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THE UNIVERSITY OF MICHIGAN
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Progress Report

STUDY OF ST. CLAIR FLY ASH IN NON-AIR-ENTRAINED CONCRETE
MADE WITH PORTLAND AND PORTLAND-SLAG CEMENTS

F. E. Legg, Jr.

Assistant Professor of Engineering Materials
and Assistant Supervisor,
Michigan State Highway Department Laboratory

Ralph H. Vogler

Research Assistant

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SYNOPSIS

With increasing production and use of portland-slag cement, a study was undertaken to determine if there were any important differences between portland-slag and normal portland cement when used in concrete containing St. Clair fly ash. Due to the preliminary nature of the study, one cement content was used, namely, 4.5 sacks per cubic yard. Three fly-ash contents as well as a control mix without fly ash were used with both types of cement.

The fly-ash mixes containing portland-slag cement generally show inferior strengths to those made with normal portland cement at 1 and 7 days but usually have superior strengths at 28 and 90 days. The relative-strength gain attained when using this fly ash with normal portland cement is not realized, however, when using this ash with the portland-slag cement, at least at ages up to 90 days. The observation follows that of the control mixes without fly ash, the strengths of the concrete made with the two types of cement were about equal at 1 and 7 days, but the portland-slag cement had considerably higher compressive strengths at 28 and 90 days.

OBJECTIVE

The purpose of this investigation is to study the properties of fly ash and concrete containing fly ash, as indicated by compressive strength, workability, durability in freezing and thawing, flexural strength, and other measures of concrete quality. The phase of the investigation covered by this report is concerned with the effect on compressive strength and workability of the use of portland-slag cement with fly ash, as compared to the use of normal portland cement with fly ash.

INTRODUCTION

To supplement their output, cement producers are now manufacturing increased quantities of portland-slag cement to increase their production without necessity for a corresponding increase of kiln capacity. By intergrinding to sufficient fineness approximately 40% granulated blast-furnace slag (a product quite different from air-cooled slag such as that used for aggregate), a cement can be produced which is of equivalent strength to normal portland cement at ages up to 28 days. At later ages the compressive strength usually becomes superior to that of normal portland cement.

Persuant to a contract between The Detroit Edison Company and the Engineering Research Institute of The University of Michigan, a study was made of the use of fly ash in concrete made with normal portland cement and with portland-slag cement. The work completed to date is of a preliminary nature, to determine if the two types of cement have pronounced difference in the effect of their reaction with St. Clair fly ash. This report covers such matters as mix proportioning and compressive strength of concrete up to 90 days of age.

Some matters pertaining to test procedures which were covered in earlier reports will be omitted here to avoid repetition. This report is concerned with St. Clair fly ash in non-air-entrained concrete exclusively. It is recommended that such concrete not be used where it will be subjected to freezing and thawing in the presence of moisture.

MIX DESIGN

The "Recommended Practice for Selecting Proportions for Concrete" (ACI 613-54), a standard of the American Concrete Institute, was used as the basis for the design of all mixes, as in previous studies. The stone contents were as recommended by the ACI in the mixes containing no fly ash, but were increased in the fly-ash mixes, taking full advantage of the added plasticity of the mortar constituent provided by the addition of fly ash.

Only one cement content, 4.5 sacks per cubic yard, was used for this

preliminary work. Three fly-ash contents, 75, 150, and 200 pounds per cubic yard, were used. Additionally, mixes with no fly ash were made for comparison purposes. These ash contents were selected to provide coverage over a wide range without an excessive number of mixes. Identical series were made with the portland cement and the portland-slag cement.

MATERIALS

The concrete materials were generally the same as those used previously. The coarse aggregate was 1-inch-maximum-size natural gravel, the fine aggregate was a natural sand having a fineness modulus of 3.0, and the fly ash was from the St. Clair station. The portland cement (ASTM Type I) consisted of a blend of equal amounts of Huron, Peerless, and Peninsular brands. There was only one brand of portland-slag cement (ASTM Type I-S), Huron, available at the time this program was started. As a result, there was no opportunity for blending to balance out minor variations which may result from the cement-manufacturing process. Both types of cement were non-air-entraining.

The results of the physical tests on the two cements are shown in the Appendix in Table I-A for the portland cement and Table II-A for the portland-slag cement. Notice should be taken of the large gain in compressive strength of the mortar cubes made with the portland-slag cement between 7 and 28 days. This acceleration seems to be typical of this type of cement, but in concrete it is usually not evident until after 28 days of age.

Properties of the fly ash are reported in Table III-A in the Appendix.

FABRICATION OF SPECIMENS AND TEST PROCEDURES

Methods of mixing, curing, and testing the specimens were generally the same as those used in the previous studies on concrete containing fly ash. Dry aggregates were generally used, although toward the end of the study it was necessary to use damp sand in a few of the mixes. Corrections were made in the batch weights to compensate for this moisture.

Two cylinders for each age of 1, 7, 28, and 90 days and 1 year were obtained from each batch, with two repeat batches for each variation of fly-ash content or type of cement, giving a total of six cylinders for each age and condition, as in previous studies. The cylinders were stored in the moist-fog room until the time for testing.

DISCUSSION OF TEST RESULTS

A detailed tabulation of the concrete-mix data and compressive-strength results is shown in the Appendix in Table IV-A for the mixes with portland cement and Table V-A for the mixes with portland-slag cement. Summaries of important aspects of the data have been prepared from these tables and are presented in the body of the report.

1. COARSE-AGGREGATE CONTENT

The greater amounts of coarse aggregate which were found to be workable in previous studies of fly-ash concrete with 1-inch-maximum-size gravel coarse aggregate were used again. These amounts appeared to be about the maximum which would still yield workable concrete. Theoretically, the portland-slag cement, being much finer than the portland cement, should have permitted higher coarse-aggregate contents. No effort was made to force more gravel into these mixes since the amount which was used would already be considered too high by some users.

The value V_s , denoting the dry-rodded volume of coarse aggregate per unit volume of concrete, is given in Tables IV-A and V-A in the Appendix.

2. COMPRESSIVE-STRENGTH RESULTS

Average values of compressive strengths are presented in Table I. The strengths of the fly-ash mixes are presented in Table II expressed as a percent of the strength of the plain-cement control mixes, and the mixes containing portland-slag cement are also expressed as a percent of the strength of the control made with portland cement.

The fly-ash mixes made with portland cement produced results similar to those obtained previously, in that the fly ash improves the strength somewhat at all ages. There is very little difference in strength between the three fly-ash contents, but at 28 and 90 days, the larger amount (200 pounds per cubic yard) appears to produce slightly higher strengths.

The addition of fly ash apparently does not benefit strength of concrete made with portland-slag cement as much as it does concrete made with the plain portland cement. At 90 days, the percentage-strength increase due to the addition of fly ash is about one-third as much for the portland-slag cement mixes as it is for the portland cement mixes. At the earlier ages of 1 and 7 days, the addition of fly ash resulted in a loss of strength with the portland-slag cement except for the lowest fly-ash addition (75 pounds per cubic yard).

TABLE I

SUMMARY OF RESULTS

Portland and Portland-Slag Cement with St. Clair Fly Ash

Nominal Cement Content, sk/cu yd	Actual Cement Content, sk/cu yd	Fly Ash, lb/cu yd	Net Mixing Water		Slump, in.	Compressive Strength, psi			
			lb/cu yd	gal/sk		1 Day	7 Days	28 Days	90 Days
4.5	4.44	0	268	7.15	3.8	519	1925	3065	3805
	4.44	75	251	6.69	3.6	701	2435	3844	5183
	4.48	150	251	6.69	4.6	753	2483	3893	5379
	4.48	200	260	6.93	4.0	698	2385	4010	5436
4.5	4.44	0	250	6.68	2.8	568	2035	3798	5268
	4.45	75	246	6.58	4.4	598	2214	4153	5902
	4.47	150	258	6.87	3.7	505	2013	4058	5884
	4.47	200	270	7.21	4.8	459	1864	3873	5385

Portland Cement (Type I)

Portland-Slag Cement (Type I-S)

TABLE II

COMPRESSIVE STRENGTH OF FLY-ASH CONCRETE
EXPRESSED AS PERCENT OF PLAIN-CEMENT CONTROL MIXES

Cement Content, sk/cu yd	Fly Ash, lb/cu yd	Age			
		1 Day	7 Days	28 Days	90 Days
Percent of Portland Cement (Type I) Control					
4.5	75	135	126	125	136
Portland Cement (Type I)	150	145	129	127	141
	200	134	124	131	143
Percent of Portland-Slag Cement (Type I-S) Control					
4.5	75	105	109	109	112
Portland-Slag Cement (Type I-S)	150	89	99	107	112
	200	81	92	102	102
Percent of Portland Cement (Type I) Control					
4.5	0	109	106	124	138
Portland-Slag Cement (Type I-S)	75	115	115	135	155
	150	97	105	132	155
	200	88	97	126	142

The portland-slag cement produces a strength effect in concrete similar to that observed when fly ash or other pozzolanic material is added to portland cement; the strength of concrete made with portland-slag cement is equivalent to that of concrete made with normal portland cement through the first 7 days, but at 28 days there is some improvement in the strength of the portland-slag cement concrete. At 90 days, the improvement is more pronounced, in this case increasing the strength by 38%, or 1460 psi, over the normal portland cement.

There does not appear to be much strength advantage in the use of fly ash with portland-slag cement on the basis of results so far available.

This work has been accomplished with one lot of one brand of portland-slag cement. Investigators have found that fly ash reacts differently with cements of varying chemical composition. No information is presently available to determine whether all portland-slag cement and fly-ash combinations produce this small amount of pozzolanic strength gain due to the fly ash, or if it is this one brand which does not have the proper chemical composition for an advantageous reaction. With the normal portland cement, three brands were combined to overcome such differences in a single cement.

The compressive-strength results are shown graphically in Figs. 1 and 2 for the concrete made with portland cement and with portland-slag cement, respectively. Results of comparable mixes from a previous report (2211-5-P) are also shown in Fig. 1. The strength of the two sets of cylinders is in very close agreement although the mixes were made nearly one year apart. The strength gain is orderly in all cases.

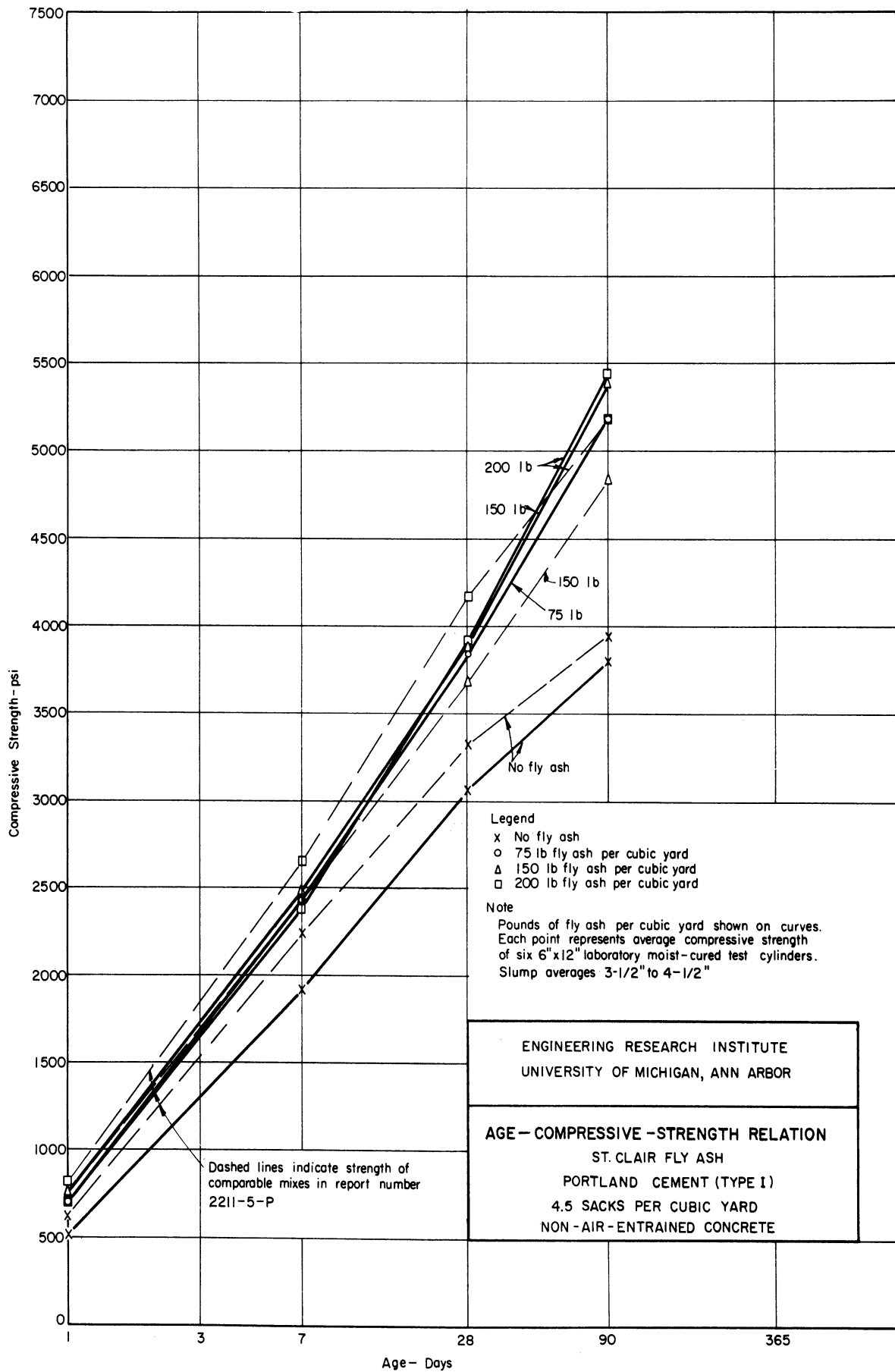


Fig. 1.

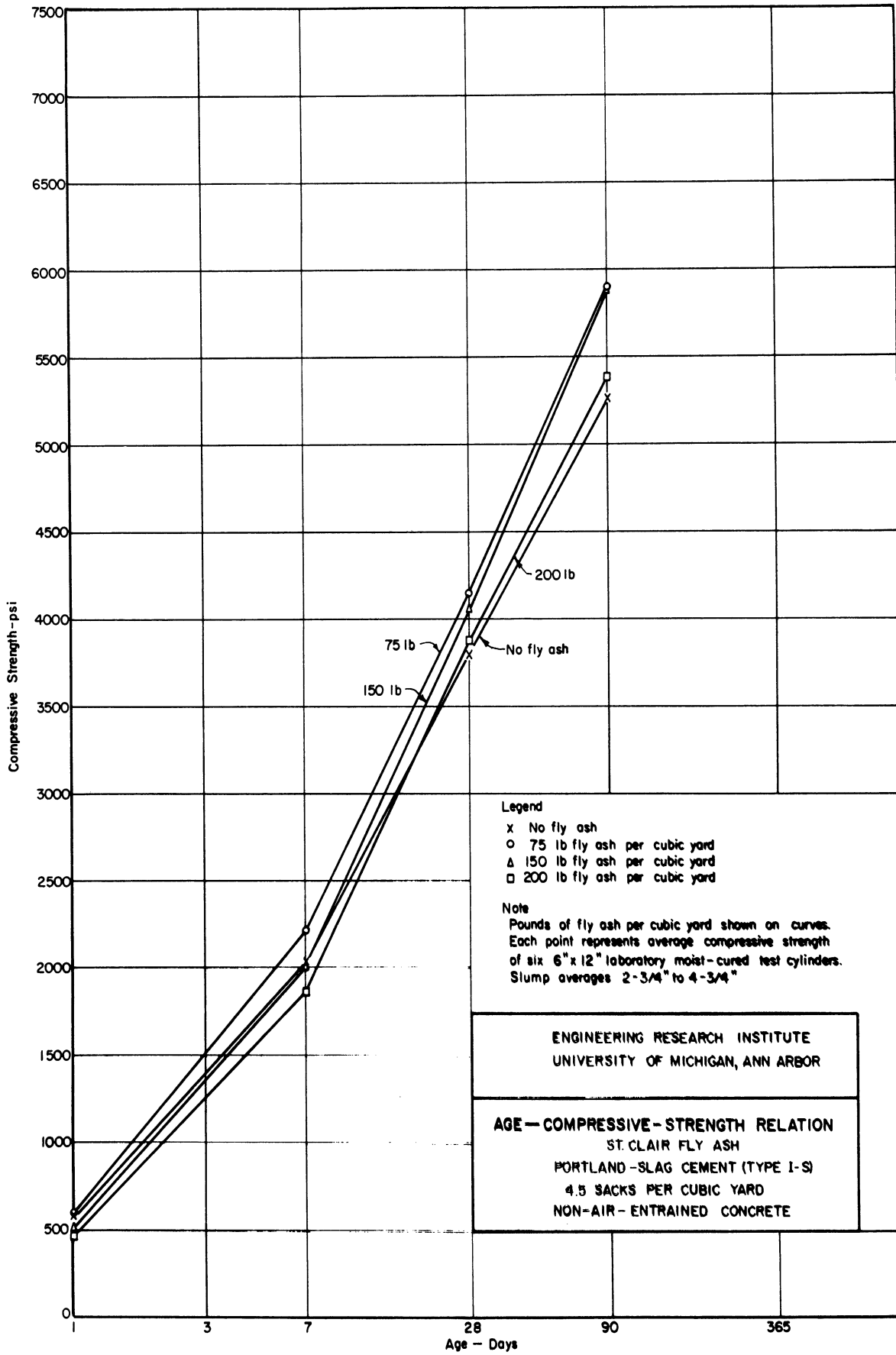


Fig. 2.

APPENDIX

TABLE I-A

PROPERTIES OF PORTLAND CEMENT
56C-108 (Type I)

PHYSICAL PROPERTIES

Specific surface, air permeability test, sq cm/gram	3116
Autoclave expansion, percent	0.07
Normal consistency, percent	24.8
Time of set, Gilmore	
Initial	4 hr, 5 min
Final	6 hr, 5 min
Compressive strength, psi	
7 days	3263
28 days	4863
Air in mortar, percent	11.3

TABLE II-A

PROPERTIES OF PORTLAND-SLAG CEMENT
56C-111 (Type I-S)

PHYSICAL PROPERTIES

Specific surface, air permeability test, sq cm/gram	4030
Autoclave expansion, percent	0.02
Normal consistency, percent	27.2
Time of set, Vicat	5 hr, 5 min
Compressive strength, psi	
7 days	3104
28 days	6150
Specific gravity	3.06
Air in mortar, percent	8.7

TABLE III-A

PROPERTIES OF FLY ASH

Physical Properties	St. Clair Fly Ash	ASTM
		Requirement C350-54T
Specific surface, air permeability test, sq cm/gram	3012	2800 min
Compressive strength, 20% by weight of portland- cement addition, hand mixing, 73°F cure, percent of control		
7 days	114	
28 days	119	
90 days	129	
Water requirement, percent of control	112	
Compressive strength, 25% by weight of sand, sand replacement, machine mixing, 73°F cure, percent of control		
7 days	162	
28 days	167	
90 days	204	
Water requirement, percent of control	115	
Compressive strength, 25% by weight of cement, sand replacement, machine mixing, 73°F cure, percent of control		
7 days	148	100 min
28 days	143	100 min
90 days	150	
Water requirement, percent of control	100	
Drying shrinkage, 28 days, percent	0.08	0.10 max
Soundness, autoclave expansion, percent	0.06	0.50 max
Specific gravity	2.47	

Chemical Properties	Percent by Weight, Moisture-Free Basis	
	St. Clair Fly Ash	ASTM Requirement C350-54T
Silicon dioxide, SiO ₂	36.9	40.0 min
Magnesium oxide, MgO	1.3	3.0 max
Sulfur trioxide, SO ₃	0.9	3.0 max
Loss on ignition	8.6	12.0 max
Moisture	0.3	3.0 max

TABLE IV-A
4.5 SACKS PORTLAND CEMENT (TYPE I) PER CUBIC YARD REGULAR CONCRETE -- ST. CLAIR FLY ASH

Batch No.	Date Made	Fly Ash, lb/cu yd	Actual Cement Content, sk/cu yd	V _s **	Material Proportions		W/C,	Weight of Fresh Concrete, lb/cu ft	Slump, in.	Compressive Strength, psi				
					Sand	Stone				Net Water	gal/sk	1 Day	7 Days	28 Days
345	3-5-56	0	4.40	0.64	1523	1815	277	7.39	148.1	2	500	1835	3090	3745
360	3-19-56	0	4.47	0.64	1491	1815	270	7.20	148.9	2.5	475	1855	2970	3605
368	3-26-56	0	4.46	0.64	1500	1815	257	6.85	148.4	7	570	2140	3305	4525
	Average	0	4.44	0.64	1505	1815	268	7.15	148.5	3.8	550	2065	3745*	4240
											610*	1855	2895	3250
											500	1800	2510*	3465
											519	1925	3065	3805
346	3-5-56	75	4.35	0.72	1250	2041	255	6.81	146.4	3.75	610	2280	3885	5140
353	3-12-56	75	4.50	0.72	1236	2041	245	6.54	150.8	3	630	2420	3870	5140
361	3-19-56	75	4.48	0.72	1236	2041	252	6.73	150.4	4	820	2490	1945*	5125
	Average	75	4.44	0.72	1241	2041	251	6.69	149.2	3.6	800	2490	3835	5090
											665	2510	3780	5300
											680	2420	3850	5300
											701	2435	3844	5183
354	3-12-56	150	4.50	0.78	977	2212	256	6.83	150.5	5.75	660	2330	3640	5335
362	3-19-56	150	4.47	0.78	1000	2212	252	6.73	150.4	4.5	650	2120	3425	5035
369	3-26-56	150	4.48	0.78	1000	2212	245	6.52	150.3	3.5	655	2440	4030	5655
	Average	150	4.48	0.78	992	2212	251	6.69	150.4	4.6	670	2580	4205	5335
											920	2720	4205	5510
											960	2705	3850	5405
											753	2483	3893	5379
355	3-12-56	200	4.48	0.81	835	2296	267	7.13	150.0	3.5	585	2245	3920	5335
363	3-19-56	200	4.50	0.81	825	2296	262	6.99	150.1	4	595	2350	3850	5335
370	3-26-56	200	4.47	0.81	835	2296	250	6.68	149.0	4.5	670	2295	4135	5830
	Average	200	4.48	0.81	832	2296	260	6.93	149.7	4.0	660	2525	3445*	5620
											840	2490	3995	5335
											835	2405	4150	5160
											698	2385	4010	5436

*Not included in average.

**Denotes volume of dry-rodded coarse aggregate per unit volume of concrete.

TABLE V-A
4.5 SACKS PORTLAND-SLAG CEMENT (TYPE I-S) PER CUBIC YARD REGULAR CONCRETE -- ST. CLAIR FLY ASH

Batch No.	Date Made	Fly Ash, lb/cu yd	Actual Cement Content, sk/cu yd	V**	Material Proportions		W/C,	Weight of Fresh Concrete, lb/cu ft	Slump, in.	Compressive Strength, psi				
					Sand	Stone				Net Water	gal/sk	1 Day	7 Days	28 Days
348	3-7-56	0	4.51	0.64	1513	1815	245	6.55	150.0	3.5	645	2100	4205	5705
356	3-14-56	0	4.42	0.64	1548	1815	251	6.69	148.5	2.5	650	2175	3850	6040
364	3-21-56	0	4.40	0.64	1548	1815	255	6.81	148.3	2.5	525	1945	3445	4770
	Average	0	4.44	0.64	1536	1815	250	6.68	148.9	2.8	505	2085	3850	4770
349	3-7-56	75	4.45	0.72	1240	2041	244	6.52	149.2	5	525	1960	3570	5160
357	3-14-56	75	4.46	0.72	1266	2041	246	6.56	150.4	3.5	560	1945	3870	5160
365	3-21-56	75	4.44	0.72	1256	2041	249	6.65	149.6	4.75	568	2035	3798	5268
	Average	75	4.45	0.72	1254	2041	246	6.58	149.7	4.4	705	2525	4540	6450
350	3-7-56	150	4.49	0.78	966	2212	249	6.64	149.7	2.5	665	2280	4715	6150
358	3-14-56	150	4.43	0.78	980	2212	268	7.15	148.8	3.75	550	2120	3730	5760
366	3-21-56	150	4.49	0.78	971	2212	256	6.83	150.0	4.75	550	2120	3570	5230
	Average	150	4.47	0.78	972	2212	258	6.87	149.5	3.7	550	2120	4365	5920
351	3-7-56	200	4.50	0.81	784	2296	269	7.18	148.7	5	370	2120	3995	5900
359	3-14-56	200	4.46	0.81	825	2296	272	7.25	149.0	4.5	598	2214	4153	5902
367	3-21-56	200	4.45	0.81	825	2296	270	7.20	148.8	5	515	1980	4295	6345
	Average	200	4.47	0.81	811	2296	270	7.21	148.8	4.8	535	2050	4045	6115
											450	1960	3920	5740
											485	2030	4045	5300
											535	2065	4240	4945*
											510	1995	3800	5920
											505	2013	4058	5884
											445	1800	3960	5300
											450	1820	3765	5740
											435	1855	3835	4860
											460	1890	2630*	5475
											490	1945	3920	5370
											475	1875	3885	5565
											459	1864	3873	5385

*Not included in average.
**Denotes volume of dry-rodded coarse aggregate per unit volume of concrete.

