ENGINEERING RESEARCH INSTITUTE

UNIVERSITY OF MICHIGAN, ANN ARBOR

A VARIATIONAL METHOD FOR THE CALCULATION OF THE

DISTRIBUTION OF ENERGY REFLECTED FROM A

PERIODIC SURFACE

William C. Meecham

November 1955

A VARIATIONAL METHOD FOR THE CALCULATION OF THE

DISTRIBUTION OF ENERGY REFLECTED FROM A PERIODIC

SURFACE

W.C. Meecham

ABSTRACT

A variational method is presented which is used to calculate the energy appearing in the various diffracted orders set up when a plane wave is incident upon a periodic reflecting surface. Either the first or the second boundary condition can be so treated. A sample problem is worked showing that if the average absolute slope of the reflecting surface is small (segments of surface with large slope may be included) and if the displacement of the surface is not large compared with the wave length of the incident radiation, the formulation gives results correct to within a few per cent. The calculation shows clearly the existence of Wood anomalies; these are discussed in some detail.

A VARIATIONAL METHOD FOR THE CALCULATION OF THE

DISTRIBUTION OF ENERGY REFLECTED FROM A PERIODIC

SURFACE *†

W.C. Meecham

I. INTRODUCTION

The problem of the reflection of radiation from non-plane surfaces has in the past received the attention of many people employing various approximations in its treatment.[1-5] It is the purpose of this paper to present a variational method for the treatment of such problems, in particular those in which the surface involved has a displacement which is of the order of magnitude of the radiation wave length and in which the surface has portions of moderately large slope , though the average absolute slope should be small. This class of problems is one which is not amenable to treatment by the other methods at present available.

---

1. B.B. Baker and E.T. Copson, The Mathematical Theory of Huygens' Principle (2nd ed.; London: Oxford University Press, 1950), chap. II.

2. Lord Rayleigh, Roy. Soc. Proc. 79A, 399 (1907).

3. V. Twersky, J. Acoust. Soc. Am. 22, 539 (1950).

4. C. Eckart, J. Acoust. Soc. Am. 25, 566 (1953).

5. L.M. Brekhovskikh, Zh. exsper. teor. Fiz. (USSR) 23, 275 (1952). Translated by G.N. Goss, U.S. Navy Electronics Laboratory, San Diego, California.

The method may be described as follows. Following Trefftz,[6] a linear combination of known solutions to the wave equation is chosen to represent the reflected field. The coefficients will be chosen here so that they minimize the square of the error in the boundary condition. (Trefftz chose them so as to minimize the Rayleigh quotient.) This process of minimization is equivalent to orthogonalizing the set of functions formed by evaluating the trial functions on the boundary. Once this set is orthogonalized one can easily construct the estimates of the reflection coefficients for the surface involved.

The class of problems to be considered will now be described. It is desired to find a solution ϕ of the two-dimensional, time-independent wave equation,

$$\left[\frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial z^2} + k^2\right] \phi^{(x,z)} = 0 \tag{1}$$

in a half-space bounded by a periodic cylindrical surface $\zeta(x)$ (see Fig. 1). In Eq. (1) $k = \omega/c$ when ω is the angular frequency of the radiation source and c is the phase velocity in the homogeneous medium bounded by $\zeta(x)$. The solution of the time-dependent wave equation is then given by $\phi e^{-i\omega t}$.
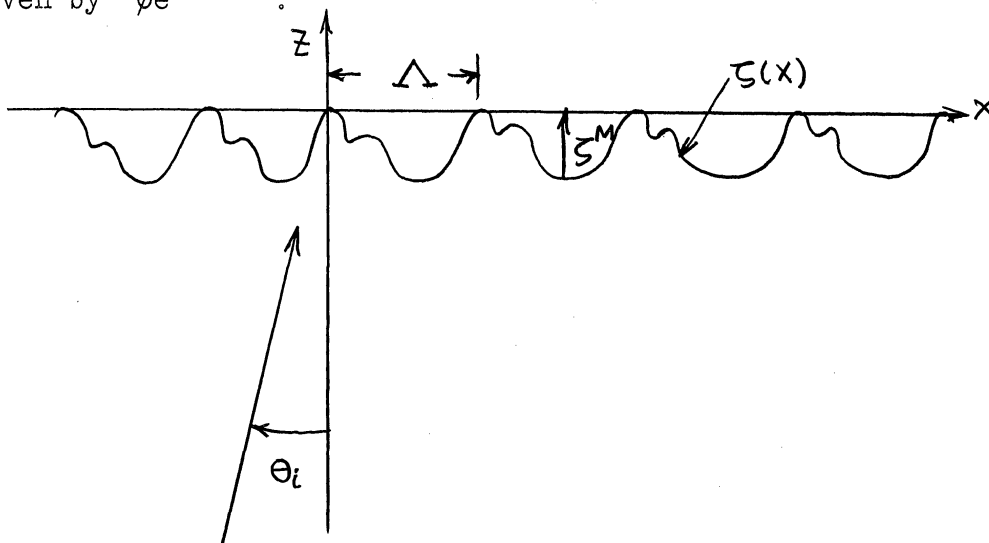

Fig. 1. Sketch showing the definition of the symbols used in the solution of the reflection problem.

6. E. Trefftz, Math. Ann. 100, 503 (1928).

Using the method described herein, one may treat either the first or the second boundary value problem.[7] Thus one may require either

$$\phi(x, \zeta(x)) = 0 \tag{2}$$

or,

$$\frac{\partial \phi(x, z)}{\partial n}\bigg|_{z = \zeta(x)} = 0 \ . \tag{3}$$

Here $\frac{\partial}{\partial n}$ represents the derivative normal to the surface. It is supposed that the incident radiation consists of a plane wave making an angle θ_i with the $+z$ direction; then one can write the total field as the sum of two components,

$$\phi = \phi_i + \phi_r \tag{4}$$

where,

$$\phi_i = e^{ik\left[x \sin \theta_i + z \cos \theta_i\right]} \tag{5}$$

The boundary conditions given by Eqs. (2) and (3) are frequently encountered in the treatment of problems involving acoustic and electromagnetic radiation. For acoustic problems, the function ϕ may be taken to represent the (time-independent) velocity potential, with ϕ defined by,

$$\vec{v} = -\nabla \phi \tag{6}$$

where $\vec{v}$ is the particle velocity at an arbitrary field point (x, z). Then the first boundary value problem, represented by Eq. (2), corresponds to a physical problem in which $\zeta(x)$ is a pressure release surface. Furthermore from Eq. (6) it is evident that the second boundary value problem corresponds to the physical problem in which $\zeta(x)$ is a rigid surface. For problems

---

7. One could use the same method to treat problems where the boundary condition is of the form $\left[A\phi + B \frac{\partial \phi}{\partial n}\right]_{z = \zeta(x)} = 0$ where A and B may be functions of x or in fact the more general problem where one is given two different media separated by a periodic surface and is asked to find the reflected and the transmitted fields.

involving electromagnetic radiation on the other hand, $\zeta(x)$ is assumed to be a perfectly conducting surface. Then for an incident plane wave which has its propagation vector lying in the x-z plane and which is polarized so that the electric vector is perpendicular to the x-z plane, one chooses the boundary condition given by Eq. (2) where it is supposed that the electric field, which has but a single cartesian component, is given by the function ϕ. Finally for incident radiation polarized so that the electric field lies in the x-z plane one lets ϕ represent the (single cartesian component) magnetic field and chooses the boundary condition given by Eq. (3).

II. REPRESENTATION OF THE REFLECTED FIELD

In order to make progress toward a solution of the above class of problems, Rayleigh[8] and others[9,10] have chosen to represent the reflected field by an infinite set of plane wave solutions of the wave equation. In addition to homogeneous, one must choose inhomogeneous waves. The waves must be chosen in such a way that they are respectively either outgoing or exponentially damped as $z \to -\infty$. Furthermore the fact that the boundary is periodic implies that one needs only a discrete set of such waves. Thus one is lead to expect that the reflected field ϕ_r can be represented by the following type of sum,

$$\sum_{\psi = -\infty}^{\infty} A_\psi e^{-ik \sin \Theta_\psi x - ik \cos \Theta_\psi z} \tag{7}$$

where

$$\sin \Theta_\psi = \psi \frac{K}{k} - \sin \Theta_i \; ; $$
$$\cos \Theta_\psi = \left[1 - \sin^2 \Theta_\psi \right]^{1/2} , \tag{8}$$

where $K = 2\pi / \Lambda$ (see Fig. 1),

and where the coefficients, A_ψ , are to be determined through the use of the boundary condition. The angles Θ_ψ of the various reflected orders are just those obtained from the ordinary grating equation.

---

8. Lord Rayleigh, _Theory of Sound_ (2nd ed.; New York: Dover Publications, 1945), vol. II, p. 89.

9. U. Fano, Phys. Rev. 51, 288 (1937).

10. K. Artmann, Z. Physik 119, 529 (1942).

Lippmann[11] has questioned the validity of the representation given by the expression (7) in the region $\zeta^M < z < \zeta(x)$, at the same time confirming its validity in the region $z < \zeta^M$ (see Fig. 1). The details of Lippman's argument are presented in an unpublished report. It will prove convenient to reproduce here the substance of his argument, though in a somewhat altered form.

One may begin by representing the reflected field through the use of the two-dimensional Helmholtz formula,[12]

$$\phi_r = -\frac{1}{4i} \int_{\zeta} H_0^{(1)}(kr_{1P}) \frac{\partial}{\partial \nu_1} \phi(1)ds_1 \quad . \tag{9}$$

The integral is to be carried over the entire surface $\zeta(x)$; the symbol $\frac{\partial}{\partial \nu_1}$ represents the derivative with respect to the outward-drawn normal, (see Fig. 2).
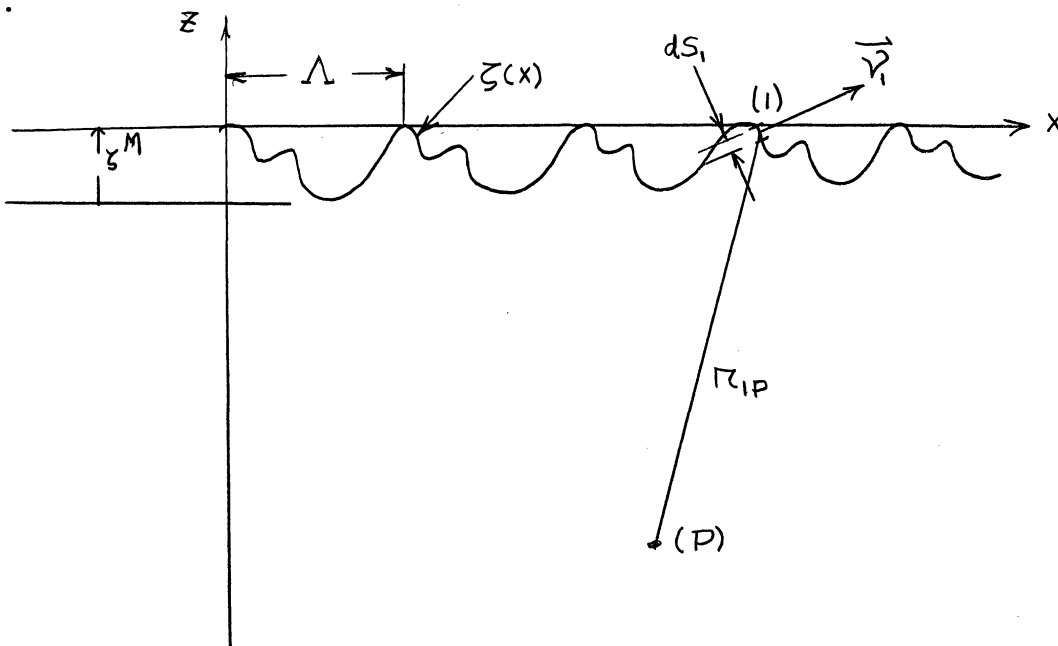

Fig. 2. The figure shows the symbols used in the Helmholtz formula.

11. B.A. Lippmann, J. Opt. Soc. Am. 43, 408 (1955).

12. Baker and Copson, loc. cit., chaps. I and II.

For the present purpose attention has been restricted to the first boundary value problem.

It is not difficult to verify that,

$$\frac{\partial}{\partial \gamma_i} \phi(x_1 + \Lambda, \zeta(x_1 + \Lambda)) = e^{ik\Lambda \sin\theta_i} \frac{\partial}{\partial \gamma_i} \phi(x_1, \zeta(x_1)) . \tag{10}$$

Using Eq. (10) one can rewrite Eq. (9).

$$\phi = -\frac{1}{4i} \sum_{n=-\infty}^{\infty} \int_{x=0}^{x=\Lambda} H_0^{(1)}(kr_n) \frac{\partial \phi(1)}{\partial \gamma_i} e^{ikn\Lambda \sin\theta_i} ds_1 \tag{11}$$

where

$$r_n = \left[(x_P - n\Lambda - x_1)^2 + (z_P - z_1)^2\right]^{1/2} . \tag{12}$$

By using Sommerfeld's contour integral representation for the Hankel function one may construct the plane wave representation for that function,

$$H_0^{(1)}(kr_{1P}) = \frac{1}{\pi} \int_{-\infty}^{\infty} \frac{e^{ik(x_P-x_1) \mp i(k^2 - \hat{k}^2)^{1/2}(z_P-z_1)}}{(k^2 - \hat{k}^2)^{1/2}} d\hat{k} , \tag{13}$$

where the minus sign applies if $z_P - z_1 < 0$ and the plus sign if $z_P - z_1 > 0$.

Then by substituting Eq. (13) in Eq. (11), by assuming the validity of interchanging the summation and the integration, and by utilizing the result

$$\sum_{n=-\infty}^{\infty} e^{-in\hat{k}\Lambda} = K \sum_{n=-\infty}^{\infty} \delta(\hat{k} - nK) \tag{14}$$

where $\delta(\hat{k} - nK)$ is the Dirac delta function, one arrives at the following representation for the reflected field:

$$\phi_r(P) = \sum_{\gamma=-\infty}^{\infty} A_\gamma e^{-ik\sin\theta_\gamma x_P - ik\cos\theta_\gamma z_P} , \tag{15}$$

when $z_P - \zeta^M < 0$,

and where

$$A_\gamma = \frac{K}{\pi k \cos\theta_\gamma} \int_0^\Lambda \left[-\frac{1}{4i} \frac{ds_1}{dx_1} \frac{\partial \phi(1)}{\partial \gamma_i}\right] e^{i\sin\theta_\gamma kx_1 + ik\cos\theta_\gamma \zeta(x_1)} dx_1 . \tag{16}$$

Further

$$\phi_r(P) = \sum_{\mathcal{V}=-\infty}^{\infty} \left\{ A_{\mathcal{V}}^{-}(z_P) \; e^{-ik \sin \Theta_{\mathcal{V}} x_P - ik \cos \Theta_{\mathcal{V}} z_P} \right. $$

$$\left. + A_{\mathcal{V}}^{+}(z_P) \; e^{-ik \sin \Theta_{\mathcal{V}} x_P + ik \cos \Theta_{\mathcal{V}} z_P} \right\} \quad , \tag{17}$$

when $\zeta^M < z_P < \zeta(x)$,

where,

$$A_{\mathcal{V}}^{\pm}(z_P) = \frac{K}{\pi k \cos \Theta_{\mathcal{V}}} \int_{C^{\pm}} \left[-\frac{1}{4i} \frac{ds_1}{dx_1} \frac{\partial \phi(1)}{\partial \mathcal{V}_1} \right] e^{i \sin \Theta_{\mathcal{V}} kx_1 \mp ik \cos \Theta_{\mathcal{V}} \zeta(x_1)} dx_1 , \tag{18}$$

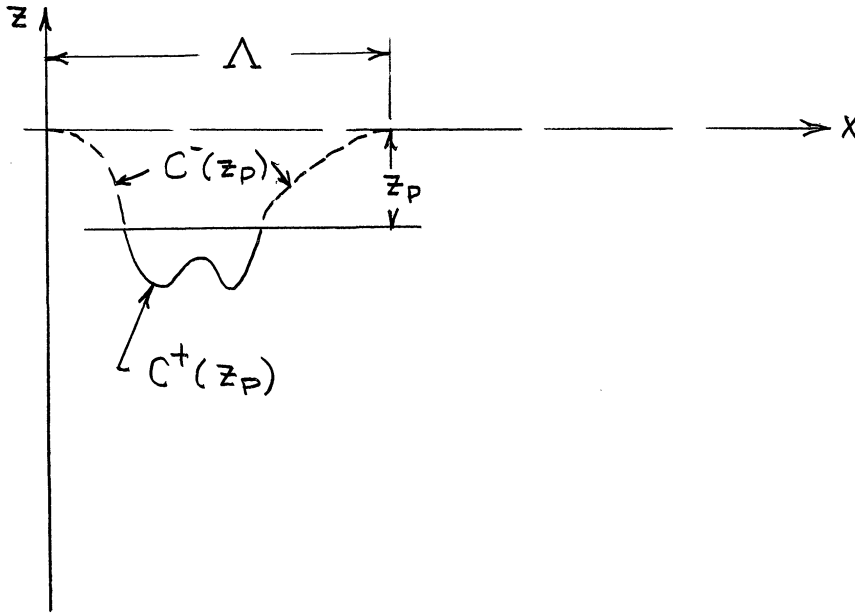and with $C^{\pm}(z_P)$ defined in Fig. 3.

Fig. 3. Diagram defining the contours $C^{\pm}(z_P)$.

The plausibility of the assertions made above concerning the reflected field now becomes evident. From Eq. (15) it is seen that when the point (P) is removed from the surface, the reflected field is composed of plane wave solutions which are either proceeding in the negative z direction

or die out exponentially in that direction. Furthermore when $\zeta^M < z_P < \zeta(x_P)$ one sees from Eq. (17) that the field may be represented in a form which appears to be a combination of waves moving in both the plus and the minus z directions with coefficients dependent upon z_P. Of course in the latter case, individual terms of the series are not solutions of the wave equation.

For certain problems it may turn out that the representation given in Eq. (17) is merely an alternate (and more complicated) form for the representation of the type given by Eq. (15). Indeed this is the case for one special problem which can be solved exactly. The problem is one in which the field satisfies the boundary condition given by Eq. (3): it is supposed that the incident wave falls normally upon one of the faces of the representative groove form (see Fig. 4);
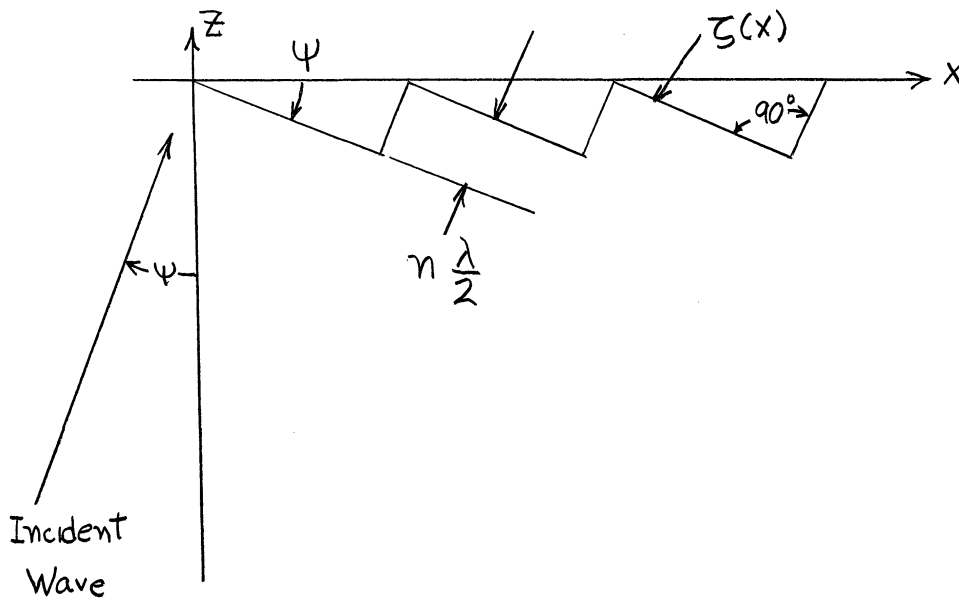

Fig. 4. Figure showing a simple reflection problem which can be solved exactly.

(in the figure, n is an integer). The reflected field for this problem obviously consists of a single plane wave moving in a direction opposed to that of the incident wave and with amplitude unity; this solution is valid in the entire region $z \leq \zeta$.

To summarize the work in this section, it is evident that for some problems one can represent the reflected field by a sum of plane waves proceeding in the negative z direction even in the region $\zeta^M < z < \zeta(x)$. However, although to the author's knowledge an exact solution indicating the necessity of using a more complicated representation of the type given by Eq. (17) is lacking, it seems reasonable to suppose that in general the plane wave representation is not sufficient in the region near the reflecting surface.

III. THE VARIATIONAL METHOD

It will be convenient to define,

$$\phi_r = \phi_{rP} + \phi_{rNP} \tag{19}$$

where

$$\phi_{rP} = - \sum_{\nu=-\infty}^{\infty} A_\nu \, e^{-ik \sin \Theta_\nu x - ik \cos \Theta_\nu z} \quad , \tag{20}$$

valid in the region $z \leq \zeta(x)$, and ϕ_{rNP} represents that part of the reflected field which cannot be written in that form. For the purposes of the present paper, attention is restricted to those problems for which

$$|\phi_{rNP}| \ll |\phi_{rP}| \quad . \tag{21}$$

Lippman and Oppenheim[13] have proposed a sufficient condition for the validity of the relation (21); it is:

$$\frac{|\zeta^M|}{\lambda} \ll 1 \quad , \tag{22}$$

when Λ and λ are of the same order of magnitude. The results given in Section IV make it evident that this condition is too restrictive for the present work, probably because of the minimal formulation of the problem.

It is possible, through a detailed consideration of the images contained in the region $\zeta(x) < z \leq 0$, to estimate the function ϕ_{rNP} using a method essentially the same as that outlined below. Problems for which

---

13. B.A. Lippmann and A. Oppenheim, Technical Research Group, 56 West 45 Street, New York 36, N.Y., Final Report on Contract No. AF18(600)-954.

such a treatment is necessary will not be considered in this paper. In order

to simplify notation it will be assumed hereafter that $\emptyset_{rNP} = 0$. Further-

more only the first boundary value problem (the boundary condition is given

in Eq. (2)) will be considered in detail. When that work is completed, it

will be shown how to alter the formulation for the second boundary value prob-

lem.

To proceed, upon using Eqs. (2), (4), (5), (19), and (20) one finds

the following relation for the determination of the constants A_γ :

$$e^{ik\left[\sin\Theta_i x + \cos\Theta_i \zeta(x)\right]} - \sum_{\gamma=-\infty}^{\infty} A_\gamma e^{-ik\left[\sin\Theta_\gamma x + \cos\Theta_\gamma \zeta(x)\right]} = 0 \qquad (23)$$

and upon applying Eq. (8), and dividing by the common factor $e^{ik\sin\Theta_i x}$,

this becomes

$$e^{ik\cos\Theta_i \zeta(x)} - \sum_{\gamma=-\infty}^{\infty} A_\gamma e^{-i\gamma Kx - ik\cos\Theta_\gamma \zeta(x)} = 0 \quad . \qquad (24)$$

To render the treatment of Eq. (24) more systematic let

$$F_1(x) = \exp(0)$$

$$F_2(x) = \exp(1)$$

$$F_3(x) = \exp(-1)$$

$$F_4(x) = \exp(2) \qquad (25)$$

$$\cdot$$
$$\cdot$$
$$\cdot$$

and

$$\overline{A}_1 = A_0$$

$$\overline{A}_2 = A_1$$

$$\overline{A}_3 = A_{-1}$$

$$\cdot$$
$$\cdot$$
$$\cdot$$

where in Eqs. (25),

$$\exp(\gamma) = e^{-i\gamma Kx - ik\cos\Theta_\gamma \zeta(x)} \quad ; \qquad (26)$$

further let

$$\bar{\phi}_i = e^{ik \cos \Theta_i} \zeta(x)$$

Then Eq. (24) becomes,

$$\bar{\phi}_i(x) - \sum_{K=1}^{\infty} \bar{A}_K F_K(x) = 0 . \tag{27}$$

If the series in Eq. (27) is broken off after the Nth term, as must be done in many problems, the left side of that equation is not in general equal to zero. It is proposed that in such a case, the constants $\bar{A}_k$ be chosen in such a way that the integral over the surface ζ of the absolute square of the left side of Eq. (27) is minimized. Since all quantities in that equation are periodic with period Λ, it is sufficient to carry the integral from x=0 to x= Λ. It is easily seen from Eq. (23) that this minimization is equivalent to carrying out the corresponding minimization of the error in the boundary condition. It is not difficult to show that if one chooses the coefficients $\bar{A}_k$ so that they satisfy the set of equations (with ℓ = 1,2,...,N)

$$\sum_{k=1}^{N} \bar{A}_k(F_\ell, F_k) = (F_\ell, \bar{\phi}_i) \tag{28}$$

when the inner product of two functions, (g,h), is defined by

$$(g,h) = \frac{1}{\Lambda} \int_0^{\Lambda} g^* h \, dx , \tag{29}$$

then the above indicated minimization is accomplished.

Rather than approach the inversion of the set of equations (28) directly, it has proved convenient for the purposes of computation to use an equivalent, though somewhat indirect, method. To see this method, let Eq. (27) be considered again. One observes that the problem is equivalent to finding that linear combination of functions F_k which is equal to the given function ϕ_i.[14] This task is complicated by the fact that the

---

14. Setting ϕ_{rNP} (of Eq. (19)) equal to zero is equivalent to assuming that this is possible.

functions F_k are not in general mutually orthogonal. This suggests that one proceed by constructing an orthonormal set of functions from linear combinations of the given set F_k. There is a well-known method for doing this.[15] Let the desired orthonormal set be G_k; then one can write

$$G_K = \sum_{\ell=1}^{k} \Gamma_{\ell}^{(k)} F_\ell \; , \tag{30}$$

with

$$(G_m, G_n) = \delta_{mn}$$

when δ_{mn} is equal to one or zero depending on whether $m=n$ or not and where the coefficients $\Gamma_{\ell}^{(k)}$ are determined as follows. Let G_1 be equal to F_1 devided by its norm; the norm of F_1 is defined as $(F_1, F_1)^{1/2}$. One then takes that linear combination of F_1 and F_2 which is orthogonal to G_1, divides it by its norm and sets it equal to G_2. Upon proceeding in this way the following recursion relations for the coefficients in Eq. (30) are easily obtained:

$$\Gamma_{\ell}^{(k)} = \frac{\gamma_{\ell}^{(k)}}{N_k^{1/2}} \tag{31}$$

where

$$\ell < k, \qquad \gamma_{\ell}^{(k)} = - \sum_{\beta=\ell}^{k-1} \sum_{\alpha=1}^{\beta} \Gamma_{\alpha}^{(\beta)*} (F_\alpha, F_k) \Gamma_{\ell}^{(\beta)} \; , \tag{32}$$

$$\ell = k, \qquad \gamma_{k}^{(k)} = 1$$

and where

$$N_k = \sum_{\mu=1}^{k} \sum_{\nu=1}^{k} \gamma_{\mu}^{(k)*} (F_\mu, F_\nu) \gamma_{\nu}^{(k)} \; , \tag{33}$$

when the star indicates the complex conjugate.

Now let

$$\phi_i^{(N)}(x) = \sum_{k=1}^{N} B_k G_k(x) \; , \tag{34}$$

---

15. For a reference concerning representations in terms of systems of functions see R. Courant and D. Hilbert, _Methods of Mathematical Physics_ (Engl. ed.; New York: Interscience Publishers Inc., 1953), vol I, chap. II, secs. 2 and 3.

where $\overline{\phi}_i^{(N)}$ represents the Nth approximation to $\overline{\phi}_i$ and where B_k are defined by

$$B_k = (G_k, \overline{\phi}_i) \tag{35}$$

or upon using Eq. (30),

$$B_k = \sum_{\alpha=1}^{K} \Gamma_\alpha^{(k)*}(F_\alpha, \overline{\phi}_i) . \tag{36}$$

Then by using Eq. (30) in connection with Eq. (34) one can write,

$$\overline{\phi}_i^{(N)}(x) = \sum_{k=1}^{N} \overline{A}_k' F_k \tag{37}$$

when

$$\overline{A}_k' = \sum_{\alpha=K}^{N} B_\alpha \Gamma_k^{(\alpha)} , \tag{38}$$

That

$$\overline{A}_k' = \overline{A}_k \tag{39}$$

where $\overline{A}_k$ are defined implicitly in Eq. (28) can be seen by observing that the B_k as defined in Eq. (35) are the Fourier coefficients of the function $\overline{\phi}_i$ with the set G_k. It follows then that the quantity

$$\frac{1}{\Lambda} \int_0^\Lambda |\overline{\phi}_i - \overline{\phi}_i^{(N)}|^2 dx \tag{40}$$

is minimized and therefore that the coefficients $\overline{A}_k'$, as obtained from the coefficients B_k in Eq. (38), must also minimize the expression (40). But Eq. (28) governing the quantities $\overline{A}_k$ was obtained by minimizing the quantity (40). Hence Eq. (39) must follow. Indeed one can verify Eq. (39) directly by substituting Eq. (38) in Eq. (28).

One of the advantages of proceeding as above toward the solution of Eq. (28) is that one obtains an estimate of the error incurred by breaking off the infinite system of equations at N , this error being combined with the error involved in the assumption that $\phi_{rNP} = 0$. The estimate is obtained in a way similar to that by which one ordinarily obtains Bessel's inequality.[15] One finds that

$$\frac{1}{\Lambda} \int_0^\Lambda |\overline{\phi}_i - \overline{\phi}_i^{(N)}|^2 dx = (\overline{\phi}_i, \overline{\phi}_i) - \sum_{k=1}^{N} |B_k|^2 , \tag{41}$$

or by observing the definition of $\overline{\phi}_i$ given by Eq. (26),

$$\text{M.S.E.} = 1 - \sum_{K=1}^{N} |B_k|^2 , \tag{42}$$

where M.S.E. stands for the mean square error in the boundary condition (the expression (40)). The error arises both as a result of considering only a finite number of diffracted waves and as a result of assuming that ϕ_{rNP} is negligible.

There is a relation which follows from the conservation of energy which can also be used as a check on the accuracy of the calculation. By considering the energy balance within the region of the x-z plane bounded by $\zeta(x)$, x=0, x=Λ , and z=-C, where C is large and positive, one obtains the following relation for the exact solution,

$$\cos \theta_i = \sum_{\gamma} \cos \theta_\gamma |A_\gamma|^2 \tag{43}$$

where the summation is carried over those values of γ for which $\cos \theta_\gamma$ is real and where the notation of Eq. (20) is used again, remembering the changes made by Eqs. (25).

A third relation which can be used to check the accuracy of the calculation arises from the reciprocity theorem.[16] To obtain this expression one treats first the problem of the reflection of radiation from a periodic surface which is finite in extent in the x direction, using the Helmholtz formula. This problem is then compared with the corresponding problem involving an infinite periodic surface. By allowing the finite surface to extend to greater and greater distances in the x direction, one finds the following relation governing the plane wave reflection coefficients,

$$\cos \theta_\gamma A_\gamma (\theta_i) = \cos \theta_i A_\gamma (\theta_\gamma) \tag{44}$$

where $A_\gamma(\theta_i)$ represents, as before, the reflection coefficient of the γth

16. Lord Rayleigh, Theory of Sound, loc. cit., vol. 2, sec. 294.

order wave but with the incident direction explicitly indicated. From Eq. (44) it is seen that the zeroth order (specular component) should be symmetrical about $\Theta_i = 0$, regardless of whether or not the surface is symmetrical.

It will now be shown how to modify the work of this section in order to make it applicable to the second boundary value problem. It will again be assumed that ϕ_{rNP} is negligible. In order to obtain the required result, consider the boundary condition given by Eq. (3) in connection with Eqs. (4), (5), and (20). One easily finds (essentially by taking $\frac{\partial}{\partial\nu}$ of Eq. (23)) the following relation governing the reflection coefficients:

$$ik(n_x\sin\Theta_i + n_z\cos\Theta_i)\, e^{ik\cos\Theta_i\,\zeta(x)}$$

$$-\sum_{\gamma=-\infty}^{\infty} A_\gamma\,(-ik)(n_x\sin\Theta_\gamma + n_z\cos\Theta_\gamma)\, e^{-i\gamma Kx - ik\cos\Theta_\gamma\,\zeta(x)} = 0 \qquad (45)$$

where

$$n_x = -\zeta'\left[1 + (\zeta')^2\right]^{-1/2}, \quad n_z = \left[1 + (\zeta')^2\right]^{-1/2} \qquad (46)$$

and

$$\zeta' = \frac{d\zeta}{dx} \, . \qquad (47)$$

The Eq. (45) is to be compared with the corresponding Eq. (24) obtained for the first boundary value problem. The quantities n_x and n_z are of course the components of a unit vector normal to the surface $\zeta(x)$ and pointing out of the physical region. Now it is not difficult to see that the approximate solution of Eq. (45) is given by Eqs. (38), (36), and (31), (32), and (33) upon replacing (F_n, F_m) by $(\mathcal{F}_n, \mathcal{F}_m)_2$; and $(F_n, \overline{\phi}_i)$ by $(\mathcal{F}_n, \overline{\Phi}_i)_2$ where

$$(g, h)_2 = \frac{1}{\Lambda k^2} \int_0^\Lambda g^* h\, dx , \qquad (48)$$

$$\overline{\Phi}_i = ik(n_x\sin\Theta_i + n_z\cos\Theta_i)\,\overline{\phi}_i \qquad (49)$$

and

$$\mathcal{K}_1 = -ik\,(n_x \sin\Theta_0 + n_z \cos\Theta_0)\,\exp(0)$$

$$\mathcal{K}_2 = -ik\,(n_x \sin\Theta_1 + n_z \cos\Theta_1)\,\exp(1) \tag{50}$$

$$\mathcal{K}_3 = -ik\,(n_x \sin\Theta_{-1} + n_z \cos\Theta_{-1})\,\exp(-1)$$

$$\circ$$
$$\circ$$
$$\circ$$

It is noted from Eq. (48) that the definition of the inner product has been changed in order to keep it dimensionless for the present functions. Furthermore for the second boundary value problem the Eq. (42) must be modified. By analogy with Eq. (41) one can write

$$\frac{1}{k^2 \Lambda} \int_0^\Lambda \left| \frac{\partial \phi_i}{\partial \gamma} - \frac{\partial \phi_i^{(N)}}{\partial \gamma} \right|^2 dx = (\overline{\Phi}_i, \overline{\Phi}_i)_2 - \sum_{K=1}^N |B_k|^2 \tag{51}$$

where the B_k are those appropriate to the present problem, and where the functions $\dfrac{\partial \phi_i}{\partial \gamma}$ and $\dfrac{\partial \phi_i^{(N)}}{\partial \gamma}$ appearing in the integral are to be evaluated at the surface. Finally then Eq. (51) can be written,

$$\frac{1}{k^2}\, M.S.E. = (\overline{\Phi}_i, \overline{\Phi}_i)_2 - \sum_{K=1}^N |B_k|^2 \tag{52}$$

where M.S.E. is again the mean square error in the boundary condition (now with dimensions of reciprocal length squared).

To sum up the results of this section, one uses Eq. (38) to obtain estimates of the reflection coefficients of the various diffracted waves. The quantities B_k are defined in Eq. (36); the quantities $\Gamma_\ell^{(k)}$ which are also needed are defined in Eqs. (31), (32), and (33). Finally if the second boundary value problem is being considered, Eqs. (36), (31), (32), and (33) are altered as indicated in Eqs. (48), (49), and (50).

IV. RESULTS OF CALCULATIONS AND CONCLUSIONS

Calculations based upon the method presented above have, to the present date, been carried out only for surfaces of the class shown in Fig. 5, and for the first boundary value problem. Hence, since the field function vanishes at the surface in such a case, the solutions are appropriate for acoustic problems involving free surfaces or for electromagnetic problems involving incident energy polarized with the electric vector parallel to the generating element of the (conducting) surface (perpendicular to the page in Fig. 5).
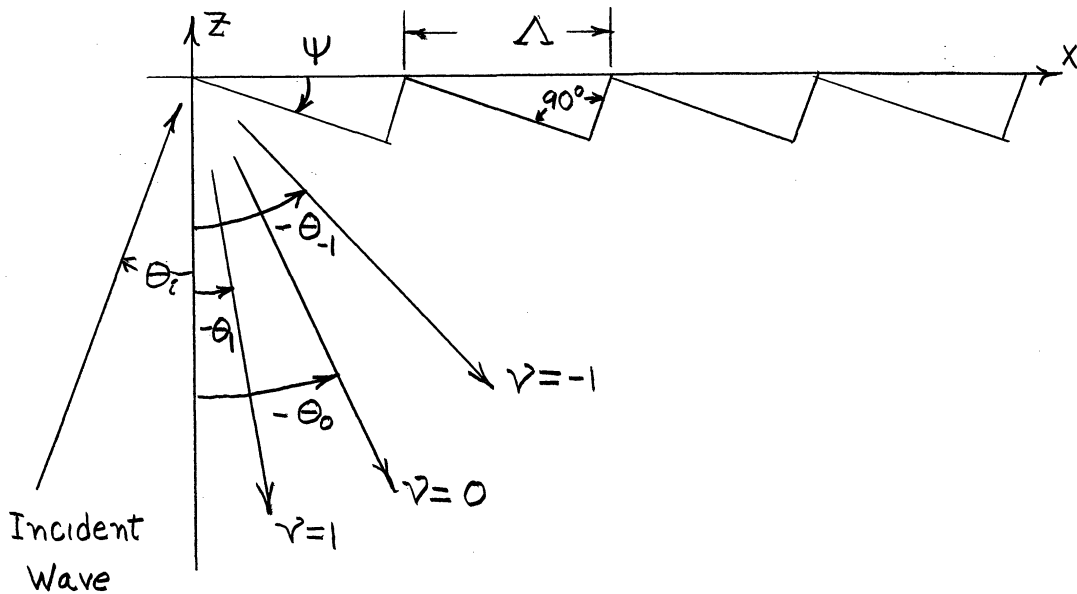

Fig. 5. Figure showing the type of surface for which computations have been made.

In the figure three representative reflected wave directions are shown, although they have not been chosen to fit any particular case.

The surface was chosen for calculation for two reasons. First, it is of some physical interest; the sea surface assumes a shape reminiscent of that shown in the figure under conditions of high wind, so that the treatment of the problem may be helpful in attaining an understanding of the distribution of acoustic or electromagnetic energy reflected from such a surface. Furthermore, the surface is of the type known as an echelette grating which is sometimes used in optical and infra-red spectral work. The second reason for choosing the indicated type of surface for the calculations is that the calculations are somewhat simplified; the integrals shown in Eq. (29) can be evaluated in terms of exponentials when the surface is composed of straight line elements.

For the sake of completeness the formulas for the inner products involved in the calculation of the distribution of energy reflected from a surface of the type shown in Fig. 5 will be given here. One finds that

$$(F_m, F_n) = (F_m, F_n)_a + (F_m, F_n)_b \tag{53}$$

where

$$(F_m, F_n)_a = \frac{1}{2\pi i} \left[(\gamma_m - \gamma_n) - \frac{k}{K} \sigma (\cos*\theta_{\gamma_m} - \cos \theta_{\gamma_n}) \right]^{-1}$$

$$\cdot \left\{ \exp i \eta_0 \left[(\gamma_m - \gamma_n) - \frac{k}{K} \sigma (\cos*\theta_{\gamma_m} - \cos\theta_{\gamma_n}) \right] - 1 \right\} \tag{54}$$

and

$$(F_m, F_n)_b = \frac{\sigma^2}{2\pi i} \left[-\sigma^2 (\gamma_m - \gamma_n) - \frac{k}{K} \sigma (\cos*\theta_{\gamma_m} - \cos\theta_{\gamma_n}) \right]^{-1}$$

$$\cdot \left\{ \exp i \eta_0 \left[-\sigma^2 (\gamma_m - \gamma_n) - \frac{k}{K} \sigma (\cos*\theta_{\gamma_m} - \cos\theta_{\gamma_n}) \right] - 1 \right\}. \tag{55}$$

Also

$$(F_m, \tilde{\phi}_i) = (F_m, \bar{\phi}_i)_a + (F_m, \bar{\phi}_i)_b , \tag{56}$$

where

$$(F_m, \overline{\phi}_i)_a = \frac{1}{2\pi i} \left[\mathcal{V}_m - \frac{k}{K} (\cos{}^*\Theta_{\gamma_m} + \cos \Theta_i) \right]^{-1}$$

$$\cdot \left\{ \exp i \eta_o \left[\mathcal{V}_m - \frac{k}{K} (\cos{}^*\Theta_{\gamma_m} + \cos\Theta_i) \right] \quad -1 \right\} \tag{57}$$

and

$$(F_m, \overline{\phi}_i)_b = \frac{\sigma^2}{2\pi i} \left[-\sigma^2 \mathcal{V}_m - \frac{k}{K} \sigma (\cos{}^*\Theta_{\gamma_m} + \cos\Theta_i) \right]^{-1}$$

$$\cdot \left\{ \exp i \eta_o \left[-\sigma^2 \mathcal{V}_m - \frac{k}{K} \sigma (\cos{}^*\Theta_{\gamma_m} + \cos\Theta_i) \right] -1 \right\}, \tag{58}$$

when

$$\eta_o = \frac{2\pi}{1+\sigma^2}, \tag{59}$$

$$\sigma = \tan \psi, \tag{60}$$

and $\mathcal{V}_1 = 0, \mathcal{V}_2 = 1, \mathcal{V}_3 = -1, \mathcal{V}_4 = 2, \ldots$.

The entire problem, starting with the calculation of the inner products (F_k, F_m) and $(F_k, \overline{\phi}_i)$, through the calculation of the quantities $\Gamma_\ell^{(k)}$, and including the calculation of the estimates of the reflection coefficients $\overline{A}_k$ (or A_γ) has been programmed for MIDAC, the University of Michigan digital computer. The recursive and cyclical form of the central part of the calculation, the central part being the computation of the quantities $\Gamma_\ell^{(k)}$ given by Eqs. (31), (32), and (33), renders the formulation easily adaptable to a digital machine. The capacity of the machine limited the calculation to ten diffracted waves (N=10).

For the calculation presented in Fig. 6 a surface of the type shown in Fig. 5 was chosen with $\psi = 10°$ and with $\Lambda = 1.155\lambda$. This ratio of Λ to λ implies that for a given incident angle, at most three diffracted orders appear. The plus second diffracted order never exceeds 0.38% and is too small to show on the graph. It is noted from the figure that the energy deficit of the calculation (as computed from the right side of Eq. (43))
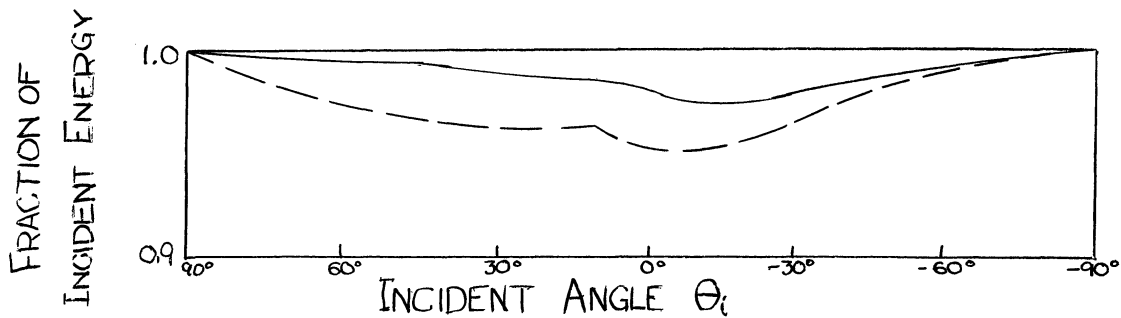
Fig. 6a. The solid curve shows 1 - M.S.E. (where M.S.E. is the mean square error in the boundary condition); the dashed curve shows the ratio of the total calculated, reflected energy to the incident energy.
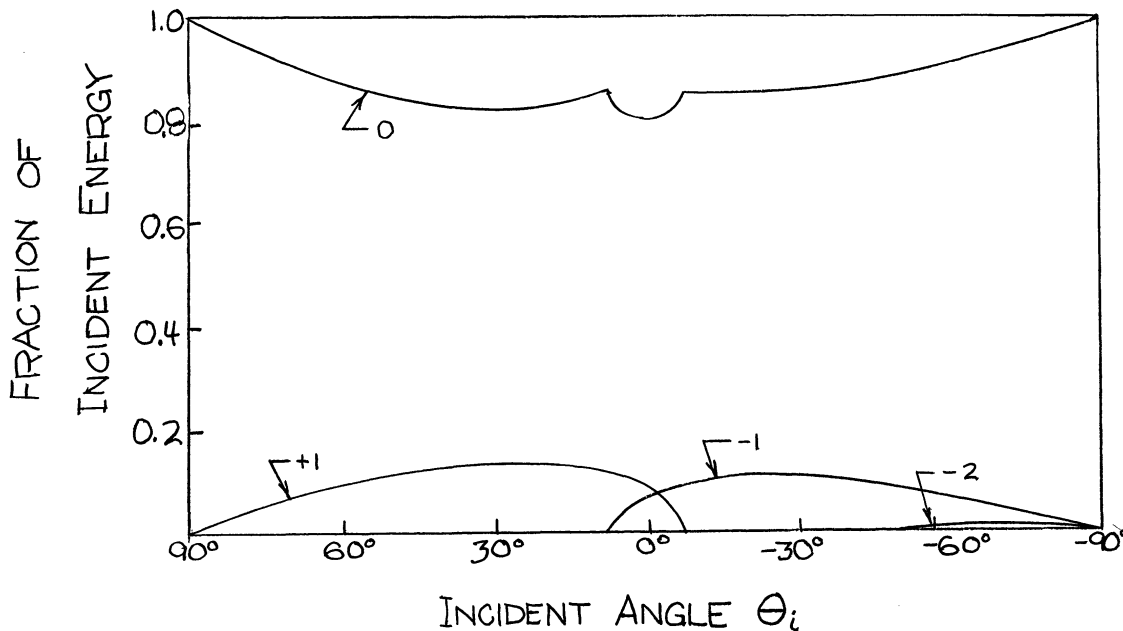

Fig. 6b. The curves show the fraction of the total incident energy which is contained within a given diffracted order when a plane wave is incident upon the periodic surface with an angle (measured from the normal) as indicated by the abcissae. The surface is described by Ψ =10° and Λ =1.155 λ.

averages about 2.5% and never exceeds 5%; furthermore the M.S.E. is less than 0.025. From these two checks, it seems reasonable to expect that the error for a given order is less than 5% (of its value).

As suggested in Section III, the reciprocity relation can also be used to check the accuracy of the calculation. It was deduced from Eq. (44) that the reflection coefficient for the zeroth order should be symmetrical about the normal; it follows then from the energy relation given by Eq. (43) that the percentage of the total incident energy in the zeroth order should also be symmetrical. It is seen from Fig. 6 that this order is symmetrical within a few per cent, the assigned error. All other reciprocity checks carried out also agree within a few per cent. For instance one should have,

$$\cos 60° \ A_1(0°) = \cos 0° \ A_1(60°) \ , \tag{61}$$

and

$$\cos 9°8' \ A_1(45°) = \cos 45° \ A_1(9°8') \ . \tag{62}$$

Actually the numbers from the calculation are $-0.1485 +0.1449i$ and $-0.1562 +0.1525i$ for the left and right sides of Eq. (61) respectively; $-0.1787 +0.2312i$ and $-0.1735 +0.2242i$ for the left and right sides of Eq. (62) respectively.

From Fig. 6 it is seen that the main part of the reflected energy is carried by the zeroth, or specular order; this component never drops below 80%. Discontinuities of the type shown in the zeroth order at $\theta \approx \pm 8°$ are known as Wood anomalies[17] (after their discoverer) and have been observed many times experimentally. Rayleigh[18] showed that the positions of

---

17. R.W. Wood, Phil. Mag. 4, 396 (1902).

18. Lord Rayleigh, Phil. Mag. 14, 60 (1907).

the anomalies were connected with those angles at which diffracted orders appear (or disappear). Both Wood and Rayleigh concluded that the anomalies appeared only for (electromagnetic) radiation incident with electric vector perpendicular to the generating element of the reflecting surface (the second boundary value problem) and that for parallel-polarized radiation no such anomalies occurred. Recent work by Palmer[19] has shown that the anomalies can occur for parallel-polarized radiation as well; Palmer concluded however that in this case the anomalies would not appear for shallow surfaces (where the angle ψ is small). The present calculation shows that they are to be expected even for such surfaces, although the effect here is not large, about 5%.

It is to be remarked that the problem of calculating the shape of the anomalies has proved intractible by previous methods. It is seen in Fig. 6 that the anomaly shows a sharp edge on the side where a new order first appears, as is often observed experimentally.[19] Existence of this edge is connected with the fact that the energy contained within an order falls off rapidly as the angle of the order approaches 90° (as the order disappears). In fact it can be shown through the use of a perturbation treatment such as Rayleigh's[2] (the treatment being useful for near grazing incidence) in conjunction with an application of the reciprocity theorem[16] that it is to be expected that the slope of the curve is infinite at this point. Indeed it is just this discontinuity, and its attendant effect upon the other orders through the conservation of energy requirement, that gives rise to the Wood anomalies.

It is of interest to compare the results of the present calculation with those obtained for the same problem using other methods. One might

---

19. C.H. Palmer, Jr., J.Opt. Soc. Am. 42, 268 (1952).

first consider Rayleigh's perturbation treatment. However it turns out that
the method, at least in first order, is not applicable, since one requirement
for its validity is that $k \zeta^M \ll 1$ whereas here $k \zeta^M \sim 1$. Secondly
one might consider using Kirchhoff's approximation;[1] the results obtained
using this approximation are essentially the same as those obtained from
Eckart's[4] and Brekhovskikh's[5] formulations. Kirchhoff's method gives re-
sults which are considerably in error; for example the complex reflection co-
efficient using Kirchhoff's approximation is compared with the corresponding
results using the present formulation in Table I. The surface chosen is
the same as that used in Fig. 6.

TABLE I. A comparison of the results of the Kirchhoff formulation
with those obtained using the variational method for normal inci-
dence.

Theory	Zeroth	Plus first	Minus first	Total energy
Kirchhoff	-0.248+0.720i	0.1900-0.313i	-0.1397+0.1546i	67%
Variational	-0.1875+0.879i	0.297 -0.290i	-0.0916+0.329i	95%

Finally the question of the rate of convergence of the calculation
is taken up. In Fig. 7 are shown the successive approximations to the values
of the reflection coefficients, as each new diffracted wave is introduced in
the calculation. It seems to be reasonable to deduce from the results shown
in Fig. 7 that including more terms (more diffracted inhomogeneous plane
waves) in the calculation is not likely to significantly improve the result.
One then concludes that the residual error arises from the incomplete form of
the representation of the reflected field (as explained in Section II). Hence
further improvement can be expected only through the introduction of images
in the region $\zeta < z \leq 0$. However it seems that for surfaces whose average

absolute slope is small (sections of surface of large slope may be included) and whose maximum displacement is not too many wave lengths, the formulation as presented is accurate to a few per cent.
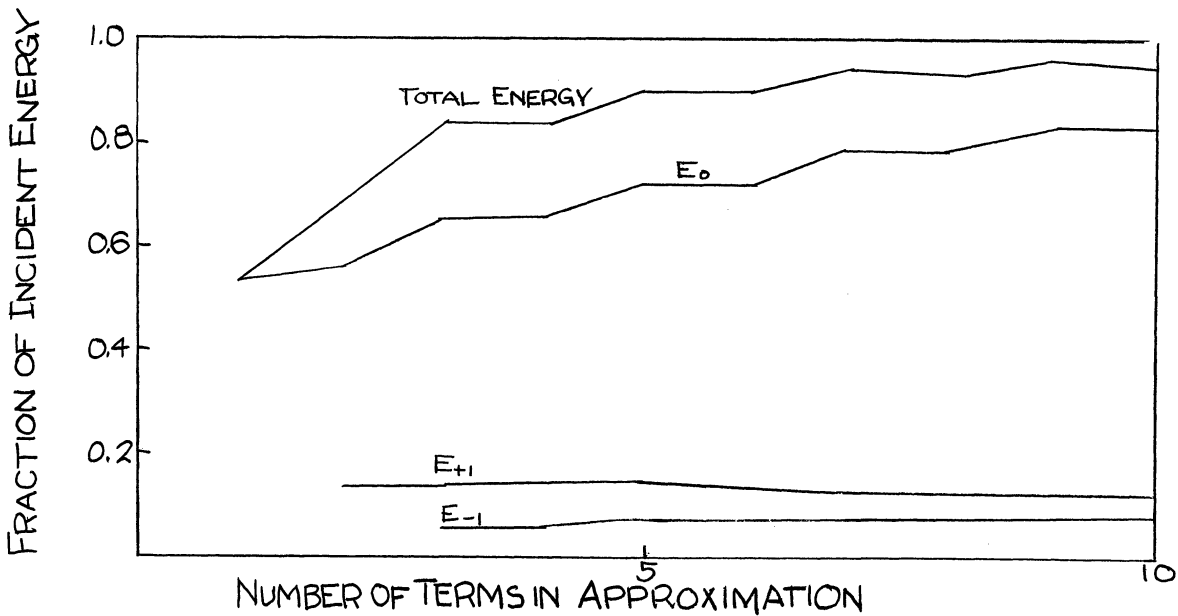

Fig. 7. The graph shows the successive approximations to the energy contained in the various orders appearing when a plane wave is normally incident upon a surface with ψ =10° and with Λ =1.23 λ . The total calculated energy is also shown.

V. ACKNOWLEDGEMENTS

DISTRIBUTION LIST

Chief of Naval Research
Undersea Warfare Branch (Code 466)
Washington 25, D.C.   (1)

Director
Naval Research Laboratory
Technical Information Officer
Washington 25, D.C.   (6)

Commanding Officer
Office of Naval Research Branch Office
Box 39, Navy 100, c/o Fleet Post Office
New York, New York   (2)

Commanding Officer
Office of Naval Research Branch Office
10th Floor
The John Crerar Library Building
86 East Randolph Street
Chicago 1, Illinois   (1)

Chief, Bureau of Ships
Code 847, Navy Department
Washington 25, D.C.   (1)

Office of Naval Research
Acoustics Branch (Code 411)
Washington 25, D.C.   (2)

Director
Woods Hole Oceanographic Institution
Woods Hole, Massachusetts   (1)
        Attn: Dr. C.B. Officer

Director
Marine Physical Laboratory
University of California
U.S. Navy Electronics Laboratory
San Diego 52, California   (1)

Commanding Officer and Director
U.S. Navy Underwater Sound Laboratory
Fort Trumbull
New London, Connecticut   (1)
        Attn: Dr. H.W. Marsh

Director
Naval Ordnance Laboratory
White Oak, Maryland
        Attn: Sound Division

Commanding Officer and Director
U S. Navy Electronics Laboratory
San Diego 52, California   (1)

Superintendent
U.S. Navy Postgraduate School
Physics Department
Monterey, California   (1)
        Attn: Prof. L.E. Kinsler

Commander
Naval Air Development Center
Johnsville, Pennsylvania   (1)

Hudson Laboratories
Columbia University
145 Palisades Street
Dobbs Ferry, New York   (1)
        Attn: Dr. I. Tolstoy

Massachusetts Institute of Technology
Acoustics Laboratory
Cambridge 39, Massachusetts   (1)

Lamont Geological Observatory
Columbia University
Torre Cliffs
Palisades, New York   (1)

NRC Undersea Warfare Committee
Navy Department
Washington 25, D.C.   (1)

Catholic University of America
Department of Physics
Washington 17, D.C.   (1)

Harvard University
Acoustics Laboratory
Division of Applied Science
Cambridge 38, Massachusetts   (1)

Office of Technical Services
Department of Commerce
Washington, D.C.   (1)

Yale University
Edwards Street Laboratory
New Haven, Connecticut   (1)

Commanding Officer
Office of Naval Research Branch Office
1030 E. Green Street
Pasadena 1, California   (1)

Commanding Officer
Office of Naval Research Branch Office
346 Broadway
New York 13, New York   (1)

Armed Services Technical Information Agency
Document Service Center
Knott Building
Dayton 2, Ohio   (5)

Director, Ordnance Research Laboratory
Post Office Box 30
Pennsylvania State University
State College, Pennsylvania   (1)
    Attn: Mr. R.J. Urick

University of Texas
Box 1, Defense Research Laboratory
Austin, Texas   (1)

David Taylor Model Basin
Washington 25, D.C.   (1)

Director
Scripps Oceanographic Institute
La Jolla, California   (1)
    Attn: Dr. C. Eckart

Applied Physics Laboratory
Johns Hopkins University
Baltimore, Maryland   (1)

Director
Underwater Sound Reference Laboratory
Orlando, Florida   (1)

Bureau of Standards
Washington 25, D C.   (1)
    Attn: Mr. Cook

Marine Laboratory
University of Miami
Coral Gables, Florida   (1)

Operations Evaluation Group (Op-374)
Navy Department
Washington 25, D.C.

U.S. Naval Academy
Physics Department
Annapolis, Maryland   (1)

Dr. R. Mittra
Antenna Laboratory
University of Toronto
Toronto 5, Canada   (1)

Dr. C.L. Pekeris
Weizmann Institute
Rehovst, Isreal.   (1)

Physics Department
Brown University
Providence 12, Rhode Island   (1)