

Report No. UMICH 014571-17-I

The University of Michigan  
Department of Mechanical Engineering  
Cavitation and Multiphase Flow Laboratory

Investigation of Secondary Liquid Phase  
Droplet Accelerations

written by:

J. J. Margle

Supported by: National Science Foundation Grant No. ENG 75-2315  
and U-M internal (SEP) funds.

April 1978



## Introduction

Due to less scheduled maintenance and the increased cost of downtime, turbine blade erosion (Fig. 1) [1]\* has become an important consideration in the design of low pressure stages of today's steam turbines. Krzyzanowski [7] has estimated turbine blade erosion for a small system (500 kw) can be as costly as \$1000/kw over the 40 year life of the system. Such economic considerations have motivated the study of turbine blade erosion.

This investigation deals with the motion of secondary droplets in a steam wake behind a stationary turbine blade. Such secondary droplets result from a thin liquid film which forms on the stationary blade due to the accumulation of primary droplets. The main stream steam flow causes this liquid film to break up at the trailing edge of the blade resulting in the formation of secondary droplets. As these droplets leave the trailing edge they are accelerated into the main stream steam wake. This acceleration was observed experimentally and the results are presented. Analytical prediction of droplet acceleration based on drag considerations is also attempted.

Figure 2 depicts the experimental apparatus while Figure 3 [8] shows its operation schematically.

Statistical approach is also attempted using a least squares regression analysis.

---

\*Numbers in brackets designate References at end of paper.

### Discussion of Results

Experimental secondary droplet accelerations were obtained from the observation of high speed motion pictures of the trailing edge of the stationary blade. Droplet size and position from the trailing edge were recorded for the steam velocities and liquid film flows shown in tables 1 and 2. Once knowing the droplet position and the motion picture film speed of 5000 frames per second, the velocity ( $U_d = \Delta x_d / \Delta t$ ) and the acceleration ( $a_d = \Delta U_d / \Delta t$ ) were easily calculated. This reduction of data (droplet position as a function of time) was accomplished through the use of a digital computer program [6]. Average accelerations for the flow conditions outlined above are also listed in tables 1 and 2 and shown graphically in Figure 4. These average accelerations were based on the arithmetic average of all those droplets observed for each liquid film flow rate.

Analytical prediction of droplet acceleration was based upon the following considerations:

- 1) the droplet after leaving the trailing edge assumed a spherical shape.
- 2) the main stream steam was one dimensional steady flow.
- 3) the main stream steam velocity is much larger than the droplet velocity,  $U_d$ .

$$\text{Hence, } U_r = U_s - U_d \quad \rightarrow 0$$
$$U_r = U_s$$

- 4) the main stream steam density,  $\rho_s$ , and the droplet density,  $\rho_d$ , remain constant.
- 5) Drag force has an overwhelming influence on the droplet acceleration. See Figure 5.

From (5) above it follows

$$m_d \frac{dU_d}{dt} = C_D A_d \rho_s \frac{U_r^2}{2} \quad \sim (1)$$

noting,

$$A_d = \pi d^2/4 \quad \text{and} \quad V_d = \pi d^3/6$$

also,  $m_d = \rho_d V_d$

Rearranging and substituting into equation (1) yields the following working equation,

$$\text{(Droplet acceleration)} \quad a_d = \frac{du_d}{dt} = \left\{ C_D \frac{\rho_s}{\rho_d} \frac{3}{4d} \right\} U_s^2 \sim (2)$$

where  $C_D$  is taken from [4] as

$$C_D = \frac{24}{R_e} (1 + 0.17 R_e^{3/3})$$

This resulted in  $C_D$  values that agreed with [5] within 2-20% for the range of Reynolds' numbers encountered. Density of the water droplet was taken to be constant,  $\rho_d = 1.0 \text{ gm/cm}^3$  ( $62.4 \text{ lbm/ft}^3$ ). The density of the steam was also taken to be constant and equal to that of saturated steam at 2.5 psia and 134.4°F, namely,  $\rho_s = 1.135 \times 10^{-4} \text{ gm/cm}^3$  ( $7.086 \times 10^{-3} \text{ lbm/ft}^3$ ). Analytically calculated droplet accelerations have been calculated for each droplet observed; however, only the average analytical accelerations for each liquid film flow are shown in tables 1 and 2 and Figure 4. Observing the ratio of experimental acceleration to analytical acceleration, as shown in tables 1 and 2, one finds this ratio to be less than 1.0 for the 305, 525 and 1100 steam velocities. This would be expected since the analytical model considers only drag effects and should tend to predict accelerations larger than those observed.

For the 825 and 975 steam velocities one notices this ratio to fluctuate about 1.0. This suggests some phenomenon in addition to simple drag considerations. Perhaps the steam velocity profile just past the trailing edge of the fixed blade is such that vortices are created. These vortices

may tend to increase or retard the droplet accelerations depending on the droplets' initial position relative to the center of the vortex.

In any case, caution should be exercised when reviewing the results of the higher steam velocities. For example, one notices the observed accelerations for the 825 ft/sec run to be double those of the 520 ft/sec run. This means that while studying every fifth frame of the high speed motion pictures, a droplet would traverse the width of the frame in one half the time or in one half the number of frames observed. Hence one would obtain nearly one half the number of raw data points. Consequently, the experimentally observed acceleration for these cases is less likely to be as precise a measure of true droplet acceleration. Perhaps a study of every second frame may result in a more accurate droplet acceleration at large steam velocities.

Figure 4 does show the droplet accelerations to be essentially independent of liquid film flow for the lower steam velocities. However, it is apparent that droplet accelerations do increase with increasing steam velocity.

### Statistical Considerations

Due to the nature of the physical phenomenon under consideration and due to the large amount of experimental data collected, certain statistical tools can be used to better understand the experimental results. The first approach was to perform a multivariate regression analysis using the MIDAS [3] package of statistical programs. This multivariate approach is shown schematically in figure 6. Specific results are contained in Appendix A. These results lead to the more meaningful first order regression analyses of experimental droplet acceleration, E.A., on flow rate, Q, and experimental droplet acceleration, E.A., on steam velocity,  $U_s$ .

Table 3 summarizes the results of a first order regression analysis of E.A. on Q. Here we see an equation of the form

$$E.A. = M(Q) + b$$

where,

E.A. = experimental droplet acceleration

$M$  = slope

b = "y" intercept

Table 3 shows the slope  $M$  not to be significantly different than zero slope in <sup>THREE</sup> ~~the~~ cases out of five. This indicates "flat" or level lines on plots of E.A. vs. Q (see Figure 4). R-SQR or "goodness of fit" parameter bears this out in the same three cases, in that, it says only a very small percentage of the variation in E.A. is explained by a variation in Q. Hence one can conclude, in a statistical sense, that E.A. is not affected by Q. Since the slopes can be considered statistically equal to zero, the intercepts, b, then become some indication of an "average" acceleration for a given steam velocity irrespective of flow rate. The statistically average values shown in table 3

compare favorably with those shown in table 1. S.E. values shown in table 3 are an estimate of standard error or standard deviation of E.A. about the regression line shown in Figure 4. Hence if  $2*(S.E.)$  lines ( $2\sigma$  bands) are drawn above and below the respective regression lines, 95.4% of the E.A.'s would lie within the bands.

When considering a first order regression analysis of E.A. on  $U_S$  one must consider the relationship shown in equation (2), namely

$$a_d = \left\{ C_D \frac{\rho_s}{\rho_d} \frac{3}{4d} \right\} U_S^2 \quad \sim (2)$$

taking the square root of both sides,

$$\sqrt{a_d} = \left\{ C_D \frac{\rho_s}{\rho_d} \frac{3}{4d} \right\}^{1/2} U_S \quad \sim (3)$$

Equation (3) shows  $\sqrt{E.A.}$  to be a linear function of  $U_S$ , hence a transformation of the experimental acceleration data is required in order to perform the most meaningful first order regression of  $\sqrt{E.A.}$  on  $U_S$ .

Table 4 shows resultant E.A. data while table 5 and Figure 7 show results of the regression analysis.

Again, one notices an equation of the form

$$\sqrt{E.A.} = M(U_S) + b$$

where:

$\sqrt{E.A.}$  = square root of experimental droplet acceleration

$M$  = slope

$b$  = "y" intercept = zero

In this case all the slopes we found to be statistically different than zero. Goodness of fit, R-SQR shows, for the  $Q = 17.7$  case, 76.1% of variation in  $\sqrt{E.A.}$  can be explained by the variation in  $U_S$ , which indicates E.A. to be a strong function of  $U_S$  (as is indicated by equation (2)). Intercept,  $b$ , equal zero, i.e.,  $E.A. = 0$  at  $U_S = 0$ . Makes sense, no droplets are being accelerated when there is no steam flow. The slope  $M$  corresponds to the term in



brackets in equation (3), hence substituting the following known quantities at  $Q = 35.3 \times 10^{-5} \text{ ft}^3/\text{min}$  and  $U_S = 305 \text{ ft}/\text{sec}^2$ :

$$R_e = 1036$$

$$C_D = \frac{24}{R_e} \left[ 1 + 0.17 (R_e)^{.667} \right] = 0.4265$$

$$d = 0.003281 \text{ ft}$$

$$\rho_d = 62.4 \text{ lbm}/\text{ft}^3$$

$$\rho_s = .007086 \text{ lbm}/\text{ft}^3$$

$$\left\{ C_D \frac{\rho_s}{\rho_d} \frac{3}{4d} \right\}^{1/2} = \frac{(0.4265) (.007086) (3)}{(62.4) (4) (.00328)} = 0.1052$$

Note 0.1052 compares favorably with the statistically obtained slopes shown in table 5. Also S.E. or standard error is an estimate of the standard deviation about the regression line shown in Figure 7. The two conditions ( $Q = 10$  and  $20$ ) are representative of the remaining data.

Conclusions

1. Droplet accelerations are unaffected by liquid film flow for steam velocities of 500 ft/sec or less.
2. The absolute magnitude of droplet acceleration does increase with increasing steam velocity.
3. Equation (2) may be used to predict the magnitude of droplet accelerations for  $305 \leq U_s \leq 1100$  feet per second.
4. First order statistical regression analysis supports all of the above conclusions.

List of Symbols

- $U$  - velocity  
 $\rho$  - density  
 $M$  - regression slope  
 $m$  - mass  
 $b$  - regression intercept  
 $C_D$  - drag coefficient  
 $A$  - crosssectional area  
 $V$  - volume  
 $a$  - acceleration  
E.A. - average experimentally observed droplet acceleration  
A.A. - average analytical droplet acceleration  
 $d$  - droplet  
 $R_e$  - Reynolds number  
 $\Delta$  - change in, as,  $\Delta U$  - change in velocity  
 $Q$  - liquid film flow rate  
 $t$  - time

Subscripts

- $d$  - droplet  
 $s$  - steam  
 $r$  - relative, as in relative velocity  $U_r$

Acknowledgements

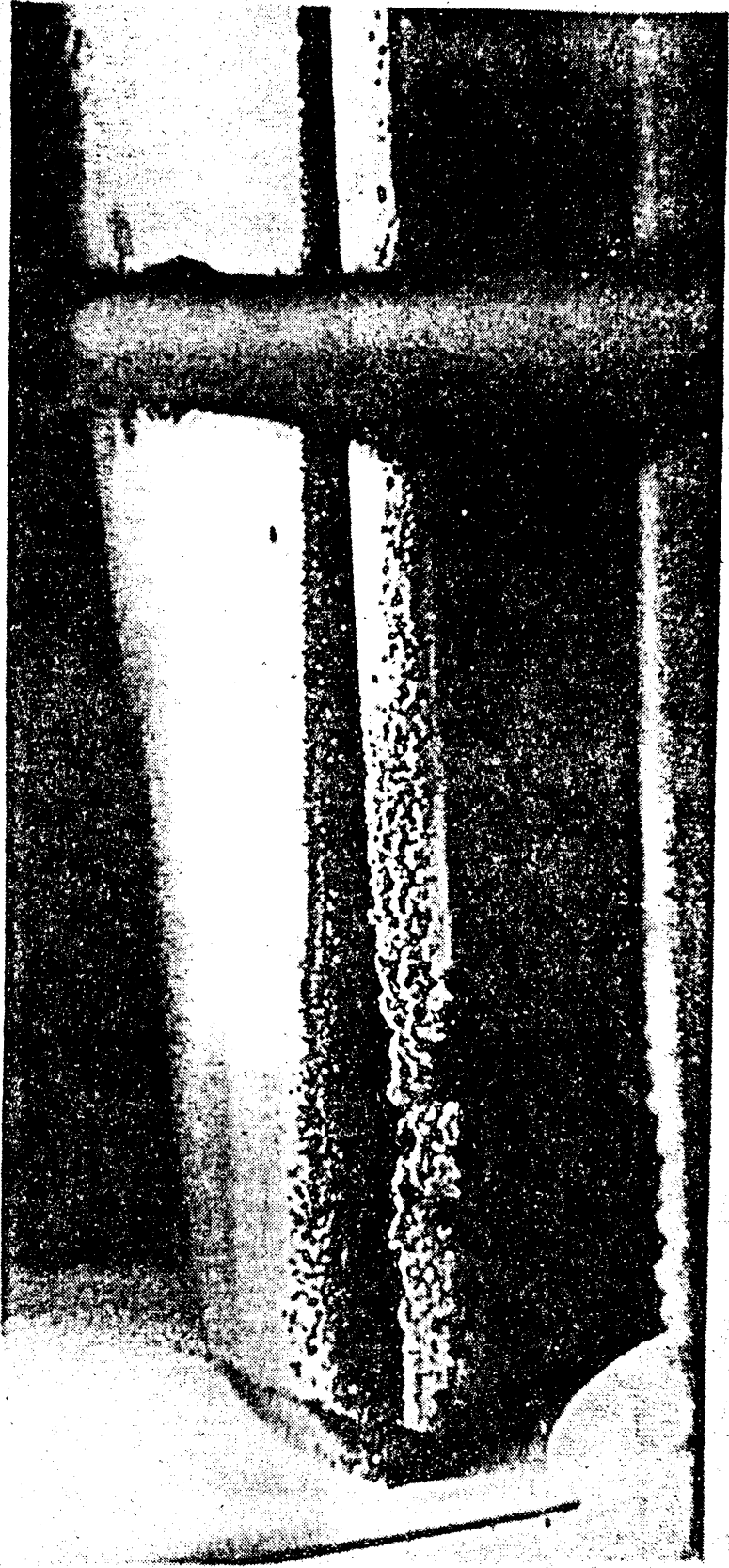
Special thanks go to:

- 1) Mr. R. Niedzielski for his diligent work in obtaining raw data by reviewing all the high speed motion pictures.
- 2) Mr. M. Wegenka for his excellent work in developing a digital computer program to reduce the raw data.
- 3) Professor F. G. Hammitt and Mr. W. Kim for their guidance and many helpful suggestions.

References

1. Christie, D. G., et. al. "The Formation of Water Drops Which Cause Turbine Blade Erosion," The Institution of Mechanical Engineers, London, April 13-15, 1966.
2. Lipson, Charles and Sheth, N.J., Statistical Design and Analysis of Engineering Experiments, McGraw - Hill Book Company, New York, 1973.
3. Staff of Statistical Research Laboratory, Elementary Statistics Using MIDAS - User's Manual, Second Edition, The University of Michigan, Ann Arbor, MI, December, 1976.
4. Serafini, J. S., Impingement of Water Droplets on Wedges and Diamond Airfoils at Supersonic Speeds, National Advisory Committee for Aeronautics, Technical Note 2971, 1953.
5. Sabersky, Acosta and Haystmann, Fluid Flow - A First Course in Fluid Mechanics, Second Edition, MacMillan Publishing Co., 1971.
6. Wegenka, M., Multiphase Flow and Cavitation Computer Analysis Programs, The University of Michigan Department of Mechanical Engineering, UMICH No. 014571-11-I, Dec. 1977.
7. Krzyzanowski, J., Erosion Problem of High Performance Steam Turbine, Seminar - University of Michigan Cavitation and Multiphase Flow Laboratory, Nov. 1977.
8. Krezczkowski, S., et. al., Investigations of Secondary Liquid Phase Structure in Steam Wake, University of Michigan Department of Mechanical Engineering, UMICH No. 014571-1-T, June, 1976 (Mod. 2, April, 1977).

D. G. CHRISTIE, G. W. HOWARD, H. E. FLOWE, A. N. McDONALD, AND P. SCHEPHER



*Fig. 4.2. Water erosion damage to blade and shield at inlet edge*

*FIGURE 1 - EXAMPLE OF WATER EROSION DAMAGE.*

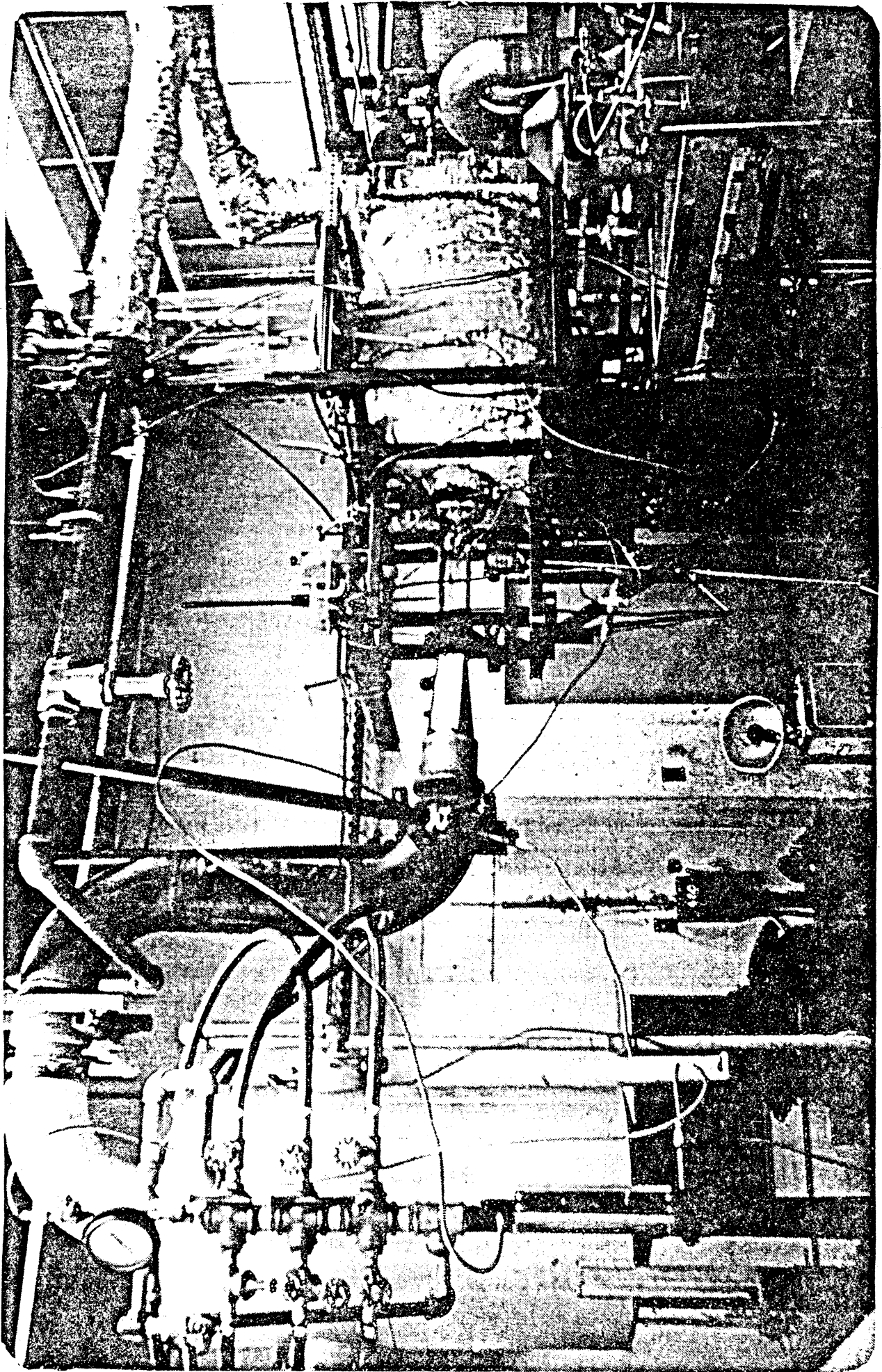


FIGURE 2 - TEST EQUIPMENT, UNIV. OF MICH. STEAM TUNNEL

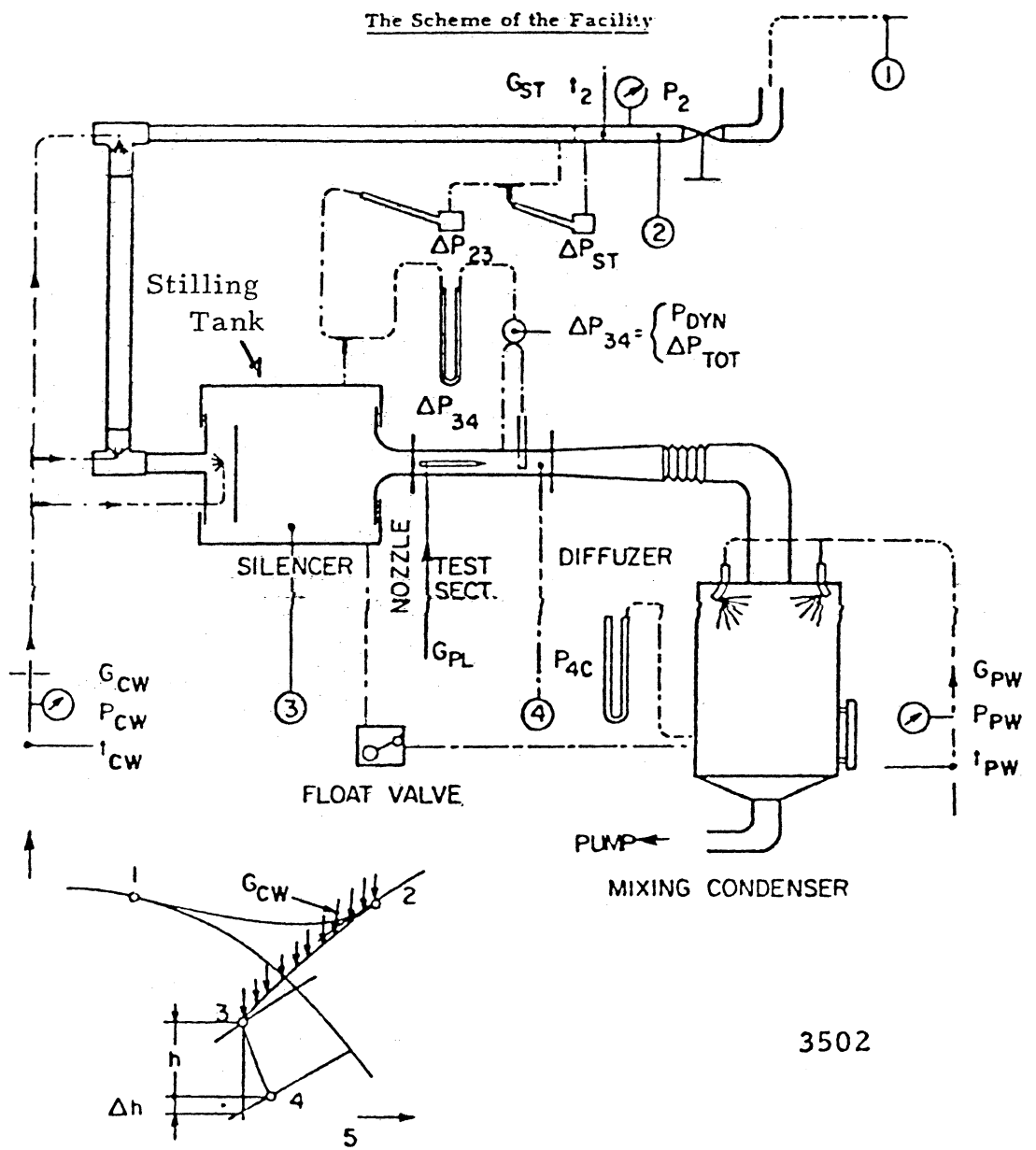


Figure 3 - Schematic Diagram of the University of Michigan Steam Tunnel



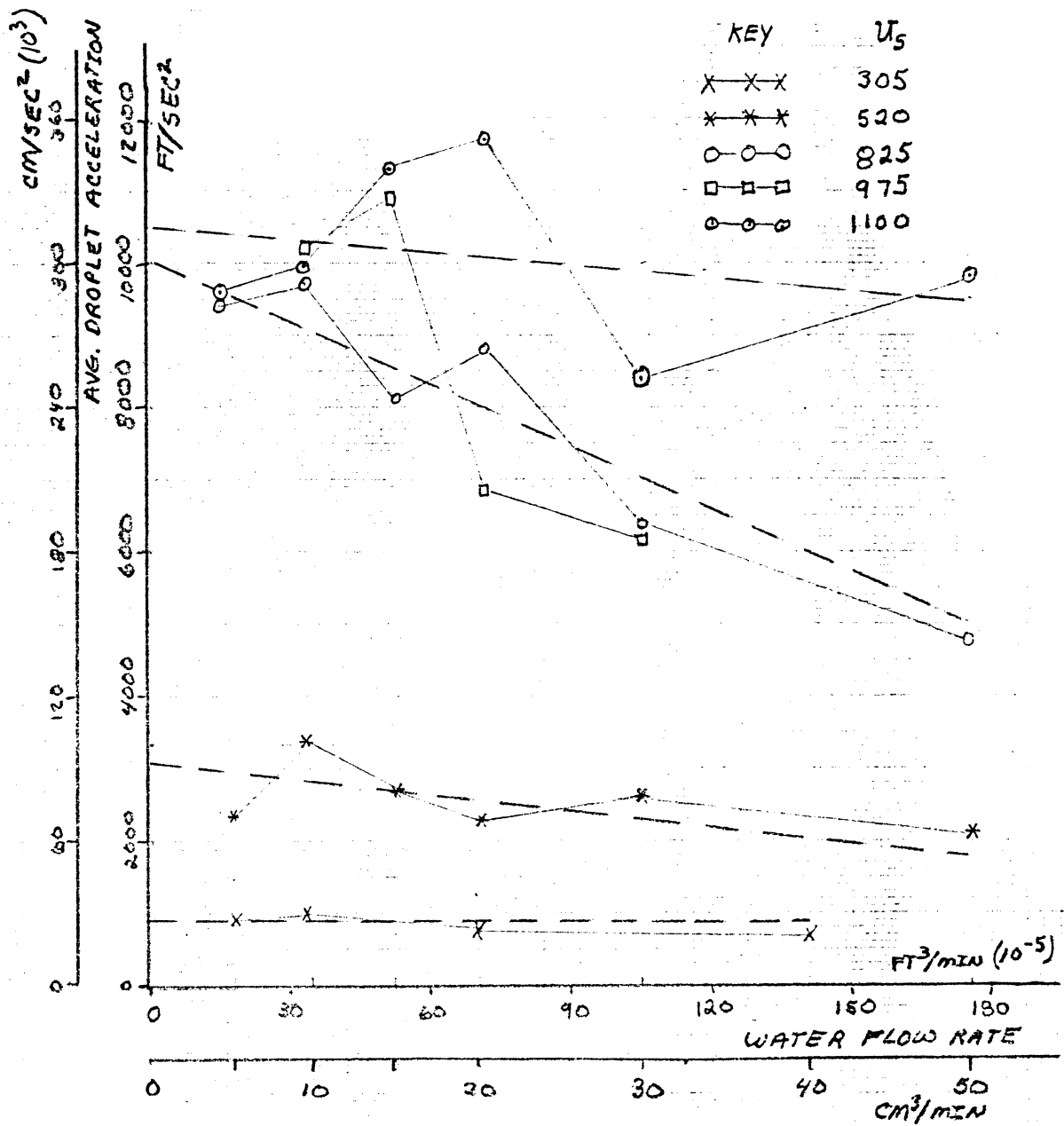
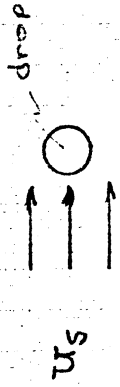


FIG. 4 - "AVERAGE OBSERVED DROPLET ACCELERATION VERSUS WATER FLOW RATE AT VARIOUS STEAM VELOCITIES". DOTTED LINES SHOW REGRESSION ANALYSIS RESULTS. NOTE: SLOPES OF REGRESSION LINES WERE NOT FOUND TO BE SIGNIFICANTLY DIFFERENT THAN ZERO. SEE STATISTICAL ANALYSIS.

FIRST ORDER ANALYTICAL MODEL

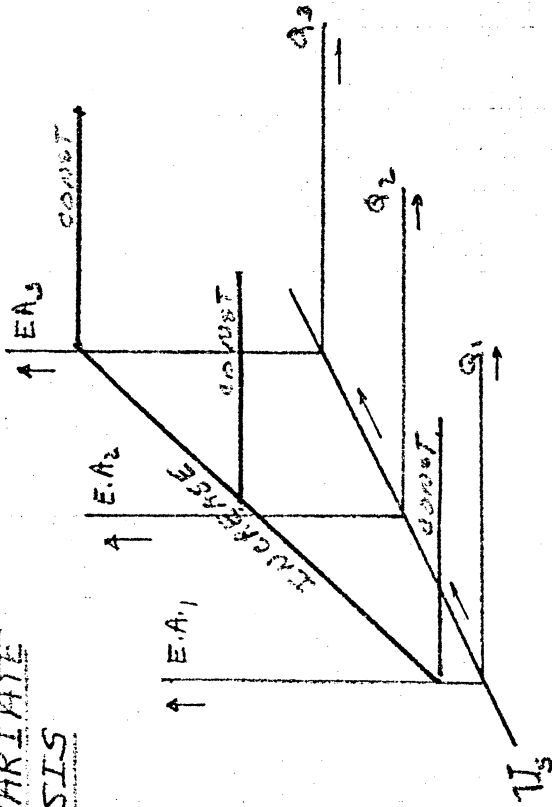


$$F = m a$$

$$a_d = \left\{ c_D \frac{\rho_s}{\rho_d} \frac{3}{4d} \right\} U_s^2$$

FIGURE 5 - SCHEMATIC OF ANALYTICAL MODEL

MULTIVARIATE ANALYSIS



REGRESSION EQA. FORM

$$EA_i = \alpha_1(q_i) + \beta(U_s) + \epsilon_i$$

↓ WEAK                      ↓ STRONG                      ↓ STD. ERROR

FIGURE 6 - SCHEMATIC OF MULTIVARIATE REGRESSION ANALYSIS

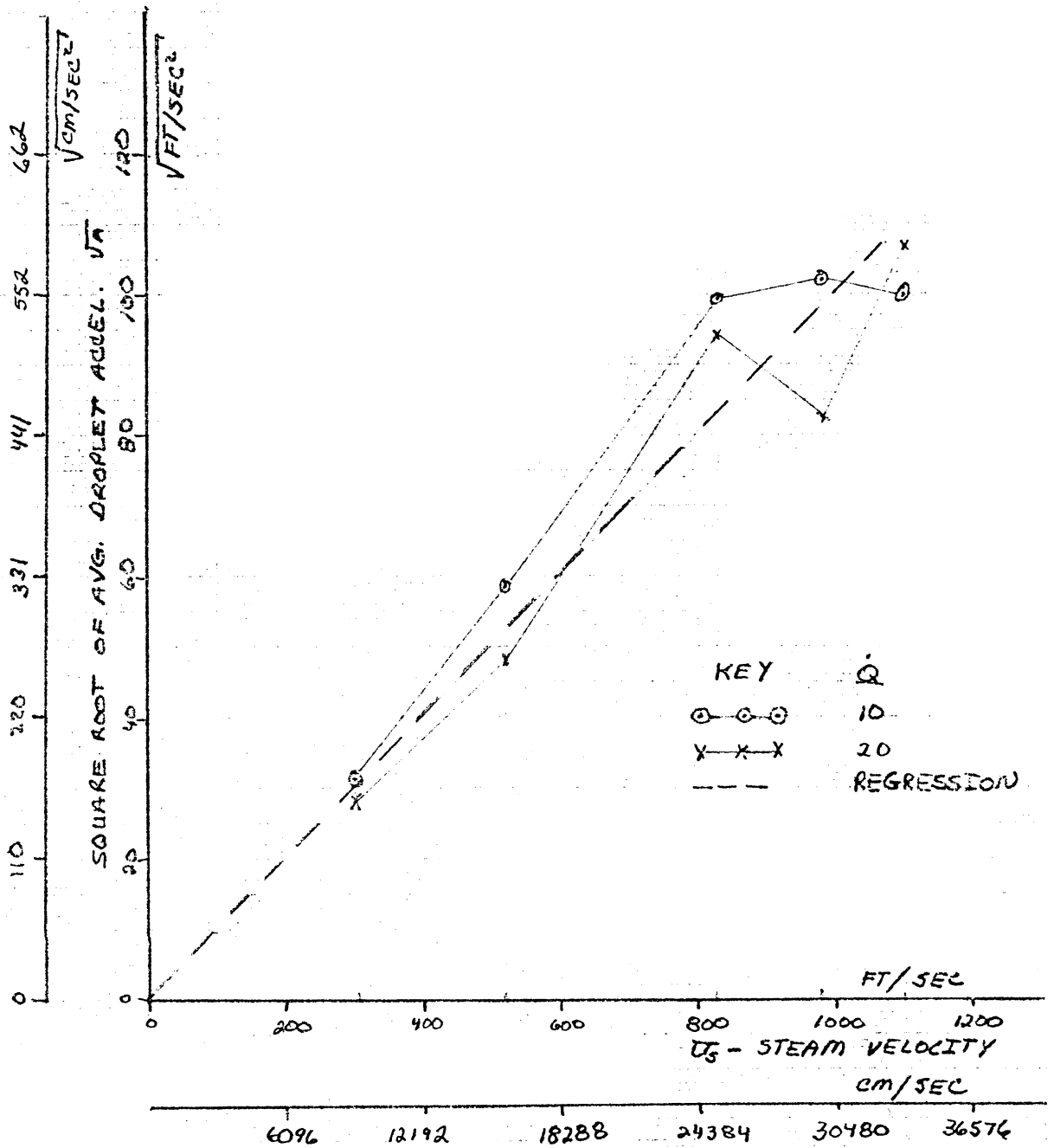


FIG. 7 - SQUARE ROOT OF AVERAGE DROPLET ACCELERATION VERSUS STEAM VELOCITY. DOTTED LINE SHOWS REGRESSION ANALYSIS RESULTS.

U <sub>5</sub> 9 10 <sup>5</sup> FT/SEC <sup>2</sup>	305		580		825		975		1100						
	E. A. FT/SEC <sup>2</sup>	A. A. FT/SEC <sup>2</sup>	R.	E. A. FT/SEC <sup>2</sup>	A. A. FT/SEC <sup>2</sup>	R.	E. A. FT/SEC <sup>2</sup>	A. A. FT/SEC <sup>2</sup>	R.	E. A. FT/SEC <sup>2</sup>	A. A. FT/SEC <sup>2</sup>	R.			
17.7	838	1242	0.782	2465	3666	0.699	9432	8018	1.418	—	9527	11916	0.910		
35.3	944	1014	1.010	3442	3867	0.983	9670	5245	2.059	10242	10173	1.152	9943	15272	0.700
53.0	—	—	—	2721	2914	0.966	8071	7044	1.262	10950	16211	1.270	11319	17346	0.690
70.6	770	1396	0.775	2282	2885	0.791	8858	5307	1.820	6861	10270	0.770	11700	16929	0.699
105.9	—	—	—	2601	3374	—	6352	6517	0.953	6205	10903	0.625	8378	16730	0.606
141.2	735	1004	0.727	—	—	—	—	—	—	—	—	—	—	—	—
176.6	—	—	—	2139	2966	0.746	4830	6089	0.964	—	—	—	9706	—	—

TABLE 1 - COMPARISON OF EXPERIMENTAL "EA" AND ANALYTICAL "AA" DROPLET ACCELERATION RATIOS. ENGLISH UNITS. R - ACCELERATION RATIO. ALL VALUES ARE AVERAGE VALUES FOR THE CONDITIONS SHOWN.

US Q cm/sec cm <sup>3</sup> /min	9296.4			15849.6			25146			29718			38528		
	E.A. cm/sec <sup>2</sup>	A.A. cm/sec <sup>2</sup>	R.	E.A. cm/sec <sup>2</sup>	A.A. cm/sec <sup>2</sup>	R.	E.A. cm/sec <sup>2</sup>	A.A. cm/sec <sup>2</sup>	R.	E.A. cm/sec <sup>2</sup>	A.A. cm/sec <sup>2</sup>	R.	E.A. cm/sec <sup>2</sup>	A.A. cm/sec <sup>2</sup>	R.
5	25550	37855	0.782	75144	109893	0.699	287500	244372	1.418	—	—	—	240390	363203	0.910
10	28780	30893	1.010	104906	117845	0.983	294750	157862	2.089	312187	310066	1.152	303406	465454	0.700
15	—	—	—	82940	88814	0.966	246000	214681	1.262	333750	31230	1.270	345000	528665	0.690
20	23454	42556	0.775	69542	87936	0.791	270000	161763	1.820	289117	312999	0.770	356625	512930	0.699
30	—	—	—	80275	102841	0.828	183593	198627	0.953	189140	332318	0.625	255374	509915	0.606
40	22117	30593	0.727	—	—	—	—	—	—	—	—	—	—	—	—
50	—	—	—	65203	90400	0.746	147187	185582	0.964	—	—	—	295833	478515	0.680

TABLE 2 - COMPARISON OF EXPERIMENTAL "EA" AND ANALYTICAL "AA" DROPLET ACCELERATIONS. CGS UNITS. R - ACCELERATION RATIO. ALL VALUES ARE AVERAGE VALUES FOR THE COUNTTAMS SHOWN.

$$E.A. = m(Q) + b$$

$U_s$ FT/SEC <sup>2</sup>	$m$ SLOPE	$b$ INTERCEPT	R-SQR <sup>①</sup> GOODNESS OF FIT, %	S.E. <sup>③</sup> STANDARD ERROR
305	(-6.0) <sup>②</sup>	945	1.1	740
520	(-29.5)	3403	2.5	2374
825	-104.6	9999	22.0	2849
975	-265.3	13526	32.5	3033
1100	(-17.3)	10512	0.4	3836

TABLE 3 - RESULTS OF STATISTICAL REGRESSION OF AVERAGE EXPERIMENTAL ACCELERATION "EA" ON FLOW RATE "Q".

- ① R-SQR, STATISTICAL PARAMETER - PER CENT VARIATION IN E.A. THAT IS ATTRIBUTABLE TO VARIATION IN Q, FLOW RATE. [2]
- ② SLOPES APPEARING IN PARENTHESES ARE NOT STATISTICAL DIFFERENT THAN ZERO SLOPE.
- ③ ESTIMATE OF STD. DEVIATION OF E.A. ALSO KNOWN AS STD. ERROR. [2]

$U_s$ $Q$ $10^{-5}$ FT <sup>3</sup> /MIN	305	520	825	975	1100
EA $\sqrt{FT/SEC^2}$	EA $\sqrt{FT/SEC^2}$	EA $\sqrt{FT/SEC^2}$	EA $\sqrt{FT/SEC^2}$	EA $\sqrt{FT/SEC^2}$	EA $\sqrt{FT/SEC^2}$
17.7	28.9	49.7	97.1	—	97.6
35.3	31	58.7	98.3	101.2	99.7
53.0	—	54	89.8	104.6	106.4
70.6	28	47.8	94.1	82.8	108.2
105.9	—	51	79.7	78.8	91.5
141.2	27	—	—	—	—
176.6	—	46.3	69.5	—	98.5

TABLE 4 - SQUARE ROOT OF EXPERIMENTAL DROPLET ACCELERATIONS. ENGLISH UNITS. AVERAGE VALUES FOR THE CONDITIONS SHOWN.



$$\sqrt{E.A.} = M(u_s) + b^{10}$$

Q FT <sup>3</sup> /MIN	M SLOPE	b INTERCEPT	R-SQR <sup>①</sup> GOODNESS OF FIT %	SE <sup>②</sup> STANDARD ERROR
17.7	0.098	0.0	76.1	16.4
35.3	0.100	0.0	75.1	15.5
53.0	0.101	0.0	60.9	17.5
70.6	0.092	0.0	74.4	16.0
105.9	0.084	0.6	42.8	16.5
141.2	0.081	0.0	—	11.7
176.6	0.085	0.0	53.2	19.4

TABLE 5 - RESULTS OF STATISTICAL REGRESSION OF SQUARE ROOT OF AVERAGE EXPERIMENTAL DROPLET ACCELERATION,  $\sqrt{E.A.}$ , ON STEAM VELOCITY,  $u_s$ ,

① R-SQR STATISTICAL PARAMETER - PERCENT VARIATION IN  $\sqrt{E.A.}$  ATTRIBUTABLE TO VARIATION IN  $u_s$ .

② ESTIMATE OF STD. DEVIATION OF  $\sqrt{E.A.}$  ALSO KNOWN AS STD. ERROR.

Appendix - A    "MIDAS Results"

Due to the nature of the physical phenomenon under consideration and due to the large amount of experimental data collected certain statistical tools were used to better understand the experimental results. Reduction of the initial raw data [6] resulted in 855 droplet accelerations for the flow condition outlined in tables 1 and 2. These 855 cases were broken into 327 subsets for which average droplet accelerations were obtained. (Do not confuse the average accelerations mentioned here with those shown in tables 1 and 2. Tables 1 and 2 data are average accelerations from the "855" dataset for each specific flow condition, i.e., for

$U_S = 305 \text{ ft/sec}$  and  $Q = 17.7 \times 10^{-5} \text{ ft}^3/\text{min}$   
average E.A. =  $838 \text{ ft/sec}^2$  is an average of the "855" dataset).

When performing a first order regression of E.A. on Q the 327 dataset was arranged into the following cases corresponding to constant steam velocity,  $U_S$ , and stored on data file "AVGACCEL":

<u>Cases</u>	<u><math>U_S</math> (ft/sec)</u>
1-45	305
46-129	520
130-185	825
186-246	975
247-327	1100

In a similar manner the "327" dataset was rearranged in order to perform a first order regression of  $\sqrt{\text{E.A.}}$  on  $U_S$  with liquid water film flow, Q, being held constant.

<u>Cases</u>	<u>Q (cm<sup>3</sup>/min)</u>
1-3	0
4-58	5
59-130	10
131-198	15
199-250	20
251-294	30
295-302	40
303-327	50

Note, these data were stored on data file "QACCEL."

MIDAS "REGRESSION" command was used to perform the regression analyses referred to throughout the text. These results can be found between the heavy dark lines on the attached output. Under "Regression" of E.A. on Q at constant  $U_S$ , for  $U_S = 520$  ft/sec the various important output parameters are noted. Consult MIDAS user's manual [3] concerning details of other output parameters or other MIDAS commands.

# *Relation Used*

AVG ACCEL  $\Rightarrow$  AA, R, U, Q

LOG ACCEL  $\Rightarrow$  AAC, R, U, Q

LOG<sub>10</sub> of AA = LAA

" of AAC = LAAC

**VARIABLE LABELS**  
 DATA FILE : AVGACCEL  
 AA - AVE. "327" DATA SET  
 ACCELERATION, FT/SEC  
 R - ACCEL RATIO  
 U - STEAM VELOCITY, FT/SEC  
 Q - FILM FLOW, CM<sup>3</sup>/MIN

RES **REGRESSION ANALYSES  
 DENOTED BY HEAVY LINES  
 SEE FOLLOWING PAGES**

COMMAND

?HIST V=AA CASES=1-45 OP=HISTZ  
 INTERVAL EXPRESSION -- #INT:(MIN,MAX) (MIN,MAX)/WIDTH #PER/(MIN,MAX)

**REGRESSION OF E.A ON Q @ CONSTANT U<sub>s</sub>**

HISTOGRAM CASES=CASE#:1-45

MIDPOINT HIST% COUNT FOR 1.AA (EACH X= 1)

*W. B. S. H.*

0.	20.0	9 +XXXXXXXXXX
676.67	46.7	21 +XXXXXXXXXXXXXXXXXXXXXXX
1353.3	22.2	10 +XXXXXXXXXXXX
2030.0	8.9	4 +XXXX
2706.7	0.	0 +
3383.4	0.	0 +
4060.0	2.2	1 +X

TOTAL 45 (INTERVAL WIDTH= 676.67)

COMMAND

?HIST V=AA CASES=1-45 OP=HISTZ  
 INTERVAL EXPRESSION -- #INT:(MIN,MAX) (MIN,MAX)/WIDTH #PER/(MIN,MAX)

HISTOGRAM CASES=CASE#:1-45

MIDPOINT HIST% COUNT FOR 1.AA (EACH X= 1)

0.	20.0	9 +XXXXXXXXXX
676.67	46.7	21 +XXXXXXXXXXXXXXXXXXXXXXX
1353.3	22.2	10 +XXXXXXXXXXXX
2030.0	8.9	4 +XXXX
2706.7	0.	0 +
3383.4	0.	0 +
4060.0	2.2	1 +X

TOTAL 45 (INTERVAL WIDTH= 676.67)

COMMAND

?DESCRIBE V=AA CASES=1-45

DESCRIPTIVE MEASURES CASES=CASE#:1-45

1.AA

45 0.

4060.0

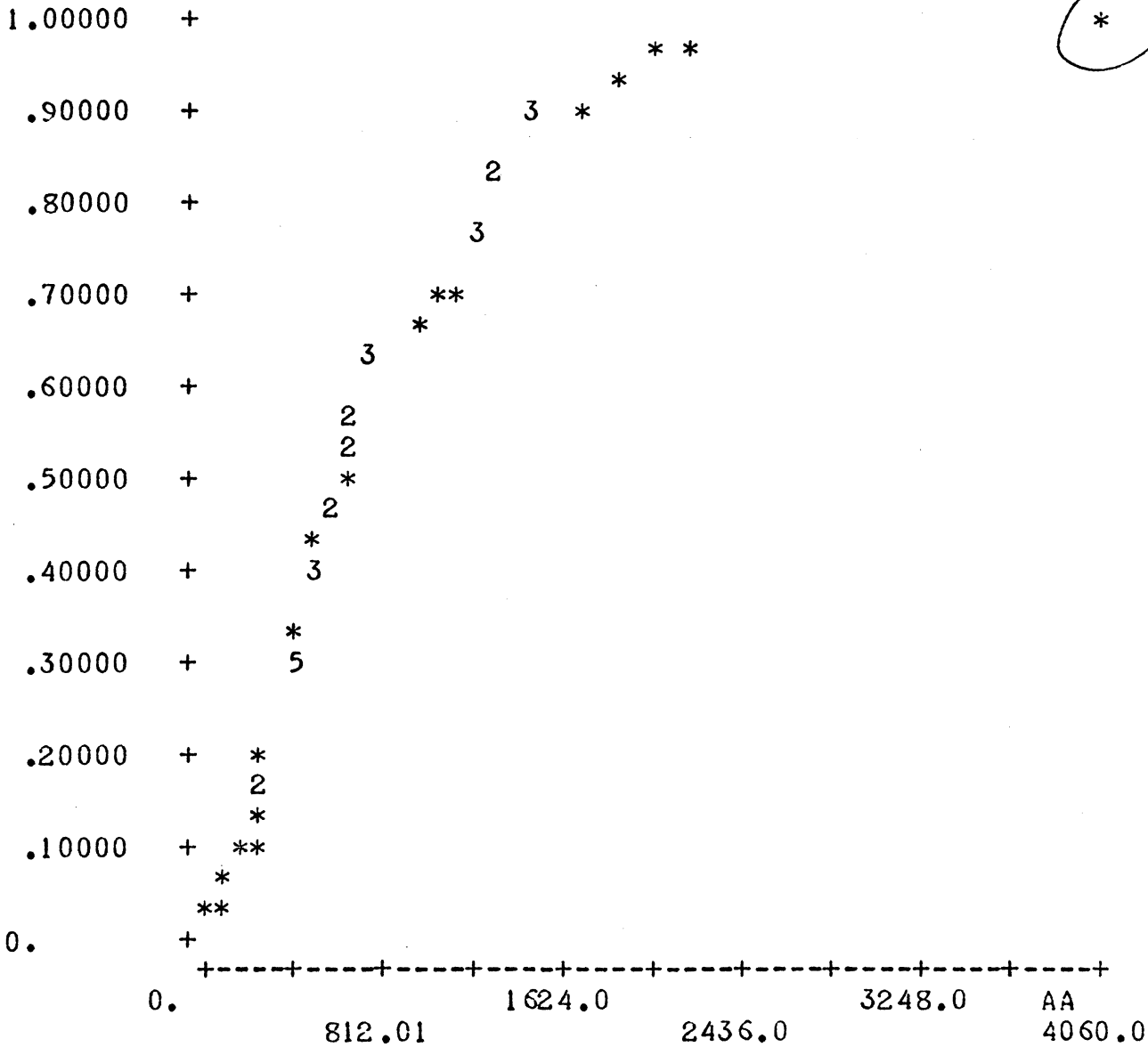
851.28

735.72

COMMAND  
?DIST V=AA CASES=1-45 PRØB=.5

DISTRIBUTIØNAL ANALYSIS CASES=CASE#:1-45

CUMULATIVE SAMPLE DISTRIBUTIØN ØF 1.AA N= 45 ØUT ØF 45



PRØB QUANTILE

.5000 632.73

COMMAND  
?REGRESS V=AA;Q CASES=1-45

LEAST SQUARES REGRESSIØN CASES=CASE#:1-45  $u = 305 \text{ ft/sec}^2$

ANALYSIS ØF VARIANCE ØF 1.AA N= 45 ØUT ØF 45

SØURCE	DF	SUM SQRS	MEAN SQR	F-STAT	SIGNIF
REGRESSIØN	1	.25527 +6	.25527 +6	.46589	.4985
ERRØR	43	.23561 +8	.54793 +6		
TØTAL	44	.23816 +8			

MULT R= .10353 R-SQR= .01072 SE= 740.22

*consistent with statistics that no relationship*

VARIABLE	PARTIAL	CØEFF	STD ERROR	T-STAT	SIGNIF
CØNSTANT		944.69	175.80	5.3736	.0000
4.Q	-.10353	-5.9627	8.7357	-.68256	.4985

*comparing to power*

COMMAND

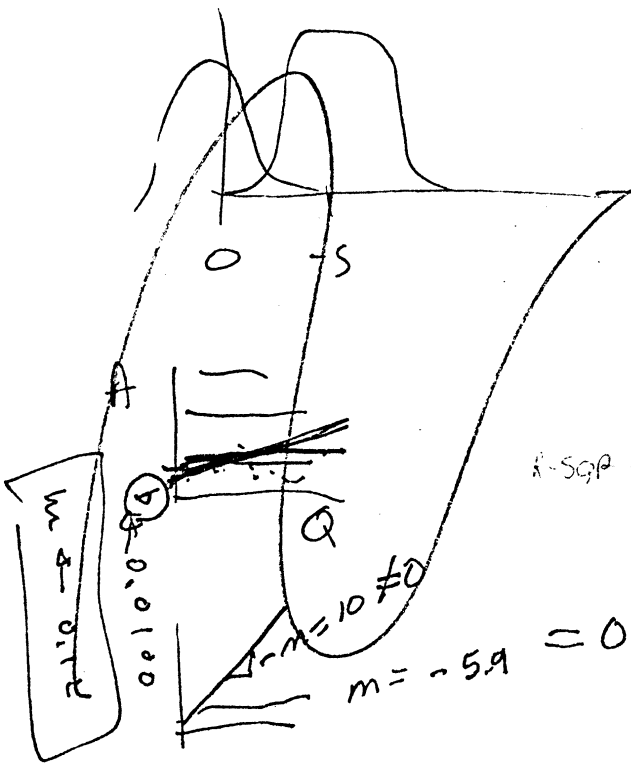
?

$$y = ax + b +$$

$$AA = 944 - 5.9(Q)$$

~~XXXXXXXXXX~~

$$\text{Std Err} (125) (8.7)$$



$$Y = mx + b$$

$$A = mQ + b$$

$$R-SQR = .01$$

*less than 1% of variation of AA can be explained by variation in Q*

$u = 520$

?HIST V=AA CASES=46-129 OP=HISTZ  
INTERVAL EXPRESSION -- #INT: (MIN,MAX) (MIN,MAX)/WIDTH #PER/(MIN,MAX)

HISTOGRAM CASES=CASE#:46-129

$u = 520 \text{ ft/sec}$

MIDPOINT HIST% COUNT FOR 1.AA (EACH X= 2)

-7381.8	1.2	1	+X
-4921.2	0.	0	+
-2460.6	1.2	1	+X
.62497	-1 3.6	3	+XX
2460.7	75.0	63	+XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX
4921.3	14.3	12	+XXXXXX
7381.9	1.2	1	+X
9842.5	2.4	2	+X
12303.	0.	0	+
14764.	1.2	1	+X
TOTAL		84	(INTERVAL WIDTH= 2460.6)

COMMAND  
?DESCRIBE V=AA CASES=46-129)←

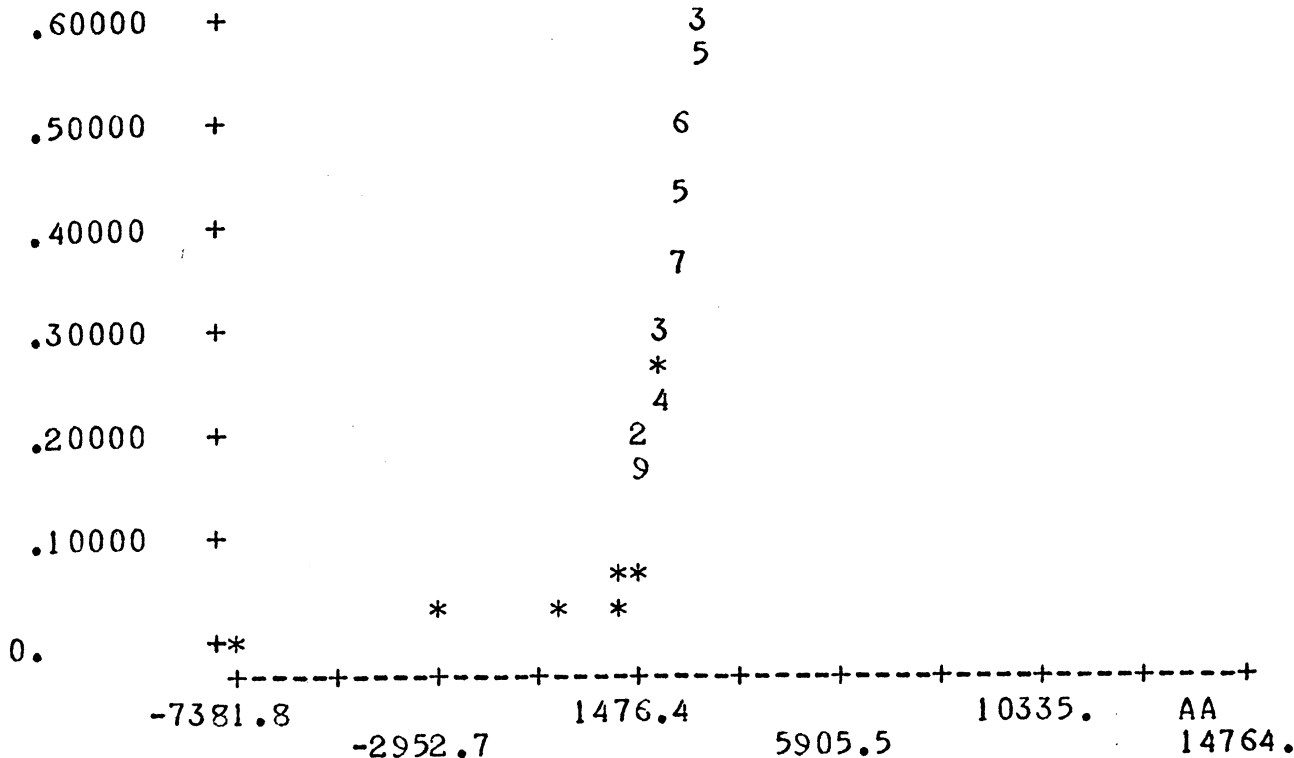
DESCRIPTIVE MEASURES CASES=CASE#:46-129

VARIABLE	N	MINIMUM	MAXIMUM	MEAN	STD DEV
1.AA	84	-7381.8	14764.	<u>2879.7</u>	2389.0

COMMAND  
?DIST V=AA CASES=46-129 PR0B=.5

DISTRIBUTIONAL ANALYSIS CASES=CASE#:46-129

CUMULATIVE SAMPLE DISTRIBUTION OF 1.AA	N= 84	OUT OF 84
1.00000	+	2 *
		* *
		4*
.90000	+	4
		2
.80000	+	5
		3*
.70000	+	2



**SAMPLE REGRESSION RESULTS**

```

COMMAND
?REGRESS V=AA;Q CASES46-129

```

LEAST SQUARES REGRESSION CASES=CASE#:46-129  $\Rightarrow U_s = \underline{520 \text{ ft/sec}}$

ANALYSIS OF VARIANCE OF 1.AA N= 84 OUT OF 84

SOURCE	DF	SUM SQRS	MEAN SQR	F-STAT	SIGNIF
REGRESSION	1	.11675 +8	.11675 +8	2.0719	.1538
ERROR	82	.46205 +9	.56347 +7		
TOTAL	83	.47372 +9			

MULT R= .15699 R-SQR= .02464 SE= 2373.8

*← Goodness of fit*  
*← Std error*

VARIABLE	PARTIAL	CØEFF	STD ERROR	T-STAT	SIGNIF
CØNSTANT		3402.7	446.23	7.6255	.0000
4.Q	-.15699	-29.388	20.417	-1.4394	.15385

$$y = b + m(x)$$

$$AA = 3402 - 29.4(9)$$

(46)      (20.4)

Compares to zero slope!  
T-stat test, anything less than .0010 bad.

```

COMMAND
?

```



u = 825

?HIST V=AA CASES=130-185 OP=HISTZ  
INTERVAL EXPRESSION -- #INT: (MIN, MAX) (MIN, MAX)/WIDTH #PER/(MIN, MAX)

u = 825 ft/sec

HISTOGRAM CASES=CASE#:130-185

MIDPOINT HISTZ COUNT FOR 1.AA (EACH X= 1)

738.19	1.8	1 +X
2952.8	8.9	5 +XXXXX
5167.3	19.6	11 +XXXXXXXXXXXX
7381.9	28.6	16 +XXXXXXXXXXXXXXXX
9596.5	23.2	13 +XXXXXXXXXXXXXXXX
11811.	12.5	7 +XXXXXXX
14026.	3.6	2 +XX
16240.	1.8	1 +X

TOTAL 56 (INTERVAL WIDTH= 2214.6)

COMMAND  
?DESV←SCRIBE V=AA CASES=130-185

ERROR -- INVALID COMMAND: "DESSCRIBE"  
COMMAND CANCELLED

COMMAND  
?DESCRIBE V=AA CASES=130-185

DESCRIPTIVE MEASURES CASES=CASE#:130-185

VARIABLE	N	MINIMUM	MAXIMUM	MEAN	STD DEV
1.AA	56	738.19	16240.	<u>7871.8</u>	3195.2

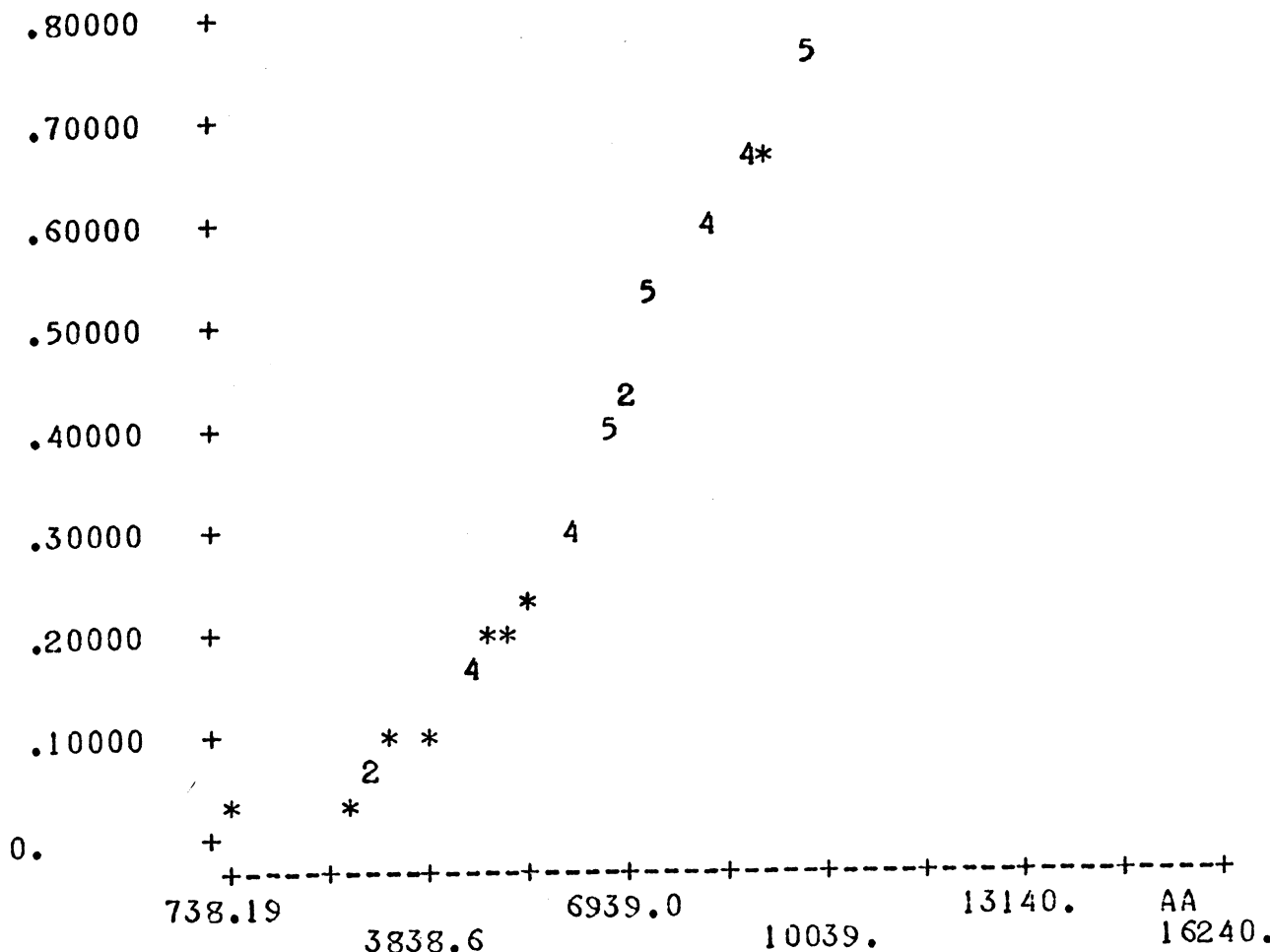
COMMAND  
?DIST V=AA CASES=130-185 PRØB=.5

DISTRIBUTIONAL ANALYSIS CASES=CASE#:130-185

CUMULATIVE SAMPLE DISTRIBUTION OF 1.AA N= 56 OUT OF 56  
1.00000 + \*

.90000 +

\* \*  
3  
3



PRØB QUANTILE

.5000 7381.9

COMMAND  
?REGRESS V=AA;Q CASES=130-185

LEAST SQUARES REGRESSION CASES=CASE#:130-185  $\Rightarrow U_s = 825 \text{ ft/sec.}$

ANALYSIS OF VARIANCE OF 1.AA N= 56 OUT OF 56

SOURCE	DF	SUM SQRS	MEAN SQR	F-STAT	SIGNIF
REGRESSION	1	.12325 +9	.12325 +9	15.185	.0003
ERROR	54	.43828 +9	.81163 +7		
TOTAL	55	.56153 +9			

MULT R= .46849 R-SQR= .21949 SE= 2848.9

VARIABLE	PARTIAL	CØEFF	STD ERRØR	T-STAT	SIGNIF
CØNSTANT		9991.2	663.89	15.050	.0000
4.Q	-.46849	-104.57	26.835	-3.8968	.0003

COMMAND  
?

AA = 9991 - 104(Q)  
Std Error

u = 975

HIST V=AA CASES=186-246 I←OP=HISTZ  
INTERVAL EXPRESSION -- #INT:(MIN,MAX) (MIN,MAX)/WIDTH #PER/(MIN,MAX)

HISTOGRAM CASES=CASE#:186-246

u = 975 *At/acc*

MIDPOINT	HISTZ	COUNT	FØR 1.AA (EACH X= 1)
2214.6	1.6	1	+X
4640.0	26.2	16	+XXXXXXXXXXXXXXXXXXXX
7065.5	31.1	19	+XXXXXXXXXXXXXXXXXXXX
9491.0	13.1	8	+XXXXXXXXXX
11916.	14.8	9	+XXXXXXXXXX
14342.	8.2	5	+XXXXXX
16767.	3.3	2	+XX
19193.	1.6	1	+X
TOTAL		61	(INTERVAL WIDTH= 2425.5)

COMMAND  
?DESCRIBE V=186-246#  
?DESCRIBE V=AAB← CASES=186-246

DESCRIPTIVE MEASURES CASES=CASE#:186-246

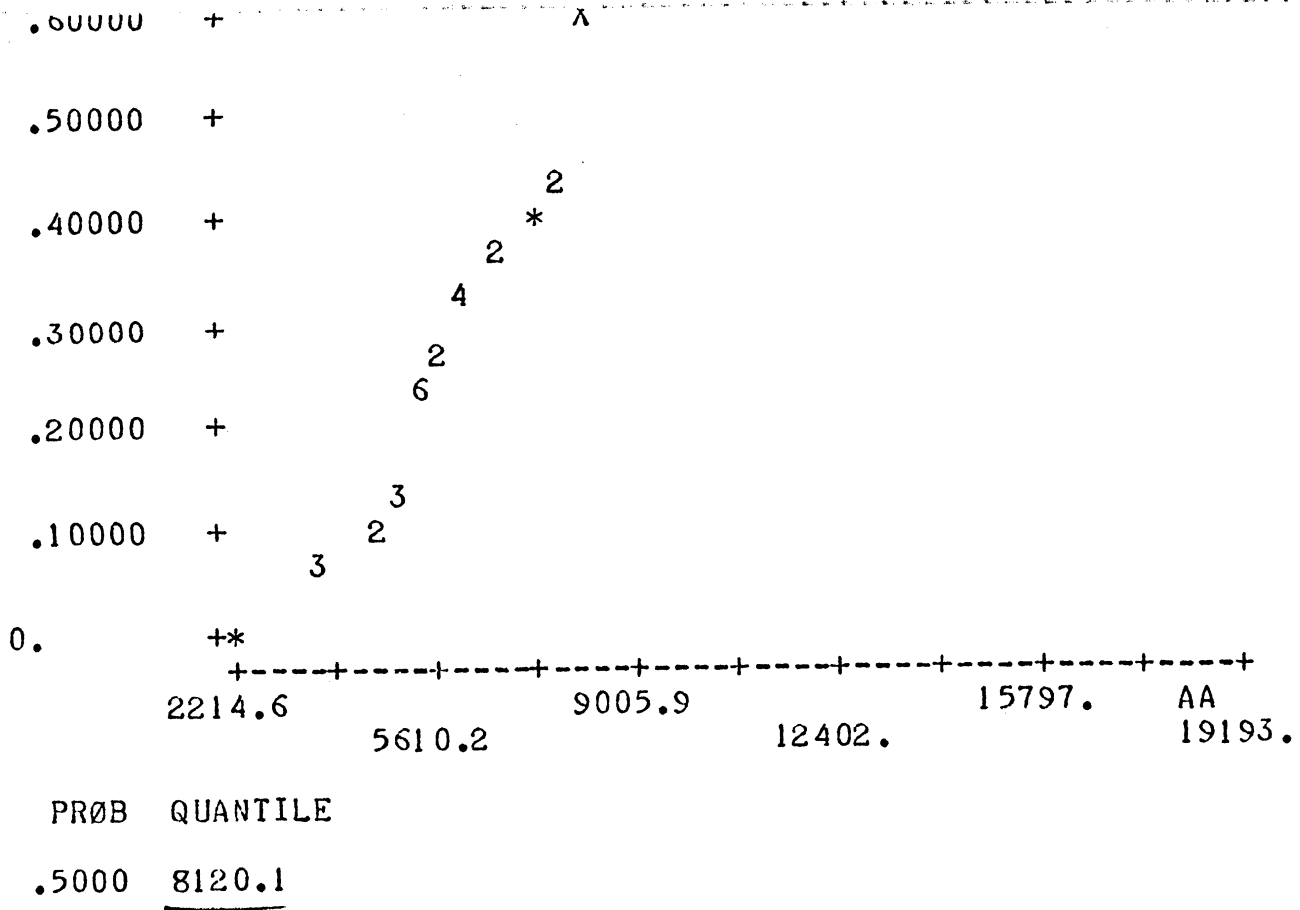
VARIABLE	N	MINIMUM	MAXIMUM	MEAN	STD DEV
1.AA	61	2214.6	19193.	8525.5	3661.7

COMMAND  
?DIST V=AA CASES=186-246 PRØB=.5

DISTRIBUTIØNAL ANALYSIS CASES=CASE#:186-246

CUMULATIVE SAMPLE DISTRIBUTIØN ØF 1.AA N= 61 ØUT ØF 61

1.00000	+				2	*
					3	*
.90000	+				4	*
					4	
.80000	+					
						*
.70000	+				2	
					5	



COMMAND  
 ?REGRESS V=AA;Q CASES=186-246  $\Rightarrow U_5 = 975 \text{ ft/sec}$

LEAST SQUARES REGRESSION CASES=CASE#:186-246

ANALYSIS OF VARIANCE OF 1.AA N= 61 OUT OF 61

SOURCE	DF	SUM SQRS	MEAN SQR	F-STAT	SIGNIF
REGRESSION	1	.26170 +9	.26170 +9	28.446	.0000
ERROR	59	.54280 +9	.92000 +7		
TOTAL	60	.80450 +9			

MULT R = .57035 R-SQR = .32530 SE = 3033.1

32%

VARIABLE	PARTIAL	CØEFF	STD ERROR	T-STAT	SIGNIF
CONSTANT		13526.	1014.8	13.328	.0000
4.Q	-.57035	-265.25	49.733	-5.3335	.0000

COMMAND  
 ?

AA = 13526 -265(4)  
 1014 49.7



HIST#  
 ?HIST V=AA CASES=247-327 OP=HISTZ  
 INTERVAL EXPRESSION -- #INT: (MIN,MAX) (MIN,MAX)/WIDTH #PER/(MIN,MAX)  
 =

*U<sub>5</sub> = 1100 ft/sec*

HISTOGRAM CASES=CASE#:247-327

MIDPOINT HIST% COUNT FOR 1.AA (EACH X= 1)

2952.8	1.2	1 +X
5085.3	12.3	10 +XXXXXXXXXX
7217.8	22.2	18 +XXXXXXXXXXXXXXXXXXXX
9350.4	25.9	21 +XXXXXXXXXXXXXXXXXXXXXXXX
11483.	19.8	16 +XXXXXXXXXXXXXXXXXXXX
13615.	2.5	2 +XX
15748.	9.9	8 +XXXXXXXXXX
17881.	3.7	3 +XXX
20013.	1.2	1 +X
22146.	1.2	1 +X
TOTAL		81 (INTERVAL WIDTH= 2132.5)

COMMAND  
 ?DESCRIBE V=AA CASES=247-327

DESCRIPTIVE MEASURES CASES=CASE#:247-327

VARIABLE	N	MINIMUM	MAXIMUM	MEAN	STD DEV
1.AA	81	2952.8	22146.	<u>10201.</u>	3819.4

COMMAND  
 ?REGRESS V=AA;Q CASES=247-2+327 ⇒ *U<sub>5</sub> = 1100 ft/sec*

LEAST SQUARES REGRESSION CASES=CASE#:247-327

ANALYSIS OF VARIANCE OF 1.AA N= 81 OUT OF 81

SOURCE	DF	SUM SQRS	MEAN SQR	F-STAT	SIGNIF
REGRESSION	1	.45454 +7	.45454 +7	.30890	.5799
ERROR	79	.11625+10	.14715 +8		
TOTAL	80	.11670+10			

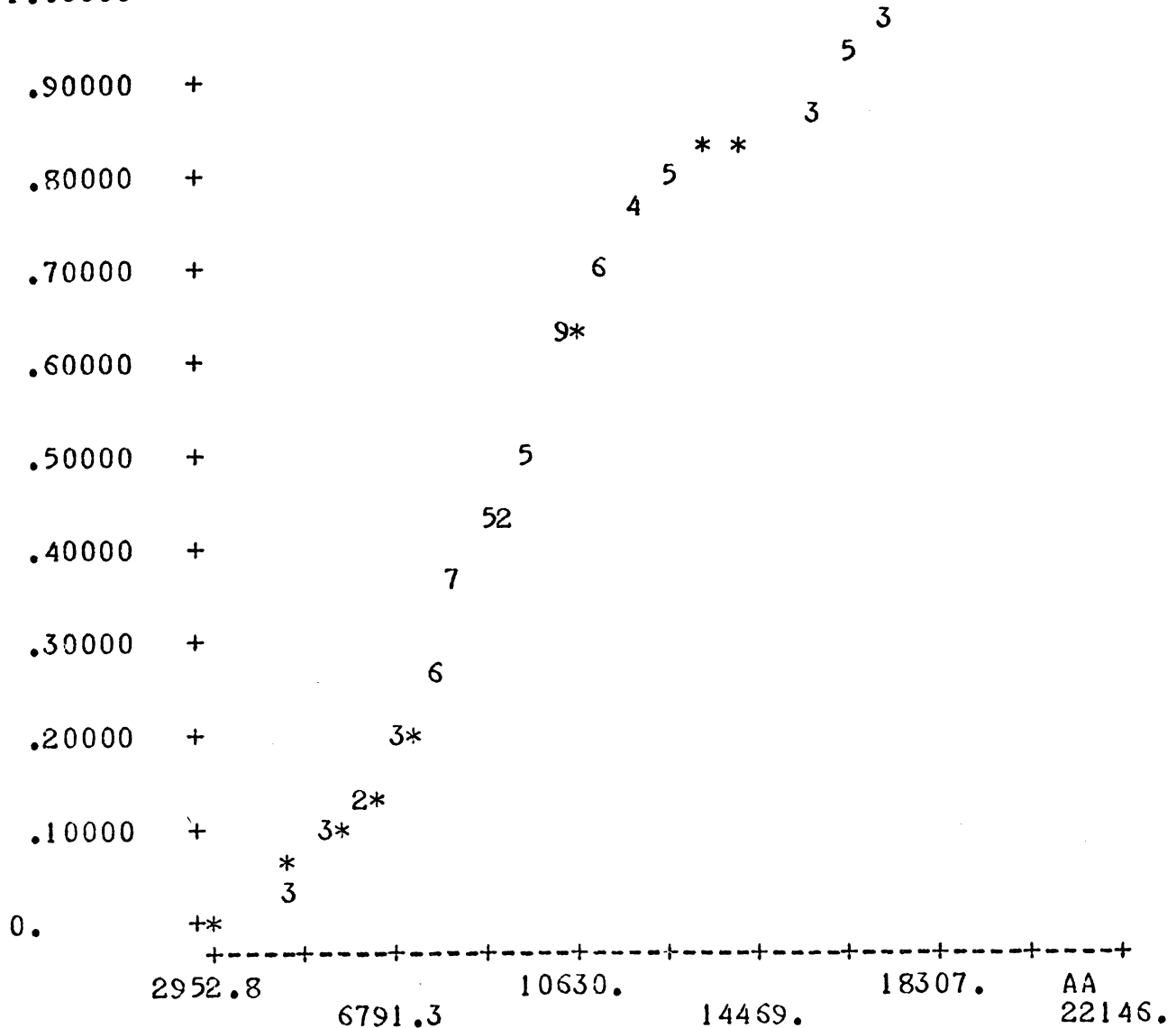
MULT R= .06241 R-SQR = .00389 SE= 3836.0

VARIABLE	PARTIAL	COEFF	STD ERROR	T-STAT	SIGNIF
CONSTANT		10512.	703.91	14.934	.0000
4.Q	-.06241	-17.273	31.079	-.55579	.5799

COMMAND  
 ?DIST V=AA CASES=247-327 P0←R0B=.5

DISTRIBUTIONAL ANALYSIS CASES=CASE#:247-327

CUMULATIVE SAMPLE DISTRIBUTION OF 1.AA N= 81 OUT OF 81  
 1.00000 + \* \*



PR0B QUANTILE

.5000 9596.5

COMMAND  
 ?

$AA = 10512 - 17.2 (9)$

703

31

↑  
Bad

Neglect Remaining  
 Output ↓

REGRESS V=AA;Q  
 CASES TO SELECT  
 =ALL

LEAST SQUARES REGRESSION

ANALYSIS OF VARIANCE OF 1.AA N= 327 OUT OF 327

SOURCE	DF	SUM SQRS	MEAN SQR	F-STAT	SIGNIF
REGRESSION	1	.71320 +8	.71320 +8	3.3347	.0688
ERROR	325	.69509+10	.21387 +8		
TOTAL	326	.70222+10			

MULT R= .10078 R-SQR= .01016 SE= 4624.6

VARIABLE	PARTIAL	CØEFF	STD ERRØR	T-STAT	SIGNIF
CØNSTANT		6998.8	450.21	15.546	.0000
4.Q	-.10078	-37.216	20.380	-1.8261	.0688

CØMMAND

?TRANS  
 TRANSFØRMATION EXPRESSION (E.G., V9=V2+V5 ØR V10=SQRT(V8) )  
 =V10=LØG10(AA) L=LA

ERRØR -- SYNTAX: "V10=LØG10(AA) L=LA"  
 ENTER NEW VALUE FØR TRANSFØRMATION EXPRESSION (E.G., V9=V2+V5 ØR  
 V10=SQRT(V8) )  
 =

ERRØR -- ILLEGAL VALUE

THE EXPRESSION STARTS WITH "VK=", WHERE 0 < K < 10000; THE RIGHT-SIDE  
 MAY BE. "A", "A ØP B", "FCN", "FCN(A)", "FCN(A,B)", WHERE A AND B ARE  
 VARIABLES AND/ØR CØNSTANTS WITH DECIMAL PØINTS, FCN IS FUNCTION NAME.

ENTER NEW VALUE FØR TRANSFØRMATION EXPRESSION (E.G., V9=V2+V5 ØR  
 V10=SQRT(V8) )  
 =V20=LØG10(AA)  
 LABEL FØR THE RESULT VARIABLE(S)  
 =LAA

LØG10 TRANSFØRMATION

VARIABLE	TØTAL	VALID	MISS
20.LAA	327	323	4

CØMMAND  
 ?REGRESS V=LAA;Q CASESE←=ALL

LEAST SQUARES REGRESSION

ANALYSIS OF VARIANCE OF 20.LAA N= 323 OUT OF 327

SOURCE	DF	SUM SQRS	MEAN SQR	F-STAT	SIGNIF
REGRESSION	1	.39460	.39460	1.9284	.1659
ERROR	321	65.685	.20463		
TOTAL	322	66.080			

MULT R= .07728 R-SQR= .00597 SE= .45236

VARIABLE	PARTIAL	COEFF	STD ERROR	T-STAT	SIGNIF
CONSTANT		3.6946	.44400	-1 83.211	0.
4.Q	-.07728	-.27783	.20007	-2 -1.3887	.1659

COMMAND

?DIST V=LAA CASES=ALL OP==←HISTZ

ERROR -- INVALID KEYWORD: "OP=HISTZ"

DISTRIBUTIONAL ANALYSIS

CUMULATIVE SAMPLE DISTRIBUTION OF 20.LAA N= 323 OUT OF 327

1.00000 + 52\*  
X  
9

.90!

\$.07 USED. CONTINUE(YES/NO) %0200 DATA CHECK.

?%0200 DATA CHECK.

??#

#

RES

"Y" OR "N"?N

COMMAND

?HIST=V#

?HIST V=LAA CASES=ALL OP=HISTZ

INTERVAL EXPRESSION -- #INT: (MIN, MAX) (MIN, MAX)/WIDTH #PER/(MIN, MAX)

=

HISTOGRAM

MIDPOINT HISTZ COUNT FOR 20.LAA (EACH X= 2)

1.8682	.6	2 +X
2.0139	0.	0 +
2.1596	0.	0 +
2.3053	.6	2 +X
2.4510	1.2	4 +XX
2.5967	1.9	6 +XXX
2.7424	3.1	10 +XXXXX
2.8882	1.5	5 +XXX
3.0339	2.5	8 +XXXX
3.1796	6.8	22 +XXXXXXXXXX
3.3253	7.7	25 +XXXXXXXXXXXXX
3.4710	7.7	25 +XXXXXXXXXXXXX



```

3.6167      9.6      51 +XXXXXXXXXXXXXXXXXXXXX
3.7624     13.0     42 +XXXXXXXXXXXXXXXXXXXXX
3.9081     17.6     57 +XXXXXXXXXXXXXXXXXXXXX
4.0539     19.2     62 +XXXXXXXXXXXXXXXXXXXXX
4.1996      5.9     19 +XXXXXXXXXXXX
4.3453      .9       3  +XX

```

```

MISSING      4
TOTAL      327 (INTERVAL WIDTH= .14571)

```

```

COMMAND
?READ

```

```

NOTE. THIS DATASET CURRENTLY HAS 5 VARIABLES AND 327 CASES
FILE CONTAINING DATA OR * TO ENTER DATA HERE
=WGABAR
FORMAT SPECIFICATION OR * TO ENTER DATA SEPARATED BY COMMAS
=: ←*
VARIABLES TO READ (E.G., 1-10)
=1-4
LABELS CORRESPONDING TO THESE VARIABLES OR * FOR STANDARD LABELS
=AA,RC,U,Q
CASES TO ASSIGN TO THE DATA BEING READ (E.G., 1-98)
=1-327

```

WG BAR

```

READ OBSERVATIONS 1-327
VARIABLES BY CASE

```

```

327 CASES READ FOR 4 VARIABLES
CASES CHANGED FOR 4 EXISTING VARIABLES

```

```

COMMAND
?REGRESS V=AA;Q CASES=ALL

```

```

LEAST SQUARES REGRESSION

```

```

ANALYSIS OF VARIANCE OF 1.AA N= 327 OUT OF 327

```

SOURCE	DF	SUM SQRS	MEAN SQR	F-STAT	SIGNIF
REGRESSION	1	.66258+11	.66258+11	3.3347	.0688
ERROR	325	.64576+13	.19869+11		
TOTAL	326	.65238+13			

```

MULT R= .10078 R-SQR= .01016 SE= .14096 +6

```

VARIABLE	PARTIAL	COEFF	STD ERROR	T-STAT	SIGNIF
CONSTANT		.21332 +6	13722.	15.546	.0000
4.Q	-.10078	-1134.4	621.19	-1.8261	.0688

```

COMMAND
?TRANS
TRANSFORMATION EXPRESSION (E.G., V9=V2+V5 OR V10=SQRT(V8) )
=V30=LOG10(AA)
LABEL FOR THE RESULT VARIABLE(S)
=LAAC

```

LØGIO TRANSFORMATION

VARIABLE	TOTAL	VALID	MISS
30.LAAC	327	323	4

COMMAND  
 ?REGRESS V=LAAC;Q CASES=ALL

LEAST SQUARES REGRESSION

ANALYSIS OF VARIANCE OF 30.LAAC N= 323 OUT OF 327

SOURCE	DF	SUM SQRS	MEAN SQR	F-STAT	SIGNIF
REGRESSION	1	.39460	.39460	1.9284	.1659
ERROR	321	65.685	.20463		
TOTAL	322	66.080			

MULT R= .07728 R-SQR= .00597 SE= .45236

VARIABLE	PARTIAL	CØEFF	STD ERRØR	T-STAT	SIGNIF
CØNSTANT		5.1786	.44400	-1 116.64	0.
4.Q	-.07728	-.27783	-.20007	-2 -1.3887	.1659

COMMAND  
 ?SIGNØFF

ERRØR -- INVALID COMMAND: "SIGNØFF"  
 COMMAND CANCELLED

COMMAND  
 ?STØP

USE \$RES TO RE-ENTER MIDAS  
 #SIGNØFF  
 #ODLU 15:39:40-17:22:21 FRI MAR 31/78  
 #TERM,NORMAL,UNIV  
 #ELAPSED TIME 102.685 MIN. \$2.40  
 #CPU TIME USED 3.021 SEC. \$.49  
 #CPU STØR VMI 4.116 PAGE-MIN. \$.24  
 #WAIT STØR VMI 141.476 PAGE-HR.  
 #DRUM READS 5806  
 #APPRØX. CØST ØF THIS RUN IS \$3.23  
 #DISK STØRAGE 128 PAGE-HR. \$.01  
 #APPRØX. REMAINING BALANCE: \$73.29  
 ©

Q ACCEL - ft/sec  
arranged by Q

SR-AA - Sq root avg accel

REGRESSION OF  $\sqrt{EA}$  ON  $U_s$  @ CONSTANT Q

REGRESSION ANALYSIS FOR EACH Q DENOTED  
BY HEAVY LINES ON FOLLOWING PAGES

### VARIABLE LABELS

DATA FILE : Q ACCEL

V1. AA - AVG ACCEL, FT/SEC<sup>2</sup>

V2. R - ACCEL RATIO

V3. U - STEAM VELOCITY, FT/SEC

V4. Q - FILM FLOW RATE, CM<sup>3</sup>/MIN

V20. SRAA - SQUARE ROOT  
AVG. ACCEL,  $\sqrt{FT/SEC^2}$

04/05/78

SIGNON ODLU  
#ENTER USER PASSWORD.  
?STEAM  
#TERM, NORMAL, UNIV  
\*\*\*LAST SIGNON WAS: 00:19:25 TUE APR 04/78  
# USER "ODLU" SIGNED ON AT 17:27:51 ON WED APR 05/78  
#F

AVGACCEL	CUMACCEL	LF	LINEFIT	MDPRDATA	PF1LE	PLOT1
PLOT2	QACCEL	TDATA	TEMP	WATERDROP	WD	WDATA
WDGRAF	WG	WGABAR	WGAVG			
#LIST QACCEL.						
> 1	19192.91406		0.75839	1100.00000		0.0
> 2	15501.96875		0.61254	1100.00000		0.0
> 3	7381.89063		0.29169	1100.00000		0.0
> 4	2030.01978		2.24796	305.00000		5.0
> 5	1328.74023		1.10043	305.00000		5.0
> 6	1722.44116		1.42648	305.00000		5.0

> !  
>ATTN!  
\*RUN STAT;\_:MIDAS  
EXECUTION BEGINS

M I D A ' S  
STATISTICAL RESEARCH LABORATORY  
UNIVERSITY OF MICHIGAN  
17:30:46  
APR 5, 1978

COMMAND  
?READ  
FILE CONTAINING DATA OR \* TO ENTER DATA HERE  
=\*\_QACCEL  
FORMAT SPECIFICATION OR \* TO ENTER DATA SEPARATED BY COMMAS  
=4(F15.5,1X)  
VARIABLES TO READ (E.G., 1-10)  
=1-4  
LABELS CORRESPONDING TO THESE VARIABLES OR \* FOR STANDARD LABELS  
=AA,R,U,Q  
CASES TO ASSIGN TO THE DATA BEING READ (E.G., 1-98)  
=1-327

READ OBSERVATIONS 1-327  
VARIABLES BY CASE

327 CASES READ FOR 4 VARIABLES

COMMAND  
?WRITE V=ALL CASES=1-6

FILE TO RECEIVE DATA OR \* TO WRITE DATA HERE  
 \*  
 FORMAT SPECIFICATION OR \* TO LIST DATA WITH HEADINGS  
 \*

WRITE OBSERVATIONS CASES=CASE#:1-6  
 VARIABLES BY CASE

1. AA	2. R	3. U	4. Q
19193.	.75839	1100.0	0.
15502.	.61254	1100.0	0.
7381.9	.29169	1100.0	0.
2030.0	2.2480	305.00	5.0000
1328.7	1.1004	305.00	5.0000
1722.4	1.4265	305.00	5.0000

*Handwritten annotations: A bracket groups the first three rows with '1-2'. A larger bracket groups the last three rows with '3-2'.*

327 CASES WRITTEN FOR 4 VARIABLES

COMMAND  
 DESCRIBE V=AA CASES=ALL

DESCRIPTIVE MEASURES

VARIABLE	N	MINIMUM	MAXIMUM	MEAN	STD DEV
1.AA	327	-7381.8	22146.	6322.2	4641.2

COMMAND  
 DIST V=AA CASES=ALL PROB=NOGRAPH:.25,.5,.75

DISTRIBUTIONAL ANALYSIS

CUMULATIVE DISTRIBUTION OF 1.AA N= 327 OUT OF 327

PROB	QUANTILE
.2500	2399.1
.5000	5659.4
.7500	9596.5

COMMAND

HIST V=AA CASES=ALL OP=HISTZ  
 INTERVAL EXPRESSION -- #INT:(MIN,MAX) (MIN,MAX)/WIDTH #PER/(MIN,MAX)  
 =

HISTOGRAM

MIDPOINT	HISTZ	COUNT FOR 1.AA	(EACH X= 2)
-7381.8	.3	1	+X
-5741.4	0.	0	+
-4101.0	0.	0	+
-2460.6	.3	1	+X
-820.14	.6	2	+X
820.28	15.9	52	+XXXXXXXXXXXXXXXXXXXXXXXXXXXX
2460.7	16.2	53	+XXXXXXXXXXXXXXXXXXXXXXXXXXXX
4101.1	10.7	35	+XXXXXXXXXXXXXXXXXXXX
5741.5	9.5	31	+XXXXXXXXXXXXXXXXXXXX
7381.9	15.0	49	+XXXXXXXXXXXXXXXXXXXX
9022.4	9.5	31	+XXXXXXXXXXXXXXXXXXXX
10663.	7.6	25	+XXXXXXXXXXXX
12303.	6.1	20	+XXXXXXXXXXXX
13944.	2.8	9	+XXXXX
15584.	3.1	10	+XXXXX
17224.	1.5	5	+XXX
18865.	.6	2	+X
20505.	0.	0	+
22146.	.3	1	+X

TOTAL 327 (INTERVAL WIDTH= 1640.4)

COMMAND  
 ?REGRESS V=AA;U CASES=ALL OPTION=MEANZERO

LEAST SQUARES REGRESSION

ANALYSIS OF VARIANCE OF 1.AA N= 327 OUT OF 327

SOURCE	DF	SUM SQRS	MEAN SQR	F-STAT	SIGNIF
REGRESSION	1	.16705+11	.16705+11	1607.8	0.
ERROR	326	.33871+10	.10390 +8		
TOTAL	327	.20092+11			

OPT: MEANZERO R-SQR= .57491 SE= 3223.4

VARIABLE	PARTIAL	COEFF	STD ERROR	T-STAT	SIGNIF
3.U	.91182	8.6755	.21636	40.098	0.

COMMAND

REGRESS V=AA;U CASES=ALL

LEAST SQUARES REGRESSION

ANALYSIS OF VARIANCE OF 1.AA N= 327 OUT OF 327

SOURCE	DF	SUM SQRS	MEAN SQR	F-STAT	SIGNIF
REGRESSION	1	.40371+10	.40371+10	439.55	.0000
ERROR	325	.29851+10	.91848 +7		
TOTAL	326	.70222+10			

MULT R= .75823 R-SQR= .57491 SE= 3030.6

VARIABLE	PARTIAL	COEFF	STD ERROR	T-STAT	SIGNIF
CONSTANT		-3204.5	484.32	-6.6164	.0000
3.U	.75823	12.325	.58787	20.965	.0000

COMMAND





TRANS  
 TRANSFORMATION EXPRESSION (E.G., V9=V2+V5 OR V10=SQRT(V8) )  
 V20=SQRT(AA) LABELS=SRAA

ERROR -- SYNTAX: "V20=SQRT(AA) LABELS=SRAA"  
 ENTER NEW VALUE FOR TRANSFORMATION EXPRESSION (E.G., V9=V2+V5 OR  
 V10=SQRT(V8) )  
 V20=SQRT(AA)  
 LABEL FOR THE RESULT VARIABLE(S)  
 SRAA

SQRT TRANSFORMATION

VARIABLE	TOTAL	VALID	MISS
20.SRAA	327	324	3

COMMAND

WRITE V=S\_ALL CASES=1-6  
 FILE TO RECEIVE DATA OR \* TO WRITE DATA HERE  
 \*  
 FORMAT SPECIFICATION OR \* TO LIST DATA WITH HEADINGS  
 \*

WRITE OBSERVATIONS CASES=CASE#:1-6  
 VARIABLES BY CASE

1. AA	2. R	3. U	4. Q	20. SRAA
19193.	.75839	1100.0	0.	138.54
15502.	.61254	1100.0	0.	124.51
7381.9	.29169	1100.0	0.	85.918
2030.0	2.2480	305.00	5.0000	45.056
1328.7	1.1004	305.00	5.0000	36.452
1722.4	1.4265	305.00	5.0000	41.502

5 CASES WRITTEN FOR 5 VARIABLES

COMMAND

DESCRIBE V=SRAA CASES=ALL

DESCRIPTIVE MEASURES

VARIABLE	N	MINIMUM	MAXIMUM	MEAN	STD DEV
20.SRAA	324	0.	148.81	73.991	30.692

COMMAND

HIST V=SRAA CASES=ALL OP=HISTZ  
 INTERVAL EXPRESSION -- #INT:(MIN,MAX) (MIN,MAX)/WIDTH #PER/(MIN,MAX)  
 =

HISTOGRAM

MIDPOINT	HISTZ	COUNT FOR 20.SRAA (EACH X= 1)
0.	.3	1 +X
8.2675	.6	2 +XX
16.535	3.4	11 +XXXXXXXXXXXX
24.802	4.9	16 +XXXXXXXXXXXXXXXX
33.070	3.4	11 +XXXXXXXXXXXX
41.337	7.7	25 +XXXXXXXXXXXXXXXXXXXXXXXXXXXX
49.605	9.0	29 +XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX
57.872	7.7	25 +XXXXXXXXXXXXXXXXXXXXXXXXXXXX
66.140	6.5	21 +XXXXXXXXXXXXXXXXXXXXXXXX
74.407	9.3	30 +XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX
82.675	8.3	27 +XXXXXXXXXXXXXXXXXXXXXXXXXXXX
90.942	12.0	39 +XX
99.209	8.6	28 +XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX
107.48	7.1	23 +XXXXXXXXXXXXXXXXXXXXXXXXXXXX
115.74	5.2	17 +XXXXXXXXXXXXXXXXXXXX
124.01	3.4	11 +XXXXXXXXXXXX
132.28	1.5	5 +XXXXX
140.55	.6	2 +XX
148.81	.3	1 +X
MISSING		3
TOTAL		327 (INTERVAL WIDTH= 8.2675)

COMMAND  
 ?DIST V=R\_SRAA CASES=ALL PROB=NOGRAPH;.25,.5,.75

DISTRIBUTIONAL ANALYSIS

CUMULATIVE DISTRIBUTION OF 20.SRAA N= 324 OUT OF 327

PROB	QUANTILE
.2500	49.605
.5000	76.847
.7500	97.962

COMMAND  
 ?

REGRESS V=SRAA;U CASES=ALL OP=MEANZERO

LEAST SQUARES REGRESSION

ANALYSIS OF VARIANCE OF 20.SRAA N= 324 OUT OF 327

SOURCE	DF	SUM SQRS	MEAN SQR	F-STAT	SIGNIF
REGRESSION	1	.19801 +7	.19801 +7	6527.6	0.
ERROR	323	97979.	303.34		
TOTAL	324	.20781 +7			

OPT: MEANZERO R-SQR= .68150 SE= 17.417

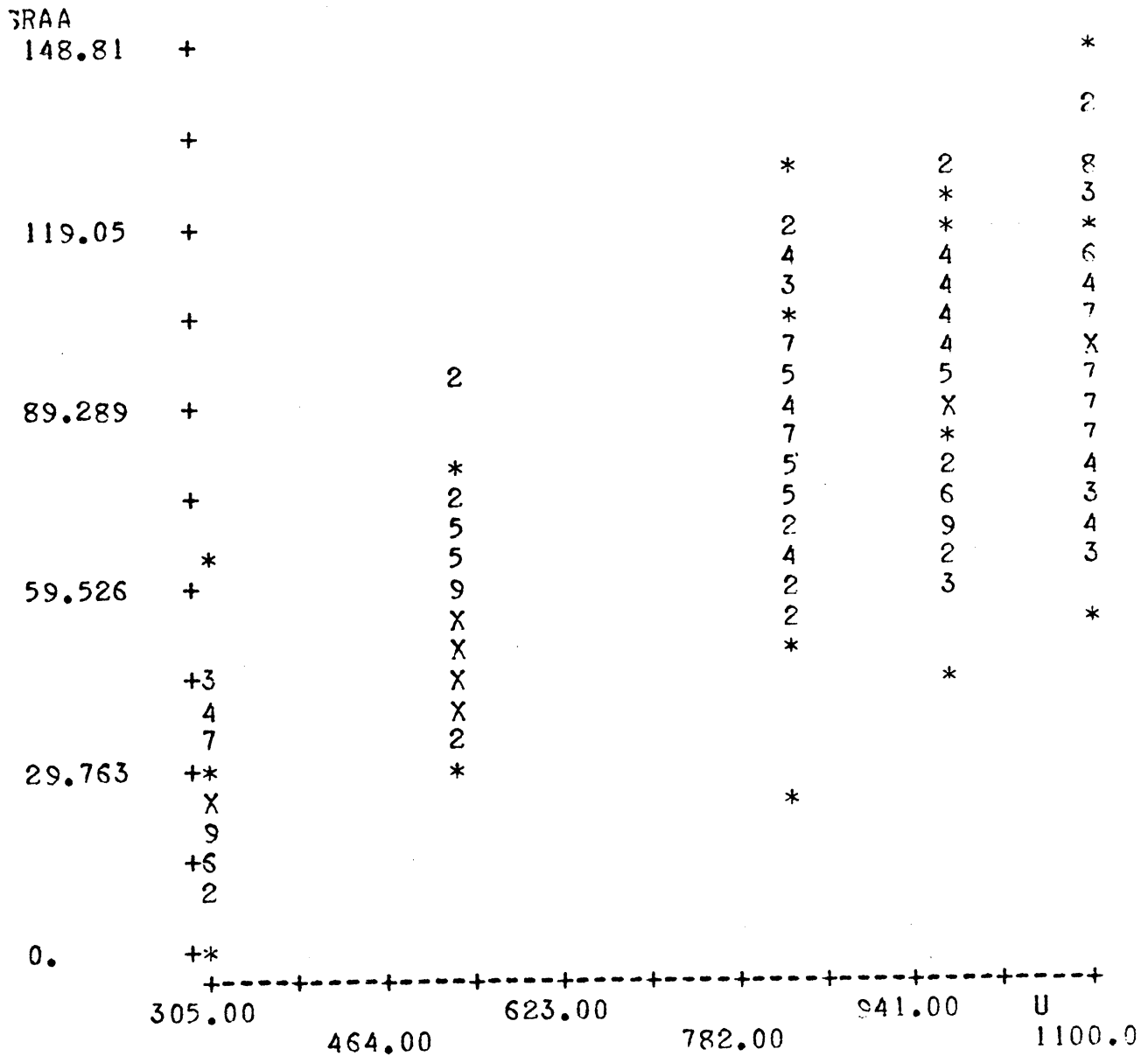
VARIABLE	PARTIAL	COEFF	STD ERROR	T-STAT	SIGNIF
3.U	.97614	.94625 -1	.11712 -2	80.794	0.

COMMAND

?SCATTER V=SRAA;U

SCATTER PLOT

N= 324 OUT OF 327 20.SRAA VS. 3.U



COMMAND

?

HIST V=R\_SRAA CASES=1-3 I=\*

HISTOGRAM CASES=CASE#:1-3

MIDPOINT COUNT FOR 20.SRAA (EACH X= 1)

85.918	1 +X
138.54	2 +XX
TOTAL	3 (INTERVAL WIDTH= 52.621)

COMMAND  
HIST V=SRAA CASES=1-3 PROB=NOGRAPH;.25,.5,.75

DISTRIBUTIONAL ANALYSIS CASES=CASE#:1-3

CUMULATIVE DISTRIBUTION OF 20.SRAA N= 3 OUT OF 3

PROB	QUANTILE
.2500	85.918
.5000	124.51
.7500	138.54

COMMAND  
DESCRIBE V=SRAA CASES=1-3

DESCRIPTIVE MEASURES CASES=CASE#:1-3

VARIABLE	N	MINIMUM	MAXIMUM	MEAN	STD DEV
20.SRAA	3	85.918	138.54	116.32	27.249

COMMAND

REGRESS V=SRAA;U CASES=1-3 OP=MEANZERO

$Q = 0 \text{ cm}^3/\text{min}$

LEAST SQUARES REGRESSION CASES=CASE#:1-3

ANALYSIS OF VARIANCE OF 20.SRAA N= 3 OUT OF 3

SOURCE	DF	SUM SQRS	MEAN SQR	F-STAT	SIGNIF
REGRESSION	1	40592.	40592.	54.670	.0178
ERROR	2	1485.0	742.49		
TOTAL	3	42077.			

OPT: MEANZERO R-SQR= .00000 SE= 27.249

VARIABLE	PARTIAL	COEFF	STD ERROR	T-STAT	SIGNIF
3.U	.98220	.10575	.14302 -1	7.3939	.0178

COMMAND  
?SCATTER V=SRAA;U CASES=1-3

SCATTER PLOT CASES=CASE#:1-3

INVALID INTERVAL FOR 3.U: 1100.0, 1100.0

N= 0 OUT OF 3 20.SRAA VS. 3.U

COMMAND  
?



HIST V=SRAA CASES=4-58 OP=HISTZ I=\*

HISTOGRAM CASES=CASE#:4-58

MIDPOINT HISTZ COUNT FOR 20.SRAA (EACH X= 1)

0.	1.9	1 +X
18.614	14.8	8 +XXXXXXXX
37.229	18.5	10 +XXXXXXXXXX
55.843	14.8	8 +XXXXXXXX
74.458	11.1	6 +XXXXXX
93.072	25.9	14 +XXXXXXXXXXXXXXXX
111.69	7.4	4 +XXXX
130.30	5.6	3 +XXX

MISSING 1  
TOTAL 55 (INTERVAL WIDTH= 18.614)

COMMAND  
?DIST V=SRAA CASES=4-58 PROB=NOGRAPH;.25,.5,.75

DISTRIBUTIONAL ANALYSIS CASES=CASE#:4-58

CUMULATIVE DISTRIBUTION OF 20.SRAA N= 54 OUT OF 55

PROB	QUANTILE
.2500	36.452
.5000	64.677
.7500	94.118

COMMAND  
?



DESCRIBE V-SRAA\_\_\_\_\_ =SRAAA\_ CASES=4-58

DESCRIPTIVE MEASURES CASES=CASE#:4-58

VARIABLE	N	MINIMUM	MAXIMUM	MEAN	STD DEV
20.SRAA	54	0.	130.30	65.850	33.073

COMMAND  
REGRESS V=SRAA;U CASES=AL\_\_4-58 OP=MEANZERO

*Q = 5 cm<sup>3</sup>/min*

LEAST SQUARES REGRESSION CASES=CASE#:4-58

ANALYSIS OF VARIANCE OF 20.SRAA N= 54 OUT OF 55

SOURCE	DF	SUM SQRS	MEAN SQR	F-STAT	SIGNIF
REGRESSION	1	.27783 +6	.27783 +6	1029.8	.0000
ERROR	53	14299.	269.79		
TOTAL	54	.29213 +6			

OPT: MEANZERO R-SQR= .76080 SE= 16.425 ~

*Std Deviation  
is errors  
about regression  
(4d out of 54)*

VARIABLE	PARTIAL	COEFF	STD ERROR	T-STAT	SIGNIF
3.U	.97522	.95737 -1	.29834 -2	32.090	.0000

COMMAND

SCATTER V=SRAA;U CASES=59-130

$\hookrightarrow Q = 10 \text{ (cc/min)}$

SCATTER PLOT CASES=CASE#:59-130

N= 72 OUT OF 72 20.SRAA VS. 3.U

SRAA

124.51 +

(FT/SEC<sup>2</sup>)

+

101.32 +

+

78.141 +

+

54.958 +

+

31.775 +

+3

3

8.5918 +\*

305.00

464.00

623.00

782.00

941.00

U 1100.0

(FT/SEC)

COMMAND

?DESCRIBE V=SRAA CASES=59-130

DESCRIPTIVE MEASURES CASES=CASE#:59-130

VARIABLE	N	MINIMUM	MAXIMUM	MEAN	STD DEV
20.SRAA	72	8.5918	124.51	77.396	30.637

COMMAND

?

HIST V=SRAA CASES=59-130 OP=HISTZ I=\*

HISTOGRAM CASES=CASE#:59-130

MIDPOINT HISTZ COUNT FOR 20.SRAA (EACH X= 1)

8.5918	2.8	2 +XX
23.081	6.9	5 +XXXXX
37.571	4.2	3 +XXX
52.060	18.1	13 +XXXXXXXXXXXXXX
66.549	6.9	5 +XXXXX
81.039	12.5	9 +XXXXXXXXXX
95.528	23.6	17 +XXXXXXXXXXXXXXXXXX
110.02	22.2	16 +XXXXXXXXXXXXXXXXXX
124.51	2.8	2 +XX

TOTAL 72 (INTERVAL WIDTH= 14.489)

COMMAND  
DIST V=SRAA CASES=59-130 PROB=NOGRAPH;.25,.5,.75

DISTRIBUTIONAL ANALYSIS CASES=CASE#:59-130

CUMULATIVE DISTRIBUTION OF 20.SRAA N= 72 OUT OF 72

PROB	QUANTILE
.2500	52.026
.5000	85.918
.7500	101.66

COMMAND

REGRESS V=SRAA;U CASES=59-130 OP=MEANZERO

*Q = 10 <sup>cm<sup>3</sup></sup> / min*

LEAST SQUARES REGRESSION CASES=CASE#:59-130

ANALYSIS OF VARIANCE OF 20.SRAA N= 72 OUT OF 72

SOURCE	DF	SUM SQRS	MEAN SQR	F-STAT	SIGNIF
REGRESSION	1	.48093 +6	.48093 +6	2007.4	.0000
ERROR	71	17010.	239.58		
TOTAL	72	.49794 +6			

OPT: MEANZERO R-SQR= .75104 SE= 15.478

VARIABLE	PARTIAL	COEFF	STD ERROR	T-STAT	SIGNIF
3.U	.98277	.10040	.22408 -2	44.804	.0000

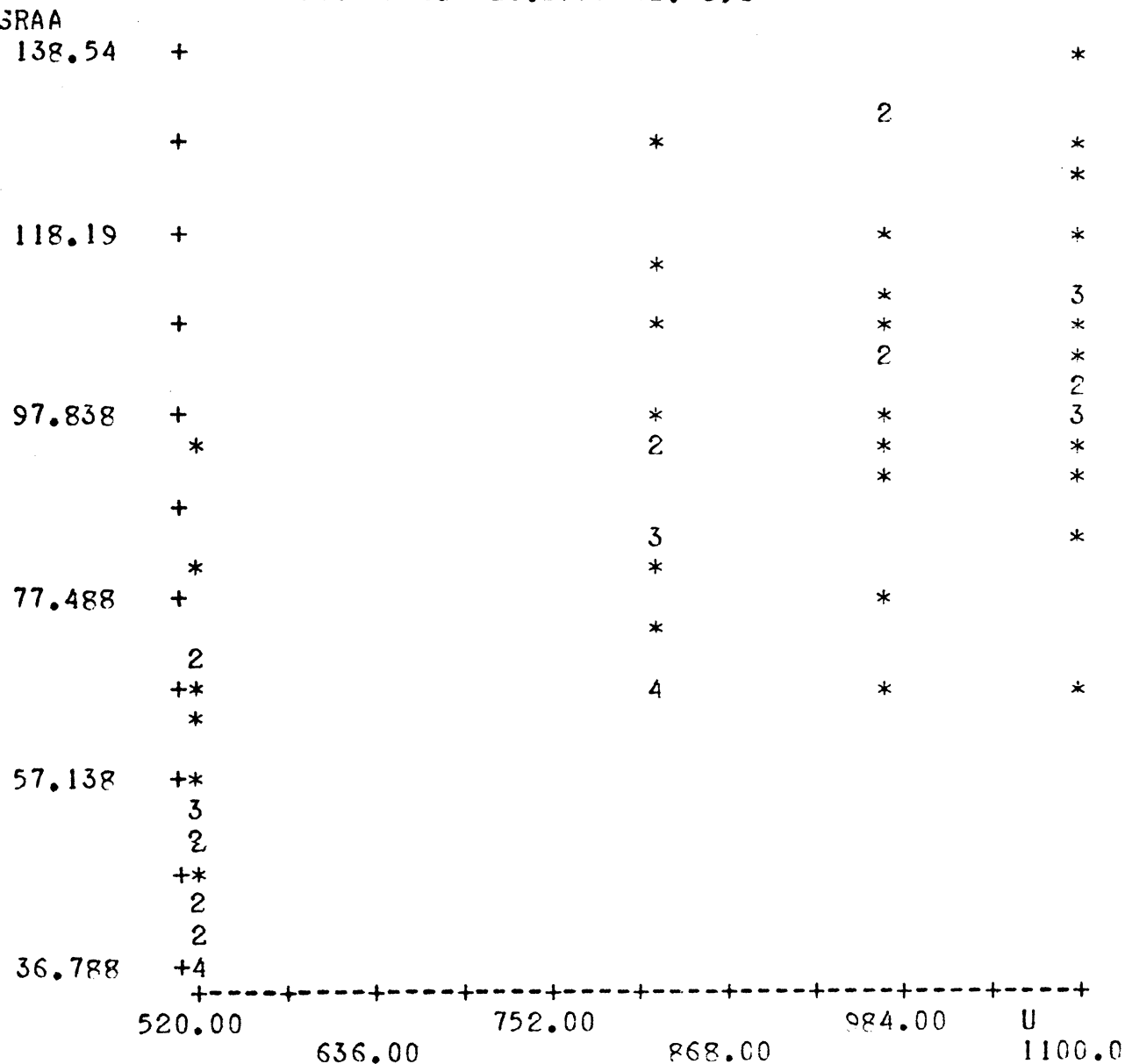
COMMAND

?

SCATTER V=SSR\_\_S\_RAA;U CASES=131-198

Q = 10

SCATTER PLOT CASES=CASE#:131-198  
N= 66 OUT OF 68 20.SRAA VS. 3.U



COMMAND

DESCRIBE V=SRAA CASES=131-198

DESCRIPTIVE MEASURES CASES=CASE#:131-198

VARIABLE	N	MINIMUM	MAXIMUM	MEAN	STD DEV
20.SRAA	66	36.788	138.54	84.547	27.825

COMMAND

RE#  
?HIST V=SRAA CASES=131-198 OP=HISTZ I=\*  $\phi = 15$

HISTOGRAM CASES=CASE#:131-198

MIDPOINT HISTZ COUNT FOR 20.SRAA (EACH X= 1)

36.788	10.6	7 +XXXXXXX
49.507	10.6	7 +XXXXXXX
62.226	13.6	9 +XXXXXXXXXX
74.944	6.1	4 +XXXX
87.663	12.1	8 +XXXXXXXXXX
100.38	22.7	15 +XXXXXXXXXXXXXXXXXX
113.10	15.2	10 +XXXXXXXXXXXX
125.82	7.6	5 +XXXXX
138.54	1.5	1 +X

MISSING 2  
TOTAL 68 (INTERVAL WIDTH= 12.719)

COMMAND  
?DIST V=SRAA CASES=131-198 PROB=NOGRAPH;.25,.5,.75

DISTRIBUTIONAL ANALYSIS CASES=CASE#:131-198

CUMULATIVE DISTRIBUTION OF 20.SRAA N= 66 OUT OF 68

PROB	QUANTILE
.2500	66.552
.5000	85.918
.7500	105.23

COMMAND  
?REGRESS V=SRAA;U CASES=131-198 OP=MEANZERO

LEAST SQUARES REGRESSION CASES=CASE#:131-198

$\phi = 15 \frac{\text{cm}^3}{\text{min}}$

ANALYSIS OF VARIANCE OF 20.SRAA N= 66 OUT OF 68

SOURCE	DF	SUM SQRS	MEAN SQR	F-STAT	SIGNIF
REGRESSION	1	.50215 +6	.50215 +6	1635.1	.0000
ERROR	65	19962.	307.10		
TOTAL	66	.52211 +6			

OPT: MEANZERO R-SQR= .60911 SE= 17.524

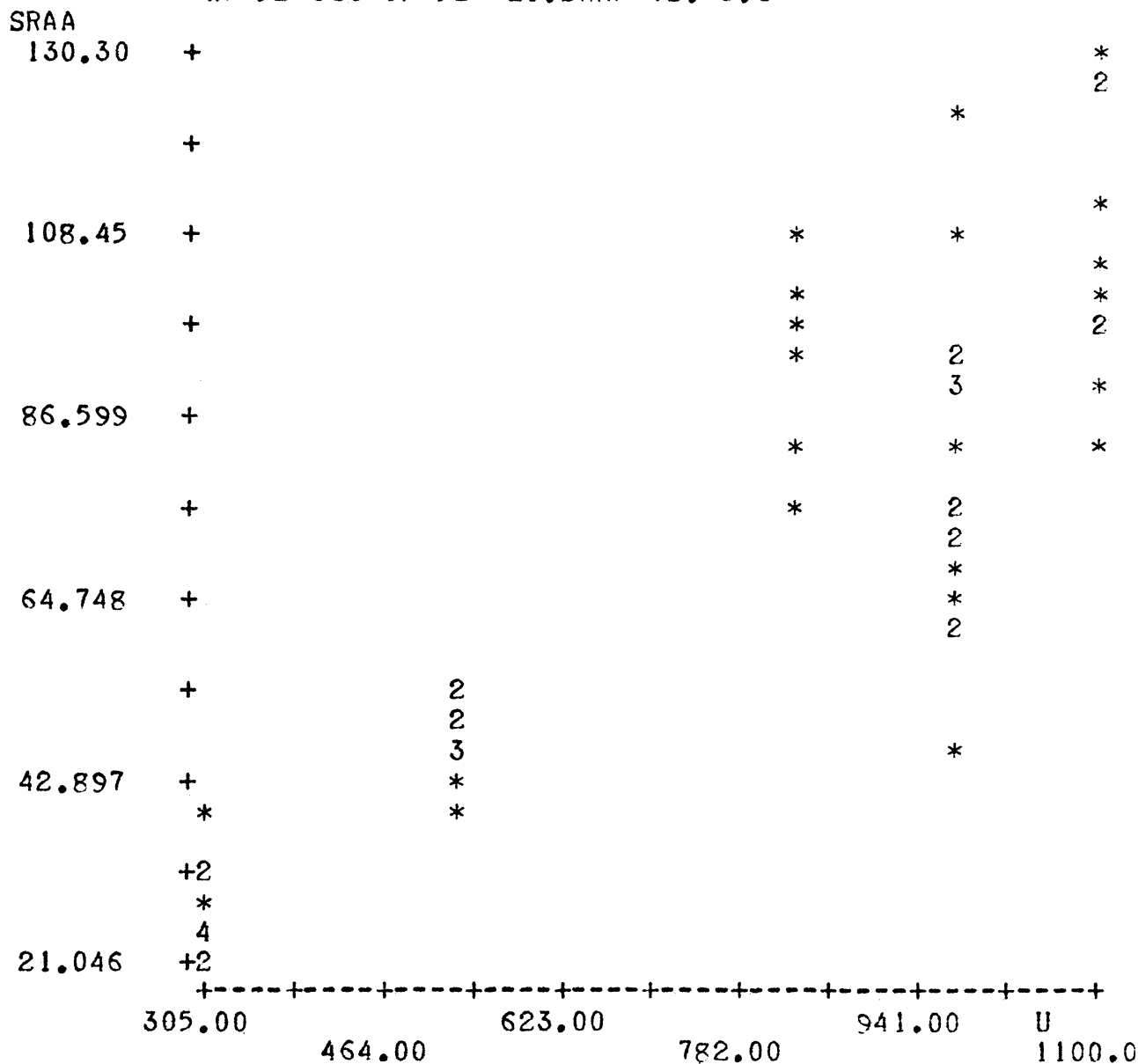
VARIABLE	PARTIAL	COEFF	STD ERROR	T-STAT	SIGNIF
3.U	.98070	.10115	.25016 -2	40.437	.0000

COMMAND

SCATTER V=SRAA CASES=199-250 *Q=20*

ERROR -- WRONG # OF VARS: "SRAA"  
ENTER NEW VALUE FOR VARIABLES -- VERTICAL; HORIZONTAL  
SRAA;U

SCATTER PLOT CASES=CASE#:199-250  
N= 52 OUT OF 52 20.SRAA VS. 3.U



COMMAND  
#  
#  
DESCRIBE V=SRAA CASES=199-250

DESCRIPTIVE MEASURES CASES=CASE#:199-250

VARIABLE	N	MINIMUM	MAXIMUM	MEAN	STD DEV
20.SRAA	52	21.046	130.30	71.219	31.705

COMMAND

?#  
?HIST V=SRAA CASES=199-250 OP=HISTZ I=\*

HISTOGRAM CASES=CASE#:199-250

MIDPOINT HISTZ COUNT FOR 20.SRAA (EACH X= 1)

21.046	13.5	7 +XXXXXXXX
36.653	9.6	5 +XXXXX
52.261	15.4	8 +XXXXXXXXXX
67.869	13.5	7 +XXXXXXXXXX
83.477	17.3	9 +XXXXXXXXXX
99.085	17.3	9 +XXXXXXXXXX
114.69	5.8	3 +XXX
130.30	7.7	4 +XXXX

TOTAL 52 (INTERVAL WIDTH= 15.608)

COMMAND  
?DIST V=SRAA CASES=199-250 PROB=NOGRAPH;.25,.5,.75

DISTRIBUTIONAL ANALYSIS CASES=CASE#:199-250

CUMULATIVE DISTRIBUTION OF 20.SRAA N= 52 OUT OF 52

PROB	QUANTILE
.2500	47.059
.5000	71.884
.7500	94.118

COMMAND  
?



#  
#  
REGRESS V=SRAA;U CASES=199-250 OP=MEANZERO

$\phi = 20 \text{ cm}^3/\text{min}$

LEAST SQUARES REGRESSION CASES=CASE#:199-250

ANALYSIS OF VARIANCE OF 20.SRAA N= 52 OUT OF 52

SOURCE	DF	SUM SQRS	MEAN SQR	F-STAT	SIGNIF
REGRESSION	1	.30189 +6	.30189 +6	1173.1	.0000
ERROR	51	13124.	257.34		
TOTAL	52	.31502 +6			

OPT: MEANZERO R-SQR= .74400 SE= 16.042

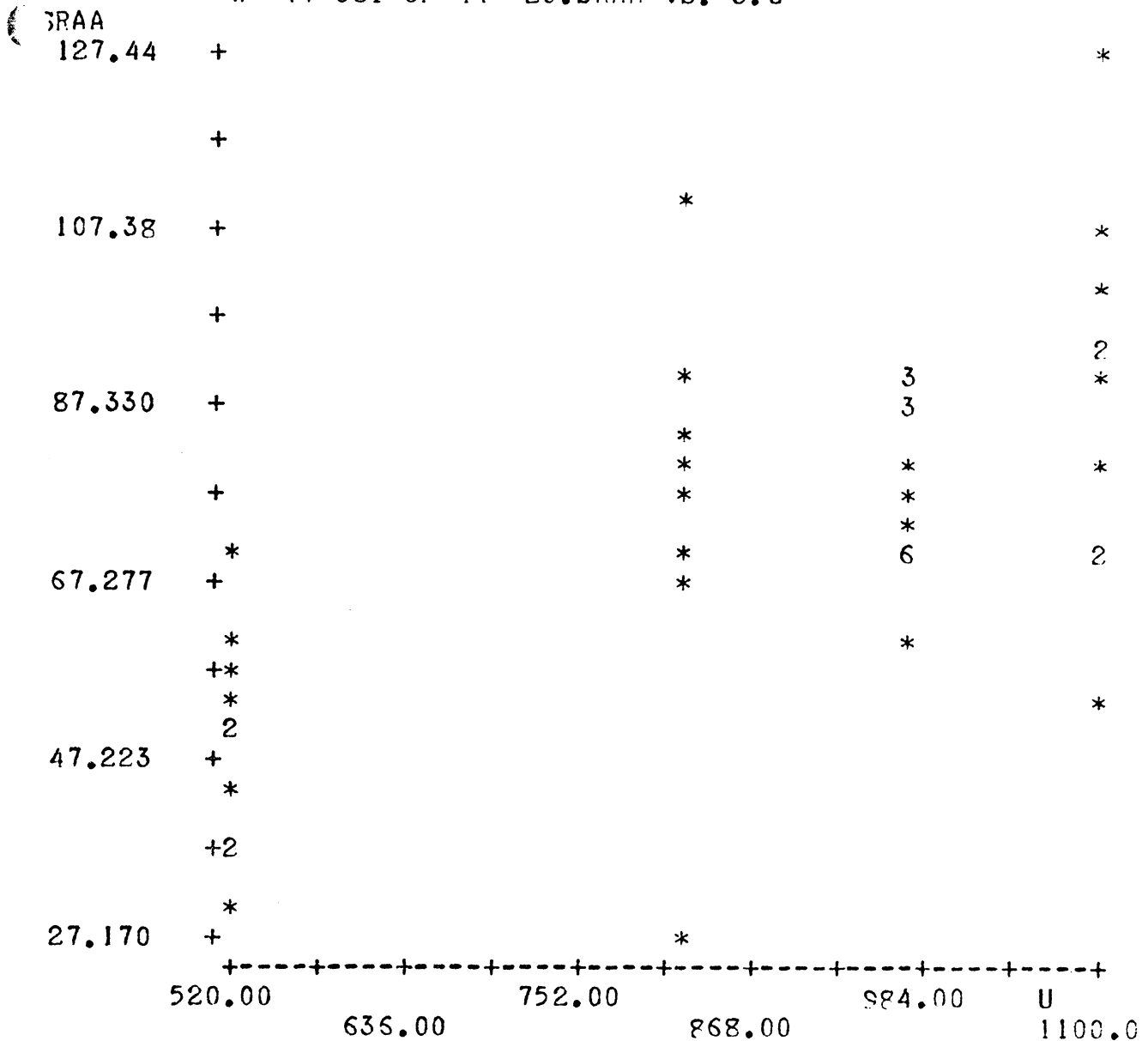
VARIABLE	PARTIAL	COEFF	STD ERROR	T-STAT	SIGNIF
3.U	.97895	.91948 -1	.26845 -2	34.251	.0000

---

COMMAND

?#  
 ?SCATTER V=SRAA CAS\_\_\_\_;U CASES=251-294 9-50

SCATTER PLOT CASES=CASE#:251-294  
 N= 44 OUT OF 44 20.SRAA VS. 3.U



COMMAND  
 ?DESCRIBE V=SRAA CASES=251-294

DESCRIPTIVE MEASURES CASES=CASE#:251-294

VARIABLE	N	MINIMUM	MAXIMUM	MEAN	STD DEV
20.SRAA	44	27.170	127.44	73.952	21.166

COMMAND  
 ?

HIST V=SRAA CASES=251-294 OP=HISTZ I=\*

HISTOGRAM CASES=CASE#:251-294

MIDPOINT HISTZ COUNT FOR 20.SRAA (EACH X= 1)

27.170	4.5	2 +XX
43.881	11.4	5 +XXXXX
60.592	13.6	6 +XXXXXX
77.303	38.6	17 +XXXXXXXXXXXXXXXXXXXX
94.014	25.0	11 +XXXXXXXXXXXX
110.73	4.5	2 +XX
127.44	2.3	1 +X

TOTAL 44 (INTERVAL WIDTH= 16.711)

COMMAND

DIST V=SRAA CASES=\* PROB=NOGRAPH;:\_\*

ERROR -- INVALID CONSTANT: "NOGRAPH;\*"
ENTER NEW VALUE FOR PROBABILITY POINTS
NOGRAPH;.5,.25,.75

DISTRIBUTIONAL ANALYSIS CASES=CASE#:251-294

CUMULATIVE DISTRIBUTION OF 20.SRAA N= 44 OUT OF 44

PROB QUANTILE

.5000 71.884

.2500 60.753

.7500 88.040

COMMAND

#  
?REGRESS V=SRAA;U CASES=251-294 OP=MEANZERO

$Q = 30 \text{ cm}^3/\text{min}$

LEAST SQUARES REGRESSION CASES=CASE#:251-294

ANALYSIS OF VARIANCE OF 20.SRAA N= 44 OUT OF 44

SOURCE	DF	SUM SQRS	MEAN SQR	F-STAT	SIGNIF
REGRESSION	1	.24816 +6	.24816 +6	909.49	.0000
ERROR	43	11733.	272.86		
TOTAL	44	.25989 +6			

OPT: MEANZERO R-SQR= .42784 SE= 16.518

VARIABLE	PARTIAL	COEFF	STD ERROR	T-STAT	SIGNIF
3.U	.97717	.83657 -1	.27740 -2	30.158	.0000

---

COMMAND  
?

SCATTER V=SRAA CASES=295-302

ERROR -- WRONG # OF VARS: "SRAA"  
ENTER NEW VALUE FOR VARIABLES -- VERTICAL; HORIZONTAL  
SRAA, \_;U

SCATTER PLOT CASES=CASE#:295-302

INVALID INTERVAL FOR 3.U: 305.00, 305.00

N= 0 OUT OF 8 20.SRAA VS. 3.U

COMMAND  
DESCRIBE V=SRAA CASES=\*

DESCRIPTIVE MEASURES CASES=CASE#:295-302

VARIABLE	N	MINIMUM	MAXIMUM	MEAN	STD DEV
20.SRAA	8	9.0565	42.959	24.830	11.166

COMMAND  
DIST V=SRAA CASES=\* PROB=NOGRAPH;.25,.5,.75

DISTRIBUTIONAL ANALYSIS CASES=CASE#:295-302

CUMULATIVE DISTRIBUTION OF 20.SRAA N= 8 OUT OF 8

PROB	QUANTILE
.2500	16.384
.5000	22.184
.7500	25.616

COMMAND

#  
?#  
?HIST V=SRAA CASES=\* OP=\* I=\*

HISTOGRAM CASES=CASE#:295-302

MIDPOINT COUNT FOR 20.SRAA (EACH X= 1)

9.0565 2 +XX  
26.008 4 +XXXX  
42.959 2 +XX

TOTAL 8 (INTERVAL WIDTH= 16.951)

---

COMMAND  
?REGRESS V=SRAA;U CASES=\* OP=MEANZERO

$Q = 40 \text{ cm}^3/\text{min}$

LEAST SQUARES REGRESSION CASES=CASE#:295-302

ANALYSIS OF VARIANCE OF 20.SRAA N= 8 OUT OF 8

SOURCE	DF	SUM SQRS	MEAN SQR	F-STAT	SIGNIF
REGRESSION	1	4932.1	4932.1	39.557	.0004
ERROR	7	872.77	124.68		
TOTAL	8	5804.8			

OPT: MEANZERO R-SQR= .00000 SE= 11.166

VARIABLE	PARTIAL	COEFF	STD ERROR	T-STAT	SIGNIF
3.U	.92176	.81409 -1	.12944 -1	6.2895	.0004

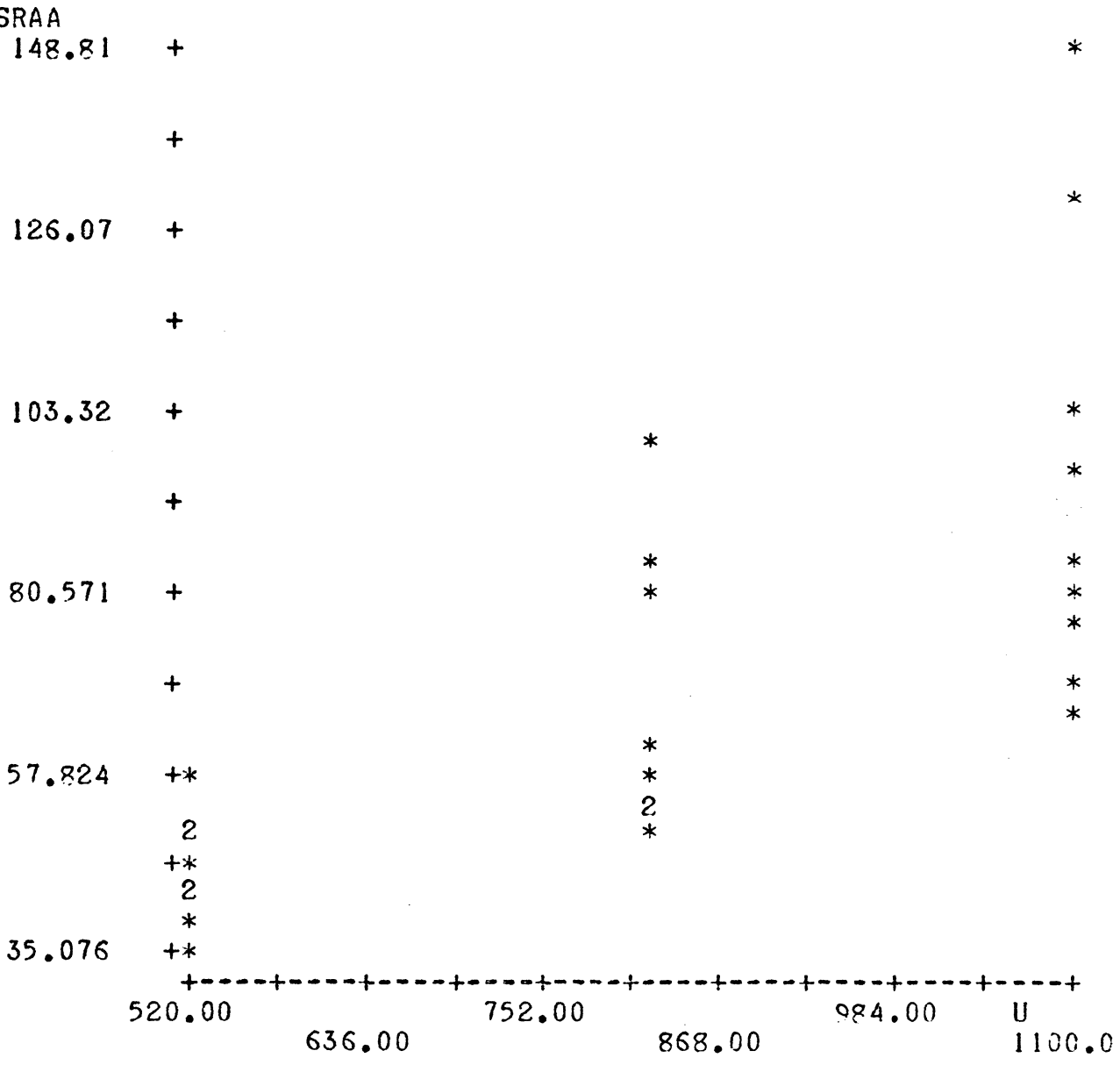
---

COMMAND  
?

SCATTER V=SRAA CASES=303-327 *F=50*

ERROR -- WRONG # OF VARS: "SRAA"  
ENTER NEW VALUE FOR VARIABLES -- VERTICAL; HORIZONTAL  
SRAA;U

SCATTER PLOT CASES=CASE#:303-327  
N= 25 OUT OF 25 20.SRAA VS. 3.U



COMMAND  
DESCRIBE V=SRAA CASES=\*

DESCRIPTIVE MEASURES CASES=CASE#:303-327

VARIABLE	N	MINIMUM	MAXIMUM	MEAN	STD DEV
20.SRAA	25	35.076	148.81	70.386	28.315

COMMAND

DI\_\_HIST V=SRAA CASES=\* OP=HISTZ I=\*\_\_\_ I=\*

HISTOGRAM CASES=CASE#:303-327

MIDPOINT HISTZ COUNT FOR 20.SRAA (EACH X= 1)

35.076	16.0	4 +XXXX
57.824	44.0	11 +XXXXXXXXXXXX
80.571	20.0	5 +XXXXX
103.32	12.0	3 +XXX
126.07	4.0	1 +X
148.81	4.0	1 +X

TOTAL 25 (INTERVAL WIDTH= 22.748)

COMMAND

?DIST V=SRAA CASES=\* PROB=NOGRAPH;.25,.5,.75

DISTRIBUTIONAL ANALYSIS CASES=CASE#:303-327

CUMULATIVE DISTRIBUTION OF 20.SRAA N= 25 OUT OF 25

PROB	QUANTILE
.2500	48.981
.5000	60.753
.7500	83.742

COMMAND

?



REGRESS V=SRAA;U CASES=\* OP=MEANZERO

$Q = 50 \text{ cm}^3/\text{min}$

LEAST SQUARES REGRESSION CASES=CASE#:303-327

ANALYSIS OF VARIANCE OF 20.SRAA N= 25 OUT OF 25

SOURCE	DF	SUM SQRS	MEAN SQR	F-STAT	SIGNIF
REGRESSION	1	.13409 +6	.13409 +6	357.18	.0000
ERROR	24	9009.8	375.41		
TOTAL	25	.14310 +6			

OPT: MEANZERO R-SQR= .53178 SE= 19.375

VARIABLE	PARTIAL	COEFF	STD ERROR	T-STAT	SIGNIF
3.U	.96801	.85139 -1	.45049 -2	18.899	.0000

COMMAND

UNIVERSITY OF MICHIGAN



3 9015 03483 8055