2009-01

ARCH 324 - Structures 2, Winter 2009

von Buelow, Peter

<http://hdl.handle.net/2027.42/64938>
http://hdl.handle.net/2027.42/64938
Unless otherwise noted, the content of this course material is licensed under a Creative Commons Attribution 3.0 License. http://creativecommons.org/licenses/by/3.0/

© 2009, Peter Von Buelow

You assume all responsibility for use and potential liability associated with any use of the material. Material contains copyrighted content, used in accordance with U.S. law. Copyright holders of content included in this material should contact open.michigan@umich.edu with any questions, corrections, or clarifications regarding the use of content. The Regents of the University of Michigan do not license the use of third party content posted to this site unless such a license is specifically granted in connection with particular content. Users of content are responsible for their compliance with applicable law. Mention of specific products in this material solely represents the opinion of the speaker and does not represent an endorsement by the University of Michigan. For more information about how to cite these materials visit https://open.umich.edu/education/about/terms-of-use.

Any medical information in this material is intended to inform and educate and is not a tool for self-diagnosis or a replacement for medical evaluation, advice, diagnosis or treatment by a healthcare professional. You should speak to your physician or make an appointment to be seen if you have questions or concerns about this information or your medical condition. Viewer discretion is advised: Material may contain medical images that may be disturbing to some viewers.
14-2 (i)

Allow f (steel) = 24 ksi  
Allow f (concrete) = 1,350 psi

\[
\frac{f}{f_s} = \frac{E}{E_s} = \frac{1}{q}
\]

Transformed Section

- Determine the Neutral Axis
  - Use top of concrete as base line

\[
x = \frac{\sum A_i x_i}{\sum A} = \frac{(4 \times 8) \times 12 + 11.8 \times 12.005}{(4 \times 8) + 11.8} = 4.695
\]

- Determine \( I_{tr} \)

\[
\begin{align*}
I_{tr} &= \frac{I}{12} = 48.87 \\
A y^2 &= 32 \times 2.695^2 = 232.42 \\
I_y &= 275.09 \\
I &= 518.9 \\
11.8 \times 7.31^2 &= 639.45 \\
1149.55 \\
1423.64 \text{ in}^4
\end{align*}
\]

1) Resisting Moment Capacity

- Steel: \( M = \frac{f_b}{f_{s,Steel}} \cdot \frac{I_{tr}}{C_s} = 24 \text{ ksi} \cdot \frac{48.87}{15.315} = 723.99 \text{ k-ft} = 185.91 \text{ k-ft} \)

- Concrete: \( M = \frac{f_c}{f_{s,Concrete}} \cdot \frac{I_{tr}}{C_n H} = 1.35 \text{ ksi} \cdot \frac{48.87}{4.695 \times \frac{1}{4}} = 3684.18 \text{ k-ft} = 307.01 \text{ k-ft} \)

Steel governs.

\[
M = 185.91 \text{ k-ft}
\]
(2) Safe uniform load on a simple span of 24 ft.

\[ M = \frac{Wl}{8} \]

\[ \therefore \, W = \frac{8M}{l} = \frac{8 \times 185.91 \text{ k-ft}}{24 \text{ ft}} = 61.97 \text{ k} \]

(3) Determine the most economical wide flange steel section needed for the same load, without composite action.

\[ M_{\text{max}} = \frac{Wl}{8} = \frac{61.97 \times 24}{8} = 185.91 \text{ k-ft} \]

\[ S \geq \frac{M_{\text{max}}}{f_{\text{steel}}} = \frac{185.91 \times 12 \text{ in}^2}{24 \text{ k}} = 92.935 \text{ in}^2 \]

From DATA SHEET D-36, choose \[ W21 \times 50 \]