E-01	0.1986-01	0.291E-01	0.41.66-01
Sin	() DEL(7.09	7.44	10.5	13.6
	1) AYMAX.(0.103	0.201	0.298	0.389	0.470
	STR5(30 ° 0	60.09	90.0	120.	150.

Figure F.14. Unloaded heavy truck, V₀^{`=} 50 mph, tire code: HTl.

) KMAX(1) PHIMAX(2.500 - 2.60	0.000 0.4200 0.4200 0.4200 0.420000000000
AYMAX.(1	00000000000000000000000000000000000000
AT(1)	NNANAN NANNA NNAA NNAA NNAA NNAA NNAA
CUVR	000000
BETDMX(()	0.195E-01 0.288E-01 0.406E-01 0.555E-01 0.721E-01
() BETAMX(()	0.185E-01 0.298E-01 0.456E-01 0.659E-01 0.987E-01
STR4(9 9 9 - 9 9

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BETAM
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UIN	30	30	30	99	30
()	10-377	<i>б</i> 0н01	07E02	196 - 90 C	Atz
DELPSI	0.1	0.1	~ • •	9 ° 9	0 × 1
	356-01	506-01	4.0 E Ü 1	27.6	
I V AGI AMXI	9.1.6	0 . 24	v (C, v (c)	9.1.6	
DEL	i ~ ~ i	1 A . A	「「「」」、「」、「」、「」、「」、「」、「」、「」、「」、「」、「」、「」、「	ti e te div	0 × 4 4
(ļ			<u>~</u> ~	j.	
Jan Maria A	0.12	0.24	0,35	$\phi \sim 4 \phi$	9 . U 4
STR5(60°09	120.	180.	240.	.00.

Figure F.15. Loaded heavy truck, V₀ = 30 mph, tire code: HTl.

РНІМАХ (5.23	3.56	J.36		15.0	15.1
() KMAX. (0.698E-01	0.116	0.189	0, 51 L	0.405	0.429
АҮМАХ.(0.156	0.253	0.382	0.000	0.627	0.640
си тимила	0.505E-01	0.741E-01	0.9706-01	01 (1 V	0.139	0.158
BETDMX())	V.160E-01	0.2546-01	0.3626-01	0.44.55	0.656E-0)	0.990E-01
1) BETAMX(1)	0.1/4E-01	0.295E-01	0.451E-01	0.648E-01	0.884E-01	0.110
STR4(0.04 0.04	0.00	0.00	70 ° 0	

Trapezoidal Steer

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Sinusoidal Steer l

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,					
UIN(50.0	0.01	50.0	20.0	50.0
DELPSI(1)	0.501E-02	0.654E-02	-0.140E-02	0.6746-03	0.344E-01
1) BETANX 1)	0.130E-01	0.276E-01	0.4006-01	0.671E-01	0.952E-01
DÉLI	10.2	. 8.42	ů. ů.	л , 68	7.60
() AYMAX.())	0.936E-01	0.177	0.253	0.325	0.392
STR5(50.05	60.0	9.09	120.	150.

Sinusoidal Steer 2

· -					
UIN	50.0	50.0	50.0	50.0	50.0
()	NO-3	E-01	E-02		
DELPSIC	0.939	0.108	-0.483	0.183	0.733
Ĵ	10.1∃	:-01	:-01		
BETHMX (0 . 1 ô 1 j	0.3861	0.7621	0.148	0.263
ļ					
DELI	₩0 * A) Ó . 4	28.7	άvộ	67.3
()					
1.1 AYMAX.(0.128	0.252	0.375	0.496	0.595
STRS(30.0	60.00	90.00	120.	150.

Figure F.16. Loaded heavy truck, V₀ = 50 mph, tire code: HT1.

	-												
	MAXI	0.649	0.862	1.07	1.27	1.46	1.64	1.79	2.84	4.72	6.29	Ç Ç	
	THY (1											N	00000 0000 00000 00000
	1) RMAX(0.149	0.200	0.250	0.299	0.347	0.394	0.437	0.480	0.521	0.555	LFSI(1) UI 0.186E-02 0.210E-02 0.229E-02 0.229E-02 0.229E-02 0.229E-02 0.229E-02 0.229E-02	0.277E-02 0.340E-02 0.463E-02 0.628E-02 0.938E-02
	1) AYMAX.(0.204	0.273	0.040	0.404	0.465	0.524	0.575	0.619	0.654	0.676	1 TAMX(1) DE 0.793E-02 0.793E-02 0.295E-01 0.205E-01 00	0.747E-02 0.142E-01 0.201E-01 0.256E-01 0.312E-01
zoidal Steer	CUVRATI	0.258	0.343	0.428	0.510	0~200	0.668	0.743	0.813	0.875	0,932	oidal Steer	
Trape	TDMX(1)	0.151E-01	0.173E-01	0.221E-01	0.260E-01	$\Theta = \mathcal{S} \Theta \mathcal{A} \Theta = \Theta \mathcal{A}$	0.342E-01	0.382E-01	0.420E-01	0.461E-01	0.500E-01	Sinus Sinus Sinu	
	AMX(1) BE	0.108E-01	0.139E-01	0.167E-01	0.192E-01	0.212E-01	0.231E-01	0.246E-01	0.258E-01	0.268E-01	0.277E-01	1) AYMAX.(0.2350 0.2350 0.445 0.442	
	(1) BET	.0	0.	0.	0.	0 .	0.	0 .	0.	0.	0.	STR5(60.0 120. 300. 300.	STR51 60.0 120. 240. 200.
	STR4	96	, N	<u>ح</u>	18	2	ন থ	27	30	33	. 36		

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Figure F.17. Unloaded heavy truck, V₀ = 30 mph, tire code: HT2.

		Trapezo	idal Steer				
30.0 1 1 1	96160X(1) 9 0.646E-02 2.535	6.895E-02	UVKALL 11 0.587E-01	АҮМАХ.(0.147	1 KAAX.		FH1MAX(0.457
40.0	0.106E-01	0.134E-01	0.882E-01	0.219		.978E-01	0.694
60.00	0.157E-01	0.189E-01	0.117	0.296	0.	.132	0.438
75.0	0.213E-01	0.254E-01	0.146	0.369	0	166	1.17
90.0	0.276E-01	0.3266-01	0.173	0.436	.0	198	1.37
105.	0.349E-01	0.3976-01	0.199	0.499	0.	229	1.57
120.	0.427E-01	0.466E-01	0.223	0.558	0	259	
135.	0.498E-01	0.545£-01	0.246	0.605	0.	268	1.97
STR5(30.0 60.0 90.0 120.	1) AYMAX.(0.106 0.209 0.325 0.375 0.473	1) DEL(10.DEL(10.1 10.28 5.28 5.28 5.28	dal Steer 1 1) BETAMX(0.66(0.23(0.333) 0.333	1) DELI 9E-02 9E-01 9E-01 10-10 10-01 10-01 10-01	FSI(1) 0.757E-03 0.118E-02 0.156E-02 0.346E-03 0.304E-03	999999 999999 999999 999999 99999 99999 9999	
		Sinusoi	dal Steer 2				
21KD.1 30.0	1) AYMAX.(0.125	1) DEL(10.2	1) BETAMX(0.45	1) DEL	PSI(1)	UIN(()
60.0	0.246						
90.0					0.18ZE-0Z	50.6	
120.	0.464		V.V.	6E01	0.273E-02	0.0 .0	
150.	0.551				A VALETON	9 4 9 4 9 4 9 4 9 4 9 4 9 4 9 4 9 4 9 4	
			14 9 m 4 - 14		0 * / 1 7 E	0 * 0 C	

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Figure F.18. Unloaded heavy truck, V₀ = 50 mph, tire code: HT2.

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		Tra	apezoidal Stu	eer			
STR4. (1) BETAMX(1)	BETDMX(1)	CUVRATI	1) AYMAX.(1) KMAX. (1) PHIMAX(Ĵ
90.09	0.105E-01	0.124E-01	0.234	0.215	0.158	3.10	
120.	0.196E-01	0.200E-01	0.312	0.301	0.224	4.32	
150.	0.341E-01	0.323E-01	0.387	0.398	0.303	5.67	
180.	0.543E-01	0.479E-01	0.460	0.493	0.394	6.93	
210.	0.805E-01	0.659E-01	0.528	0.570	0.466	7.80	
240.	0.111	0.926E-01	0.590	0.601	0.537	15.1	
270.	0.142	0.124	0.646	0.615	0.577	15.1	
300.	0.174	0.156	0.694	0.624	0.612	15.1	

Sinusoidal Steer 1

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FHIMAX(1.16	2.51	4.95	6.85	8.04
;					
UINI	30.0	30.0	30.0	30.0	30.0
; ;	-05	-07	10-	10-	0-
DELPSI(0 . ò 4 ∠it	0.118E	-0.1186	-0.209E	-0.1946
(l		10-	10	10-	10-
BE FAMA (r	0.1656	0.3546	0 × 5 6 2 E	0.6326
()					
1) DEL(8.39	¢*23	4.74	6.05
1) AYMAX.($\tilde{W} + 1 W \tilde{W}$	0.230	0.349	0.421	0.462
STR5I	60°09	120.	180.	240.	.000

Sinusoidal Steer 2

-					
1) FHIMAX(1.60	3.21	5.10	6.73	8.33
UIN(30.0	30.0	30.0	30.0	30.0
DELPSI(()	0.110E-01	0.113E-01	0.7286-02	0.373E-01	0.144
BELANX(1)	0,653E-02	0.177E-01	0.4386-01	0.VZ6E-01	. 0.158
1) DEL(1)	8,22	14.5	24.5	6 . 0	46.9
1) AYMAX.(0.131	0.258	0.384	0.492	0.576
STR5(60.09	120.	180.	240.	300.

Figure F.19. Loaded heavy truck, V₀ = 30 mph, tire code: HT2.

STR4 (36.0 40.0 60.0 100.0 100.0 100.0	1) BETAMX(1) 0.122E-01 0.214E-01 0.254E-01 0.369E-01 0.841E-01 0.115	BETDMX(1) 0.1236-01 0.1966-01 0.2816-01 0.4166-01 0.7056-01 0.112	CUVRA1(1) 0.136E-01 0.196 0.132 0.155 0.172	AYMAX.(0.15 0.15 0.420 0.420 0.625 0.631 0.631) KMAX(1) 0.674E-01 0.118 0.210 0.337 0.332 0.392 0.415	FH1MAX(2 2 5 5 5 5 5 5	~
STR5(30.0 60.0 120.	1) AYMAX.(1) 0.103 0.201 0.302 0.377 0.448	Si DEL(51 8.35 6.21 9.03	nusoidal Steer 1 BETAMX(1) 0.112E-01 0.239E-01 0.404E-01 0.4654E-01 0.9656E-01	DELPSI(1) 0.467E-02 0.182E-02 -0.117E-01 -0.561E-02 0.660E-01	UTN(0.02 0.02 0.02 0.02 0.02 0.02 0.02	FHIMAX(1.06 5.11 5.28 5.78 5.78	1 2

Figure F.20. Loaded heavy truck, $V_0 = 50 \text{ mph}$, tire code: HT2.

1.64 3.40 5.86 7.40 15.1 1) FHIMAX(JELFXII 1] UIN...(0.798E-02 50.0 0.602E-02 50.0 -0.319E-01 50.0 0.221 50.0 1) GETAMAI ().DELPSI(0.120E-01 0.307E-01 Sinusoidal Steer 2 0-34C/*0 0.157 0.264 16.6 32.0 56.3 6.ê2 8.73 1) DEL....(0.133 0.268 0.425 0.554 0.622 () AYMAX.(30.0 60.09 9.04 120. 150. STR5..(

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		Traj	oezoidal Stee	4		
STR4 (1) BETAMX(1)	BETDMX(1)	CUVRATI	1) AYMAX.(1) KMAX(1) PHIMAX(
90.09	0.112E-01	0.124E-01	0.243	0.193	0.139	0.606
120.	0.145E-01	0.170E-01	0.324	0.255	0.186	0.809
150.	0.176E-01	0.213E-01	0.405	0.319	0.234	1.01
180.	0.203E-01	0.254E-01	0.463	0.380	0.279	1.19
210.	0.227E-01	0.311E-01	0.560	0.438	0.324	1.37
240.	0.247E-01	0.335E-01	0.634	0.494	0.368	1.54
270.	0.265E-01	0.374E-01	0.706	0.545	0.410	1.70
300.	0.280E-01	0.414E-01	0.774	. 0.591	0.446	1.84
330.	0.292E-01	0.454E-01	0.837	0.625	0.486	3.12
360.	0.302E-01	0.494E-01	0.694	0.653	0.517	4.58

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Sinusoidal Steer 1

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STR5(() AYMAX.(1) DEL(ļ	BETAMX(1)	DELPSI(1)
60.0	0.115	10.2		0.793E-02	0.180E-02
120.	0.226	8.45		0.154E-01	0.228E-02
100.	0.332	6.70		0.2226-01	0.289E-02
240				∾ × 267E-01	0.311E-02
300.	0.511	3.94		0.350E-01	0.308E-02

Sinusoidal Steer 2

DELPSI(1)	0.278E-02 0.333E-02 0.419E-02 0.555E-02 0.793E-02
()	0.00 0.00 0.00 0.00
BETAMX(0.761E 0.166E 0.208E 0.262E 0.315E
ĺ	
1) DEL(0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0
1) AYMAX.(0.120 0.238 0.353 0.453 0.154
VTP5	200. 200. 200. 200.

Figure F.21. Unloaded heavy truck, V_Q = 30 mph, tire code: HT3.

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Sinusoidal Steer 1

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()	<u>.</u> 03-	-05	0 0 1	00 	-03
DELPSI(0.566E	0.149E	0.187E	0.131E	-0.392E
()	0	-01	-01	10-	10-
BETAMX (0.522E	0.113E	0.1856	0.269E	0.359E
()					
)EL(10.4	8.67	6.96	5.32	4.51
1) 1	01				
АҮМАХ.(0.966E-	0.192	0.285	0.374	0.447
Ĵ					
STR5(30.0	60.09	90.09	120.	150.

Sinusoidal Steer 2

()	48E-02	416-02	60E-02	32E-02	13E-02	
DELPSI	0.1	ି ତ	ି ତ	ିଂତ	0.2	
í í	~0~-	10-	01	10	۰۰. 0 (
BETAMX(0.4666	0.1116	0.1916	0.2806	0.3846	
()						
DEL I	10.9	ó.26	6.40	11.8	15.3	
ļ						
1) AYMAX.(0.100	0.220	0.331	0.427	0.512	
STR5(30.0	60.0	0.09	120.	150.	

Figure F.22. Unloaded heavy truck, $V_0 = 50$ mph, tire code: 13.

T

	()	•										()	•									()						
	1 PHIMAXI	2.70	3.77	4 98	ó.17	7.13	7.81	15.1	15.0			I DHTMAX(4 4 4 ° O	2.04	4.38	2. 4.6					() PHIMAX(1.43	2.87	4.56	6.22	7.76	
	RMAX I	0.138	0.194	W = 261	409×0	0.411	0.469	0.544	0.582			1 1 1 1		30.0	30.0	30.0		00.00	50 . 0			UIN(30.0	30.0	30.0	30.0	30.0	
	AVMAX ())	0.188	0.263	© . 347	0.452	0.509	0.569	0.596	0.609				ſ -	0.6226-02	0,652E-02	-0-3XAF-02		-0.137E-01	-0.1656-01			DELPSI(1)	0.152E-01	0.1826-01	0.586E-02	0.144E-01	0.690E-01	
oidal Steer	CINEATI (6.270 	0.261	w. 353	O = A Z Z	0,467	0.547	0.601	0.049		idal Steer l		BETANXU	v, oy/E-02			V. JVAETVI	0.525E-01	0.758E-01		idal Steer 2	BETAMX(1)	0,5766-02	0.144E-01	0.348E-01	0.7286-01	0°1°0	
Trapez	DETINNY ())	DE LUNAL 13	0.1546-01	V - 268cm V I	0.400E-01	0.558E-01	0.746E-01	0.994E-01	0.128		Sinuso		$\mathbf{DEL} : \cdot \cdot \cdot (1)$	10 10 10			> 0	2×5 1	5,33		Sinuso	DEL(()	9.15	12.7	21.0	31.3	41 × 4	
	() DETAMVI ()	1) DETHIA(1) 0.897E-02	0.150E-01	0.264E-01	0-3024.0	0.638E-01	0.8965-01	0.118	0.147				1) AYMAX.(1)		0, 20,00	0 × 204	0,324	0.202	0.476			() AYMAX.()	0.117	0.233	0.350	0.454	0,534	
	CTDA (0.09.0	120.	150.	180.	210.	240.	270.	300.	,			CTPS		60.0	120.	180.	WVC.	2009 2009			STR5I	60.05	120.	180.	240.	300.	

Figure F.23. Loaded heavy truck, V₀ = 30 mph, tire code: HT3.

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		Tr	apezoidal Steer				
84 (1) BETAMX(1)	I BETDMX()) CUVRATI 1)	H AYMAX.(() RMAX(1)	PHIMAX(
30.0	0.974E-02	2 0.980E-0	2 0.450E-01	0.118	0.525E-01	0/.1	
45.0	0.155E-01	0.155E-0	n 0.670E-01	0.180	0.803E-01	2.59	
10 20 0	0.248E-01	0.227E-0	1 0.898E-01	0.279	0.127	3.95	
75.0	0.394E-01	0.298E-0	0.113	0.413	0.203	5°.05	
90.09	0.591E-01	0.426E-0	0.136	0.538	0.291	1.42	
105.	0.820E-01	0.611E-0	4 V.156	0,602	0.372	11.8	

Sinusoidal Steer 1

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-					
J PHIMAX(0.866	1.76	3.63	1.5.1	6.81
Ļ	0	0	0	0	0
UIN(. O'I	50.	50.	50.	50.
	E-02	E 0 2	E-02	E01	<u> </u>
DELPSIL	0.445	0.429	-0.789	-0.207	-0.176
į	:0 <i>`</i> 5	0 (10-	10	10-
BELENXI	0.9876	0.2096	0.3576	9575Y0	0.7668
-					
DEL	10.5	9.05	7.58	1. 5¢	6, 30
ļ	0.				
1 J AYMAX.(0.859E	0.172	0.281	0.354	0.409
	30.0	60.00	0.04	120.	.00

	~					
	1) FHIMAX(1.31	2.70	4.78	6.71	7.99
	11N(50.0	50.0	50.0	50.0	50.0
		0.642E-02	0.954E-02	-0.165E-01		0.109
Sinusoidal Steer 2	()	0,967E-02	0.220E-01	0,5096-01	0 - 105	0.172
	1) DEL(10.2	12.1	21.5	36.5	54.7
	1) AYMAX.(0.107	0.217	0.357	0.463	0.557
	STR5(30.0	60.09	90.09	120.	150.

Figure F.24. Loaded heavy truck, V₀ [≜] 50 mph, tire code: HT3.

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LIGHT VAN SIMULATION RESULTS

		1	apezoidal Steer				
STR4. (A	1) BETAMX(1)	BETDMX(1) CUVRATE ()	AYMAX.(1)	RMAX	1) PHIMAX(o 1	C
66.70	0.909E-02	0.175E-0	1 0.181	0.177	0.130	1.62	
88.9	0.143E-01	0.232E-0	1 0.266	0.254	0.188	2.43	
111.	0.202E-01	0.281E-0	1 0.348	0.325	0.242	3.16	
133.	0.277E-01	0.328E-0	1 0.428	0.396	0.298	3.85	
156.	0.371E-01	0.393E-0	1 0,507	0.465	0.354	4. 5N	
178.	0.484E-01	0.492E-0	1 0.583	0.534	0.412	5.17	
200.	0.629E-01	0.619E-0	1 0.656	0.608	0.484	5.83	
222.	0.822E-01	0.760E-0	1 0.727	0,700	0.618	6.58	
•							
							K
		S	inusoidal Steer l				
STR5(1) AYMAX.(1)	DEL(() BETAMX(1)	DELFSI(1)	UIN(1) PHIMAX(1)
44.4	0.646E-01	11.0	0.487E-02	0.732E-02	30.0	0.237	
4 88 4 88	0.1/4	- 8. 8. 9.	0.1XXE-01		- O - O	2 04	
178.	0.377	4.92	0.347E-01	0.497E-01	30.0	4.17	
NNN 1	0.460	5.23	0.499E-01	0.493E-01	30.0	5.12	
			Sinusoidal Steer	2			
STR5(1) AYMAX.(1)	DELAAI	1) BETAMX(1)	DELPSI(1)		1) PHIMAX(1
- 3 - 3 - 1 - 1 - 1					0,05	0.317 1.76	
133. 133.	0.329	⊕,54	0.253E-01	0.562E-01	30.0	3.08	
178.	0.428	12.6	0.407E-01	0.610E-01	30.0	4.17	
222	0.523	16.8	0.0146-01	0,0700-01	5 () () ()		
	vo E 25 Inloaded	light van. V	$\chi = 30 \text{ mph}, \text{ tire } 0$	ode: EO.			
		(

	2	-	÷.
	FHIMAX 6.341 6.23 7.23 5.49 5.49 5.49 5.49 5.49 5.49 5.49 5.49 5.49 5.49 5.49 5.49 5.49 5.49 5.49 5.40 5.4) FHIMAX(0.108 0.785 3.33 4.17	D FHIMAX(
	RMAX. (1) 0.297E-01 0.657E-01 0.112 0.153 0.197 0.251	- 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.0	LIN. 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0
	YMAX.(1) 1 0.442E-01 0.148 0.251 0.341 0.345 0.542	DELFSI(1) -0.889E-02 0.366E-01 0.435E-01 0.480E-01 0.512E-01	DELPSI(1) -0.112E-01 0.153E-01 0.210E-01 0.199E-01 0.148E-01 E0.
oidal Steer	CUVRAT(1) A 0.781E-02 0.371E-01 0.669E-01 0.964E-01 0.151 0.151	idal Steer 1 BETAMX(1) 0.414E-02 0.178E-01 0.321E-01 0.491E-01 0.678E-01	oidal Steer 2 BETAMX(1) B.437E-02 0.231E-01 0.231E-01 0.430E-01 0.661E-01 0.927E-01 0.927E-01
Trapez	BETDMX(1) 0.769E-02 0.205E-01 0.334E-01 0.454E-01 0.557E-01 0.661E-01	Sinuso DEL(1) 12.2 10.1 5.80 5.71 5.71	Sinus DEL(1) 15.8 10.9 6.93 11.4 17.0 ght van, Vo = 50
	BETAMX(1) 0.401E-02 0.153E-01 0.268E-01 0.394E-01 0.531E-01 0.686E-01	AYMAX.(1) 0.365E-01 0.121 0.221 0.316 0.400) AYMAX.(1) 0.322E-01 0.188 0.313 0.313 0.421 0.510 26. Unloaded li
	STR4(1) 22.22 33.3 33.3 66.7 66.7 77.8	STR5.(1) 22.22 44.4 66.7 88.9 111.	STR5(1 22.2 44.4 66.7 68.9 111. Figure F.

÷.	÷.	
1) PHIMAX(2019) 2014 2014 2016 2016 2016 2016 2016 2016	1) FHIMAX(3.97 6.20 7.66 8.83	1) PHIMAX(1.10 3.88 5.87 7.59 9.42
KMAX. 6 0.121 0.121 0.221 0.280 0.349 1.95 1.95 1.95	UIN(30.0 30.0 30.0 30.0	UIN(30.0 30.0 30.0 30.0 30.0 30.0 30.0
YMAX.(0.174 0.174 0.239 0.376 0.376 0.376 0.726 0.726 0.728	DELPSI(1) 0.516E-02 0.246E-01 0.379E-01 0.362E-01 0.426E-01	DELFSI(1) 0.125E-02 0.175E-01 0.392E-01 0.432E-01 0.432E-01
szoidal Steer CUVRAT (1) / 0.162 0.312 0.387 0.462 0.536 0.608 0.675	soidal Steer 1 BETAMX(1) 0.939E-02 0.233E-01 0.315E-01 0.454E-01 0.709E-01	soidal Steer 2 BETAMX(1) 0.976E-02 0.200E-01 0.323E-01 0.542E-01 0.883E-01
Trape BETDMX(1) 0.272E-01 0.341E-01 0.477E-01 0.727E-01 0.727E-01 0.727E-01 0.146	Sinu DEL(1) 9.02 7.18 5.30 5.56	Sinu DEL(1) 13.2 7.82 8.04 12.0
<pre>BETAMX(1) BETAMX(1) 0.148E-01 0.191E-01 0.245E-01 0.348E-01 0.348E-01 0.728E-01 0.728E-01 0.143</pre>) AYMAX.(1) 0.658E-01 0.200 0.314 0.361 0.462 0.462	1) AYMAX.(1) 0.909E-01 0.215 0.322 0.425
STR4.(66.7 666.7 666.7 111. 133. 133. 133. 133. 133. 133. 13	STR5(1 44.4 88.9 133. 178. 222.	STR5(1 44.4 88.9 133. 128. 222.
	124	

Figure F.27. Loaded light van, V_O = 30 mph, tire code: EO.

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	PHIMAX(0.661	2.33	3.80	5.06	6.33	10.2	10.7	10.7	
	RMAX. (1)	0.421E-01	0.683E-01	0.104	0.135	0.173	0.796	1.79	1.79	
	AYMAX.(1)	0.599E-01	0.149	0.221	0.295	0.384	0.721	0.735	0.731	
coldal Steer	CUVRAT(1)	0.304E-02	0.317E-01	0.591E-01	0.854E-01	0.110	0.135	0.160	0.184	
Trapez	BELIDMX(1)	0.112E-01	0.302E-01	0.451E-01	0.563E-01	0.663E-01	0.745E-01	0.820E-01	0.139	
	1) BETAMX(1)	0.707E-02	0.183E-01	0.263E-01	0.350E-01	0.485E-01	0.687E-01	0.965E - 01	0.132	
	STR4(22.2	33.3	44.4	52.52	66.7	77.8	88.9	100.	

	1) PHIMAX(2.70	5.68	7.19	8.06
		0.0	50.0	50.0	50.0	0.02
	DELFSI(1)	-0.692E-02	0.249E-01	0.292E-01	0.371E-01	0.469E-01
inusoidal Steer l	1) BETAMX(1)	0.707E-02	0.250E-01		0.535E-01	0.727E-01
S	DEL (12.3	10.2		6.44	5.72
) AYMAX.(1)	0 5445-01			0 77 V	0.416
	-					

	YMAX.(1) 0.646E-01 0.214	DEL(1 16.3 11.4) BETAMX(1). 0.938E-02 0.252E-01	DELFSI(1) UIN(-0.163E-01 50.0 -0.697E-02 50.0	1) FHIMAX(0.409 3.93 5.91	-
1 00 1 00	0.312 0.464 0.591	6.33 10.0 17.1 17.1 17.1	0.776E-01 0.776E-01 0.131 0 mph. tire code:	-0.127 50.0 -0.127 50.0 E0	10.2	

Figure F.28. Loaded light van, V_o = 50 mph, tire code:

125

STR5..(22.2 44.4 66.7 68.9 111.

		Trape:	zoidal Steer				
STR4(1) BETAMX(1)	BETDMX(1)	CUVRATE 11	AYMAX.(1)	RMAX(1) FHIMAX(1)
66.7	0.514E-02	0.143E-01	0.188	0.176	0.129	1.64	
88.9	0.861E-02	0.170E-01	0.277	0.255	0.188	2.48	
111.	0.131E-01	0.204E-01	0.364	0.330	0.245	3.24	•
133.	0.190E-01	0.249E-01	0.450	0.405	0.303	3.95	
156.	0.272E-01	0.306E-01	0.534	0.479	0.364	4.65	
178.	0,387E-01	0.427E-01	0.616	0.558	0.432	5.39	
200.	0.560E-01	0.574E-01	0.696	0.666	0.567	6.29	
222.	0.814E-01	0.762E-01	0.771	0.755	1.36	7.19	
		Sinus	oidal Steer 1				
STR5(44.4 88.9 133.	1) AYMAX.(1) 0.715E-01 0.193 0.309	DEL(1) 11.1 8.80 6.69	BETAMX(1) 0.367E-02 0.925E-02 0.169E-01	DELFSI(1) 0.115E-02 0.192E-01 0.384E-01	UIN(30.0 30.0	1) PHIMAX(0.240 1.88 3.51	4)
178. 222.	0.410 0.500	4.70 5.36	0.275E-01 0.432E-01	0.373E-01 0.454E-01	30.0 0	5,80 5,80	
		Sinus	oidal Steer 2				
STR5(44.4 88.9	1) AYMAX.(1) 0.833E-01 0.222	DEL(1)	BETAMX(1) 0.365E-02 0.939E-02	DELPSI(1) 0.161E-02 0.169E-01	20.0	1) PHIMAX(0.333	1)
133. 178.	0.348 0.455	8.61 12.9	0.184E-01 0.322E-01	0.417E-01 0.485E-01	30.0	3.31 4.48	
222.	0.554	17.9	0.541E-01	0.694E-01	30.0	5.67	
Figure	F.29. Unloaded ligh	it van, $V_0 = .30$	mph, tire code:	El.			

	2	Ę	2
	FHIMAX(0.341 1.26 1.2) PHIMAX(5.21 5.00 5.00 5.00) FHIMAX(6.133 1.53 3.02 4.42 5.64
	KMAX. (0.256 0.6566 0.6566 0.157 0.152 0.750 0.9750 0.9750 0.9750 0.9750 0.9750	UIN. 50.0 50.0 50.0 50.0 50.0 50.0	, 00000 00000 00000 00000 000000
	AYMAX. (1) 0.447E-01 0.149 0.252 0.253 0.253 0.2516 0.616 0.761	DELFSI(1) -0.896E-02 0.174E-01 0.348E-01 0.348E-01 0.403E-01	DELPSI(1) -0.109E-01 0.108E-02 0.911E-02 0.731E-02
idal Steer	UVRAT(0.748E-02 0.394E-01 0.718E-01 0.164 0.164 0.162 0.162 0.162	dal Steer 1 8ETAMX(1) 0.328E-02 0.163E-01 0.295E-01 0.451E-01 0.644E-01	dal Steer 2 ETAMX(1)] 0.333E-02 0.168E-01 0.372E-01 0.578E-01 0.578E-01
Trapezo	BETDMX(1) C 0.783E-02 0.193E-01 0.309E-01 0.506E-01 0.593E-01 0.689E-01 0.689E-01 0.944E-01	DEL(Sinusoi 12.3 10.2 7.92 5.73 5.73	Sinusoi DEL(1) E 16.0 10.7 7.01 72.2 19.1
	<pre>1) BETAMX(1) 0.339E-02 0.127E-01 0.224E-01 0.337E-01 0.468E-01 0.625E-01 0.823E-01 0.108</pre>	() AYMAX.(1) 0.373E-01 0.148 0.259 0.3552 0.444) AYMAX.(1) 0.306E-01 0.193 0.334 0.453 0.555
	STR4. (22.2 33.3 33.3 55.5 55.5 56.7 56.7 56.7 56.7 56.7 56.7	STR5(22.2 44.4 66.7 88.9 111.	STR5(22.2 44.4 66.7 88.9 111.

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Figure F.30. Unloaded light van, $V_0 = 50 \text{ mph}$, tire code:

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1) FHIMAX(2.86 4.19 5.41 5.62	8.7 40.7 10.1
1) RMAX(0.119 0.172 0.232 0.232	4.44 1.77 1.81
1) AYMAX.(0.173 0.243 0.315 0.411	0.678 0.678 0.680
CUVRAT(0.175 0.256 0.337 0.421	0.5586 0.6586
BETDMX(1) 0.199E-01 0.254E-01 0.310E-01 0.352E-01 0.552E-01	0.810E-01 0.147
<pre>1) BETAMX(1) 0.106E-01 0.142E-01 0.194E-01 0.327E-01 0.533E-01</pre>	0.839E-01 0.127
STR4(66.7 68.9 111. 133. 156.	178. 200.

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1) FHIMAX(0.778	4.47	6.78	8,41	9.58
UIN(30.0	30.0	30.0	30.0	30.0
DELPSI(1)	0.449E-02	0.140E-01	0.212E-01	0.297E-01	0.546E-01
BETAMX(1)	$\Sigma $ () and () $\Sigma $	0.192E-01	0.288E-01	0.431E-01	0.734E-01
() DEL(1)	01 11	9.01	7.09	4.86	6.14
1) AYMAX.(0.7336-	0.219	0.348	0.437	0.489
STR5(44.4	88.9	133.	178.	. 222.

128

Sinusoidal Steer 2

-					
1) PHIMAX(1.14	3.98	6.16	8.21	10.4
UIN(30.0	30.0	30.0	30.0	30.0
()) ISJ.	-0.324E-02	0.360E-02	0.275E-01	0.395E-01	0.111
). DEI	N		<i>.</i>	, ,	
BETAMX(1	0.711E-0	0.151E-0	0.280E-0	0.530E-0	0.103
1)					
DEL(13.2	7.76	8.23	13.2	20.4
1) AYMAX.(1)	0.926E-01	0.222	0.338	0.461	0.571
STR5(44.4	88 . 9	133.	178.	222.

Figure F.31. Loaded light van, V₀ = 30[°]mph, tire code: El.

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FHIMAX(0.557	2.19	3.75	5.33	9.88	10.2	
RMAX(1)	0.307E-01	0.642E-01	0.983E-01	0.136	0.719	1.67	
AYMAX.(1)	0.492E-01	0.143	0.219	0.309	0.673	0.685	
CUVRAT(1)	0.765E-02	0.384E-01	0.674E-01	0.965E-01	0.126	0.155	
BETDMX(1)	0.936E-02	0.249E-01	0.371E-01	0.468E-01	0.546E-01	0.718E-01	
1) BETAMX(1)	0.493E-02	0.140E-01	0.209E-01	0.302E-01	0.501E-01	0.787E-01	
STR4(22.2	33.3	44.4	5.25	66.7	77.8	

÷	1 I I I I I	.217	5.72	5.44	3.08	9.22
	HINF (.0	1.1	J	ι.	
	UIN(1	50.0	50.0	50.0	50.0	50.0
	DELFSI(1)	-0.131E-01	-0.118E-02	0.485E-02	0.188E-01	0.336E-01
Sinusoidal Steer l	1) BETAMX(1)	0.485E-02	0.226E-01	0.366E-01	0.537E-01	0.787E-01
	DEL(12.2	10.3	8.46	6.03	6.22
	1) AYMAX.(1)	0.410E-01	0.183	0.325	0.416	0.463
	STR5(22.2	44.4	66.7	88.9	111.

2 3.75 6.30 9.10 10.4 0.269 1) PHIMAX(0.00.0 0.00.0 0.00.0 1) UIN...(-0.140E-01 -0.620E-01 0.289 -0.137E-01 -0.120E-01 1) BETAMX(1) DELPSI(Figure F.32. Loaded light van, $V_0 = 50$ mph, tire code: 0.199E-01 0.371E-01 0.921E-01 0.155 0.563E-02 11.0 6.21 11.9 15.7 30.7 1) DEL...(0.377E-01 0.203 0.338 0.531 0.577 1) AYMAX.(44.4 22,22 66.7 88.9 111. STR5..(

Sinusoidal Steer 2

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_	1) BETAMX(1)	BETDMX(;	CUVRAT (Ĵ	AYMAX.(1) KMAX(()	PHIMAX	-
	0.551E-02	0.149E	-01	0.194		0.178	0.117	~	2.91	
	0.708E-02	0.161E	-01	0.278		0.249	0.171		4.28	
	0.867E-02	0.203E	-01	0.364		0.319	0.231		5,52	
	0.156E-01	0.229E	-01	0.459		0.414	0.305		6.61	
	0.347E-01	0.421E	-01	0.556		0.556	0.433	~	<u>6.59</u>	

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Trapezoidal Steer - 50 mph

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PHIMAX(0.628	2.16	4.02	5.39	9.97	10.2
RMAX(1)	0.202E-01	0.632E-01	0.957E-01	0.134	1.14	1.67
AYMAX.(1)	0.481E-01	0.145	0.229	0.315	0.693	0.691
CUVRAT(1)	0.178E-01	0.492E-01	0.783E-01	0.111	0.147	0.183
BETDMX(1)	0.797E-02	0.227E-01	0.306E-01	0.339E-01	0.360E-01	0.883E-01
1) BETAMX(1)	0.249E - 02	0.938E-02	0.144E-01	0.185E-01	0.377E-01	0.732E-01
STR4(22.2	33.3	44.4		66.7	77.8

Figure F.33. Loaded light van, tire code: E2.

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STR4. (1) BETAMX(1.	BETDMX(1)	CUVRATI	1) AYMAX.(1] KMAX (1 J FNIMAAL
66.7	0.129E-01	0.242E-01	0.181	0.186	0.129	2.95
88.9	0.169E-01	0.290E-01	0.264	0.258	0.186	4.29
111.	0.250E-0	1 0.342E-01	0.344	0.339	0.247	79.5
1 3 3	0.399E-0	0.407E-01	0.429	0.428	0.321	6.78
156.	0.583E-0	1 0.627E-01	0.515	0.530	0.416	8.10
178.	0.856E-0	1 0.835E-01	0.596	0.703	0.742	9.96

Trapezoidal Steer - 50 mph

-						
PHIMAX(0,595	2.63	4.12	6.25	11.9	
RMAX(1)	0.321E-01	0.726E-01	0.110	0.182	/ 1.25	
1)	-01				1	
AYMAX.(0.667E	0.166	0.254	0.401	. 0.786	
()	-05	÷0;-	-01			•
CUVRAT (0.958E-	0.4256-	0.710E-	0.102	0.133	
Ĵ	-0	-01	-01	-01	-01	
BETDMX(0.125E	0.298E	0.370E	0.516E	0.616E	
()	N 0 −	-01	-01	-01	-01	
1) BETAMX(0.653E	0.174E·	0.261E	0.399E	0.611E	
STR4(22.2	33.3	44.4	in " in In	66.7	

Figure F.34. Loaded light van, tire code: E3.

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hqm
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1) FHIMAX(3.43 5.11 7.02 10.2
1) RMAX(0.154 0.228 0.367 2.48
1) AYMAX.(0.212 0.310 0.460 0.711
CUVRAT(0.193 0.283 0.373 0.464
BETDMX(1) 0.296E-01 0.392E-01 0.461E-01 0.737E-01
1) BETAMX(1) 0.184E-01 0.297E-01 0.503E-01 0.809E-01
STR4(66.7 88.9 111. 133.

Trapezoidal Steer - 50 mph

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PHIMAX(1.05 3.81 10.2
RMAX(1) 0.478E-01 0.111 1.43
AYMAX.(1) 0.984E-01 0.244 0.718
CUVRAT(1) 0.932E-02 0.452E-01 0.804E-01
BETDMX(1) 0.145E-01 0.332E-01 0.542E-01
1) BETAMX(1) 0.862E-02 0.259E-01 0.460E-01
STR4(22.2 33.3 44.4

Figure F.35. Loaded light van, tire code: E4.

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PICKUP TRUCK SIMULATION RESULTS

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1) UIN(30.	30.	30.	30.	30.	30.	
1) PHIMAX(1.73	2.41	3.01	3.59	4.16	4.69	
1) RMAX(0.169	0.225	0.282	0.339	0.399	0.460	
1) AYMAX.(0.230	0.304	0.377	0,453	0.523	0.591	
CUVRAT (0.275	0.362	0.448	0.533	0.615	0.693	
(ETDMX(1)	0.907E-02	0.124E-01	0.174E-01	0.279E-01	0.382E-01	0.469E-01	
1) BETAMX(1) B	0.275E-02	0.437E-02	0.821E-02	0.138E-01	0.215E-01	0.318E-01	
STR4(60.05	80.0	100.	120.	140.	160.	

Sinusoidal Steer 1

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1) PHIMAX(0.483	2.09	3.19	4.03	4.71
UIN(30.0	30.0	30.0	30.0	30.0
DELPSI(1)	-0.418E-03	0.177E-02	0.226E-02	0.149E-02	0.107E-02
BETAMX(1)	0.572E-02	0.106E-01	0.170E-01	0.266E-01	0.397E-01
1) DEL(1)	9.94	7.94	5.99	4.27	5.11
1) AYMAX.(0.124	0.244	0.352	0.443	0.517
STR5(40.0	80.0	120.	160.	200.

Sinusoidal Steer 2

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FHIMAX(0.679	1.99	3.10	3.92	4.74	
Ĵ						
UINI	30.0	30.0	30.0	30.0	30.0	
;	-04	201	20-	-01	-01	
DELPSI (0.107E	0.283E	0.515E	0.112E	0.257E	
Ĵ	N 0.0	¢ ₽	-01	-01	•	
BETAMX(0.405E-	0.824E-	0.157E-	0.287E-	0.484E-	
1)						
1) DEL(9.80	6.47	10.2	14.5	18.9	
) AYMAX.(0.143	0.270	0.383	0.489	0.574	
STR5(1	40.0	80.0	120.	160.	200.	

Figure F.36. Unloaded pickup truck, $V_0 = 30$ mph, tire code: F0.

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Trapezoidal Steer

۷(50.0	50.0	50.0	50.0	50.0	50.0		
IN ()								
HIMAX(1.31	2.17	3.02	3.83	4.74	6.08		
1 (1)	44E-01	26	70	20	BĠ	43		
RMAX	0.6	0.1	0.1	0.0	0.2	0. U		
1								
AYMAX.(0.192	0.286	0.381	0.486	0.606	0.775		
1)	-01							
CUVRAT (0.692E	0.101	0.133	0.163	0.191	0.218		
1)	-01	-01	-01	-01	-01	-01		
BETDMX(0.160E	0.239E	0.302E	0.388E	0.497E	0.648E		
1)	-01	101	-01	-01	-01	-01		
) BETAMX(0.146E	0.231E	0 3335E	0.460E	0.610E	0.791E		
-	0	0	0	0	0	0		
STR4(20.	30.	40.	50.	60.	70.		

Sinusoidal Steer 1

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1)					
1) FHIMAX(0.405	1.87	2.90	3.62	4.24
UIN(50.0	50.0	50.0	0.00	50.0
DELFSI(1)	-0.201E-02	0.224E-02	0.176E-02	0.243E-02	0.768E-02
1) BETAMX(1)	0.116E-01	0.235E-01	0.375E-01	0.545E-01	0.744E-01
1) DEL(9.69	7.36	5.08	5.86	7,64
1) AYMAX.(0.125	0.239	0.340	0.423	0.492
STR5(20.0	40.0	60.0	80.0	100.

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Sinusoidal Steer 2

-					
PHIMAX(0.844	2.17	3.24	4.23	4.87
Ĵ					
UIN(0.01	50.02	50.0	50.0	50.0
1)	<u>۳</u> 0-	N ⊙-	N0-	- 0-	Ģ
DELPSIC	-0.179E-	0.186E-	0.352E	0.114E [.]	0.550E
()	÷0.	÷0-	-01	÷	
BETAMX (0.131E-	0.275E-	0.468E-	0.729E-	0.109
()					
DEL(8.98	<u>8.45</u>	13.6	20.0	27.7
Ĵ					
1) AYMAX.(0.157	0.289	0.414	0.524	0.613
STR5(20.0	40.0	60.0	80.0	100.

Figure F.37. Unloaded pickup truck, V_o = 50 mph, tire code: F0.

BETAMX (1) BETDMX	(1)	CUVRAT (1)	AYMAX.(1) FMAX. (1) PHIMAX	-
O 774F-	01 0.0	50E-01	0.286		0.280	0.208	2.75	
0 4545	01 0 0	49E-01	0.377		0.376	0.283	3.74	
		045-04	0 445		0.482	0.373	4.83	
						022	20 7	
0.731E-	01 0.0	20E-01	9,54V		0 Y 0 0 0			
0.995E-	01 0.7	10-326-01	0.027		0.719	0.838	15./	
0.131	0.1	í 4	0.699		0.747	1.40	2.71	

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1).					
FHIMAX(0.887	2.38	3.57	4.58	5.44
1					
U UIN	30.0	30.0	30.0	30.0	30.0
1)	201	201	-04	00-	-01
DELFSI(-0.812E	-0.202E	0.177E	0.730E	0.250E
1)	-01	÷0-	•0.1	-07	-01
BETAMX (0.111E	0.257E-	0.435E-	0.661E-	0.938E-
;					
1) DEL(9.71	7.39	5.12	5,69	7.25
1) AYMAX.(0.123	0.239	0.336	0.417	0.494
STR5'(40.0	80.0	120.	160.	200.

Sinusoidal Steer 2

-					
1) PHIMAX(1.16	2.81	4.11	5.18	6.04
	30.0	30.0	30.0	30.0	30.0
DELFSI(1)	-0.634E-03	0.922E-03	0.125E-01	0.561E-01	0.183
1) BETAMX(1)	0.123E-01	0.295E-01	0.541E-01	0.912E-01	0.145
11 DEL(9.04	8.33	13.4	19.5	26.3
1) AYMAX.(0.148	0.285	0.409	0.516	0.603
STR5(40.0	80.0	120.	160.	200.

Figure F.38. Loaded pickup truck, V₀ = 30 mph, tire code: F0.

	· · · · ·	7	
) FHIMAX(3.27 6.71 7.68 7.68) FHIMAX(
			-
	RMAX(0.159 0.418 0.961 1.18		UIN(
	;		÷ 0,
	AYMAX.(0.341 0.578 0.749 0.753		DELFSI(0.712E-
٤		-	<u>.</u>
ezoidal Stee	CUVRAT(0.772E- 0.114 0.178 0.178	soidal Steer	BETAMX(0.188E-
Trap		Sinu	1)
	BETDMX(0.276E 0.430E 0.669E 0.112		DEL(8.91
	$- \frac{1}{2} - $		1)
	1) BETAMX(0.335E- 0.557E- 0.630E- 0.116) AYMAX.(0.136
	• •		-
	STR4. (20. 30. 50.		STR5(20.(40.6

- -
1) FHIMAX(0.986 2.58 3.74 4.72 5.56
UIN(50.0 50.0 50.0 50.0 50.0
DELFSI(1) 0.712E-02 0.245E-01 0.692E-01 0.178 0.365
) BETAMX(1) 0.188E-01 0.418E-01 0.687E-01 0.103 0.145
1) DEL(1 8.91 6.10 7.80 11.2 15.5
1) AYMAX.(0.136 0.258 0.367 0.464
STR5 (20.0 40.0 60.0 80.0 100.

Sinusoidal Steer 2

1.60 3.46 5.02 7.78 7.78 1) PHIMAX(0.00.00 0.00.00 0.00.00 1) UIN...(0.100E-01 0.508E-01 0.262 2.51 1) DELFSI(0.248E-01 0.586E-01 0.112 0.897 1) BETAMX(496. 1) DEL...(0.181 0.358 0.510 0.748 0.750 1) AYMAX.(20.0 40.0 60.0 100. STR5..(

Figure F.39. Loaded pickup truck, V₀ = 50 mph, tire code: F0.

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		irap	ezolual Steer				
STR4(1) BETAMX(1) BETDMX(1) 02 0.100E-01	CUVRAT(1) 0.284	AYMAX.(1) 0.230	RMAX(0.169	1) PHIMAX(1.77	1
80.0	0.428E-(02 0.139E-01	0.375	0.305	0.225	2.46	
100.	0.514E-(92 0.260E-01	0.464	0.380	0.280	3.05	
120.	0.581E-(92 0.201E-01	0.552	0.447	0.335	3.59	
140.	0.643E-(02 0.255E-01	0.639	0,518	0,390	4.12	
160.	0.112E(01 0.313E-01	0.723	0.586	0.448	4.65	
180.	0.221E-0	01 0.399E-01	0.805	0.662	0.521	5.24	
		Sinu	soidal Steer l				
STR5(1) AYMAX.(1 0.130) DEL(1) 9.90	BETAMX(1) 0.485E-02	DELPSI(1) 0.347E-03	UIN(1) PHIMAX(0.614	1)
100.0	0.374		0.108F-01	0.207E-02	0.0K	3.48	
160.	0.480	4.15	0.174E-01	0.351E-02	30.0	4.40	
200.	0.562	5.05	0.264E-01	0.443E-02	30.0	5.18	
	·	Sinu	soidal Steer 2				
STR5 (1) AYMAX.(1) DEL(1)	BETAMX(1)	DELFSI(1)	UIN(1) PHIMAX(1
40.0	0.148	9.73	0.365E-02	0.702E-03	30.0	0.730	
80.0	0.281	6.39	0.602E-02	0.312E-02	30.0	2.11	
120.	0,399	10.1	0.872E-02	0.505E-02	30.0	3.28	
160.	0.512	14.4	0.152E-01	0,103E-01	30.0	4.19	
200.	0.408	18.9	0.286E-01	0.233E-01	30.0	4.95	
Figur	re F. 40. Unloade	ed pickup truck, V _c	= 30 mph, tire	code: Fl.			
1							

			code: Fl.	₅ ₹ 50 mph, tire	pickup truck, V _c	re F.41. Unloaded	Figu
	5.40	50.0	0.351E-01	0.905E-01	27.2	0.651	100.
	4.49	50.0	0.661E-02	0.573E-01	19.4	0.555	80.0
	3.45	50.0	0.319E-02	0.374E-01	13.4	0.437	60.0
	2.35	50,0	0.232E-02	0.227E-01	8.39	0.307	40.0
	0.930	50.0	0.820E-03	0.106E-01	8.84	0.165	20.0
	PHIMAX(UIN(1)	DELPSI(1)	BETAMX(1)	DEL(1)	1) AYMAX.(1)	STR5(
				nusoidal Steer 2	Sir		
	4.92	50.0	0.109E-02	0.631E-01	7.38	0.541	100.
	4.20	50.0	0.523E-03	0.460E-01	5.66	0.466	80.0
	3.32	50.0	0.207E-02	0.319E-01	4.91	0.374	60.0
	2.21	50.0	0.227E-02	0.200E-01	7.25	0.258	40.0
	0.617	50.0	-0.609E-03	0.999E-02	5.63	0.134	20.0
5	PHIMAX(UIN(1)	DELFSI(1)	BETAMX(1)	DEL(1)	1) AYMAX.(1)	STR5(
				usoidal Steer l	Sin		
Ŗ							•
	5.73	0.373	0.726	0.233	0.527E-01		10.0
	4.47	0.254	0.560	0.204	0.404E-01	0,460E-01	200 200 200
	3.74	0.208	0.466	0.174	0.322E-01	0.352E-01	0.00
	3.03	0.168	0.378	0.142	0.247E-01	0.265E-01	40.0
	2.19	0.126	0.286	0.108	0.199E-01	0.184E-01	0.02
1) FHIMAX(1.32	RMAX(1) 0.838E-01	AYMAX.(1) 0.190	CUVRAT(1) 0.728E-01	BETDMX(1) 0.133E-01	1) BETAMX(1) 0.115E-01	STR4(
				pezoidal Steer	Tra		

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1) PHIMAX(2.73	3.73	4.79	6.05	7.68	B .04	
1) KMAX(0.205	0.278	0.364	0.486	0.977	1.56	
1) AYMAX.(0.276	0.372	0.477	0.603	0.752	0.778	
CUVRAT (0.298	0.394	0.488	0.580	0.667	0.748	
BETDMX(1)	0.204E-01	0.290E-01	0.409E-01	0.550E-01	0.705E-01	0.111	
1) BETAMX(1)	0.177E-01	0.273E-01	0.412E-01	0.608E-01	0.868E-01	0.120	
STR4. (60.0	80°0	100.	120.	140.	160.	

Sinusoidal Steer 1

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*					
FHIMAX(1.06	2.67	3.90	5.01	5.96
1					
)NIU	30.0	30.0	30.0	30.0	30.0
1)	N 0 ∩	N 0	-04	20	-01
DELPSI (-0.182E	-0.222E	0.576E	0.798L	0.290E
1)	N () 	-01	-01	-01	-01
D BETAMX(0.917E	0.215E	0,372E	0,585E	0.865E
~	0	•	<u>_</u>	~	m
1) DEL(97.70	7.3(4.94	5.67	7.48
1) AYMAX.(0.130	0.256	0.361	0.448	0.534
STR5(40.0	80.0	120.	160.	200.

Sinusoidal Steer 2

~	3.99 0.964E-02	-0.121E-02	30.0	4 N N																	
	3.20 0.236E-01	0.607E-03	30.0	2.96																	
	3.4 0.451E-01	0.110E-01	30.0	4.37																	
	9.9 0.804E-01	0.531E-01	30.0	5.55																	
	27.8 0.138	0.203	30.0	6.52																	
	•						*								-	-					
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	1) FHIMAX(3.16	8.05	8.11	8.14	B.10		1) FHIMAX(1.17	2.87	4.15	5.27	6.18		1 PHTMAY	CC 1		5 V V V		8.13	
	RMAX(0.151 0.431	1.14	1.40	1.40	1.40		UIN(50.0	50.0	50.0	50.0	50.0		IIIN .	0.07			50.0	50.0	
	AYMAX.(1)	507.0	0.783	0.782	0.784	0.782		DELPSI(1)	0.444E-02	0.164E-01	0.588E-01	0.182	0.446		DELPSI(1)	0.6556-02	0.374F-01	0.266	2.67	2.42	code: Fl
apezoidal Steer	CUVRAT(1)	0.832E-01 0.123	0.161	0.195	0.225	0.249	nusoidal Steer 1	BETAMX(1)	0.173E-01	0.389E-01	0.655E-01	0.101	0.152	nusoidal Steer 2	BETAMX(1)	0.223E-01	0.533F-01	0.108	0.965E 04	356.	= 50 mph, tire (
Tr	BETDMX(1)	0.253E-01 0.392E-01	0.644E-01	0.118	0.193	0.277	Si	DEL(1)	8.82	5.89	2.93	12.0	17.8	Si	DEL(1)	7.73	15.3	29.6	36.4	18.8	oickup truck, V _O
	1) BETAMX(1)	0.297E-01 0.502E-01	0.777E-01	0.113	0.156	0.204		1) AYMAX.(1)	0.147	0.282	0.403	0.511	0.596		1) AYMAX.(1)	0.194	0.362	0.553	0.781	0.780	ure F.43. Loaded p
	STR4(20.00 30.0	40.0	50.0	60.05	70.0	•	STR5(20.0	40.0	60.09	80.0	100.		STR5(20.0	40.0	60.0	80.0	100.	Fig

	÷							, -		.
	1) FHIMAX(1 1 1			1 - 1 C	1) FHIMAX(0.684 2.40	и 4 и • • • • • и и ч	1) FHIMAX(0.783 2.20 3.37 4.28 5.05
	RMAX. (0.175	0.233	0.290	0.345	0.401	0 457	0.526	0,05 0,05 0,05 0,05	9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	UIN(30.0 30.0 30.0 30.0 30.0 30.0
	AYMAX.(1) 0.238	0.316	0.390	0.462	0.530	0.598	0.470	DELFSI(1) 0.116E-02 0.300E-02	0.331E-02 0.425E-02 0.425E-02	DELFSI(1) 0.104E-02 0.348E-02 0.564E-02 0.110E-01 0.237E-01
szoidal Steer	CUMMEN 11	0.387	0.480	0.570	0.658	0.743	0.626	oidal Steer 1 BETAMX(1) 0.483E-02 0.744E-02 0.109E-01	0.179E-01 0.271E-01 0.371E-01	BETAMX(1) 0.383E-02 0.624E-02 0.938E-02 0.155E-01 0.283E-01
Trape	0.110E-01	0.142E-01	0.182E-01	0.210E-01	0.261E-01	0.310E-01	0.384E-01	DEL(5.82 7.70 5.65	4.22 5.22 Sinus	EL(1)] 9.53 6.59 10.6 19.5
1) BETAMXI	0.378E-02		0.J66E-02	0.644E-02 0.555	0.712E-02	0.100E-01	0.199E-01	1) AYMAX.(1) I 0.135 0.272 0.391	0.579 0.579	1) AYMAX.(1) D 0.153 0.289 0.289 0.410 0.526 0.620
STR4(0 ° 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0					160.	180.	STR5(80.0 80.0	700. 100.	STR5(40.0 80.0 120. 200.

Figure F.44. Unloaded pickup truck, V₀ = 30 mph, tire code: F2.

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STR4(()	BETAMX (•	BETDMX(()	CUVRAT((AYMAX.(4) R	MAX	(PHIMAX	-
20.0		0.120E-	01	0.142E	- - -	0.776E-	-0-	0.207		0.904E-	-0-	1.45	•
30.0		0.198E-	÷01	0.199E	-0-	0.115		0.312		0.138		2.42	
40.0		0.234E-	0 1	0.256E	-01	0.150		0.406		0.181		3.25	
50.0		0.375E-	·01	0.344E	-01	0.184		0.498		0.223		3.98	
60.09		0.488E-	<u>6</u> 1	0.446E	-01	0.215		0.596		0.271		4.73	
70.0		0.637E-	01	0.567E	-01	0.245		0.797		0.462		6.26	
•												** s	
				0)	inus	oidal Steer							
						nr t'AMV (NEL DOT 1		Th	•	PHTMAY	-

-					
1) PHIMAX(0.728	2.35	3.47	4.34	5.04
UIN(50.0	50.0	50.0	50.0	50.0
DELFSI(1)	0.137E-03	0.284E-02	0.233E-02	0.852E-03	0.235E-02
) BETAMX(1)	0.101E-01	0.209E-01	0.336E-01	0.483E-01	0.660E-01
1) DEL(1	9.45	6.88	4.85	6.16	8.06
1) AYMAX.(0.142	0.274	0.393	0.486	0.561
STR5(20.0	40.0	60.0	80.0	100.

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1) FHIMAX(1.02 2.52 3.63 4.70 5.60	
UIN(50.0 50.0 50.0 50.0	
ELFSI(1) 0.117E-02 0.313E-02 0.399E-02 0.850E-02 0.464E-01	: F2.
<pre>() BETAMX(1) DE 0.110E-01 0.241E-01 0.394E-01 0.601E-01 0.947E-01</pre>	₀ = 50 mph, tire code
1) DEL(8.37 9.20 14.7 21.0 29.4	d pickup truck, V
1) AYMAX.(0.174 0.324 0.462 0.580 0.673	F.45. Unloade
STR5 (20.0 40.0 60.0 80.0 100.	Figure

Steer	
Trapezoidal	

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) BETAMX(1) BETDMX(1) CUVR	AT(1 300) AYMAX.(0.270	1) KMAX(0.199	1) FHIMAX(2.67	-
0.215E-0	1 0.250E	-01	.396	0.560	0.207	20.0	
0.331E-0	1 0.356E	-01 0	.492	0.458	0.347	4.61	
0.499E-0	1 0.484E	-01 0	.584	0.569	0.444	5.70	
0.725E-0	1 0.623E	-01 0	.674	0.718	0.645	7.15	
0.102	0.866E	-01 0	.758	0.794	1.52	ġ.16	¥
		Sinusoid	al Steer	-		-	•
AYMAX. (1) DEL(9.68	1) BETAN 0.	1X(1) 754E-02	DELPSI(2 -0.191E	1) UIN(-02 30.0	1) FHIMAX(1.16	Ţ
0.264	7.34	• •	182E-01	-0.259E	-02 30.0	2.84	
0.370	5.03	.0	322E-01	-0.112E	-02 30.0	4.15	
		<			0 02 00	UC U	

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							-								
1.16	2.84	4.15	5.25	6.11			1) FHIMAX(- C		2.99		4.40	5.60		6.40
30.0	30.0	30.0	30.0	30.0) T N (000	0.00	30.0	< < >	30.0	30.0		30.0
-0.191E-02	-0.259E-02	-0.112E-02	0.371E-02	0.181E-01	·		DELPSI(1) (CV JAAF V		0.120E-03		0.809E-0Z	0 3905-01		0.146
0.754E-02	0.182E-01	0.322E-01	0.517E-01	0.778E-01		Sinusoidal Steer 2	1) BETAMX(1)		0 /01F-0X	0.193E-01		0.361E-01	0 4095-01		0.120
9.68	7.34	5.03	5.45	7.19			11 DF1 (9.06	7.95		13.0			26.6
0.134	0.264	0.370	0.460	0 × 0 4 4			I AVMAY		0.155	9 201		0.436		9 n n • 9	0.655
40.0	80.0	120.	160.	200.			CTD5		40 0		0.00	1 20		160.	200.

Figure F.46. Loaded pickup truck, Vo = 30 mph, tire code: F2.

			•	÷
	1) PHIMAX(2.8 5.2 8.1 8.1	1	1) FHIMAX(2.95 2.95 5.38 5.38	1) FHIMAX(1.73 5.73 5.73 8.27 8.23 8.23
) RMAX(0.136 0.258 1.02 1.35		0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	UIN(0.02 0.02 0.02 0.02 0.02 0.02
	AYMAX.(1 0.302 0.531 0.799 0.799		0.205 0.205 0.834 0.400 0.138 0.357 0.357	DELFSI(1) 0.297E-02 0.204E-01 0.167 2.68 2.68 2.46 F2.
Jaanc Iphi	CUVRAT(1) 0.841E-01 0.125 0.163 0.198	dal Steer 1	0.156E-01 0.356E-01 0.603E-01 0.937E-01 0.141 0.141 dal Steer 2	BETAMX(1)] 0.196E-01 0.4775-01 0.945E-01 6.32 365. 365.
nzadp.11	BETDMX(1) 0.227E-01 0.352E-01 0.523E-01 0.966E-01	Sfnusoic	6.87 5.70 7.51 11.4 17.1 Sinusoic	DEL(1) E 7.40 14.3 27.1 46.0 20.4 truck_V = 50.1
	<pre>J BETAMX(1) 0.254E-01 0.435E-01 0.679E-01 0.100</pre>		AYNAX 4 0.151 0.290 0.412 0.524 0.607	AYMAX.(1) 0.192 0.381 0.550 0.797 0.795
	STR4. (20.0 30.0 40.0 50.0		STR5(1) 20.0 40.0 60.0 80.0 100.	STR5(1) 20.0 40.0 60.0 80.0 100.

Trapezoidal Steer

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1) PHIMAX(3.81 5.20 5.88 7.72 7.72
1) RMAX(0.223 0.306 0.419 0.653 1.38 1.49
1) AYMAX.(0.302 0.531 0.533 0.752 0.756
CUVRAT(0.302 0.397 0.489 0.577 0.578 0.732
BETDMX(1) 0.280E-01 0.385E-01 0.529E-01 0.669E-01 0.955E-01 0.955E-01
1) BETAMX(1) 0.253E-01 0.388E-01 0.577E-01 0.826E-01 0.151
STR4. (60.0 80.0 100. 120.

Trapezoidal Steer - 30 mph

Trapezoidal Steer - 50 mph

PHIMAX(4.37 7.60 7.60 0.202E 0.435E 0.435E
1)
KMAX(0.217 0.870 1.18 0.426F 0.8916 0.1926
AYMAX.(0.452 0.752 0.762 0.762 0.7529 0.5296 0.9036
() () () () () () () () () () () () () (
CUVRAT(0.851E 0.125 0.161 0.0 0.0 0.0
BETDMX(1) 0.316E-01 0.9492E-01 0.948E-01 0.0 0.0 0.0
<pre>1) beigmx(1) 0.388F-01 0.652E-01 0.987E-01 0.0 0.0 0.0</pre>
STR4. (20.0 30.0 40.0 60.0 20.0 70.0

Figure F.48. Loaded pickup truck, tire code: F3.

APPENDIX G

A ROLLOVER INCIDENT WHICH OCCURRED DURING TESTING OF A HEAVY TRUCK

On May 30, 1975, a heavily loaded straight truck rolled over during the conduct of vehicle dynamics experiments at the facilities of the Texas Transportation Institute (TTI). The incident was unexpected, unplanned for, and involved the injury of a test driver. This document is intended to provide answers to a series of questions regarding the event itself, as well as regarding the significance of this experience to NHTSA-sponsored research.

The questions to be addressed are as follows:

- What was the nature of the experiment which was being attempted?
- 2) What actually occurred in the course of that experiment?
- 3) From a mechanistic point of view, why did the rollover anomaly occur?
- 4) What lessons are to be learned from this experience?

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In responding to these questions, the writer wishes to be as informative as our current state of knowledge on the matter permits, and to establish an understanding of the overall event which will promote practices that prevent recurrence of any similar situation in the future.

1) What was the nature of the experiment which was being attempted?

The test vehicle, shown in Figure G-1, was a White Road Boss, two-axle truck, outfitted with a hybrid driver/automatic control system. The vehicle was being employed in a series of





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experiments, designed to be <u>sublimit</u> in nature, which were primarily intended as a means to validate a computerized simulation.

The test procedure was based upon the methods employed in a previous NHTSA-sponsored study entitled "Analysis of Truck and Bus Handling" [1]. These procedures applied automaticallycontrolled test techniques to commercial vehicles by way of a hybrid scheme of driver control and pre-programmed servo control. The severity of turning maneuvers was constrained, in concern for heavy vehicle rollover, but no steps were taken to assure the prevention of a rollover should a constrained level experiment become inadvertently unconstrained.

These procedures and test practices were applied, without significant modification, in the current study. Calculations were made to predict the limits of lateral acceleration beyond which rollover would occur and vehicle test levels were prescribed with an accordingly large margin of safety.

The particular experiment being conducted at the time of the subject incident involved a set of steering-only maneuvers as a preliminary to combined steering/braking tests. The purpose of the preliminary test was to determine that steer angle value at which a steady turn of .35 g lateral acceleration (A_v) level would be attained, at a test speed of 50 mph. The test is conducted by first establishing a straight-line path at a speed slightly above 50 mph, whereupon the driver shifts the transmission into neutral and presses a button initiating automatic control. When the truck has slowed to exactly 50 mph, the steering servo motor becomes clutched through a drive pulley to the steering shaft and the stored steering function begins. The steering waveshape is a trapezoidal time history with an initial ramp function followed by a sustained steering level. The steady steering level is incremented in successive test runs in search of the value needed to attain the .35 g condition.

In the tests being conducted here, the test vehicle was fully loaded to approximately its gross vehicle weight rating of 30,000 lbs. As shown in Figure G.2, the weights consisted of three cast concrete sections which were mounted directly to the vehicle's frame rails, giving a composite c.g. height in the vicinity of 48 inches.

2) What actually occurred in the course of the previously defined experiments?

A sequence of left-hand-turning runs was conducted in which the steering wheel displacement was incremented from 100° amplitude to 120° and, finally, to 140°. At the 100° level, a 0.3 g A_v level was obtained. In two following runs with 120° applied, a 0.3 g level was again obtained, but, due to the noisy character of the signal output from the truck-mounted accelerometer, the lack of an acceleration response commensurate with the 20° steering increment was merely considered a resolution problem. In the following run, with 140° now programmed as the steering level, the vehicle elicited a diverging yaw response which concluded with the rollover of the vehicle. In the course of the roll transient, the first ground contact of the truck body was at the right roof edge and exhaust stack position followed by a thorough crushing of the roofestructure and then another apparently airborne roll motion. Next, the left side wheels and driver's-side sheet metal hit the pavement. failing all frame cross-members and three out of four rear suspension spring attachments. The vehicle then slid along the pavement, remaining overturned onto the left side of the cab, as shown in Figure G.3.

Although one fuel tank parted from the vehicle and both tanks ruptured completely, no fire ensued.

The driver was extracted very quickly from the vehicle through the backlight, in fear of the prevailing fire hazard.



Figure G.2. Concrete loading weights.



Figure G.3. Final position of overturned test vehicle.

The minimization of the driver's injuries to include only a broken shoulder blade and minor lacerations is attributed in large measure to his having pulled himself down toward the floor, upon first realizing that rollover was imminent. The driver was restrained by a competition-type shoulder and lap harness and he wore a helmet which remained lodged in the deformed roof structure upon his removal.

3) From a mechanistic point of view, why did the rollover anomaly occur?

Since HSRI had calculated, simply on the basis of equilibrium roll moment considerations, that rollover would occur in the vicinity of 0.7 g's ${\rm A}^{}_{\rm V},$ it is not surprising that the vehicle rolled over on TTI's dry asphalt test surface (whose dry skid number was 80). In the actual event, however, the rollover occurred at 0.6 g due to the failure of the outside front wheel rim which permitted an abrupt, and large, reduction in effective track width. Nevertheless, it is generally taken for granted that heavy trucks, with any commonly-elevated load configuration, will roll over on dry surfaces if subjected to a sufficiently large sideslip excursion. Thus the relevant question here is not so much "why did the truck roll over?" but rather "why did the truck become exposed to a condition in which rollover was inevitable?" The latter question can be condensed to an even more specific query which relates to the evidence of this incident; namely, "why did this truck elicit a yaw divergency in response to a steering input which was expected to yield a steady turn of 0.35 g A_v ?"

The answer to this question has two parts. Firstly, due to an oversight in the conduct of the test sequence we should not have "expected" a .35 g level response to the final steering input of 140° amplitude. Rather, it would appear that we should have expected a response in the range of .40 to .45 g. To explain the manner in which the effective input magnitudes became confused, consider the four sets of time histories in Figure G.4. This figure is reconstructed from A_y recordings and includes the presumed steering wheel displacements which were not being recorded during the preliminary setup tests. Since the steering input was generated through the automatic controller and since there is no evidence that the controller either misbehaved or was mis-programmed, it appears very likely that the steer inputs were as shown.

The significant feature of the Figure G.4 time histories is the existence of initial offsets in the measured A_y and presumably in steering wheel displacement, δ_{sw} . Offset in the "zero value" of δ_{sw} is possible in the hybridized driver/automatic system because the driver himself must establish zero steer just prior to initiating the automatic sequence in each test run. When the controller switches "on," the steering servo becomes clamped to the truck's steering shaft at whatever angular position the shaft happens to occupy at that instant. The controller then applies its programmed displacements in reference to that "zero" position. In the severe vibration environment presented in a truck such as that tested, it is not unlikely that the driver, distracted by his many chores, could have missed the intended zero position by the 20° or so needed to explain the A_y data shown in Figure G.4.

Thus, in Run No. 1, it would appear that a true 100° steering angle was applied since the "zero value" was virtually zero degrees. Upon observing that the A_y response provided only 0.3 g, the test operator then selected to conduct Runs No. 2 and 3 at a 120° setting on the automatic controller. These two runs, however, were coincidentally accompanied by zero steer offset values of sufficient magnitude, and consistent polarity, to effectively nullify the influence of the 20° increment in δ_{sw} which had been added relative to the 100° setting of Run No. 1. Accordingly, an A_y level of approximately 0.3 g was again observed in both Run No. 2 and No. 3.

100 1st RUN, at $\delta_{\underline{\epsilon}\psi}$ 100° d 5w 0.3G's Ay 120° 2ND RUN, at Ssu 120° Sow 0.3G's -0.054 Ry 120 3RD RUN, at Ssw 120° Jow 0.36's -0.054 Ry 51 (Seconds) 0 3 41 1 140° Ssw ATH RUN, at $140^{\circ} S_{sw}$ (ROLLOVER) 0.665 +0.03G A, Figure G.4 :

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in side force generation prior to the saturation or frictionlimiting, of tires on the other axle.

In contrast, it appears that a heavy truck spinout can initiate when maneuvering severity exceeds an A_y of about 0.45 to 0.50 as illustrated by the simulated and experimentallyrecorded A_y time histories of Figure G.5. The simulation runs cover a sequence of trapezoidal steering levels spanning the range of conditions which were tested. Beginning with the "2.5 DEG TRAP" (roughly equivalent to a run at 107° steering wheel angle) the simulated responses indicate convergent behavior up to the "4.0 DEG TRAP" condition. With a simulated 4.0° nominal input at the front wheels, the truck shows a diverging yaw behavior (Figure G.6) and slews to a 14-degree sideslip angle in four seconds (the point in time at which the test truck completely unloaded its inside wheels and initiated the rapid roll divergency).

In Figure G.5 the simulation results are compared with measured data from the 2.3 Deg (100° steering wheel amplitude) and 3.7 Deg (140° steering wheel amplitude) test runs which were discussed previously. Although the simulated vehicle shows less understeer than the test vehicle (comparing data from the roughly equivalent "2.5 DEG TRAP" and "2.3 DEG δ_{sw} " conditions), the abupt change in the simulated vehicle's behavior between the 3.5- and 4.0-DEG conditions basically confirms the divergency of the test run with nominally 3.7 DEG input at the front wheels. It would appear from the simulated sideslip and roll angle plots of Figures G.7 and G.8 that a heavily diverging sideslip response, with the simulated 4.0 DEG input, was definitely leading to a rollover.

The occurrence or non-occurrence of a simulated vehicle rollover is of little significance to this examination, however. Rather, the significant observations are related to the narrow regime of tire slip angles within which the vehicle is apparently stable. The simulated response to the 3.5 DEG input, for





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Figure G.6





Figure G.8

example, shows that front and rear tires are operating at slip angles of 8 to 9°—and that beyond that level, in the 4.0 DEG run, the vehicle exhibits a yaw divergency. Referring to the carpet plot of Figure G.9 (describing the tires which were installed on the test truck), we see that the vehicle's more heavily loaded tires, which are running at 8000 lbs or so, are far from being side force saturated at an 8° slip angle. Thus the spinout anomaly occurs while effective front and rear lateral force rates (lb/deg slip angle) are still rather stiff. In examining this, it can be shown that the vehicle becomes destabilized by a classical mechanism which is explainable through linear vehicle mechanics. Namely, the vehicle arrives at a lateral acceleration level at which the prevailing velocity exceeds the critical speed of the system linearized about that operating point.

To demonstrate this linearized systems explanation we evaluated the lateral force rates for each tire of the vehicle under those conditions of slip angle and load which were computed by the major simulation in the 3.5 DEG TRAP run. Together with parameters describing the vehicle's mass, wheelbase, and longitudinal location of c.g., the critical speed of the (now oversteer) truck can be obtained through the relation:

$$V_{c} = \frac{L^{2}C_{\alpha}C_{\alpha}}{m(C_{\alpha}a - C_{\alpha}b)}$$

where

$$V_c$$
 = critical speed
L = wheelbase
 $C_{\alpha r}$, = total cornering stiffness at rear
 $C_{\alpha f}$ (front) axle



- m = mass
- a = position of c.g. aft of front axle
- **b** = position of c.g. forward of rear axle

The solution of this expression yields a 75 ft/sec or 51.2 mph critical speed. Thus, it confirms our observation that at some steering level between the 3.5 DEG and 4.0 DEG run, the system exceeds a stability threshold, with its 50 mph test velocity, which instability is manifested by a small positive exponential time response. This slowly growing divergency, while contrasting with the abrupt spinout limits of some passenger cars, is unusual because it can be stimulated, as seen, in near proximity to the normal maneuvering range.

In summary, the truck rolled over because it entered a medium level turn, within which its yaw behavior was unstable. The instability was sustained long enough for the truck to accumulate a sideslip angle of about 25°, producing a tire side force-induced rolling moment sufficiently large, with the help of the outside front wheel failure, to initiate the rollover.

4) What lessons can be learned from this incident?

A variety of lessons would appear to be demonstrated by the scenario surrounding this incident. From a technical point of view, the heavy commercial vehicle clearly deserves to be treated with special care in vehicle dynamics experimentation. Indeed, this class of vehicles presents certain behavior characteristics which differ so markedly from passenger car properties that we need to "recalibrate" much of our thinking before planning truck measurement studies. Particularly in regard to mechanisms which determine load distribution around the vehicle's various tire positions, the heavy truck possesses certain first-order parametric sensitivities which are virtually insignificant in passenger cars.

More importantly than the mechanisms themselves, we must recognize our limited knowledge of the ways in which these mechanisms are influential in determining vehicle response. In the face of a very limited base of experience, it would appear that <u>caution</u> is the primary virtue. In the context of research into truck maneuvering dynamics, "caution" means that the full-scale experiment should never be used for exploring areas about which we have not already gained a considerable insight through simulation. In the current vacuum of technology concerning heavy truck directional response, the areas of "no considerable insight" far out-number those which are ripe for examination through testing.

With regard to full-scale experimentation, as it may be warranted and desirable in the future, it appears that either the total removal of the driver or his total protection, with anti-rollover outriggers, is the only prudent course. In addition, the reliability of either the fully automaticallycontrolled truck or the outrigger-protected truck, should be assessed through appropriate trial. While the automatic control of an automatic transmission-equipped truck would be straightforward, the formidable hazard posed by a runaway requires special consideration—and there have been at least two passenger car runaways in NHTSA-sponsored automatic control testing. Likewise, we must recognize that an outrigger which fails is worse than no outrigger at all since it may serve merely to pole-vault the vehicle from an increased altitude. Thus the assured performance of a heavy truck outrigger system must be demonstrated in an unoccupied vehicle prior to adoption for driver-controlled testing.