

Anisotropic Thermal Expansion of Tetragonal Zirconia Polycrystals

Tzer-Shin Sheu*.+

Department **of** Materials Science and Engineering, **The** University of Michigan, Ann Arbor, Michigan **48109-2136**

Thermal expansion coefficients $(\alpha_a \text{ and } \alpha_c)$ in two crystallo**graphic axes** *(a* **and c) of the tetragonal phase are measured** at $25^{\circ} - 1200^{\circ}$ C in $ZrO_2 - M_2O_3$ ($\tilde{M} = \tilde{S}c$, In, Yb) and in **Zr0,-YTaO,. The difference between these two thermal** expansion coefficients, $\alpha_c - \alpha_a$, decreases with M₂O₃ or **YTaO₄** composition even though the tetragonality (c/a) behaves differently in these two systems. The locus of $\alpha_c =$ α_a represents a maximum tetragonality for the tetragonal **phase, but not the phase boundary for the cubic phase. The relationships among thermal expansion, temperature, and composition are discussed.**

I. Introduction

IVALENT and trivalent metal oxides such as MgO, CaO, Y_3O_3 , and rare-earth oxides have been found to be the stabilizing agents in zirconia solid solutions.^{1,2} This is because the tetragonal phase *(t)* decreases both its tetragonality *(cia)* and its transformation temperature to the monoclinic phase (m) by adding these oxides to the pure zirconia.^{3.6} Conversely, pentavalent metal oxides such as Ta_2O_5 and Nb_2O_5 act as destabilizers, 6.7 because these oxides increase both the tetragonality and the transformation temperature of $t \rightarrow m$ when they are added to the 2 or 3 mol% Y_2O_3 -tetragonal zirconia polycrystalline material (TZP). Therefore, it is generally believed that the transformation temperature of $t \rightarrow m$ is correlated with tetragonality.

However, the above correlation does not exist in the $ZrO₂$ YTaO₄ system, whose isothermal ternary oxide phase diagram at 1500°C is shown in Fig. I. **A** stable tetragonal phase with a tetragonality larger than that in the pure zirconia has been reported to exist in the composition range $15-25$ mol% YTaO₄ at 25° C.⁷ With composition less than 14.0 mol% YTaO₄, $t \rightarrow m$ transformation temperature decreases with increasing $YTaO_4$ composition. This suppression of $t \rightarrow m$ transformation temperature indicates that $YTaO_4$ oxide is a stabilizing agent. However, there is no strong evidence to prove whether the unquenchable tetragonal phase with $0-14$ mol% YTaO₄ has the same crystal structure as the stable tetragonal phase with 15-25 mol% YTaO₄. In this study, a lattice parameter measurement at high temperature is used to investigate the phase continuity in the composition range $0-25\%$ YTaO₄.

Anisotropic thermal expansion behavior $(\alpha_c \neq \alpha_a)$ has been reported to affect tetragonality *(cia)* for the tetragonal zirconia crystals,⁸⁻¹⁰ where α_a and α_c are thermal expansion coefficients for the crystallographic *a* and *c* axes, respectively. In the $ZrO₂$ Y_2O_3 system, c/a and α_c/α_a are temperature-dependent, and both of them decrease as Y_2O_3 composition increases at temperatures of $25^{\circ} - 800^{\circ}$ C.⁸ In the pure zirconia, c/a first increases and then decreases as temperature increases from $\sim 1100^{\circ}$ C up to \sim 2370°C.⁹ This reverse *c/a* behavior also exists in the *t*

Fig. 1. Part of the ternary phase diagram for the system $ZrO_2-Y_2O_3$ Ta, O_5 at 1500°C. Tss is t-ZrO₂ solid solution, Css is c-ZrO₂ solid solution, TZ is $Ta_2Zr_6O_{17}$, YT is YTaO₄, YT₃ is YTa₃O₉ (Ref. 7).

phase,"' which is the product of the diffusionless phase transformation from the cubic phase to the tetragonal phase. The maximum c/a is shifted to a lower temperature as \dot{Y}_2O_3 composition increases. Based on these temperature- and compositiondependent tetragonality curves in the $ZrO₂-Y₂O₃$ system, the anisotropic thermal expansion of the tetragonal phase will be discussed in this study. In the $ZrO₂-YTaO₄$ system, the tetragonal phase shows some interesting phenomena for its tetragonality and its $t \rightarrow m$ transformation temperature. Its anisotropic thermal expansions will be measured to compare with those in the ZrO ₇-M₂O₃ (M = Y, Yb, In, Sc) systems.

11. Experimental Procedure

Different compositions of tetragonal zirconia polycrystalline materials were produced by making fine powder, sintering, and heat-treating. Fine powder was prepared from precursor metal hydroxide using a coprecipitation method. Starting materials were 99.9% pure M,O, **(M** = Y, Yb, In, Sc), 99.9% pure Ta₂O₅, and 93.1% pure $ZrOCl₂–8H₂O$ (the remaining balance is H_2O). M_2O_3 and Ta_2O_5 were dissolved in hot acid (HCl or HNO₃), and $ZrOCl₂-8H₂O$ was dissolved in distilled water. Two solutions, containing M^{+3} (or Ta⁺⁵) plus Zr^{+4} and NH₄OH (10 wt%), were added simultaneously and mixed together to let a gellike metal hydroxide precipitate out by controlling the pH value above 9. Precipitate was separated by filtration and was washed with water to eliminate chlorine ions. Then it was dried in an oven at 80°C. Dried precipitates were calcined in an air oven for 2 h at 650°C. Pellets were formed under a uniaxial pressure and were then isostatically pressed at 340 MPa. Subsequently, green pellets were sintered and heat-treated in air in a furnace with $MoSi₂$ heating elements.

D. B. Marshall-contributing editor

Manuscript No. 195164. Received March 26, 1992;approved March 29, **1003.**

^{&#}x27;Member, American Ceramic Society. 'Current address: Department of Biologic and Materials Science, School of Den tistry, University *of* Michigan, Ann Arhor, MI.

For the lattice parameter measurement, samples in either a sintered powder or pellet form were used. Diffraction patterns of these samples were obtained using a high-temperature X-ray diffractometer (Geigerflex, Rigaku, Tokyo, Japan). An Al₂O₃ plate was used as a sample holder and as an internal standard to calculate the lattice parameters. The reference diffraction peaks of Al_2O_3 were calibrated by pure Pt powder. The lattice constants of pure Pt metal at different temperatures were calculated from the thermal expansion data published by the National Bureau of Standards¹² and from the Pt lattice constant at room temperature shown in JCPDS card number 4-802. Transformation temperatures between the tetragonal and the monoclinic phases were measured by a dilatometer unit. The operating temperature range was 25° -1300°C; heating and cooling rates were 10°C/min.

111. Results

(1) Phase Continuity in the Composition Range 625 mol% YTaO,

A sample with 13.0 mol% $YTaO_4$ contains both the tetragonal phase and monoclinic phase at room temperature. Its phase evolution at high temperatures is shown in Fig. 2. The characteristic monoclinic and tetragonal peaks $(111)_m$, $(111)_m$, $(111)_i$, **(004),,** and **(400),** are used to identify these two phases. **At** 600" and 900°C, the tetragonal phase and the monoclinic phase coexist. **At** 1200"C, only the tetragonal phase exists. This phase evolution indicates that the monoclinic phase at low temperatures is progressively transformed into the tetragonal phase at high temperatures. The same phase evolution is also found in the samples with composition less than 13.0 mol% YTaO,. The diffraction peaks in Fig. 2 shift to the low 2θ angle as the temperature increases, due to the larger lattice constants at high temperatures.

At 1200"C, only the tetragonal phase is present in the composition range $0-25$ mol% YTaO₄. Its lattice constants versus composition are shown in Fig. 3. Both lattice constants **c** and *a* are linearly dependent on composition. Figure 3 also shows the relationships between lattice constants and composition at 25°C. Lattice constants for samples with composition less than 14.0 mol% $YTaO_4$ are obtained from data at high temperatures by using an extrapolation method, because the tetragonal phase is unstable at room temperature. **A** linear regression method indicates that pure tetragonal zirconia has lattice constants $a =$

Fig. 2. X-ray diffraction patterns of a 13.0 mol% YTaO, sample at three different temperatures.

Fig. 3. Lattice parameters at 25° and 1200°C. Open symbols are for lattice constant *a* and closed symbols are for lattice constant *c.*

5.0887 Å and $c = 5.1849$ Å at 25°C, which is consistent with previous data.3.4 Based on the above lattice constant continuities at 1200°C and at room temperature, it is suggested that only one tetragonal phase exists in the composition range 0-25 mol% YTaO,.

(2) Tetragonality and Anisotropic Thermal Expansion Coefficients

Tetragonality (c/a) in the ZrO₂-YTaO₄ and ZrO₂-M₂O₃ systems at 1200" and 25°C is presented in Fig. 4. **As** YTaO, or MO, composition increases, tetragonality increases in the $ZrO₂-YTaO₄$ system but it decreases in the $ZrO₂-M₂O₃$ system. The slope of tetragonality versus composition, as indicated under each curve, is smaller at 1200°C than at 25°C in both cases. The $t \rightarrow m$ transformation temperature in these two cases, measured by the dilatometric method, is suppressed as $MO_{1.5}$ or YTaO₄ composition increases. It implies that the $t \rightarrow m$ transformation temperature in the $ZrO₂-YTaO₄$ system decreases with increasing tetragonality, but it is reversed in the $ZrO₂-M₂O₃$.

Thermal expansion coefficients of the tetragonal phase versus its lattice constants are given in Fig. *5.* The ordinate and the abscissa represent the average thermal expansion coefficients $(\alpha_a \text{ or } \alpha_c)$ in the two different crystallographic axes *(c or <i>u)* at temperatures 900"-1200"C and the lattice constants *(c* or *a)* at

Fig. 4. Tetragonality in the $ZrO₂-YTaO₄$ and $ZrO₂-MO_{1.5}$. Open symbols are for temperature at 1200°C and full symbols are for temperature at 25°C. Data under each curve is the slope of tetragonality versus composition.

Fig. 5. Relationships between thermal expansion Coefficient *(a,* or α_{μ}) and lattice constant (*a* or *c*). Arrows indicate data for pure ZrO₂.

1200°C, respectively. In $ZrO_2-M_2O_3$, α_a and α_c increase with increasing lattice constants. It is reversed in the $ZrO₂-YTaO₄$ system. For the crystallographic *a* direction, pure zirconia has the highest thermal expansion coefficient in $ZrO₂-YTaO₄$ but not in $ZrO₂-M₂O₃$. For the crystallographic *c* direction, pure zirconia has the highest thermal expansion coefficient in both systems. The anisotropic thermal expansion coefficient ratio $(\alpha_{\rm r}/\alpha_{\rm q})$ versus composition is shown in Fig. 6. $\alpha_{\rm r}/\alpha_{\rm q}$ decreases with increasing $MO_{1.5}$ or YTaO₄ composition. Schubert's data at 25°-800°C for the $ZrO₂-Y₂O₃$ system⁸ is close to $ZrO₂$ - $Yb₂O₃$ in this study.

IV. Discussion

(I) Thermal Expansion in ZrO,-Y,O,

Alderbert and Traverse' and Sheu *et al."'* have reported on the tetragonal phase $(t \text{ or } t')$ containing a temperature-dependent tetragonality, which first increases to a maximum and then decreases as temperature increases. Fundamentally, the *t* and *t'* phases are the same tetragonal polymorph in the zirconia solid

Fig. 6. Thermal expansion coefficient ratio (α_r/α_a) versus composition in the temperature range 900° -1200°C. Data for $ZrO₂-YO_{1.5}$ are taken from Ref. 8.

solutions.¹⁰ Based on these previous data, the thermal expansion behavior of the tetragonal phase in the $ZrO₂-Y₂O₃$ system is discussed as follows.

There are two critical temperatures for each composition in this temperature-dependent tetragonality curve. One is at T_c , the transformation temperature of the cubic phase (c) to the tetragonal phase $(t$ or t^7). At T_c , the tetragonal phase shows a tetragonality anomaly, which decreases from $c/a \neq 1$ to $c/a =$ $1.^{9,10}$ This T_c temperature has been measured for the pure zirconia and the sample with 13.5 mol% $\text{YO}_{1.5}$. The other critical temperature is at T_a which has a maximum tetragonality $(c/a)_{\text{max}}$. At T_a , this temperature-dependent tetragonality $(c/a = f(T))$ has the following relationships: $f'(T) = 0$, and $f''(T) < 0$. Alternatively, $f'(T) = 0$ can be expressed as $\partial f(T)/\partial T = \partial (c/a)/\partial T = 0$. From $\partial (c/a)/\partial T = 0$, we obtain $(\partial c/\partial T) \times a - (\partial a/\partial T) \times c = 0$. Subsequently, $(\partial c/\partial T)/c =$ $(\partial a/\partial T)/a$, i.e., $\alpha_c = \alpha_a$, is obtained at T_a . This derivation indicates that the tetragonal phase has the same thermal expansion coefficients in the crystallographic *a* and c directions when its tetragonality reaches a peak maximum, $(c/a)_{\text{max}}$

Based on Alderbert's and Sheu's experimental data, 9.10 a $ZrO₂-Y₂O₃$ phase diagram containing $(c/a)_{max}$, $\alpha_c = \alpha_a$, $c/a =$ 1, T_{μ} , and T_{ν} is shown in Fig. 7. Several published phase boundaries of the tetragonal and cubic phases¹³⁻¹⁶ are also included. Symbols " $*$ " are used to represent T_c temperatures. There are three data points for $c/a = 1$, at 25° , 600°, and 1200°C, respectively.¹⁰ This $c/a = 1$ curve at high temperatures is close to one of the cubic phase boundaries.¹⁶ Compared with the $c/a = 1$ curve, the $\alpha_c = \alpha_a$ or $(c/a)_{\text{max}}$ curve is very far from the cubic phase boundary. This locus of $\alpha_c = \alpha_a$ represents only a maximum tetragonality for the tetragonal phase, but not the phase boundary for the cubic phase. This is why the data point of $\alpha_c = \alpha_d$ does not match the cubic phase boundary in Schubert **'s** paper.

(2) Thermal Expansion in $ZrO₂-M₂O₃$ *and* $ZrO₂-YTaO₄$

By introducing the lattice constants from a linear regression method and the lattice constants of pure zirconia' at 25°C in $ZrO₂-M₂O₃$ and $ZrO₂-YTaO₄$, the average thermal expansion coefficients $(\alpha_c \text{ or } \alpha_a)$ of the tetragonal phase at 25°-1200°C versus its composition are shown in Fig. 8. For α_c , it decreases with increasing $MO_{1.5}$ or YTaO₄ composition. For α_a , it increases with increasing $MO_{1.5}$ composition (except for $ScO_{1.5}$) but decreases with increasing $YTaO₄$. Although thermal expansion coefficients $(\alpha_c \text{ and } \alpha_a)$ versus composition behave differently, the thermal expansion coefficient difference $\Delta \alpha$ (= α_c –

Fig. 7. Diagram showing the relationships among $\alpha_n/\alpha_n = 1$. $(c/a)_{\text{max}}$, and $c = a$. Tss is *t*-ZrO, solid solution, Css is c -ZrO, solid solution, T is temperature. Symbols "*" are for temperatures T_{α} .

Fig. 8. Average thermal expansion coefficient at 25°-1200°C. Open symbols are for α_c and closed symbols are for α_a .

 α_a) versus composition in these two systems shows the same trend, that is, it decreases with $MO_{1.5}$ or $YTaO_4$ composition. Compared with $ZrO_2-Sc_2O_3$ and $ZrO_2-Yb_2O_3$, $ZrO_2-In_2O_3$ and $ZrO₂-YTaO₄$ show a smaller change of $\Delta\alpha$ versus composition.

The relationships among the thermal expansion coefficient, the lattice constant, and composition in $ZrO₇-YTaO₄$ and $ZrO₇ M₂O₃$ are discussed as follows. For the thermal expansion coefficient $(\alpha_a$ or $\alpha_c)$ versus lattice constant *(a or c)* shown in Fig. 5, $(\partial \alpha_c/\partial c)$ > 0 and $(\partial \alpha_a/\partial a)$ > 0 in ZrO₂-M₂O₃, and $(\partial \alpha_c/\partial c)$ < 0 and $(\partial \alpha_a/\partial a)$ < 0 in ZrO₂-YTaO₄. For the lattice constant (c or *a)* versus composition (X) shown in Refs. 3 and 10 and in Fig. 3, $\partial c/\partial X < 0$ (except for M = Nd, when $\partial c/\partial X > 0$)³ and $\partial a/\partial X > 0$ (except for M = Sc, when $\partial a/\partial X \le 0$)¹⁰ in ZrO₇- M_2O_3 , and $\partial c/\partial X > 0$ and $\partial a/\partial X > 0$ in ZrO_2-YTaO_4 . From the above two relationships, it can be inferred that for the thermal expansion coefficient $(\alpha_a \text{ or } \alpha_c)$ versus composition (X), $(\partial \alpha_c/\partial X) < 0$ and $(\partial \alpha_a/\partial X) > 0$ in ZrO₂–M₂O₃ (except for M = Nd, Sc), and $(\partial \alpha_c/\partial X) < 0$ and $(\partial \alpha_a/\partial X) < 0$ in ZrO₂-YTaO₄. **A** schematic diagram to represent these relationships is given in Fig. 9. There exists $c = a$ in $ZrO_2-M_2O_3$, but not in ZrO_2 -YTaO₄. $\alpha_c/\alpha_a = 1$ is present in both systems. By extrapolating data to $\alpha_c/\alpha_a = 1$ in Fig. 6, the locus of $\alpha_c = \alpha_a$ at 900°-1200°C in $\overline{Z}IO_2-M_2O_3$ is approximately at 6 mol% ScO_{1.5}, 7 mol% YbO_{1.5}, and 9 mol% InO_{1.5}, respectively. This $\alpha_c/\alpha_a = 1$ is far from the cubic phase boundary in $ZrO₂-M₂O₃$. In $ZrO₂-$ YTaO₄, the locus of $\alpha_c = \alpha_a$ is approximately at 25 mol% $YTaO₄$ at 900°–1200°C, even though the cubic phase does not exist in this system. This locus of $\alpha_c = \alpha_a$ is close to the tetragonal phase boundary at $900^{\circ} - 1200^{\circ}C$ in $ZrO_2 - YTaO_4$. data to $\alpha_c/\alpha_u = 1$ in Fig. 6, the locus of $\alpha_c = \alpha_u$ at 900°-

1200°C in ZrO₂-M₂O₃ is approximately at 6 mol% ScO_{1.5}, 7

mol% YbO_{1.5}, and 9 mol% InO_{1.5}, respectively. This $\alpha_c/\alpha_u = 1$

is far from the cubic p

Fig. 9. Relationships among lattice constant, thermal expansion, and composition in the (a) $ZrO_2-M_2O_3$ and (b) ZrO_2-YTaO_4 systems.

Tetragonality is related to the magnitude of oxygen sheartype shifting in $[001]$ $\{110\}$.¹⁷ This oxygen shifting produces two different Zr-0 bonds, four short ones and four long ones, for each Zr atom. In pure zirconia, Alderbert and Traverse' have found that the long Zr-0 bond has a higher thermal expansion coefficient up to a certain temperature, and then it is reversed because this long Zr-0 bond becomes unstable. This phenomenon causes the presence of $(c/a)_{\text{max}}$ or $\alpha_c = \alpha_a$ in the curve of tetragonality versus temperature. The presence of $\alpha_c = \alpha_a$ in the $ZrO_2-M_2O_3$ and ZrO_2-YTaO_4 systems suggests that the bond length change due to the effect of temperature in these two systems behaves like that in pure zirconia. However, why the thermal expansion coefficients of the tetragonal phase decrease with increasing lattice constants in the $ZrO₂-YTaO₄$ system is not fully understood.

(3) Thermal Stresses

In the tetragonal zirconia polycrystals, partially stabilized zirconia, and zirconia-toughened ceramic materials, $^{11,18-20}$ the thermal stresses from different kinds of mismatch (volume, expansion. etc.) have been shown to affect the transformability of tetragonal grains (or particles) in these materials. In the classical nucleation theory, the thermal stresses have accounted for the stress- induced transformation from the tetragonal *(t)* to the monoclinic (*m*) phase.^{21,22} The anisotropic thermal expansion causes thermal stresses among differently orientated grains in the tetragonal zirconia polycrystals. Some grains are locally subjected to high thermal stresses. With increasing grain size, these thermal stresses are further increased up to the critical stresses to trigger the $t \to m$ transformation. In $ZrO_2-M_2O_3$ and $ZrO₂$ -YTaO₄, the anisotropic thermal expansion coefficient difference $(\Delta \alpha = \alpha_c - \alpha_a)$ in the two crystallographic axes of the tetragonal phase decreases with $MO_{1.5}$ or YTaO₄ content. Lower thermal stresses are expected to exist in the tetragonal polycrystals with a higher MO_{1.5} or YTaO₄ content. As a result, the $t \rightarrow$ *m* transformation is more difficult to trigger by these thermal stresses.

Anisotropic thermal expansion is also temperature-dependent. A transition temperature T_a has been shown in Fig. 7. When $T < T_a$, then $\alpha_c > \alpha_a$, when $T > T_a$, then $\alpha_c < \alpha_a$. This reverse anisotropic thermal expansion behavior changes the magnitude of thermal stresses for the tetragonal zirconia polycrystals. For example, with the same grain size, tetragonal polycrystalline material being heat-treated above *T,* and then quenched to the ambient temperature has lower thermal stresses than the sample being heat-treated at T_a . This is because the thermal stresses arising from cooling from T_a to the ambient temperature are relaxed by the reverse type of stresses arising from the heat-treating temperature T to T_a . Because of this characteristic curve of α_c/α_a versus temperature, a post-heat treatment just below temperature T_a for a long period of time is suggested to improve the transformability of the tetragonal polycrystals.

V. Conclusions

From the lattice parameter measurements at high tem-(I) peratures, a single tetragonal phase is determined to exist from $0-25$ mol% YTaO₄ in the ZrO₂-YTaO₄ system. Its tetragonality *(cla)* is larger than that in pure zirconia and increases with increasing $YTaO₄$ composition. However, with composition higher than 15 mol% YTaO₄, this tetragonal phase is stable at room temperature.

(2) Anisotropic thermal expansion coefficients of the tetragonal phase are measured at $25^{\circ}-1200^{\circ}$ C in $ZrO_2-M_2O_3$ and $ZrO₂-YTaO₄$. Thermal expansion coefficients, α_c and α_a , vary with M_2O_3 or YTaO₄ composition. However, the ratio and the difference of these two thermal expansion coefficients, α_c/α_a and $\alpha_c - \alpha_a$, decrease with increasing M₂O₃ or YTaO₄ composition, respectively.

From the relationships among thermal expansion, tem-(3) perature, and composition, the locus of $\alpha_c = \alpha_a$ exists in both $ZrO₂-M₂O₃$ and $ZrO₂-YTaO₄$. This locus of $\alpha_r = \alpha_a$ indicates a maximum tetragonality $((c/a)_{max})$ for the tetragonal phase, but not the phase boundary for the cubic phase.

References

'M. Marezio, "Refinement of the Crystal Structure of In,O, at Two Wavelengths," *Acta Crystallogr.*, **20,** 723-28 (1966).

 ${}^{2}D$. K. Hohnke, "Ionic Conductivity of Z_{r_1-2} , In₂, O₂, *a*," *J. Phys. Chem. Solih,* **41,** 777-84 (1980).

'M. Yoshimura, "Phase Stability of Zirconia," *Am. Ceram. Soc. Bull.*, **67** [I21 1950-55 (1988).

"J. Lefevre, "Fluorite-Type Structural Phase Modification in Systems Having a Zirconium or Hafnium Oxide Base," *Ann. Chim. (Paris)* (in Fr.) **8** [1-21 117-

49 (1963); or translated by A. L. Monka, Report No. ORNL-TR-201.
⁵R. R. Lee, and A. H. Heuer, "Morphology of Tetragonal ZrO₂ in a Ternary (Mg, Y)-PSZ, J. Am. Ceram. Soc., 70 [4] 208-13 (1987).
(Mg, Y)-PSZ, J. *Xim*, "

formability of Y,O,-Stdbilized Tetragonal ZrO,," *J. Am. Cernm. Soc.,* **73** [I] I 15-20 (1990).

'D. J. Kim, and T. *Y.* Tien, "Phase Stability and Physical Properties of Cubic and Tetragonal ZrO_2 in the System $ZrO_2-Y_2O_3-Ta_2O_5$, $'J.$ *Am. Ceram. Soc.*, **74** [12]3061-65 **(1991).**

⁸H. Schubert, "Anisotropic Thermal Expansion Coefficients of Y_1O_3 -Stabilized Tetragonal Zirconia," J. Am. Ceram. Soc., 69 [3] 270-71 (1986).
⁹P. Alderbert, and J. P. Traverse, "Structure and Ionic Mobility of Zirc

mation in Zirconia-Containing Systems," *J. Am. Ceram. Soc.*, 75 [5] 1108-16

(1992). **"A.** H. Heuer, and M. Ruhle. "On the Nucleation of the Martensitic Tranaformation in Zirconia (ZrO₂)," Acta Metall., **33** [12] 2101-12 (1985).

IT. **A,** Hahn, and R. K. Kirby, "Thermal Expansion of Platinum from 293 to **1900°K."** Institute *of* Materials Research, National Bureau *of* Standards, Washington, **DC,** 1971.

^{[9}H. G. Scott, "Phase Relations in the Zirconia-Yttria System," *J. Mater*, *Sci.,* **10[9]** 1527-35 (1975).

¹⁴A. H. Heuer, and M. Ruhle, "Phase Transformations in ZrO₂-Containing **I, The Instability of** c **-ZrO₂** and the Resulting Diffusion-Controlled Reactions"; pp. 1-13 in Advances in Ceramics, Vol. 12, *Science and Technology cfZirt'onin /I.* Edited by N. Claussen. M. Ruhls, and A. H. Heuer. Amencan Ceramic Society, Columbus, OH, 1984.

"E E Lange, "Transformation Toughening: Thermodynamic Approach to the Phase Retention and Toughening"; pp. 255-74 in *Fracture Mechanics of Ceramics,* Vol. 6. Edited by R. C. Bradt, A. *G.* Evans, D. **I? H.** Hasselmann, and F. F. Lange. Plenum Press, New York, 1983.

'"V. *S.* Stubican, G. **S.** Corman, **J.** R. Hellmann, and *G.* Senft, "Phase Relationship in Some ZrO₂ Systems"; see Ref. 12, pp. 96-106.

"G. Teufer, "The Crystal Structure of Tetragondl ZrO,," *Acra Crystallogr..* **15,** 1137 (1962).

¹⁸R. C. Garvie and M. V. Swain, "Thermodynamics of the Tetragonal-to-Monoclinic Phase Transformation in Constrained Zirconia Microcrystals ," *J. Mum-. Sci.,* **20,** 1193-200 (1985).

"S. Schniauder. W. Mader, and M. Ruhle, "Calculations of Strain Distributions in and **around** ZIO, Inclusions"; see Ref. 14, **pp.** 251-55.

²⁰A. H. Heuer, M. Ruhle, and D. B. Marshall, "On the Thermoelastic Martensjtic Transformation in Tetragonal Zirconia," *I. Am. Ceram. Soc.,* **73** [4] 1084-93 (1990).

"I-W. Chen and **Y.** H. Chiao, "Martensitic Nucleation in *ZtO,,"Acta Metull.,* **31** [I01 1627-38 (1983).

'Y. H. Chiao, "Nucleation and Growth Processes of Martensitic Transformation in ZrO₂ Particles"; Ph.D. Thesis. Massachusetts Institute of Technology, Cambridge, MA, Sept. 1986.