# ENGINEERING RESEARCH INSTITUTE UNIVERSITY OF MICHIGAN ANN ARBOR

#### PROGRESS REPORT

# STUDY OF CONCRETE CONTAINING FLY ASH FROM MARYSVILLE STATION

Ву

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Project 2211

DETROIT EDISON COMPANY DETROIT, MICHIGAN

June 15, 1954

#### SYNOPSIS

This is the second progress report pertaining to use of Detroit Edison Company fly ash in air-entrained concrete. The first progress report, dated May 15, 1954, dealt with Trenton Channel ash exclusively. This report gives similarly acquired data for fly ash from the Marysville station and draws a few comparisons with the results from the Trenton study.

Concrete containing the Marysville ash developed slightly lower strengths under comparable conditions than that containing Trenton ash. The most significant difference between the two ashes, judged from the presently available data including compressive-strength tests up to the 28-day age, is their different requirement for air-entraining admixture to obtain the air content considered necessary for maximum weather resistance. Marysville ash requires three or more times more Darex than Trenton ash, making the Darex requirement of some consequence in the cost of the concrete.

Caution is again advised against predicting strength of job concrete from the data contained herein unless suitable safety factors are utilized to compensate for possible field variations in mixing, curing, and proportioning.

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# STUDY OF CONCRETE CONTAINING FLY ASH FROM MARYSVILLE STATION

#### Introduction

On May 15, 1954, a progress report was issued concerning the use of Trenton Channel fly ash in air-entrained concrete. The data presented therein were developed from laboratory studies started by the Engineering Research Institute of the University of Michigan persuant to a contract between the Institute and the Detroit Edison Company.

This second report contains similarly acquired data for Marysville fly ash. Again, only data obtained from compressive-strength tests up to 28-day age is now available and can be presented at this time. Results from volume-change bars and strength specimens of 90-day and 1-year age will be given in a later report.

Repetitious matter pertaining to test procedures, etc. which were covered in the Trenton Channel report will be omitted here since the testing procedures for the two fly ashes remained unchanged.

This report pertains to the use of Marysville fly ash in airentrained concrete exclusively. Darex air-entraining admixture was used in all the mixes in such amounts as to obtain the amount of air considered desirable to obtain maximum weather resistance.

#### Mix Design

Mix-design procedure was identical with that used in the Trenton Channel fly-ash series, viz., full advantage was taken of the added plasticity of the mortar constituent provided by the addition of fly ash, and, consequently, increased stone contents were used over those normally employed in concrete not containing fly ash.

Control specimens with no fly ash were not made in this series since the procedures and materials were identical with those of the Trenton Channel series and it was considered that the control specimens just

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previously made in that study would suffice. It will be recalled that the "Recommended Practice for Selecting Proportions for Concrete" currently being considered for adoption by the American Concrete Institute was used as the design basis for the mixes not containing fly ash.

Concrete with three cement contents have again been investigated, viz., 4, 5, and 6 sacks per cubic yard. Three fly-ash contents for the 5-and 6-sack concrete and four fly-ash contents for the 4-sack concrete have been used. Attention is particularly called to the fact that the increments of fly ash have been stepped down 50 pounds per cubic yard from that used in the Trenton Channel lean-concrete series (4 sacks per cubic yard), since preliminary examination of the concrete strengths appeared to indicate the desirability of lower ash contents for the Marysville material.

#### Materials

With the exception of the fly ash, all concrete materials were identical with those used previously in the Trenton Channel fly-ash study, viz., l-inch maximum size natural-gravel coarse aggregate, natural sand having fineness modulus of 3.0, and an "anonymous" cement consisting of a blend of equal amounts of Peerless, Wyandotte, and Huron. The Marysville ash used was furnished in January, 1954. The portion of the analysis of this ash now available is shown in Table I-A in the appendix.

#### Fabrication of Specimens and Test Procedures

The methods of mixing, curing, and testing the specimens were identical with those used in the Trenton Channel study.

#### Discussion of Test Results

Detailed tabulation of the Concrete-mix data and compressive-strength results are shown in the appendix in Tables II-A, III-A, and IV-A, for the 4-sack, 5-sack, and 6-sack concrete, respectively.

1. Coarse-Aggregate Content. Use of a lower increment of fly ash in the 4-sack concrete for Marysville ash (100 lb per cubic yard) required an additional evaluation of the stone content to obtain proper workability. Table I gives the values found satisfactory for both Trenton Channel and Marysville ashes for 1-inch maximum size aggregate and a sand having a fineness modulus of 3.0. The value  $V_{\rm S}$  is expressed as dry rodded volume of coarse aggregate per unit volume of concrete.

TABLE I  $\mbox{VOLUME, $V_{\mathtt{S}}$, OF DRY RODDED COARSE } \\ \mbox{AGGREGATE PER UNIT VOLUME OF CONCRETE}$ 

Fly Ash lb/cyd	4 Sack	5 Sack	6 Sack
0 100 150 200 250 300	0.64 0.72 0.78 0.81 0.81 0.81	0.64 0.78 0.78 0.78	0.64 0.75 0.75 0.75

2. Strength Results. Average values of compressive strengths up to the 28-day age have been tabulated in Table II. Attention is called to the fact that the strengths of the control specimens not containing fly ash are results from the Trenton Channel study. New control specimens were not made, as previously indicated.

As in the case of Trenton Channel fly ash, the most prominent feature of the strength results is the substantial increase of strength of the lean fly-ash mixes over the lean plain cement mixes at the 28-day age. Table III shows the strength of both Trenton Channel and Marysville fly ash at each age expressed as percentage of strength of the plain cement mixes having the same cement content. With few exceptions, the tabulation indicates reduced strength for the Marysville ash with respect to the Trenton ash for a corresponding fly-ash content, cement content, and age. Better strength equivalence of the two ashes is obtained if comparison is made of the strengths of the concrete containing, in each case, 50 lb per cubic yard less Marysville ash than Trenton ash.

Comparison of the rate-of-strength gain between 7- and 28-day age has been summarized in Table IV. As indicated in the Trenton Channel study, the leaner mixes gain strength faster, and increased amounts of either Trenton or Marysville ash tend to hasten this strength gain.

Figures 1 to 3 show the average strengths plotted against age. Strength gain is again orderly as in the case of Trenton ash.

TABLE II

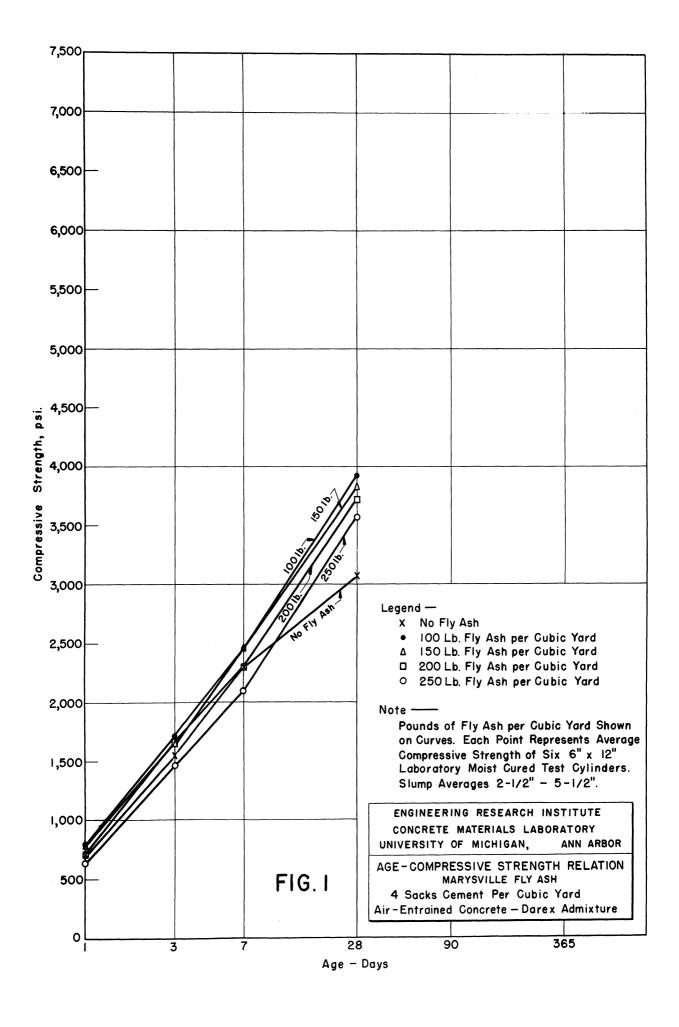
SUMMARY OF RESULTS - MARYSVILLE FLY ASH

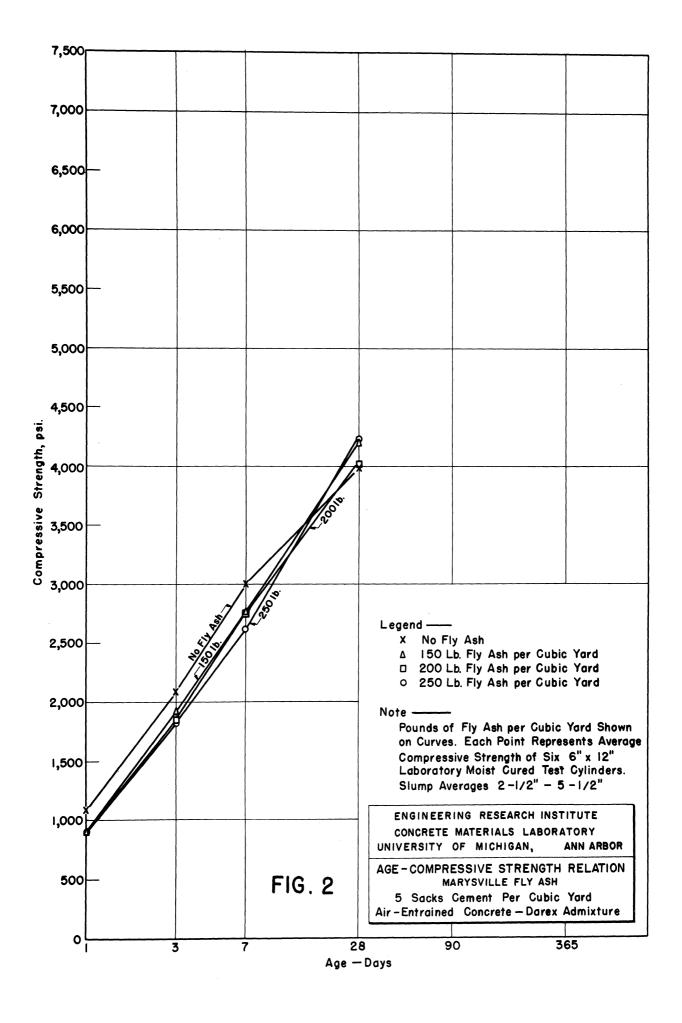
	~	·			
	l vear				
th, psi	90 davs				
Strength,	28 davs	3070 3922 3823	3724 3569	3993 4211 4028 4237	4633 4266 4243 4123
	7 davs	2282 2456 2456	2396 2095	3002 2768 2762 2615	3576 3152 3145 2901
Compressive	3 days	1546 1714 1641	1663	2088 1917 1867 1851	2505 2404 2113 2153
	1 day	702 792 786	723	1080 898 880 886	1449 1191 1126 1145
Darex,	fluid oz/ cyd	4.2 16.3 27.4	38°3 49°7	4°5 31°5 42°5 49°4	4.2 27.2 36.9 45.1
Slump,	în,	0 m m	0. T.	ル い い い す す ず	4.7 4.3 4.3
Air	Content, percent	₩ ₩ ₩ ₩ ₩ ₩ ₩ ₩ ₩ ₩ ₩ ₩ ₩ ₩ ₩ ₩ ₩ ₩ ₩	8° 4 6° 4	らろうらららうう	5.6
Fly Ash Wet Mixing Water	gal/sk	6.95 7.12 7.38	7, 81 8,51	5,48 6,47 6,82 7,14	4.77 5.17 5.61 5.92
Net Mix	lb/cyd	231 237 246	283	228 270 284 298	239 259 280 296
Fly Ash	lb/cyd	0 100 150	200 250	0 150 200 250	0 100 150 200
Actual Cement	Content, sk/cyd	4.10 4.05 4.00	5, 50 98, 98	5.11 5.04 4.96 5.02	6.06 5.99 5.96 5.98
Nominal Cement	Content, sk/cyd	٥٠4		5.0	0.9

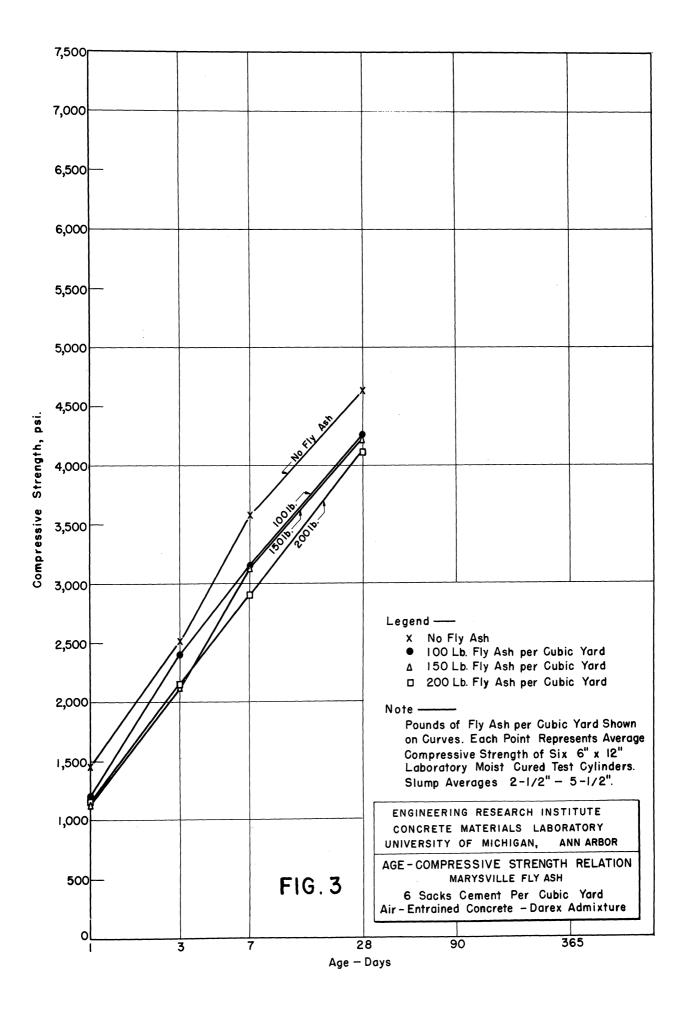
TABLE III

COMPRESSIVE STRENGTHS OF FLY-ASH MIXES EXPRESSED AS PERCENT OF STRENGTH OF PLAIN CEMENT MIXES OF SAME CEMENT CONTENT

Cement				Com	Compressive Str	Strengths, Percent	ercent		
Content,	Fly Ash	H	1 day	3 d	3 days	7 days	ays	28	28 days
sk/cyd	l.b/cyd	Trenton Marys	Marysville	Trenton	Trenton Marysville	Trenton	Trenton Marysville	Trenton	Trenton Marysville
7	100		113		111		1.08		128
<b>.</b>	150	130	112	121	106	116	108	131	125
† .	200	112	103	108	108	108	105	122	121
<b>†</b>	250	104	91	101	95	100	92	122	116
. <del></del>	200	<del>1</del> 76		66		8	<b>.</b>	115	
ľĊ	150	107	83	76	92	26	92	66	105
70	200	96	82	101	89	- 86	92	700	[0]
<u>.</u>	250	93	82	76	88	92	87	103	106
\		,	ı						
9 '	100	96	82	101	96	76	88	96	92
9 '	150	66	62	96	†8	93	88	97	92
9	200	75	80	93	98	89	81	26	86
						******			
				***************************************					







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TABLE IV

AVERAGE RATIO OF 28-DAY TO 7-DAY

COMPRESSIVE STRENGTHS

Cement Content sk/cyd	Fly Ash lb/cyd	to 7-Day	Day Strength Strength
		Trenton	Marysville
4	0	1.35	1.35
4	100		1.60
4	150	1.51	1.56
4	200	1.52	1.55
4	250	1.65	1.70
4	300	1.62	
5	0	1.33	1.33
5	150	1.37	1.52
5	200	1.48	1.46
5	250	1.50	1.62
6	0	1.30	1.30
6	100	1.32	1.35
6	150	1.35	1.35
6	200	1.42	1.42

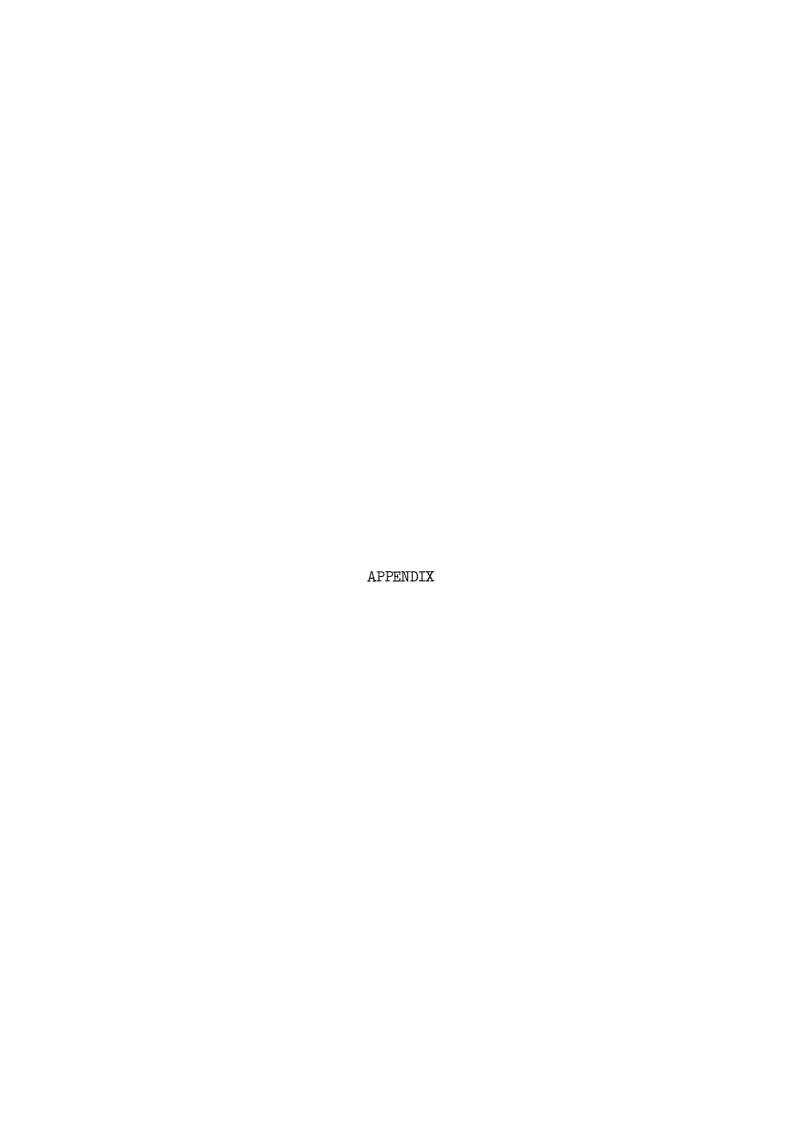
3. Air-Entraining Admixture Requirement. Substantially greater amounts of Darex air-entraining admixture were required for Marysville ash than for Trenton ash under comparable conditions of use. Table V summarizes the amounts used for the two ashes.

The large amounts of Darex which must be used with Marysville ash make it doubtful that it is economically feasible to use this admixture. Vinsol resin air-entraining admixture would be considerably cheaper.

TABLE V

AMOUNTS OF DAREX AIR-ENTRAINING
ADMIXTURE PER CUBIC YARD OF CONCRETE

Cement Content sk/cyd	Fly Ash lb/cyd	Dare fluid o	
		Trenton Ash	Marysville Ash
7+ 7+ 7+ 7+	0 100 150 200 250	4.2 10.3 11.4 14.4	16.3 27.4 38.3 49.7
5 5 5 5 5	300 0 150 200 250	17.3 4.2 11.9 13.0 16.5	31.5 42.3 49.4
6 6 6 6	0 100 150 200	4.2 9.9 11.6 14.3	27.2 36.9 45.1



### TABLE I-A

# PROPERTIES OF FLY ASH (54C-4)

Physical Properties	
Specific surface, air permeability test, sq cm per gm	4578
Compressive strength, 20 percent by weight of portland-cement addition, hand mixing, 73°F cure, percent of control	
7 days	107
28 days	106
90 days	137
Water requirement, percent of control	111
Compressive strength, 25 percent by weight of sand, sand replacement, machine mixing, 73°F cure, percent of control	
7 days	164
28 days	181
90 days	
Water requirement, percent of control	126
Compressive strength, 25 percent by weight of cement, sand replacement, machine mixing, 73°F cure,	
percent of control	153
7 dáys 28 days	155
90 days	±//
Water requirement, percent of control	105
Drying Shrinkage, 28 days, percent	0.08
Soundness, autoclave expansion, percent	0.03
Specific gravity	2.28
Chemical Properties	
Silicon dioxide (SiO2), percent	44.5
Magnesium dioxide (MgO), percent	1.5
Sulfur trioxide (SO3), percent	0.5
Loss on ignition, percent	10.3

## TABLE I-A (Concluded)

### MARYSVILLE FLY ASH

## Mortar Strength Tests

		Compres	sive Strer	ngth, psi
	(F	ercent of	control in	n parentheses
		7 days	28 days	90 days
20 Percent	by Weight of Cement Ad	ldition (Ha	nd Mix)	
Control (54C-7)		3252	4969	5171
Fly Ash (54C-2)		3440	5231	7027
		(107)	(106)	(137)
Control Mix	Fly-Ash Mix			
750 g cement	750 g cement			
2062 g graded sand	150 g fly ash			
360 ml water	2062 g graded sand			
	400 ml water			
105.8% Flow	112.3% Flow			
25 Percent by W	eight of Sand, Sand Re	placement	(Machine M	Mix)
Control (5)(C 150)		0050	4271	
Control (54C-158)		2950 4825	• •	
Fly Ash (54C-4)		(164)	, , -	
Control Mix	Fly Ach Mix	(104)	(101)	
750 g cement	Fly-Ash Mix 750 g cement			
2062 g graded sand				
	1547 g graded gand			
365 ml water	1547 g graded sand 460 ml water			
365 ml water	460 ml water	Replacemen	t (Machine	e Mix)
365 ml water  115.4% Flow  25 Percent by We	460 ml water			e Mix)
365 ml water  115.4% Flow  25 Percent by We  Control (540-158)	460 ml water	2950	4271	e Mix)
365 ml water  115.4% Flow  25 Percent by We	460 ml water	2950 4521	4271 6600	e Mix)
365 ml water  115.4% Flow  25 Percent by We  Control (540-158)	460 ml water	2950	4271	e Mix)
365 ml water  115.4% Flow  25 Percent by We  Control (54C-158)  Fly Ash (54C-4)	460 ml water  112.5% Flow eight of Cement, Sand	2950 4521	4271 6600	e Mix)
365 ml water  115.4% Flow  25 Percent by Water  Control (54c-158)  Fly Ash (54c-4)  Control Mix  750 g cement	460 ml water  112.5% Flow eight of Cement, Sand  Fly-Ash Mix	2950 4521	4271 6600	e Mix)
365 ml water  115.4% Flow  25 Percent by We Control (54C-158) Fly Ash (54C-4)  Control Mix	460 ml water  112.5% Flow eight of Cement, Sand  Fly-Ash Mix 750 g cement	2950 4521	4271 6600	e Mix)
365 ml water  115.4% Flow  25 Percent by We  Control (54C-158)  Fly Ash (54C-4)  Control Mix  750 g cement  2062 g graded sand	460 ml water  112.5% Flow eight of Cement, Sand  Fly-Ash Mix 750 g cement 188 g fly ash	2950 4521	4271 6600	e Mix)

TABLE II-A

- MARYSVILLE FLY ASH 4-SACK. CONCRETE DATA

ab. Cord         38ad         Stock of Action         Water         paj/kit         lije ir fri         Per Cent         11.0         o.j.cycl         I day         3 days         12.0 </th <th>Batch No.</th> <th>Date Made</th> <th>Fly Ash lb/cyd</th> <th>Actual Cement Content</th> <th>*** A</th> <th>Material Proportion 1b/cyd</th> <th>al Propo 1b/cyd</th> <th>ortions Net</th> <th>Actual w/c.</th> <th>Wt. Fresh</th> <th>Pressure Air Content.</th> <th>S</th> <th>Darex,</th> <th></th> <th></th> <th>Compress</th> <th>Compressive Strength</th> <th>gth</th> <th></th>	Batch No.	Date Made	Fly Ash lb/cyd	Actual Cement Content	*** A	Material Proportion 1b/cyd	al Propo 1b/cyd	ortions Net	Actual w/c.	Wt. Fresh	Pressure Air Content.	S	Darex,			Compress	Compressive Strength	gth	
7.24         146.2         4.9         3.5         16.3         770         1575         2295           7.03         149.5         3.1         3.25         16.3         770         1945         2740           7.09         145.8         4.6         4.25         16.3         760         1945         2740           7.12         145.8         4.6         4.25         16.3         792         1714         2450           7.37         145.8         4.9         3.25         27.7         705         1625         2440           7.21         145.1         5.1         3.25         27.7         705         1655         2445           7.22         145.1         5.3         4.0         26.7         705         1645         2445           7.23         145.1         5.9         4.0         26.7         705         1645         2445           7.24         146.4         5.1         3.5         27.4         706         1645         2445           7.75         145.1         5.3         3.75         37.7         706         1645         2445           7.75         144.4         4.8         5.75 <t< th=""><th></th><th></th><th></th><th>sk/cyd</th><th></th><th></th><th></th><th>Water</th><th>gal/sk</th><th></th><th>Per Cent</th><th></th><th>oz/cyd</th><th></th><th>5 даув</th><th></th><th>days</th><th><math>\vdash</math></th><th></th></t<>				sk/cyd				Water	gal/sk		Per Cent		oz/cyd		5 даув		days	$\vdash$	
7.03         149.5         3.1         3.25         16.3         765         1945         2740           7.09         145.8         4.6         4.25         16.3         985         1715         2490           7.12         147.2         4.6         4.25         16.3         989         1711         2490           7.21         147.2         4.2         3.7         16.3         792         1714         2456           7.21         145.8         5.1         3.25         27.7         705         1645         2490           7.21         145.1         5.2         27.7         705         1645         2490           7.22         145.1         5.2         27.7         705         1645         2490           7.22         145.1         5.2         27.7         705         1625         2740           7.24         145.1         5.3         27.7         725         1775         1795         2245           7.75         145.1         5.3         37.5         27.4         786         1625         2245           7.75         145.1         4.8         36.3         38.3         1653         1360	53	5-30-54	100	4.02	.18	476	2211	241	4.5.7	146.2	6.4	3.5	16.3	7 <sup>4</sup> 0 690	1555 1500	2295 2190	3515 3885		
7.09         145.8         4.6         4.29         16.3         900         1715         2490           7.12         147.2         4.2         3.7         16.3         792         1714         2456           7.37         145.8         4.9         3.25         27.7         705         1685         2440           7.21         146.4         5.1         3.25         27.7         705         1645         2490           7.21         146.4         5.1         3.25         27.7         705         1645         2490           7.54         146.4         5.1         3.25         27.7         705         1645         2490           7.56         145.1         5.2         27.7         705         1625         2740           7.75         145.1         5.5         27.4         706         1641         2456           7.75         145.1         4.0         26.7         39.1         657         1659         2245           7.75         145.1         4.1         3.75         37.5         37.5         175         1450         2245           8.48         144.1         4.1         4.25         38.3	29	4-2-54	100	4.12	.78	426	2211	234	7.03	149.5	5.1	3.25	16.3	760	1945 1945	2740 2580	4205 4295		
7.12         147.2         4.2         3.7         16.3         792         1714         2456           7.37         145.8         4.9         3.25         27.7         705         1665         2430           7.21         146.4         5.1         3.25         27.7         726         1655         2430           7.56         145.1         5.9         4.0         26.7         776         1655         2740           7.75         145.1         5.3         3.75         27.4         786         1610         2245           7.75         145.1         4.4         3.75         27.4         786         1610         2245           7.75         145.1         4.4         3.75         27.4         786         1610         2245           7.75         145.1         4.4         3.75         37.5         175         165         2245           7.75         145.1         4.8         3.75         38.4         775         1450*         2140           8.46         146.1         4.8         3.9         38.3         725         1450*         2140           8.46         146.2         38.7         48.9	02	4-7-4	100	4.02	.72	2111	2041	236	7.09	145.8	9.4	4.25	16.3	900	1715 1625	2490 2440	3850 3780		
7.37         145.8         4.9         3.25         27.7         705         1645         2490           7.21         146.4         5.1         3.25         27.7         725         1715         2490           7.56         145.1         5.9         4.0         26.7         935         1625         2740           7.56         145.1         5.3         3.75         27.4         786         1641         2456           7.73         145.1         5.3         3.75         27.4         786         1641         2456           7.75         145.1         4.4         3.75         27.5         1625         2245           7.75         145.1         4.4         3.75         38.1         650         1520         2245           7.75         144.4         4.7         4.25         38.4         775         1450         2156           8.46         144.4         4.7         4.25         38.3         723         1663         2340           8.46         144.4         4.25         38.3         723         1663         2196           8.46         141.5         4.25         49.8         740         1750		Average	100	4.05	92.	1007	2154	237	7.12	147.2	4.2	5.7	16.3	792	1714	5456	3922		
7.21         146.4         5.1         3.25         27.7         725         1715         2790           7.56         145.1         5.9         4.0         26.7         920         1625         2740           7.58         145.1         5.3         3.5         27.4         786         1640         2845           7.73         145.1         6.3         3.75         37.5         77.5         1650         2245           7.75         145.1         4.4         3.75         37.5         775         1850         2245           7.76         144.4         4.7         4.25         38.4         775         14508         2155           7.81         144.4         4.7         4.25         38.3         725         14508         2150           8.48         142.7         4.8         3.9         38.3         725         14508         2150           8.48         142.7         4.8         3.9         38.3         725         14508         2140           8.50         141.5         4.9         3.7         38.3         72         1653         2240           8.46         142.5         4.8         740         <	<b>L</b> †1	3-26-54	150	7.00	.78	905	2211	546	7.37	145.8	6.4	3.25	27.7	705	1625 1645	2315 2490	3920 3465		
7.56 145.1 5.9 4.0 26.7 935 1625 2155  7.38 145.1 5.3 5.5 27.4 786 1641 2456  7.73 145.8 5.3 3.75 39.1 635 1500 2245  7.75 145.1 4.4 3.75 37.5 775 120 1625*  7.81 144.4 4.8 3.9 38.3 725 1663 2396  8.48 142.7 4.4 4.2 4.2 48.9 560 1290 1960  8.40 141.5 5.5 3.75 50.5 585 1280 2180  8.40 142.2 4.9 4.25 49.8 740 1680 2065  8.41 142.1 4.9 4.2 40.8 740 1680 2065  8.51 142.1 4.9 4.1 40.7 638 1464 2095	95	3-31-54	150	4.06	.78	871	2211	240	7.21	1,46,4	5.1	3.25	27.7	725 740	1715	2790 2740	4205 4030		
7.38         145.1         5.3         3.5         27.4         786         1641         2456           7.73         143.8         5.3         3.75         39.1         635         1500         2245           7.75         145.1         4.4         3.75         37.5         775         1500         1625*           7.36         144.4         4.7         4.25         38.4         775         1450*         2140           7.81         144.4         4.8         3.9         38.3         725         1653         2366           8.48         142.7         4.4         4.25         38.3         725         1653         2366           8.46         141.5         5.5         3.75         50.5         585         1290         1200           8.46         142.2         4.9         4.25         49.8         740         1680         205           8.46         142.1         4.9         4.25         50.5         585         1290         2140           8.46         142.1         4.9         4.1         49.7         638         1464         2095	69	η-1-5 <del>4</del>	150	3.94	.78	888	2211	252	7.56	145.1	5.9	7.0	26.7	935 920	1625 1610	2155 2245	3500 3815		
7.75 145.8 5.3 3.75 39.1 635 1500 2245 7.75 145.1 4.4 3.75 37.5 775 1765 2630 7.96 144.4 4.8 3.9 38.3 725 1663 2346 8.48 142.7 4.4 4.2 48.9 565 1380 2180 8.60 141.5 5.5 3.75 50.5 585 1290 2140 8.46 142.2 4.9 4.25 49.8 740 1680 2065 8.51 142.1 4.9 4.1 49.7 638 1464 2095	-	Average	150	7.00	.78	888	2211	942	7.38	145.1	5.3	3.5	4.72	786	1641	2456	3823	*****	
7.75	94	3-24-54	200	3.96	.81	247	5296	258	7.73	143.8	5.3	3.75	39.1	635	1500° 1520	2245 1625*	3655 3500		
7.96 144.4 4.7 4.25 38.4 775 1450* 2155 2140 7781 144.4 4.8 5.9 38.3 725 1665 2346 2140 8.48 142.7 4.4 4.25 48.9 565 1380 2120 8.60 141.5 5.5 3.75 50.5 500 1290 1960 8.46 142.2 4.9 4.25 49.8 740 1680 2065 8.51 142.1 4.9 4.1 49.7 638 1464 2095	89	4-5-54	200	4.03	.81	217	5296	258	7.73	145.1	η·η	3.75	37.5	775 725	1765 1800	2630 2810	3850 4185		
7.81         144.4         4.8         3.9         36.3         723         1663         2396           8.48         142.7         4.4         4.25         48.9         565         1380         2120           8.60         141.5         5.5         3.75         5.05         585         1290         2140           8.46         142.2         4.9         4.25         49.8         740         1680         2065           8.51         142.1         4.9         4.1         49.7         638         1464         2095	<i>L</i> 9	t-6-54	200	3.99	.81	730	5296	265	7.96	<b>ተ-ተተ</b> ፒ	4.7	4.25	38.4	775 740	1450* 1730	2155 2140	3465 3690		
8.48 142.7 4.44 4.25 48.9 565 1380 2120 8.60 141.5 5.5 3.75 50.5 585 1290 2140 8.46 142.2 4.9 4.25 49.8 740 1680 2065 8.51 142.1 4.9 4.1 49.7 638 1464 2095 of concrete		Average	200	3.99	.81	728	5296	560	7.81	1,441	4.8	3.9	38.3	723	1663	2396	3724		
8.60 141.5 5.5 3.75 50.5 585 1290 2140 600 142.2 4.9 4.25 49.8 740 1680 2065 8.51 142.1 4.9 4.1 49.7 638 1464 2095 concrete	43	3-23-54	250	3.98	.81	†79	2296	282	8,48	142.7	<b>π.</b> π	4.25	148.9	565 600	1380 1415	2120 1820*	3320 3695		
8.46 142.2 4.9 4.25 49.8 740 1680 2065 8.51 142.1 4.9 4.1 49.7 638 1464 2095 of concrete	<u></u> <u>2</u>	3-29-54	250	3.95	.81	612	5296	586	8.60	141.5	5.5	3.75	50.5	585	1290	2140 1960	3500	***************************************	
8.51 142.1 4.9 4.1 49.7 638 1464 2095 of concrete	99	h-6-54	250	4.02	.81	578	5296	282	94.8	142.2	6.4	4.25	49.8	740	1680 1730	2065 2190	3885 3570		
*Not included in average ** Denotes volume of dry rodded coarse aggregate per unit volume of concrete		Average	250	5.98	.81	605	5256	283	8.51	142.1	4.9	4.1	7.64	638	1464	2095	3569		
	*Not ** Deno	included in tes volume c	average of dry rod	ded coars	ie aggr	egate p	er unit	volume	of conci	ete									

TABLE III-A

5-SACK CONCRETE DATA - MARYSVILLE FLY ASH

		П								<del></del>			
	T West												
kth	90 days												
ive Strength		4170 4115	4170 4330	4345 4135	4211	3960 4080	4100 4010	4150 3870	4028	4525 4715	3885 3885	4310 4100	4257
Compressive	7 days	2650 2740	2860 2775	2650 2935	2768	2755 2615	2755 2720	2755 2970	2762	2670 2740	2490 2420	2755 2615	2615
	3 dava	1730 1820	2015 1995	1855 2085	1917	1785 1785	1765 1855	2065 1945	1867	1785 1785	1800 1820	1835	1831
	1 day	795	1060	885 830	898	865 885	830 775	990	88	795 777	920 970	920 935	988
Darex,	fluid oz/cyd	30.9	50.9	32.6	31.5	42.3	42.3	42.3	42.3	50.5	148.9	148.9	4.64
Slump		5.5	4.75	6.75	5.7	5.0	4.75	0.4	9.4	4.75	0.4	4.5	†. †
Pressure	Air Content, Per Cent	5.5	4.5	0.9	5.3	5.5	4.5	5.1	5.3	5.0	5.1	5.2	5.1
Wt. Fresh	Concrete, lb/cu ft	143.8	145.4	143.2	144.1	142.3	142.3	142.8	142.5	141.8	142.5	142.0	142.1
Actual	w/c, gal/sk	19.9	6.27	6.54	24.9	6.82	6.93	6.72	6.82	7.24	7.05	7.14	7.14
rtions	Net Water	276	261	273	270	787	589	280	284	302	762	298	298
Material Proportions lb/cyd	Stone		2212	2212	2212	2212	2212	2212	2212	2212	2212	2212	2212
Materia	Sand	724	635	754	717	669	919	632	667	543	543	565	550
***	a	.78	.78	.78	.78	.78	٠. ه	. 78	.78	.78	82	. 78	.78
Actual Cement	lb/cyd Content sk/cyd	16.4	5.20	4.95	5.04	4.92	ħ6. ħ	5.02	7.96	5.01	5.05	5.00	5.02
Actual Fly Ash Cement	lb/cyd	150	150	150	150	200	200	200	200	250	250	250	250
Date Made		3-26-54	3-30-54	4-2-54	Average	η <b>ς-</b> ηΖ- <b>ς</b>	3-29-54	4-5-54	Average	5-51-54	4-6-54	4-6-4	Average
Batch	No.	817	47	9		54	51	63		57	65	77	

\*\*Denotes volume of dry rodded coarse aggregate per unit volume of concrete

TABLE IV-A

6-SACK CONCRETE DATA - MARYSVILLE FLY ASH

·	Т					<b>†</b>				1			
	l year								-				
th	90 даув												
Compressive Strength	28 days	3940 1450	4115 4240	1450 1400	9924	4115 4205	4330 4450	4510 4045	5424	4260 4205	4065 4135	3940 4135	4123
Compress	7 days	3075 2935	3040 3305	3250 3305	3152	3235 3145	3235 3110	2985 3160	3145	2970 2810	2755 2775	3005 3110	2901
	3 days	2280 2385	2475 2370	2545 2370	2404	2085 2190	2065	2120 2120	2113	2155 2120	2120 2155	2210 2155	2153
	1 day	1080	1185	1220 1310	1191	1150	990	1185	1126	970 990	1325	1165	1143
Darex,	oz/cyd	27.7	27.7	26.1	27.2	39.1	35.8	35.8	36.9	45.6	45.6	0.44	45.1
Slump	-111.	5.0	4.25	4.5	9.4	4.25	4.5	4.25	4.3	4.25	0.4	5.0	<b>†.</b> †
Pressure	Per Cent	5.6	5.9	0.9	5.8	6.1	5.5	5.2	5.6	5.2	0.9	5.5	5.6
Wt. Fresh	1b/cu ft	144.5	144.2	0.441	144.2	142.8	143.1	143.4	143.1	7.541	142.3	141.3	142.1
Actual	gal/sk	5.32	5.05	5.14	5.17	5.51	5.63	5.68	5.61	5.92	5.88	5.95	5.92
Material Proportions 1b/cyd	Water	566	253	257	259	275	281	78z	280	596	294	298	296
al Prop 1b/cyd	Stone	2126	2126	. 2126	2126	2126	2126	5156	2126	2126	2126	2126	2126
Materi	Sand	826	800	800	809	731	743	70 <del>/</del>	726	622	622	622	622
****		.75	.75	55.	.75	.75	5.	.75	.75	.75	.75	5	.75
Actual Ty Ash Cement	8k/cyd	5.95	6.01	6.00	5.99	5.95	5.93	00.9	5.96	6.01	5.99	5.95	5.98
Fly Ash Cement		100	100	100	100	150	150	150	150	200	200	500	200
Date Made		3-26-54	3-30-54	4-2-54	Average	3-24-54	3-29-54	45-5-4	Average	3-31-54	t2-7-4	ħ5-6-ħ	Average
Batch		61	55	19		‡	22	₫		28	8	72	