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# Tissue engineering osteocondral implants for temporomandibular joint repair

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## **Abstract**

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Tissue engineering has provided an alternative to traditional strategies to repair and regenerate temporomandibular joints (TMJ). A successful strategy to engineer osteocondral tissue, such as that found in the TMJ, will produce tissue that is both biologically and mechanically functional. Image-based design (IBD) and solid free-form (SFF) fabrication can be used to generate scaffolds that are load bearing and match patient and defect site geometry. The objective of this study was to demonstrate how scaffold design, materials, and biological factors can be used in an integrated approach to regenerate a multi-tissue interface. IBD and SFF were first used to create biomimetic scaffolds with appropriate bulk geometry and microarchitecture. Biphasic composite scaffolds were then manufactured with the same techniques and used to simultaneously generate bone and cartilage in discrete regions and provide for the development of a stable interface between cartilage and subchondral bone. Poly-L-lactic acid/hydroxyapatite composite scaffolds were differentially seeded with fibroblasts transduced with an adenovirus expressing bone morphogenetic protein-7 in the ceramic phase and fully differentiated chondrocytes in the polymeric phase, and were subcutaneously implanted into mice. Following implantation in the ectopic site, the biphasic scaffolds promoted the simultaneous growth of bone, cartilage, and a mineralized interface tissue. Within the ceramic phase, the pockets of tissue generated included blood vessels, marrow stroma, and adipose tissue. This combination of IBD and SFF-fabricated biphasic scaffolds with gene and cell therapy is a promising approach to regenerate osteocondral defects and, ultimately, the TMJ.

**Key words:** biomaterials; bone; cartilage; temporomandibular joint; tissue engineering

## Introduction

In response to the significant need to reconstruct the temporomandibular joint (TMJ), autogenous tissue grafting and alloplastic materials are regularly employed (1–3). Neither therapy is ideal, however, because allografts are associated with donor site morbidity and are poorly shaped for placement in TMJ defects, and alloplastics do not respond to normal biochemical or mechanical signals (4,5). Tissue engineering approaches have the potential to overcome the lack of donor tissue and create a TMJ replacement that is both biologically and mechanically functional. Engineering of such a graft will require the production of both bone and fibrocartilage. Strides have been made in tissue engineering of these tissues separately (6–13), but a combined approach to generate both bone and cartilage simultaneously will likely be required to regenerate an articulating osteochondral joint. We propose the use of a designed biphasic scaffold to guide the growth of these two different tissues into a single implant.

Biphasic scaffolds contain discrete regions that are optimized for selective growth of the desired tissue by utilizing different material types, material properties, internal architectures (e.g. porosity, pore interconnectivity), cells, and biological factors. Such scaffolds have previously been investigated for osteochondral regeneration (14–16). Taken together, these studies demonstrated the ability of biphasic scaffolds to support cell growth and differentiation into bone and cartilage. The scaffolds used in these studies did not control the scaffold internal architecture, which may enhance osteochondral tissue regeneration. Control over the biphasic scaffold internal pore architecture may be used to create scaffolds with mechanical and biological properties that provide immediate mechanical function while promoting tissue ingrowth (17,18). Similarly, control over the exterior shape of the scaffold may be used to match the scaffold geometry with a temporomandibular defect site or the contours of the articular surface. To create a scaffold with complex internal structures and correctly matched anatomic shape while providing for rapid and flexible manufacturing, computational design and solid free-form (SFF) fabrication techniques may be needed.

Solid free-form fabrication is a highly flexible manufacturing technique in which scaffolds are built in

a layer-by-layer fashion from computer-generated design files. When image-based design (IBD) is employed, these computationally designed files are matched to magnetic resonance imaging (MRI) or computer tomographic (CT) data of the patient defect site (19). Additionally, the microstructure of these designed scaffolds can be optimized to allow both mechanical function and tissue invasion (20,21). This flexible design and manufacturing platform can also be used to manufacture biphasic scaffolds in which discrete regions are optimized for the growth of specific tissue types. Already, SFF has been used to create biphasic scaffolds that allow for selective seeding and the growth of tissues in the appropriate phases (22,23).

Scaffolds produced via SFF fabrication would have numerous advantages but must be combined with a biological factor to trigger tissue formation; we propose gene therapy to serve this role. *Ex vivo* gene therapy, in which cells are isolated, transduced *in vitro*, and then implanted into the host, was chosen for this work. This is because regeneration of large defects, such as the TMJ, may require seeding the designed scaffolds with cells in order to provide a cell pool for tissue regeneration. In this study, we aimed to initiate the formation of bone using fibroblasts virally transduced to express bone morphogenetic protein-7 (BMP-7) and the formation of cartilage using primary chondrocytes.

We hypothesized that designed biphasic scaffolds, in conjunction with *ex vivo* gene therapy and specific progenitor cells, are excellent candidates for the engineering of TMJ. Here we have demonstrated how IBD and SFF can be used to design scaffolds that match articulating surface geometry and manufactured from materials that may allow bearing of functional loads while promoting regeneration. We then investigated the generation of osteochondral tissue when bone and cartilage progenitor cells were simultaneously cultured in discrete regions of the scaffolds in a subcutaneous murine model.

## Methods

### Scaffold design and manufacture

The scaffold shape and internal pore architecture can be defined using the IBD method previously described (19). In this method, an image of the joint to be reconstructed is obtained by MRI and/or CT. The tissue replacement area is then defined by image processing

and digitization; this creates the external scaffold design. The heterogeneous internal scaffold architecture designs can then be created and optimized as separate image databases. The porous architecture can be created either using geometric primitive shapes like cylinders or spheres (16), or using microstructure topology optimization methods (17). The external scaffold design database is then combined with the architecture databases to create the final complete scaffold design as an image database. The internal scaffold design can then be designed and optimized. Finally, the entire scaffold design is then translated from image data to stl. or a similar format for manufacture using SFF fabrication. Using this procedure, a biomimetic scaffold, containing an orthogonal porous region was designed and fabricated from a single polymeric material via SFF (Fig. 1).

Scaffolds with a simpler geometry were used for *in vivo* evaluation of how scaffold design and material properties effected tissue formation. These composite scaffolds were composed of two bonded cylinders, one hydroxyapatite (HA) and one poly-L-lactic acid [PLA,  $MW_{(weight\ avg)} = 147\ 000$ ; Birmingham Polymers, Inc., Birmingham, AL, USA], each 5 mm in diameter and 3 mm in height. The HA phase contained either 300  $\mu\text{m}$  diameter orthogonal pores with a porosity of 50%. These were manufactured using indirect SFF fabrication as previously described (24). Briefly, the computer-designed molds were created on a Model Maker II (SolidScape, Inc., Merrimack, NH, USA) wax inkjet printer and an HA/acrylic slurry was cast into the molds and sintered (25). The polymer sponges were created using a salt leaching technique as described previously (24). Sieved NaCl (100–120  $\mu\text{m}$  diameter; Sigma, St Louis, MO, USA) were packed into 5 mm diameter by 3 mm high molds and 70  $\mu\text{l}$  of 7.5% w/v

PLA in methylene chloride (Sigma) were cast into the molds. Finally, the solvent was evaporated and the salt porogen removed by soaking water for 48 h.

The two phases of the scaffold were assembled prior to cell seeding and implantation as shown in Fig. 2. Completed scaffolds were allowed to dry overnight and sterilized by soaking in 70% ethanol for 24 h.

#### Seeding and implantation of scaffolds

The biphasic scaffolds were seeded with chondrocytes in the polymeric phase and transduced fibroblasts in the ceramic phase to trigger the growth of cartilage and bone, respectively. Articular cartilage was harvested from domestic pig knee joints and the chondrocytes were isolated by agitating the tissue overnight in 1.5 mg/ml collagenase II (Sigma) in  $\alpha$ -minimum essential medium ( $\alpha$ -MEM). The chondrocytes were resuspended in culture medium [CM,  $\alpha$ -MEM with 10% FBS and 1% penicillin/streptomycin (Gibco, GIBCO Invitrogen, San Diego, CA, USA)], and plated in tissue culture flasks (BD Biosciences, Lexington, KY, USA). After 24 h, adherent cells were used for cell seeding. Primary human gingival fibroblasts (HGFs) were prepared from discarded tissue following oral surgery in compliance with the University of Michigan Institutional Review Board. Cells migrating from diced tissue onto tissue culture polystyrene were isolated and expanded in CM (26). Passage 4 fibroblasts were infected with AdCMV-BMP-7, a recombinant adenovirus construct expressing the murine BMP-7 gene under a cytomegalovirus (CMV) promoter (27). Infections were performed overnight with 1000 plaque forming units per cell. Such infected primary cells have been shown to form bone *in vivo* (28–31).

Transduced HGFs were suspended in 50 mg/ml bovine plasma-derived fibrinogen in  $\alpha$ -MEM (Sigma).

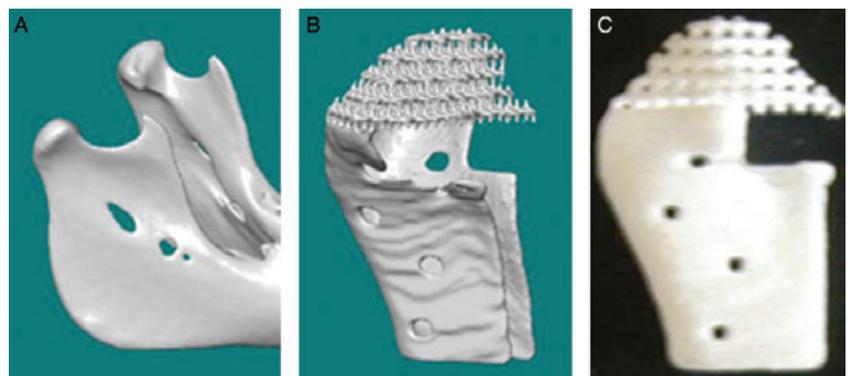
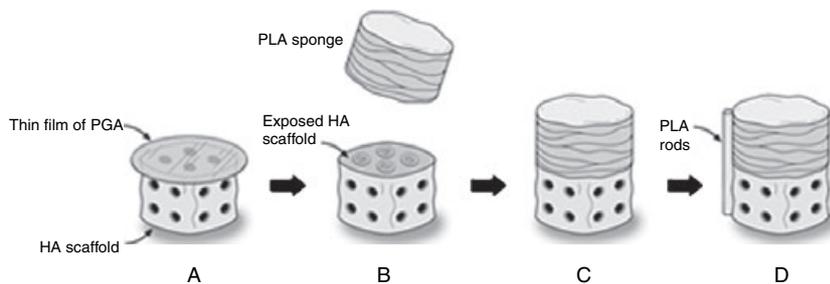


Fig. 1. Image-based design allowing creation of defect site-specific scaffolds. The patient image (A) is used in conjunction with appropriate microstructure architecture to create the design for the implant (B). This design can then be produced using solid free-form fabrication, as in this prototype constructed from a single polymeric material (C).



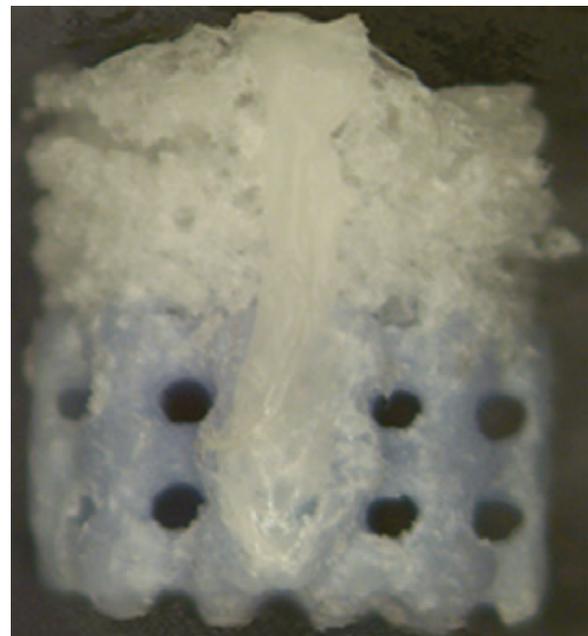
**Fig. 2.** Poly-L-lactic acid (PLA) was used to join the polymer and ceramic phases of the composite scaffold. One face of the ceramic was coated with a thin film of poly-gamma-glutamic acid (PGA) (A). The film was removed from the circumference and 10  $\mu\text{l}$  of PLA (7.5% in methylene chloride) was applied (B). The polymer sponge was pressed onto the ceramic scaffold, allowing the solubilized PLA to serve as adhesive (C). PLA (25% in methylene chloride) struts were extruded on two opposite sides of the scaffold to further stabilize the composite (D).

$10^6$  cells in 20  $\mu\text{l}$  were pipetted into the ceramic phase of the composite scaffold and the scaffold was immediately placed onto a 20  $\mu\text{l}$  drop of 100 U/ml bovine plasma derived thrombin (Sigma). Fibrinogen gelation occurred quickly upon contact with the thrombin. Chondrocytes were suspended in CM and  $10^6$  cells in 20  $\mu\text{l}$  were pipetted into the polymer sponge phase and allowed to adhere for 1 h in a 37° incubator. The scaffolds were immediately implanted subcutaneously into immunocompromised mice (N:NIH-bg-nu-xid; Charles River, Wilmington, MA, USA). Animals were anesthetized with intra-mesenteric injections of ketamine/xylazine (50 and 5  $\mu\text{g/g}$ , respectively) in saline. Dorsal subcutaneous pockets were created using blunt dissection and the surgical sites were closed with wound clips.

Mice were killed after 4 weeks. The harvested implants were fixed using Z-Fix (Anatech, Battle Creek, MI, USA) and then demineralized using RDO (APEX Engineering Products Corp., Plainfield, IL, USA), which also removed the HA phase of the scaffold (24). The specimens were then embedded in paraffin, sectioned at 7  $\mu\text{m}$ , and stained with either hematoxylin and eosin (H&E) or safranin O and fast green. The safranin O stained glycosaminoglycans (GAGs) red and the fast green stained collagenous tissues brown.

## Results

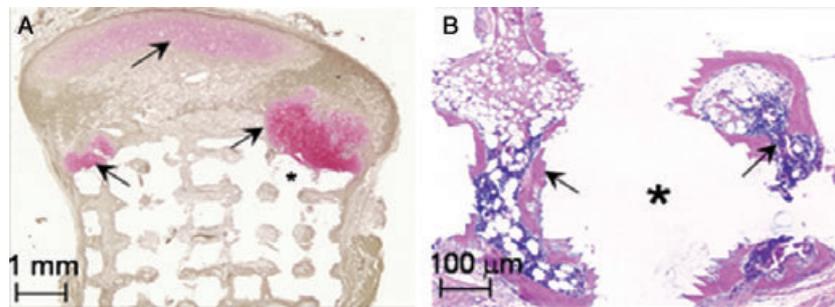
The final manufactured scaffolds matched the IBDs. This was true of both the biomimetic design (Fig. 1) and the simple cylindrical geometry design used for *in vivo* testing (Fig. 3). In the latter composite scaffold, the polymer sponge consisted of 50–100  $\mu\text{m}$  wide



**Fig. 3.** The assembled composite: the upper polymer phase (white) and the lower ceramic phase (blue) are transversely by the two PLA struts, one of which is visible on the front of the construct.

interconnected pores. The PLA rods connecting the phases were in intimate contact with both the PLA and HA phases and the integrity of the composite scaffold was sufficient to withstand surgical manipulation and subsequent implantation.

The biphasic scaffolds were seeded with appropriate progenitor cells and implanted *in vivo* for 4 weeks. Demineralization of the implants allowed paraffin sectioning of the scaffold by removing the ceramic portion of the scaffold. In histological sections, areas that were formerly occupied by HA appear empty (Fig. 4, white areas). The upper, polymeric sponge phase of the scaffold appears rounded and stained positively with safranin O. This staining revealed the



**Fig. 4.** Scaffolds were demineralized prior to sectioning, resulting in empty areas (marked with \*) that were previously occupied by HA. Safranin O and fast green staining showed a large area of pink-stained cartilage (arrow) in the polymer sponge, in contact with the green-brown-stained bone that formed in the ceramic phase (A). Small pockets of cartilage were also observed within the pores of the ceramic phase of the scaffold (A, arrow). Hematoxylin and eosin staining of the ceramic phase showed the formation of bone (B, arrow) with marrow space within the pores of the HA.

presence of GAGs in the PLA sponge phase, indicating chondrocyte synthesis of cartilage matrix (Fig. 4A). Apical regions of the polymer sponge consistently stained with safranin O. Small pockets of cartilage were also observed invading the pores of the ceramic phase (Fig. 4A, arrow in the lower region).

The ceramic region of the scaffold supported the generation of morphologically normal bone. Within the pores of the HA, bone with marrow space was observed via H&E staining (Fig. 4B). Other types of tissue including blood vessels, fibrous tissue, and fat were also observed in the HA phase of the scaffold. Taken together, these data demonstrate the development of a bone–cartilage interface on the designed, biphasic scaffolds.

## Discussion

In this study, we have demonstrated the potential for combining IBD, SFF fabrication, and appropriate biological factors to tissue engineering a bone–cartilage interface that may be adapted for use in TMJ replacement. We first demonstrated the potential for this approach to create biomimetic scaffolds to replace and regenerate the joint. Our results demonstrate how these methods can be used to manufacture biphasic polymer/ceramic scaffolds that support the concurrent formation of bone and cartilage in discrete phases of the assembled scaffold. The polymeric phase of the scaffolds supported the formation of cartilage by the implanted chondrocytes, while the ceramic phase supported the formation of bone by the implanted BMP-7-transduced fibroblasts. The SFF designed

channels within the ceramic phase-guided vascularization, a process that is critical to produce a biologically functional tissue. These scaffolds also supported the growth of fat and stroma, demonstrating their potential to fully mimic native skeletal tissue. Taken together, SFF-manufactured biphasic scaffolds differentially seeded with osteo- and chondro-progenitors can generate osteochondral tissue resembling native tissue, including vascularized subchondral bone and an interface tissue between bone and articular cartilage. The design and manufacturing methods presented here can be used to create biphasic scaffolds with biomimetic geometry, which can then be combined with differential seeding of progenitor cells to regenerate a joint. We have demonstrated the growth of bone and cartilage on our composite scaffolds, but the design and composition of the scaffolds may be easily modified to satisfy the mechanical requirements of the TMJ (18).

The IBD/SFF approach used here is advantageous for several reasons. As we have shown, it allows the manufacture of scaffolds to fit patient-specific injuries and match articular surface geometry using image data (19). The biphasic components can be used to differentially regulate cell differentiation and growth, promoting the regeneration of bone and vasculature in the ceramic component while maintaining the growth of cartilage in the polymeric component. Each phase may be differentially seeded with cells or loaded with biofactors. Additionally, biphasic SFF scaffolds may be designed to carry functional loads (32). Compared with the structures tested here, scaffolds designed for TMJ regeneration will likely be exposed to larger mechanical forces. However, because IBD/SFF allows great

flexibility in scaffold design, modifications will allow the creation of scaffolds with increased ability to bear physiologic loads.

The combined use of gene therapy and SFF biphasic scaffolds represents a new strategy for the repair of human osteochondral defects and for joint replacement. The *ex vivo* gene therapy strategy employed here allows introduction of cells to trigger tissue formation. This approach may be advantageous for treating human defects in which disease or therapeutic irradiation have depleted progenitor cell populations or in which large joints must be reconstructed (33–36). In this study, we have demonstrated that implantation of our cell-containing scaffolds led to growth of skeletal tissues in a non-orthotopic (subcutaneous) site, in which a similar lack of progenitor cells exists. Bone formation was induced by the presence of non-osseous progenitor cells transduced with a BMP-7 adenoviral construct. This gene therapy approach provides for bone formation from cell populations that are easily harvested and expanded compared with osteoblasts or bone marrow stromal cells (30,31).

While results of this study suggest that SFF-fabricated biphasic scaffolds may be useful in engineering osteochondral tissues, some improvements may be required. Tissue was not entirely confined to the area in which it was intended, specifically pockets of cartilage were observed in the ceramic phase. Therefore, although the biphasic scaffolds were designed to control cell seeding, greater control over the spatial distribution of regenerate tissue is desired. Altering the interface between geometry may improve cell seeding and decrease the interaction between the progenitor cells in the two scaffold phases. Additionally, an advanced understanding of how the scaffold internal architecture regulates interface tissue formation may be used to enhance formation of a uniform mineralized tissue interface between bone and cartilage similar to the tidemark.

In conclusion, IBD and SFF-manufactured HA and PLA biphasic composite scaffolds, coupled with differential cell seeding and gene therapy, generated osteochondral tissue, including cartilage, vascularized bone, and an organized bone–cartilage interface. In an ectopic site, the tissue formation was not highly uniform, but these results suggest that these methods may be effective in regenerating osteochondral tissue *in situ*. IBD and SFF fabrication can be used to

manufacture biphasic composites that are capable of carrying functional loads upon implantation, replicating articular surface geometry and promoting integration with host tissues. We hope to combine these biological results with the biomimetic scaffold designs presented here and investigate the potential of this approach in regenerating a mechanically and biologically functional joint in an orthotopic site.

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