

ENGINEERING RESEARCH INSTITUTE  
THE UNIVERSITY OF MICHIGAN  
ANN ARBOR

Progress Report

STUDY OF FLY ASH FROM ST. CLAIR AND  
CONNERS CREEK STATIONS  
IN NONAIR-ENTRAINED CONCRETE

F. E. Legg, Jr.  
Assistant Professor of Engineering Materials  
and Assistant Supervisor  
Michigan State Highway Department Testing Laboratory

and

Ralph H. Vogler, Research Assistant

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DETROIT EDISON COMPANY  
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## SYNOPSIS

This report gives the results of a study of the use of fly ash from the St. Clair and Conners Creek stations of the Detroit Edison Company in nonair-entrained concrete. Previous reports have dealt with the use of fly ash from these stations in air-entrained concrete.

The strengths of comparable mixes made with the St. Clair and with the Conners Creek fly ashes are very close, indicating that there may be no appreciable difference in the effect of the two fly ashes on the compressive strength of nonair-entrained concrete up to 28 days of age. As in the earlier studies with air-entrained concrete, fly ash in lean mixes improves the strength over lean, plain cement mixes at early ages, while the fly ash in the richer mixes tends to depress the strength somewhat.

The fly ash suppresses the already small amount of air entrained in this concrete, thus making it more susceptible to frost action if exposed to weathering. Data to support this conclusion are not contained herein but will be reported separately. Mention of this is made here, however, as an important precaution in the use of nonair-entrained fly-ash concrete.

The strength of job concrete should not be predicted from the data contained in this report unless suitable safety factors are utilized to compensate for possible field variations in proportioning, mixing, and curing.

## OBJECTIVE

The purpose of this investigation is to study the properties of fly ash and concrete containing fly ash. The specific purpose of the phase of the research covered by this report is to determine the effect of fly ash from the St. Clair and Conners Creek stations of the Detroit Edison Company in nonair-entrained concrete, as indicated by workability, compressive strength, and volume change.

It is anticipated that the results of this investigation will provide useful information for those interested in the use of fly ash in portland-cement concrete.

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## INTRODUCTION

This report on the use of Detroit Edison Company fly ash covers the use of such ash from the St. Clair and Conners Creek power plants in nonair-entrained concrete. The data presented herein were developed in laboratory studies performed by the Engineering Research Institute of the University of Michigan, pursuant to a contract between the Institute and the Detroit Edison Company.

As in the preceding reports on air-entrained concrete containing fly ash, this report contains only data from compressive-strength tests up to 28 days of age. Results from compressive-strength specimens for testing at 90 days and one year and from volume-change bars will be given in a later report.

Some matter pertaining to test procedures which was covered previously will be omitted here to avoid repetition.

This report is concerned with the use of St. Clair and Conners Creek fly ashes in nonair-entrained concrete exclusively. It is recommended that this concrete be used only where it will not be exposed to freezing action in the presence of moisture.

## MIX DESIGN

The mix-design procedure was identical with that used in the previous studies of fly ash in concrete. Increased stone contents over those recommended by the American Concrete Institute for use in normal concrete were again employed in the fly-ash mixes to take full advantage of the plasticity of the mortar constituent provided by the addition of fly ash.

Concrete with cement contents ranging from 3.0 to 6.5 sacks per cubic yard of concrete was investigated. Cement contents were selected so that in most cases, a comparison could be made with the air-entrained concrete containing fly ash, the results of which were previously reported. St. Clair fly ash in four ash contents for 3.5-, 4.5-, and 5.5- sack mixes was used. Four ash contents of Conners Creek fly ash were used in mixes with 4.0, 5.0, and 5.5 sacks of cement per cubic yard. Mixes containing 6.5 sacks of cement without fly ash were made for comparison. In addition, mixes were made with four different amounts of

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St. Clair fly ash and 3.0 sacks of high-early-strength cement per cubic yard.

The "Recommended Practice for Selecting Proportions for Concrete" (ACI 613-54), the standard of the American Concrete Institute, was again used as the design basis for mixes containing no fly ash and was modified for use as the design basis for the fly-ash mixes.

## MATERIALS

The concrete materials were the same as those used previously, with the exception of the cement. The series was started using the same cement as was used in the previous series with St. Clair fly ash in air-entrained concrete. This cement was a blend of equal amounts of Huron, Peerless, and Wyandotte brands. Near the end of the making of the batches it was necessary to order additional cement. Due to labor troubles and the high demand for cement during the spring, it was not possible to obtain Wyandotte cement from suppliers in the Ann Arbor area. Thus, it was decided to substitute Peninsular cement. The results do not indicate that this substitution caused any noticeable difference in the concrete.

High-early-strength cement was used for one group of mixes. This consisted of a blend of equal amounts of Aetna, Huron, and Peerless brands. The results of chemical and physical tests of this cement are shown in the appendix.

The other materials were the same as previously reported, namely, one-inch maximum-size natural-gravel coarse aggregate, natural sand having a fineness modulus of 3.0, and fly ash from the St. Clair and Conners Creek stations. The fly ashes were from the same drums as those used in the study of fly ash in air-entrained concrete, and the analyses of these ashes have been presented in the reports on their use in air-entrained concrete.

## FABRICATION OF SPECIMENS AND TEST PROCEDURES

The methods of mixing, molding, curing, and testing remained the same as in the previous series with St. Clair fly ash in air-entrained concrete. The paraffined cardboard molds were again removed from the cylinders approximately 24 hours after molding, just prior to placing the cylinders in the moist-fog room for curing.

## DISCUSSION OF TEST RESULTS

The concrete-mix data and compressive-strength results are shown in detail in the appendix in the tables for the various cement contents and for the two fly ashes. Important aspects of the data have been summarized from these tables and are presented in the body of the report.

## 1. COARSE-AGGREGATE CONTENT

The greater amounts of coarse aggregate, which were workable in air-entrained concrete containing fly ash, were found to be equally workable in nonair-entrained concrete with both the St. Clair and Conners Creek ashes. The coarse-aggregate content was varied according to both the cement content and the fly-ash content since the increased fines in the mix from either source will give greater plasticity. Table I gives the values found satisfactory for one-inch maximum-size-pebble coarse aggregate and sand with a fineness modulus of 3.0 used in nonair-entrained mixes with St. Clair and Conners Creek fly ashes. The value used for mixes with no fly ash is as recommended by the American Concrete Institute. The value,  $V_s$ , is expressed as the dry-rodded volume of coarse aggregate per unit volume of concrete.

TABLE I

VOLUME,  $V_s$ , OF DRY-RODDED COARSE AGGREGATE  
PER UNIT VOLUME OF CONCRETE

| Fly Ash,<br>lb/cu yd | Cement Content, sack/cu yd |     |     |     |     |     |     |
|----------------------|----------------------------|-----|-----|-----|-----|-----|-----|
|                      | 3.0                        | 3.5 | 4.0 | 4.5 | 5.0 | 5.5 | 6.5 |
| 0                    | .64                        | .64 | .64 | .64 | .64 | .64 | .64 |
| 50                   |                            |     |     | .72 | .72 | .72 |     |
| 70                   | .68                        |     |     |     |     |     |     |
| 100                  |                            | .72 | .72 | .75 | .75 | .75 |     |
| 140                  | .72                        |     |     |     |     |     |     |
| 150                  |                            | .75 | .75 | .78 | .78 | .78 |     |
| 200                  |                            | .78 | .78 | .81 | .81 | .81 |     |
| 210                  | .76                        |     |     |     |     |     |     |
| 250                  |                            | .81 | .81 |     |     |     |     |
| 280                  | .80                        |     |     |     |     |     |     |

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## 2. WORKABILITY OF LEAN MIXES

In the low-cement-content mixes without fly ash (3-sack, particularly), there was not sufficient fine material for easy finishing. The fresh concrete had the appearance of a wet sand-gravel mixture. As soon as the concrete was dumped from the mixer, large quantities of water drained from the mixture. As a result, the concrete caked so that low slumps were obtained with little reference to the amount of water added at the mixer.

The addition of at least 70 pounds of fly ash per cubic yard of concrete to the 3-sack mixes provides the necessary fines to give the concrete plasticity and workability. The 3.5-sack concrete also requires some fly ash for good workability. With the air-entrained concrete, the addition of fly ash was not necessary for good plasticity in the 3.5-sack mixes since the entrained air bubbles acted to supplement the fine material in the mix.

## 3. COMPRESSIVE STRENGTH

Average values of compressive strengths up to 28 days of age are presented in Tables II and III. The results are much the same as with these fly ashes in air-entrained concrete, in that the fly ash in the lean mixes improves the compressive strength over the lean, plain cement mixes at all ages through 28 days, while fly ash in the richer mixes depresses the strength somewhat in nearly every case.

There do not appear to be any great differences in the strengths attained for comparable mixes with the two fly ashes. Variations between comparable 5.5-sack mixes with St. Clair and Conners Creek fly ashes up to 28 days of age appear to be in the range as might be caused by experimental error.

The mixes containing 3 sacks of high-early-strength cement plus St. Clair fly ash were investigated because there have been reports indicating that such a mixture is presently being used in some operations. As indicated previously, when fly ash is not used in such a mix, it is unworkable. The addition of fly ash improves the physical characteristics, resulting in a strength improvement over the plain cement mix from the first day. These mixes with high-early-strength cement show strength improvement over mixes with a higher cement content but made with regular cement.

Table IV shows the strength of the fly-ash mixes at each age expressed as a percent of the strength of the plain cement mixes of the same cement content.

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TABLE II

SUMMARY OF RESULTS  
ST. CLAIR FLY ASH

| Nominal Cement Content, sack/cu yd | Actual Cement Content, sack/cu yd | Fly Ash, lb/cu yd | Net Mixing Water 1b/cu yd | Air Content, percent | Slump, in. | Compressive Strength, psi |        |         |
|------------------------------------|-----------------------------------|-------------------|---------------------------|----------------------|------------|---------------------------|--------|---------|
|                                    |                                   |                   |                           |                      |            | 1 day                     | 7 days | 28 days |
| (High-Early-Strength Cement)       |                                   |                   |                           |                      |            |                           |        |         |
| 3.0                                | 3.01                              | 0                 | 272                       | 10.87                | 1.6        | 2.92                      | 523    | 1606    |
|                                    | 3.01                              | 70                | 259                       | 10.37                | 1.1        | 4.58                      | 593    | 1934    |
|                                    | 3.00                              | 140               | 264                       | 10.56                | 0.8        | 4.58                      | 633    | 1894    |
|                                    | 3.01                              | 210               | 262                       | 10.46                | 0.9        | 5.00                      | 686    | 2019    |
| 3.5                                | 2.95                              | 280               | 284                       | 11.36                | 0.9        | 4.58                      | 617    | 1841    |
|                                    | 3.50                              | 0                 | 268                       | 9.21                 | 1.8        | 2.50                      | 407    | 1593    |
|                                    | 3.51                              | 100               | 250                       | 8.57                 | 1.1        | 3.83                      | 507    | 2000    |
|                                    | 3.52                              | 150               | 258                       | 8.83                 | 0.9        | 5.08                      | 493    | 1940    |
| 4.0                                | 3.53                              | 200               | 256                       | 8.80                 | 1.0        | 3.75                      | 515    | 1893    |
|                                    | 3.50                              | 250               | 263                       | 9.01                 | 0.9        | 4.17                      | 576    | 2017    |
|                                    | 4.49                              | 0                 | 261                       | 6.96                 | 1.8        | 3.25                      | 622    | 2244    |
|                                    | 4.50                              | 50                | 246                       | 6.58                 | 1.1        | 3.00                      | 922    | 2898    |
| 4.5                                | 4.50                              | 100               | 253                       | 6.75                 | 1.0        | 4.17                      | 891    | 2918    |
|                                    | 4.49                              | 150               | 260                       | 6.94                 | 0.9        | 4.17                      | 765    | 2438    |
|                                    | 4.52                              | 200               | 277                       | 7.40                 | 0.9        | 3.83                      | 816    | 2658    |
|                                    | 5.48                              | 0                 | 258                       | 5.57                 | 1.9        | 4.08                      | 1202   | 3189    |
| 5.5                                | 5.56                              | 50                | 251                       | 5.49                 | 1.1        | 4.58                      | 1193   | 3528    |
|                                    | 5.55                              | 100               | 262                       | 5.72                 | 0.9        | 4.33                      | 1131   | 3162    |
|                                    | 5.50                              | 150               | 276                       | 6.02                 | 0.9        | 4.33                      | 1069   | 3023    |
|                                    | 5.51                              | 200               | 284                       | 6.21                 | 1.0        | 4.25                      | 1024   | 3003    |
| 6.5                                | 6.47                              | 0                 | 262                       | 4.85                 | 1.7        | 5.00                      | 1520   | 3689    |
|                                    |                                   |                   |                           |                      |            |                           |        | 4690    |

TABLE III

SUMMARY OF RESULTS  
CONNERS CREEK FLY ASH

| Nominal Cement Content, sack/cu yd | Actual Cement Content, sack/cu yd | Fly Ash, lb/cu yd | Net Mixing Water 1b/cu yd | Air Content, percent | Slump, in. | Compressive Strength, psi |        |         |         |
|------------------------------------|-----------------------------------|-------------------|---------------------------|----------------------|------------|---------------------------|--------|---------|---------|
|                                    |                                   |                   |                           |                      |            | 1 day                     | 7 days | 28 days | 90 days |
| 4.0                                | 4.02                              | 0                 | 273                       | 8.19                 | 1.2        | 4.17                      | 455    | 1908    | 2768    |
|                                    | 4.02                              | 100               | 252                       | 7.55                 | 1.0        | 3.25                      | 617    | 2423    | 3584    |
|                                    | 4.01                              | 150               | 250                       | 7.52                 | 1.0        | 3.75                      | 592    | 2325    | 3898    |
|                                    | 4.00                              | 200               | 263                       | 7.92                 | 1.0        | 4.08                      | 688    | 2450    | 3957    |
|                                    | 4.00                              | 250               | 275                       | 8.26                 | 0.9        | 5.25                      | 658    | 2213    | 3643    |
|                                    | 4.97                              | 0                 | 259                       | 6.22                 | 1.9        | 4.08                      | 890    | 2856    | 3568    |
| 5.0                                | 4.99                              | 50                | 254                       | 6.10                 | 1.1        | 3.67                      | 1042   | 3349    | 4254    |
|                                    | 5.01                              | 100               | 261                       | 6.27                 | 1.0        | 4.67                      | 961    | 3144    | 4093    |
|                                    | 5.01                              | 150               | 274                       | 6.59                 | 0.8        | 5.17                      | 887    | 2851    | 3883    |
|                                    | 5.05                              | 200               | 277                       | 6.66                 | 0.8        | 4.00                      | 952    | 2870    | 4063    |
|                                    | 5.48                              | 0                 | 258                       | 5.57                 | 1.9        | 4.08                      | 1202   | 3189    | 4114    |
| 5.5                                | 5.47                              | 50                | 262                       | 5.71                 | 1.1        | 4.17                      | 1056   | 3278    | 4584    |
|                                    | 5.50                              | 100               | 264                       | 5.75                 | 1.0        | 4.00                      | 1158   | 3148    | 4024    |
|                                    | 5.47                              | 150               | 274                       | 5.98                 | 1.0        | 4.83                      | 1106   | 3061    | 3984    |
|                                    | 5.50                              | 200               | 292                       | 6.38                 | 1.0        | 3.92                      | 955    | 3031    | 4201    |
| 6.5                                | 6.47                              | 0                 | 262                       | 4.85                 | 1.7        | 5.00                      | 1520   | 3689    | 4690    |

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TABLE IV

COMPRESSIVE STRENGTH OF FLY-ASH MIXES EXPRESSED AS PERCENT OF STRENGTH  
OF PLAIN CEMENT MIXES OF THE SAME CEMENT CONTENT.

| Cement,<br>sack/cu yd                      | Source           | Fly Ash<br>lb/cu yd | 1 day | 7 days | 28 days |
|--|------------------|---------------------|-------|--------|---------|
| 3.0<br>(High-Early-<br>Strength<br>Cement) | St. Clair        | 70                  | 113   | 120    | 128     |
|  |                  | 140                 | 121   | 118    | 131     |
|  |                  | 210                 | 131   | 126    | 151     |
|  |                  | 280                 | 118   | 115    | 141     |
| 3.5  | St. Clair        | 100                 | 125   | 126    | 142     |
|  |                  | 150                 | 121   | 122    | 145     |
|  |                  | 200                 | 127   | 119    | 146     |
|  |                  | 250                 | 142   | 127    | 137     |
| 4.0  | Connors<br>Creek | 100                 | 136   | 127    | 129     |
|  |                  | 150                 | 130   | 122    | 141     |
|  |                  | 200                 | 151   | 128    | 142     |
|  |                  | 250                 | 145   | 116    | 132     |
| 4.5  | St. Clair        | 50                  | 148   | 129    | 127     |
|  |                  | 100                 | 143   | 130    | 115     |
|  |                  | 150                 | 123   | 109    | 111     |
|  |                  | 200                 | 131   | 118    | 125     |
| 5.0  | Connors<br>Creek | 50                  | 117   | 117    | 119     |
|  |                  | 100                 | 108   | 110    | 115     |
|  |                  | 150                 | 100   | 100    | 109     |
|  |                  | 200                 | 107   | 100    | 114     |
| 5.5  | St. Clair        | 50                  | 99    | 110    | 105     |
|  |                  | 100                 | 94    | 99     | 101     |
|  |                  | 150                 | 89    | 95     | 97      |
|  |                  | 200                 | 85    | 94     | 101     |
| 5.5  | Connors<br>Creek | 50                  | 88    | 103    | 111     |
|  |                  | 100                 | 96    | 99     | 98      |
|  |                  | 150                 | 92    | 96     | 97      |
|  |                  | 200                 | 79    | 95     | 102     |

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The average strengths for each of the cement and fly-ash contents have been plotted against the age in Figures 1 to 7. Strength gain is generally orderly, as in the case of the fly ashes used in air-entrained concrete.

## 4. AIR CONTENT OF CONCRETE

This study was designed and conducted as an investigation of fly ash in nonair-entrained concrete. However, all cement entrains a small amount of air to give the concrete some degree of durability in weathering. The air content of the mixes with both St. Clair and Conners Creek fly ashes was considerably below that of the plain cement mixes. The air contents for the fly-ash mixes range from 0.8 to 1.1 percent with an average of 0.97 percent. The air contents of the plain cement mixes range from 1.2 to 1.9 percent with an average of 1.70 percent entrained air.

While the air content in both cases is too small to prevent deterioration of concrete exposed to weathering in the presence of moisture, the fly-ash concrete, because of its lower air content, will be more susceptible to frost action than the plain cement concrete. Thus, it becomes increasingly necessary to use proper air entrainment in all fly-ash concrete which may be exposed to the weather in northern climates, particularly where moisture is supplied to the concrete, such as in the case of sidewalks, pavement slabs, or retaining walls with poorly drained backfills.

Data to support the above observations on the weather resistance of fly-ash concrete are now being acquired and will be separately reported. For view of its importance, however, salient features are here presented.

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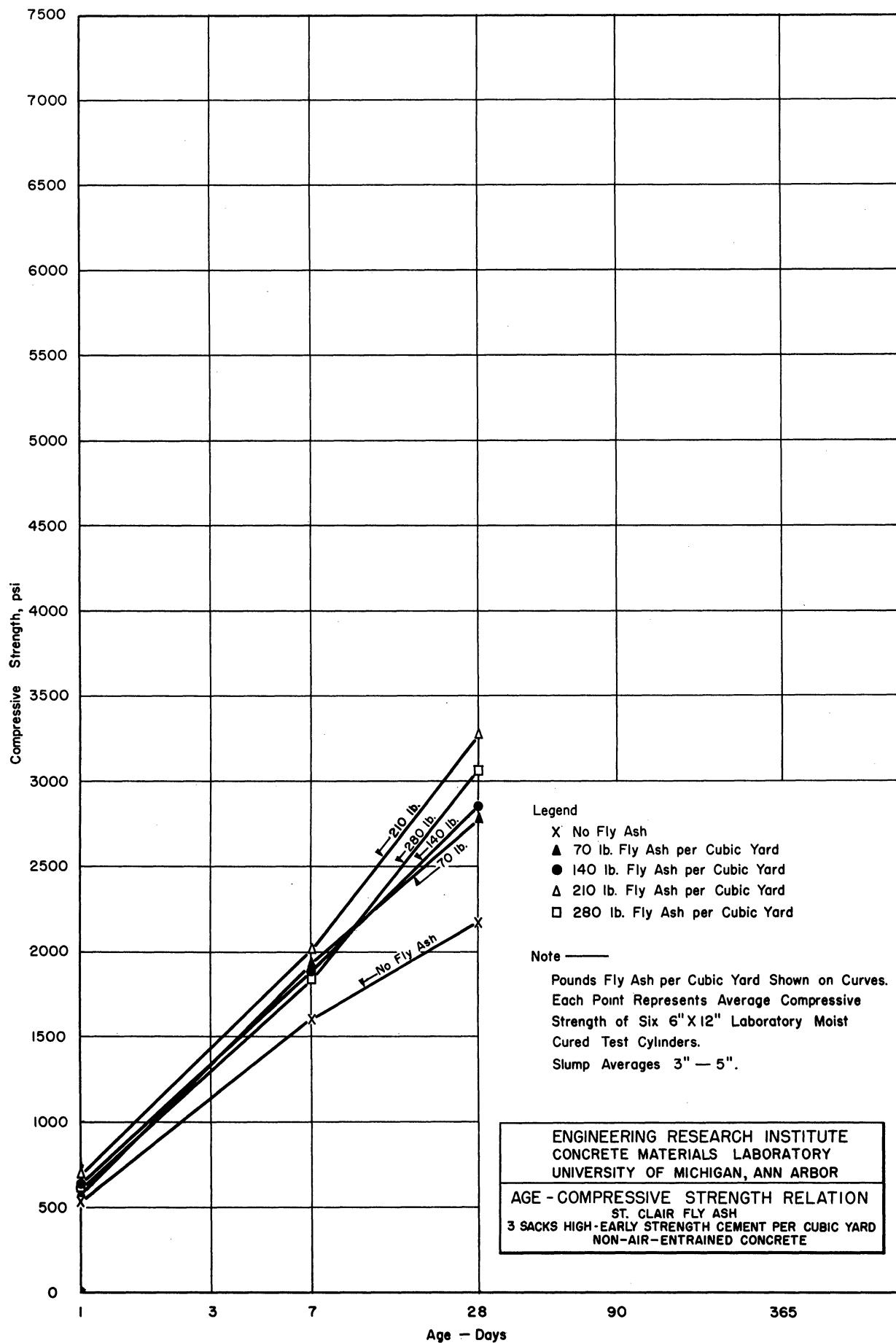


Fig. 1

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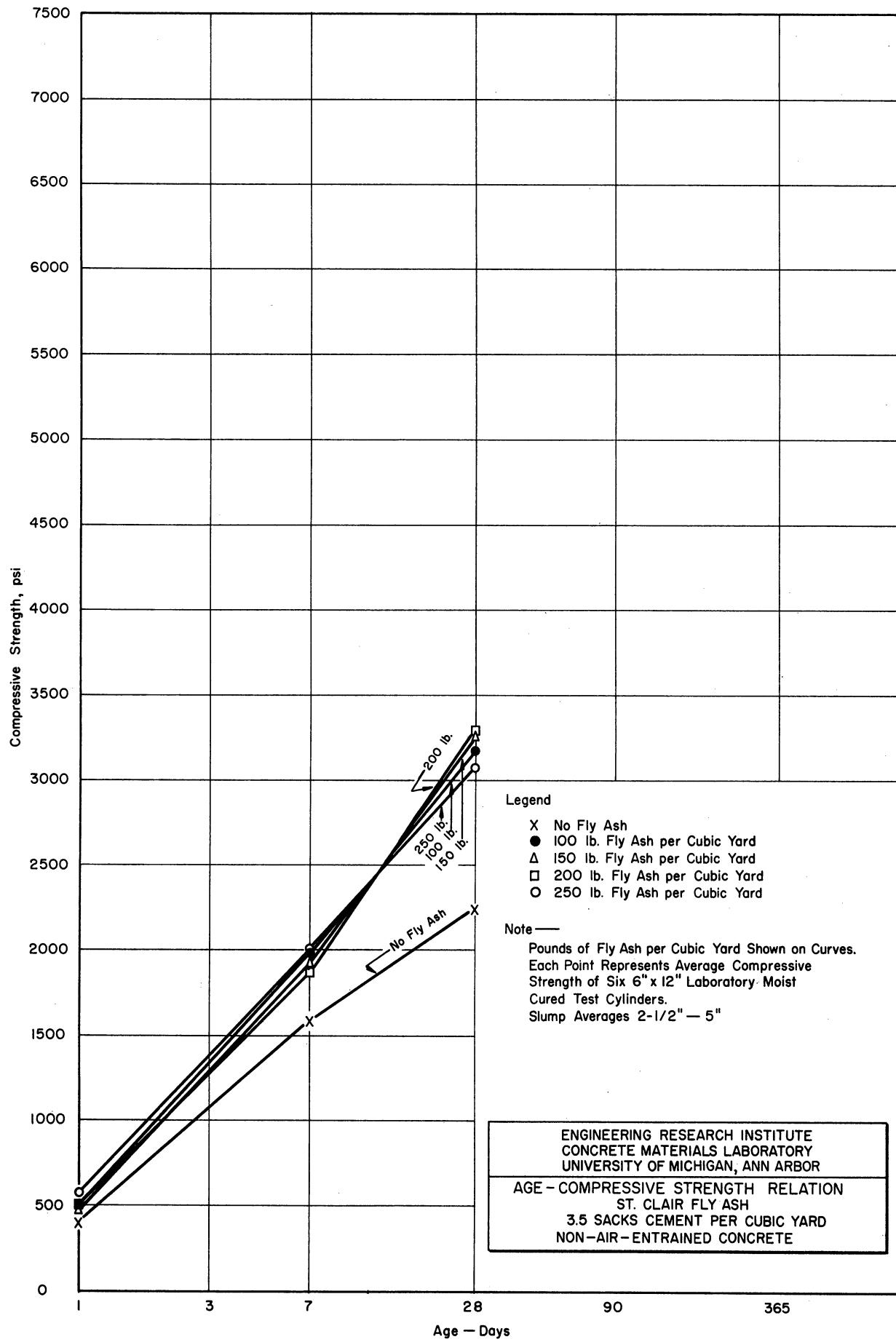


Fig. 2

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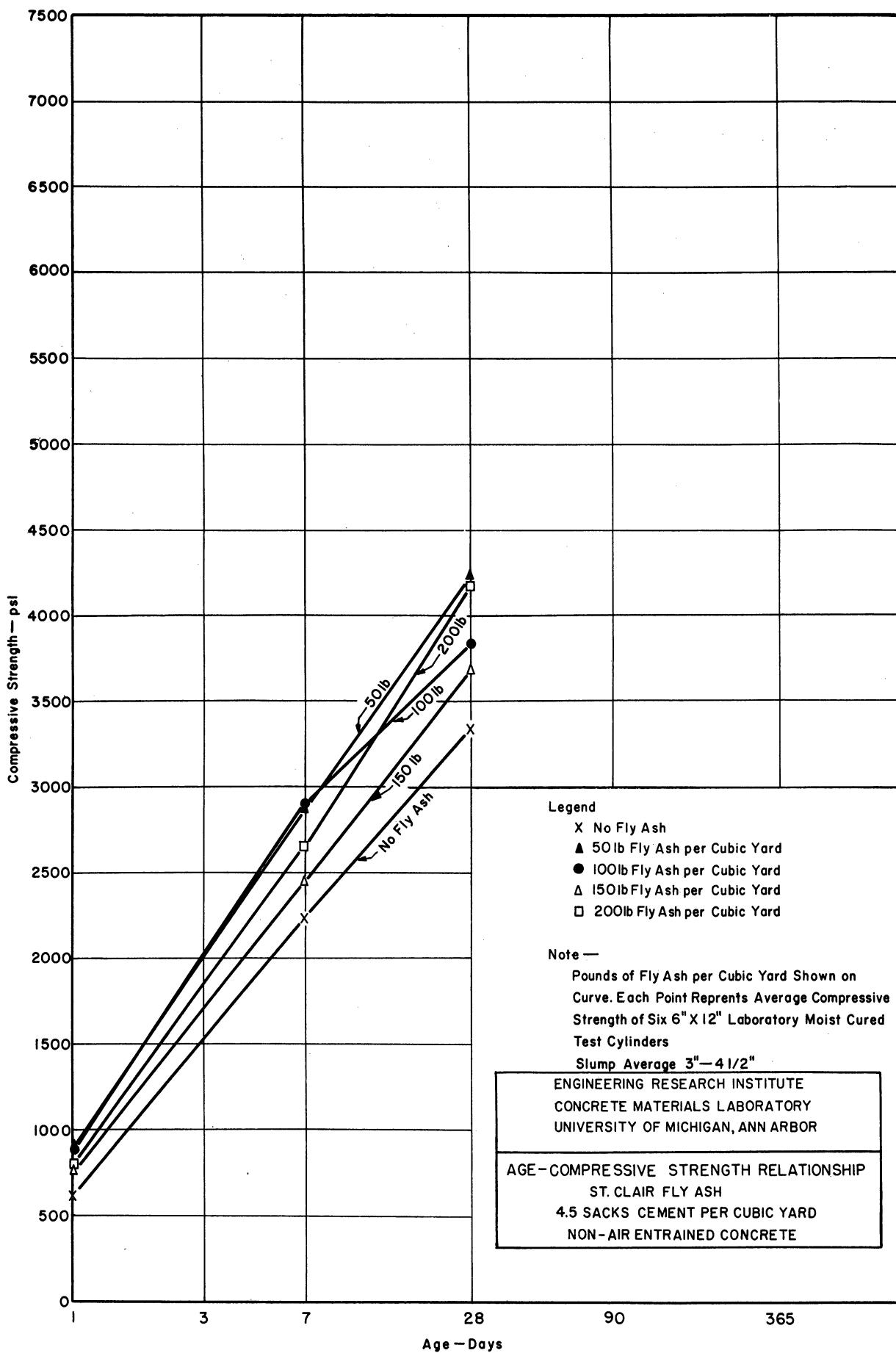


Fig. 3

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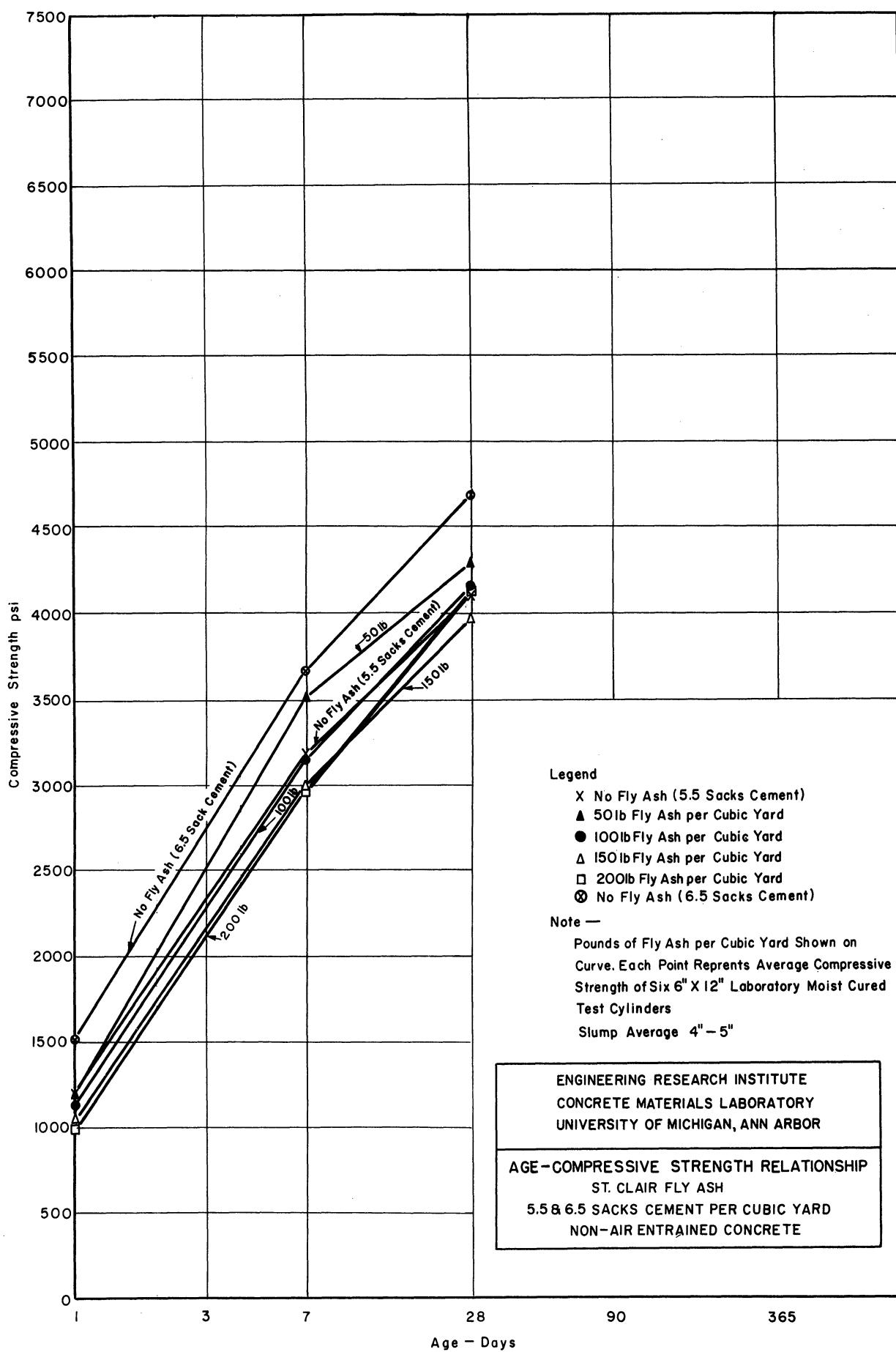


Fig. 4

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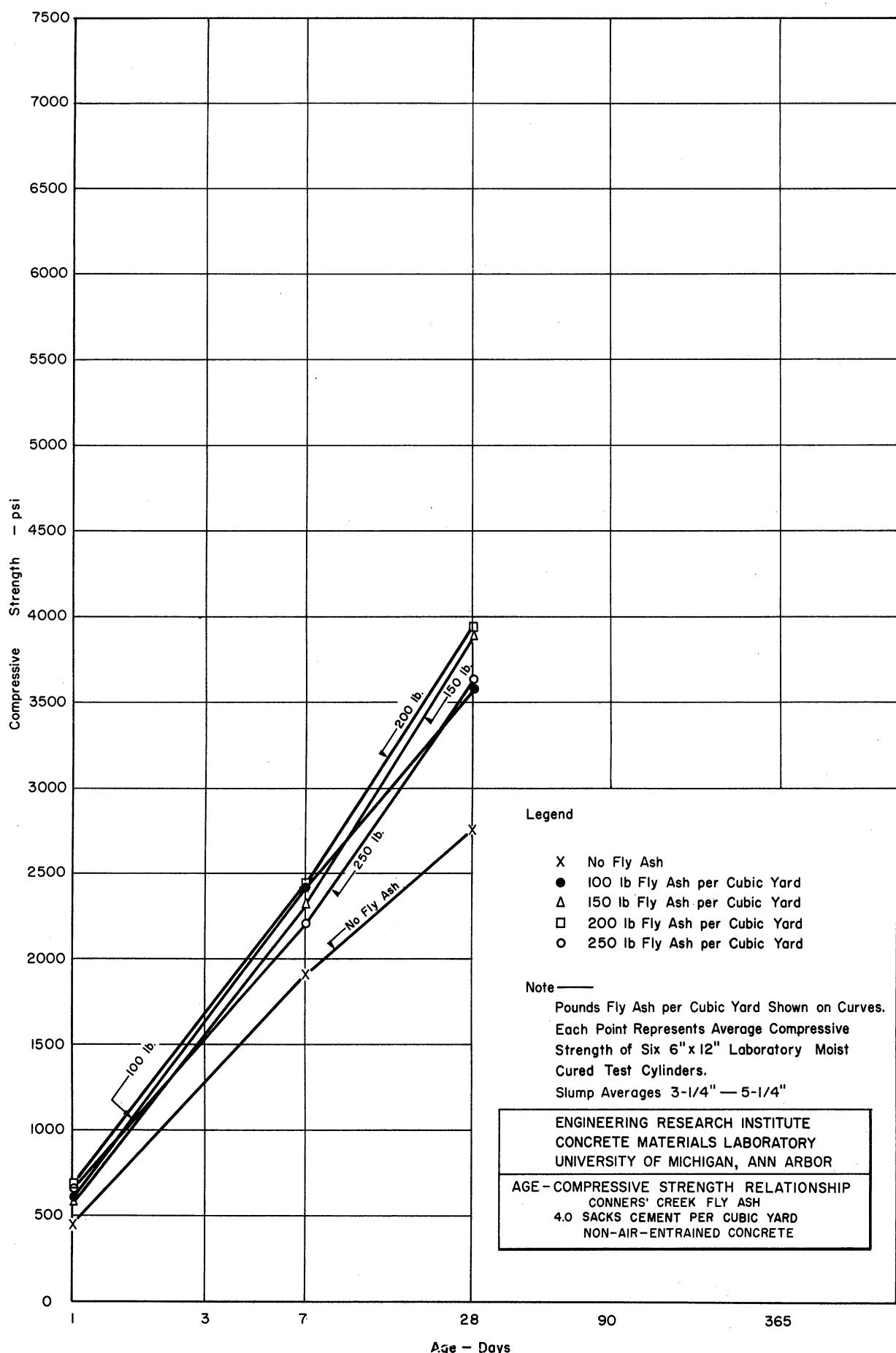


Fig. 5

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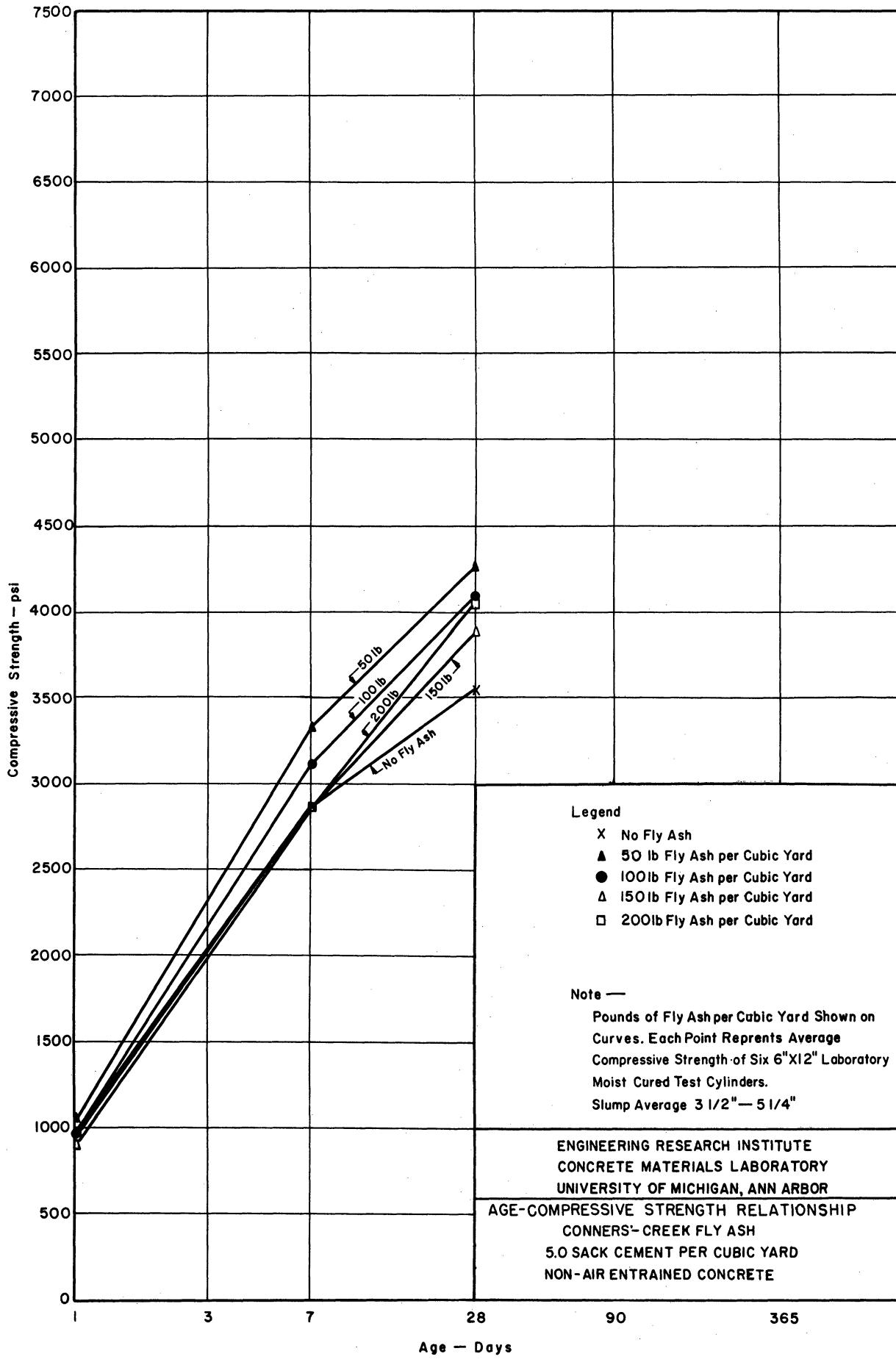


Fig. 6

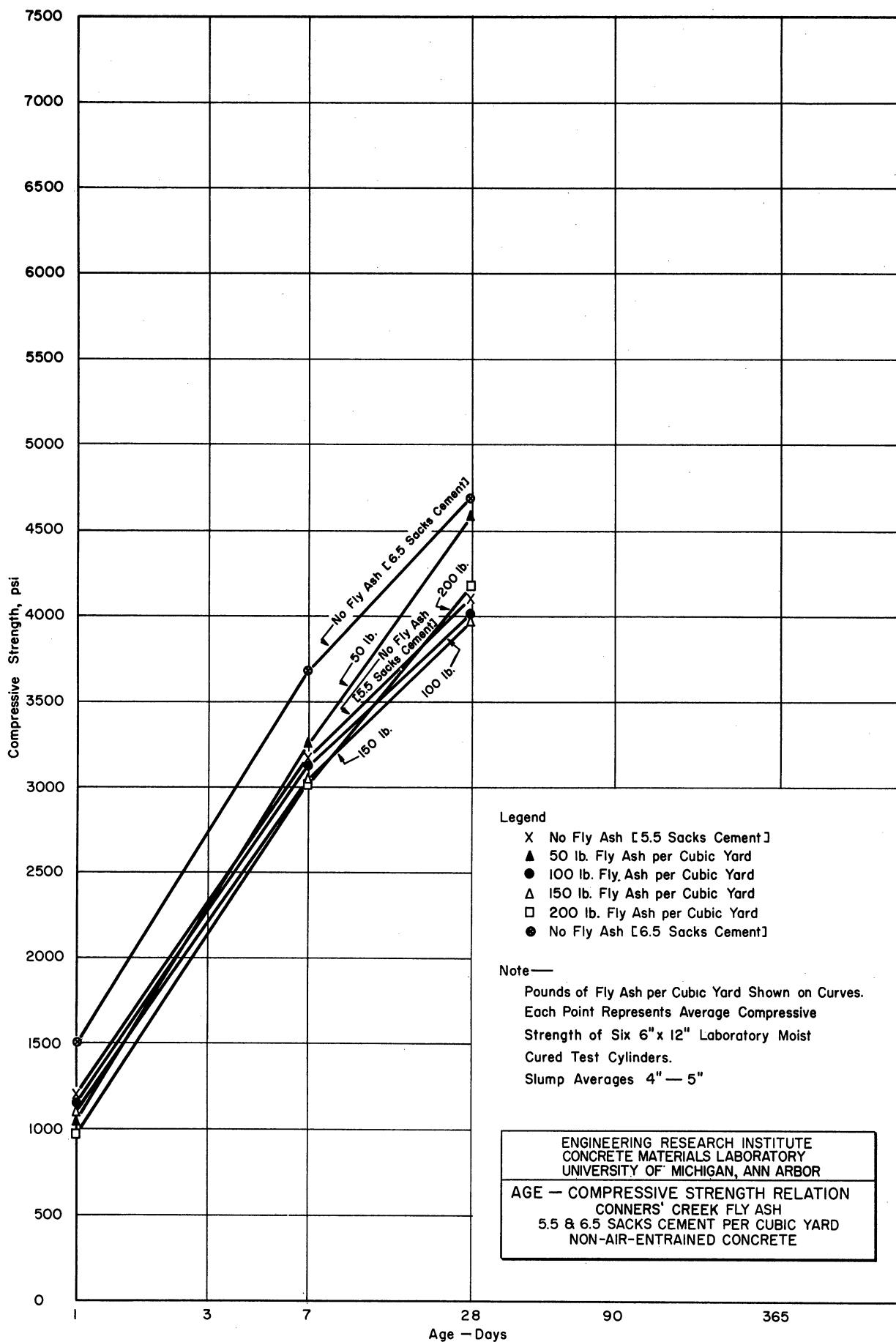


Fig. 7

## APPENDIX

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TABLE I-A

PROPERTIES OF HIGH-EARLY-STRENGTH CEMENT

55C-120

Physical Properties

|                              |              |
|------------------------------|--------------|
| Normal consistency, percent  | 26.4         |
| Time of set, Gillmore        |              |
| Initial                      | 3 hr, 50 min |
| Final                        | 5 hr, 50 min |
| Autoclave expansion, percent | 0.07         |
| Air in mortar, percent       | 9.9          |
| Tensile strength, psi        |              |
| 1 day                        | 278          |
| 3 days                       | 402          |
| 7 days                       | 422          |
| 28 days                      | 473          |
| Compressive strength, psi    |              |
| 1 day                        | 1750         |
| 3 days                       | 3933         |
| 7 days                       | 4292         |
| 28 days                      | 5650         |

Chemical Properties

|                  | <u>Ultimate analysis</u>       | <u>Percent by weight</u> | <u>Proximate analysis</u>                   | <u>Percent by weight</u>                 |
|------------------|--------------------------------|--------------------------|---|--|
| Silicon dioxide  | SiO <sub>2</sub>               | 20.6                     | Loss on ignition                            | 2.0                                      |
| Aluminum oxide   | Al <sub>2</sub> O <sub>3</sub> | 5.6                      | Tricalcium silicate                         | 3CaO.SiO <sub>2</sub> 50.0               |
| Ferric oxide     | Fe <sub>2</sub> O <sub>3</sub> | 3.0                      | Dicalcium silicate                          | 2CaO.SiO <sub>2</sub> 22.0               |
| Calcium oxide    | CaO                            | 63.0                     | Tricalcium aluminate                        | 3CaO.Al <sub>2</sub> O <sub>3</sub> 10.0 |
| Magnesium oxide  | MgO                            | 2.3                      | Tetracalcium                                | 4CaO.Al <sub>2</sub> O <sub>3</sub> .    |
| Sulfur trioxide  | SO <sub>3</sub>                | 2.9                      | aluminoferrite                              | Fe <sub>2</sub> O <sub>3</sub> 9.0       |
| Loss on ignition |                                | 2.1                      | Calcium sulphate                            | CaSO <sub>4</sub> 5.0                    |
| Sodium oxide     | Na <sub>2</sub> O              | 0.21                     | Magnesia                                    | MgO 2.0                                  |
| Potassium oxide  | K <sub>2</sub> O               | 0.66                     | Total alkali expressed as Na <sub>2</sub> O | 0.65                                     |

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TABLE II - A

3-SACK, REGULAR-CONCRETE DATA — ST. CLAIR FLY ASH  
(HIGH EARLY-STRENGTH CEMENT, TYPE III)

| Batch No. | Date Made | Fly Ash, lb./cu. yd. | Actual Cement Content, sack/cu. yd. | Material Proportions. |                    |                | W/C, lb./cu. yd. | Concrete, Net Water gal./sack | Wt. Fresh Concrete, lb./cu. ft. | Air Content, percent | Slump, in.              | Compressive Strength, psi (6" x 12" cylinders) |
|-----------|-----------|----------------------|-------------------------------------|-----------------------|--------------------|----------------|------------------|-------------------------------|---------------------------------|----------------------|-------------------------|--|
|           |           |                      |                                     | Sand, lb./cu. yd.     | Stone, lb./cu. yd. | Water, cu. ft. |                  |                               |                                 |                      |                         |  |
| 214       | 4-11-55   | 0                    | 3.01                                | 0.64                  | 1612               | 1814           | 269              | 10.77                         | 149.8                           | 2.1                  | 1.25                    | 580 1890 2455                                  |
| 249       | 5-12-55   | 0                    | 3.03                                | 0.64                  | 1553               | 1814           | 267              | 10.69                         | 148.3                           | 1.3                  | 3.5                     | 565 1750 2615                                  |
| 295       | 6-14-55   | 0                    | 3.00                                | 0.64                  | 1569               | 1814           | 279              | 11.16                         | 148.0                           | 1.5                  | 4.0                     | 620 1715 2295                                  |
| Average   | 0         | 3.01                 | 0.64                                | 1578                  | 1814               | 272            | 10.87            | 148.7                         | 1.6                             | 2.92                 | 523                     | 1680 2350 1606 1680 2182                       |
| 216       | 4-11-55   | 70                   | 2.99                                | 0.68                  | 1483               | 1928           | 264              | 10.56                         | 150.4                           | 1.3                  | 2.75                    | 600 1890 2915                                  |
| 245       | 4-27-55   | 70                   | 3.04                                | 0.68                  | 1451               | 1928           | 258              | 10.32                         | 150.9                           | 1.0                  | 5.75                    | 615 1945 2705                                  |
| 293       | 6-13-55   | 70                   | 2.99                                | 0.68                  | 1464               | 1928           | 256              | 10.22                         | 149.7                           | 0.9                  | 5.25                    | 555 1890 2720                                  |
| Average   | 70        | 3.01                 | 0.68                                | 1459                  | 1928               | 259            | 10.37            | 150.3                         | 1.1                             | 4.58                 | 530                     | 1835 2930 1934 2791                            |
| 215       | 4-11-55   | 140                  | 3.00                                | 0.72                  | 1510               | 2041           | 264              | 10.57                         | 151.2                           | 1.2                  | 4.0                     | 760 2140 2860                                  |
| 241       | 4-25-55   | 140                  | 3.01                                | 0.72                  | 1501               | 2041           | 269              | 10.77                         | 150.4                           | 0.6                  | 4.75                    | 710 2140 3250*                                 |
| 296       | 6-14-55   | 140                  | 3.00                                | 0.72                  | 1259               | 2041           | 258              | 10.33                         | 149.4                           | 0.7                  | 5.0                     | 560 1680 2580                                  |
| Average   | 140       | 3.00                 | 0.72                                | 1290                  | 2041               | 264            | 10.56            | 150.3                         | 0.8                             | 4.58                 | 570 1610 2650           |  |
| 217       | 4-11-55   | 210                  | 3.02                                | 0.76                  | 1112               | 2155           | 268              | 10.72                         | 152.1                           | 1.2                  | 5.00                    | 585 2030 3075                                  |
| 239       | 4-25-55   | 210                  | 3.01                                | 0.76                  | 1080               | 2155           | 267              | 10.67                         | 150.4                           | 0.7                  | 5.75                    | 635 1800 2175                                  |
| 291       | 6-13-55   | 210                  | 3.00                                | 0.76                  | 1086               | 2155           | 250              | 10.00                         | 149.5                           | 0.7                  | 4.25                    | 655 1800 2670                                  |
| Average   | 210       | 3.01                 | 0.76                                | 1093                  | 2155               | 262            | 10.46            | 150.7                         | 0.9                             | 5.00                 | 775 2155 3885           |  |
| 218       | 4-14-55   | 280                  | 2.99                                | 0.80                  | 913                | 2268           | 278              | 11.14                         | 150.2                           | 1.2                  | 3.25                    | 740 2030 3110                                  |
| 240       | 4-25-55   | 280                  | 2.86                                | 0.80                  | 1065               | 2268           | 287              | 11.50                         | 149.5                           | 1.0                  | 4.50                    | 585 1910 2815                                  |
| 292       | 6-13-55   | 280                  | 3.01                                | 0.80                  | 856                | 2268           | 286              | 11.43                         | 148.4                           | 0.6                  | 6.0                     | 515 1765 2790                                  |
| Average   | 280       | 2.95                 | 0.80                                | 938                   | 2268               | 284            | 11.36            | 149.4                         | 0.9                             | 4.58                 | 535 1715 3320 1841 3074 |  |

\* Not included in average

\*\* Denotes volume of dry-rodded coarse aggregate per unit volume of concrete

TABLE III - A

## 3-5-SLACK REGULAR-CONCRETE DATA — ST. CLAIR FLY ASH

| Batch No. | Date Made | Fly Ash, 1b/cu yd | Actual Cement Content, sack/cu yd | Material Proportions, 1b/cu yd | W/C, Weight, lb./cu ft. | Pressure Concrete, lb./cu ft. | Slump, in. | Compressive Strength, psi (6" x 12" Cylinders) |        |         |         |        |
|-----------|-----------|-------------------|-----------------------------------|--------------------------------|-------------------------|-------------------------------|------------|--|--------|---------|---------|--------|
|           |           |                   |                                   |                                |                         |                               |            | 1 day  | 7 days | 28 days | 90 days | 1 year |
| 206       | 4-7-55    | 0                 | 3.54                              | 0.64                           | 1553                    | 1814                          | 256        | 8.79   | 149.9  | 2.3     | 1.0     | 460    |
| 234       | 5-19-55   | 0                 | 3.49                              | 0.64                           | 1546                    | 1814                          | 276        | 9.48   | 148.1  | 1.6     | 4.5     | 440    |
| 266       | 5-27-55   | 0                 | 3.48                              | 0.64                           | 1568                    | 1814                          | 273        | 9.35   | 148.5  | 1.4     | 2.0     | 350    |
| Average   | 0         | 3.50              | 0.64                              | 1556                           | 1814                    | 268                           | 9.21       | 148.8  | 1.8    | 2.5     | 450     | 1590   |
| 201       | 4-5-55    | 100               | 3.52                              | 0.72                           | 1284                    | 2041                          | 257        | 8.14   | 150.6  | 1.2     | 2.5     | 600    |
| 225       | 4-15-55   | 100               | 3.50                              | 0.72                           | 1321                    | 2041                          | 260        | 8.95   | 152.1  | 1.1     | 6.0     | 490    |
| 278       | 6-2-55    | 100               | 3.51                              | 0.72                           | 1299                    | 2041                          | 252        | 8.64   | 151.2  | 1.0     | 3.0     | 440    |
| Average   | 100       | 3.51              | 0.72                              | 1301                           | 2041                    | 250                           | 8.57       | 151.3  | 1.1    | 3.85    | 507     | 2000   |
| 198       | 4-5-55    | 150               | 3.52                              | 0.75                           | 1139                    | 2126                          | 259        | 8.88   | 151.1  | 1.1     | 4.0     | 565    |
| 256       | 5-19-55   | 150               | 3.51                              | 0.75                           | 1139                    | 2126                          | 261        | 8.95   | 150.7  | 0.8     | 6.0     | 510    |
| 279       | 6-2-55    | 150               | 3.53                              | 0.75                           | 1139                    | 2126                          | 253        | 8.66   | 150.9  | 0.8     | 5.25    | 565    |
| Average   | 150       | 3.52              | 0.75                              | 1139                           | 2126                    | 258                           | 8.85       | 150.9  | 0.9    | 5.08    | 495     | 3605   |
| 199       | 4-5-55    | 200               | 3.49                              | 0.78                           | 995                     | 2211                          | 265        | 9.09   | 149.5  | 1.1     | 4.0     | 530    |
| 231       | 4-19-55   | 200               | 3.55                              | 0.78                           | 988                     | 2211                          | 245        | 8.40   | 151.1  | 1.3     | 4.05    | 495    |
| 267       | 5-27-55   | 200               | 3.54                              | 0.78                           | 988                     | 2211                          | 259        | 8.90   | 151.3  | 0.6     | 4.0     | 405    |
| Average   | 200       | 3.53              | 0.78                              | 990                            | 2211                    | 256                           | 8.80       | 150.6  | 1.0    | 3.75    | 495     | 3620   |
| 197       | 3-10-55   | 250               | 3.47                              | 0.81                           | 874                     | 2296                          | 263        | 9.05   | 148.9  | 1.0     | 4.0     | 610    |
| 236       | 4-21-55   | 250               | 3.54                              | 0.81                           | 859                     | 2296                          | 260        | 8.95   | 151.3  | 0.9     | 4.0     | 645    |
| 294       | 6-13-55   | 250               | 3.50                              | 0.81                           | 859                     | 2296                          | 265        | 9.08   | 149.9  | 0.8     | 4.5     | 475    |
| Average   | 250       | 3.50              | 0.81                              | 864                            | 2296                    | 263                           | 9.01       | 150.0  | 0.9    | 4.17    | 576     | 2017   |

\* Not included in average

\*\* Denotes volume of dry-rodded coarse aggregate per unit volume of concrete

TABLE IV - A  
4-SACK REGULAR-CONCRETE DATA — CONNERS CREEK FLY ASH

| Batch No. | Date Made | Fly Ash, lb./cu. yd. | Actual Cement Content, sack/cu. yd. | Material Proportions, |       |           | W/C, gal./sack | Wt. Fresh Concrete, lb./cu. ft. | Pressure Air Content, percent | Slump, in. | Compressive Strength, psi (6" x 12" cylinders) |        |         |         |       |
|-----------|-----------|----------------------|-------------------------------------|-----------------------|-------|-----------|----------------|---------------------------------|-------------------------------|------------|--|--------|---------|---------|-------|
|           |           |                      |                                     | Sand                  | Stone | Net Water |                |                                 |                               |            | 1 day  | 7 days | 28 days | 90 days |       |
| 207       | 4-7-55    | 0                    | 4.04                                | 0.64                  | 1539  | 1814      | 266            | 7.97                            | 151.2                         | 1.7        | 2.75   | 460    | 2100    | 3055    |       |
| 250       | 5-12-55   | 0                    | 4.02                                | 0.64                  | 1487  | 1814      | 271            | 8.13                            | 148.7                         | 0.8        | 5.75   | 470    | 480     | 2120    | 285   |
| 277       | 6-2-55    | 0                    | 3.99                                | 0.64                  | 1509  | 1814      | 283            | 8.48                            | 148.9                         | 1.2        | 4.00   | 495    | 1660*   | 2475    |       |
| Average   | 0         | 4.02                 | 0.64                                | 1512                  | 1814  | 273       | 8.19           | 149.6                           | 1.2                           | 4.17       | 455  | 405    | 1680    | 2740    |       |
| 208       | 4-7-55    | 100                  | 4.02                                | 0.72                  | 1262  | 2011      | 249            | 7.47                            | 151.8                         | 1.4        | 2.75   | 585    | 420     | 1765    | 2860  |
| 223       | 4-15-55   | 100                  | 4.02                                | 0.72                  | 1253  | 2011      | 252            | 7.56                            | 151.7                         | 1.0        | 3.0  | 670    | 710     | 2405    | 3375  |
| 275       | 6-1-55    | 100                  | 4.02                                | 0.72                  | 1244  | 2011      | 254            | 7.62                            | 151.4                         | 0.7        | 4.0  | 575    | 560     | 2225    | 3375  |
| Average   | 100       | 4.02                 | 0.72                                | 1253                  | 2011  | 252       | 7.55           | 151.6                           | 1.0                           | 3.25       | 617  | 600    | 2455    | 3370    |       |
| 209       | 4-7-55    | 150                  | 4.03                                | 0.75                  | 1108  | 2126      | 250            | 7.52                            | 151.3                         | 1.2        | 3.75   | 670    | 710     | 2525    | 3345  |
| 251       | 5-12-55   | 150                  | 3.99                                | 0.75                  | 1125  | 2126      | 250            | 7.51                            | 150.7                         | 0.9        | 4.0  | 545    | 600     | 2260    | 3355  |
| 268       | 5-27-55   | 150                  | 4.00                                | 0.75                  | 1117  | 2126      | 251            | 7.54                            | 150.8                         | 0.9        | 3.5  | 520    | 545     | 2190    | 3355* |
| Average   | 150       | 4.01                 | 0.75                                | 1117                  | 2126  | 250       | 7.52           | 150.9                           | 1.0                           | 3.75       | 592  | 560    | 2190    | 3355*   |       |
| 195       | 3-9-55    | 200                  | 3.99                                | 0.78                  | 971   | 2211      | 260            | 7.81                            | 150.2                         | 1.1        | 4.0  | 695    | 710     | 2650    | 3620  |
| 224       | 4-15-55   | 200                  | 4.02                                | 0.78                  | 963   | 2211      | 267            | 8.03                            | 151.3                         | 0.9        | 5.5  | 675    | 660     | 2145    | 3745  |
| 289       | 6-9-55    | 200                  | 3.99                                | 0.78                  | 963   | 2211      | 263            | 7.91                            | 150.1                         | 0.9        | 2.75   | 735    | 670     | 2120    | 3270  |
| Average   | 200       | 4.00                 | 0.78                                | 966                   | 2211  | 263       | 7.92           | 150.5                           | 1.0                           | 4.08       | 688  | 650    | 2450    | 3937    |       |
| 190       | 3-8-55    | 250                  | 3.97                                | 0.81                  | 809   | 2296      | 277            | 8.33                            | 149.2                         | 0.9        | 5.75   | 635    | 670     | 2030    | 3160  |
| 230       | 4-19-55   | 250                  | 4.06                                | 0.81                  | 792   | 2296      | 280            | 8.40                            | 151.9                         | 0.9        | 6.0  | 670    | 680     | 2120    | 3270  |
| 287       | 6-8-55    | 250                  | 3.96                                | 0.81                  | 818   | 2296      | 269            | 8.06                            | 148.9                         | 0.9        | 4.0  | 630    | 680     | 2215    | 3270  |
| Average   | 250       | 4.00                 | 0.81                                | 806                   | 2296  | 275       | 8.26           | 150.0                           | 0.9                           | 5.25       | 658  | 675    | 2455    | 4170    |       |

\* Not included in average

\*\* Denotes volume of dry-rodded coarse aggregate per unit volume of concrete

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TABLE V - A

4.5-SACK REGULAR-CONCRETE DATA — ST. CLAIR FLY ASH

| Batch No. | Date Made | Fly Ash,<br>lb/cu yd | Actual Cement<br>Content,<br>sack/cu yd | Material Proportions, |      |       | W/C,<br>lb/cu yd | Wt. Fresh<br>Concrete,<br>lb/cu ft | Pressure<br>Air Content,<br>percent | Compressive Strength, psi<br>(6" x 12" Cylinders) |              |              |
|-----------|-----------|----------------------|---|-----------------------|------|-------|------------------|------------------------------------|-------------------------------------|---|--------------|--------------|
|           |           |                      |   | V <sub>s</sub> **     | Sand | Stone |                  |                                    |                                     | 28 days   | 28 days      | 1 year       |
| 202       | 4-6-55    | 0                    | 4.18                                    | 0.64                  | 1543 | 1814  | 253              | 6.75                               | 150.7                               | 2.0   | 2.75         | 705*         |
| 255       | 5-19-55   | 0                    | 4.50                                    | 0.64                  | 1485 | 1814  | 268              | 7.14                               | 149.5                               | 1.7   | 3.5          | 635<br>2970  |
| 274       | 6-1-55    | 0                    | 4.50                                    | 0.64                  | 1507 | 1814  | 262              | 7.00                               | 150.2                               | 1.8   | 3.5          | 640<br>2950  |
| Average   | 0         | 4.19                 | 0.64                                    | 1512                  | 1814 | 261   | 6.96             | 150.1                              | 1.8                                 | 3.25  | 630<br>2950  |              |
| 213       | 4-8-55    | 50                   | 4.17                                    | 0.72                  | 1512 | 2041  | 240              | 6.41                               | 151.4                               | 1.4   | 2.25         | 1020<br>4735 |
| 243       | 4-26-55   | 50                   | 4.52                                    | 0.72                  | 1283 | 2041  | 249              | 6.64                               | 152.2                               | 1.0   | 3.75         | 935<br>3940  |
| 270       | 5-30-55   | 50                   | 4.50                                    | 0.72                  | 1273 | 2041  | 250              | 6.68                               | 151.3                               | 1.0   | 3.0          | 815<br>2705  |
| Average   | 50        | 4.50                 | 0.72                                    | 1289                  | 2041 | 246   | 6.58             | 151.6                              | 1.1                                 | 3.00  | 922<br>3535* |              |
| 219       | 4-14-55   | 100                  | 4.19                                    | 0.75                  | 1156 | 2126  | 258              | 6.88                               | 152.1                               | 1.1   | 4.5          | 885<br>2720  |
| 218       | 4-28-55   | 100                  | 4.51                                    | 0.75                  | 1127 | 2126  | 252              | 6.71                               | 151.2                               | 1.1   | 4.0          | 945<br>3780  |
| 286       | 6-8-55    | 100                  | 4.50                                    | 0.75                  | 1137 | 2126  | 250              | 6.67                               | 151.2                               | 0.8   | 4.0          | 885<br>4233  |
| Average   | 100       | 4.50                 | 0.75                                    | 1140                  | 2126 | 253   | 6.75             | 151.5                              | 1.0                                 | 4.17  | 891<br>3595  |              |
| 191       | 3-8-55    | 150                  | 4.51                                    | 0.78                  | 961  | 2211  | 254              | 6.76                               | 150.2                               | 1.1   | 3.0          | 725<br>3550  |
| 257       | 5-19-55   | 150                  | 4.18                                    | 0.78                  | 990  | 2211  | 257              | 6.87                               | 150.5                               | 1.0   | 4.0          | 860<br>3540  |
| 260       | 5-20-55   | 150                  | 4.18                                    | 0.78                  | 981  | 2211  | 270              | 7.20                               | 150.6                               | 0.6   | 5.5          | 785<br>3710  |
| Average   | 150       | 4.19                 | 0.78                                    | 977                   | 2211 | 260   | 6.94             | 150.4                              | 0.9                                 | 4.17  | 765<br>3885  |              |
| 212       | 4-8-55    | 200                  | 4.16                                    | 0.81                  | 844  | 2296  | 281              | 7.51                               | 150.1                               | 1.1   | 3.5          | 970<br>3885  |
| 252       | 4-19-55   | 200                  | 4.54                                    | 0.81                  | 776  | 2296  | 282              | 7.52                               | 150.2                               | 0.9   | 3.0          | 755<br>3945  |
| 285       | 6-8-55    | 200                  | 4.56                                    | 0.81                  | 776  | 2296  | 269              | 7.17                               | 150.4                               | 0.6   | 5.0          | 725<br>4275  |
| Average   | 200       | 4.52                 | 0.81                                    | 799                   | 2296 | 277   | 7.40             | 150.2                              | 0.9                                 | 3.83  | 816<br>4176  |              |

\* Not included in average

\*\* Denotes volume of dry-rodded coarse aggregate per unit volume of concrete

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TABLE VI - A  
5-SACK REGULAR-CONCRETE DATA — CONNERS CREEK FLY ASH

| Batch No. | Date Made | Fly Ash, 1b/cu yd | Actual Cement Content, sack/cu yd | Material Proportions,— |      |       | W/C, gal./sack | Concrete, 1b/cu ft | Wt. Fresh Air Content, percent | Slump, in. | Pressure, 1 day 7 days 28 days 90 days 1 year | Compressive Strength, psi (6" x 12" cylinders) |
|-----------|-----------|-------------------|-----------------------------------|------------------------|------|-------|----------------|--------------------|--------------------------------|------------|---|--|
|           |           |                   |                                   | V <sub>s</sub> **      | Sand | Stone |                |                    |                                |            |   |  |
| 192       | 3-9-55    | 0                 | 1.92                              | 0.64                   | 1513 | 1814  | 255            | 6.13               | 149.5                          | 2.1        | 3.0   | 920 2560 3110                                  |
| 234       | 4-20-55   | 0                 | 5.00                              | 0.64                   | 1447 | 1814  | 269            | 6.45               | 150.0                          | 1.6        | 5.25  | 895 2755 3275                                  |
| 288       | 6-9-55    | 0                 | 5.00                              | 0.64                   | 1469 | 1814  | 254            | 6.09               | 150.2                          | 1.9        | 4.0   | 840 2615 3275                                  |
| Average   | 0         | 4.97              | 0.64                              | 1476                   | 1814 | 259   | 6.22           | 149.9              | 1.9                            | 4.08       | 890 2856 3568                                 |  |
| 211       | 4-8-55    | 50                | 5.01                              | 0.72                   | 1215 | 201   | 249            | 5.97               | 151.1                          | 1.5        | 2.75  | 1200 3640 4840                                 |
| 242       | 4-26-55   | 50                | 4.98                              | 0.72                   | 1227 | 201   | 256            | 6.15               | 151.0                          | 0.9        | 4.0   | 1220 3780 5070                                 |
| 261       | 5-20-55   | 50                | 4.98                              | 0.72                   | 1227 | 201   | 257            | 6.18               | 150.9                          | 0.9        | 4.25  | 1015 3125 2405* 3940                           |
| Average   | 50        | 4.99              | 0.72                              | 1223                   | 201  | 254   | 6.10           | 151.0              | 1.1                            | 3.67       | 895 3110 3620 4254                            |  |
| 203       | 4-6-55    | 100               | 5.02                              | 0.75                   | 1058 | 2126  | 267            | 6.40               | 151.4                          | 1.2        | 5.5   | 885 3040 4275                                  |
| 247       | 4-28-55   | 100               | 5.01                              | 0.75                   | 1079 | 2126  | 262            | 6.29               | 151.6                          | 1.0        | 5.0   | 865 3215 4505                                  |
| 265       | 5-26-55   | 100               | 5.00                              | 0.75                   | 1101 | 2126  | 255            | 6.11               | 152.0                          | 0.9        | 3.5   | 935 3125 3995                                  |
| Average   | 100       | 5.01              | 0.75                              | 1079                   | 2126 | 261   | 6.27           | 151.7              | 1.0                            | 4.67       | 961 3344 4093                                 |  |
| 220       | 4-14-55   | 150               | 5.01                              | 0.78                   | 921  | 2211  | 274            | 6.57               | 151.2                          | 1.1        | 4.5   | 955 2845 3305*                                 |
| 228       | 4-18-55   | 150               | 5.03                              | 0.78                   | 909  | 2211  | 270            | 6.49               | 151.2                          | 0.9        | 5.5   | 990 2915 3305                                  |
| 276       | 6-1-55    | 150               | 4.98                              | 0.78                   | 921  | 2211  | 279            | 6.70               | 150.3                          | 0.4        | 5.5   | 995 2845 3815                                  |
| Average   | 150       | 5.01              | 0.78                              | 917                    | 2211 | 274   | 6.59           | 150.9              | 0.8                            | 5.17       | 887 2851 3883                                 |  |
| 187       | 3-7-55    | 200               | 5.18                              | 0.81                   | 644  | 2296  | 270            | 6.49               | 150.6                          | 0.9        | 4.0   | 935 2755 3745                                  |
| 258       | 5-20-55   | 200               | 4.98                              | 0.81                   | 733  | 2296  | 278            | 6.68               | 149.9                          | 0.7        | 4.5   | 855 2740 4345                                  |
| 284       | 6-6-55    | 200               | 4.99                              | 0.81                   | 774  | 2296  | 284            | 6.81               | 150.4                          | 0.8        | 3.5   | 985 2755 4065                                  |
| Average   | 200       | 5.05              | 0.81                              | 717                    | 2296 | 277   | 6.66           | 150.3              | 0.8                            | 4.0        | 1035 3090 4210 4063                           |  |

\* Not included in average  
\*\* Denotes volume of dry-rodded coarse aggregate per unit volume of concrete

TABLE VII - A

## 5.5-SACK REGULAR-CONCRETE DATA — ST. CLAIR FLY ASH

| Batch No. | Date Made | Fly Ash, lb/cu. yd | Actual Content, sack/cu. yd | Cement, V <sub>s</sub> ** | Material Proportions, |      |       | W/C, Concrete, lb/cu. ft. | Wt. Fresh Concrete, lb/sack | Pressure Air Content, percent | Slump, in. | Compressive Strength, psi (6" x 12" Cylinders) | 7 days<br>20 days<br>28 days<br>90 days<br>1 year |       |
|-----------|-----------|--------------------|-----------------------------|---------------------------|-----------------------|------|-------|---------------------------|-----------------------------|-------------------------------|------------|--|---|-------|
|           |           |                    |                             |                           | 1b./cu. yd            | Sand | Stone |                           |                             |                               |            |  |   |       |
| 196       | 3-10-55   | 0                  | 5.43                        | 0.64                      | 1469                  | 1814 | 250   | 5.46                      | 149.9                       | 2.2                           | 3.0        | 1235   | 3180  | 3815  |
| 222       | 4-15-55   | 0                  | 5.59                        | 0.64                      | 1413                  | 1814 | 248   | 5.41                      | 152.1                       | 1.5                           | 5.25       | 1260   | 2880  | 4100  |
| 283       | 6-6-55    | 0                  | 5.43                        | 0.64                      | 1459                  | 1814 | 267   | 5.83                      | 150.2                       | 2.1                           | 4.0        | 1205   | 3180  | 4365  |
| Average   | 0         | 5.48               | 0.64                        | 1447                      | 1814                  | 258  | 5.57  | 150.7                     | 1.9                         | 4.08                          | 1202       | 3189   | 4114  | 3995  |
| 189       | 3-7-55    | 50                 | 5.70                        | 0.72                      | 1064                  | 2041 | 255   | 5.57                      | 152.6                       | 0.9                           | 5.0        | 975  | 3285  | 3905  |
| 244       | 4-27-55   | 50                 | 5.51                        | 0.72                      | 1205                  | 2041 | 246   | 5.37                      | 152.5                       | 1.4                           | 3.25       | 1345   | 3800  | 4150  |
| 269       | 5-30-55   | 50                 | 5.46                        | 0.72                      | 1205                  | 2041 | 253   | 5.53                      | 151.4                       | 1.0                           | 5.5        | 1210   | 3375  | 4310  |
| Average   | 50        | 5.56               | 0.72                        | 1158                      | 2041                  | 251  | 5.49  | 152.2                     | 1.1                         | 4.58                          | 1193       | 3528   | 4301  |       |
| 188       | 3-7-55    | 100                | 5.68                        | 0.75                      | 915                   | 2126 | 259   | 5.65                      | 151.6                       | 1.0                           | 4.75       | 1090   | 3180  | 4170  |
| 237       | 4-21-55   | 100                | 5.47                        | 0.75                      | 1044                  | 2126 | 273   | 5.97                      | 151.0                       | 0.9                           | 5.0        | 1155   | 2895  | 3815  |
| 273       | 5-31-55   | 100                | 5.50                        | 0.75                      | 1056                  | 2126 | 253   | 5.53                      | 151.6                       | 0.9                           | 3.25       | 1165   | 2810  | 3800  |
| Average   | 100       | 5.55               | 0.75                        | 1005                      | 2126                  | 262  | 5.72  | 151.5                     | 0.9                         | 4.35                          | 1131       | 3162   | 4173  |       |
| 221       | 4-14-55   | 150                | 5.46                        | 0.78                      | 896                   | 2211 | 283   | 6.18                      | 150.9                       | 0.9                           | 4.5        | 1080   | 3090  | 3745  |
| 229       | 4-18-55   | 150                | 5.54                        | 0.78                      | 849                   | 2211 | 271   | 5.92                      | 150.8                       | 0.9                           | 4.0        | 1130   | 3340  | 3840  |
| 271       | 5-30-55   | 150                | 5.51                        | 0.78                      | 872                   | 2211 | 273   | 5.96                      | 151.1                       | 0.9                           | 4.5        | 950  | 2755  | 4070  |
| Average   | 150       | 5.50               | 0.78                        | 872                       | 2211                  | 276  | 6.02  | 150.9                     | 0.9                         | 4.35                          | 1069       | 3023   | 3584  |       |
| 200       | 4-5-55    | 200                | 5.44                        | 0.81                      | 749                   | 2296 | 289   | 6.31                      | 150.1                       | 1.4                           | 3.5        | 955  | 2985  | 4860* |
| 235       | 4-20-55   | 200                | 5.55                        | 0.81                      | 677                   | 2296 | 290   | 6.34                      | 150.4                       | 0.9                           | 5.25       | 1020   | 3200  | 3995  |
| 280       | 6-3-55    | 200                | 5.54                        | 0.81                      | 689                   | 2296 | 274   | 5.99                      | 150.1                       | 0.8                           | 4.0        | 1100   | 3200  | 4295  |
| Average   | 200       | 5.51               | 0.81                        | 705                       | 2296                  | 284  | 6.21  | 150.2                     | 1.0                         | 4.25                          | 1024       | 3003   | 4135  |       |

\* Not included in average

\*\* Denotes volume of dry-rodded coarse aggregate per unit volume of concrete

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TABLE VIII - A

5.5-SACK REGULAR-CONCRETE DATA — CONNERS CREEK FLY ASH

| Batch No.                             | Date Made | Fly Ash, lb./cu. yd. | Actual Content, sack/cu. yd. | V <sub>s</sub> ** | Material Proportions, |       |                     | W/C, lb./cu. ft. | Concrete Air Content, percent | Pressure in., 1 day | Slump, in. | Compressive Strength, psi (6" x 12" Cylinders) |        |         |
|---------------------------------------|-----------|----------------------|------------------------------|-------------------|-----------------------|-------|---------------------|------------------|-------------------------------|---------------------|------------|--|--------|---------|
|                                       |           |                      |                              |                   | Sand                  | Stone | Net Water gal./sack |                  |                               |                     |            | 1 day  | 7 days | 28 days |
| 204                                   | 4-6-55    | 50                   | 5.46                         | 0.72              | 1205                  | 2041  | 262                 | 5.72             | 151.7                         | 1.3                 | 4.0        | 1060   | 3515   | 5210    |
| 216                                   | 4-27-55   | 50                   | 5.51                         | 0.72              | 1169                  | 2041  | 253                 | 5.53             | 151.4                         | 1.0                 | 4.0        | 1040   | 3285   | 4715    |
| 290                                   | 6-9-55    | 50                   | 5.45                         | 0.72              | 1181                  | 2041  | 270                 | 5.89             | 150.6                         | 0.9                 | 4.5        | 1075   | 3160   | 3800    |
| Average                               | 50        | 5.47                 | 0.72                         | 1185              | 2041                  | 262   | 5.71                | 151.2            | 1.1                           | 4.17                | 1060       | 3110   | 3975   | 4895    |
| 193                                   | 3-9-55    | 100                  | 5.48                         | 0.75              | 1044                  | 2126  | 257                 | 5.61             | 151.1                         | 1.2                 | 3.5        | 1165   | 3215   | 3250*   |
| 238                                   | 4-21-55   | 100                  | 5.51                         | 0.75              | 1032                  | 2126  | 264                 | 5.76             | 151.5                         | 1.2                 | 3.75       | 1230   | 2845   | 3850    |
| 264                                   | 5-26-55   | 100                  | 5.52                         | 0.75              | 1021                  | 2126  | 270                 | 5.89             | 151.6                         | 0.7                 | 4.75       | 1060   | 3355   | 4310    |
| Average                               | 100       | 5.50                 | 0.75                         | 1032              | 2126                  | 264   | 5.75                | 151.4            | 1.0                           | 4.00                | 1158       | 3148   | 4240   | 4024    |
| 194                                   | 3-9-55    | 150                  | 5.45                         | 0.78              | 968                   | 2211  | 276                 | 6.01             | 150.7                         | 1.1                 | 5.25       | 1080   | 2670*  | 3885    |
| 227                                   | 4-18-55   | 150                  | 5.52                         | 0.78              | 884                   | 2211  | 276                 | 6.02             | 151.9                         | 0.9                 | 5.0        | 1175   | 3375*  | 3905    |
| 259                                   | 5-20-55   | 150                  | 5.45                         | 0.78              | 884                   | 2211  | 271                 | 5.92             | 149.7                         | 0.9                 | 4.25       | 1145   | 2985   | 4045    |
| Average                               | 150       | 5.47                 | 0.78                         | 892               | 2211                  | 274   | 5.98                | 150.8            | 1.0                           | 4.83                | 1106       | 3075   | 3780   | 4065    |
| 205                                   | 4-6-55    | 200                  | 5.49                         | 0.81              | 713                   | 2296  | 293                 | 6.40             | 150.2                         | 1.2                 | 4.0        | 885  | 2970   | 4875    |
| 233                                   | 4-19-55   | 200                  | 5.52                         | 0.81              | 677                   | 2296  | 290                 | 6.32             | 149.6                         | 1.0                 | 3.75       | 945  | 3040   | 4715    |
| 281                                   | 6-3-55    | 200                  | 5.50                         | 0.81              | 677                   | 2296  | 294                 | 6.42             | 149.1                         | 0.8                 | 4.0        | 980  | 3130   | 3885    |
| Average                               | 200       | 5.50                 | 0.81                         | 689               | 2296                  | 292   | 6.38                | 149.6            | 1.0                           | 3.92                | 1020       | 3270   | 4065   | 4201    |
| <b>6.5-SACK REGULAR-CONCRETE DATA</b> |           |                      |                              |                   |                       |       |                     |                  |                               |                     |            |  |        |         |
| 210                                   | 4-8-55    | 0                    | 6.39                         | 0.64              | 1398                  | 1814  | 270                 | 4.99             | 150.7                         | 1.9                 | 6.0        | 1645   | 3920   | 5245    |
| 226                                   | 4-18-55   | 0                    | 6.55                         | 0.64              | 1340                  | 1814  | 266                 | 4.91             | 151.8                         | 1.5                 | 6.0        | 1490   | 3780   | 5245    |
| 272                                   | 5-31-55   | 0                    | 6.19                         | 0.64              | 1349                  | 1814  | 251                 | 4.64             | 150.7                         | 1.8                 | 3.0        | 1520   | 3570   | 4045    |
| Average                               | 0         | 6.47                 | 0.64                         | 1362              | 1814                  | 262   | 4.85                | 151.1            | 1.7                           | 5.0                 | 1430       | 3800   | 4700   | 4665    |

\* Not included in average  
\*\* Denotes volume of dry-rodded coarse aggregate per unit volume of concrete

