

THE UNIVERSITY OF MICHIGAN
COLLEGE OF ENGINEERING
Department of Naval Architecture and Marine Engineering
Ship Hydrodynamics Laboratory

Final Report

HULL FORM DEVELOPMENT AND RESISTANCE AND PROPULSION TEST RESULTS
OF A SERIES OF SHIP HULLS HAVING EXTREME "V" SECTIONS
(Variations in Geometrical Transverse Inertia)

James L. Moss
Hun Chol Kim

Project Director: R. B. Couch

ORA Project 04652

under contract with:

U. S. DEPARTMENT OF COMMERCE
MARITIME ADMINISTRATION
CONTRACT NO. MA-2564, TASK II
WASHINGTON, D.C.

administered through:

OFFICE OF RESEARCH ADMINISTRATION ANN ARBOR

July 1963

TABLE OF CONTENTS

	Page
LIST OF TABLES	v
LIST OF FIGURES	vii
INTRODUCTION	1
LINES DEVELOPMENT	3
TEST RESULTS	8
REFERENCES	11

LIST OF TABLES

Table

I	Propeller Data for 600-Foot (LBP) Ship
II	Ship Model Particulars
A-I	Curves of Form for the Series 60, $C_B = .60$
A-II	Curves of Form for the Series 60, $C_B = .65$
A-III	Curves of Form for the Series 60, $C_B = .70$
A-IV	Curves of Form for the Series 60, $C_B = .75$
A-V	Curves of Form for the Series 60, $C_B = .80$
A-VI	Curves of Form for the U of M "V" Series, $C_B = .60$
A-VII	Curves of Form for the U of M "V" Series, $C_B = .65$
A-VIII	Curves of Form for the U of M "V" Series, $C_B = .70$
A-IX	Curves of Form for the U of M "V" Series, $C_B = .75$
A-X	Curves of Form for the U of M "V" Series, $C_B = .80$
A-XI	Nondimensional Offsets for the U of M "V" Series, $C_B = .60$
A-XII	Nondimensional Offsets for the U of M "V" Series, $C_B = .65$
A-XIII	Nondimensional Offsets for the U of M "V" Series, $C_B = .70$
A-XIV	Nondimensional Offsets for the U of M "V" Series, $C_B = .75$
A-XV	Nondimensional Offsets for the U of M "V" Series, $C_B = .80$

LIST OF FIGURES

Figure

1. Original extreme "V" and extreme "U" proposals, $C_B = .60$.
2. Original extreme "V" and extreme "U" proposals, $C_B = .75$.
3. Composite body plan of $C_B = .60$ Series 60 parent, U of M "V" Series, and intermediate "V" Series.
4. Composite body plan of $C_B = .65$ Series 60 parent and U of M "V" Series.
5. Composite body plan of $C_B = .70$ Series 60 parent and U of M "V" Series.
6. Composite body plan of $C_B = .75$ Series 60 parent and U of M "V" Series.
7. Composite body plan of $C_B = .80$ Series 60 parent and U of M "V" Series.
8. Orthogonal plot of nondimensional load waterlines for Series 60 and the U of M "V" Series.
9. Half-angle of entrance at the load waterline for various hull form series.
10. Orthogonal plot of transverse moment of inertia coefficients at the load waterline for Series 60 and the U of M "V" Series.
11. Orthogonal plot of wetted surface coefficients at the load waterline for Series 60 and the U of M "V" Series.
12. Effective horsepower, shaft horsepower, and propulsive coefficient versus speed in knots for the $C_B = .60$ U of M "V" Series and the DTMB Series 60.
13. Revolutions per minute, wake fraction, and thrust deduction versus speed in knots for the $C_B = .60$ U of M "V" Series and the DTMB Series 60.
14. Effective horsepower, shaft horsepower, and propulsive coefficient versus speed in knots for the $C_B = .65$ U of M "V" Series and the DTMB Series 60.
15. Revolutions per minute, wake fraction, and thrust deduction versus speed in knots for the $C_B = .65$ U of M "V" Series and the DTMB Series 60.

LIST OF FIGURES (Continued)

Figure

16. Effective horsepower, shaft horsepower, and propulsive coefficient versus speed in knots for the $C_B = .70$ U of M "V" Series and the DTMB Series 60.
17. Revolutions per minute, wake fraction, and thrust deduction versus speed in knots for the $C_B = .70$ U of M "V" Series and the DTMB Series 60.
18. Effective horsepower, shaft horsepower, and propulsive coefficient versus speed in knots for the $C_B = .75$ U of M "V" Series and the DTMB Series 60.
19. Revolutions per minute, wake fraction, and thrust deduction versus speed in knots for the $C_B = .75$ U of M "V" Series and the DTMB Series 60.
20. Effective horsepower, shaft horsepower, and propulsive coefficient versus speed in knots for the $C_B = .80$ U of M "V" Series and the DTMB Series 60.
21. Revolutions per minute, wake fraction, and thrust deduction versus speed in knots for the $C_B = .80$ U of M "V" Series and the DTMB Series 60.
22. Propeller efficiency versus speed in knots for the U of M "V" Series and the DTMB Series 60.
23. Open water propeller characteristics for U of M and DTMB propellers used on the $C_B = .60$ models.
24. Open water propeller characteristics for U of M and DTMB propellers used on the $C_B = .65$ models.
25. Open water propeller characteristics for U of M and DTMB propellers used on the $C_B = .70$ models.
26. Open water propeller characteristics for U of M and DTMB propellers used on the $C_B = .75$ models.
27. Open water propeller characteristics for U of M and DTMB propellers used on the $C_B = .80$ models.
- A-1. Orthogonal plot of nondimensional baseline tangent waterlines for Series 60 and the U of M "V" Series.

LIST OF FIGURES (Concluded)

Figure

- A-2. Orthogonal plot of nondimensional 0.25 waterlines for Series 60 and the U of M "V" Series.
- A-3. Orthogonal plot of nondimensional 0.50 waterlines for Series 60 and the U of M "V" Series.
- A-4. Orthogonal plot of nondimensional 0.75 waterlines for Series 60 and the U of M "V" Series.
- A-5. Orthogonal plot of nondimensional load waterlines for Series 60 and the U of M "V" Series.

INTRODUCTION

Under contract with the Society of Naval Architects and Marine Engineers and the Maritime Administration, the Ship Hydrodynamics Laboratory of the Department of Naval Architecture and Marine Engineering of The University of Michigan has developed the lines of a series of systematic hull forms using Series 60 as a parent series. The transverse sections of the new series are of a pronounced "V" shape as opposed to the "U" shape of the parents. Models were built and tested for both EHP and SHP. The results of the tests as well as the geometric properties of the forms are reported herein.

Under the same contracts, but previously reported, (1,2) The University of Michigan built and tested three of the parent Series 60 hulls with apparent good success. A fourth model, that of the Maritime Administration's high speed cargo liner, PD-108, was also built and tested but with notable discrepancies in results as compared with those obtained on a larger model at David Taylor Model Basin.

At the outset careful consideration was given to the selection of model size. It was thought that in order to avoid appreciable propeller scale effect that model propeller diameters should be six inches or greater. Because of the physical size of the towing tank presently available, ship models of greater than 14 feet LBP were not feasible if the blockage effect was to be small. Therefore, all of the above mentioned models were built 14 feet LBP long and the

resulting model propeller diameters were between six and seven inches.

Further analysis of previous results along with analysis of the results reported herein shows evidence of scale effects⁽³⁾. As part of the long-range research program of the Maritime Administration The University of Michigan will test a 17 foot LBP model of the $C_B = .60$ Series 60 parent as well as the "V" form. The results, which will include a blockage correction, will be analyzed for scale effects by comparison with results of tests of the two 14 foot models and the 20 foot model, the latter tested at DTMB. Until the scale effect study is complete, the results in this report should not be considered final.

LINES DEVELOPMENT

The purpose of the current investigation has been set by the Society of Naval Architects and Marine Engineers, H-2 Panel, Task Group VII, as the exploration of the effects of "U" and "V" forms on resistance, propulsion, and stability within and beyond the limits of design currently in practice in the United States. The sectional area curves of the Series 60 parent forms were to be retained (4), and also the parent profiles within practical limits. The criteria were chosen after consideration of the two principal factors in the following. (5)

1. Desirability of reducing the number of variables so as to accentuate the effect of variation in shape of transverse sections, and
2. The paucity of good hull form data in the extreme "V" range.

Inasmuch as the hull forms to be tested fell beyond the category of normal design, the usual method of developing lines from a knowledge of good performance could not be adopted, and the development of lines of the "V" forms was carried to the practical extremity of fairing lines drawings. The first proposal by the Maritime Administration included extreme "V", moderate "V" or "U" lines for each of the two hull forms initially chosen for the investigation, i. e., hulls of $C_B = .60$ and $.75$. Figs. 1 and 2 show the extreme "U" and "V" sections as originally advanced for the above. However, upon further discussion, it was decided to exclude the extreme "U" lines from the present investigation as the parent series is

already quite "U" in section shape.

Thus for the $C_B = .60$ and $.75$ hulls, extreme "V" and moderate "V" lines were developed the body plans of which are shown in Figs. 3 and 6.

In developing extreme "V" lines for the remaining hulls, mathematical means were discarded and the following geometric method was adopted. Fig. 8 shows a nondimensional plot of load waterlines of all Series 60 parents and two extreme "V" models and is typical of many such curves prepared for the cross-fairing. By connecting offsets at various stations, a surface representing the waterlines of the parent model is generated. This is a three-dimensional surface and it is faired. A similar surface representing the waterlines of the extreme "V" forms follows the parent surface but should include the two hulls already developed and the surface must likewise be a faired one. The second surface is sketched in and offsets are read off. Lines drawings for the other block models are drawn up using the offset obtained above. If the obtained offsets are unsatisfactory for fairing lines, the surface is modified and the procedure is repeated. All such surfaces actually used in the development are included in the Appendix in Figs. A-1 through A-5. It is to be noted that these plots can be used to obtain nondimensional offsets for a hull of any block coefficient. Nondimensional offsets are given in the Appendix in Tables A-XI through A-XV. Figs. 4, 5, and 7 show the body plans of the remaining hull forms as developed by the method just explained.

The sectional area curves of the original series have been well

preserved, although at the stem and stern a small portion of the lines had to be faired irrespective of the sectional area curve. The resulting discrepancy is very small and need not be of concern from a practical standpoint.

In developing the stern lines the extent of the "V" shape near the load waterline was not made as pronounced as originally proposed. Although the load waterlines may still be considered as conforming to the general extreme "V" class of "V" hull shape, reduction of the half-breadths made possible development of moderately deep "U" shaped sections immediately forward of the propeller aperture, a design consideration which is desirable in that a more uniform wake field and less vibration may result. Moderate "V" forms diminished, i. e., with load waterlines about midway between those of the series developed and the parent series, and as developed for the $C_B = .60$ and $.75$ models in Figs. 3 and 6, have not been included in the present testing program.

An effort has been made to retain the waterline length of the parents. Occasionally, however, a slight change in the profile is introduced in fairing, but since it is small, changes in waterline length may be assumed nonexistent.

Above the load waterlines each hull was developed so as to form a deck with nearly the same area as that of the corresponding parent because the deck area of either a "U" or "V" form depends largely upon the intended service which is not known. Therefore, it seemed best to conform to the parent deck areas. Had a knuckle been introduced immediately above the load waterline, even more extreme "V"

sections could have been developed. Adoption of such a procedure would have resulted in a higher vertical prismatic coefficient.

Most foreign ships of "V" form have a rather pronounced cut-away at the forefoot, sometimes extending as far aft as Station 2 (1/10 LBP). Modern American practice is to have a plumb bow for deep "U" forms. The parent models have an arbitrary bow profile which is the same for all Series 60 hulls. The effect of cutting away the forefoot is not well understood, although it is easy to understand that partial removal of the forefoot might improve maneuverability and course stability. Changes in resistance were expected to be small ⁽⁶⁾. The $C_B = .60$ and $.75$ models were tested for resistance with both the parent profile and the forefoot cut away. The results confirmed that changes in resistance were negligible so that, consequently, the remaining lines were developed retaining the parent profiles.

To follow the trend of half angle of entrance of the parent would have made the angle of entrance for the extreme "V" series quite excessive on the large block models. Fig. 9 shows the half angles of entrance at the load waterlines for various well known series. After some discussion the H-2 panel adopted the angles as indicated in the same figure for the present series. It should be noted that the parent series is increasingly "V" shaped for fuller forms. Hence, the trend of the curve of half angle of entrance versus block coefficient, Fig. 9, of the present series is quite natural if one compares with the other hull form series.

Curves of form for Series 60 parent and the U of M "V" series are included in the Appendix, Tables A-I through A-X. In general, these calculations check closely to those of DTMB. The main discrepancy was in vertical prismatic coefficient and is indicated in Fig. 10. Also, a small difference in block coefficient of the $C_B = .65$ hull was noted. Bonjean's curves are tabulated at the end of each curves of form.

Fig. 10 has been constructed from the curves of form to show the variations in transverse waterplane inertia. The three dimensional surface indicates a smooth variation in vertical prismatic and the transverse waterplane inertia. Similar curves for other variables may be plotted as Fig. 11 shows the wetted surface variations which, due to change in hull form, are not appreciable.

TEST RESULTS

Table I lists the geometric properties of the UM propeller models and compares them with those of the parent propeller models. There were slight discrepancies in pitch owing to model construction inaccuracies which would affect full scale RPM predictions and also the open water characteristics.

Table II lists the particulars of the ship models.

The results of the resistance and self-propulsion tests are given in Figs. 12 through 21 for a 600 foot LBP ($\lambda = 42.857$) ship. Open water propeller characteristics are given in Figs. 23 through 27. In addition, propeller efficiency versus ship speed is plotted in Fig. 22. In all the above mentioned figures results obtained at DTMB from the parent Series 60 and propeller models are also plotted.

In general, predicted EHP was higher for the "V" forms than for the parents throughout the speed range except that at high speeds the $C_B = .60, .65, \text{ and } .80$ "V" forms had decreased resistance over that of the parents. The increases were the greatest for the hulls of medium fullness, being less for the finest and fullest block models.

The differences in EHP are reflected in SHP, but additionally the shaft horsepower increased owing to decreased propeller efficiency or decreased hull efficiency which gave a lower value

of overall propulsion efficiency. Again, the greatest difference occurred for the $C_B = .70$ form.

Since the largest differences between the parent and "V" hull form were observed for the $C_B = .70$ hull, those results warrant detailed discussion. Similar analyses could be made for the other block models. At 18 knots, or a speed-length ratio of about .75, the effective horsepower increased by 13 percent and the shaft horsepower by 45 percent whereby the propulsive coefficient decreased from .76 to .60, or 21 percent. See Fig. 16. In Fig. 22 the propeller efficiency dropped from 67 to 61 percent, or a decrease of 9 percent. Therefore, had the propeller used been as efficient behind the "V" form model as it was behind the parent, the P. C. would have decreased about 12 percent instead of 21. That is, the parent propeller design was not as nearly optimum in combination with the "V" hull, or had another propeller been designed from wake survey information, or otherwise, lower shaft horsepower results would have been obtained. In addition, referring to Fig. 25, the U of M Propeller No. 10 had slightly lower efficiency than the parent DTMB Propeller No. 3376 in the operating range of advance coefficient so that not quite all of the decrease in propeller efficiency shown in Fig. 22 is the result of having less than an optimum propeller design for the "V" hull.

There remains approximately 11 percent in propulsive coefficient as yet unaccounted for. Fig. 17 shows an abnormally high thrust deduction which, when combined with an only slightly higher wake fraction than that obtained on the parent model, yields a substantially lower hull efficiency. However, it should be noted that the

relative rotative efficiency at a speed corresponding to 18 knots was 1.01 which indicates that serious propeller scale effects in the self-propulsion test were lacking, and therefore, should not be considered as a possible cause of the large differences just discussed.

The differences in SHP and other propulsion components between the "U" form and the "V" form for the finer hulls seems excessive and it is believed reflects some scale effects not understood. This being the case this report is not considered to be a final statement of accurate results for at least the finer hulls. Further investigation of this problem is being made and will be reported at a later date under a different task number.

REFERENCES

1. F. C. Michelsen, R. B. Couch, H. C. Kim, "Resistance and Propulsion Tests on Two Series 60 Models", The University of Michigan, Department of Naval Architecture and Marine Engineering, Report 03509-1-F, April 1961.
2. F. C. Michelsen, R. B. Couch, H. C. Kim, "Resistance and Propulsion Test Results on Two Models: 1. Series 60, $C_B = .80$, 2. High Speed Cargo Ship PD 108-S5-0". The University of Michigan, Department of Naval Architecture and Marine Engineering, Report 04652-1-F, March 1962.
3. H. C. Kim, J. L. Moss, "Research in Resistance and Propulsion: Part III. Blockage Correction in a Ship Model Towing Tank and Scale Effect on Propulsive Parameters". The University of Michigan, Department of Naval Architecture and Marine Engineering, Report 04542-3-F, March 1963.
4. F. H. Todd, "Some Further Experiments of Single Screw Merchant Ship Forms--Series 60". TSNAME, vol. 61, 1953.
5. Minutes of Task Group VII, Panel 2, Hydrodynamics Committee, SNAME, January 12, 1960.
6. See, for instance, Edstrand, Freimanis, and Lindgren, Experiments with Tanker Models, I, Goteborg, Sweden, 1953, Report No. 23, Fig. 9.

TABLE II

SHIP MODEL PARTICULARS

MODEL NO.	924	959	958	952	966
Ship C_B	.60	.65	.70	.75	.80
LBP(ft)	600	600	600	600	600
LWL(ft)	610.048	610.048	610.048	610.048	610.048
B(ft)	40.0	41.379	42.859	44.446	46.155
H(ft)	31.996	33.104	34.290	35.551	36.931
Δ (tons)	26,331	30,433	35,275	40,658	46,711
WS(sq ft)	62,166	66,449	71,799	77,317	84,313
Model					
$\lambda=42.857$					
LBP(ft)	14.000	14.000	14.000	14.000	14.000
LWL(ft)	14.235	14.235	14.235	14.235	14.235
B(in)	22.399	23.171	23.999	24.89	25.848
H(in)	8.959	9.269	9.601	9.954	10.344
∇ (cu ft)	11.708	13.532	15.684	18.078	20.769
WS(sq ft)	33.846	36.178	39.091	42.095	45.904
A (sq ft)	1.361	1.465	1.578	1.533	1.857
LE/LBP	0.50	.472	.410	.350	.290
LX/LBP	0	.035	.119	.210	.300
LR/LBP	0.50	.493	.471	.440	.410
C _X	.977	.982	.986	.989	.994
C _p	.614	.661	.710	.759	.805
C _{PF}	.581	.651	.721	.792	.861
C _{PA}	.646	.672	.698	.721	.750
C _{PF}	.581	.630	.660	.704	.761
C _{PR}	.646	.667	.680	.686	.695
C _{pV}	.774	.803	.831	.851	.871
C _w	.741	.807	.843	.882	.918
C _{IT}	.586	.678	.732	.793	.844
$\frac{1}{2} \alpha$ E (deg)	12.0	17.0	25.0	36.0	57.5
LCB(%LBP)	-1.500	-.500	+.490	+1.490	+2.540
L/B	7.500	7.230	7.000	6.750	6.500
B/H	2.500	2.500	2.500	2.500	2.500
$L/\nabla^{1/3}$	6.156	5.869	5.593	5.335	5.092
$S/\nabla^{2/3}$	6.564	6.350	6.240	6.080	6.040
$K R = R/\sqrt{BH}$.229	.205	.181	.153	.118

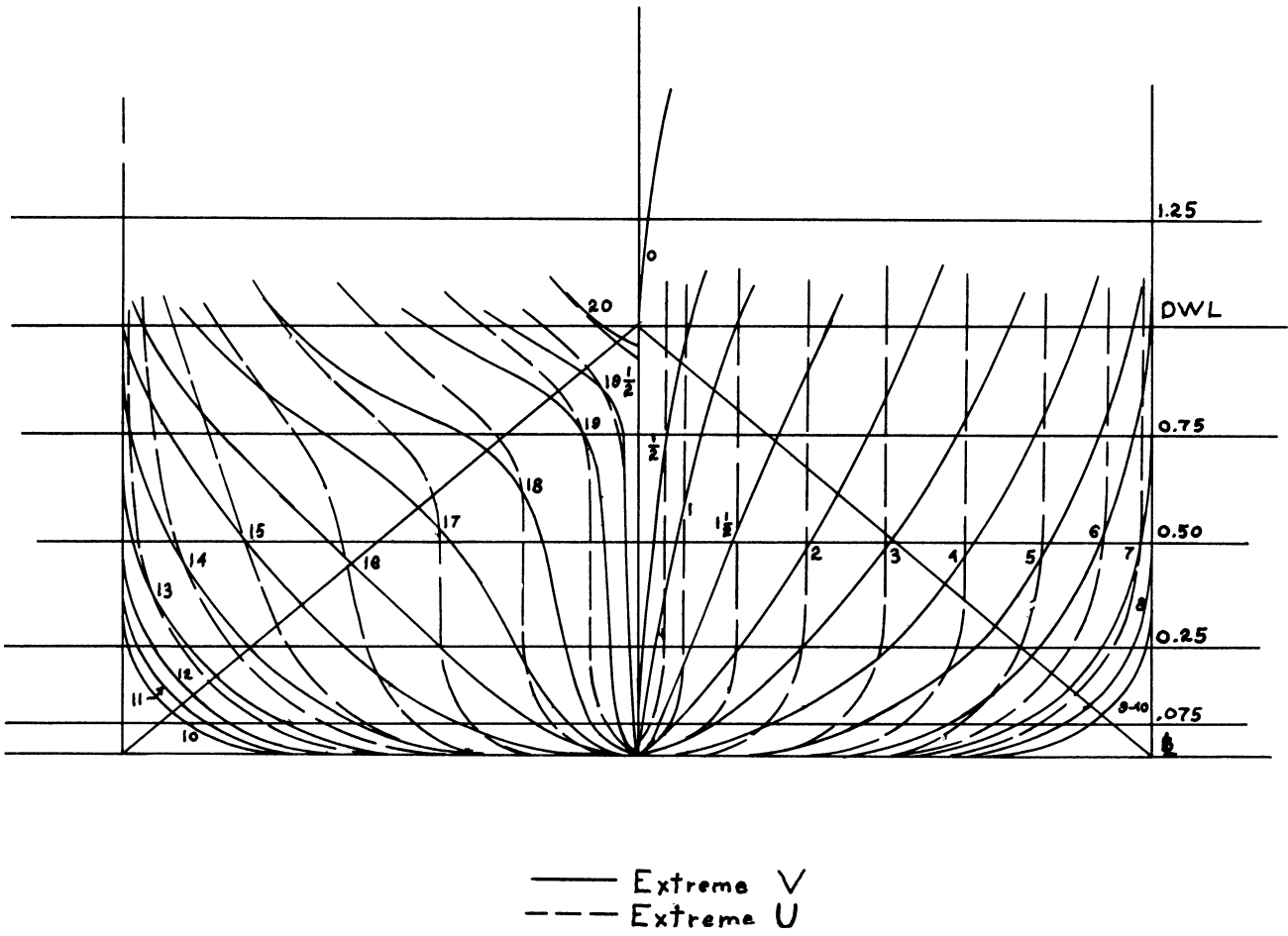


Fig. 1. Original extreme "V" and extreme "U" proposals, $C_B = .60$.

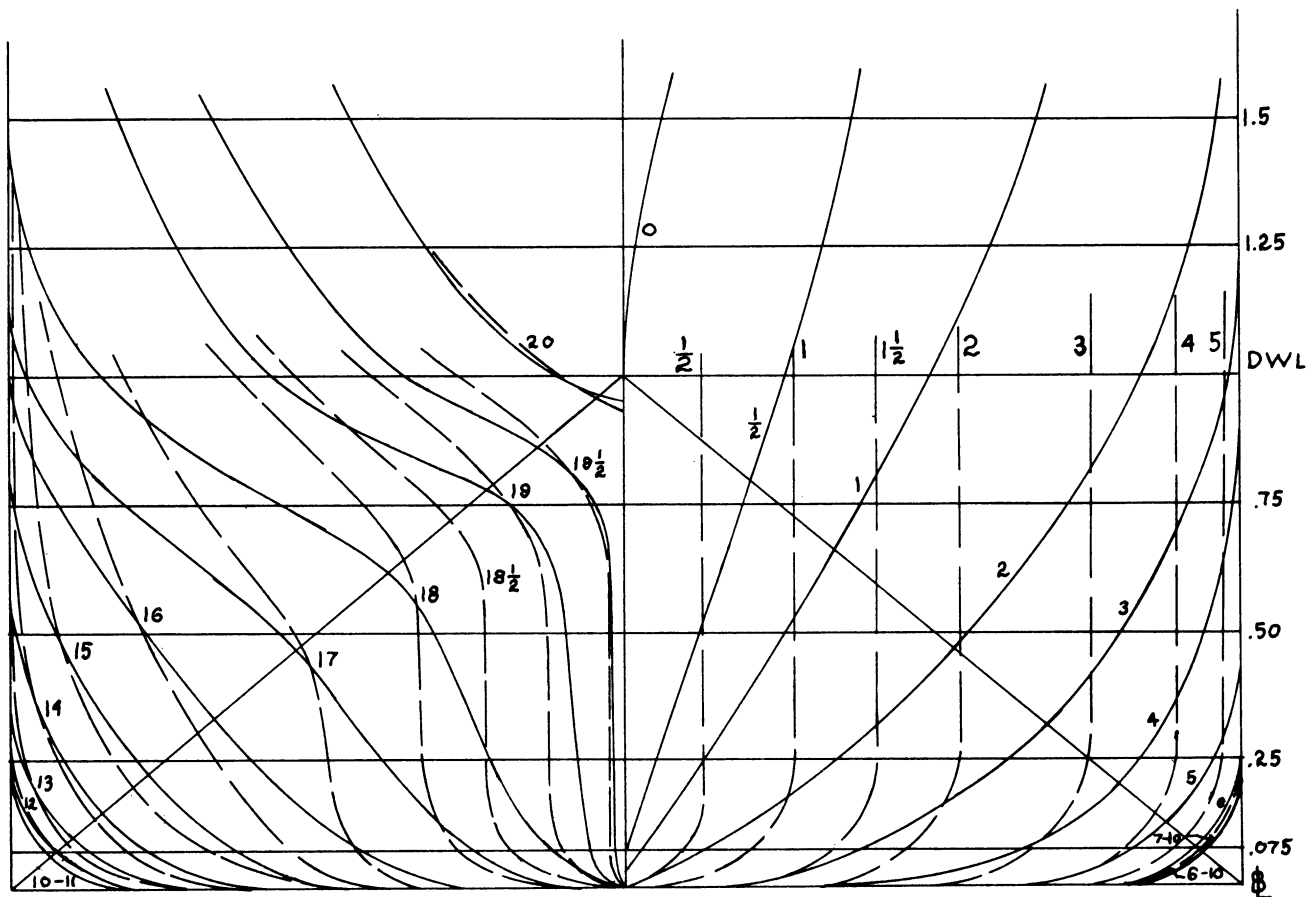


Fig. 2. Original extreme "V" and extreme "U" proposals, $C_B = .75$.

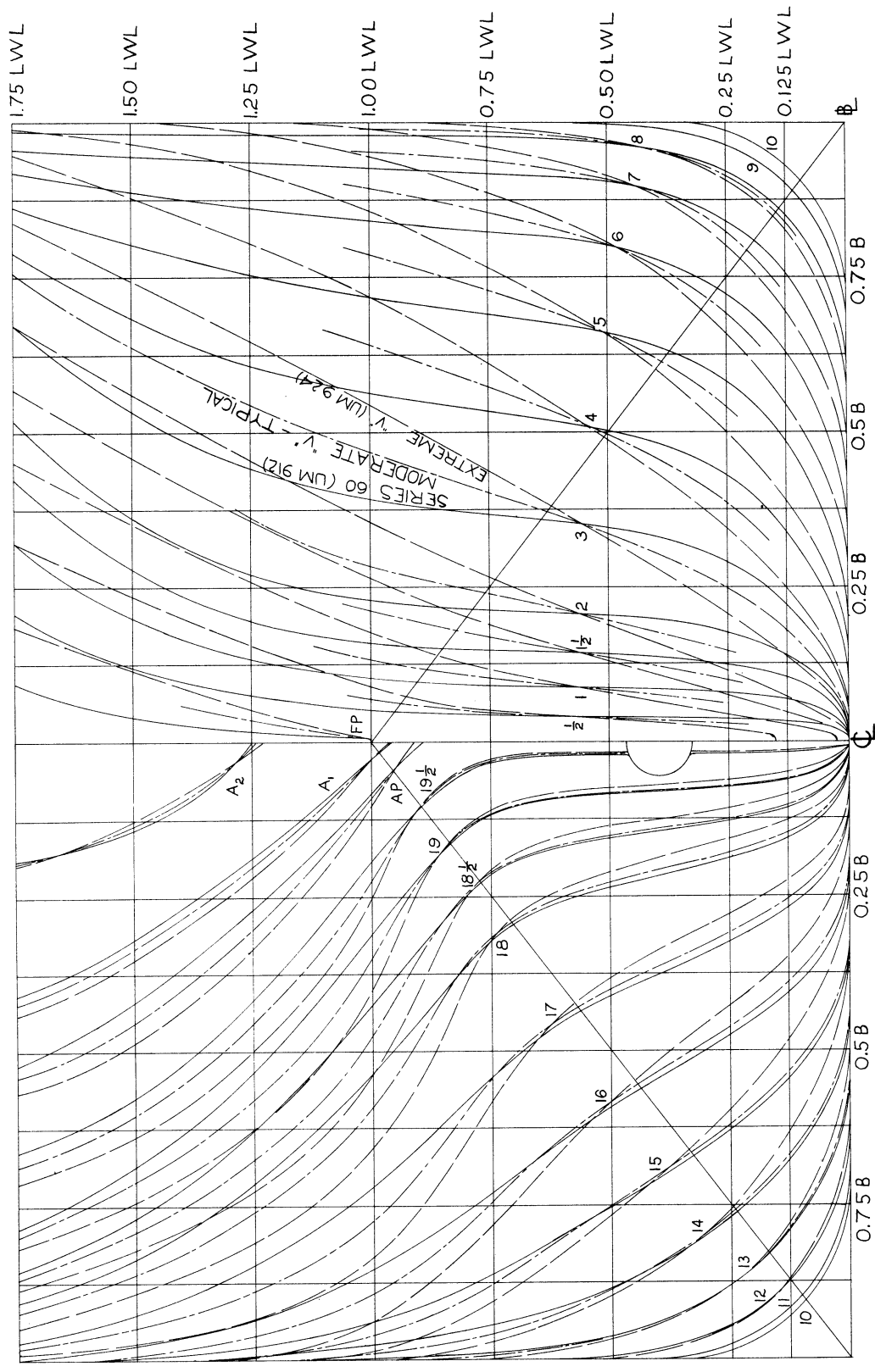


Fig. 3. Composite body plan of $C_B = .60$ Series 60 parent, U of M "V" Series, and intermediate "V" Series.

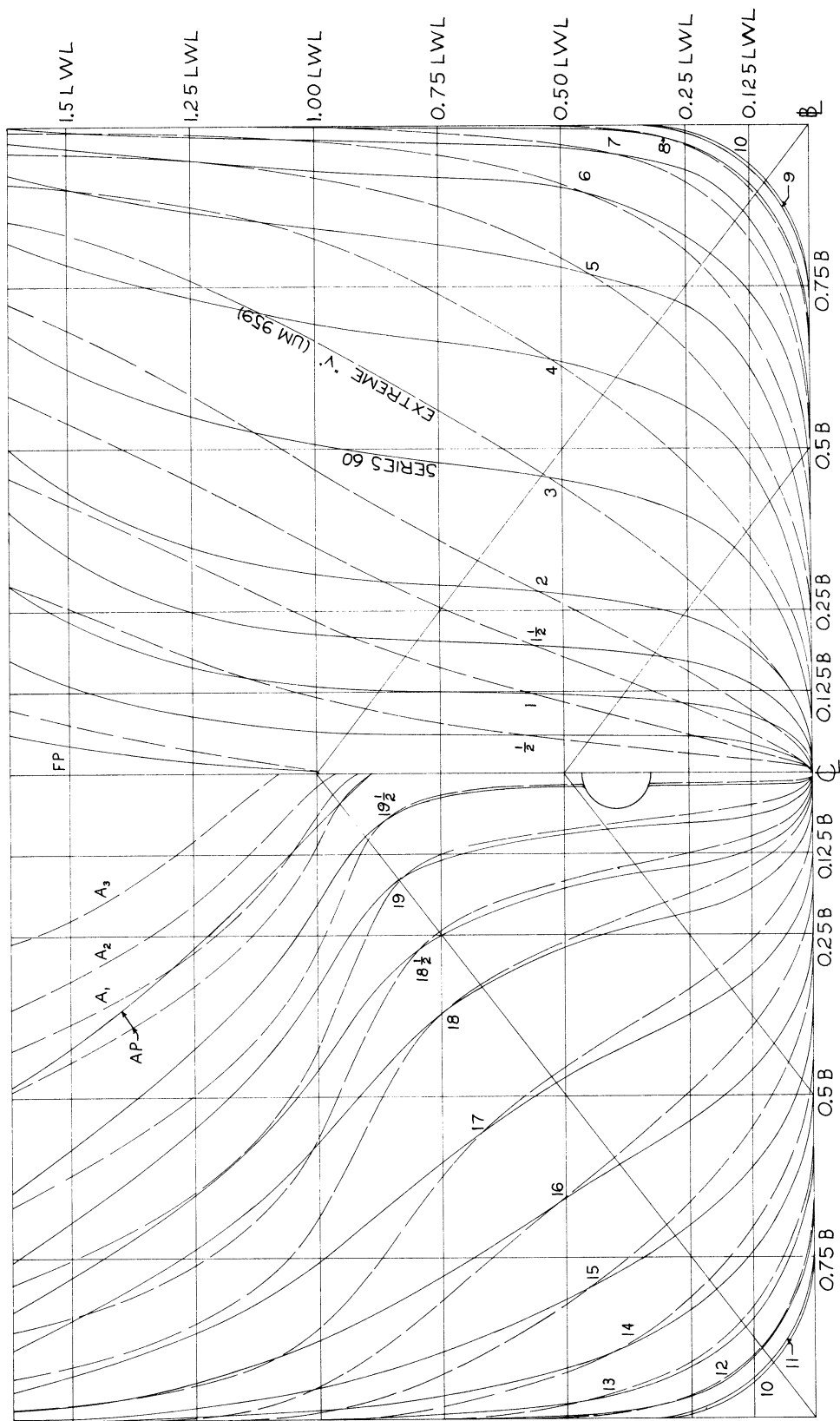


Fig. 4. Composite body plan of $C_B = .65$ Series 60 parent and U of M "V" Series.

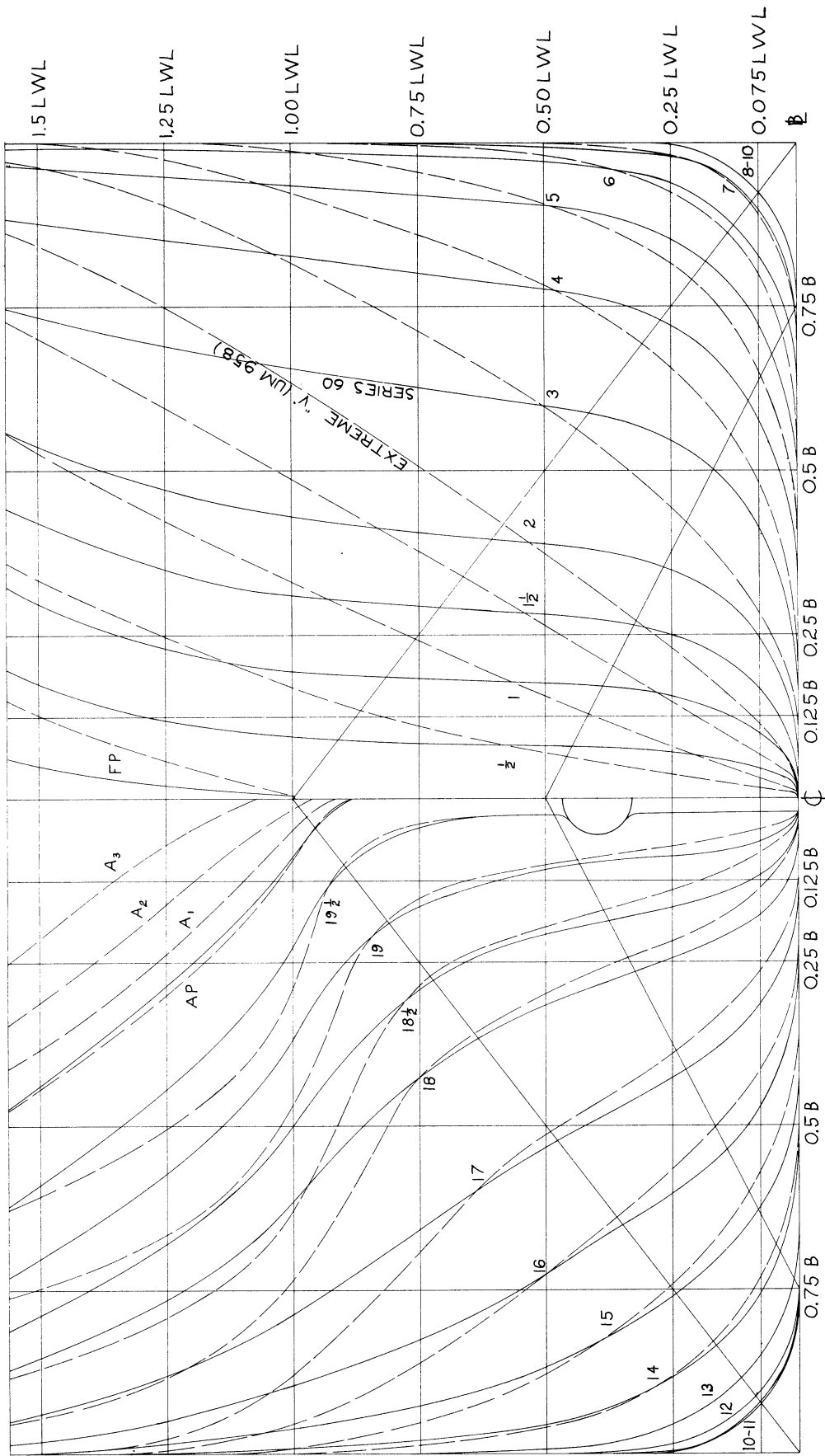


Fig. 5. Composite body plan of $C_B = .70$ Series 60 parent and U of M "V" Series.

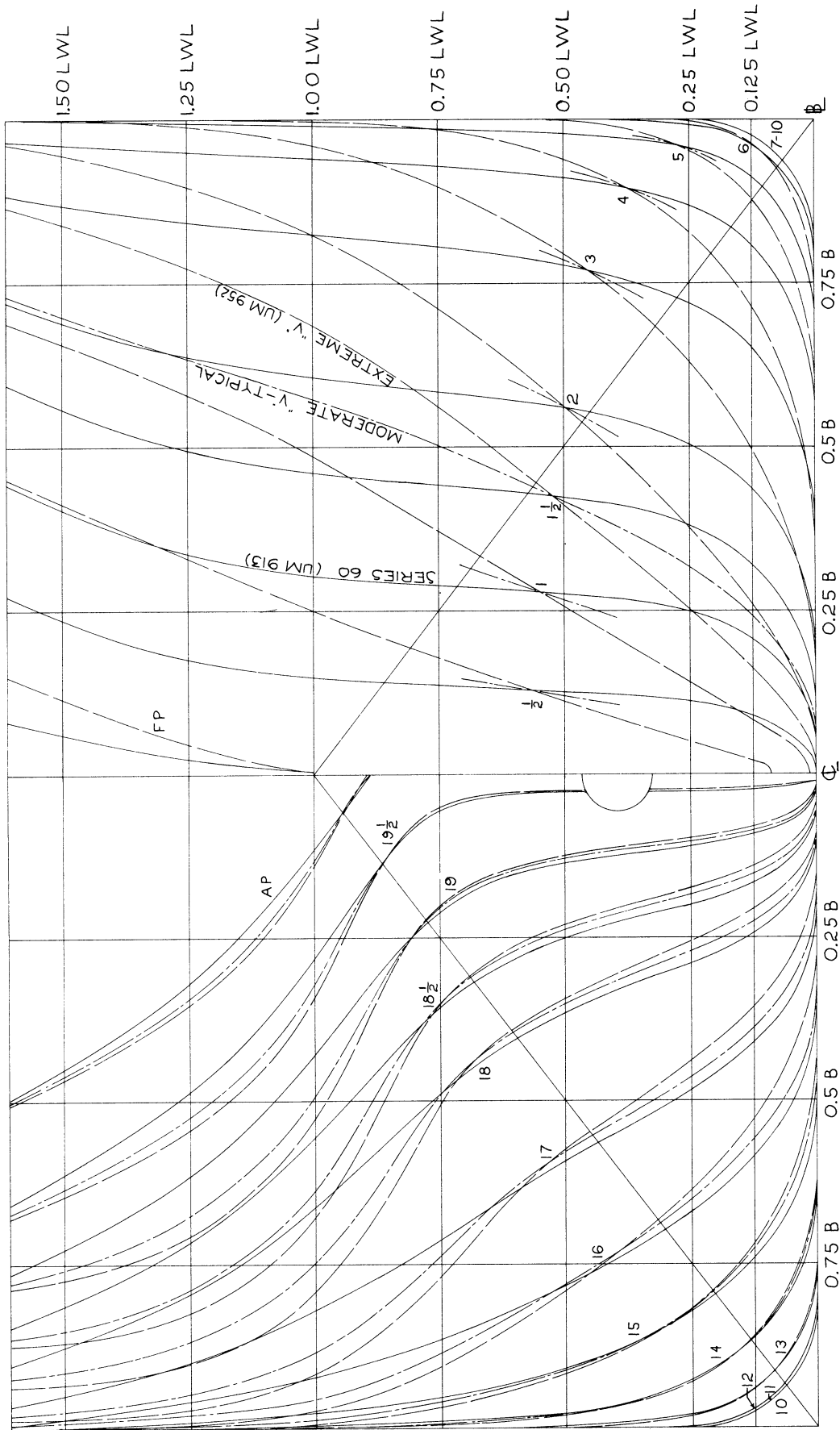


Fig. 6. Composite body plan of $C_B = .75$ Series 60 parent and U of M "V" Series.

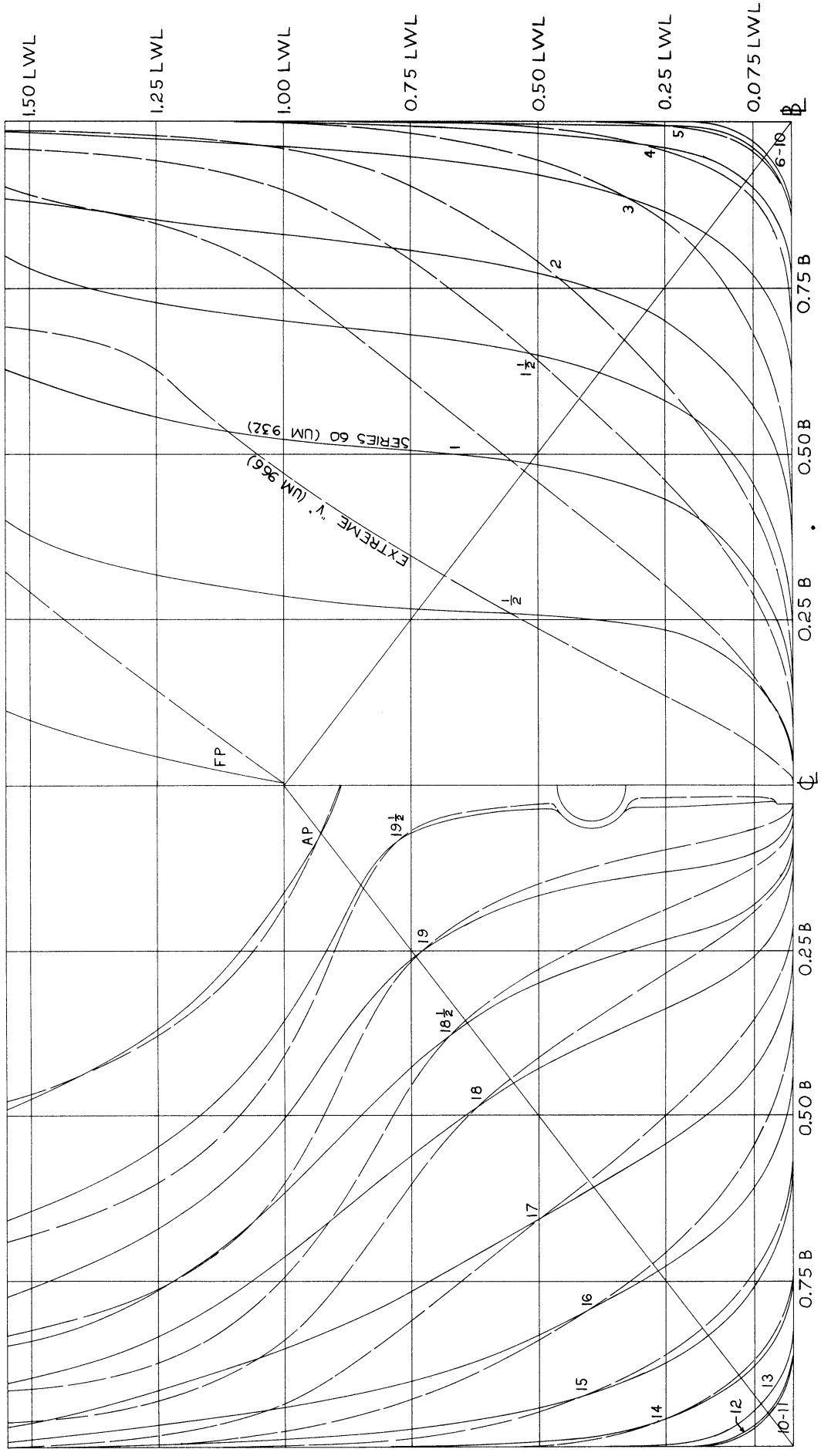


Fig. 7. Composite body plan of $C_B = .80$ Series 60 parent and U of M "V" Series.

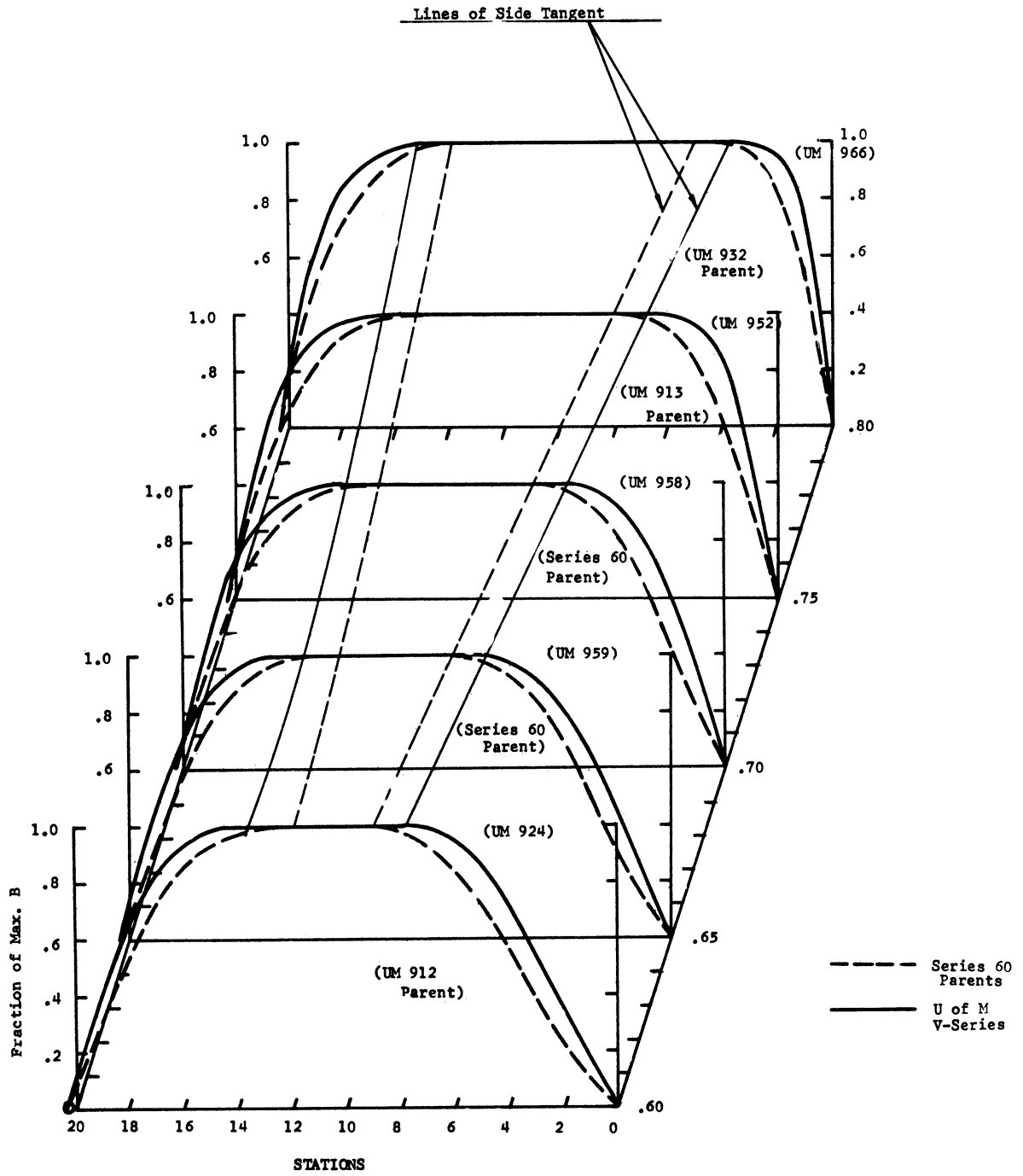


Fig. 8. Orthogonal plot of nondimensional load waterlines for Series 60 and the U of M "V" Series.

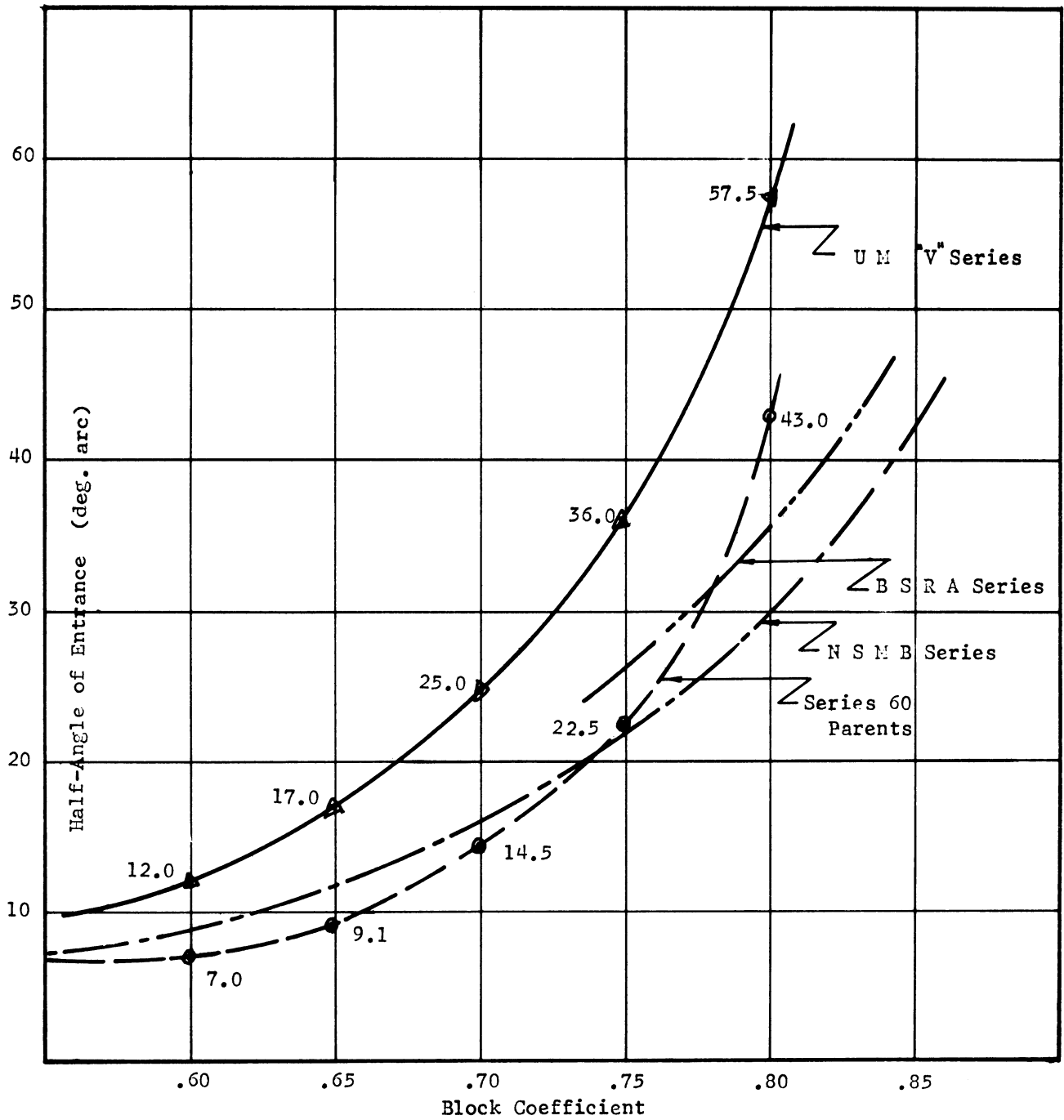
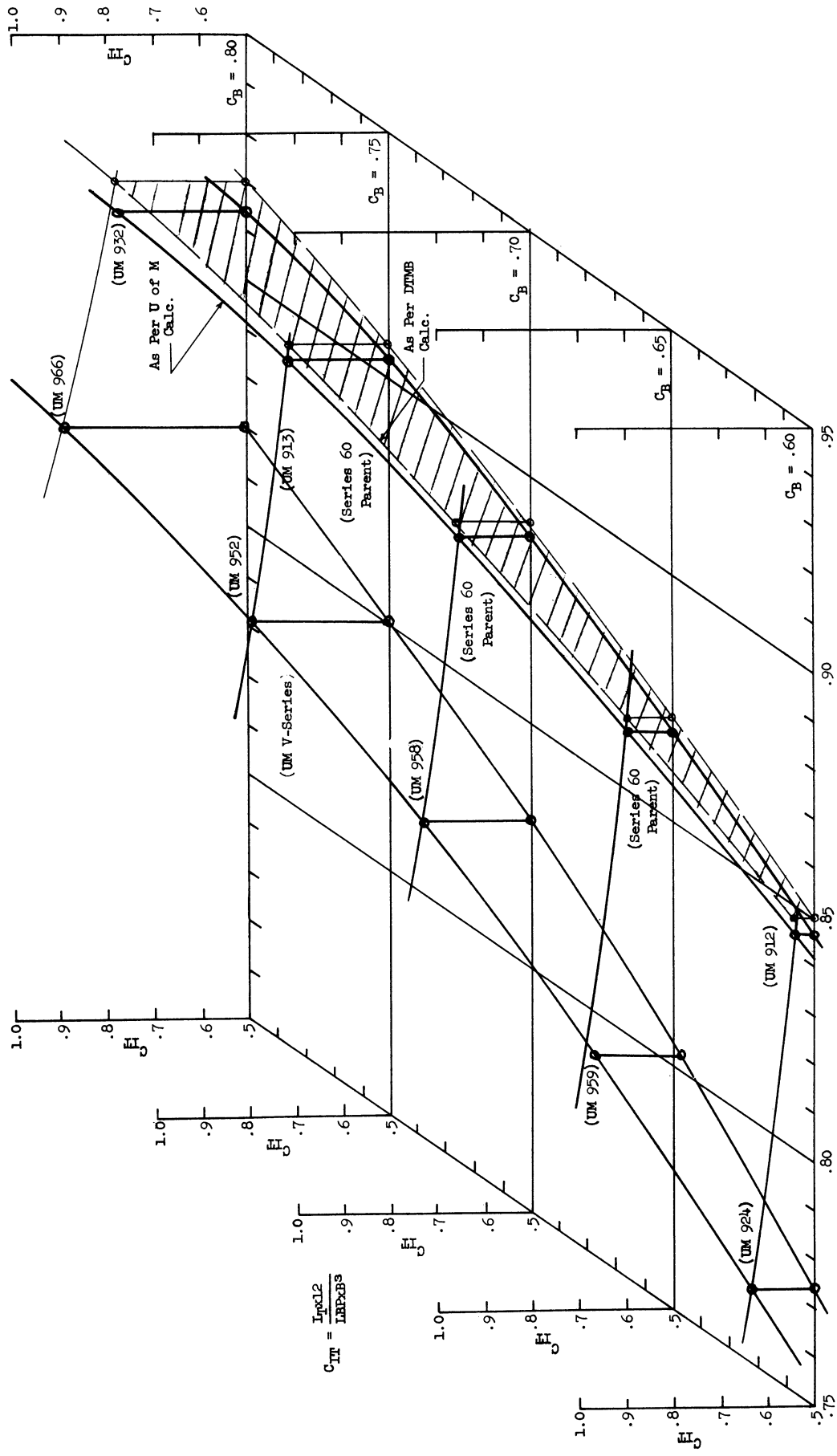
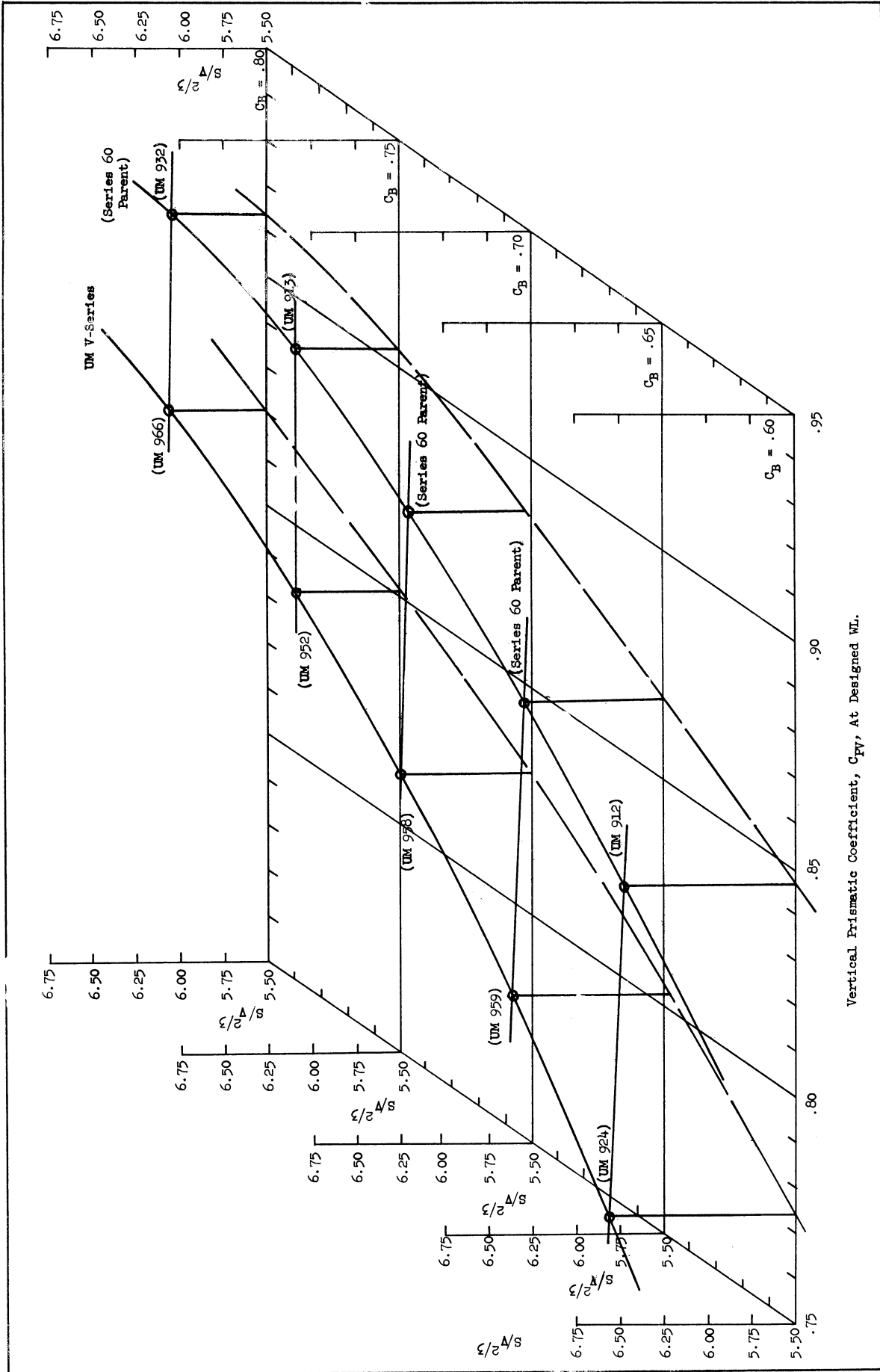


Fig. 9. Half-angle of entrance at the load waterline for various hull form series.



Vertical Prismatic Coefficient, C_{PV} , At Designed WL.

Fig. 10. Orthogonal plot of transverse moment of inertia coefficients at the load waterline for Series 60 and the U of M "V" Series.



Vertical Prismatic Coefficient, C_{pv} , At Designed WL.

Fig. 11. Orthogonal plot of wetted surface coefficients at the load waterline for Series 60 and the U of M "V" Series.

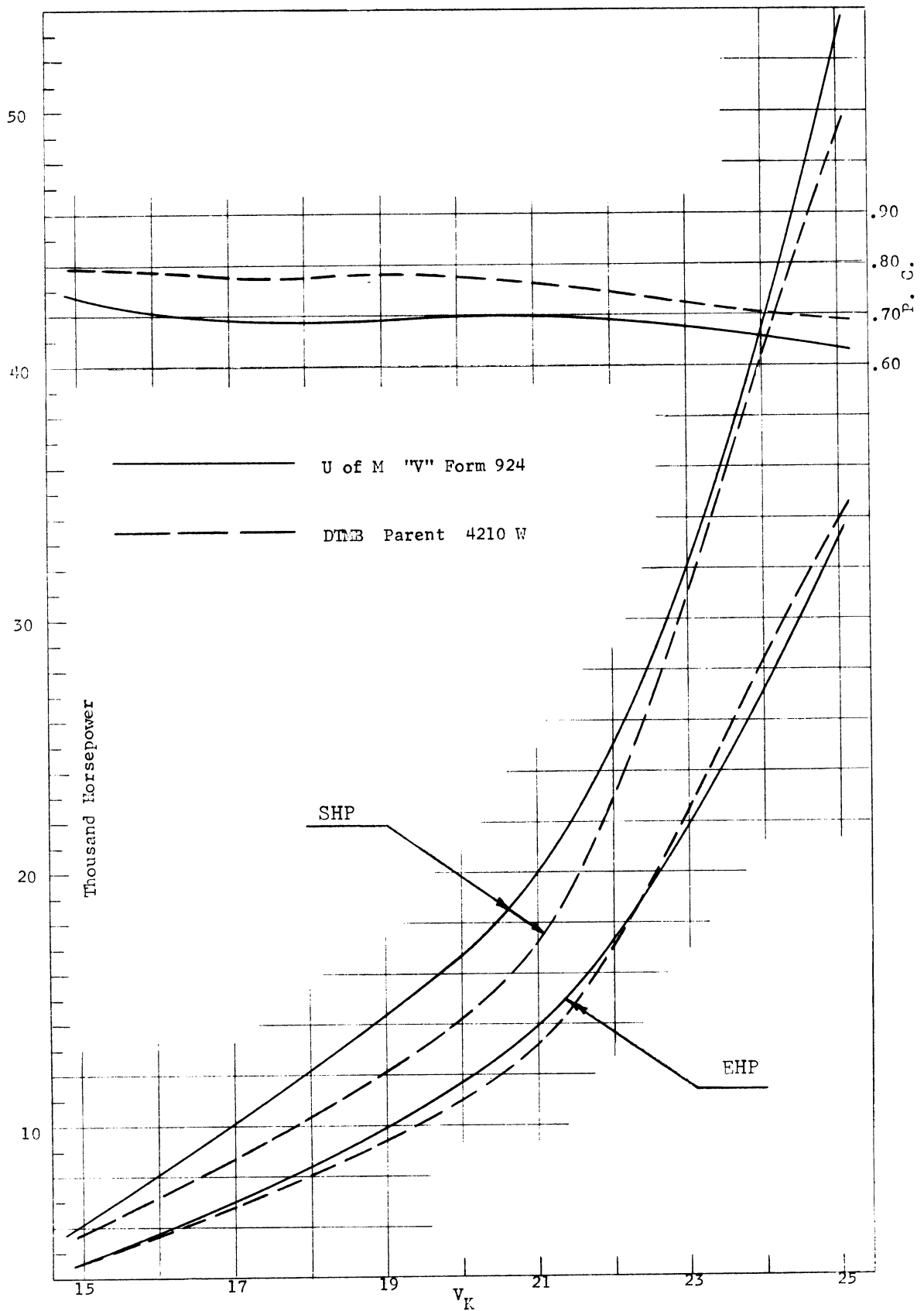


Fig. 12. Effective horsepower, shaft horsepower, and propulsive coefficient versus speed in knots for the $C_B = .60$ U of M "V" Series and the DTMB Series 60.

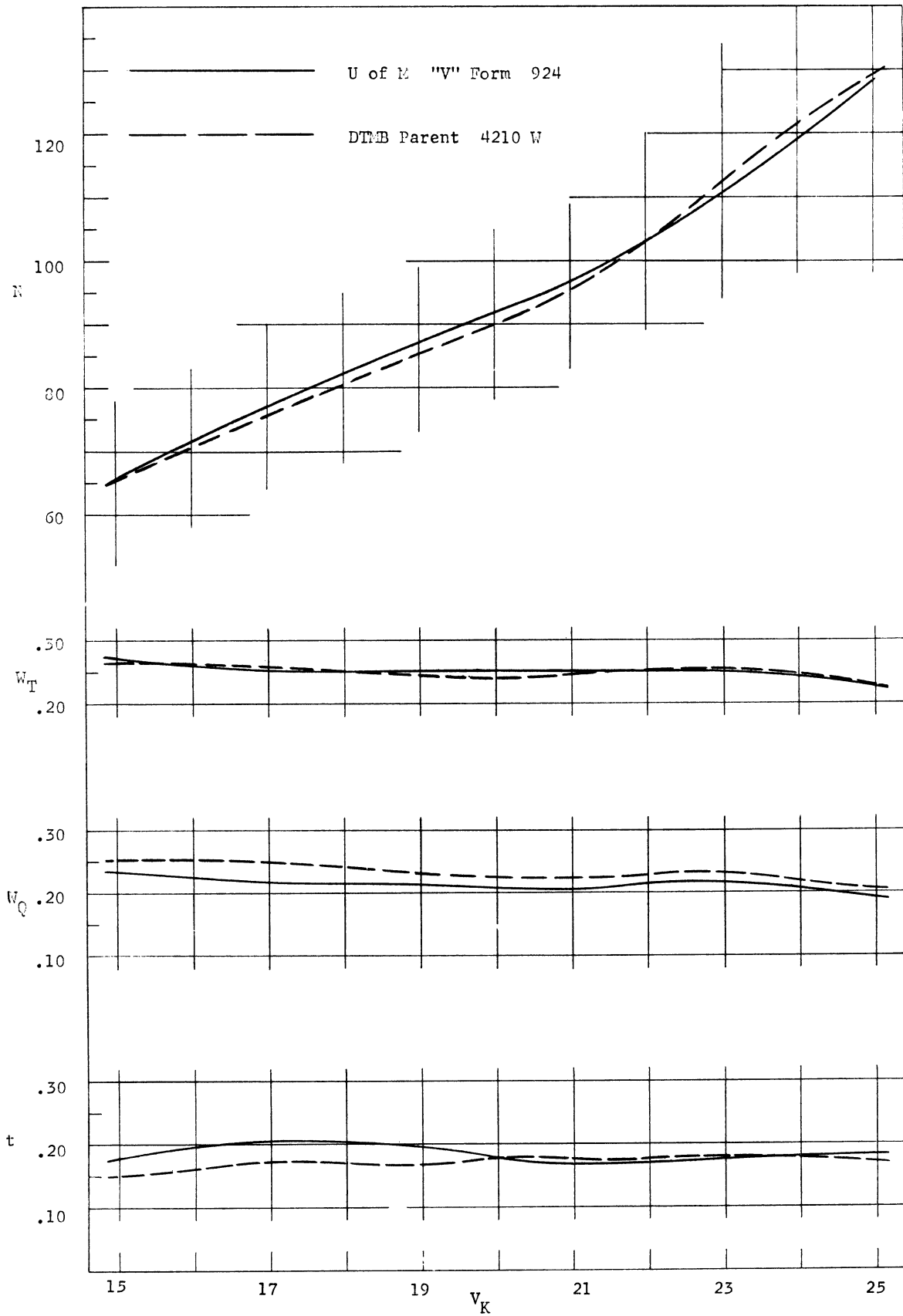


Fig. 13. Revolutions per minute, wake fraction, and thrust deduction versus speed in knots for the $C_B = .60$ U of M "V" Series and the DTMB Series 60.

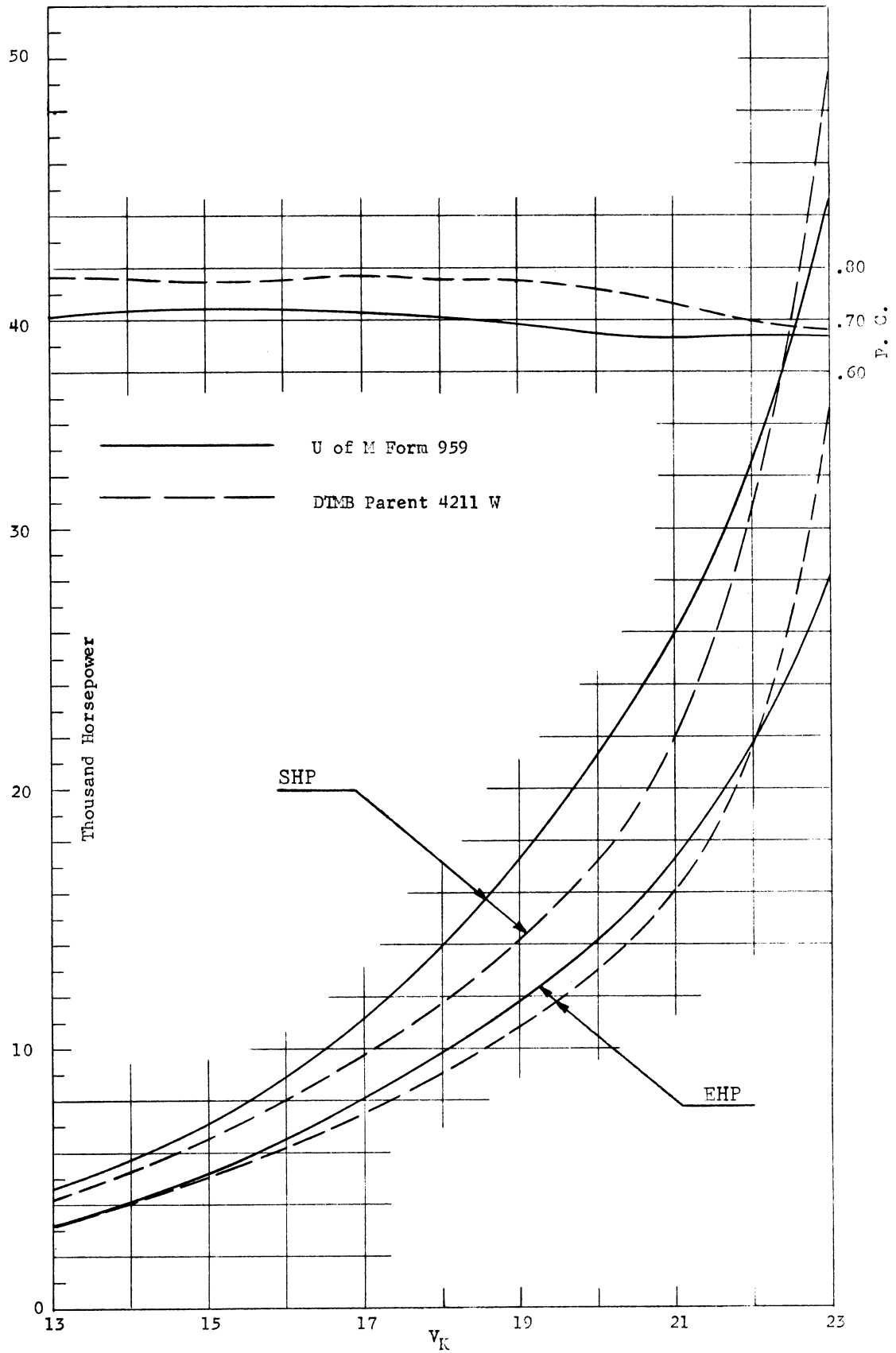


Fig. 14. Effective horsepower, shaft horsepower, and propulsive coefficient versus speed in knots for the $C_B = .65$ U of M "V" Series and the DTMB Series 60.

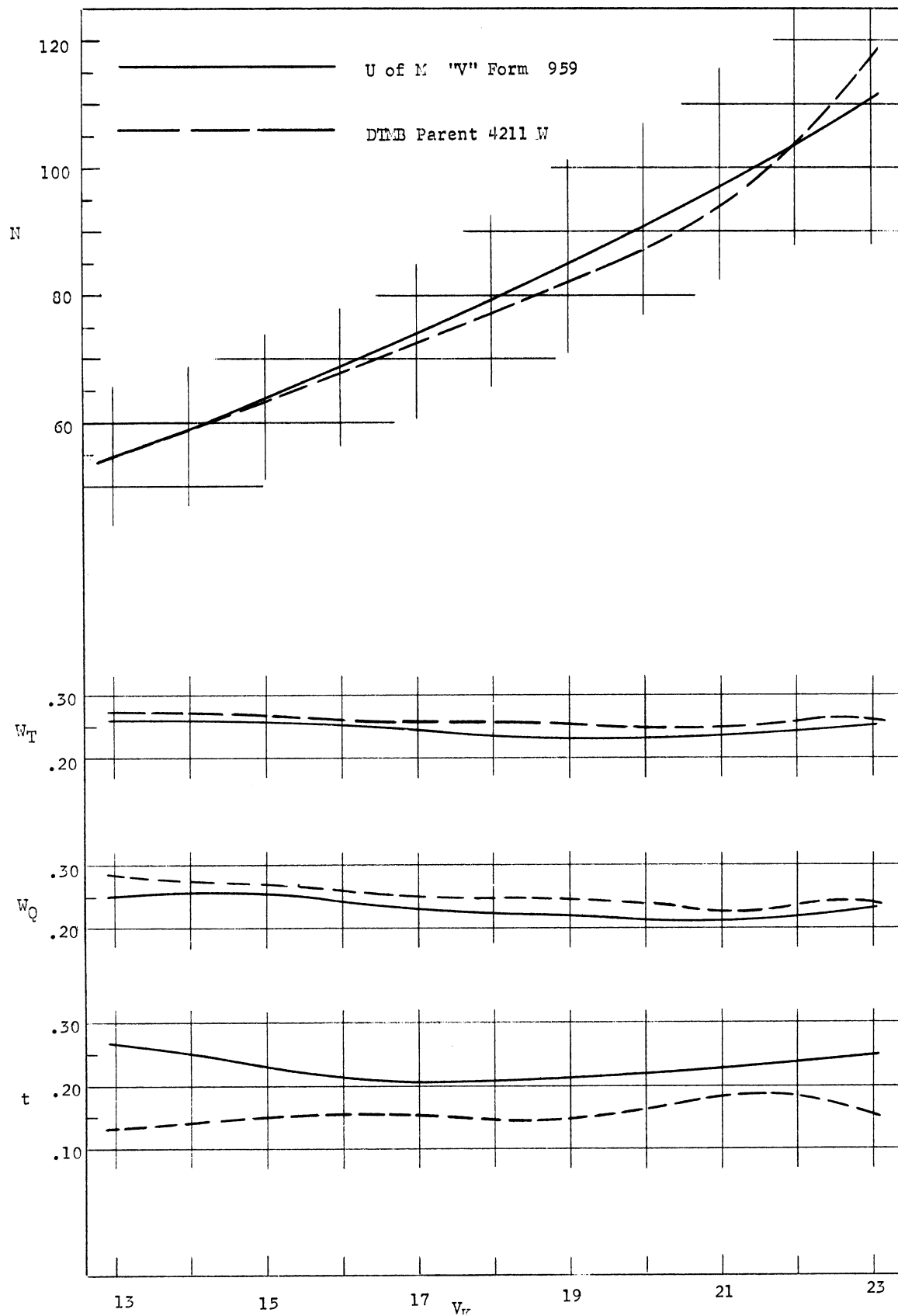


Fig. 15. Revolutions per minute, wake fraction, and thrust deduction versus speed in knots for the $C_B = .65$ U of M "V" Series and the DTMB Series 60.

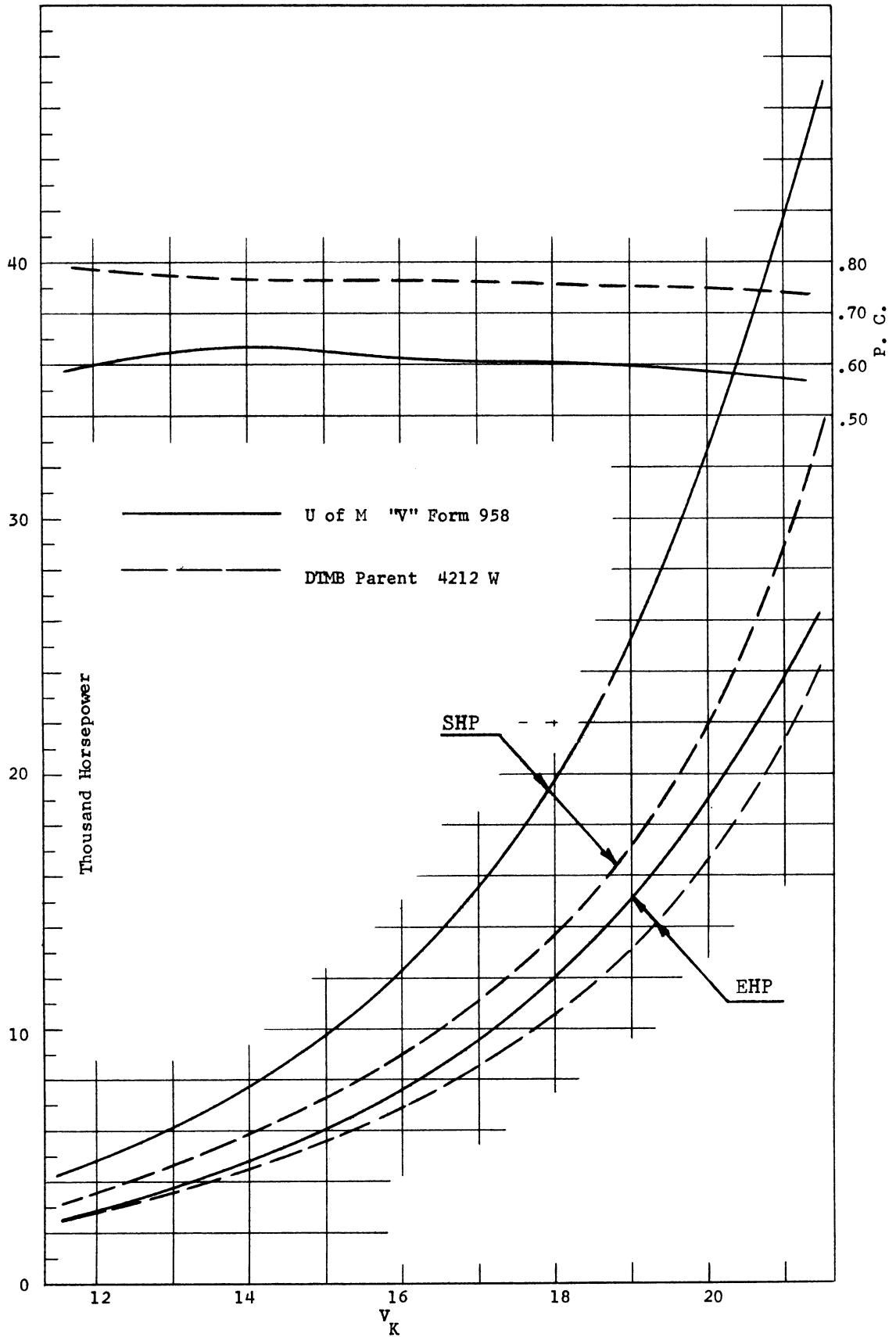


Fig. 16. Effective horsepower, shaft horsepower, and propulsive coefficient versus speed in knots for the $C_B = .70$ U of M "V" Series and the DTMB Series 60.

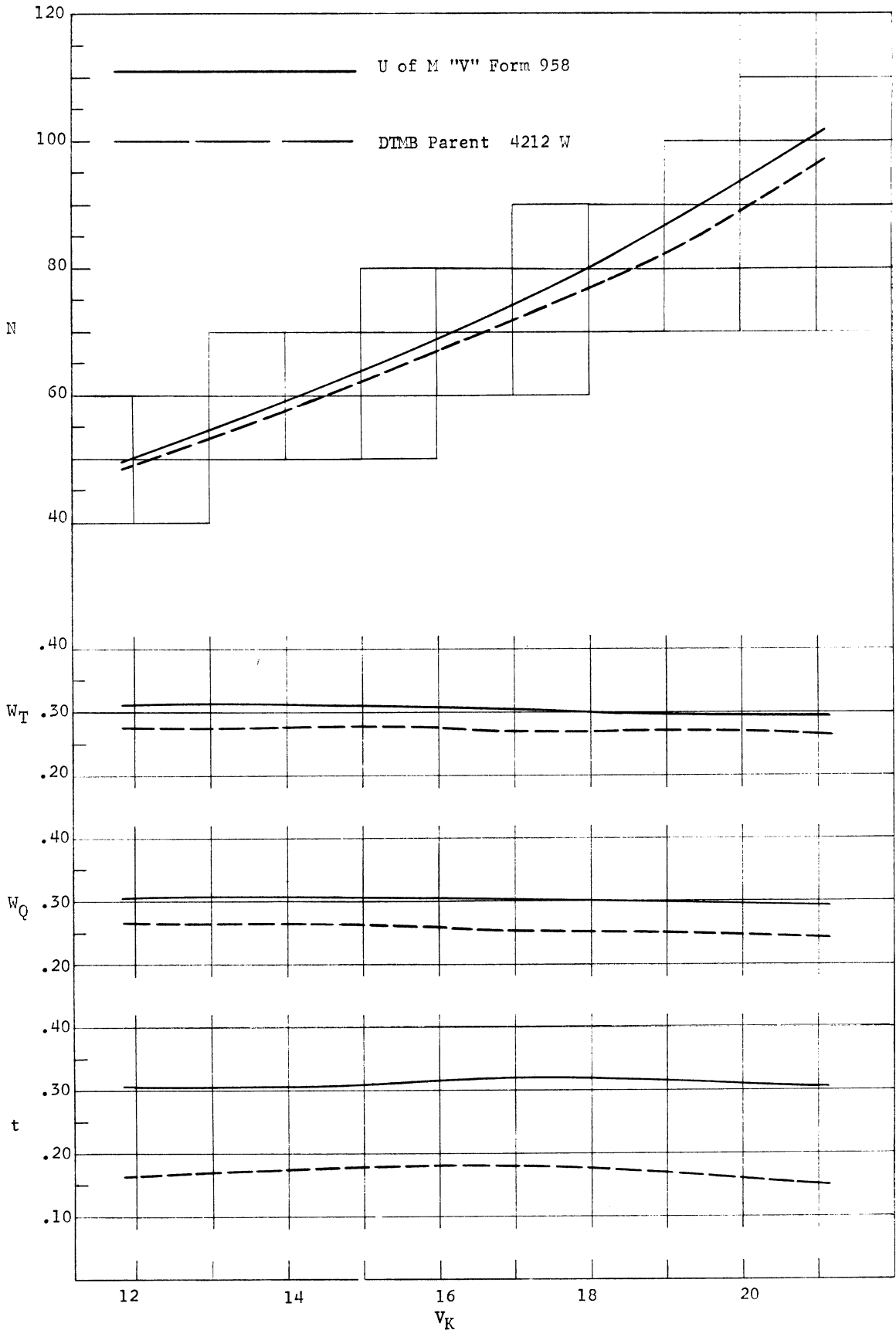


Fig. 17. Revolutions per minute, wake fraction, and thrust deduction versus speed in knots for the $C_B = .70$ U of M "V" Series and the DTMB Series 60.

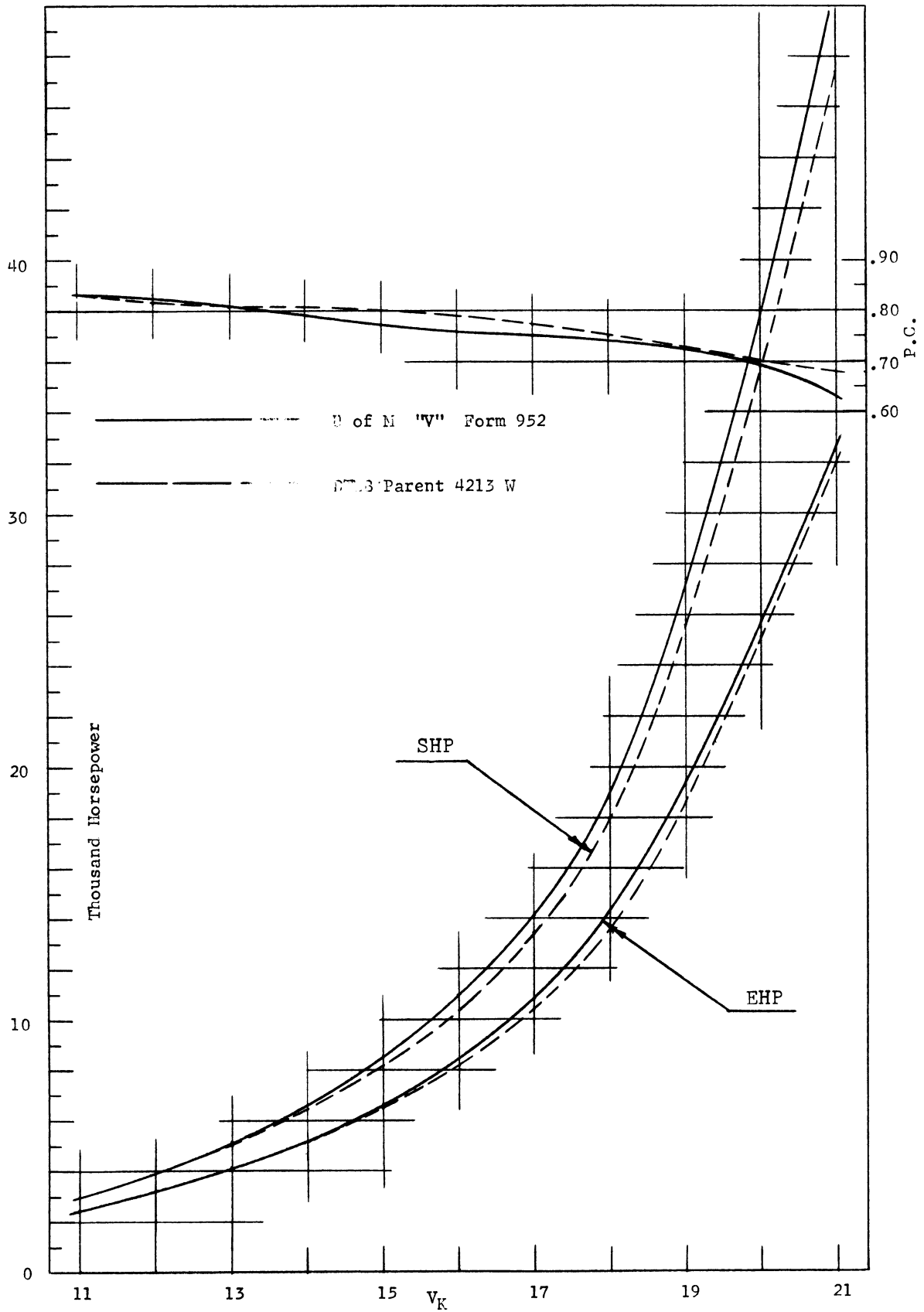


Fig. 18. Effective horsepower, shaft horsepower, and propulsive coefficient versus speed in knots for the $C_B = .75$ U of M "V" Series and the DTMB Series 60.

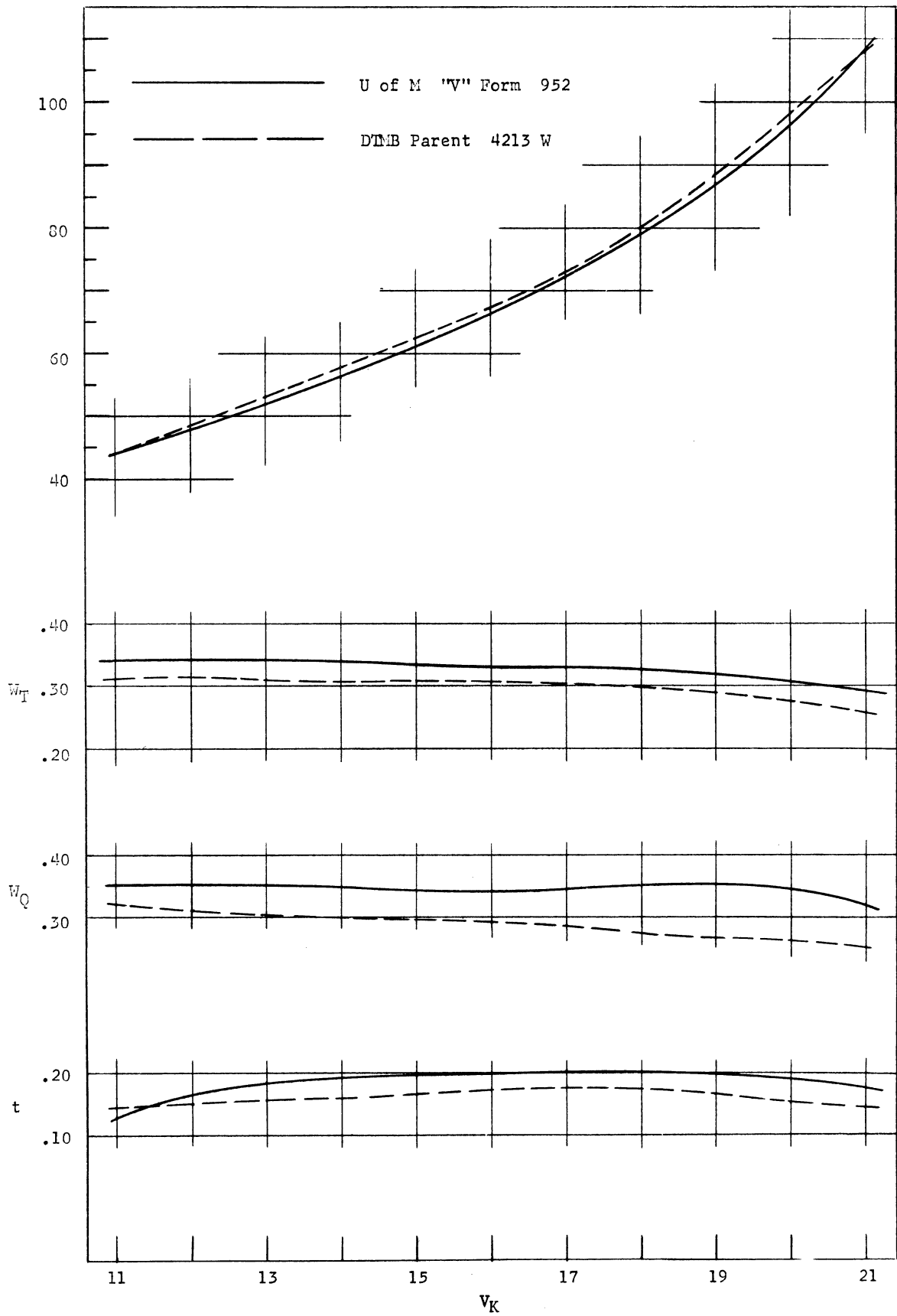


Fig. 19. Revolutions per minute, wake fraction, and thrust deduction versus speed in knots for the $C_B = .75$ U of M "V" Series and the DTMB Series 60.

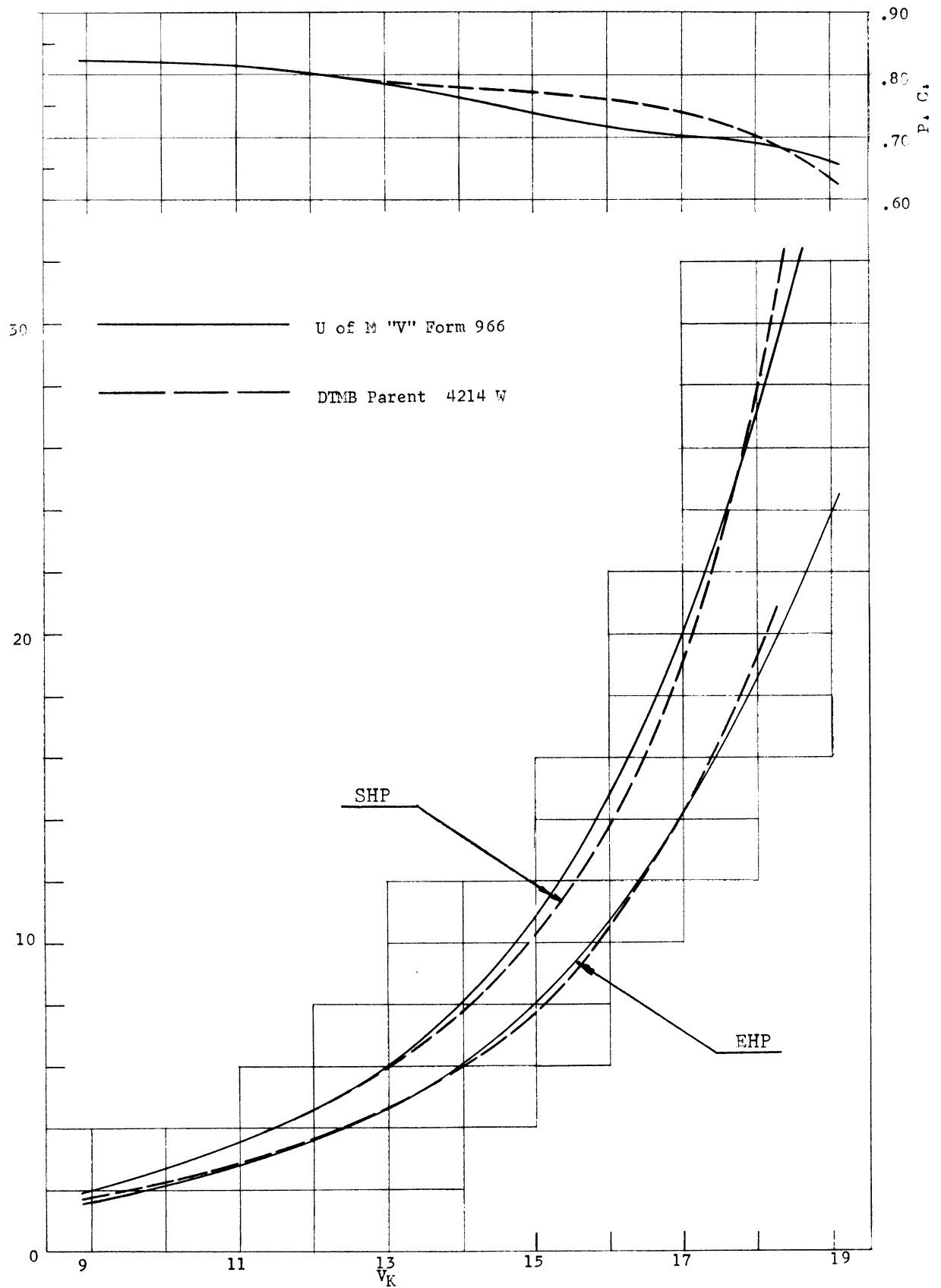


Fig. 20. Effective horsepower, shaft horsepower, and propulsive coefficient versus speed in knots for the $C_B = .80$ U of M "V" Series and the DTMB Series 60.

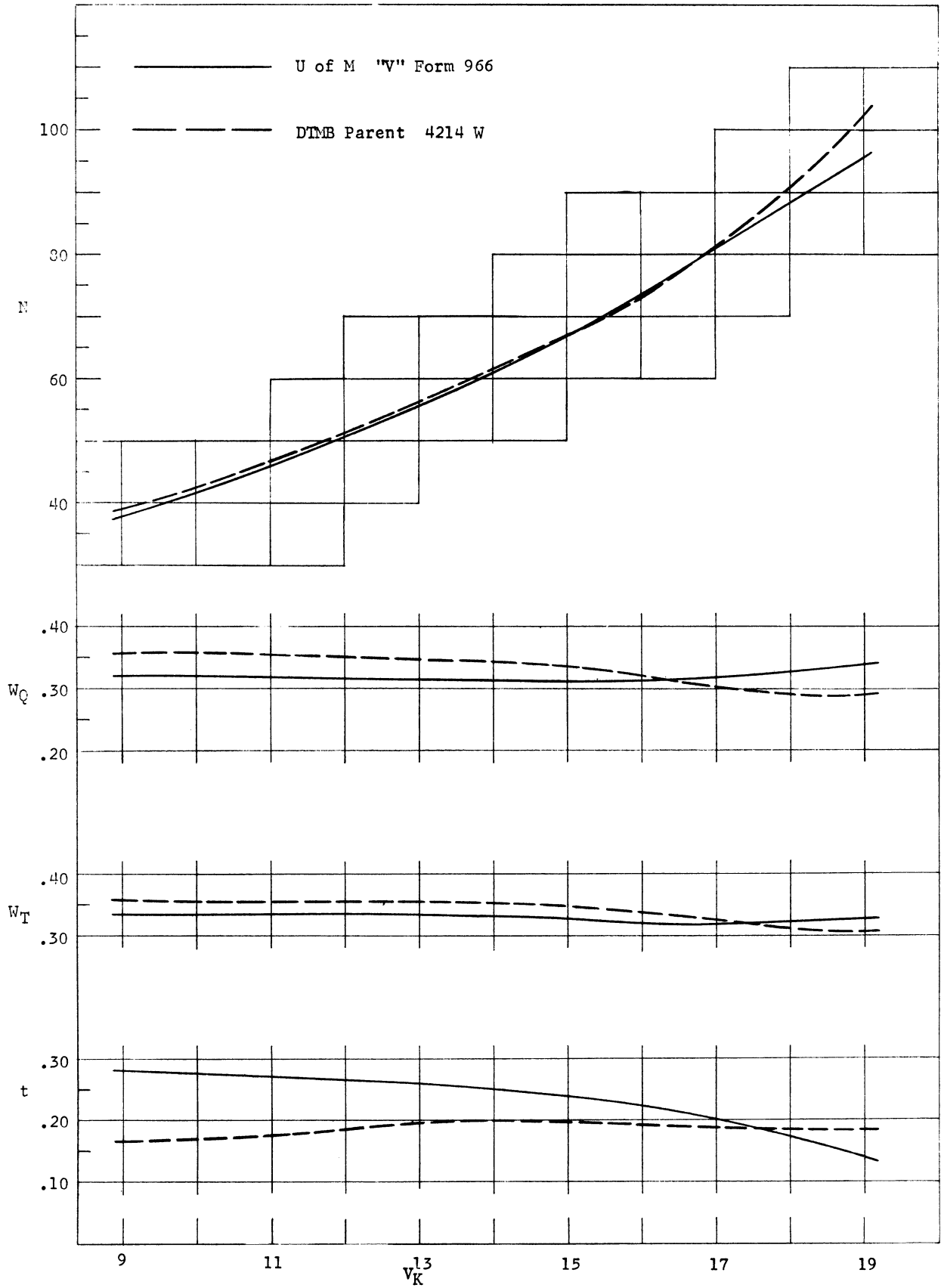


Fig. 21. Revolutions per minute, wake fraction, and thrust deduction versus speed in knots for the $C_B = .80$ U of M "V" Series and the DTMB Series 60.

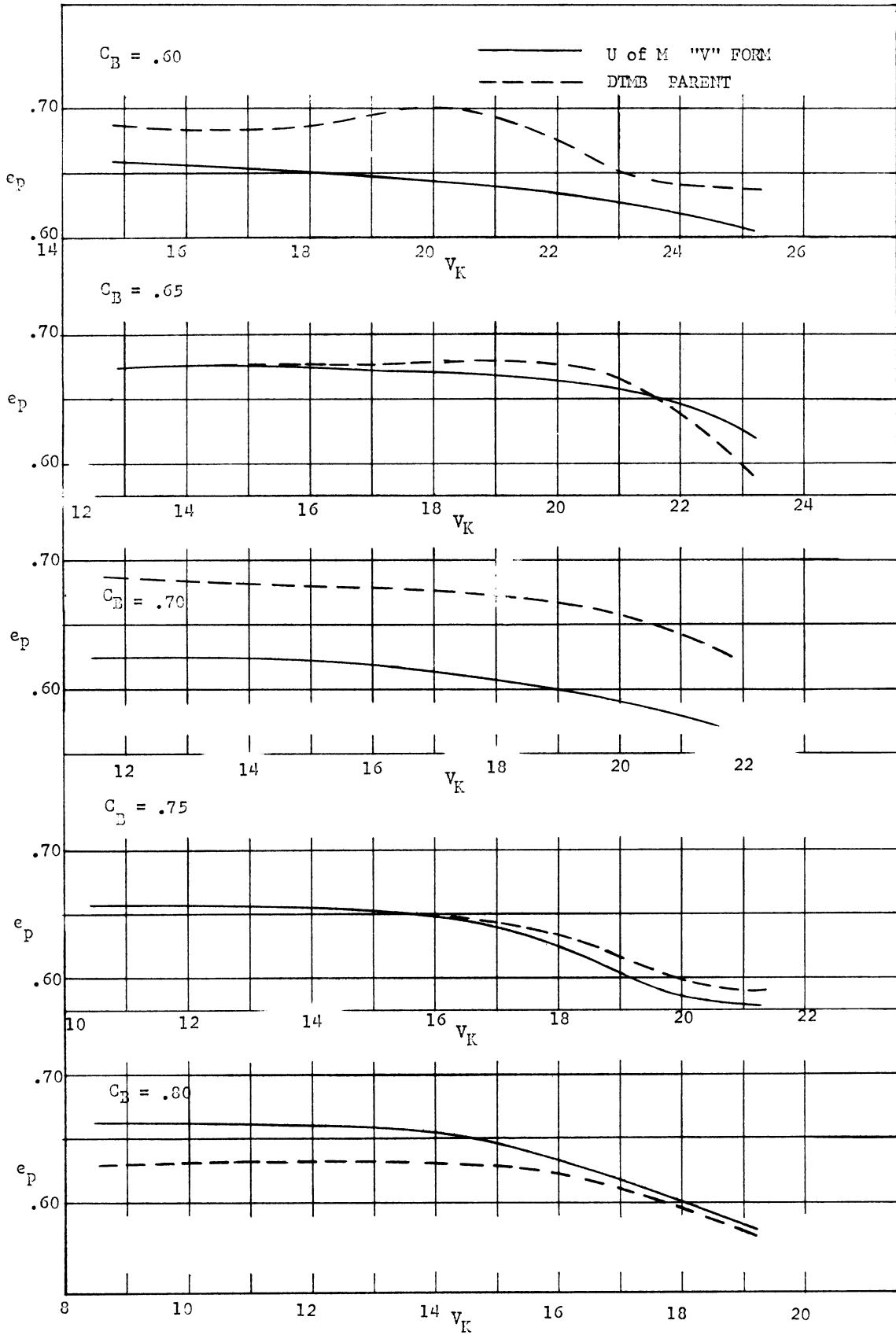


Fig. 22. Propeller efficiency versus speed in knots for the U of M "V" Series and the DTMB Series 60.

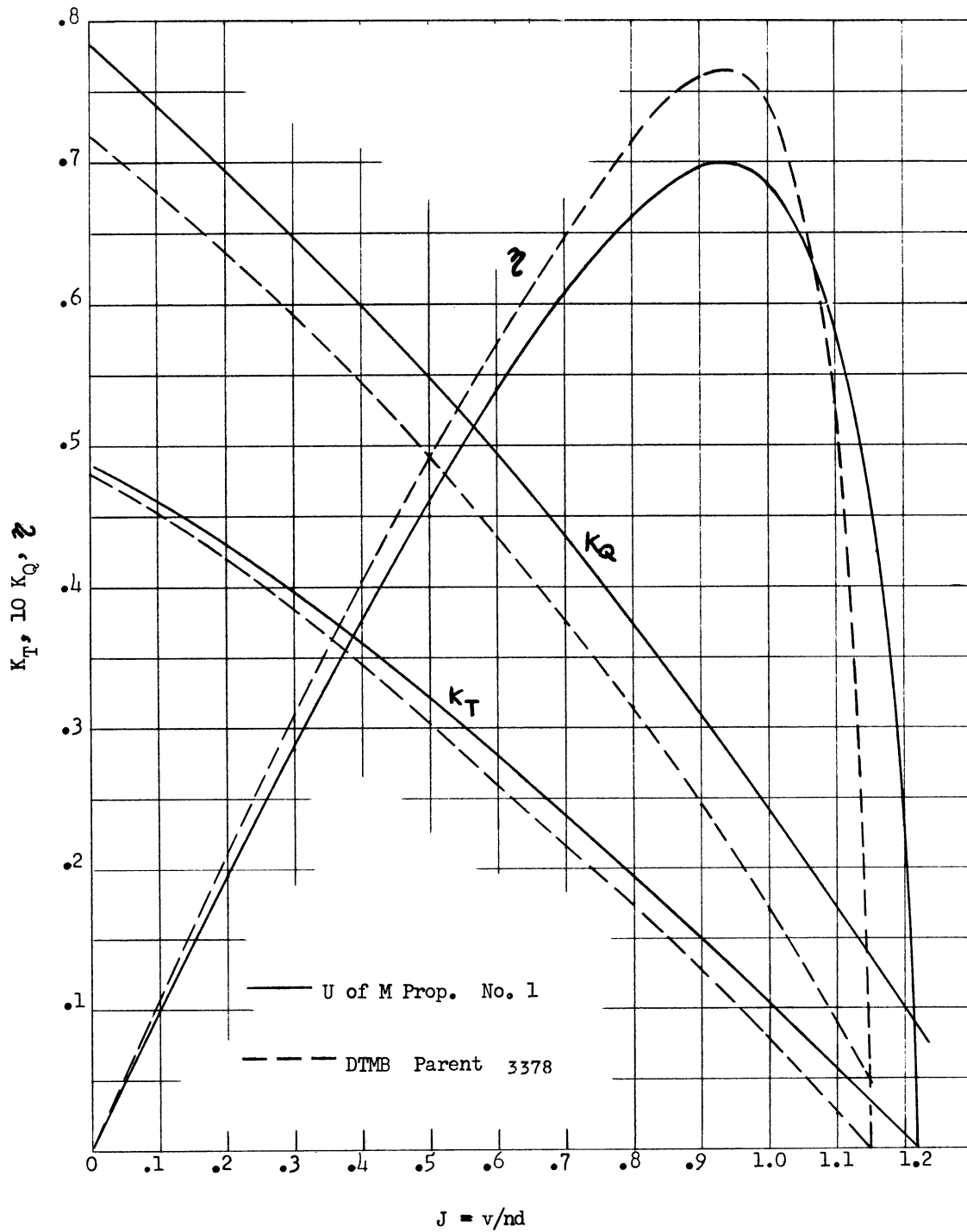


Fig. 23. Open water propeller characteristics for U of M and DTMB propellers used on the $C_B = .60$ models.

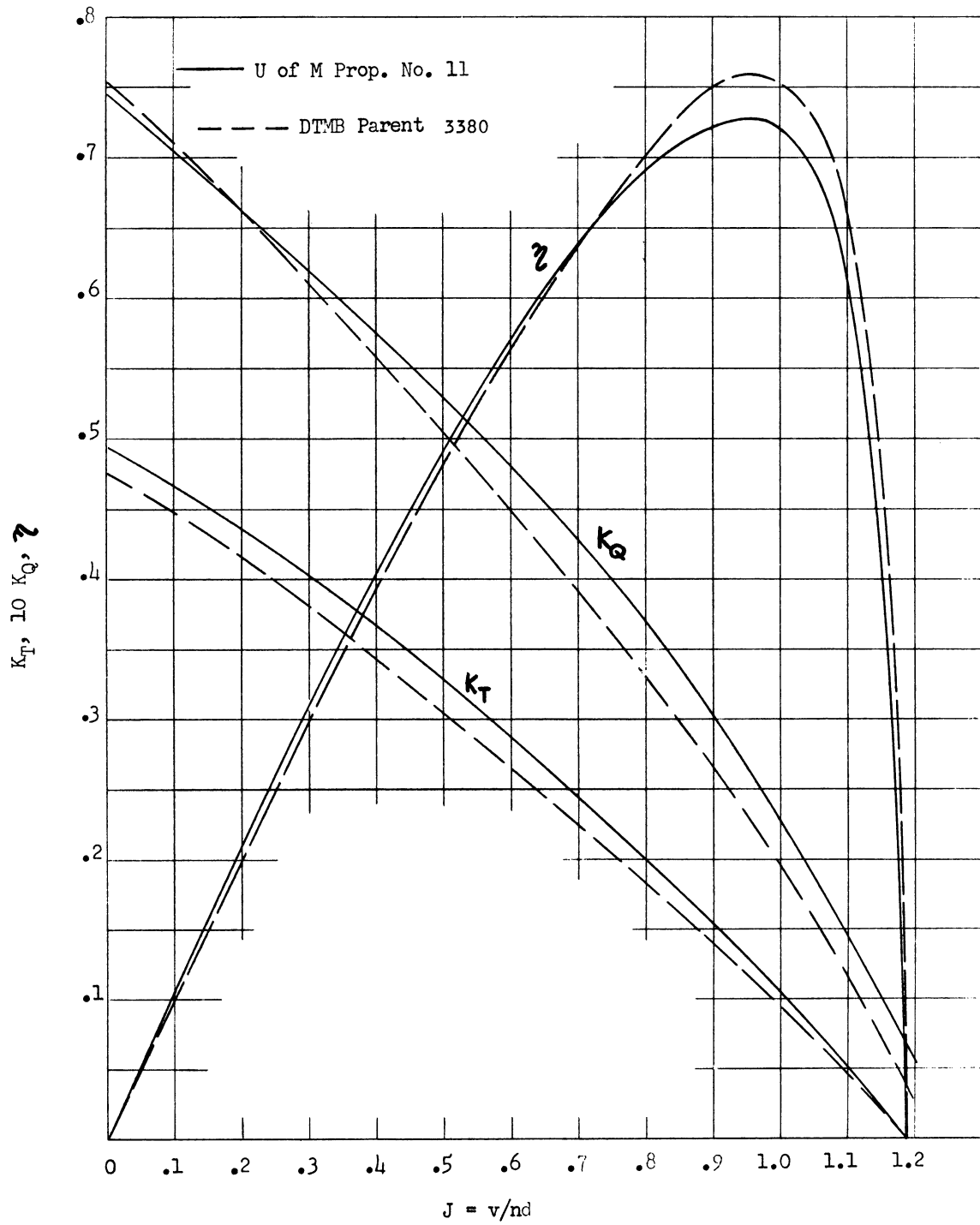


Fig. 24. Open water propeller characteristics for U of M and DTMB propellers used on the $C_B = .65$ models.

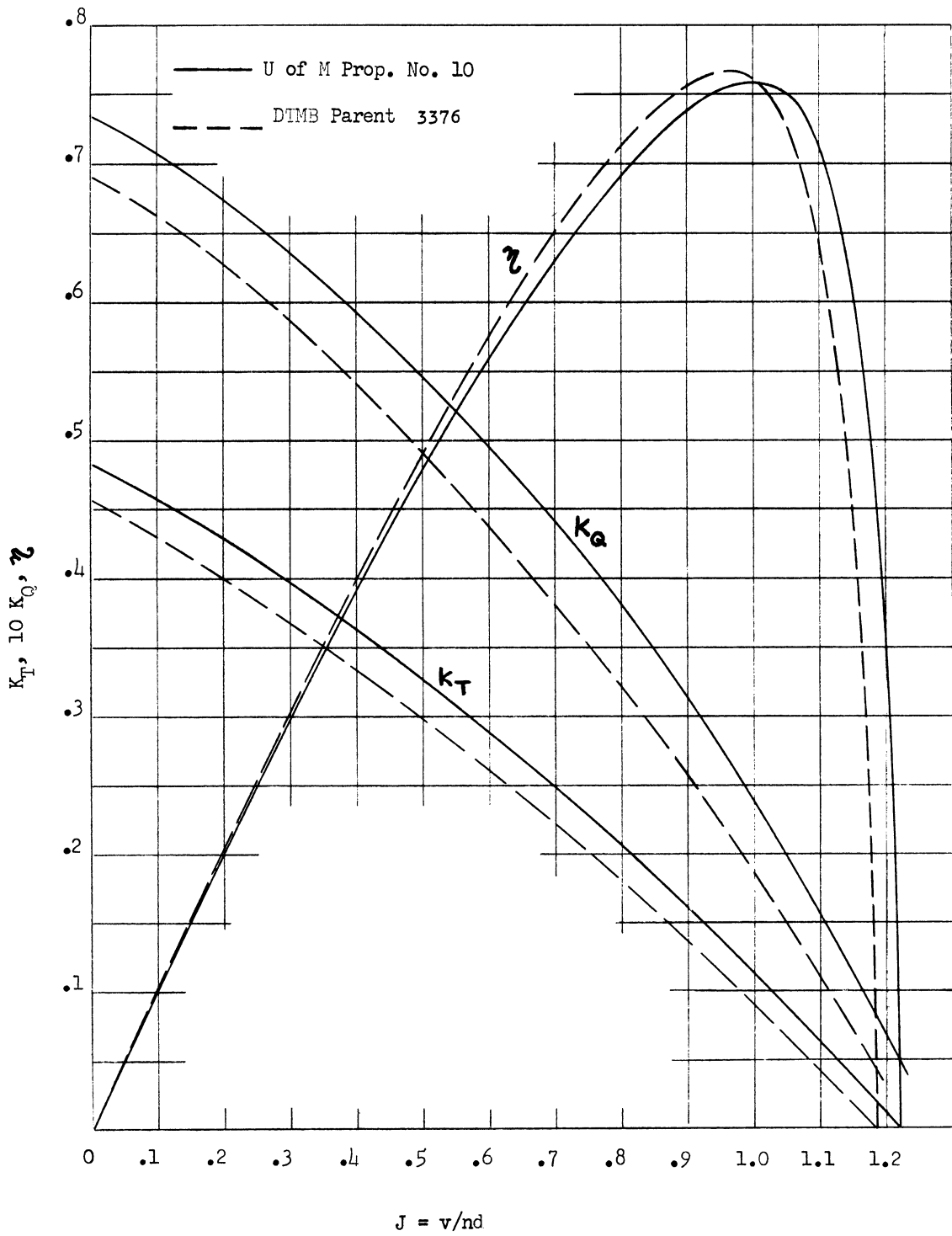


Fig. 25. Open water propeller characteristics for U of M and DIMB propellers used on the $C_B = .70$ models.

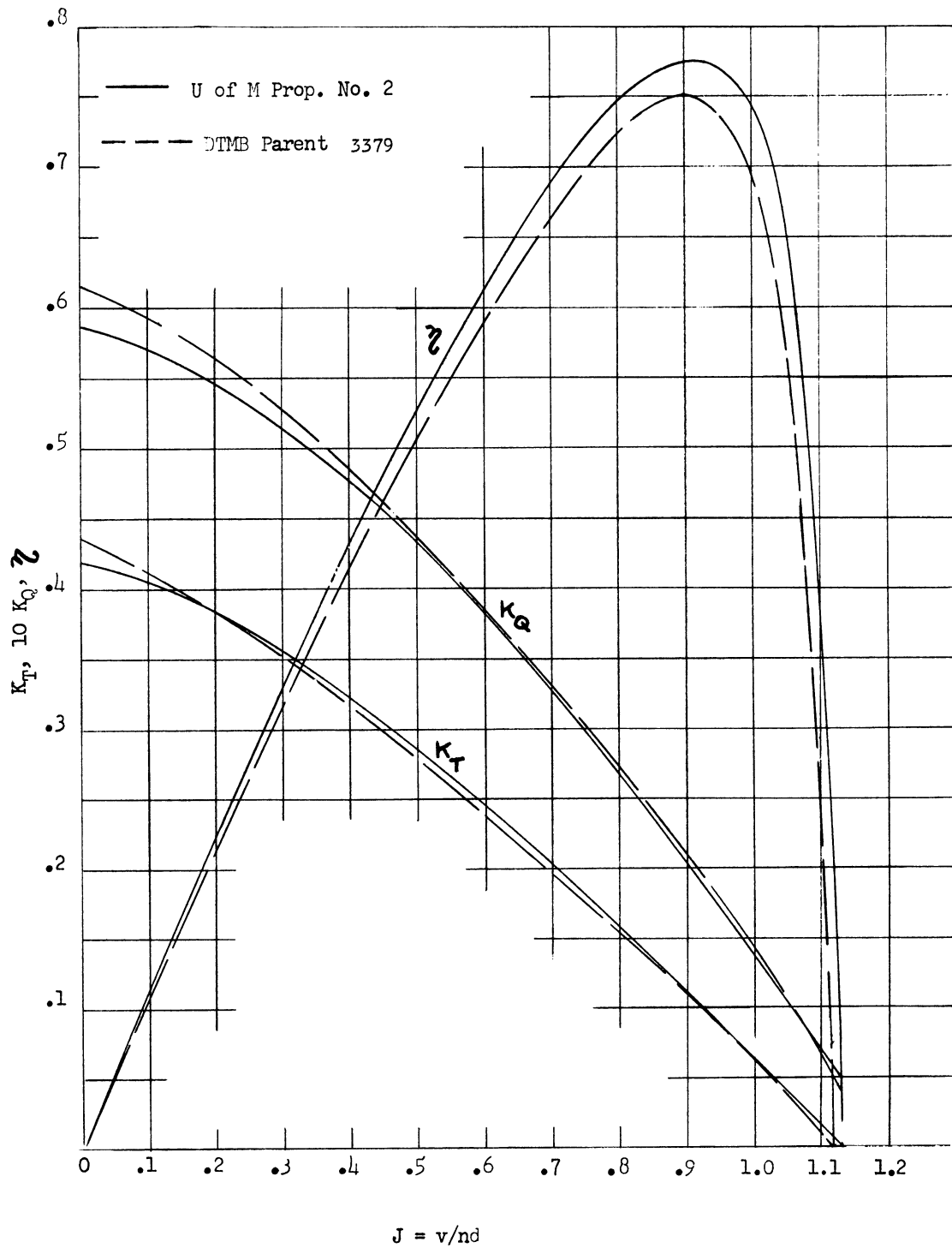


Fig. 26. Open water propeller characteristics for U of M and DTMB propellers used on the $C_B = .75$ models.

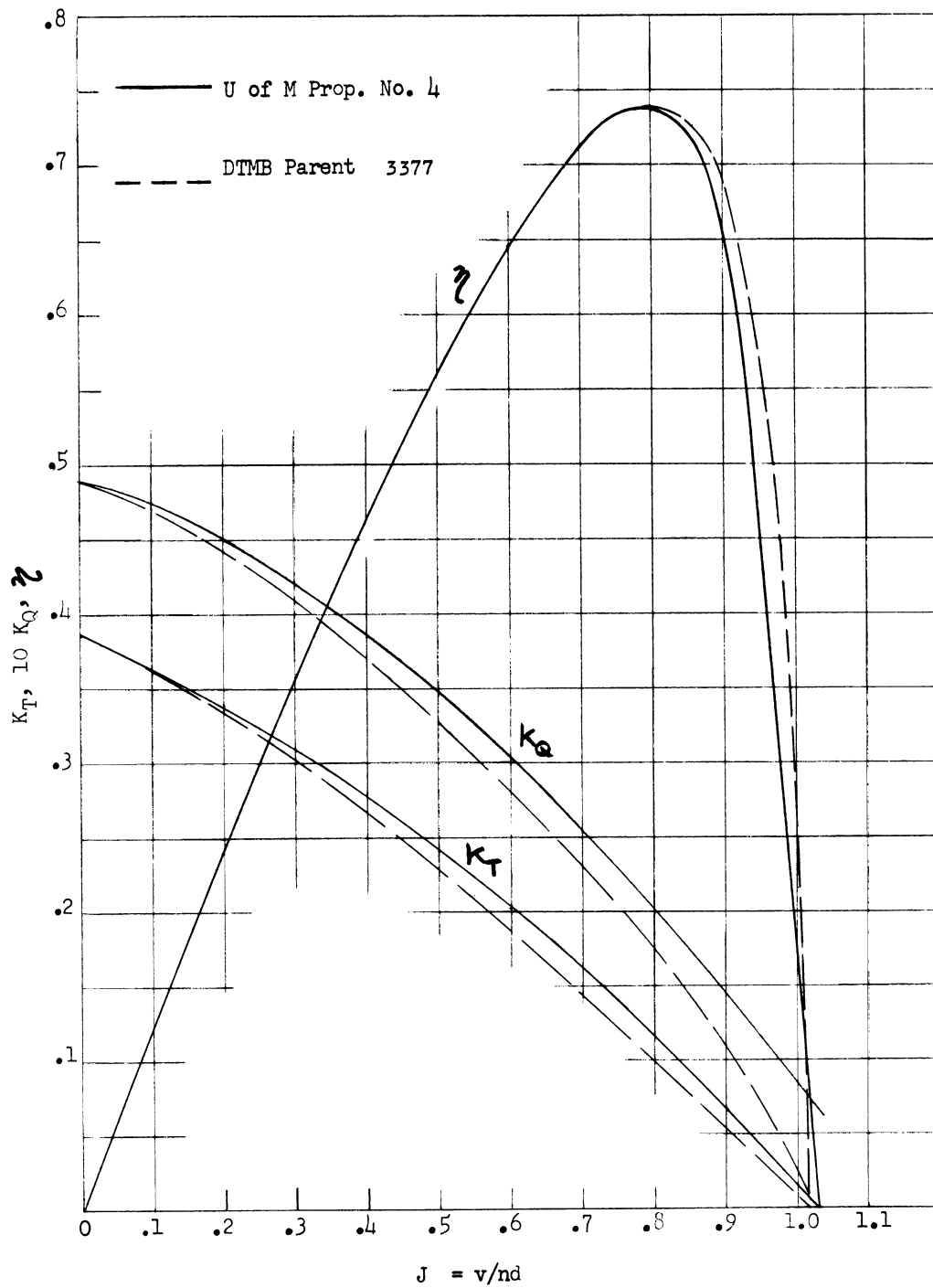


Fig. 27. Open water propeller characteristics for U of M and DTMB propellers used on the $C_B = .80$ models.

APPENDIX

TABLE A-I

CURVES OF FORM FOR THE SERIES 60, $C_B = .60$

CALCULATIONS FOR THE CURVES OF FORM AND HONJEAN CURVES

SHIP NO.912

R. A. YAGLE, H. C. KIM

BASIC DIMENSIONS

THE LENGTH BETWEEN PERPENDICULARS IS 600.000 FEET

THE MOLDED HALF BEAM IS 39.997 FEET

THERE ARE 5 DIFFERENT STATION SPACINGS ALONG THE SHIP

THERE ARE 2 DIFFERENT WATERLINE SPACINGS UP THE SHIP

MIDSHIP IS LOCATED AT STATION 14

CALCULATED ON 8/22/62

TABLE A-I (Continued)

WATERPLANE CALCULATIONS
SHIP NO.912

CF IS IN FEET FORWARD (+) OR AFT (-) OF MIDSHIPS							
WATERLINE	WP AREAS	CF (FROM MID.)	TONS PER INCH	WP COEFF.	TRANSV. I. COEFF.	LONG. I. COEFF.	
.000	14768	-14.504	35.161	.3077	.09383	.12483	
4.000	24142	-4.343	57.480	.5030	.27574	.27151	
8.000	27003	-2.915	64.292	.5625	.36036	.31663	
15.999	29751	-5.261	70.836	.6199	.44542	.36689	
23.997	31475	-11.329	74.940	.6558	.49057	.41039	
31.996	33994	-23.217	80.937	.7082	.54383	.49491	
39.994	36569	-31.600	87.070	.7619	.60010	.59163	
47.993	39010	-33.202	92.880	.8128	.66079	.68884	

MOLDED DISPLACEMENTS
SHIP NO.912

ALL VALUES ARE IN LONG TONS		
WATERLINE	DISP. SALT WATER	DISP. FRESH WATER
4.000	2285	2222
8.000	5270	5124
15.999	11830	11502
23.997	18846	18322
31.996	26312	25581
39.994	34373	33419
47.993	43012	41817

TABLE A-I (Continued)

LONGITUDINAL AND VERTICAL CENTERS OF BUOYANCY
SHIP NO.912

VCB IS IN FEET ABOVE THE BASELINE WATERLINE	VCB	LCB
4.000	2.319	-7.630
8.000	4.354	-5.149
15.999	8.578	-4.297
23.997	12.831	-5.678
31.996	17.155	-8.875
39.994	21.586	-13.295
47.993	26.094	-17.236

TRANSVERSE AND LONGITUDINAL METACENTRIC HEIGHTS
SHIP NO.912

ALL VALUES ARE IN FEET ABOVE THE BASE LINE WATERLINE	KM TRANS.	KM LONG.
4.000	32.341	2249.319
8.000	42.617	2123.857
15.999	30.853	1109.658
23.997	30.114	813.741
31.996	30.790	658.833
39.994	33.155	613.922
47.993	36.297	591.974

TABLE A-I (Continued)

MOMENT TO TRIM ONE INCH AND
CHANGES IN DISPLACEMENT FOR A ONE INCH TRIM AFT
SHIP NO.912

THE MOMENTS ARE IN FOOT LONG TONS
THE CHANGE IN DISP. IS IN LONG TONS

WATERLINE	MOM. TO TRIM 1 IN.	CHANGE IN DISP.
4.000	713.244	.416
8.000	1809.207	-.312
15.999	2096.378	.621
23.997	2344.936	1.415
31.996	2827.861	3.132
39.994	3380.505	4.586
47.993	3935.986	5.140

BLOCK, PRISMATIC, MIDSHIP, AND VERTICAL PRISMATIC COEFFICIENTS
SHIP NO.912

WATERLINE	BLOCK	PRISMATIC	MIDSHIP	VERTICAL PRISMATIC
4.000	.4166	.4992	.8346	.8283
9.000	.4804	.5317	.9034	.8538
15.999	.5392	.5658	.9531	.8699
23.997	.5727	.5909	.9691	.8733
31.996	.5997	.6139	.9768	.8467
39.994	.6267	.6386	.9815	.8226
47.993	.6535	.6638	.9846	.8041

TABLE A-I (Continued)

SECTIONAL AREAS FROM BONJEAN CURVES
SHIP NO.912

LOCATION OF STATIONS	STATION	DISTANCE FROM STA. 0
	0	.000
	1	2.176
	2	4.352
	3	19.352
	4	34.352
	5	49.352
	6	64.352
	7	94.352
	8	124.352
	9	154.352
	10	184.352
	11	214.352
	12	244.352
	13	274.352
	14	304.352
	15	334.352
	16	364.352
	17	394.352
	18	424.352
	19	454.352
	20	484.352
	21	514.352
	22	544.352
	23	559.352
	24	574.352
	25	589.352
	26	604.352
	27	608.495
	28	612.637
	29	616.780
	30	620.923

TABLE A-I (Continued)

002936 11/27/62 9 23 5.3 AM

\$ DATA

MAP ERROR 0000* SYSTEM 0000* SPRINT 0000* SKIP5 0000* SCARDS 0000* SPEEK 0000*
 .EXIT 0000* FRAP 0000* (MAIN) 1000 .IDH 47671* .READ 52107* .PRINI 52247*
 .PRSLT 52330* .PCOMT 53026* .01301 53045* ZERO 53137* .03311 53173* .ERR 53210*
 BNBCD 53272* (PROG) 53315 (SUBT) 74712 (ERAS) 77776
 21365 LOCS. CAN BE SAFELY USED IN EXPANDING PROG. (OCIAL)

INPUT VALUES READ WERE

LBP = 168.000000, BE = 11.199300, INCH = IR, LAMBDA = 42.85714D
 NBL = 5, NBV = 2, DST = 14

L(1)...L(5)

1.218500E 00 1.801850E 01 1.524185E 02 1.692185E 02 1.738585E 02

LN(1)...LN(5)

2 4 4 16 4 4

D(1)...D(2)

2.240000E 00 1.343800E 01

VN(1)...VN(2)

2 5

DFS(10,0)...DFS(30,7)

.000000E 00 .000000E 00 .000000E 00 .000000E 00 .000000E 00 .000000E 00 .000000E 00
 .000000E 00 .000000E 00 .000000E 00 .000000E 00 .000000E 00 .000000E 00 .000000E 00
 .000000E 00 .000000E 00 .000000E 00 .000000E 00 .000000E 00 .000000E 00 .000000E 00
 7.200000E-02 3.600000E-01 4.590000E-01 4.630000E-01 4.820000E-01 5.712000E-01 8.510000E-01 1.344000E 00
 1.030000E-01 7.600000E-01 9.050000E-01 9.740000E-01 1.008000E 00 1.142000E 00 1.490000E 00 2.218000E 00
 1.110000E-01 1.160000E 00 1.390000E 00 1.579000E 00 1.658000E 00 1.792000E 00 2.184000E 00 3.113000E 00
 1.910000E-01 1.560000E 00 1.964000E 00 2.285000E 00 2.386000E 00 2.553000E 00 3.024000E 00 4.032000E 00
 4.370000E-01 2.470000E 00 3.243000E 00 3.875000E 00 4.121000E 00 4.379000E 00 4.928000E 00 5.947000E 00
 1.066000E 00 3.780000E 00 4.810000E 00 5.622000E 00 5.992000E 00 6.294000E 00 6.798000E 00 7.649000E 00
 2.187000E 00 5.420000E 00 6.497000E 00 7.392000E 00 7.739000E 00 8.041000E 00 8.444000E 00 9.004000E 00

TABLE A-II

CURVES OF FORM FOR THE SERIES 60, $C_B = .65$

CALCULATIONS FOR THE CURVES OF FORM AND RCNJEAN CURVES

SHIP NO..65PAR

R. A. YAGLE, H. C. KIM

BASIC DIMENSIONS

THE LENGTH BETWEEN PERPENDICULARS IS 600.000 FEET

THE MIDDLE HALF BEAM IS 41.379 FEET

THERE ARE 5 DIFFERENT STATION SPACINGS ALONG THE SHIP

THERE ARE 2 DIFFERENT WATERLINE SPACINGS UP THE SHIP

MIDSHIP IS LOCATED AT STATION 14

CALCULATED ON 8/22/62

TABLE A-II (Continued)

WATERPLANE CALCULATIONS
SHIP NO..65PAR

CF IS IN FEET FORWARD (+) OR AFT (-) OF MIDSHIPS		WATERPLANE CALCULATIONS SHIP NO..65PAR					
WATERLINE	WP AREAS	CF (FROM MID.)	TUNS PER INCH	WP COEFF.	TRANSV. I. COEFF.	LONG. I. COEFF.	
.000	17553	-5.787	41.794	.3535	.12687	.15317	
4.137	27734	2.044	66.034	.5585	.34046	.32018	
8.275	30746	2.708	73.205	.6192	.43442	.37103	
16.551	33160	-.054	78.951	.6678	.50743	.42157	
24.828	34791	-5.820	82.837	.7007	.54959	.46684	
33.104	37109	-16.362	88.356	.7474	.59780	.54898	
41.381	39546	-24.534	94.157	.7964	.65214	.64258	
49.657	41760	-26.535	99.430	.8410	.70817	.73168	

MOLDED DISPLACEMENTS
SHIP NO..65PAR

ALL VALUES ARE IN LONG TONS		
WATERLINE	DISP. SALT WATER	DISP. FRESH WATER
4.137	2747	2671
8.275	6275	6100
16.551	13925	13539
24.828	21975	21365
33.104	30463	29616
41.381	39524	38426
49.657	49141	47776

TABLE A-II (Continued)

LONGITUDINAL AND VERTICAL CENTERS OF BUOYANCY
SHIP NO..65PAR

VCH IS IN FEET ABOVE THE BASELINE		LCR
WATERLINE	VCH	
4.137	2.379	-0.494
8.275	4.480	1.309
16.551	8.811	1.542
24.828	13.165	-0.018
33.104	17.586	-3.024
41.381	22.103	-7.070
49.657	26.692	-10.777

TRANSVERSE AND LONGITUDINAL METACENTRIC HEIGHTS
SHIP NO..65PAR

ALL VALUES ARE IN FEET ABOVE THE BASE LINE		
WATERLINE	KM TRANS.	KM LONG.
4.137	39.770	2375.116
8.275	48.413	2176.235
16.551	34.070	1142.612
24.828	31.862	829.647
33.104	32.194	669.828
41.381	34.350	613.265
49.657	37.437	583.225

TABLE A-II (Continued)

MOMENT TO TRIM ONE INCH AND
CHANGES IN DISPLACEMENT FOR A ONE INCH TRIM AFT
SHIP NO..65PAR

THE MOMENTS ARE IN FOOT LONG TONS
THE CHANGE IN DISP. IS IN LONG TONS

WATERLINE	MOM. TO TRIM 1 IN.	CHANGE IN DISP.
4.137	905.413	-.225
8.275	2193.260	-.330
16.551	2491.970	.007
24.828	2759.588	.804
33.104	3245.123	2.410
41.381	3798.435	3.850
49.657	4325.141	4.397

BLOCK, PRISMATIC, MIDSHIP, AND VERTICAL PRISMATIC COEFFICIENTS
SHIP NO..65PAR

WATERLINE	BLOCK	PRISMATIC	MIDSHIP	VERTICAL PRISMATIC
4.137	.4681	.5480	.8542	.8380
8.275	.5345	.5826	.9174	.8632
16.551	.5930	.6167	.9617	.8880
24.828	.6239	.6401	.9747	.8904
33.104	.6486	.6612	.9810	.8679
41.381	.6732	.6836	.9848	.8453
49.657	.6976	.7065	.9873	.8294

TABLE A-II (Continued)

SECTIONAL AREAS FROM BONJEAN CURVES
SHIP NO..65PAR

LOCATION OF STATIONS	STATION	DISTANCE FROM STA. 0 .000
	0	0.000
	1	2.176
	2	4.352
	3	19.352
	4	34.352
	5	49.352
	6	64.352
	7	94.352
	8	124.352
	9	154.352
	10	184.352
	11	214.352
	12	244.352
	13	274.352
	14	304.352
	15	334.352
	16	364.352
	17	394.352
	18	424.352
	19	454.352
	20	484.352
	21	514.352
	22	544.352
	23	574.352
	24	604.352
	25	638.495
	26	604.352
	27	612.637
	28	616.780
	29	620.923
	30	620.923

TABLE A-II (Concluded)

SHIP NO. .65PAR

INPUT VALUES READ WERE	BE =	11.586000,	INCH =	18,	LAMBDA =
LBP = 168.000000,					42.857140
NBL = 5,	NBV = 2,		DST =	14	
L(1)...L(5)					
1.218500E 00	1.524185E 02	1.692185E 02	1.738585E 02		
LN(1)...LN(5)					
2	4	16	4		
O(1)...O(2)					
2.317000E 00	1.390400E 01				
VN(1)...VN(2)					
2	5				
OFS(3,0)...OFS(30,7)					
.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00
.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00	2.300000E-01
.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00	5.210000E-01
6.800000E-02	5.200000E-01	6.440000E-01	6.720000E-01	7.650000E-01	1.043000E 00
1.370000E-01	1.030000E 00	1.264000E 00	1.413000E 00	1.564000E 00	1.923000E 00
2.050000E-01	1.600000E 00	2.000000E 00	2.248000E 00	2.503000E 00	2.908000E 00
3.510000E-01	2.230000E 00	2.804000E 00	3.209000E 00	3.568000E 00	4.055000E 00
9.330000E-01	3.700000E 00	4.609000E 00	5.272000E 00	5.886000E 00	6.395000E 00
2.046000E 00	5.490000E 00	6.551000E 00	7.369000E 00	8.041000E 00	8.504000E 00

TABLE A-III

CURVES OF FORM FOR THE SERIES 60. CB = .70

CALCULATIONS FOR THE CURVES OF FORM AND BONJEAN CURVES

SHIP NO. 913

R. A. YAGLE, H. C. KIM

BASIC DIMENSIONS

THE LENGTH BETWEEN PERPENDICULARS IS 600.000 FEET

THE MOLDED HALF BEAM IS 44.446 FEET

THERE ARE 5 DIFFERENT STATION SPACINGS ALONG THE SHIP

THERE ARE 2 DIFFERENT WATERLINE SPACINGS UP THE SHIP

MIDSHIP IS LOCATED AT STATION 14

CALCULATED ON 8/22/62

TABLE A-III (Continued)

WATERPLANE CALCULATIONS
SHIP NO. 70PAR

WATERLINE	WP AREA	CF (FROM MID.)	TCNS PER INCH	WP COEFF.	TRANSV. I. COEFF.	LONG. I. COEFF.
.000	21606	6.833	51.443	.4202	.17908	.20257
4.286	31479	8.887	76.141	.6219	.42324	.38182
8.571	34747	8.671	82.732	.6757	.51275	.43322
17.144	36813	5.020	87.650	.7159	.57294	.48339
25.717	38328	-.331	91.257	.7453	.61084	.52960
34.290	40485	-9.893	96.393	.7873	.65318	.61157
42.863	42729	-17.935	101.737	.8309	.70159	.70212
51.436	44579	-20.853	106.141	.8669	.74679	.77954

MOLDED DISPLACEMENTS
SHIP NO. 70PAR

ALL VALUES ARE IN LONG TONS		
WATERLINE	DISP. SALT WATER	DISP. FRESH WATER
4.286	3358	3265
8.571	7521	7312
17.144	16380	15925
25.717	25593	24883
34.290	35233	34254
42.863	45422	44160
51.436	56123	54564

TABLE A-III (Continued)

LONGITUDINAL AND VERTICAL CENTERS OF BUOYANCY
SHIP NO. 70PAR

VCB IS IN FEET ABOVE THE BASELINE			
WATERLINE	VCB	LCB	
4.286	2.426	8.236	
8.571	4.591	8.606	
17.144	9.035	7.837	
25.717	13.502	5.904	
34.290	18.032	2.963	
42.863	22.650	- .858	
51.436	27.325	-4.469	

TRANSVERSE AND LONGITUDINAL METACENTRIC HEIGHTS
SHIP NO. 70PAR

ALL VALUES ARE IN FEET ABOVE THE BASE LINE			
WATERLINE	KM TRANS.	KM LONG.	
4.286	50.386	2661.119	
8.571	55.202	2242.255	
17.144	37.189	1174.838	
25.717	33.636	846.007	
34.290	33.625	680.590	
42.863	35.583	616.126	
51.436	38.568	578.762	

TABLE A-III (Continued)

MOMENT TO TRIM ONE INCH AND
CHANGES IN DISPLACEMENT FOR A ONE INCH TRIM AFT
SHIP NO. 70PAR

THE MOMENTS ARE IN FOOT LONG TONS
THE CHANGE IN DISP. IS IN LONG TONS

WATERLINE	MCM. TO TRIM 1 IN.	CHANGE IN DISP.
4.286	1240.108	-1.128
8.571	2652.153	-1.196
17.144	2959.260	-0.733
25.717	3242.165	.050
34.290	3744.009	1.589
42.863	4298.350	3.041
51.436	4772.269	3.689

BLOCK, PRISMATIC, MIDSHIP, AND VERTICAL PRISMATIC COEFFICIENTS
SHIP NO. 70PAR

WATERLINE	BLOCK	PRISMATIC	MIDSHIP	VERTICAL PRISMATIC
4.286	.5333	.6081	.8771	.8576
8.571	.5972	.6396	.9338	.8839
17.144	.6503	.6699	.9707	.9083
25.717	.6773	.6908	.9805	.9088
34.290	.6993	.7097	.9854	.8883
42.863	.7212	.7298	.9883	.8680
51.436	.7426	.7499	.9903	.8567

TABLE A-III (Continued)

SECTIONAL AREAS FROM BCNJEAN CURVES
SHIP NO. 70PAR

LOCATION OF STATIONS	STATION	DISTANCE FROM STA. 0
	C	.000
	1	2.176
	2	4.352
	3	19.352
	4	34.352
	5	49.352
	6	64.352
	7	94.352
	8	124.352
	9	154.352
	10	184.352
	11	214.352
	12	244.352
	13	274.352
	14	304.352
	15	334.352
	16	364.352
	17	394.352
	18	424.352
	19	454.352
	20	484.352
	21	514.352
	22	544.352
	23	559.352
	24	574.352
	25	589.352
	26	604.352
	27	608.495
	28	612.637
	29	616.780
	30	620.923

TABLE A-III (Continued)

SHIP NO. .7CPAR

INPUT VALUES READ HERE	RE =	11.999000,	INCH =	16,	LAMBDA =
LPP = 168.000000,	NEV =	2,	OST =	14	42.857140
NEL =	5,				
L(1)...L(5)					
1.216500E 00	1.601800E 01	1.524185E 02	1.692185E 02	1.738585E 02	
LN(1)...LN(5)					
2	4	16	4	4	
U(1)...U(2)					
2.400000E 00	1.440000E 01				
VM(1)...VM(2)					
2	5				
OFS(0,0)...OFS(30,7)					
.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00
.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00	3.900000E-01
.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00	6.120000E-01
8.300000E-02	6.700000E-01	8.620000E-01	9.720000E-01	1.128000E 00	2.112000E 00
2.410000E-01	1.400000E 00	1.892000E 00	2.124000E 00	2.328000E 00	3.588000E 00
5.000000E-01	2.400000E 00	3.018000E 00	3.372000E 00	3.720000E 00	5.052000E 00
9.250000E-01	3.510000E 00	4.191000E 00	4.668000E 00	5.160000E 00	6.431000E 00
2.211000E 00	5.650000E 00	6.586000E 00	7.187000E 00	7.859000E 00	8.807000E 00
4.044000E 00	7.670000E 00	8.670000E 00	9.335000E 00	9.923000E 00	1.052300E 01

TABLE A-IV

CURVES OF FORM FOR THE SERIES 60, $C_B = .75$

CALCULATIONS FOR THE CURVES OF FORM AND BONJEAN CURVES

SHIP NC.913

R. A. YAGLE, H. C. KIM

BASIC DIMENSIONS

THE LENGTH BETWEEN PERPENDICULARS IS 600.000 FEET

THE MLCED HALF BEAM IS 44.446 FEET

THERE ARE 5 DIFFERENT STATION SPACINGS ALONG THE SHIP

THERE ARE 2 DIFFERENT WATERLINE SPACINGS UP THE SHIP

MIDSHIP IS LOCATED AT STATION 14

...CALCULATED ON 8/22/62

TABLE A-IV (Continued)

WATERPLANE CALCULATIONS
SHIP NO. 913

CF IS IN FEET FORWARD (+) OR AFT (-) OF MIDSHIPS

WATERLINE	WP AREAS	CF (FROM MID.)	TCNS PER INCH	WP COEFF.	TRANSV. I. COEFF.	LONG. I. COEFF.
.000	26734	17.023	63.651	.5012	.25225	.27579
4.445	36571	15.531	87.075	.6857	.51491	.45339
8.889	36867	14.583	92.540	.7287	.52734	.50267
17.776	40711	11.020	96.931	.7633	.63793	.55398
26.664	42213	5.667	100.508	.7915	.67385	.60447
35.551	44256	-3.783	105.372	.8298	.71136	.68810
44.438	46301	-11.650	110.242	.8681	.75479	.77451
53.325	47863	-14.604	113.959	.8974	.79467	.84030

MOLOED DISPLACEMENTS
SHIP NO. 913

ALL VALUES ARE IN LONG TONS

WATERLINE	DISP. SALT WATER	DISP. FRESH WATER
4.445	4099	3985
8.889	8969	8720
17.776	19150	18618
26.664	29685	28860
35.551	40652	39522
44.438	52149	50700
53.325	64114	62333

TABLE A-IV (Continued)

LONGITUDINAL AND VERTICAL CENTERS OF BUOYANCY
SHIP NO. 913

VCB IS IN FEET ABOVE THE BASELINE		
WATERLINE	VCB	LCB
4.445	2.465	16.141
8.889	4.699	15.546
17.776	9.271	14.186
26.664	13.873	12.160
35.551	18.536	9.207
44.438	23.274	5.438
53.325	28.055	1.896

TRANSVERSE AND LONGITUDINAL METACENTRIC HEIGHTS
SHIP NO. 913

ALL VALUES ARE IN FEET ABOVE THE BASE LINE		
WATERLINE	KM TRANS.	KM LONG.
4.445	64.212	3078.071
8.889	62.307	2315.640
17.776	40.048	1209.296
26.664	35.438	867.028
35.551	35.169	698.310
44.438	36.962	626.498
53.325	39.869	580.319

TABLE A-IV (Continued)

MOMENT TO TRIM ONE INCH AND
CHANGES IN DISPLACEMENT FOR A ONE INCH TRIM AFT
SHIP NO.913

THE MOMENTS ARE IN FOOT LONG TONS
THE CHANGE IN DISP. IS IN LONG TONS

WATERLINE	MOM. TO TRIM 1 IN.	CHANGE IN DISP.
4.445	1751.115	-2.254
8.889	3191.681	-2.249
17.776	3517.479	-1.782
26.664	3838.045	-.949
35.551	4369.076	.664
44.438	4917.749	2.148
53.325	5335.454	2.774

BLOCK, PRISMATIC, MIDSHIP, AND VERTICAL PRISMATIC COEFFICIENTS
SHIP NO.913

WATERLINE	BLOCK	PRISMATIC	MIDSHIP	VERTICAL PRISMATIC
4.445	.6052	.6657	.9038	.8827
8.889	.6621	.6955	.9520	.9086
17.776	.7069	.7223	.9786	.9261
26.664	.7306	.7411	.9858	.9231
35.551	.7504	.7585	.9893	.9043
44.438	.7701	.7767	.9915	.8871
53.325	.7890	.7946	.9929	.8792

TABLE A-IV (Continued)

SECTIONAL AREAS FROM HCNJEAN CURVES
SHIP NO. 913

LOCATION OF STATIONS	STATION	DISTANCE FROM STA. 0
	C	.000
	1	2.176
	2	4.352
	3	19.352
	4	34.352
	5	49.352
	6	64.352
	7	96.352
	8	124.352
	9	154.352
	10	184.352
	11	214.352
	12	244.352
	13	274.352
	14	304.352
	15	334.352
	16	364.352
	17	394.352
	18	424.352
	19	454.352
	20	484.352
	21	514.352
	22	544.352
	23	559.352
	24	574.352
	25	589.352
	26	604.352
	27	608.495
	28	612.637
	29	616.780
	30	620.923

TABLE A-IV (Continued)

SECTIONAL AREAS	WATERLINES				
	4.445	8.889	17.776	26.664	35.551
0	.000	.000	.000	.000	.000
1	.000	.000	.000	.000	.000
2	.000	.000	.000	.000	.000
3	22.564	64.098	162.141	267.533	380.807
4	54.608	148.123	362.205	586.505	821.126
5	90.060	233.185	557.150	900.061	1255.891
6	129.335	320.776	748.142	1202.444	1673.785
7	209.705	486.953	1084.063	1711.321	2355.850
8	276.846	613.964	1324.946	2053.580	2793.805
9	326.168	701.035	1472.515	2248.680	3028.913
10	351.312	742.911	1535.223	2325.623	3115.626
11	357.079	752.287	1546.451	2336.454	3126.457
12	357.079	752.287	1546.451	2336.454	3126.457
13	357.079	752.287	1546.451	2336.454	3126.457
14	357.079	752.287	1546.451	2336.454	3126.457
15	357.079	752.287	1546.451	2336.454	3126.457
16	353.635	747.589	1542.052	2322.127	3087.021
17	336.819	721.323	1507.036	2296.817	2985.501
18	304.402	666.538	1421.544	2200.528	2752.484
19	245.319	562.469	1251.483	1989.407	2374.725
20	187.916	446.644	1016.992	1668.457	1852.108
21	123.971	304.786	732.825	1247.169	1220.143
22	68.392	176.928	436.043	769.930	883.529
23	44.825	119.317	296.470	531.159	538.658
24	24.043	65.167	162.484	295.860	192.470
25	6.704	16.424	37.517	70.674	37.850
26	.000	.000	.000	.000	27.772
27	.000	.000	.000	.000	9.522
28	.000	.000	.000	.000	.000
29	.000	.000	.000	.000	.000
30	.000	.000	.000	.000	.000

AREAS (SQ. FT.)

44.438

53.325

26.664

17.776

8.889

4.445

SECTIONAL AREAS

STATION

0	.000	.000	.000	.000	.000
1	.000	.000	.000	.000	.000
2	.000	.000	.000	.000	.000
3	508.110	1073.378	1632.071	2165.794	2689.421
4	8.226	508.110	1073.378	1632.071	2165.794
5	508.110	1073.378	1632.071	2165.794	2689.421
6	1073.378	1632.071	2165.794	2689.421	3691.069
7	1632.071	2165.794	2689.421	3691.069	4300.213
8	2165.794	2689.421	3691.069	4300.213	4599.461
9	2689.421	3691.069	4300.213	4599.461	4706.464
10	3691.069	4300.213	4599.461	4706.464	4706.464
11	4300.213	4599.461	4706.464	4706.464	4706.464
12	4599.461	4706.464	4706.464	4706.464	4706.464
13	4706.464	4706.464	4706.464	4706.464	4706.464
14	4706.464	4706.464	4706.464	4706.464	4706.464
15	4706.464	4706.464	4706.464	4706.464	4706.464
16	4706.464	4706.464	4706.464	4706.464	4706.464
17	4706.464	4706.464	4706.464	4706.464	4706.464
18	4706.464	4706.464	4706.464	4706.464	4706.464
19	4706.464	4706.464	4706.464	4706.464	4706.464
20	4706.464	4706.464	4706.464	4706.464	4706.464
21	4706.464	4706.464	4706.464	4706.464	4706.464
22	4706.464	4706.464	4706.464	4706.464	4706.464
23	4706.464	4706.464	4706.464	4706.464	4706.464
24	4706.464	4706.464	4706.464	4706.464	4706.464
25	4706.464	4706.464	4706.464	4706.464	4706.464
26	4706.464	4706.464	4706.464	4706.464	4706.464
27	4706.464	4706.464	4706.464	4706.464	4706.464
28	4706.464	4706.464	4706.464	4706.464	4706.464
29	4706.464	4706.464	4706.464	4706.464	4706.464
30	4706.464	4706.464	4706.464	4706.464	4706.464

TABLE A-IV (Continued)

SHIP NO. 913

INPUT VALUES READ WERE	BE =	12.445000,	INCH =	18,	LAMBDA =	42.857140
LRP =	168.330000,					
NEL =	5,	2,	OST =	14		
L(1)...L(5)						
1.218500E CC	1.801850E C1	1.524185E C2	1.692185E C2	1.738585E C2		
LN(1)...LN(5)						
2	4	16	4	4		
C(1)...C(2)						
2.489000E CC	1.453100E C1					
VA(1)...VN(2)						
2	5					
CFS(1,0)...CFS(30,7)						
.000000E CC	.000000E CC	.000000E CC	.000000E CC	.000000E CC	.000000E CC	.000000E CC
.000000E CC	.000000E CC	.000000E CC	.000000E CC	.000000E CC	.000000E CC	5.000000E-01
.000000E CC	.000000E CC	.000000E CC	.000000E CC	.000000E CC	.000000E CC	7.720000E-01
2.110000E-01	1.110000E CC	1.406000E CC	1.593000E CC	1.717000E CC	1.854000E CC	2.925000E CC
6.730000E-01	2.590000E CC	3.124000E CC	3.435000E CC	3.609000E CC	3.783000E CC	5.015000E CC
1.386000E CC	3.980000E CC	4.729000E CC	5.264000E CC	5.488000E CC	5.725000E CC	6.932000E CC
2.360000E CC	5.420000E CC	6.272000E CC	6.969000E CC	7.280000E CC	7.566000E CC	8.587000E CC
4.680000E CC	8.160000E CC	8.935000E CC	9.670000E CC	1.003000E C1	1.025400E C1	1.079000E C1
7.030000E CC	1.004000E C1	1.082700E C1	1.133700E C1	1.157400E C1	1.173500E C1	1.197200E C1

TABLE A-IV (Concluded)

8.868000E CC	1.136000E 01	1.193400E 01	1.217100E 01	1.225800E 01	1.232000E 01	1.237000E 01	1.242000E 01
9.832000E CC	1.200000E 01	1.237000E 01	1.244500E 01	1.244500E 01	1.244500E 01	1.244500E 01	1.244500E 01
1.004300E 01	1.215000E 01	1.244500E 01	1.244500E 01	1.244500E 01	1.244500E 01	1.244500E 01	1.244500E 01
1.004300E 01	1.215000E 01	1.244500E 01	1.244500E 01	1.244500E 01	1.244500E 01	1.244500E 01	1.244500E 01
1.004300E 01	1.215000E 01	1.244500E 01	1.244500E 01	1.244500E 01	1.244500E 01	1.244500E 01	1.244500E 01
1.004300E 01	1.215000E 01	1.244500E 01	1.244500E 01	1.244500E 01	1.244500E 01	1.244500E 01	1.244500E 01
1.004300E 01	1.215000E 01	1.244500E 01	1.244500E 01	1.244500E 01	1.244500E 01	1.244500E 01	1.244500E 01
9.892000E CC	1.208000E 01	1.243200E 01	1.244500E 01	1.244500E 01	1.244500E 01	1.244500E 01	1.244500E 01
9.179000E CC	1.170000E 01	1.218300E 01	1.240700E 01	1.244500E 01	1.244500E 01	1.244500E 01	1.244500E 01
7.874000E CC	1.090000E 01	1.151100E 01	1.214600E 01	1.232000E 01	1.239500E 01	1.244500E 01	1.244500E 01
6.146000E CC	9.200000E 00	1.020500E 01	1.130000E 01	1.186000E 01	1.213400E 01	1.232000E 01	1.244500E 01
4.218000E CC	7.280000E 00	8.301000E 00	9.719000E 00	1.074000E 01	1.146200E 01	1.192200E 01	1.228300E 01
2.440000E CC	5.090000E 00	6.011000E 00	7.367000E 00	8.861000E 00	1.016700E 01	1.118800E 01	1.183500E 01
1.055000E CC	3.020000E 00	3.584000E 00	4.542000E 00	6.073000E 00	8.213000E 00	9.881000E 00	1.088900E 01
5.830000E-01	2.060000E 00	2.452000E 00	3.099000E 00	4.405000E 00	6.894000E 00	8.898000E 00	1.010500E 01
2.810000E-01	1.130000E 00	1.357000E 00	1.680000E 00	2.626000E 00	5.314000E 00	7.641000E 00	9.035000E 00
1.210000E-01	2.800000E-01	3.110000E-01	3.480000E-01	7.590000E-01	3.460000E 00	6.048000E 00	7.591000E 00
.000000E CC	.000000E CC	.000000E CC	.000000E CC	.000000E 00	1.431000E 00	3.982000E 00	5.613000E 00
.000000E CC	.000000E CC	.000000E CC	.000000E CC	.000000E 00	1.050000E 00	3.600000E 00	5.040000E 00
.000000E CC	.000000E CC	.000000E CC	.000000E CC	.000000E 00	3.600000E-01	2.680000E 00	4.120000E 00
.000000E CC	.000000E CC	.000000E CC	.000000E CC	.000000E 00	.000000E 00	1.540000E 00	2.860000E 00
.000000E CC	.000000E CC	.000000E CC	.000000E CC	.000000E 00	.000000E 00	.000000E 00	.000000E 00

TABLE A-V

CURVES OF FORM FOR THE SERIES 60, $C_B = .80$

CALCULATIONS FOR THE CURVES OF FORM AND BONJEAN CURVES

SHIP NO. 932

R. A. YAGLE, H. C. KIM

BASIC DIMENSIONS

THE LENGTH BETWEEN PERPENDICULARS IS 600.000 FEET

THE MOLDED HALF BEAM IS 46.154 FEET

THERE ARE 5 DIFFERENT STATION SPACINGS ALONG THE SHIP

THERE ARE 2 DIFFERENT WATERLINE SPACINGS UP THE SHIP

MIDSHIP IS LOCATED AT STATION 14

CALCULATED ON 8/22/62

TABLE A-V (Continued)

WATERPLANE CALCULATIONS
SHIP NO. 932

CF IS IN FEET FORWARD (+) OR AFT (-) OF MIDSHIPS						
WATERLINE	WP AREAS	CF (FROM MID.)	TONS PER INCH	WP COEFF.	TRANSV. I. COEFF.	LONG. I. COEFF.
.000	32140	23.576	76.523	.5803	.34048	.35700
4.616	41220	21.491	98.144	.7443	.59963	.53233
9.232	43773	20.374	102.556	.7777	.65327	.57987
18.465	44870	17.108	106.833	.8102	.70209	.63474
27.698	46371	11.968	110.408	.8373	.73866	.68834
36.931	48471	2.357	115.408	.8752	.77548	.77998
46.164	51331	-4.953	119.835	.9088	.81523	.86215
55.396	51655	-7.496	122.987	.9327	.85086	.91897

MOLDED DISPLACEMENTS
SHIP NO. 932

ALL VALUES ARE IN LONG TONS		
WATERLINE	DISP. SALT WATER	DISP. FRESH WATER
4.616	4917	4780
9.232	10555	10262
18.465	22211	21594
27.698	34252	33300
36.931	46748 ✓	45450
46.164	59785	58124
55.396	73249	71214

TABLE A-V (Continued)

LONGITUDINAL AND VERTICAL CENTERS OF BUOYANCY
SHIP NO.932

VCG IS IN FEET ABOVE THE BASELINE		
WATERLINE	VCB	LCB
4.616	2.514	22.347
9.232	4.826	21.570
18.465	9.554	20.144
27.698	14.316	18.222
36.931	19.140	15.346
46.164	24.031	11.673
55.396	28.949	8.314

TRANSVERSE AND LONGITUDINAL METACENTRIC HEIGHTS
SHIP NO.932

ALL VALUES ARE IN FEET ABOVE THE BASE LINE		
WATERLINE	KM TRANS.	KM LONG.
4.616	80.317	3449.201
9.232	68.656	2399.014
18.465	42.601	1248.936
27.698	37.347	894.048
36.931	36.894	718.138
46.164	38.606	643.369
55.396	41.454	587.708

TABLE A-V (Continued)

MOMENT TO TRIM ONE INCH AND
CHANGES IN DISPLACEMENT FOR A ONE INCH TRIM AFT
SHIP NO.932

THE MOMENTS ARE IN FOOT LONG TONS
THE CHANGE IN DISP. IS IN LONG TONS

WATERLINE	MOM. TO TRIM 1 IN.	CHANGE IN DISP.
4.616	2353.837	-3.515
9.232	3823.271	-3.482
18.465	4185.048	-3.046
27.698	4538.449	-2.202
36.931	5142.671	-1.453
46.164	5684.491	.989
55.396	6059.123	1.536

BLOCK, PRISMATIC, MIDSHIP, AND VERTICAL PRISMATIC COEFFICIENTS
SHIP NO.932

WATERLINE	BLOCK	PRISMATIC	MIDSHIP	VERTICAL PRISMATIC
4.616	.6732	.7221	.9322	.9045
9.232	.7225	.7451	.9697	.9290
18.465	.7601	.7711	.9857	.9383
27.698	.7815	.7890	.9955	.9334
36.931	.7999	.8057	.9929	.9140
46.164	.8184	.8231	.9943	.9006
55.396	.8356	.8396	.9952	.8959

TABLE A-V (Continued)

SECTIONAL AREAS FROM HONJEAN CURVES
SHIP NO. 932

LOCATION OF STATIONS	STATION	DISTANCE FROM STA. 0
	0	.000
	1	2.176
	2	4.352
	3	19.352
	4	34.352
	5	49.352
	6	64.352
	7	94.352
	8	124.352
	9	154.352
	10	184.352
	11	214.352
	12	244.352
	13	274.352
	14	304.352
	15	334.352
	16	364.352
	17	394.352
	18	424.352
	19	454.352
	20	484.352
	21	514.352
	22	544.352
	23	559.352
	24	574.352
	25	589.352
	26	604.352
	27	608.495
	28	612.637
	29	616.780
	30	620.923

TABLE A-V (Continued)

SECTIONAL AREAS	WATERLINES					55.396
	4.616	9.232	18.465	27.692	36.931	
STATION	AREAS (SQ. FT.)					
C	.000	.000	.000	.000	.000	.000
1	.000	.000	.000	.000	.000	21.433
2	.000	.000	.000	.000	.000	75.442
3	54.165	148.802	364.870	589.564	824.685	1080.961
4	112.236	288.175	689.238	1113.787	1551.562	2008.984
5	167.173	406.324	937.947	1507.840	2097.193	2735.061
6	214.765	502.481	1145.334	1817.157	2516.318	3232.751
7	304.183	667.022	1434.720	2233.071	3046.018	3875.250
8	366.326	774.082	1606.948	2450.089	3299.770	4151.886
9	393.237	819.166	1670.433	2521.926	3374.327	4226.566
10	397.207	826.365	1680.133	2532.391	3384.649	4236.908
11	397.207	826.365	1680.133	2532.391	3384.649	4236.908
12	397.207	826.365	1680.133	2532.391	3384.649	4236.908
13	397.207	826.365	1680.133	2532.391	3384.649	4236.908
14	397.207	826.365	1680.133	2532.391	3384.649	4236.908
15	397.207	826.365	1680.133	2532.391	3384.649	4236.908
16	395.724	824.122	1678.477	2530.735	3382.994	4235.252
17	385.522	809.736	1664.310	2516.854	3369.113	4221.371
18	353.308	755.332	1592.258	2442.401	3295.297	4147.555
19	300.514	662.571	1441.803	2259.702	3095.974	3941.978
20	232.653	531.958	1199.594	1939.788	2726.307	3541.145
21	159.312	379.408	893.075	1498.937	2189.181	2943.280
22	91.621	228.594	555.083	972.617	1513.505	2173.847
23	63.243	159.243	384.375	688.125	1127.510	1719.166
24	34.483	88.519	214.317	392.791	709.055	1214.065
25	8.740	21.948	51.017	93.840	257.075	646.492
26	.000	.000	.000	.000	56.799	279.080
27	.000	.000	.000	.000	36.547	285.761
28	.000	.000	.000	.000	12.915	119.313
29	.000	.000	.000	.000	.000	52.210
30	.000	.000	.000	.000	.000	.000

TABLE A-V (Continued)

SHIP NO. 932

INPUT VALUES READ WERE		LBP =	168.000000,	BE =	12.923000,	INCH =	IB,	LAMBDA =	42.857142
		NBL =	5,	NBY =	2,	DST =	14		
L(1)...L(5)									
1.218500E 00	1.871850E 01	1.524185E 02	1.692185E 02	1.738585E 02					
LN(1)...LN(5)									
2	4	16	4	4					
D(1)...D(2)									
2.585000E 00	1.591100E 01								
VN(1)...VN(2)									
2	5								
DFS(0,0)...DFS(30,7)									
.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00
.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E-01
.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00	1.266000E 00
5.820000E-01	2.480000E 00	3.037000E 00	3.334000E 00	3.450000E 00	3.696000E 00	4.110000E 00	4.885000E 00	4.885000E 00	
1.758000E 00	4.710000E 00	5.622000E 00	6.281000E 00	6.526000E 00	6.746000E 00	7.158000E 00	7.922000E 00	7.922000E 00	
3.142000E 00	6.500000E 00	7.508000E 00	8.400000E 00	8.801000E 00	9.046000E 00	9.408000E 00	1.006700E 01	1.006700E 01	
4.647000E 00	8.000000E 00	9.072000E 00	1.000200E 01	1.044200E 01	1.072600E 01	1.101000E 01	1.150100E 01	1.150100E 01	
7.646000E 00	1.046000E 01	1.120400E 01	1.190200E 01	1.225100E 01	1.245800E 01	1.260000E 01	1.271600E 01	1.271600E 01	
9.919000E 00	1.272000E 01	1.243200E 01	1.270300E 01	1.284500E 01	1.291000E 01	1.292300E 01	1.292300E 01	1.292300E 01	

TABLE A-VI

CURVES OF FORM FOR THE U OF M "V" SERIES, $C_B = .60$

CALCULATIONS FOR THE CURVES OF FORM AND BUNJEAN CURVES
SHIP NO. 924

R. A. YAGLE, H. C. KIM

BASIC DIMENSIONS

THE LENGTH BETWEEN PERPENDICULARS IS 600.000 FEET
THE MIDDLE HALF BEAM IS 40.000 FEET
THERE ARE 5 DIFFERENT STATION SPACINGS ALONG THE SHIP
THERE ARE 2 DIFFERENT WATERLINE SPACINGS UP THE SHIP
MIDSHIP IS LOCATED AT STATION 14

CALCULATED ON 8/22/62

TABLE A-VI (Continued)

WATERPLANE CALCULATIONS
SHIP NC.924

CF IS IN FEET FORWARD (+) OR AFT (-) OF MIDSHIPS	WP AREAS	CF (FROM MID.)	ICNS PER INCH	WP COEFF.	TRANSV. I. COEFF.	LCNG. I. COEFF.
.000	13372	-12.640	31.839	.2786	.36410	.10113
4.000	22024	-9.874	52.439	.4588	.24833	.22037
8.000	25438	-7.580	60.567	.5300	.33836	.27478
15.999	29533	-5.125	70.316	.6153	.44799	.35610
23.997	32918	-7.760	78.377	.6858	.53529	.44423
31.996	37208	-10.338	88.590	.7752	.63599	.59496
39.994	40272	-21.917	95.885	.8390	.71196	.72093
47.993	42364	-20.704	100.868	.8826	.76876	.81418

ALL VALUES ARE IN LONG TONS

WATERLINE	DISP. SALT WATER	DISP. FRESH WATER
4.000	2073	2015
8.000	4835	4700
15.999	11185	10875
23.997	18335	17825
31.996	26331	25599
39.994	35207	34229
47.993	44668	43427

TABLE A-VI (Continued)

LONGITUDINAL AND VERTICAL CENTERS OF BUOYANCY
SHIP NO. 924

VCB IS IN FEET ABOVE THE BASELINE		
WATERLINE	VCB	LCB
4.000	2.303	-10.992
8.000	4.300	-9.706
15.999	8.712	-7.693
23.997	13.132	-7.077
31.996	17.679	-8.764
39.994	22.302	-11.756
47.993	26.899	-13.856

TRANSVERSE AND LONGITUDINAL METACENTRIC HEIGHTS
SHIP NO. 924

ALL VALUES ARE IN FEET ABOVE THE BASE LINE		
WATERLINE	KM. TRANS.	KM. LONG.
4.000	31.983	2009.810
8.000	41.951	1879.764
15.999	30.838	1019.450
23.997	31.004	812.211
31.996	32.548	711.810
39.994	35.515	717.572
47.993	38.557	690.932

TABLE A-VI (Continued)

MOMENT TO TRIM ONE INCH AND
CHANGES IN DISPLACEMENT FOR A ONE INCH TRIM AFT
SHIP NO. 924

THE MOMENTS ARE IN FOOT LONG TONS
THE CHANGE IN DISP. IS IN LONG TONS

WATERLINE	MOM. TO TRIM 1 IN.	CHANGE IN DISP.
4.000	577.871	.863
8.000	1570.185	.765
15.999	2034.846	.601
23.997	2538.450	1.014
31.996	3399.776	2.708
39.994	4119.590	3.503
47.993	4652.459	3.481

BLOCK, PRISMATIC, MIDSHIP, AND VERTICAL PRISMATIC COEFFICIENTS
SHIP NO. 924

WATERLINE	BLOCK	PRISMATIC	MIDSHIP	VERTICAL PRISMATIC
4.000	.3778	.4527	.8345	.8234
8.000	.4407	.4878	.9033	.8315
15.999	.5098	.5350	.9529	.8286
23.997	.5571	.5749	.9690	.8124
31.996	.6001	.6144	.9767	.7741
39.994	.6419	.6541	.9814	.7651
47.993	.6787	.6894	.9845	.7689

TABLE A-VI (Continued)

SECTIONAL AREAS FROM RCNJEAN CURVES
SHIP NC.924

LOCATION OF STATIONS	STATION	DISTANCE FROM STA. C
	0	.000
	1	2.176
	2	4.352
	3	19.352
	4	34.352
	5	49.352
	6	64.352
	7	94.352
	8	124.352
	9	154.352
	10	184.352
	11	214.352
	12	244.352
	13	274.352
	14	304.352
	15	334.352
	16	364.352
	17	394.352
	18	424.352
	19	454.352
	20	484.352
	21	514.352
	22	544.352
	23	559.352
	24	574.352
	25	589.352
	26	604.352
	27	608.495
	28	612.637
	29	616.780
	30	620.923

TABLE A-VI (Continued)

STATION	WATERLINES						
	4.000	8.000	15.999	23.997	31.996	39.994	47.993
C	.000	.000	.000	.000	.000	.000	.000
1	.000	.000	.000	.000	.000	.000	.000
2	.000	.000	.000	.000	.000	.000	.000
3	2.310	7.333	26.346	54.150	97.333	13.807	38.469
4	5.000	16.000	55.548	118.299	211.092	174.176	298.297
5	9.119	28.667	94.019	195.906	339.547	348.829	542.651
6	13.976	44.095	141.537	286.368	484.380	742.572	797.751
7	20.857	83.429	255.745	501.130	814.788	1194.768	1567.036
8	31.333	146.381	418.044	770.648	1196.143	1685.294	2227.626
9	46.400	233.809	608.152	1065.999	1585.215	2155.828	2762.528
10	66.000	329.524	804.007	1348.862	1936.233	2554.884	3191.175
11	90.000	426.857	983.135	1587.218	2212.392	2849.730	3490.125
12	118.809	510.476	1118.238	1749.649	2388.320	3028.477	3668.305
13	151.690	588.381	1192.329	1832.191	2472.252	3112.081	3751.909
14	189.571	657.048	1219.639	1860.272	2500.100	3139.929	3775.757
15	232.452	716.929	1246.115	1847.272	2487.101	3126.929	3766.757
16	280.333	766.810	1272.600	1834.272	2474.101	3114.929	3757.757
17	332.214	807.691	1298.085	1821.272	2461.101	3102.929	3748.757
18	388.095	839.572	1322.570	1808.272	2448.101	3090.929	3739.757
19	447.976	862.453	1347.055	1795.272	2435.101	3078.929	3730.757
20	511.857	876.334	1370.540	1782.272	2422.101	3066.929	3721.757
21	580.738	881.215	1393.025	1769.272	2409.101	3054.929	3712.757
22	654.619	877.096	1414.510	1756.272	2396.101	3042.929	3703.757
23	734.500	863.977	1435.995	1743.272	2383.101	3030.929	3694.757
24	820.381	841.858	1456.480	1730.272	2370.101	3018.929	3685.757
25	912.262	810.739	1475.965	1717.272	2357.101	3006.929	3676.757
26	1010.143	770.620	1494.450	1704.272	2344.101	2994.929	3667.757
27	1114.024	722.501	1511.935	1691.272	2331.101	2982.929	3658.757
28	1223.905	666.382	1528.420	1678.272	2318.101	2970.929	3649.757
29	1339.786	622.263	1543.905	1665.272	2305.101	2958.929	3640.757
30	1462.667	580.144	1558.390	1652.272	2292.101	2946.929	3631.757

AREAS (SQ. FT.)

TABLE A-VI (Continued)

MAP		SYSTEM		SKIP6		SCARDS		SPEEK	
ERROR	CC000*	(MAIN)	10000*	.10H	47637*	.READ	52166*	.PRIN	52231*
.EXIT	00000*	.PCGMT	53012*	ZERU	53123*	.03311	53157*	.ERR	53174*
.PRSLT	52314*	(PRCG)	53371	(SUHT)	74712	(ERAS)	77776		
BNRCC	53256*	21401 LOCS. CAN BE SAFELY USED IN EXPANDING PRCG. (LOCAL)							
SHIP NO. 924									
INPUT VALUES READ WERE									
LBP =	168.000000,	BE =	11.200000,	INCH =		LB,		LAMBDA =	42.857140
NBL =	5,	NRY =	2,	OBT =		14			
L(1)...L(5)									
1.218500E 00	1.801000E 01	1.524185E 02	1.692185E 02	1.738585E 02					
LN(1)...LN(5)									
2	4	16	4	4					
D(1)...D(2)									
2.240000E 00	1.243600E 01								
VN(1)...VN(2)									
2	5								
DFS(3,6)...DFS(30,7)									
.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00
.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00	2.100000E-01	1.070000E 00
.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00	5.800000E-01	1.290000E 00
5.900000E-02	1.220000E-01	2.400000E-01	4.100000E-01	5.600000E-01	1.000000E 00	1.740000E 00	2.640000E 00		
7.000000E-02	2.400000E-01	4.900000E-01	8.900000E-01	1.310000E 00	1.980000E 00	2.880000E 00	3.930000E 00		
10.000000E-02	5.200000E-01	8.300000E-01	1.460000E 00	2.110000E 00	2.950000E 00	4.000000E 00	5.140000E 00		

TABLE A-VII

CURVES OF FORM FOR THE U OF M "V" SERIES, $C_B = .65$

CALCULATIONS FOR THE CURVES OF FORM AND BONJEAN CURVES

SHIP NO. 959

R. A. YAGLE, H. C. KIM

BASIC DIMENSIONS

THE LENGTH BETWEEN PERPENDICULARS IS 600.000 FEET

THE MIDDLE HALF BEAM IS 41.379 FEET

THERE ARE 5 DIFFERENT STATION SPACINGS ALONG THE SHIP

THERE ARE 2 DIFFERENT WATERLINE SPACINGS UP THE SHIP

MIDSHIP IS LOCATED AT STATION 14

CALCULATED ON 8/22/62

TABLE A-VII (Continued)

WATERPLANE CALCULATIONS
SHIP NO. 959

CF IS IN FEET FORWARD (+) OR AFT (-) OF MIDSHIPS	WATERLINE	WP AREAS	CF (FROM MID.)	TONS PER INCH	WP COEFF.	TRANSV. I. COEFF.	LONG. I. COEFF.
	.000	16163	-5.363	38.484	.3255	.11612	.12691
	4.137	25611	-3.819	60.978	.5158	.31231	.26486
	8.275	29207	-1.669	69.540	.5882	.40992	.32822
	16.551	33053	-.356	78.699	.6657	.51086	.41475
	24.828	36027	-2.066	85.778	.7256	.58741	.49844
	33.104	40055	-12.774	95.369	.8067	.67777	.64847
	41.381	42712	-16.989	101.695	.8602	.74364	.76002
	49.657	44456	-17.178	105.847	.8953	.78700	.84088

MOLDED DISPLACEMENTS
SHIP NO. 959

ALL VALUES ARE IN LONG TONS	
WATERLINE	DISP. SALT WATER
4.137	2527
8.275	5825
16.551	13274
24.828	21459
33.104	30433
41.381	40246
49.657	50571

WATERLINE	DISP. FRESH WATER
4.137	2457
8.275	5663
16.551	12905
24.828	20863
33.104	29588
41.381	39128
49.657	49166

TABLE A-VII (Continued)

LONGITUDINAL AND VERTICAL CENTERS OF BUOYANCY
SHIP NO.959

VCB IS IN FEET ABOVE THE BASELINE		
WATERLINE	VCB	LCB
4.137	2.363	-4.551
8.275	4.503	-3.563
16.551	8.934	-1.981
24.828	13.431	-1.609
33.104	18.042	-3.169
41.381	22.726	-6.141
49.657	27.381	-8.437

TRANSVERSE AND LONGITUDINAL METACENTRIC HEIGHTS
SHIP NO.959

ALL VALUES ARE IN FEET ABOVE THE BASE LINE		
WATERLINE	KM TRANS.	KM LONG.
4.137	39.573	2140.537
8.275	47.918	1939.860
16.551	33.939	1061.329
24.828	32.707	836.034
33.104	33.670	715.106
41.381	36.362	708.493
49.657	39.287	667.019

TABLE A-VII (Continued)

MOMENT TO TRIM ONE INCH AND
CHANGES IN DISPLACEMENT FOR A ONE INCH TRIM AFT
SHIP NO. 959

THE MOMENTS ARE IN FOOT LONG TONS
THE CHANGE IN DISP. IS IN LONG TONS

WATERLINE	MOM. TO TRIM 1 IN.	CHANGE IN DISP.
4.137	750.254	.388
8.275	1940.177	.193
16.551	2451.663	.047
24.828	2946.390	.295
33.104	3833.279	2.030
41.381	4492.625	2.879
49.657	4970.656	3.030

BLCK, PRISMATIC, MIDSHIP, AND VERTICAL PRISMATIC COEFFICIENTS
SHIP NO. 959

WATERLINE	BLCK	PRISMATIC	MIDSHIP	VERTICAL PRISMATIC
4.137	.4305	.5040	.8542	.8346
8.275	.4961	.5408	.9174	.8435
16.551	.5653	.5878	.9617	.8492
24.828	.6092	.6251	.9747	.8397
33.104	.6480	.6606	.9810	.8033
41.381	.6856	.6961	.9848	.7970
49.657	.7178	.7271	.9873	.8018

TABLE A-VII (Continued)

SECTIONAL AREAS FROM BENJAN CURVES
SHIP NO. 959

LOCATION OF STATIONS	STATION	DISTANCE FROM STA. 0
	C	.000
	1	2.176
	2	4.352
	3	19.352
	4	34.352
	5	49.352
	6	64.352
	7	94.352
	8	124.352
	9	154.352
	10	184.352
	11	214.352
	12	244.352
	13	274.352
	14	304.352
	15	334.352
	16	364.352
	17	394.352
	18	424.352
	19	454.352
	20	484.352
	21	514.352
	22	544.352
	23	559.352
	24	574.352
	25	589.352
	26	604.352
	27	608.495
	28	612.637
	29	616.780
	30	620.923

TABLE A-VII (Continued)

SHIP NO. 959

INPUT VALUES READ HERE	BE =	11.586000,	INCH =	LB,	LAMBDA =
LBP =	168.000000,				42.857140
NEL =	5,	NBV =	2,	14	
L(1)...L(5)					
1.218500E 00	1.601850E 01	1.524185E 02	1.692185E 02	1.738585E 02	
LN(1)...LN(5)					
2	4	16	4	4	
D(1)...D(2)					
2.317500E 00	1.353400E 01				
VN(1)...VN(2)					
2	5				
OFS(0,0)...OFS(30,7)					
.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00
.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00	3.800000E-01
.000000E 00	.000000E 00	.000000E 00	.000000E 00	5.000000E-02	8.820000E-01
1.100000E-01	2.200000E-01	3.400000E-01	5.800000E-01	8.900000E-01	1.910000E 00
1.100000E-01	3.500000E-01	6.900000E-01	1.270000E 00	1.880000E 00	3.768000E 00
1.100000E-01	7.160000E-01	1.220000E 00	2.086000E 00	2.970000E 00	5.228000E 00
1.640000E-01	1.119000E 00	1.818000E 00	3.036000E 00	4.170000E 00	6.780000E 00
5.600000E-01	2.286000E 00	3.480000E 00	5.130000E 00	6.490000E 00	8.820000E 00
1.440000E 00	4.230000E 00	5.540000E 00	7.286000E 00	8.600000E 00	9.580000E 00
					1.013800E 01
					1.044400E 01

TABLE A-VIII

CURVES OF FORM FOR THE U OF M "V" SERIES, $C_B = .70$

CALCULATIONS FOR THE CURVES OF FORM AND RONJEAN CURVES

SHIP NO. 956

R. A. YAGLE, H. C. KIM

BASIC DIMENSIONS

THE LENGTH BETWEEN PERPENDICULARS IS 600.000 FEET

THE MIDDLE HALF BEAM IS 42.854 FEET

THERE ARE 5 DIFFERENT STATION SPACINGS ALONG THE SHIP

THERE ARE 2 DIFFERENT WATERLINE SPACINGS UP THE SHIP

MIDSHIP IS LOCATED AT STATION 14

CALCULATED ON 8/22/62

TAFIE A-VIII (Continued)

WATERPLANE CALCULATIONS
SHIP NO. 958

CF IS IN FEET FORWARD (+) OR AFT (-) OF MIDSHIPS	WP AREAS	CF (FROM MID.)	TONS PER INCH	WP COEFF.	TRANSV. I. COEFF.	LONG. I. COEFF.
WATERLINE						
0.000	19736	2.022	46.990	.3838	.16135	.16410
4.286	31722	3.352	73.123	.5972	.42515	.33306
8.571	33305	4.369	79.298	.6477	.49074	.38926
17.144	36734	5.295	87.463	.7143	.57681	.47737
25.717	39486	3.662	94.014	.7678	.64422	.56278
34.290	43350	-6.004	103.215	.8430	.73242	.71230
42.863	46354	-10.203	109.653	.8956	.80512	.82675
51.436	47633	-9.993	113.531	.9272	.84680	.90239

MOLODED DISPLACEMENTS
SHIP NO. 958

ALL VALUES ARE IN LONG TONS	DISP. SALT WATER	DISP. FRESH WATER
WATERLINE		
4.286	3174	3086
8.571	7179	6980
17.144	15805	15366
25.717	25153	24454
34.290	35275	34295
42.863	46248	44964
51.436	57750	56146

TABLE A-VIII (Continued)

LONGITUDINAL AND VERTICAL CENTERS OF BUOYANCY
SHIP NO. 958

VCB IS IN FEET ABOVE THE BASELINE		
WATERLINE	VCH	LCB
4.286	2.467	2.821
8.571	4.616	3.395
17.144	9.126	4.240
25.717	13.711	4.395
34.290	18.414	2.936
42.863	23.211	.221
51.436	27.971	-1.902

TRANSVERSE AND LONGITUDINAL METACENTRIC HEIGHTS
SHIP NO. 958

ALL VALUES ARE IN FEET ABOVE THE BASE LINE		
WATERLINE	KM TRANS.	KM LONG.
4.286	48.185	2281.226
8.571	57.880	2049.548
17.144	37.053	1094.741
25.717	34.337	850.251
34.290	34.839	721.626
42.863	37.445	702.072
51.436	40.510	658.990

TABLE A-VIII (Continued)

MOMENT TO TRIM ONE INCH AND
 CHANGES IN DISPLACEMENT FOR A ONE INCH TRIM AFT
 SHIP NC-958

THE MOMENTS ARE IN FOOT LONG TONS
 THE CHANGE IN DISP. IS IN LONG TONS

WATERLINE	MOM. TO TRIM 1 IN.	CHANGE IN DISP.
4.280	1004.601	-0.408
8.571	2383.010	-0.577
17.144	2922.440	-0.772
25.717	3445.276	-0.574
34.290	4360.640	1.033
42.863	5001.311	1.865
51.436	5524.385	1.891

BLOCK, PRISMATIC, MIDSHIP, AND VERTICAL PRISMATIC COEFFICIENTS
 SHIP NC-958

WATERLINE	BLOCK	PRISMATIC	MIDSHIP	VERTICAL PRISMATIC
4.280	.5041	.5659	.8907	.8441
8.571	.5701	.6017	.9474	.8802
17.144	.6274	.6434	.9752	.8783
25.717	.6657	.6768	.9835	.8670
34.290	.7002	.7089	.9877	.8306
42.863	.7344	.7417	.9901	.8200
51.436	.7642	.7705	.9918	.8241

TABLE A-VIII (Continued)

SECTIONAL AREAS FROM BDNJEAN CURVES
SHIP NO. 958

LOCATION OF STATIONS	STATION	DISTANCE FROM STA. 0
	0	.000
	1	2.176
	2	4.352
	3	19.352
	4	34.352
	5	49.352
	6	64.352
	7	79.352
	8	94.352
	9	109.352
	10	124.352
	11	139.352
	12	154.352
	13	169.352
	14	184.352
	15	199.352
	16	214.352
	17	229.352
	18	244.352
	19	259.352
	20	274.352
	21	289.352
	22	304.352
	23	319.352
	24	334.352
	25	349.352
	26	364.352
	27	379.352
	28	394.352
	29	409.352
	30	424.352
	31	439.352
	32	454.352
	33	469.352
	34	484.352
	35	499.352
	36	514.352
	37	529.352
	38	544.352
	39	559.352
	40	574.352
	41	589.352
	42	604.352
	43	619.352
	44	634.352
	45	649.352
	46	664.352
	47	679.352
	48	694.352
	49	709.352
	50	724.352
	51	739.352
	52	754.352
	53	769.352
	54	784.352
	55	799.352
	56	814.352
	57	829.352
	58	844.352
	59	859.352
	60	874.352
	61	889.352
	62	904.352
	63	919.352
	64	934.352
	65	949.352
	66	964.352
	67	979.352
	68	994.352
	69	1009.352
	70	1024.352
	71	1039.352
	72	1054.352
	73	1069.352
	74	1084.352
	75	1099.352
	76	1114.352
	77	1129.352
	78	1144.352
	79	1159.352
	80	1174.352
	81	1189.352
	82	1204.352
	83	1219.352
	84	1234.352
	85	1249.352
	86	1264.352
	87	1279.352
	88	1294.352
	89	1309.352
	90	1324.352
	91	1339.352
	92	1354.352
	93	1369.352
	94	1384.352
	95	1399.352
	96	1414.352
	97	1429.352
	98	1444.352
	99	1459.352
	100	1474.352
	101	1489.352
	102	1504.352
	103	1519.352
	104	1534.352
	105	1549.352
	106	1564.352
	107	1579.352
	108	1594.352
	109	1609.352
	110	1624.352
	111	1639.352
	112	1654.352
	113	1669.352
	114	1684.352
	115	1699.352
	116	1714.352
	117	1729.352
	118	1744.352
	119	1759.352
	120	1774.352
	121	1789.352
	122	1804.352
	123	1819.352
	124	1834.352
	125	1849.352
	126	1864.352
	127	1879.352
	128	1894.352
	129	1909.352
	130	1924.352
	131	1939.352
	132	1954.352
	133	1969.352
	134	1984.352
	135	1999.352
	136	2014.352
	137	2029.352
	138	2044.352
	139	2059.352
	140	2074.352
	141	2089.352
	142	2104.352
	143	2119.352
	144	2134.352
	145	2149.352
	146	2164.352
	147	2179.352
	148	2194.352
	149	2209.352
	150	2224.352
	151	2239.352
	152	2254.352
	153	2269.352
	154	2284.352
	155	2299.352
	156	2314.352
	157	2329.352
	158	2344.352
	159	2359.352
	160	2374.352
	161	2389.352
	162	2404.352
	163	2419.352
	164	2434.352
	165	2449.352
	166	2464.352
	167	2479.352
	168	2494.352
	169	2509.352
	170	2524.352
	171	2539.352
	172	2554.352
	173	2569.352
	174	2584.352
	175	2599.352
	176	2614.352
	177	2629.352
	178	2644.352
	179	2659.352
	180	2674.352
	181	2689.352
	182	2704.352
	183	2719.352
	184	2734.352
	185	2749.352
	186	2764.352
	187	2779.352
	188	2794.352
	189	2809.352
	190	2824.352
	191	2839.352
	192	2854.352
	193	2869.352
	194	2884.352
	195	2899.352
	196	2914.352
	197	2929.352
	198	2944.352
	199	2959.352
	200	2974.352
	201	2989.352
	202	3004.352
	203	3019.352
	204	3034.352
	205	3049.352
	206	3064.352
	207	3079.352
	208	3094.352
	209	3109.352
	210	3124.352
	211	3139.352
	212	3154.352
	213	3169.352
	214	3184.352
	215	3199.352
	216	3214.352
	217	3229.352
	218	3244.352
	219	3259.352
	220	3274.352
	221	3289.352
	222	3304.352
	223	3319.352
	224	3334.352
	225	3349.352
	226	3364.352
	227	3379.352
	228	3394.352
	229	3409.352
	230	3424.352
	231	3439.352
	232	3454.352
	233	3469.352
	234	3484.352
	235	3499.352
	236	3514.352
	237	3529.352
	238	3544.352
	239	3559.352
	240	3574.352
	241	3589.352
	242	3604.352
	243	3619.352
	244	3634.352
	245	3649.352
	246	3664.352
	247	3679.352
	248	3694.352
	249	3709.352
	250	3724.352
	251	3739.352
	252	3754.352
	253	3769.352
	254	3784.352
	255	3799.352
	256	3814.352
	257	3829.352
	258	3844.352
	259	3859.352
	260	3874.352
	261	3889.352
	262	3904.352
	263	3919.352
	264	3934.352
	265	3949.352
	266	3964.352
	267	3979.352
	268	3994.352
	269	4009.352
	270	4024.352
	271	4039.352
	272	4054.352
	273	4069.352
	274	4084.352
	275	4099.352
	276	4114.352
	277	4129.352
	278	4144.352
	279	4159.352
	280	4174.352
	281	4189.352
	282	4204.352
	283	4219.352
	284	4234.352
	285	4249.352
	286	4264.352
	287	4279.352
	288	4294.352
	289	4309.352
	290	4324.352
	291	4339.352
	292	4354.352
	293	4369.352
	294	4384.352
	295	4399.352
	296	4414.352
	297	4429.352
	298	4444.352
	299	4459.352
	300	4474.352
	301	4489.352
	302	4504.352
	303	4519.352
	304	4534.352
	305	4549.352
	306	4564.352
	307	4579.352
	308	4594.352
	309	4609.352
	310	4624.352
	311	4639.352
	312	4654.352
	313	4669.352
	314	4684.352
	315	4699.352
	316	4714.352
	317	4729.352
	318	4744.352
	319	4759.352
	320	4774.352
	321	4789.352
	322	4804.352
	323	4819.352
	324	4834.352
	325	4849.352
	326	4864.352
	327	4879.352
	328	4894.352
	329	4909.352
	330	4924.352
	331	4939.352
	332	4954.352
	333	4969.352
	334	4984.352
	335	4999.352
	336	5014.352
	337	5029.352
	338	5044.352
	339	5059.352
	340	5074.352
	341	5089.352
	342	5104.352
	343	5119.352
	344	5134.352
	345	5149.352
	346	5164.352
	347	5179.352
	348	5194.352
	349	5209.352
	350	5224.352
	351	5239.352
	352	5254.352
	353	5269.352

TABLE A-VIII (Continued)

SECTIONAL AREAS	WATERLINES					
	4.286	8.571	17.144	25.717	34.290	42.863
STATION						
0	.000	.000	.000	.000	.000	.000
1	.000	.000	.000	.000	.000	.000
2	.000	.000	.000	.000	.000	.000
3	5.168	10.673	56.789	123.484	225.695	378.118
4	5.758	32.786	119.434	265.938	476.381	753.213
5	19.747	64.337	216.513	454.410	774.259	1173.458
6	34.135	100.459	332.050	658.176	1079.215	1588.637
7	85.324	235.133	623.377	1107.284	1669.980	2303.402
8	152.360	383.439	919.951	1528.020	2184.966	2993.046
9	214.089	507.500	1148.391	1836.057	2550.819	3282.650
10	272.997	610.847	1316.408	2045.203	2778.667	3513.723
11	310.319	672.173	1401.319	2137.396	2872.151	3606.900
12	326.084	695.132	1432.120	2166.997	2901.752	3636.507
13	327.168	696.000	1432.987	2167.864	2902.619	3637.374
14	327.168	696.000	1432.987	2167.864	2902.619	3637.374
15	326.780	695.694	1432.681	2167.558	2902.313	3637.068
16	316.569	680.965	1413.789	2149.356	2884.111	3618.865
17	251.597	642.796	1363.026	2097.204	2832.362	3567.117
18	247.525	644.633	1245.973	1984.460	2695.168	3430.734
19	189.837	451.306	1049.476	1726.068	2443.815	3179.514
20	132.324	329.500	805.677	1389.958	2059.559	2779.955
21	82.594	216.296	549.939	988.889	1565.516	2253.385
22	42.467	116.969	307.152	568.726	982.468	1585.732
23	25.635	72.010	196.175	373.745	690.645	1225.223
24	14.064	38.459	101.892	193.081	404.187	828.492
25	4.435	12.857	29.629	51.112	155.976	450.719
26	.000	.000	.000	.000	29.086	168.242
27	.000	.000	.000	.000	9.695	97.924
28	.000	.000	.000	.000	4.848	62.102
29	.000	.000	.000	.000	.000	21.432
30	.000	.000	.000	.000	.000	.000

AREAS (SQ. FT.)

51.436

42.863

34.290

25.717

17.144

8.571

4.286

TABLE A-VIII (Continued)

SHIP NO. 958

INPUT VALUES READ WERE		BL =	11.995000,	INCH =	13,	LAMBDA =
LBP =	168.000000,	NBV =	2,	OST =	14	42.857140
NBL =	5,					
L(1)...L(5)						
1.218500E 06	1.801850E 01	1.524185E 02	1.692185E 02	1.738585E 02		
LN(1)...LN(5)						
2	4	16	4	4		
D(1)...D(2)						
2.400000E 00	1.440200E 01					
VA(1)...VA(2)						
2	5					
DFS(0,0)...DFS(30,7)						
.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00
.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00	1.090000E 00
.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00	1.530000E 00
4.600000E-02	2.870000E-01	4.600000E-01	8.600000E-01	1.330000E 00	2.960000E 00	4.010000E 00
9.300000E-02	5.400000E-01	9.600000E-01	1.890000E 00	2.910000E 00	3.970000E 00	5.080000E 00
1.570000E-01	1.052000E 00	1.780000E 00	3.200000E 00	4.560000E 00	5.880000E 00	7.150000E 00
3.050000E-01	1.832000E 00	2.800000E 00	4.920000E 00	6.110000E 00	7.630000E 00	8.960000E 00
1.147000E 00	4.134000E 00	5.360000E 00	7.180000E 00	8.590000E 00	9.810000E 00	1.084000E 01
2.757000E 00	6.730000E 00	7.900000E 00	9.430000E 00	1.034000E 01	1.109000E 01	1.168000E 01

TABLE A-IX

CURVES OF FORM FOR THE U OF M "V" SERIES, $C_B = .75$

CALCULATIONS FOR THE CURVES OF FORM AND FONJEAN CURVES
SHIP NO. 952 E

R. A. YAGLE, H. C. KIM

BASIC DIMENSIONS

THE LENGTH BETWEEN PERPENDICULARS IS 600.000 FEET

THE MIDDLE HALF BEAM IS 44.446 FEET

THERE ARE 5 DIFFERENT STATION SPACINGS ALONG THE SHIP

THERE ARE 2 DIFFERENT WATERLINE SPACINGS UP THE SHIP

MIDSHIP IS LOCATED AT STATION 14

CALCULATED ON 6/19/1962

TABLE A-IX (Continued)

WATERPLANE CALCULATIONS
SHIP NO. 952 E

CF IS IN FEET FORWARD (+) OR AFT (-) OF MIDSHIPS	WP AREAS	CF (FROM MID.)	TONS PER INCH	WP COEFF.	TRANSV. I. COEFF.	LONG. I. COEFF.
WATERLINE						
0.00	22861	6.389	56.813	.4474	.21630	.21523
4.445	34304	9.169	82.151	.6469	.48446	.39160
8.889	37497	10.427	89.279	.7030	.56796	.45727
17.776	41773	12.081	97.078	.7645	.64827	.55048
26.664	43564	9.359	103.724	.8168	.71654	.64528
35.551	47033	-7.008	111.984	.8818	.79321	.78974
44.438	47167	-5.690	117.064	.9218	.84603	.88586
53.325	50275	-6.376	119.702	.9426	.87264	.93953

MOLDED DISPLACEMENTS
SHIP NO. 952 E

ALL VALUES ARE IN LONG TONS	DISP. SALT WATER	DISP. FRESH WATER
WATERLINE		
4.445	3787	3682
8.889	8439	8205
17.776	18453	17940
26.664	29171	28360
35.551	40658	39529
44.438	52900	51431
53.325	65547	63726

TABLE A-IX (Continued)

LONGITUDINAL AND VERTICAL CENTERS OF BUOYANCY
SHIP NO. 952 E

VC ₆ IS IN FEET ABOVE THE BASELINE		
WATERLINE	VCB	LCB
4.445	2.497	8.126
8.889	4.749	9.087
17.776	9.403	10.305
26.664	14.126	10.565
35.551	18.944	8.925
44.438	23.816	6.032
53.325	28.651	3.639

TRANSVERSE AND LONGITUDINAL METACENTRIC HEIGHTS
SHIP NO. 952 E

ALL VALUES ARE IN FEET ABOVE THE BASE LINE.		
WATERLINE	KM. TRANS.	KM. LONG.
4.445	59.814	2600.841
8.889	62.352	2126.037
17.776	40.289	1142.277
26.664	36.426	876.847
35.551	36.629	744.496
44.438	38.863	706.311
53.325	41.603	646.505

TABLE A-IX (Continued)

MOMENT TO TRIM ONE INCH AND
CHANGES IN DISPLACEMENT FOR A ONE INCH TRIM AFT
SHIP NO. 952 E

THE MOMENTS ARE IN FOOT LONG TONS
THE CHANGE IN DISP. IS IN LONG TONS

WATERLINE	MDM. TO TRIM 1 IN.	CHANGE IN DISP.
4.445	1366.592	-1.258
8.889	2903.456	-1.552
17.776	3495.290	-1.955
26.664	4097.198	-1.609
35.551	5014.462	.132
44.438	5624.781	1.110
53.325	5965.558	1.272

BLOCK, PRISMATIC, MIDSHIP, AND VERTICAL PRISMATIC COEFFICIENTS
SHIP NO. 952 E

WATERLINE	BLOCK	PRISMATIC	MIDSHIP	VERTICAL PRISMATIC
4.445	.5591	.6229	.8975	.8643
8.889	.6230	.6559	.9498	.8862
17.776	.6812	.6969	.9775	.8911
26.664	.7179	.7289	.9850	.8790
35.551	.7505	.7591	.9887	.8511
44.438	.7812	.7883	.9910	.8474
53.325	.8066	.8127	.9925	.8557

TABLE A-IX (Continued)

SECTIONAL AREAS FROM BONJEAN CURVES
SHIP NO. 952 E

LOCATION OF STATIONS	STATION	DISTANCE FROM STA. C
	0	.000
	1	2.176
	2	4.352
	3	19.352
	4	34.352
	5	49.352
	6	64.352
	7	94.352
	8	124.352
	9	154.352
	10	184.352
	11	214.352
	12	244.352
	13	274.352
	14	304.352
	15	334.352
	16	364.352
	17	394.352
	18	424.352
	19	454.352
	20	484.352
	21	514.352
	22	544.352
	23	559.352
	24	574.352
	25	589.352
	26	604.352
	27	608.495
	28	612.637
	29	616.780
	30	620.923

TABLE A-IX (Continued)

SECTIONAL AREAS	WATERLINES				
	4.445	8.889	17.776	26.664	35.551
STATION	AREAS (SQ. FT.)				
0	.000	.000	.000	.000	.000
1	.000	.000	.000	.000	.000
2	.000	.000	.000	.000	.000
3	6.297	23.079	90.569	206.525	375.380
4	21.324	65.823	223.250	471.561	810.436
5	38.626	122.333	387.392	771.972	1266.161
6	64.553	192.601	566.491	1072.423	1681.721
7	138.472	364.249	925.897	1600.156	2337.259
8	221.227	533.569	1445.053	2008.405	2794.705
9	295.675	734.636	1525.592	2238.050	3028.079
10	340.174	750.562	1544.585	2319.728	3159.731
11	354.606	750.562	1544.585	2334.588	3124.591
12	354.606	750.562	1544.585	2334.588	3124.591
13	354.606	750.562	1544.585	2334.588	3124.591
14	354.606	750.562	1544.585	2334.588	3124.591
15	354.606	750.562	1544.585	2334.588	3124.591
16	352.291	745.853	1539.963	2330.099	3120.102
17	336.735	721.725	1510.333	2301.527	3091.530
18	297.315	655.902	1418.429	2201.873	2990.316
19	231.121	540.976	1233.745	1981.429	2758.022
20	164.028	399.171	965.283	1642.061	2387.417
21	103.973	264.774	667.513	1194.181	1863.891
22	58.733	152.388	390.152	721.092	1225.331
23	38.838	102.438	259.302	485.607	879.392
24	20.477	56.510	144.182	268.602	538.390
25	5.979	14.181	31.955	59.674	196.473
26	.000	.000	.000	.000	46.023
27	.000	.000	.000	.000	27.772
28	.000	.000	.000	.000	9.257
29	.000	.000	.000	.000	.000
30	.000	.000	.000	.000	.000

44.438

53.325

44.438

53.325

44.438

53.325

44.438

53.325

44.438

53.325

44.438

53.325

TABLE A-IX (Continued)

\$ DATA

MAP
 ERRCR C000C* SYSTEM 00000* SPRINT C0000* SKIP6 00000* SCARDS C0000* SPEEK 00000*
 .EXIT 00000* FTRAP 00000* (MAIN) 10000* .IOH 47637* .READ 52066* .PRINT 52231*
 .PKSLT 52314* .PCGMT 53012* .CI3GI 53031* ZERO 53123* .ERR 53174*
 8NBGD 53256* (PRGG) 53301 (SUBT) 74712 (ERAS) 77776
 21401 LUCS. CAN BE SAFELY USED IN EXPANDING PRUG. (OCTAL)

SHIP NO. 952 E

INPUT VALUES READ WERE

LHP = 168.000000, BE = 12.445000, INCH = LB, LAMBDA = 42.857140
 NBL = 5, NBV = 2, OST = 14

L(1)...L(5)

1.218500E 00 1.801850E 01 1.524185E 02 1.692185E 02 1.738585E 02

LN(1)...LN(5)

2 4 4 4 4

D(1)...D(2)

2.489000E 00 1.493100E 01

VN(1)...VN(2)

2 5

DFS(7,0)...DFS(30,7)

.000000E 00 .000000E 00 .000000E 00 .000000E 00 .000000E 00 .000000E 00 .000000E 00
 .000000E 00 .000000E 00 .000000E 00 .000000E 00 .000000E 00 .000000E 00 .000000E 00
 .000000E 00 .000000E 00 .000000E 00 .000000E 00 .000000E 00 .000000E 00 .000000E 00
 4.000000E-02 3.600000E-01 7.000000E-01 1.440000E 00 2.220000E 00 3.120000E 00 4.100000E 00 5.160000E 00
 3.000000E-01 1.040000E 00 1.760000E 00 3.200000E 00 4.620000E 00 6.060000E 00 7.200000E 00 8.180000E 00
 3.200000E-01 2.000000E 00 3.160000E 00 5.120000E 00 6.980000E 00 8.540000E 00 9.620000E 00 1.046000E 01

TABLE A-X

CURVES OF FORM FOR THE U OF M "V" SERIES, $C_B = .80$

CALCULATIONS FOR THE CURVES OF FORM AND BONJEAN CURVES

SHIP NO. 966

R. A. YAGLE, H. C. KIM

BASIC DIMENSIONS

THE LENGTH BETWEEN PERPENDICULARS IS 600.000 FEET

THE MCLD ED HALF BEAM IS 46.155 FEET

THERE ARE 5 DIFFERENT STATION SPACINGS ALONG THE SHIP

THERE ARE 2 DIFFERENT WATERLINE SPACINGS UP THE SHIP

MIDSHIP IS LOCATED AT STATION 14

CALCULATED ON 20/3/63

TABLE A-X (Continued)

WATERPLANE CALCULATIONS
SHIP NO.966

CF IS IN FEET FORWARD (+) OR AFT (-) OF MIDSHIPS	MP AREAS	CF (FROM MID.)	TONS PER INCH	WP COEFF.	TRANSV. I. COEFF.	LONG. I. COEFF.
WATERLINE						
.000	29940	15.743	71.285	.5406	.31965	.29684
4.616	39362	19.283	93.720	.7107	.57127	.47174
9.232	41862	18.908	99.672	.7558	.63586	.53624
18.465	44867	17.615	106.826	.8101	.70873	.63058
27.698	47466	13.925	113.014	.8570	.77148	.72557
36.931	50818	3.313	120.995	.9175	.84402	.87235
46.164	52701	-.534	125.479	.9515	.89112	.95916
55.396	53559	-1.660	127.521	.9670	.91093	1.00153

MOLDED DISPLACEMENTS
SHIP NO.966

ALL VALUES ARE IN LONG TONS		
WATERLINE	DISP. SALT WATER	DISP. FRESH WATER
4.616	4646	4517
9.232	10079	9799
18.465	21576	20977
27.698	33764	32826
36.931	46711	45413
46.164	60397	58719
55.396	74435	72367

TABLE A-X (Continued)

LONGITUDINAL AND VERTICAL CENTERS OF BUOYANCY
SHIP NO. 966

VCB IS IN FEET ABOVE THE BASELINE		
WATERLINE	VCB	LCB
4.616	2.524	18.067
9.232	4.856	18.752
18.465	9.651	18.519
27.698	14.511	17.588
36.931	19.465	15.225
46.164	24.468	11.974
55.396	29.428	9.468

TRANSVERSE AND LONGITUDINAL METACENTRIC HEIGHTS
SHIP NO. 966

ALL VALUES ARE IN FEET ABOVE THE BASE LINE		
WATERLINE	KM TRANS.	KM LONG.
4.616	79.833	3035.637
9.232	68.549	2226.919
18.465	42.767	1189.527
27.698	38.098	901.136
36.931	38.024	756.893
46.164	40.171	710.164
55.396	42.881	641.170

TABLE A-X (Continued)

MOMENT TO TRIM ONE INCH AND
CHANGES IN DISPLACEMENT FOR A ONE INCH TRIM AFT
SHIP NO. 966

THE MOMENTS ARE IN FOOT LONG TONS
THE CHANGE IN DISP. IS IN LONG TONS

WATERLINE	MOM. TO TRIM 1 IN.	CHANGE IN DISP.
4.616	1957.259	-3.012
9.232	3535.761	-3.141
18.465	4157.753	-3.136
27.698	4784.128	-2.623
36.931	5751.927	-.668
46.164	6324.291	.112
55.396	6603.683	.353

BLOCK, PRISMATIC, MIDSHIP, AND VERTICAL PRISMATIC COEFFICIENTS
SHIP NO. 966

WATERLINE	BLOCK	PRISMATIC	MIDSHIP	VERTICAL PRISMATIC
4.616	.6360	.6835	.9306	.8950
9.232	.6899	.7128	.9678	.9127
18.465	.7384	.7496	.9851	.9115
27.698	.7703	.7780	.9901	.8989
36.931	.7993	.8053	.9926	.8711
46.164	.8268	.8317	.9941	.8689
55.396	.8491	.8533	.9950	.8781

TABLE A-X (Continued)

SECTIONAL AREAS FROM BONJEAN CURVES
SHIP NO. 966

LOCATION OF STATIONS	STATION	DISTANCE FROM STA. 0
	0	.000
	1	2.176
	2	4.352
	3	19.352
	4	34.352
	5	49.352
	6	64.352
	7	94.352
	8	124.352
	9	154.352
	10	184.352
	11	214.352
	12	244.352
	13	274.352
	14	304.352
	15	334.352
	16	364.352
	17	394.352
	18	424.352
	19	454.352
	20	484.352
	21	514.352
	22	544.352
	23	559.352
	24	574.352
	25	589.352
	26	604.352
	27	608.495
	28	612.637
	29	616.780
	30	620.923

TABLE A-X (Continued)

5 DATA

```

MAP      ERROR 00000*  SYSTEM 00000*  SPRINT 00000*  SKIP6  00000*  SCARDS 00000*  SPEEK  00000*
          FTRAP 00000*  (MAIN) 10000  .IOH  47637*  .ERR  52066*  .READ  52150*  .PRINT 52314*
          .PRSLT 52400*  .PCOMT 53076*  .EXIT  53115*  .ATLOC 53172*  .01301 53220*  ZERO   53312*
          .03311 53346*  .BNBCD  53363*  (PRG)  53406  (SUBT) 74676  (ERAS) 77776
21260 LOCS. CAN BE SAFELY USED IN EXPANDING PROG. (OCTAL)
    
```

SHIP NO. 966

INPUT VALUES READ WERE

```

LBP = 168.000000, BE = 12.923400, INCH = 18, LAMBDA = 42.857140
NBL = 5, NRV = 2, DST = 14
    
```

L(1)...L(5)

1.218500E 00 1.801850E 01 1.524185E 02 1.692185E 02 1.738585E 02

LN(1)...LN(5)

2 4 16 4

O(1)...O(2)

2.585000E 00 1.551100E 01

VN(1)...VN(2)

2 5

OFS(0,0)...OFS(30,7)

.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00
.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00
.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00	.000000E 00
1.600000E-01	1.090000E 00	1.750000E 00	3.070000E 00	4.490000E 00	6.080000E 00	8.090000E 00	8.870000E 00	8.870000E 00	8.870000E 00
4.900000E-01	2.700000E 00	3.920000E 00	5.930000E 00	7.900000E 00	9.820000E 00	1.094000E 01	1.137000E 01	1.137000E 01	1.137000E 01
1.040000E 00	4.470000E 00	5.960000E 00	8.280000E 00	1.024000E 01	1.159000E 01	1.216000E 01	1.238000E 01	1.238000E 01	1.238000E 01

TABLE A-XI

NONDIMENSIONAL OFFSETS FOR THE U OF M "V" SERIES, $C_B = .60$

STA.	NON-DIMENSIONAL OFFSETS - HALF BREADTH											UM V-SERIES						
	TANGENT	.075 WL	.125 WL	.25 WL	.50 WL	.75 WL	1.00 WL	1.25 WL	1.50 WL									
FP	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1	0.0063	0.0111	0.0150	0.0217	0.0366	0.0500	0.0893	0.1152	0.1554	0.2348	0.3509	0.4590	0.5607	0.7447	0.8849	1.0000	1.0000	1.0000
2	0.0089	0.0212	0.0268	0.0444	0.0795	0.1170	0.1768	0.2572	0.3572	0.4590	0.5607	0.7447	0.8849	1.0000	1.0000	1.0000	1.0000	1.0000
3	0.0125	0.0372	0.0500	0.0752	0.1304	0.1884	0.2634	0.3545	0.4545	0.5607	0.7447	0.8849	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
4	0.0189	0.0574	0.0767	0.1161	0.1875	0.2661	0.3545	0.4545	0.5607	0.7447	0.8849	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
5	0.0301	0.1158	0.1486	0.2100	0.3277	0.4375	0.5420	0.6456	0.7447	0.8849	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
6	0.0817	0.2186	0.2656	0.3490	0.4884	0.6099	0.7179	0.8081	0.8849	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
7	0.2010	0.3675	0.4161	0.5068	0.6563	0.7652	0.8563	0.9233	0.9697	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
8	0.3812	0.5377	0.5801	0.6682	0.8054	0.8867	0.9496	0.9849	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
9	0.6050	0.7099	0.7440	0.8132	0.9152	0.9617	0.9893	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
10	0.8112	0.8197	0.8869	0.9202	0.9724	0.9938	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
11	0.9446	0.9627	0.9664	0.9791	0.9954	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
12	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
13	0.9648	0.9839	0.9827	0.9900	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
14	0.8579	0.9134	0.9300	0.9601	0.9983	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
15	0.6918	0.7996	0.8341	0.8912	0.9661	0.9983	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
16	0.5106	0.6323	0.6769	0.7697	0.8956	0.9706	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
17	0.3460	0.4713	0.5177	0.6056	0.7661	0.9045	0.9849	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
18	0.2176	0.3383	0.3720	0.4343	0.5831	0.7813	0.9349	0.9938	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
19	0.1182	0.2186	0.2407	0.2829	0.3831	0.5831	0.8331	0.9313	0.9733	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
18½	0.0478	0.1238	0.1381	0.1604	0.2116	0.3232	0.4563	0.6081	0.8911	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
19½	0.0227	0.0795	0.0920	0.1106	0.1366	0.2080	0.3402	0.5402	0.8215	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
19	0.0113	0.0433	0.0537	0.0625	0.0741	0.1107	0.2009	0.3438	0.5438	0.7438	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
19½	0.0089	0.0131	0.0140	0.0154	0.0170	0.0277	0.0527	0.0991	0.1684	0.2584	0.4009	0.6259	0.7438	0.8849	1.0000	1.0000	1.0000	1.0000
AP	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
MAX. B. TANGENT	0.7099	0.8867	0.934	0.9849	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000

MODEL NO.: 924
 $C_B = .60$ EXT "V"

TABLE A-XII

NONDIMENSIONAL OFFSETS FOR THE U OF M "V" SERIES, $C_B = .65$

STA	NON-DIMENSIONAL OFFSETS - HALF BREADTH										UM V-SERIES			MODEL NO.: 959 $C_B = 65^* \text{ EXT "V"}$
	TANGENT	.075 WL	.125 WL	.25 WL	.50 WL	.75 WL	1.00 WL	1.25 WL	1.50 WL	1.50 WL				
FP	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0043	0.0354	0.0761					
1/2	0.0128	0.0172	0.0201	0.0296	0.0508	0.0768	0.1174	0.1649	0.2574					
1	0.0128	0.0269	0.0357	0.0600	0.1096	0.1623	0.2339	0.3252	0.4143					
1 1/2	0.0128	0.0474	0.0655	0.1062	0.1800	0.2563	0.3504	0.4512	0.5451					
2	0.0192	0.0783	0.1023	0.1582	0.2620	0.3559	0.4704	0.5852	0.6839					
3	0.0654	0.1804	0.2091	0.3028	0.4428	0.5602	0.6698	0.7613	0.8320					
4	0.1678	0.3397	0.3870	0.4820	0.6286	0.7423	0.8269	0.8750	0.9014					
5	0.3224	0.5156	0.5636	0.6613	0.7958	0.8761	0.9201	0.9458	0.9563					
6	0.5267	0.6889	0.7345	0.8135	0.9111	0.9546	0.9762	0.9872	0.9909					
7	0.7393	0.8478	0.8790	0.9214	0.9717	0.9891	0.9986	1.0000	1.0000					
8	0.9180	0.9528	0.9585	0.9771	0.9978	1.0000	1.0000	1.0000	1.0000					
9	0.9977	0.9948	0.9932	0.9973	1.0000	1.0000	1.0000	1.0000	1.0000					
10	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000					
11	0.9776	0.9929	0.9932	0.9954	1.0000	1.0000	1.0000	1.0000	1.0000					
12	0.9040	0.9492	0.9588	0.9728	1.0000	1.0000	1.0000	1.0000	1.0000					
13	0.7650	0.8520	0.8790	0.9214	0.9780	1.0000	1.0000	1.0000	1.0000					
14	0.5933	0.7176	0.7502	0.8205	0.9299	0.9822	1.0000	1.0000	1.0000					
15	0.3920	0.5468	0.5837	0.6726	0.8251	0.9322	0.9900	1.0000	1.0000					
16	0.2474	0.3834	0.4192	0.5000	0.6578	0.8182	0.9494	0.9979	1.0000					
17	0.1110	0.2436	0.2763	0.3385	0.4557	0.6248	0.8597	0.9480	0.9762					
18	0.0432	0.1337	0.1537	0.1893	0.2607	0.3715	0.6896	0.8543	0.9201					
18 1/2	0.0220	0.0955	0.1056	0.1262	0.1666	0.2443	0.5679	0.7623	0.8415					
19	0.0119	0.0477	0.0540	0.0661	0.0872	0.1260	0.4298	0.6118	0.7530					
19 1/2	0.0110	0.01623	0.0157	0.0148	0.0186	0.0344	0.2796	0.4592	0.6231					
AP	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.1139	0.2914	0.4488					
MAX. Z	0.7390	0.9040	0.9434	0.9920	1.0000	1.0000	1.0000	1.0000	1.0000					

* $C_B = .648$

TABLE A-XIV

NONDIMENSIONAL OFFSETS FOR THE U OF M "V" SERIES, $C_B = .75$

STA	NON-DIMENSIONAL OFFSETS - HALF BREADTH											UM V-SERIES	
	TANGENT	.075 WL	.125 WL	.25 WL	.50 WL	.75 WL	1.00 WL	1.25 WL	1.50 WL	1.50 WL	1.50 WL	MODEL NO. : 952	CB = .75 EXT. "V"
FP	0	0	0	0	0	0	0	0	0.0466	0.1157			
1	0.0398	0.0187	0.0296	0.0562	0.1157	0.1783	0.2505	0.3293	0.4146				
1	0.0149	0.0612	0.0855	0.1414	0.2570	0.3711	0.4867	0.5783	0.6573				
1½	0.0319	0.1259	0.1661	0.2538	0.4112	0.5606	0.6859	0.7727	0.8405				
2	0.0657	0.2126	0.2648	0.3743	0.5622	0.7116	0.8241	0.8964	0.9466				
3	0.2131	0.4388	0.5066	0.6137	0.7952	0.8980	0.9606	0.9912	0.9996				
4	0.4560	0.6752	0.7303	0.8289	0.9398	0.9863	0.9976	1.0000	1.0000				
5	0.7189	0.8707	0.8997	0.9526	0.9992	1.0000	1.0000	1.0000	1.0000				
6	0.8961	0.9779	0.9868	0.9950	1.0000	1.0000	1.0000	1.0000	1.0000				
7	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000				
8	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000				
9	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000				
10	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000				
11	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000				
12	0.9778	0.9949	0.9918	0.9980	1.0000	1.0000	1.0000	1.0000	1.0000				
13	0.9141	0.9524	0.9622	0.9815	1.0000	1.0000	1.0000	1.0000	1.0000				
14	0.7667	0.8520	0.8783	0.9285	0.9815	0.9944	1.0000	1.0000	1.0000				
15	0.5178	0.6888	0.7352	0.8161	0.9157	0.9687	0.9916	1.0000	1.0000				
16	0.3445	0.4915	0.5411	0.6378	0.7904	0.9060	0.9718	0.9964	0.9964				
17	0.1872	0.3248	0.3635	0.4692	0.5734	0.7695	0.9173	0.9723	0.9867				
18	0.0976	0.1871	0.2105	0.2554	0.3438	0.5060	0.7903	0.9105	0.9337				
18½	0.0538	0.1786	0.1447	0.1689	0.2297	0.3534	0.6763	0.8244	0.8694				
19	0.0219	0.0714	0.0806	0.0964	0.1237	0.1992	0.5253	0.7055	0.7730				
19½	0.0119	0.0170	0.0197	0.0209	0.0241	0.0498	0.3406	0.5432	0.6460				
AP	0	0	0	0	0	0	0.1396	0.3519	0.4661				
MAX ^B	0.8067	0.9449	0.973	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000				

TABLE A-XV

NONDIMENSIONAL OFFSETS FOR THE U OF M "V" SERIES, C_B = .80

STA	NON-DIMENSIONAL OFFSETS - HALF BREADTH											UM V-SERIES			
	TANGENT	.075 WL	.125 WL	.25 WL	.50 WL	.75 WL	1.00 WL	1.25 WL	1.50 WL	1.75 WL	2.00 WL	2.25 WL	2.50 WL	2.75 WL	3.00 WL
FP	0	0	0	0	0	0	0.0039	0.1424	0.2925						
1	0.0145	0.0606	0.0853	0.1354	0.2376	0.3474	0.4705	0.6260	0.6864						
1	0.0445	0.1683	0.2113	0.3033	0.4589	0.6113	0.7599	0.8465	0.8798						
1½	0.0945	0.2943	0.3498	0.4612	0.6409	0.7924	0.8968	0.9409	0.9580						
2	0.1645	0.4266	0.4867	0.6067	0.7901	0.9038	0.9595	0.9789	0.9866						
3	0.4600	0.7026	0.7574	0.8496	0.9425	0.9835	0.9982	1.0000	1.0000						
4	0.7672	0.9114	0.9256	0.9556	0.9928	0.9990	1.0000	1.0000	1.0000						
5	0.9881	0.9832	0.9874	0.9928	0.9998	1.0000	1.0000	1.0000	1.0000						
6	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000						
7	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000						
8	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000						
9	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000						
10	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000						
11	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000						
12	0.9963	0.9960	0.9984	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000						
13	0.9554	0.9736	0.9812	0.9943	1.0000	1.0000	1.0000	1.0000	1.0000						
14	0.8436	0.8939	0.9123	0.9572	0.9599	1.0000	1.0000	1.0000	1.0000						
15	0.6445	0.7560	0.7895	0.8597	0.9464	0.9866	0.9974	1.0000	1.0000						
16	0.4091	0.5590	0.6088	0.7065	0.8372	0.9270	0.9758	0.9990	1.0000						
17	0.2472	0.3628	0.4053	0.4983	0.6554	0.8078	0.9340	0.9835	0.9974						
18	0.1200	0.1962	0.2230	0.2824	0.4109	0.6020	0.8458	0.9332	0.9611						
18½	0.0700	0.1260	0.1455	0.1870	0.2778	0.4527	0.7545	0.8744	0.9115						
19	0.0373	0.0670	0.0759	0.0952	0.1478	0.2670	0.6175	0.7645	0.8233						
19½	0.0119	0.0160	0.0164	0.0170	0.0255	0.0673	0.4264	0.6043	0.6794						
AP	0	0	0	0	0	0	0.2004	0.3815	0.4674						
MAX	0.850	0.970	0.991	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000						

MODEL NO.: UM966
C_B: 80 EXT "V"

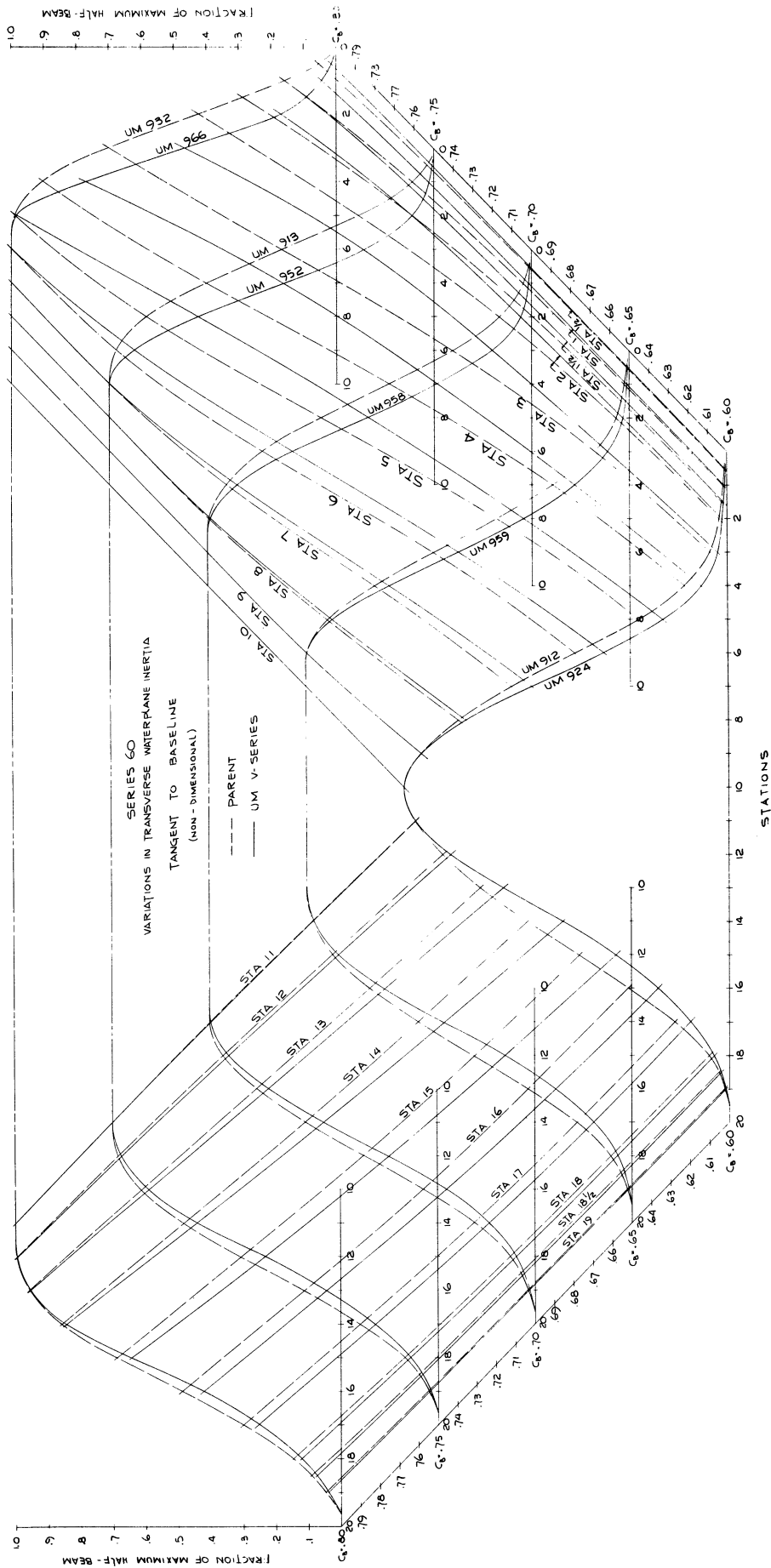


Fig. A-1. Orthogonal plot of nondimensional baseline tangent waterlines for Series 60 and the U of M "V" Series.

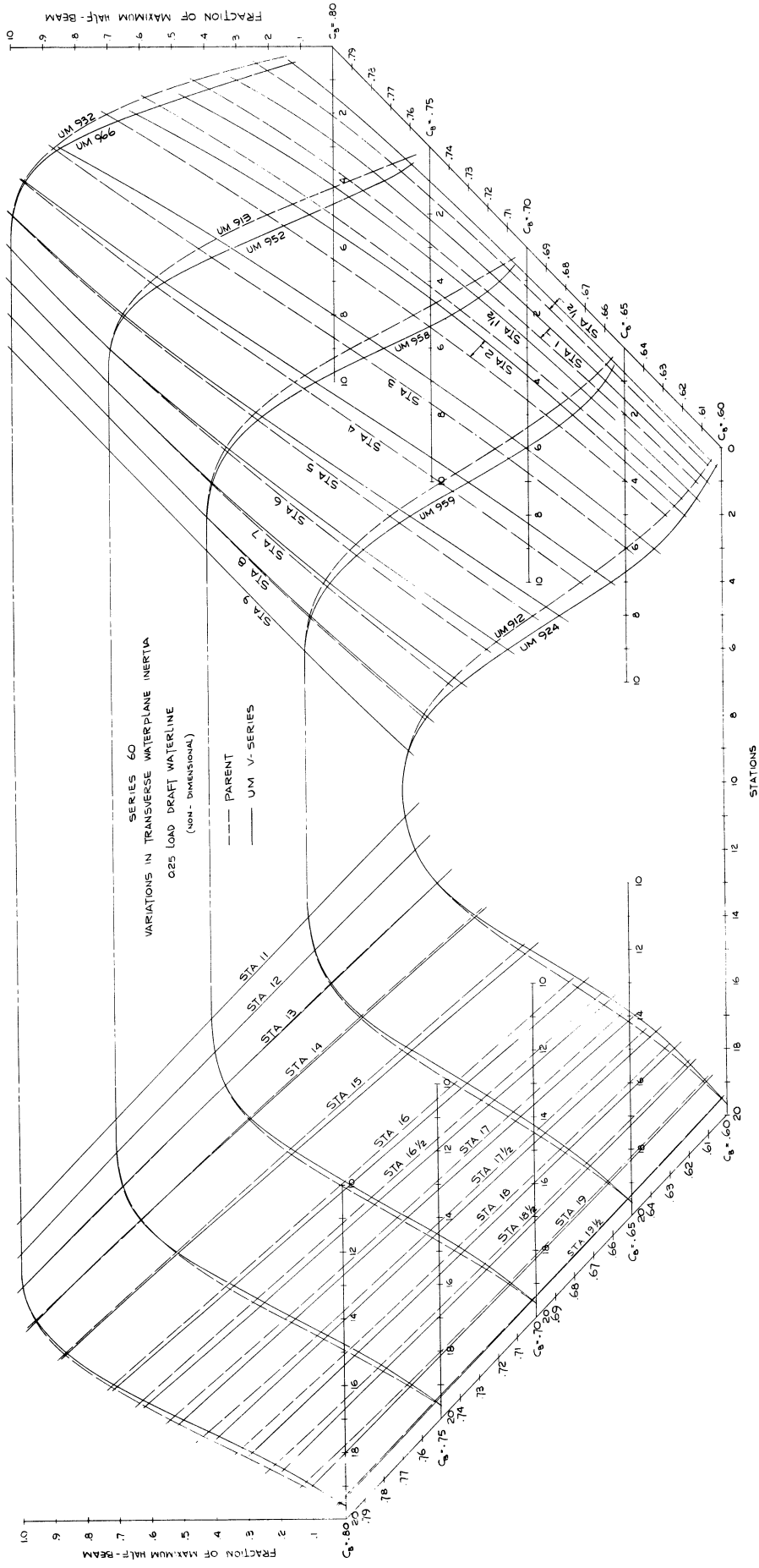


Fig. A 2. Orthogonal plot of nondimensional 0.25 waterlines for Series 60 and the U of M "V" Series.

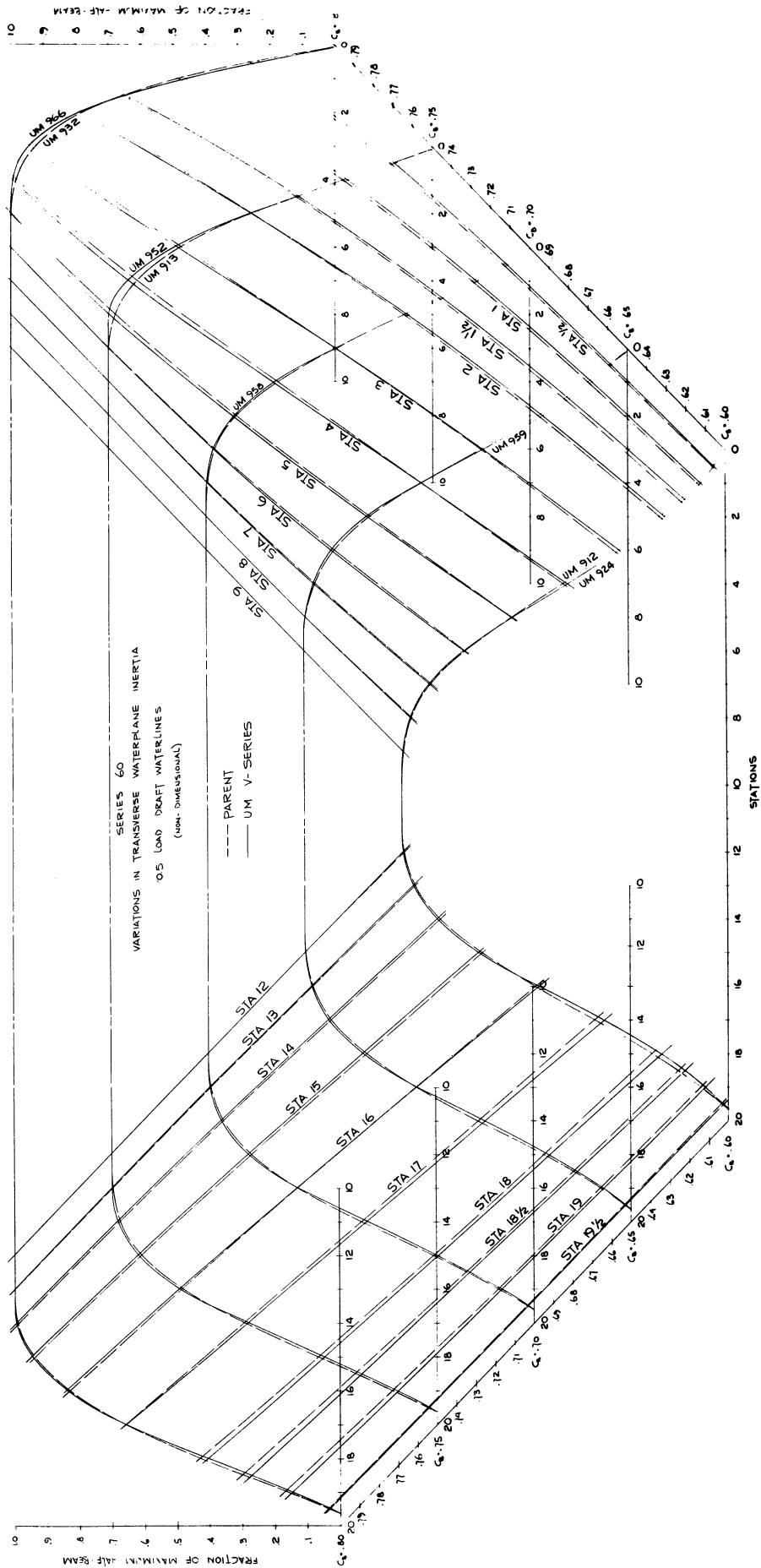


Fig. A-3. Orthogonal plot of nondimensional 0.50 waterlines for Series 60 and the U of M "V" Series.

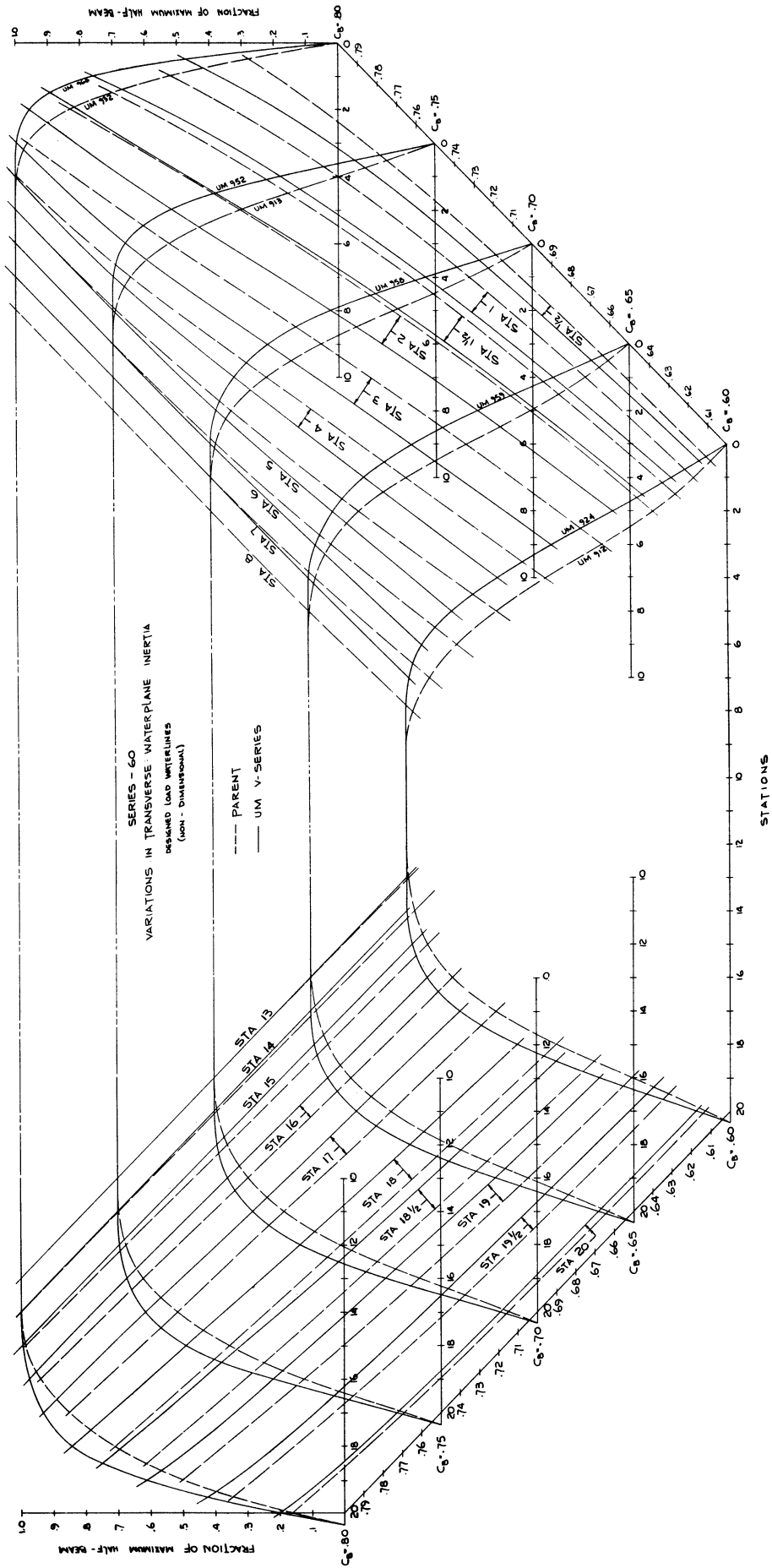


Fig. A-5. Orthogonal plot of nondimensional load waterlines for Series 60 and the U of M "V" Series.

