

**DESIGN AND IMPLEMENTATION OF A L-BAND
SINGLE ANTENNA POLARIMETRIC ACTIVE
RADAR CALIBRATOR**

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TABLE OF CONTENTS

LIST OF FIGURES	iv
LIST OF TABLES	vi
LIST OF APPENDICES	vii
CHAPTER	
ABSTRACT	1
I. INTRODUCTION	2
II. PARC THEORY / DESIGN CRITERIA ...	4
2.1 PARC Radar Cross Section	
2.2 Antenna Design	
2.2.1 L-Band Antenna Specifications	
2.2.2 L-Band Antenna System Performance	
2.2.3 Summary of Horn Performance	
2.3 G _{Loop} Design	
2.3.1 Delay Line	
2.3.2 Amplifiers	
2.3.2.1 Input Power Calculations	
2.3.2.2 Feedback Oscillations	
2.3.3 Attenuation Switches	
2.3.4 Notch Filter	

- 2.4 Control and RF Detection Circuitry
 - 2.4.1 Control Circuitry / Control Panel
 - 2.4.1.1 LED Battery Power Monitor
 - 2.4.1.2 Battery Over-discharge Protection
 - 2.4.1.3 Automatic System Activation Timers
 - 2.4.1.4 Voltage Regulation
 - 2.4.1.5 Auxiliary Switching Capability
 - 2.4.1.6 External Source Hook-up
 - 2.4.1.7 Recharge Ports
 - 2.4.2 Detection Circuitry
- 2.5 Temperature Stabilization
- 2.6 Assembled Prototype

III. EXPERIMENTAL RESULTS 41

- 3.1 Anechoic Chamber Tests
 - 3.1.1 SAPARC Time Domain Response
 - 3.1.2 0° Orientation Test
 - 3.1.3 45° Orientation Test
- 3.2 G_{Loop} Measurements
- 3.3 Thermal Gain Testing
- 3.4 Field Deployment Conditions
 - 3.4.1 Battery Capacity
 - 3.4.2 All-Weather Performance

IV. CONCLUDING REMARKS 63

REFERENCES

APPENDICES

LIST OF FIGURES

Figure

- 2.1 Basic PARC Configuration
- 2.2 L-Band SAPARC System Block Diagram
- 2.3 Magnitude and Phase Patterns For a Two Antenna PARC
- 2.4 Side View of the L-Band Tapered Square Horn Antenna
- 2.5 Depiction of Adequate and Inadequate Beamwidths For a Horn Antenna
- 2.6 Multipath Contribution Scenarios For Horn Antennas With and without Significant Sidelobes
- 2.7a L-Band SAPARC Antenna System
- 2.7b View of the L-Band OMT
- 2.7c Detail Drawings of the L-Band OMT
- 2.8 The Effects of Placing a Delay Line Within the PARC System
- 2.9 S_{21} Frequency Domain Response of the L-Band Delay Line
- 2.10a JPL AIRSAR Fly-by Geometry
- 2.10b NASA SIR-C Fly-by Geometry
- 2.11 Frequency Response of the Notch Filter
- 2.12 SAPARC Control Printed Wiring Assembly (Unstuffed)
- 2.13 SAPARC Control Printed Wiring Assembly (Stuffed)
- 2.14 Blueprint of the SAPARC Front Control Panel
- 2.15 SAPARC Front Control Panel
- 2.16 Internal Components of the L-Band SAPARC Unit
- 2.17 a Disassembled L-band Antenna Unit and Support
- 2.17 b Assembled L-band Antenna Unit and Support
- 2.18 a Fully Assembled L-Band SAPARC for the 0° Antenna Orientation
- 2.18 b Fully Assembled L-Band SAPARC for the 45° Antenna Orientation

- 3.1 Frequency Domain Response of G_{Loop} at 24°C
- 3.2 L/C/X-Band POLARSCAT Test Equipment
- 3.3 Anechoic Chamber Measurements at the University of Michigan's Radiation Laboratory
- 3.4 SAPARC Time Domain Response
- 3.5 SAPARC 0° Orientation Phasor Polarizations
- 3.6 SAPARC 0° Orientation RCS Azimuthal Patterns at 20°C (SIR-C Mode)
- 3.7 SAPARC 45° Orientation Phasor Polarizations
- 3.8 SAPARC 45° Orientation RCS Azimuthal Patterns at 20°C (SIR-C Mode)
- 3.9 SAPARC 45° Orientation Phase Patterns at 20°C (SIR-C Mode)
- 3.10 Phasor Diagrams for the 45° Orientation
- 3.11 L-Band SAPARC Thermal Gain Variations
- 3.12 Battery Capacity Test (1.0 A Load, 22° C)
- 3.13 Full Load Battery Capacity Test (1.2 A Load, 22° C)
- 3.14 Cold Weather Battery Capacity Test (1.2 A Load, -10° C)
- A-1 Isolation of L-band OMT
- A-2 Return Loss of L-band OMT (Side Arm, 1.1-1.4 GHz)
- A-3 Return Loss of L-band OMT (Streight Arm, 1.1-1.4 GHz)
- B-1 Gain of the Pre-amplifier at 24° C
- B-2 Gain of the Power Amplifier at 24° C

LIST OF TABLES

Table

- | | |
|-----|---------------------------------------|
| 2.1 | L-Band Antenna System Characteristics |
| 2.2 | JPL AIRSAR Parameters |
| 2.3 | NASA SIR-C Parameters |
| 3.1 | L-Band Measurement System Parameters |
| 3.2 | Marker Identification for Figure 3.4 |
| 3.3 | Power Demands on Supply 2 |

LIST OF APPENDICES

Appendix

- A OMT Specifications
- B Amplifier Specifications
- C Control Circuitry Schematics
- D Measurement and Calibration Programs

ABSTRACT

This report serves as a documentation of the design parameters and performance characteristics of a L-band single antenna polarimetric active radar calibrator (SAPARC) developed for JPL and NASA at the University of Michigan's Radiation Laboratory. The device is one of four which are currently being constructed for future JPL/NASA Synthetic Aperture Radar (SAR) missions. The report includes details of the SAPARC's RF and digital / analog electronics design, as well as test results from a number of anechoic chamber measurements. Application notes and suggestions are also included throughout.

CHAPTER I

INTRODUCTION

Active and passive radar calibrators are often used in conjunction with airborne and space borne polarimetric imaging SAR platforms. When strategically placed, these devices serve as ground-based calibration targets with specified radar cross sections (RCS). Trihedrals / corner reflectors are by far the most common type of calibration device used; however, their physical size and weight make them undesirable for field deployment. The drawbacks associated with trihedrals are two-fold. First, an actual deployment of the device can be physically awkward and inconvenient. Trihedrals can be as large as 12 ft by 12 ft by 12 ft, and they can weigh up to 300 pounds. In addition to their cumbersome size and weight, trihedrals tend to act like large rain and snow collectors, thus complicating the chances of performing an accurate calibration.

The second drawback is a bit more subtle, but just as significant. The accuracy of an external calibration of a radar system directly relies on the knowledge of the scattering matrix of the calibration target. Although it is possible to estimate the elements of the scattering matrix of a calibration target analytically, manufacturing tolerances may leave a fair amount of uncertainty in the estimated values. Therefore, it is necessary to measure the calibration targets against a precise calibration target, such as a metallic sphere. This reveals the second drawback of passive calibrators with large physical dimensions, namely that the far field condition and uniform illumination criteria are difficult to meet in the laboratory. Hence, it becomes difficult to accurately define the performance characteristics of passive calibrators of this size and type.

Polarimetric active radar calibrators (PARCs), on the other hand, tend to be much smaller and easier to handle than their passive counterparts. A PARC also yields better calibration measurements since its SAR image can be translated over a dark background, thus providing a higher signal to background ratio. As a result of these advantages,

PARCs are rapidly becoming the calibration device of choice for future space borne missions.

As a final point, PARCs traditionally are designed with two antennas which can cause severe degradation in their performance, as will be explained later. Here a new design for the L-band PARC is used which requires a single antenna.

The purpose of this report is to outline of the theory, design, and implementation of the L-band single antenna PARCs developed for NASA and JPL at the University of Michigan. The content of this project reflects the modifications and improvements made to previous PARC and SAPARC units (specifically, an L-band SAPARC prototype built by Sarabandi et al. for the University of Michigan's Radiation Laboratory [2]). Currently, the L-Band SAPARCs are tentatively planned for field deployment in April 1994, where they will be used as calibration devices for NASA's SIR-C (Shuttle Imaging Radar -C) mission.

CHAPTER II

PARC THEORY / DESIGN CRITERIA

In its simplest form, a PARC consists of a receive antenna, an amplifier, and a transmit antenna (see Figure 2.1). With this configuration, the PARC merely acts like a repeater, whereby an incoming radar signal is received, amplified, and re-transmitted back to the SAR platform. Variations on this simple design do, however, lead to a variety of merits.

Figure 2.2 depicts the modifications which are employed in this project's SAPARC units. The most notable difference is the addition of a delay line along with an orthogonal mode transducer (OMT) / single antenna implementation. The device now serves as a specialized type of repeater, where the signal is captured with respect to one polarization and re-transmitted via its opposite polarization. The pre-amplifier and power amplifier ensure the proper amplification of the signal, while the delay line electrically delays the signal for reasons which will be given later. As a final note, the switches provide the attenuation needed for applicability to SIR-C as well a JPL AIRSAR missions.

2.1 PARC Radar Cross Section

The fundamental equation defining the radar cross section (RCS) of a PARC is given by [2]

$$\sigma = G_{Loop} \frac{G_T G_R \lambda^2}{4\pi}$$

where G_T and G_R are the transmit and receive antenna gains, and G_{Loop} is the net loop gain associated with the gains and losses from the system's amplifiers, switches, and delay line. Generally speaking, a larger RCS is more desirable. Hence, the driving

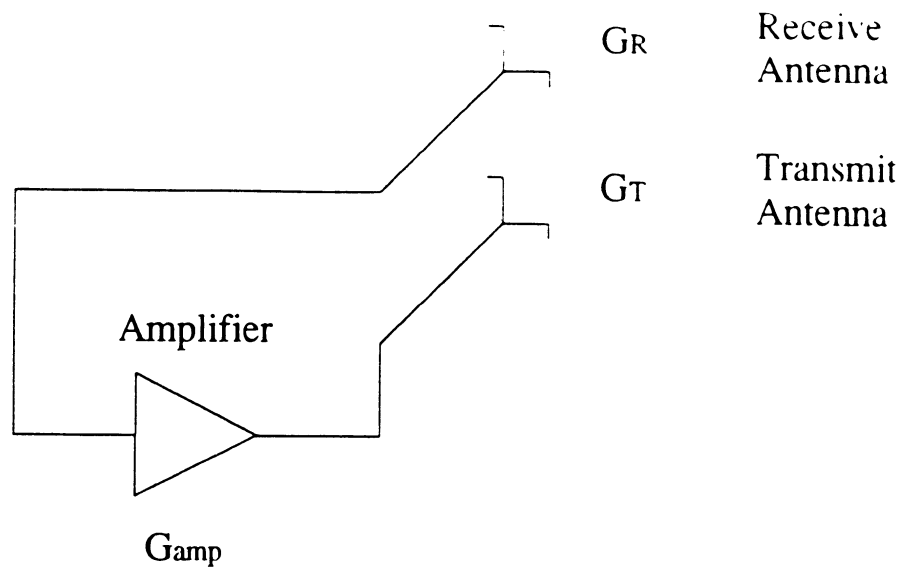


Figure 2.1: Basic PARC Configuration

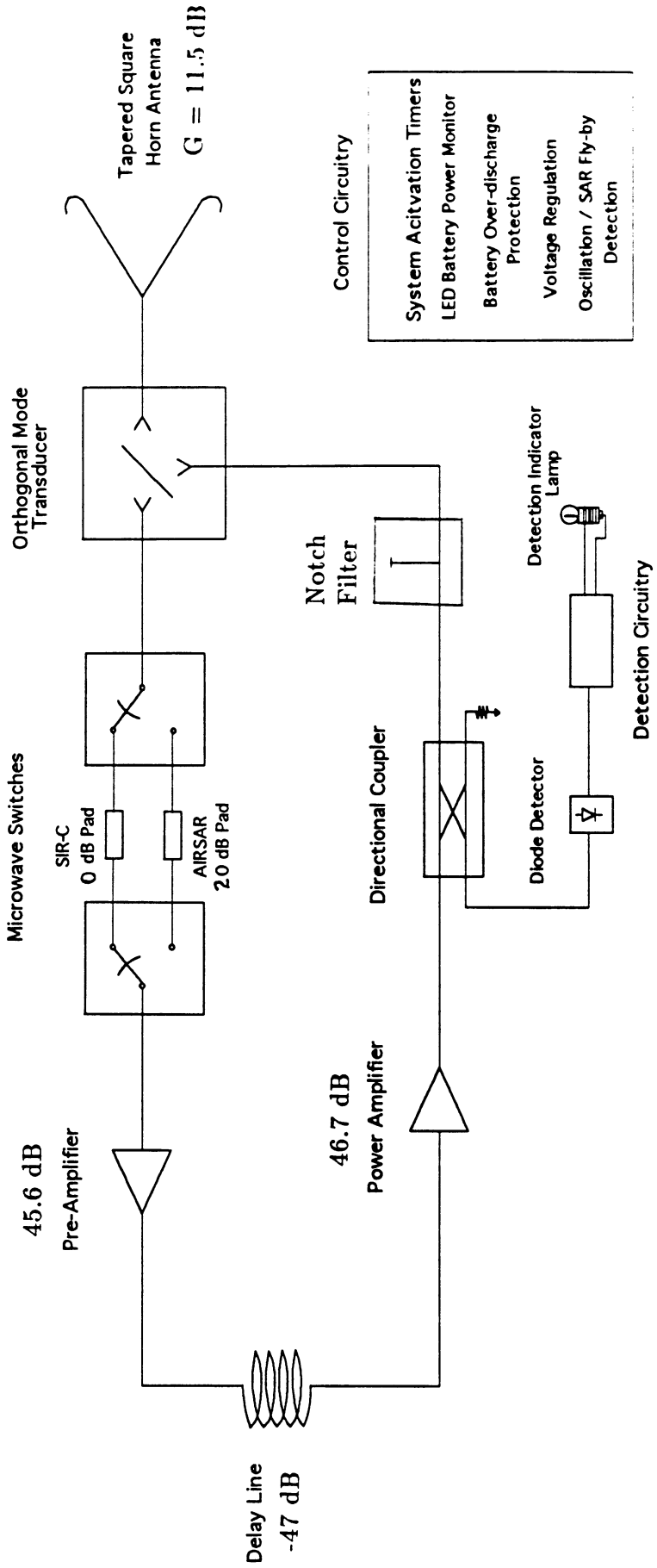


Figure 2.2: L-Band SAPARC Block Diagram

impetus behind most PARC designs is the maximization of G_{Loop} , G_T , and G_R . These parameters, in turn, are limited by beamwidth requirements, transducer isolation performance, and physical size and weight considerations. The following sections address each of these parameters in more detail.

2.2 Antenna Design

In the design of early PARC systems, two antennas, one for transmit and one for receive, were employed to achieve the necessary isolation between the receiver and transmitter modes of the PARC. The transmit and receive antennas were placed in close proximity to one another to meet the compactness requirement of the PARC design. However, since the antennas are in the near field of each other, the RCS pattern of the PARC becomes asymmetric and causes ripples in the phase and amplitude responses which tend to mar the PARC's performance [1] (see Figure 2.3). In order to counter these setbacks and yet to meet the compactness requirement, a single antenna PARC was considered. In this design, the PARC employs a dual polarized horn antenna with a very good polarization isolation and low return loss for both polarization channels. Wide bandwidth and beamwidth with high cross polarization isolation can be achieved through the implementation of an OMT (Orthogonal Mode Transducer) in conjunction with a piecewise tapered square horn.

The geometry of a piecewise tapered horn is shown in Figures 2.4. The waveguide discontinuity at a flared intersection excites higher order waveguide modes which are proportional to the flare angle. Since the waveguide is square, the higher order modes can couple energy into the orthogonal channel (TE_{10} to TE_{01} , for example). It was noticed that when the flare angle is less than 5° , the energy transfer from between the orthogonal channels is minimized. However, in order to get the desired aperture over a reasonable length, the square horn can be flared (with angles less than 5°) at many points along its length, thereby simulating an exponential taper. Note that the length of each section should be longer than the wavelength.

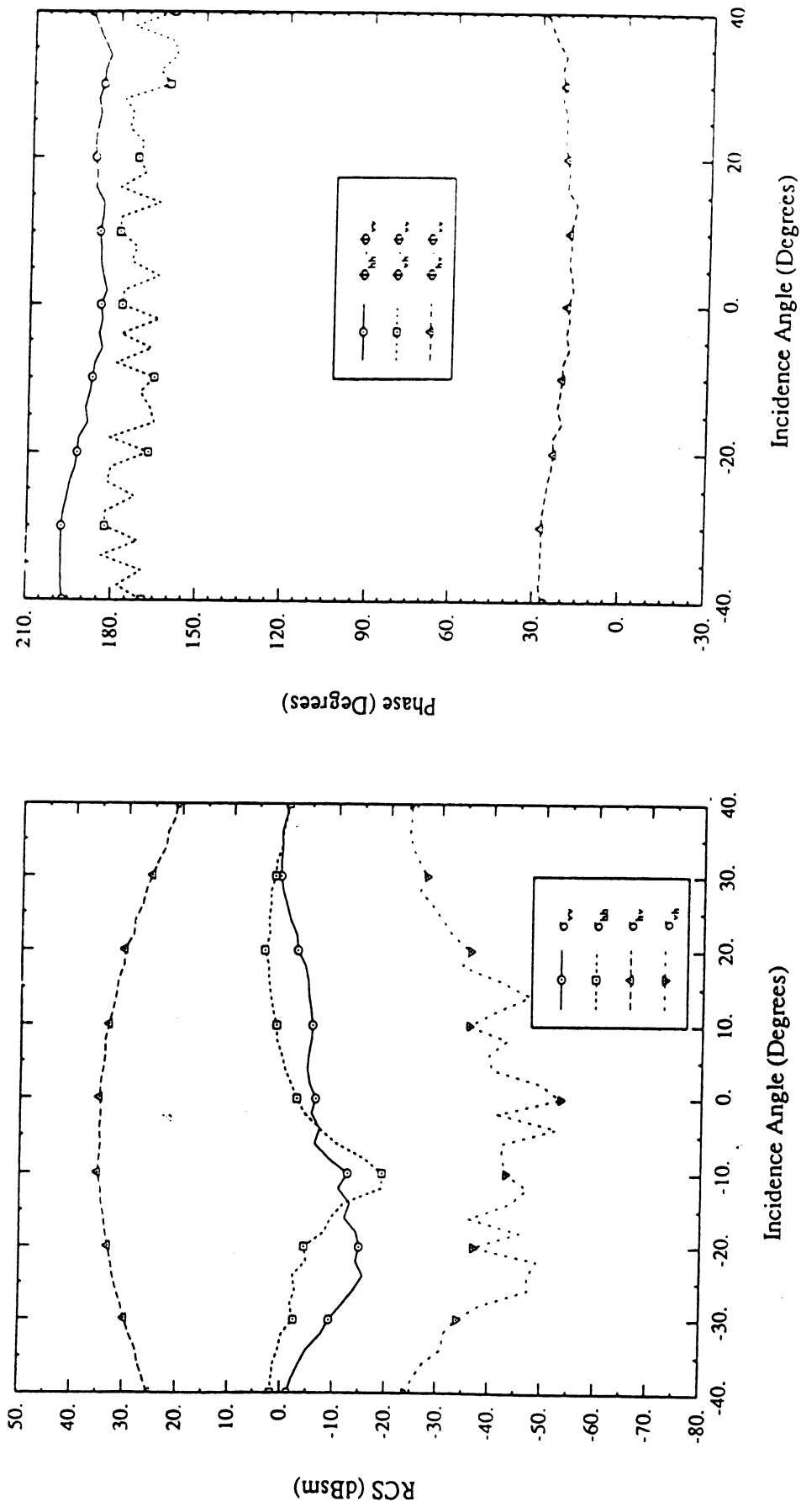


Figure 2.3: Magnitude and Phase Patterns for a Two Antenna PARC System

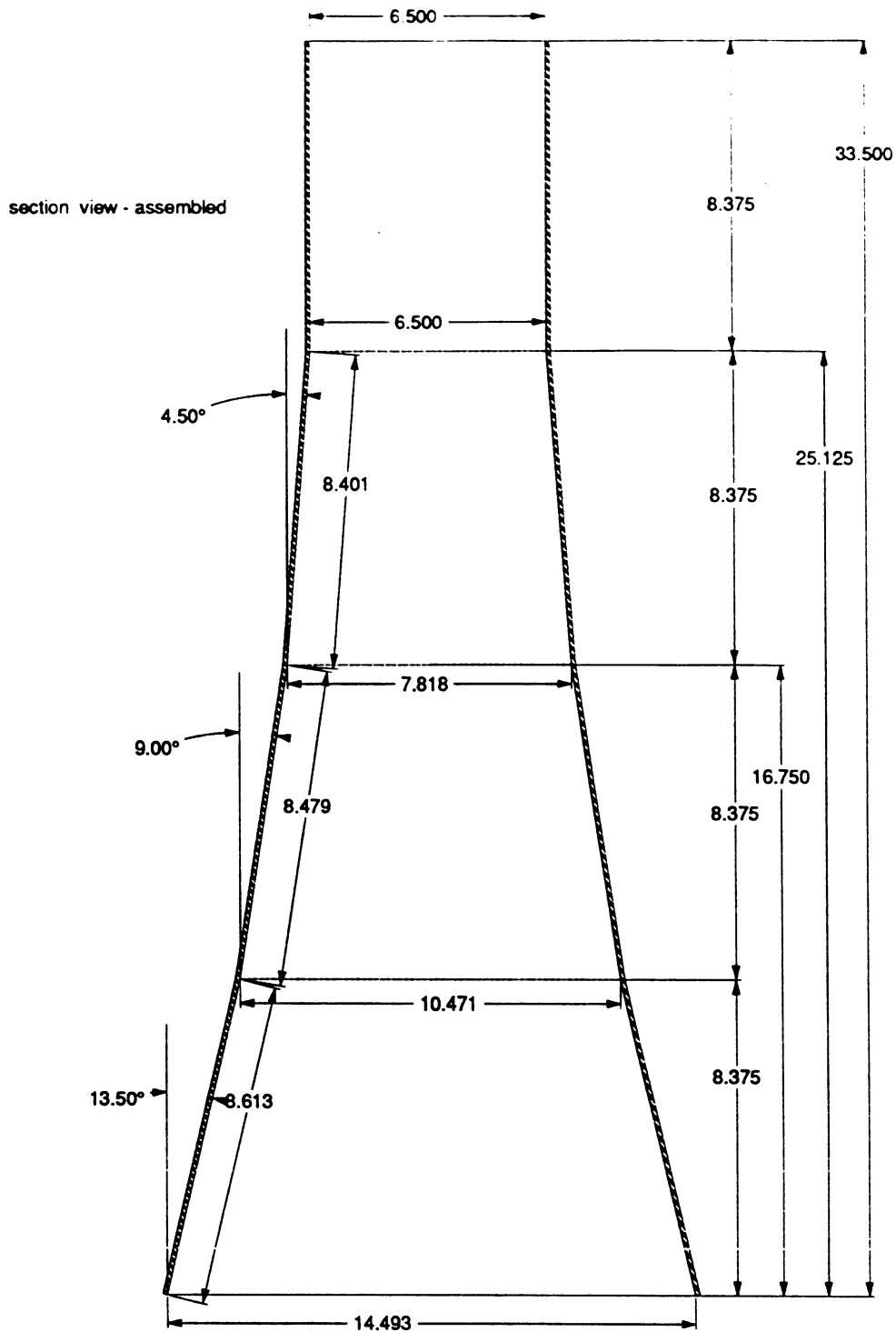


Figure 2.4: Side View of the L-band Tapered Squared Horn Antenna

2.2.1 L-Band Antenna Specifications

The goal of the SAPARC's antenna design is to reduce the RF mismatch and cross-talk (i.e. cross polarization generation) while at the same time providing adequate gain, beamwidth, and bandwidth. For the L-band SAPARC, the primary concern of the design was the trade-off between the reciprocal parameters of antenna gain and beamwidth. Physical size and weight were also considered due to the relatively large wavelength of the L-band system.

From a practical point of view, the scattering matrix of the SAPARC must be rather insensitive to orientation angles, i.e. a SAPARC should be immune to possible pointing errors). Thus, one of the design goals is to achieve a two-way antenna beamwidth of around 20° . Note that the relatively large beamwidth ensures a successful calibration even if the SAPARC is not directly within the line of sight of the SAR platform. Figure 2.5 demonstrates pictorially the importance of having a wide antenna beamwidth.

A secondary goal was to reduce the sidelobes radiating from the aperture, thereby minimizing the effect of multipath reflections to and from the SAPARC's ground-based position. Multipath contributions yield inaccurate RCS responses since unwanted electromagnetic energy is effectively being collected by the SAPARC antenna system (see Figure 2.6). The nominal RCS response, however, is measured within an anechoic chamber where multipath contributions are negligible. Hence, measurements taken within anechoic chamber and field environments may differ considerably. Using an antenna with small sidelobes is advantageous in that multipath contributions will be reduced; thus, measurements taken during actual field deployment conditions will more closely resemble measurements taken within the chamber environment.

One of the project's early prototypes incorporated the use of a corrugated horn with a square aperture. Note that corrugated horns generally offer improved performance since they reduce the side lobes in the antenna pattern. Unfortunately, this prototype yielded a high degree of co-polarized mismatch and extremely poor cross polarization isolation. The concept of employing a dielectric lense was also tried; however, the costs of constructing adequate lenses or custom made corrugated horns became much too

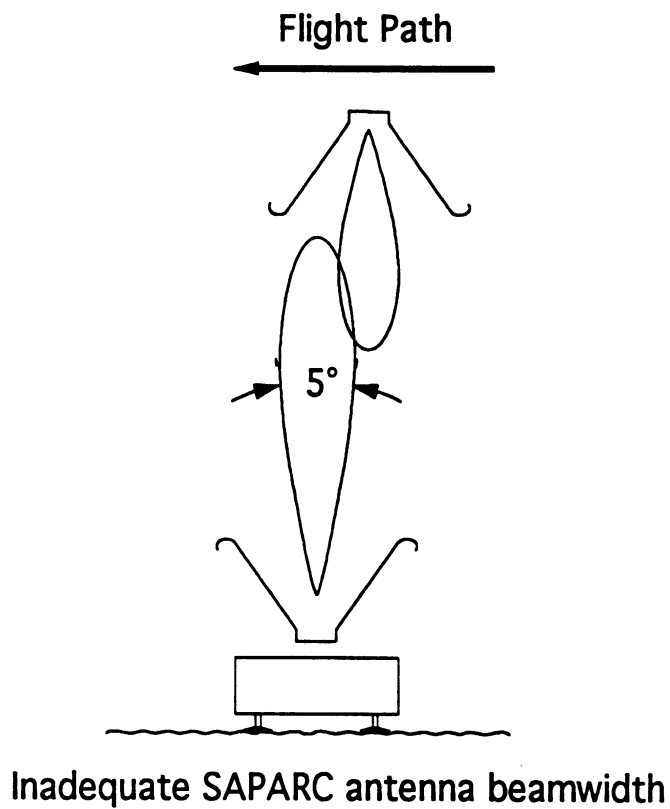
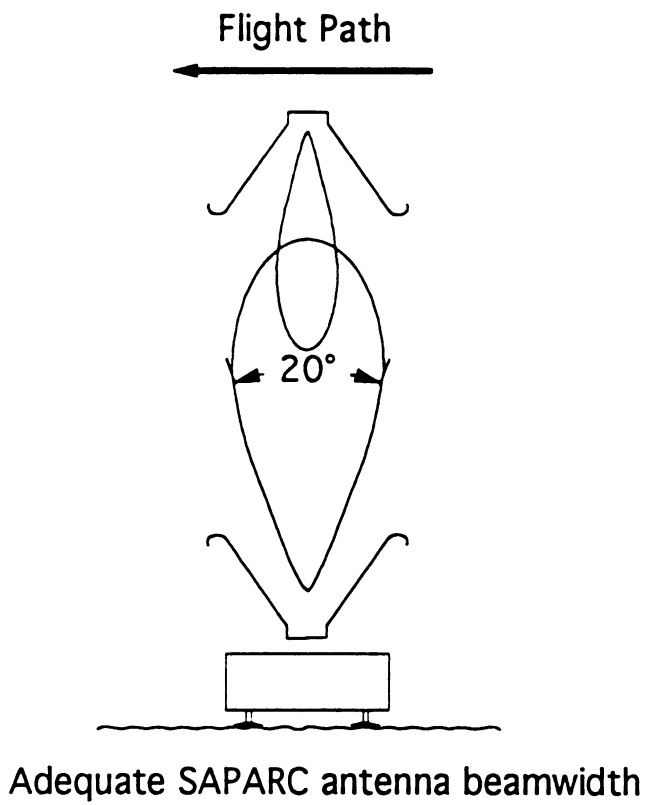


Figure 2.5: Depiction of Adequate and Inadequate Beamwidths for the Tapered Square Horn

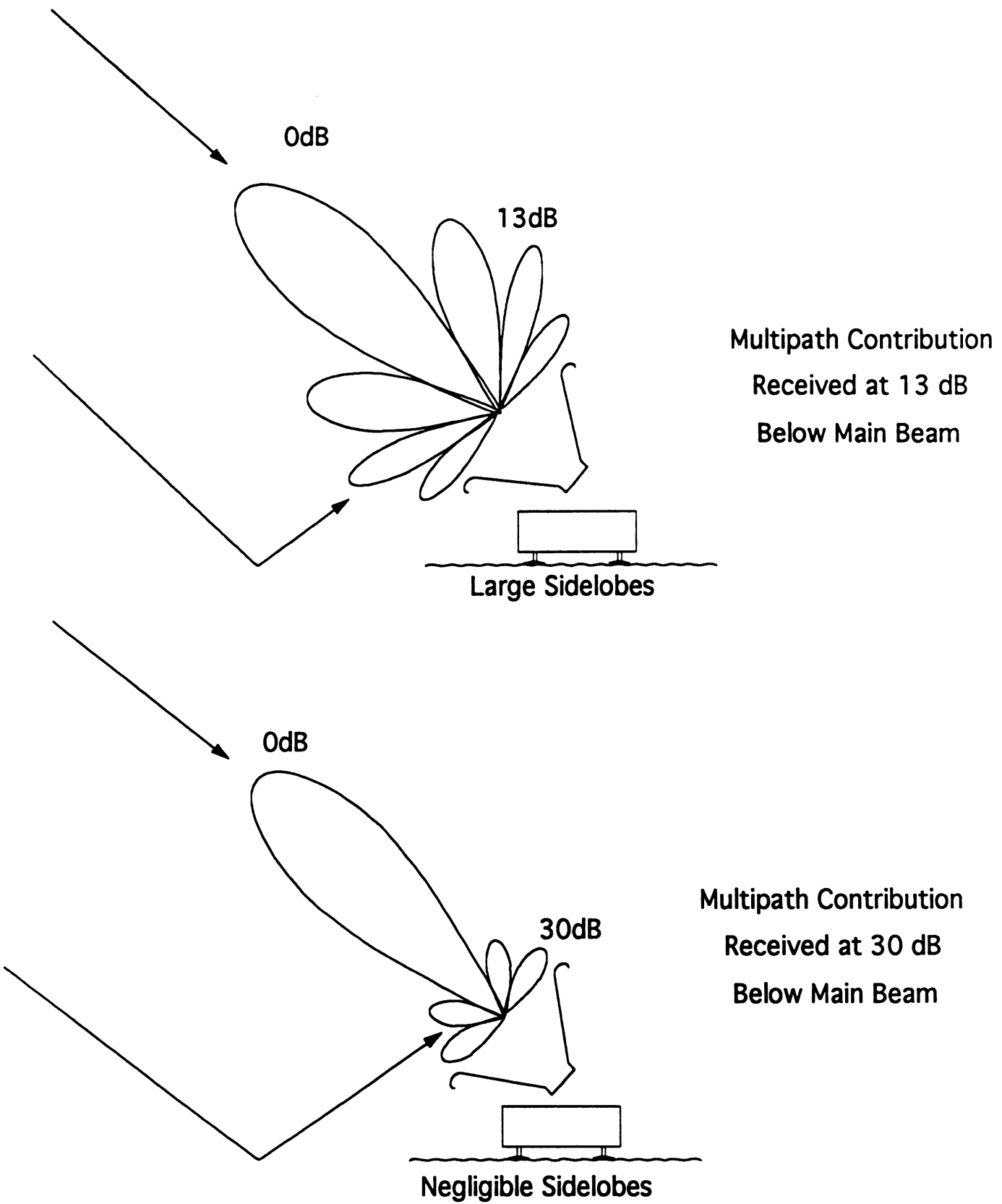


Figure 2.6: Multipath Contribution Scenarios for Horn Antennas With and Without Significant Sidelobes

prohibitive. Therefore, it was decided that the most economically feasible design would forego the multipath considerations.

The physical dimensions of the prototype horn was chosen to be 84.2 cm in length with a square aperture of 36.8 cm by 36.8 cm (1.5λ by 1.5λ). Based on these promising results, a final design was implemented using four equi-length sections flared in 4.5° steps. As shown in Figure 2.4, the overall length of the horn is 86 cm with an aperture of 36.8 cm by 36.8 cm (1.5λ by 1.5λ).

As a final point, the L-band SAPARC employs an OMT designed and fabricated in the Radiation Laboratory of the University of Michigan [2]. The polarization separation is realized in a squared T-junction using wire grids (Figs. 2.7b and 2.7c). The positions of the wires are chosen such that the return-loss and cross-talk are minimum. This device provides cross polarization isolation of better than 40 dB with a return loss less than -18 dB over the frequency range of 1.1 - 1.4 GHz. See Appendix A for the detailed OMT test specifications. Figure 2.7a depicts the completed horn and OMT combination.

2.2.2 L-Band Antenna Performance

From the plots given in Figure 3.6, we can deduce that the antenna system (horn and OMT combination) yields a cross polarization isolation exceeding 32 dB. It should be noted that the maximization of G_{Loop} is dependent upon the level of isolation between the receive and transmit ports on the antenna. Refer to Figure 2.1. From this simple diagram, one can see how a feedback scenario results whenever a small fraction of energy is coupled from the transmit antenna to the receive antenna. The coupled electromagnetic wave is then repeatedly amplified as the energy continues along the feedback loop. Eventually, the coupled energy will increase to a magnitude which saturates the amplifiers. For obvious reasons, this situation cannot be tolerated for a PARC design. Therefore, the antenna system's cross polarization isolation must be large enough to prevent the occurrence of a feedback loop.

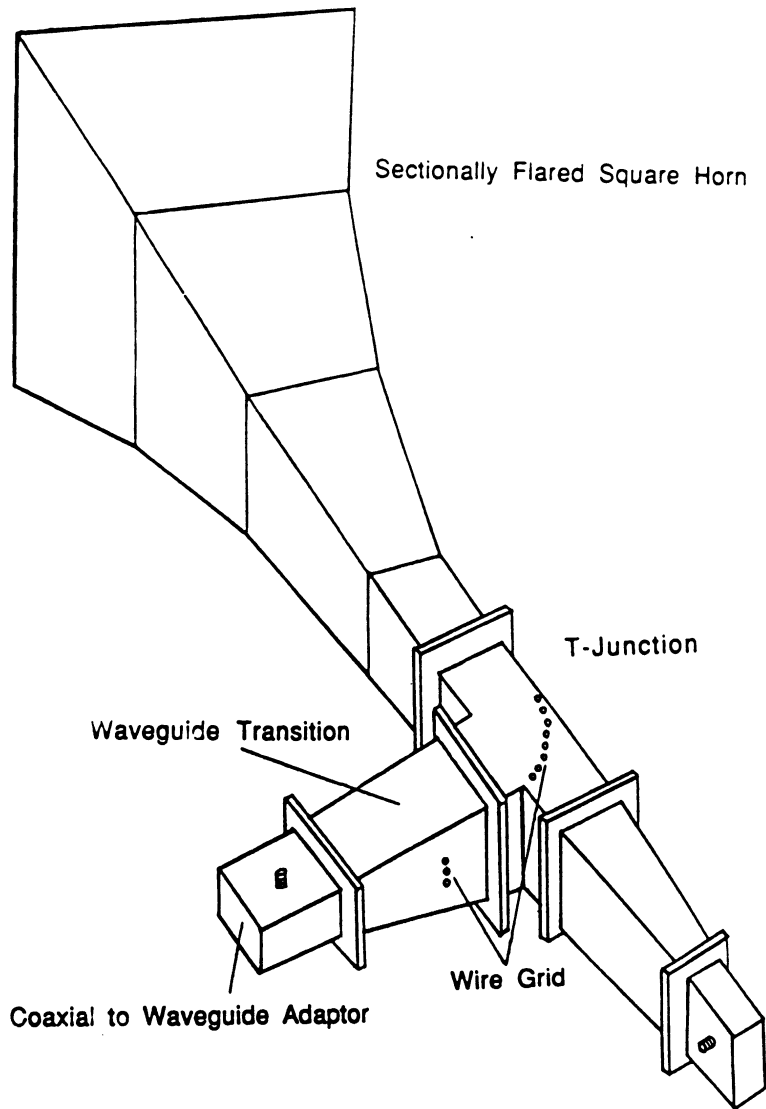
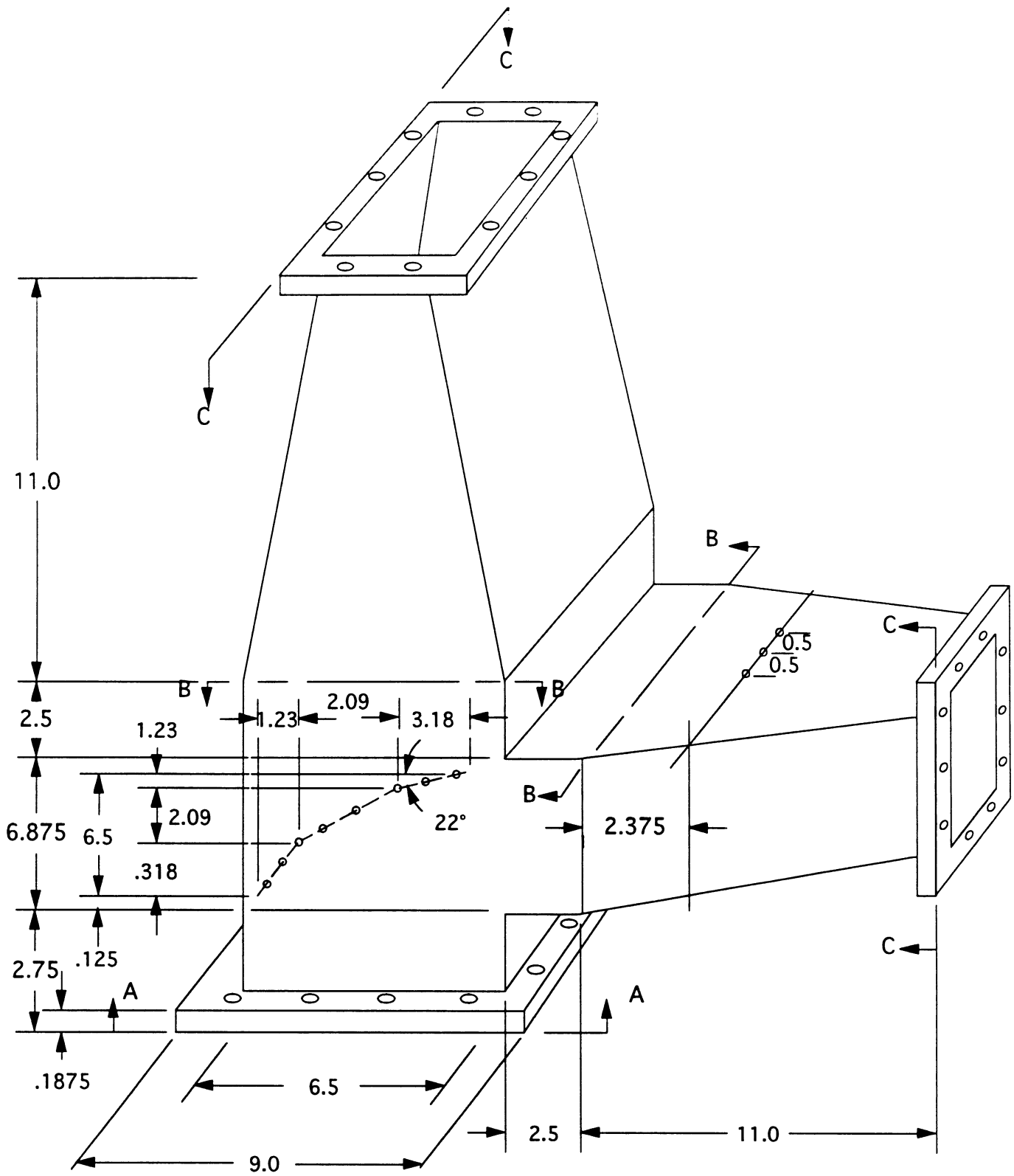


Figure 2.7a: L-band SAPARC Antenna System

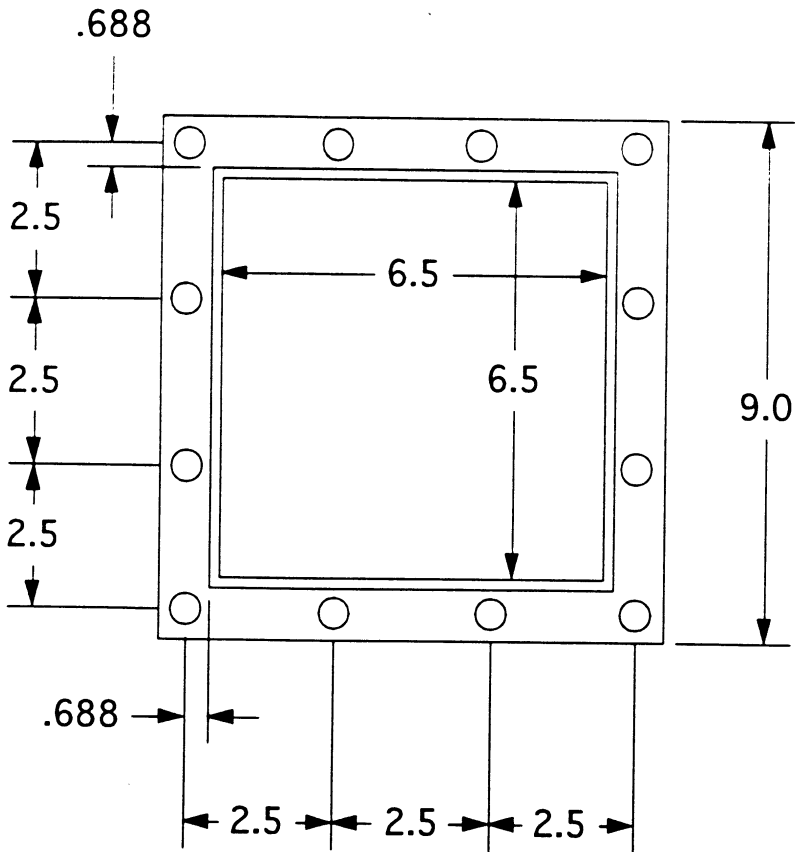


L-Band SAPARC OMT Design

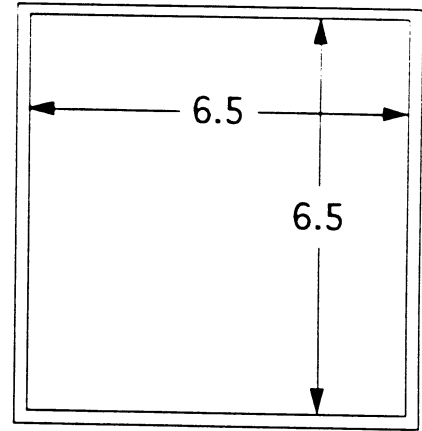
- All dimensions in inches
- Refer to detail drawings for views A-A, B-B and C-C

Figure 2.7b: View of the L-band OMT

View A-A



View B-B



View C-C

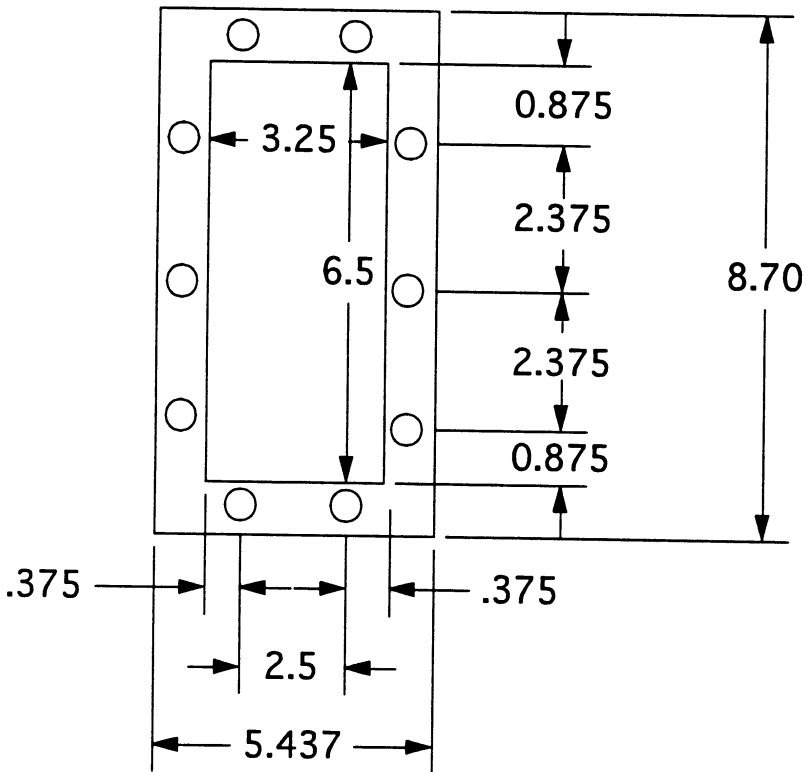


Figure 2.7c: Detail Drawings of the L-band OMT

2.2.3 Summary of Horn Performance

<u>Physical Characteristics</u>	<u>Electrical Characteristics</u>
Aperture Size: 36.8cm X 36.8cm	Gain: 11.5 dB
Length: 86 cm	2-Way 3 dB
Weight: 15 lbs.	Beamwidth: 25°
Material: Aluminum	

Table 2.1: L-Band Antenna System Characteristics

2.3 GLoop Design

2.3.1 Delay Line

At the heart of any PARC system is the G_{Loop} component of the RCS. As mentioned above, a PARC can enhance a calibration measurement by translating its SAR response over a dark background (i.e. a background with a specular surface, such as an airport runway or a large body of water -- See Figure 2.8). This technique is easily implemented by adding a low loss delay line between the receiver and transmitter, as shown in Figure 2.2.

When calculating the length of the delay line, a number of system parameters had to be incorporated in order to insure an adequate SAR delay. The slant range resolution, r_y , is given as 6.67 m for JPL's AIRSAR. As shown in Figure 2.8, the SAPARC should "appear" as if it is situated directly over a body of water. The quantity Δp corresponds to the distance between the physical location of the PARC and its desired SAR image position. An acceptable Δp is approximately 10 pixels (i.e. 10 range bins); therefore,

$$\Delta p = 10r_y = 66.7m$$

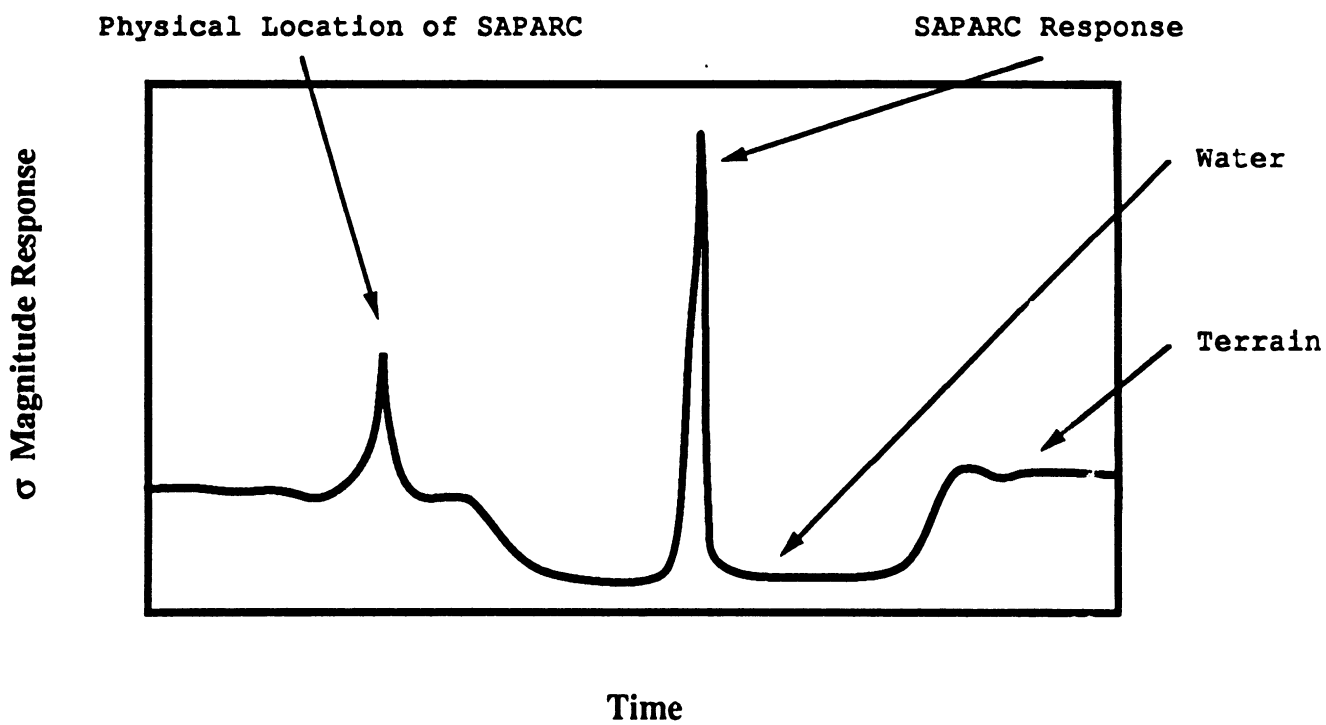
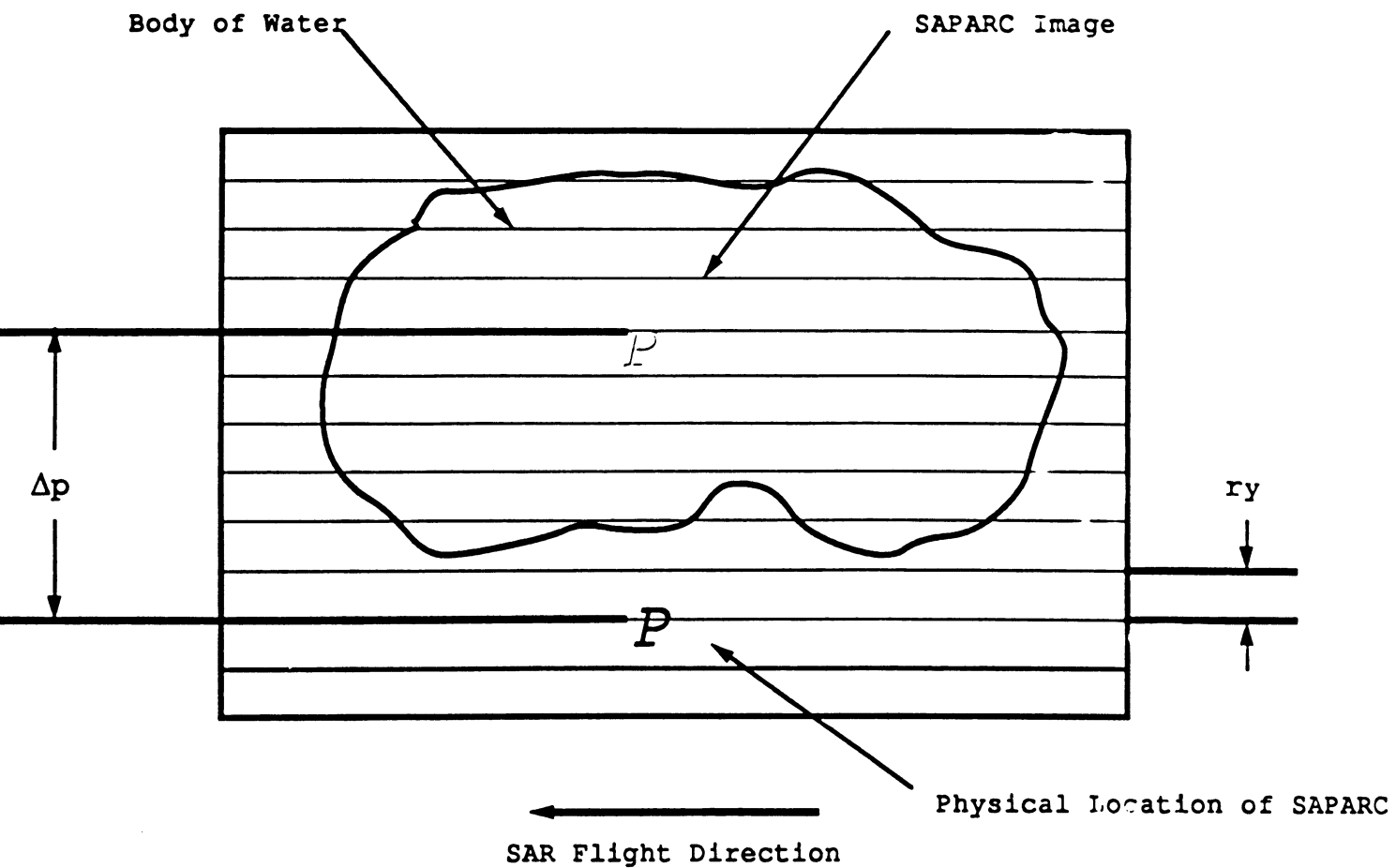


Figure 2.8: The Effects of Placing a Delay Line Within the PARC System

With Δp now known, the delay D can be found through the simple relationship

$$D = \frac{\Delta p}{c}$$

where c is the speed of light in free space. L_{\min} , the minimum length of line needed, is

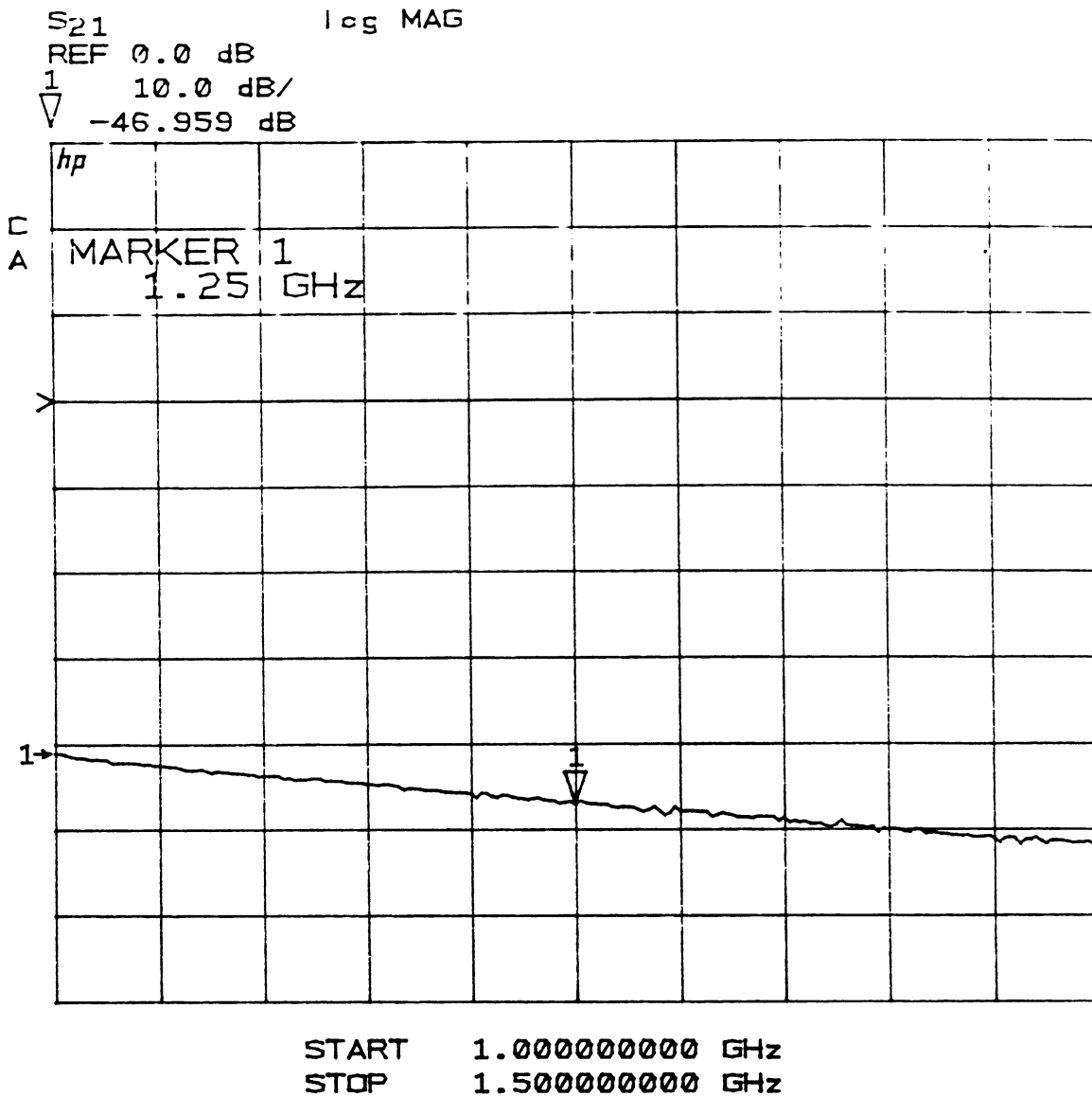
$$L_{\min} = Dv_{\text{coax}} = \frac{\Delta p(0.69c)}{c} = 46.02m = 150.99ft$$

Note that v_{coax} is the velocity of the wave within a coaxial medium. The minimum length of line required is approximately 151 feet, yet in actuality, all of the L- and C-band SAPARCs developed for this project use line lengths of 200 feet (therefore guaranteeing a sufficient delay).

At L-band frequencies, the 0.085 inch semirigid microporous coaxial cable (manufactured in 25 ft-long pieces by Precision Tube, Inc.) was used. The total attenuation resulting from the eight 25 ft-long sections was measured with a Hewlett Packard 8510 Network Analyzer, and was found to be approximately 47 dB at 1.25 GHz (see Figure 2.9).

2.3.2 Amplifiers

The role of amplification in a PARC is to increase the RCS of the antenna system and to compensate for the losses associated with the PARC's delay line and other passive components. The amplifier gain of a SAPARC system must be chosen such that the amplifier operates in the linear region. Amplifier saturation may occur for two reasons: 1. saturation due to high levels of input power received from the SAR platform, and 2. saturation due to feedback oscillations. The latter of the two results from a finite receive and transmit channel isolation (determined by the performance of the OMT and horn antenna).



**Figure 2.9: S_{21} Frequency Domain Response of
 the L-band Delay Line at 24°C**

2.3.2.1 Input Power Calculations

In order to insure that the amplifiers would not be saturated by the received RF, a number of preliminary calculations were made using the Friis transmission formula and known system parameters for JPL's AIRSAR and NASA's Shuttle Imaging Radar (SIR-C). Tables 2.2 and 2.3, respectively, summarize the JPL AIRSAR and NASA SIR-C parameters.

Peak Power	$P_t = 6 \text{ kW (67.8 dBm)}$
Wavelength	$\lambda = 0.24 \text{ m}$
Antenna Gain	$G = 18.3 \text{ dB}$
Altitude	15,000 - 40,000 ft (4,572 - 12,192 m)
Incidence Angles	$20^\circ - 70^\circ$
Pixel Resolution	3.03 m or 12.01 m (1 or 4 Look Azimuth) 6.67 m (Slant Range)

Table 2.2: JPL AIRSAR Parameters

Peak Power	$P_t = 4.45 \text{ kW (66.5 dBm)}$
Wavelength	$\lambda = 0.24 \text{ m}$
Antenna Gain	$G = 18 \text{ dB}$
Altitude	200 - 225 km
Incidence Angles	$15^\circ - 55^\circ$
Pixel Resolution	10 - 60 m Range Resolution

Table 2.3: SIR-C Parameters

For JPL's AIRSAR system, the following Friis transmission calculations are applicable. Figure 2.10a depicts the geometry of a typical fly-by, where h is the height of the platform and R is the corresponding range (i.e. distance between the SAR and the calibration unit). The values used in this calculation are for the "worst case" scenario with respect to possible amplifier saturation. Therefore, the dimensions correspond to the case where the maximum amount of power will be received by the SAPARC

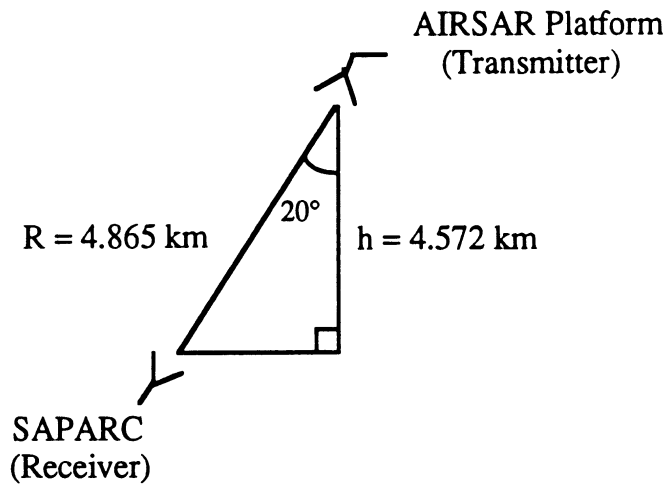


Figure 2.10a: JPL AIRSAR Fly-by Geometry

The general form of the Friis transmission formula is

$$P_R = P_T \left(\frac{\lambda}{4\pi R} \right)^2 G_T G_R \quad [4]$$

whereas

$$R = \frac{h}{\cos(\theta)} = 4.8654 \text{ km}$$

$$P_T = 6 \text{ KW} = 67.8 \text{ dBm}$$

$$\left(\frac{\lambda}{4\pi R} \right)^2 = \left(\frac{0.24 \text{ m}}{4\pi(4865.4 \text{ m})} \right)^2 = -108.1 \text{ dB}$$

$$G_T = 18.3 \text{ dB}$$

$$G_R \approx 11.5 \text{ dB}$$

Therefore, the maximum input power received by the first stage amplifier will be

$$P_R = 67.8 + 18.3 + 11.5 - 108.1 = -10.5dBm$$

Similarly, NASA's SIR-C system, shown in Figure 2.10b, will yield the following results.

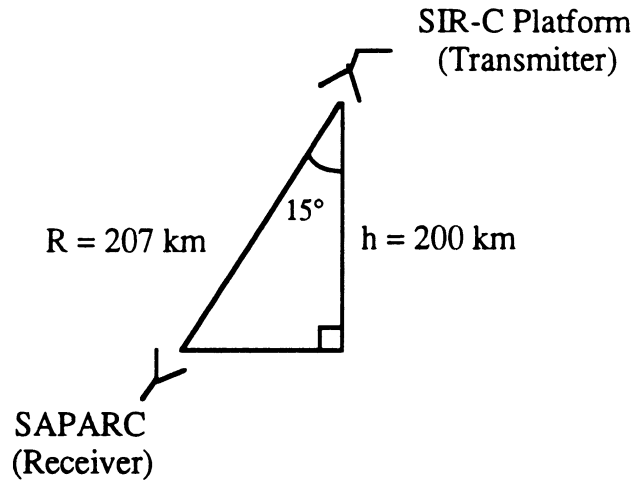


Figure 2.10b: NASA SIR-C Fly-by Geometry

The Friis transmission formula gives

$$P_R = P_T \left(\frac{\lambda}{4\pi R} \right)^2 G_T G_R \quad [4]$$

whereas

$$R = \frac{h}{\cos(\theta)} = 207.05 \text{ km}$$

$$P_T = 4.45 \text{ KW} = 66.5 \text{ dBm}$$

$$\left(\frac{\lambda}{4\pi R} \right)^2 = \left(\frac{0.24 \text{ m}}{4\pi(207.05 \text{ km})} \right)^2 = -140.7 \text{ dB}$$

$$G_T = 18 \text{ dB}$$

$$G_R \approx 11.5 \text{ dB}$$

Therefore, the maximum input power received by the first stage amplifier will be

$$P_R = 66.5 + 18.0 + 11.5 - 140.7 = -44.7 \text{ dBm}$$

The gain of the first stage amplifier (i.e. the pre-amplifier) is about 45.6 dB (see Appendix B). Hence, the first stage amplifier must be capable of producing the following output power levels in order to insure operation within the linear range of the amplifier.

$$\text{AIRSAR } P_{out} = P_R + G_{preamp} = -10.5 \text{ dBm} + 45.6 \text{ dB} = 35.1 \text{ dBm}$$

$$\text{SIR-C } P_{out} = P_R + G_{preamp} = -44.7 \text{ dBm} + 45.6 \text{ dB} = 0.9 \text{ dBm}$$

As shown in Figure 2.2, an additional attenuator of 20 dB was added to the front end of the pre-amplifier as an extra precaution to deter possible saturation during AIRSAR calibrations. Figure B-1 shows the gain of the pre-amplifier at 24°C.

Adding an attenuator "in front" of the amplifier degrades the signal to noise ratio; however, in this case, the signal level is much higher than the thermal noise, thus the effect of the additional attenuator is negligible. As will be pointed out in the next section, the noise inherent within the loop can lead to internal oscillations. Therefore, minimizing the noise will theoretically lead to a maximization of G_{Loop} . Yet, in light of the seriousness of amplifier saturation, it was agreed that the benefits resulting from this potentially lower noise performance could not outweigh the assurance that the pre-amplifier is operating within its proper linear range.

2.3.2.2 Feedback Oscillations

An equally serious problem can arise when the system is driven into a state of feedback oscillation. Section 2.3.2.1 alluded to the fact that noise inherent within the system can be amplified just as easily as any incoming RF signal. Oscillations result whenever the amplified noise exceeds the isolation of the antenna system. For the L-band SAPARC design, the net G_{Loop} gain must not exceed 32 dB (the antenna system's cross polarization isolation).

Since G_{Loop} must be less than 32 dB, it follows that

$$G_{Loop} = G_{Amp} + L_{Line} < 32 \text{ dB}$$

where L_{Line} is the loss from the delay line, component insertion, and flexible cables.

Rearranging this equation gives

$$G_{Amp} < 32 \text{ dB} + L_{Line} = 32 \text{ dB} + 47 \text{ dB} + 2.2 \text{ dB} + 1.8 \text{ dB}$$

Therefore

$$G_{Amp} < 83 \text{ dB}$$

Due to the relatively high loss of the delay line, a second amplifier is needed to help boost the signal before it is transmitted back to the SAR platform. As was done with the preamplifier, care must be taken to insure that the second stage amplifier is not driven into saturation. Figure B-2 shows the gain of the power amplifier at 24°C.

2.3.3 Attenuation Switches

The principle goal of the attenuation switch (see Figure 2.2 and Appendix C, pg. C-6) is to reduce the loop gain thereby allowing the SAPARC to be used for both JPL AIRSAR and NASA SIR-C missions with the maximum allowable RCS. As pointed out in Section 2.3.2.1, JPL's AIRSAR, which flies at significantly lower altitudes than SIR-C, has a correspondingly higher risk for saturating the SAPARC's amplifiers. Conversely, an excessively large G_{Loop} can lead to the saturation of the SAR platform's own receiver.

Note that the results shown throughout this report reflect the SAPARC's operation within the SIR-C mode. Similar results can easily be found for the AIRSAR case by simply subtracting 20 dB from the overall SIR-C RCS measurements.

2.3.4 Notch Filter

It was found that the system would slip into a feedback oscillation with SIR-C mode at about 990 MHz. Since the frequency of 990 MHz is outside of the frequency band of the system (1.1 - 1.4 GHz), a notch filter was inserted at the outgoing port (See Fig. 2.2) to eliminate the feedback oscillation at 990 MHz. The notch filter consists simply of a half-wavelength short stub of a rigid coaxial cable. Figure 2.11 shows the frequency response of the notch filter. The insertion loss at 1.25 GHz is about 0.8 dB and the attenuation at 990 MHz is about 17 dB as shown in Fig. 2.11.

2.4 Control and RF Detection Circuitry

The control and RF detection circuitry serves a two-fold purpose. First, it provides the necessary switching and timing functions for the various power loads; secondly, the circuits display the operating status of the entire system, thereby alerting the user of changes in battery capacity and calibration readiness. The system is comprised of three major components: the Control Printed Wiring Assembly (PWA), the Detection PWA, and the Control Panel. A more detailed description of each of these subsystems is given in the following sections.

2.4.1 Control Circuitry / Control Panel

The single antenna PARCs developed through this project feature custom made control and detection circuits. The features of the control circuitry are as follows:

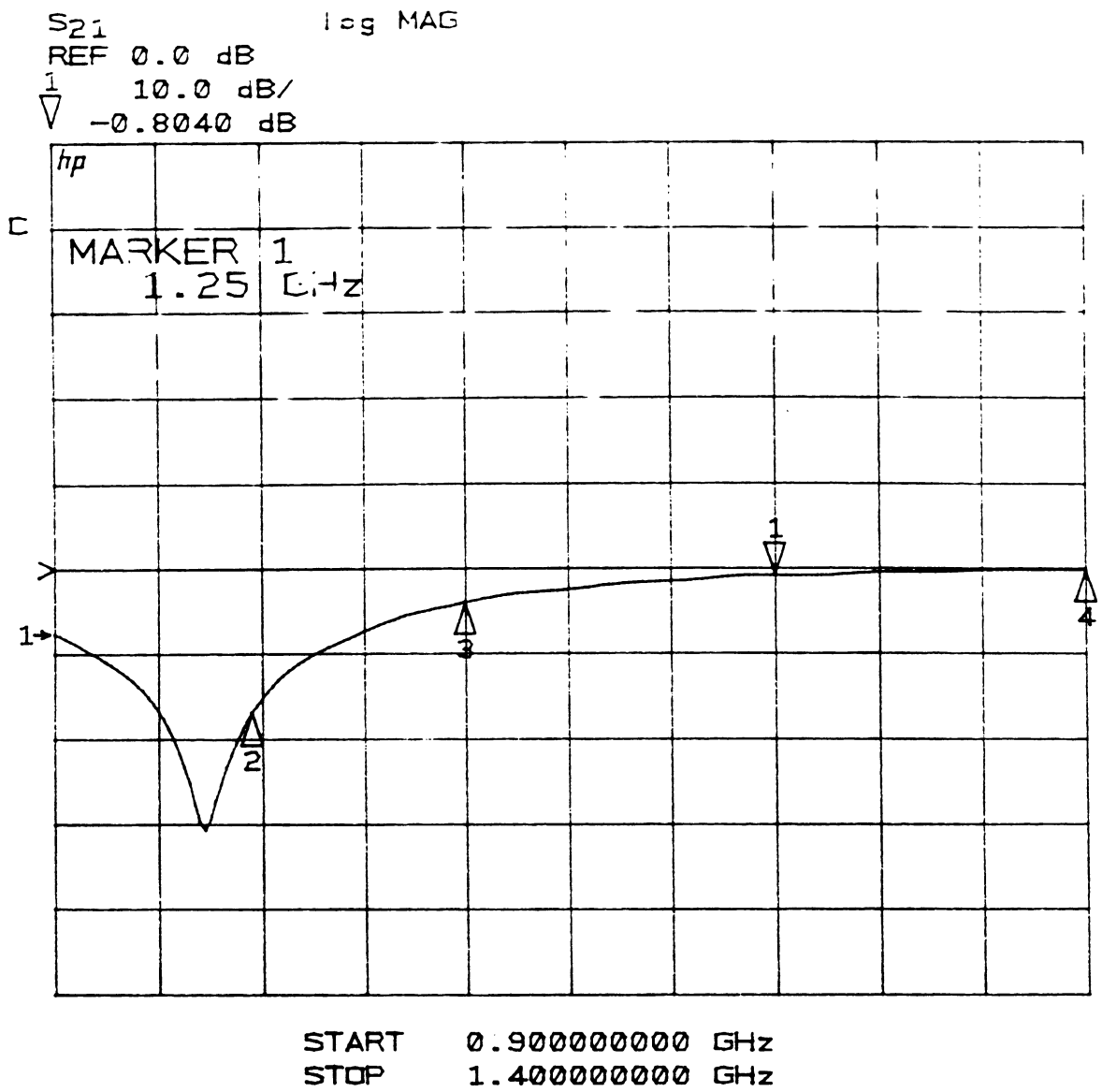


Figure 2.11: Frequency Response of the Notch Filter

- LED Battery Power Monitor
- Battery Over-discharge Protection
- Automatic System Activation Timers
- Voltage Regulation
- Auxiliary Switching Capability
- External Source Hook-up
- Recharge Ports for Internal Sources
- Easy Detachability for Maintenance

Most of the circuitry (for the functions listed above) is mounted on the Control PWA. This board was designed with EE Designer, a PWA layout software package which can be run on most IBM pc's. The PWA was then manufactured by L. Ross industries in Ann Arbor. (See Figures 2.12 and 2.13).

As a final note, the entire Control PWA / Detection PWA combination can be removed from the system chassis by disconnecting the 50 - pin connector. Before doing so, however, it is advised that the user first disconnect the internal supplies by removing the 7A fuses; the "BATTERIES" switch must then be turned on, and the "POWER RESET" button depressed (for 10 seconds) so that all residual charge held by the internal capacitance of the system can be safely discharged. (See Figure 2.14 and 2.15, both of which depict the front control panel).

2.4.1.1 LED Battery Power Monitor

The LED display mounted on the control panel is driven by a differential amplifier circuit which monitors the gradual drop in voltage of each separate lead acid battery (see Appendix C, pg. C-3). Preliminary tests showed that this drop is a linear function of time, whereby the safe operating range exists between $10V \leq V \leq 12.5V$ (refer to the battery operating curves given in Figures 3.13, 3.14, and 3.15). The entire system becomes fully loaded whenever the LED display is activated, thus yielding a more accurate measurement of the battery's remaining capacity. Note that under room temperature conditions, the Yuasa 7 A-hr 12V batteries can operate for up to 5.5 hours (under a full load of 1.2A) before the lower operating voltage threshold is reached. Colder temperatures will significantly limit this capacity; at $-10^{\circ}C$, the system can only operate for 4.5 hours before the same lower threshold causes the system to shut down.

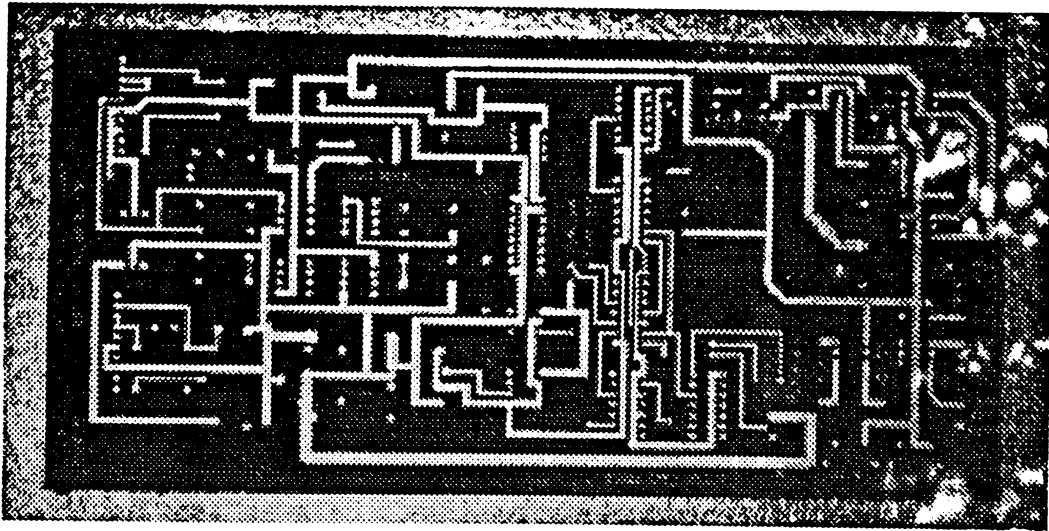


Figure 2.12: SAPARC Control Printed Wiring Assembly (Unstuffed)

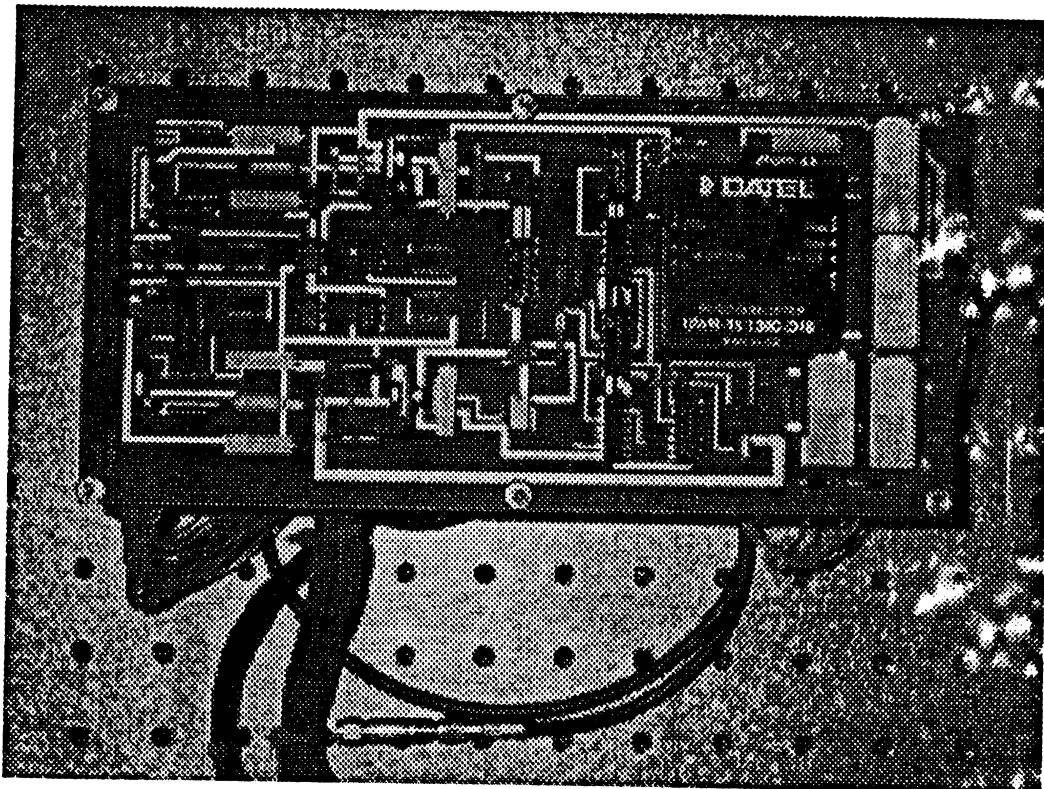


Figure 2.13: SAPARC Control Printed Wiring Assembly (Stuffed)

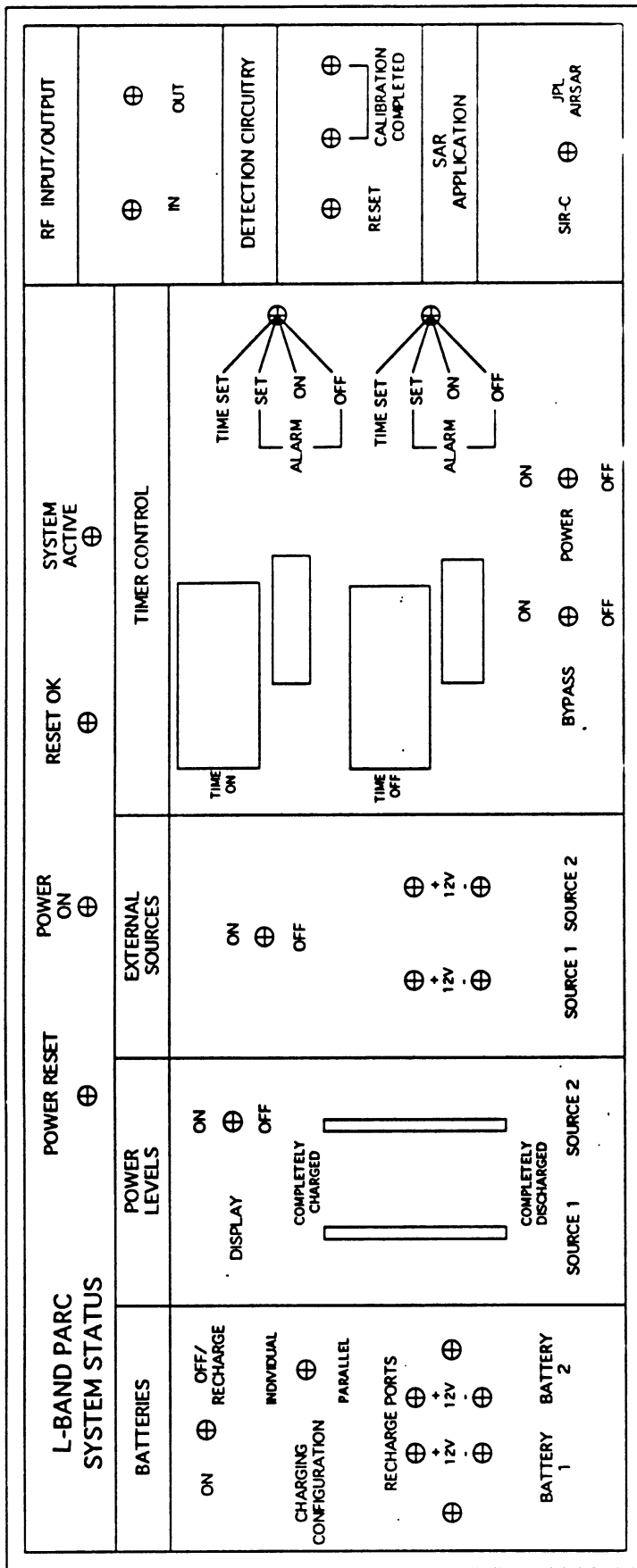


Figure 2.14: Blueprint of the SAPARC Front Control Panel

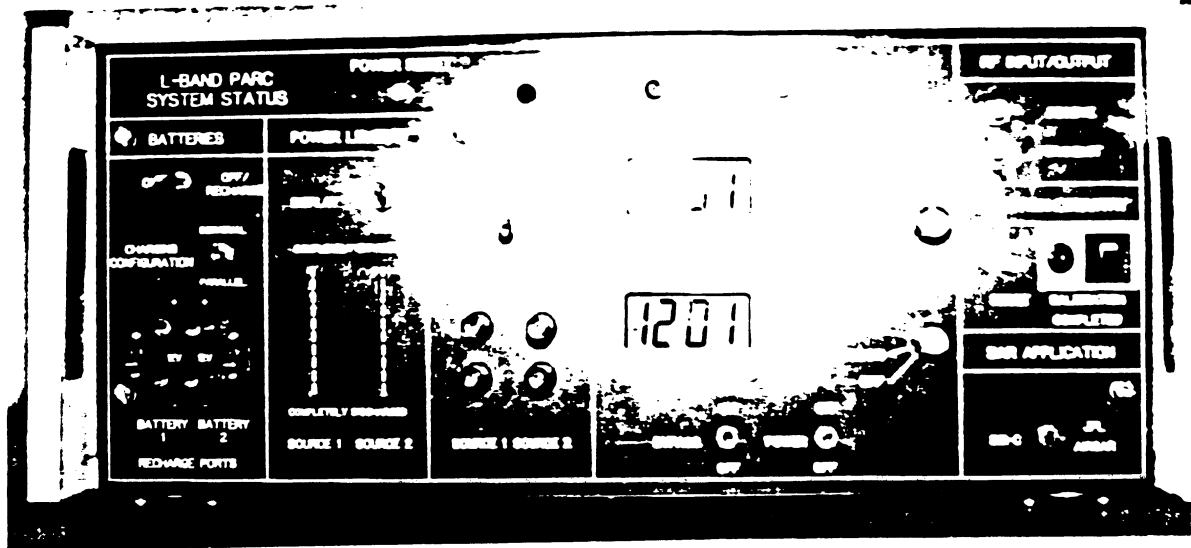


Figure 2.15: SAPARC Front Control Panel



Figure 2.16: Internal Components of the L-band SAPARC Unit

The LED display is currently set to measure a voltage range of $10.5V \leq V \leq 12.5V$ for each supply. This range can be adjusted for supplies 1 and 2 by tweaking the potentiometers R8 and R17, respectively.

2.4.1.2 Battery Over-discharge Protection

In conjunction with the LED bar graph display, the discharge protection circuitry similarly monitors the supply voltages through the use of comparitors (see Appendix C, pg. C-4). When the lower voltage threshold is reached (i.e. 10V), power to the entire system will be shut off, thus protecting the lead acid batteries from excessive discharging. (The battery's capacity is severely degraded whenever this lower voltage threshold is exceeded for extended periods of time.) This lower threshold can be easily adjusted by tweaking potentiometers R3 and R15 (for supplies 1 and 2, respectively).

2.4.1.3 Automatic System Activation Timers

The system's built-in activation timers can control the operation interval for the SAPARC. In almost all practical situations, the SAPARC needs to be on for a relatively short period of time which can be programmed using the activation timers, thus prolonging the SAPARC's use by conserving battery capacity (see Appendix C, pp. C-5-6). Two separate clocks are used: one for activating the high load components, and one for deactivating the entire circuit. The wiring design consists of a number of buffers and opto-isolators which connect the output of the timers (i.e. piezo-electric connections) with the rest of the control circuitry. Note that these connections were made with shielded 20 gauge wire; the first prototype, which did not use shielded wire, experienced occasional transient responses resulting from the switching of the high load components (e.g. amplifiers etc.). Proper shielding and the use of opto-isolators eliminated this problem altogether.

The timer activation mode can be bypassed for manual operation as well. In the manual mode, the system loads are all activated for immediate and constant operation, thus making this mode ideal for testing purposes. When deploying the SAPARC within a field environment, one should use the bypass in order to insure that the system cannot be

driven into a feedback state. Feedback oscillations will occur whenever an object is placed within the SAPARC's antenna beam pattern. Hence, a low-lying tree branch or other similar object may drive the system into an oscillation state. Using the bypass allows the user to "see" if any objects are within range of causing such problems. If the system can operate correctly in the bypass state, then the user will have confidence that the SAPARC will also work while in the automatic mode.

As a last note, the activation timers are independently powered by small cell 1.25V batteries. These cells can be easily replaced by removing the top cover on the SAPARC chassis. A small plastic cover on the clock units must also be removed in order to gain access to the battery compartments.

2.4.1.4 Voltage Regulation

The various subsystems within the SAPARC require supply voltages of $\pm 15V$, $\pm 8V$, and $+5V$. The $+5V$ and $\pm 8V$ regulation is performed by basic 7800 series regulators, whereas the $\pm 15V$ modes are supplied from DC-DC converters (one on the Detection PWA, and the second on the Control PWA - see Appendix C, pp. C-3,4, and 7). The $+15V$ DC-DC converter possesses an efficiency of greater than 80%; hence, the converter outperforms conventional voltage regulation by a considerable margin (i.e. in terms of efficient power use). It should also be noted that conventional regulators cannot supply the relatively large amount of current which is required for the operation of the amplifiers and other possible auxiliary loads.

2.4.1.5 Auxiliary Switching Capability

As mentioned above, the Control PWA is configured so that additional loads can be added (and thus controlled) as the user sees fit (see Appendix C, pg. C-2). The voltage output for these auxiliary ports includes $\pm 15V$ and $+24V$. Possible loads include recording devices which can monitor the RF power levels received during SAR fly-bys, thereby providing a means for measuring the pattern of the SAR's illuminating footprint.

The Detection PWA does provide a correlation between detected RF and a specific DC output voltage. This capability may be utilized for use with recording devices. Heaters can also be connected to this circuit; however, testing has shown that their use is of little value for reliable temperature stabilization. (See section 2.5).

2.4.1.6 External Source Hook-up

The user can bypass the internal battery supplies by employing the use of the external hook-up jacks located on the front control panel (see Figures 2.14 and 2.15, as well as Appendix C, pg. C-1). If external sources are to be used, simply flip the "EXTERNAL SOURCES" switch to the ON position. Hit the "POWER RESET" pushbutton and continue the system operation in the normal fashion. As a final note, **DO NOT CONNECT THE GROUNDS FROM THE EXTERNAL BATTERIES TOGETHER.**

2.4.1.7 Recharge Ports

The user can also recharge the internal batteries via the recharging ports located on the front control panel (see Figures 2.14 and 2.15, as well as Appendix C, pg. C-1). Two different port types are provided for the support of varying recharging devices. When recharging, have the "BATTERIES" switch in the OFF / RECHARGE position. The "CHARGING CONFIGURATION" switch permits the user to charge the batteries individually or together in a parallel mode.

2.4.2 Detection Circuitry

The Detection PWA was acquired from an existing two-antenna PARC system developed by Applied Microwave (see Appendix C, pg. C-7). This subsystem monitors the power levels which exist at the output of the power amplifier. The threshold for this detection has been set low enough ($P_{\min \text{ detection}} = -48.6 \text{ dBm}$) so that oscillations as well as SAR fly-bys can be recorded. In the original circuit design, a detection would illuminate a

small red bulb; in addition to this, a .25A circuit breaker switch (which serves as a permanent recording device) has been added to signal the user that a successful calibration is complete. Note that the circuit breaker takes approximately 60 seconds to trip once a detection is made.

When deploying the SAPARC, the user must be certain that feedback oscillations will not occur during the calibration. Therefore, one must always monitor the detection lamp during final setup preparations. (Recall that the SAPARC system is extremely sensitive to adjacent objects which may reside within the antenna's beamwidth. These objects include nearby bushes, tree limbs, etc.). If a feedback scenario is present, simply press the RESET to clear the Detection PWA circuitry. Continue to re-position the SAPARC as needed so that no errant detections are made.

2.5 Temperature Stabilization

During the initial design phase, one of the primary goals was to develop a system which was insensitive to changes in the ambient temperature. It was assumed that the most sensitive devices would be those which are active, namely the preamp and power amp. To this end, a 24W hybrid heater had been placed on the amplifier combination. Unfortunately, the temperature stabilization tests showed that the most sensitive device was the passive delay line, and not the amplifiers as first suspected (Refer the test results reported in the report for C-band SAPARC [6])

Temperature stabilization would require either a number of high power heaters or a variable attenuator / gain feedback circuit. The former of these alternatives is somewhat impractical since it would require excessive amounts of battery power. Similarly, the latter option is too expensive for a practical implementation.

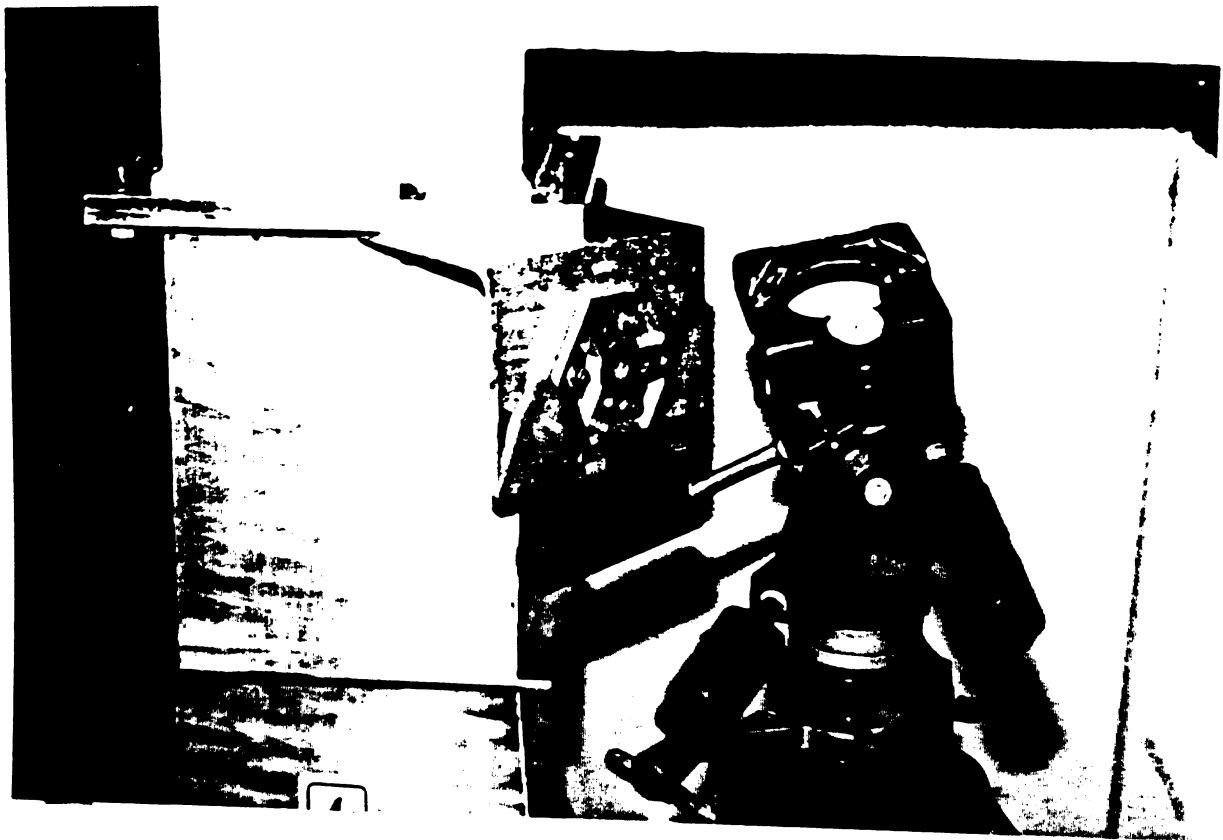
An acceptable solution requires a mapping of the G_{Loop} component of the RCS as a function of temperature. Such a mapping is shown in Section 3.3. The goal, then, is to accurately record the system's temperature during an actual field test. The temperature (recorded as a function of time) will then be compared to the G_{Loop} vs. Temperature chart from Section 3.3.

Hence, an accurate description of the system's total RCS can be calculated for the exact fly-by time of the SAR platform.

An automatic measurement is obtained through the use of a Dickson 24-hour Temperature Recorder. This device is nestled within the delay line loop located at the base of the SAPARC chassis. For an actual field deployment scenario, the user must activate the temperature recorder while noting the exact time of initial operation. Once this is done, the user is free to leave the deployment area while the rest of the equipment remains in its automated mode.

2.6 Assembled Prototype

Figures 2.17a and b show how to attach the OMT unit to a tripod. Figures 2.18 a and b show the SAPARC in its completed state for 0° and 45° orientations, respectively. Note how the horn antenna is detachable for quick and easy transport of the device.



**Figure 2.17a: Disassembled L-band Antenna Unit
and Support**

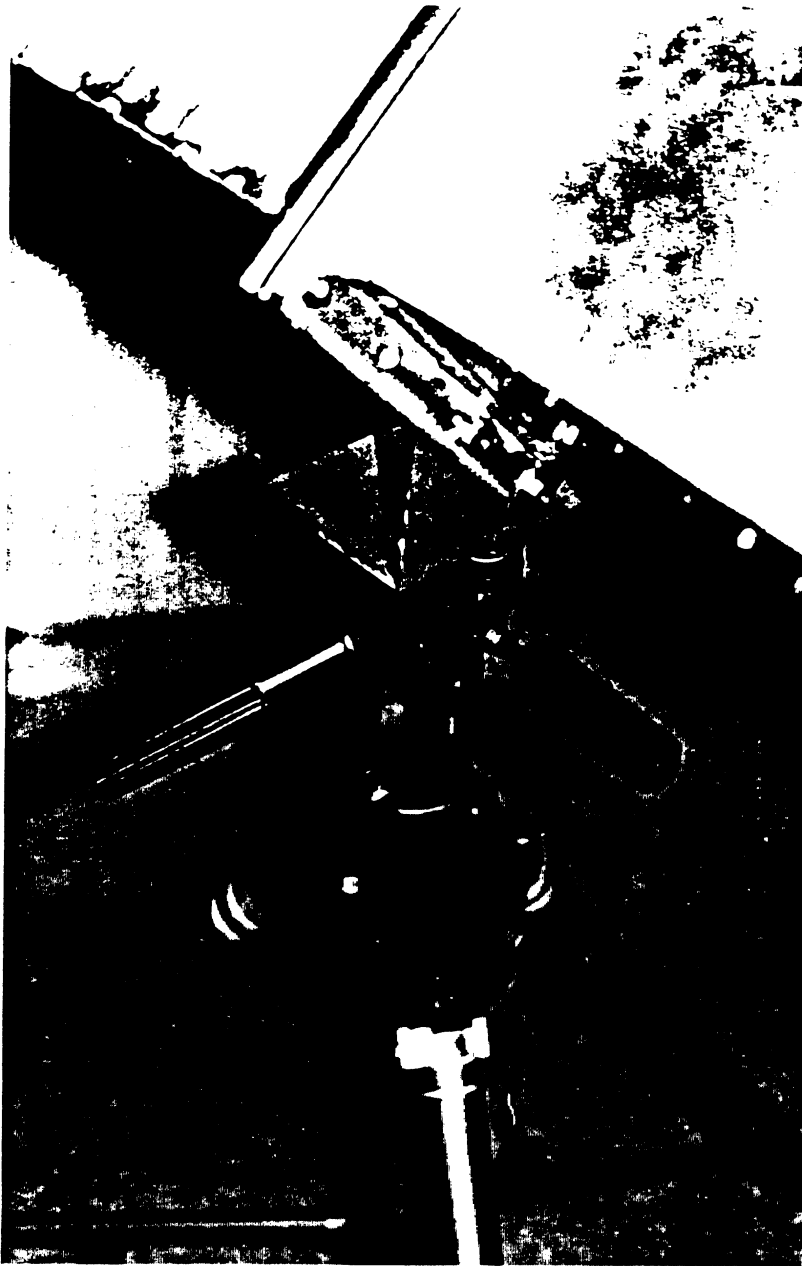
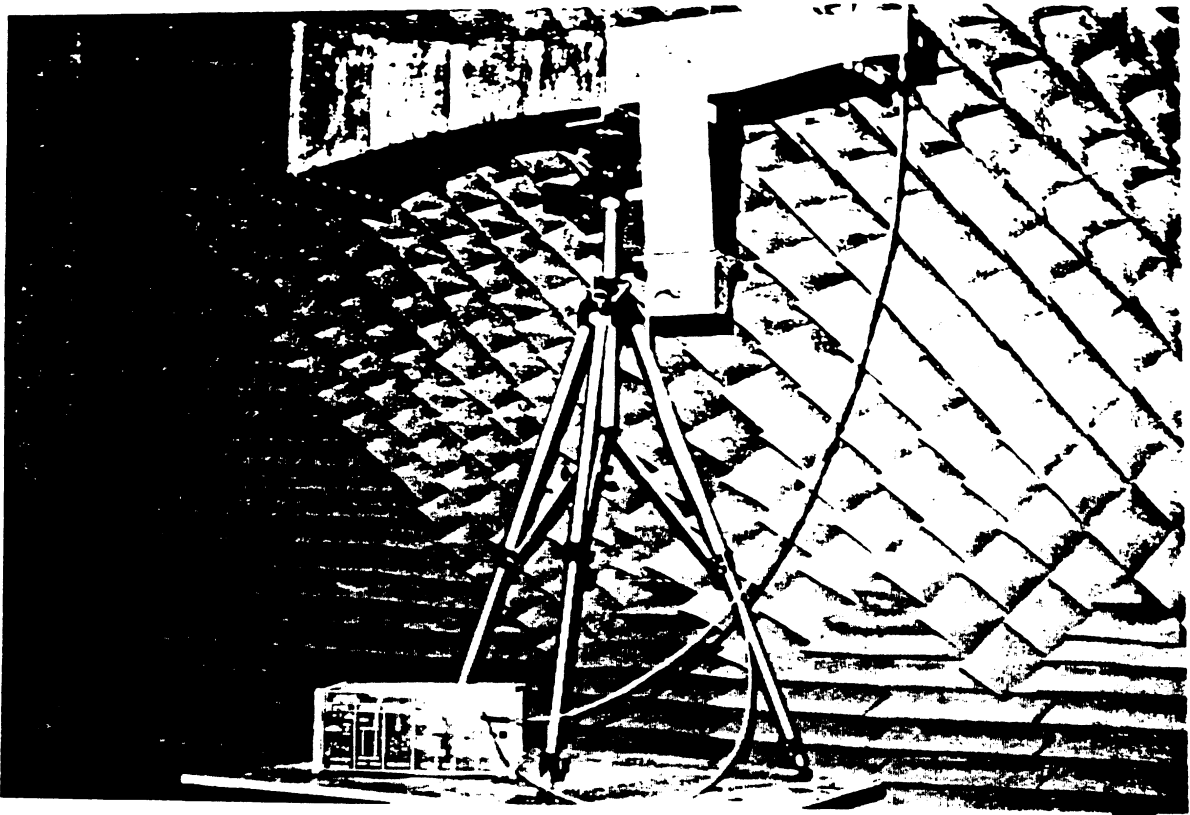
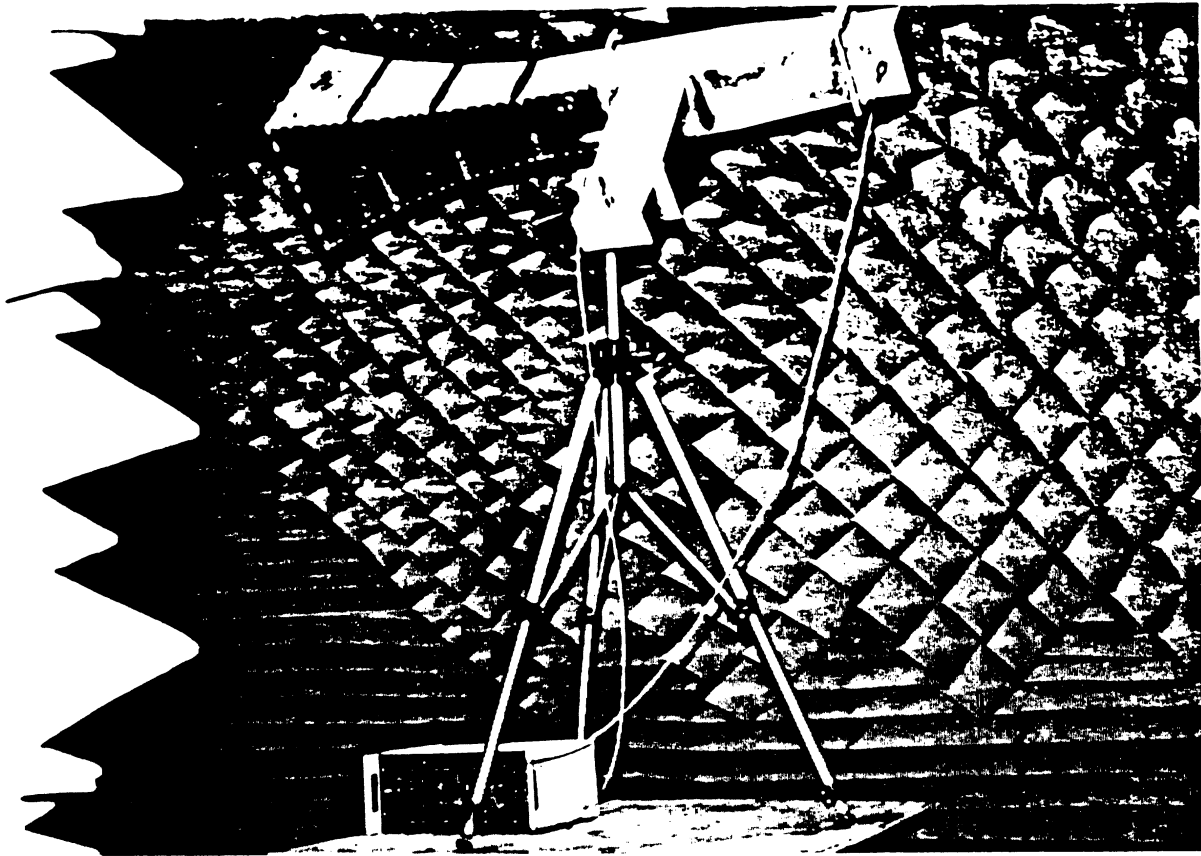


Figure 2.17b: Assembled L-band Antenna Unit and Support



**Figure 2.18a: Fully Assembled L-band SAPARC for
the 0° Antenna Orientation**



**Figure 2.18b: Fully Assembled L-band SAPARC for
the 45° Antenna Orientation**

CHAPTER III

EXPERIMENTAL RESULTS

As mentioned in Chapter 1, the accuracy of a SAR calibration is highly dependent upon the measured performance of the calibration device. Hence, the measurements taken in accordance with this project must adhere to the following goals:

- Accurate measurement of the scattering matrix for the 0° and 45° antenna orientations.
- 0.2 dB accuracy in the mapping of the thermal gain variations.
- Overall characterization of SAPARC performance with respect to field deployment conditions, including extremes in temperature, all-weather performance, and battery capacity.

3.1 G_{Loop} Measurements

Figure 3.1 depicts the S_{21} frequency responses of G_{Loop} for room temperature operation (24°C). For this measurement, a 40 dB attenuator was placed on the receive channel of the SAPARC in order to prevent amplifier saturation. From these measurements, G_{Loop} is found to be 43.14 dB at 1.25 GHz. However, as section 3.3 will show, G_{Loop} is highly dependent upon the SAPARC's operating temperature. To find the correct value of G_{Loop} for each SAR calibration, one must refer to the thermal variation chart shown in Figure 3.12.

The SAPARC anechoic chamber tests were performed at room temperature

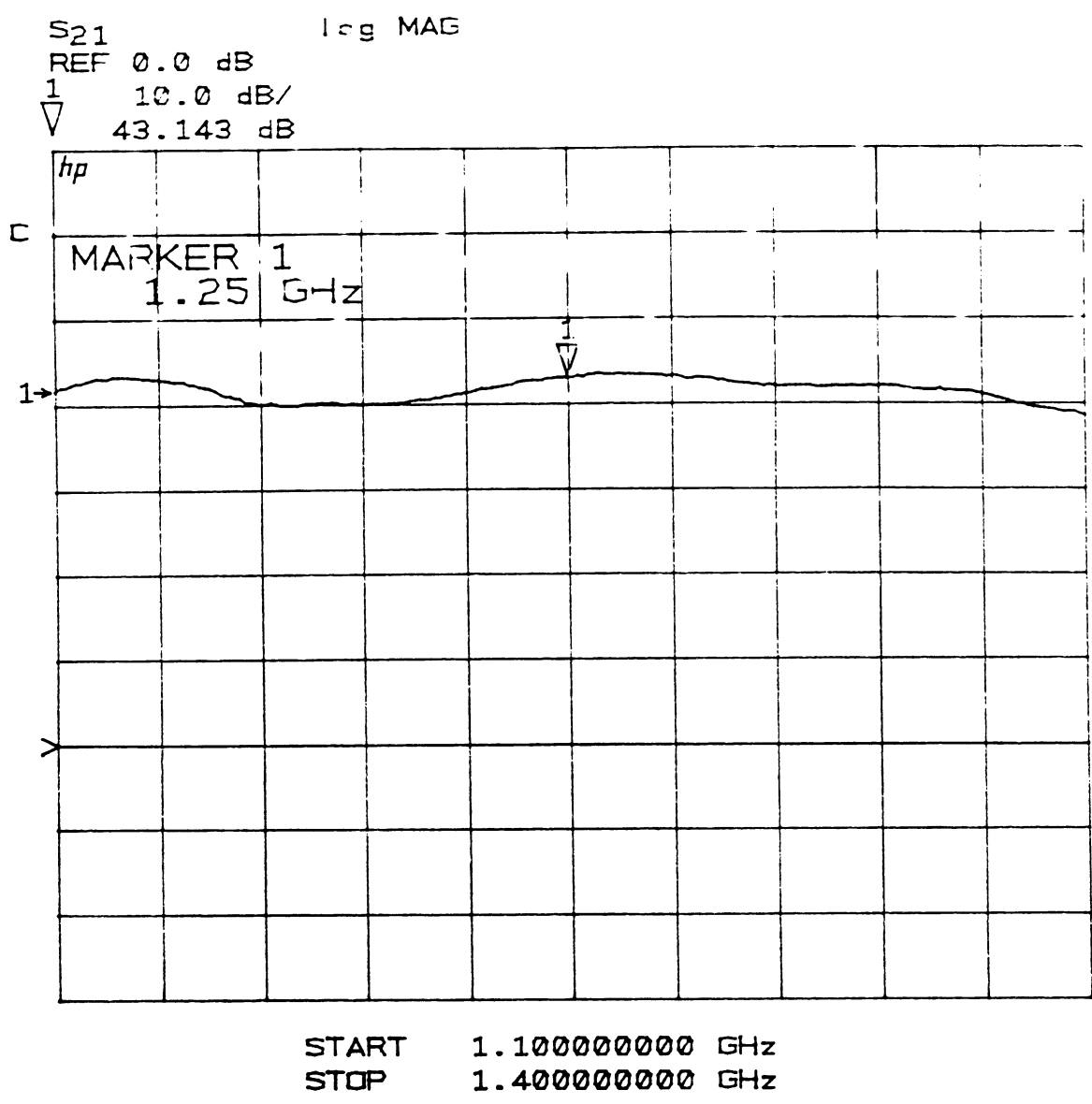


Figure 3.1: Frequency Domain Response of G_{Loop} at $24^{\circ}C$

(approximately 20° C). Figure 3.6 (SAPARC RCS for the 0° Orientation) shows that the maximum achievable value for the RCS is 42.6 dBsm. Using this data in conjunction with the theoretical equation given in section 2.1, the gain of the L-band antenna system is found to be 11.5dB. The following calculations demonstrate this result.

$$\sigma = G_{Loop} \frac{G_T G_R \lambda^2}{4\pi} L_{cable}$$

where

$$L_{cable} = -1.8dB$$

$$\sigma \approx 42.6dBsm$$

$$G_{Loop} = 44.8dB$$

$$G_T = G_R = G_{Antenna}$$

$$\frac{\lambda^2}{4\pi} = \frac{(0.24m)^2}{4\pi} = -23.4dB$$

Rearranging the equation gives

$$G_{Antenna} = \sqrt{\frac{\sigma}{G_{Loop} \frac{\lambda^2}{4\pi} L_{cable}}} = \frac{1}{2}(42.6dBsm - 44.8 + 1.8dB + 23.4dB)$$

$$G_{Antenna} = 11.5dB$$

The equations above demonstrate how the user can easily find the RCS of the SAPARC for any given operating temperature. In other words, when the operating temperature is known, the corresponding value of G_{Loop} will also be known, and hence so will the RCS of the SAPARC unit. The equations are similarly applicable to the 45° SAPARC orientation. For this case, simply subtract the 6 dB difference from the 0° orientation antenna results described above.

3.2 Anechoic Chamber Tests

The University of Michigan Radiation Laboratory maintains a fully equipped 60-foot-

long, tapered anechoic chamber which is used for conducting antenna pattern measurements and for measuring the scattering characteristics of man-made and natural targets. This chamber is ideal for making accurate measurements of the SAPARC's RCS within a relatively noise-free environment.

A major component of the Radiation Laboratory's polarimetric radar measurement facility is the LCX POLARSCAT system. The parameters of the L-band subsystem used for this measurement are as follows:

Center Frequency	1.25 GHz
Frequency Bandwidth	0.3 GHz
Antenna Type	Dual Polarized Pyramidal Horn
Antenna Gain	15 dB
Beamwidth	17.0°
Far Field ($2d^2 / \lambda$)	2.6 m
XPOL Isolation	35 dB
Calibration Accuracy	± 0.3 dB
Phase Accuracy	$\pm 3^\circ$

Table 3.1: L-Band Measurement System Parameters

A large percentage of this system consists of Hewlett Packard components, including an HP 8753 Network Analyzer and HP 9000 Computer with an additional disc drive. Using computer control, polarimetric measurements of the phase and magnitude responses can be taken with respect to changes in target elevation and azimuth angles (Figure 3.2).

The chamber experiments required a center frequency of 1.25 GHz with a 300 MHz bandwidth. Calibrations were performed by using a 14" metallic sphere in accordance with a calibration technique developed by Sarabandi [5] (See Appendix D). Time gating was also employed, whereby a gate span of 10 ns (centered on the target's response) provides an automatic subtraction of background scatterers. A block diagram of the measuring facility is given in Figure 3.3.

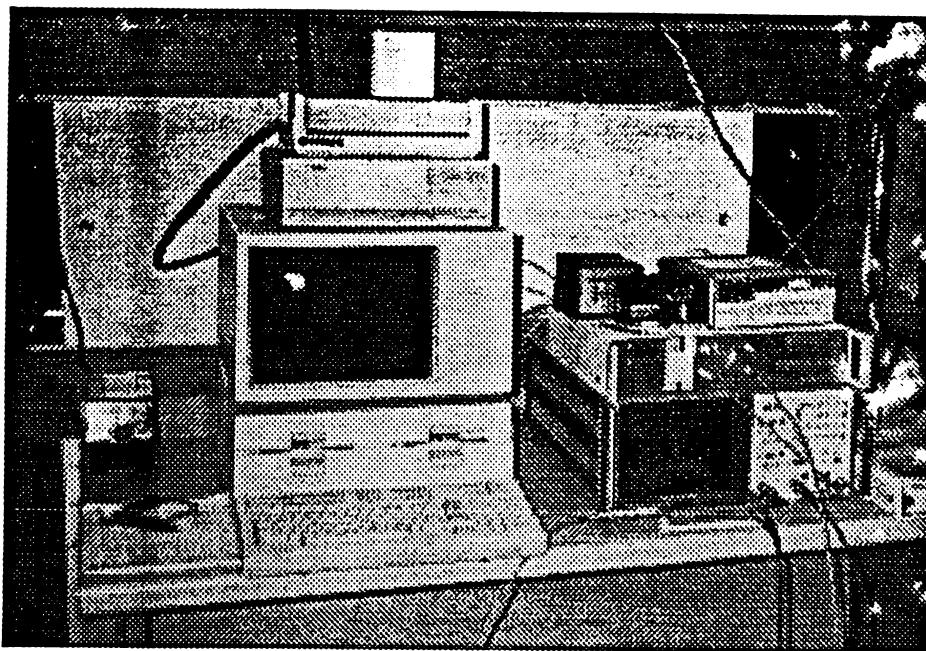


Figure 3.2: L/C/X-Band POLARSCAT Test Equipment

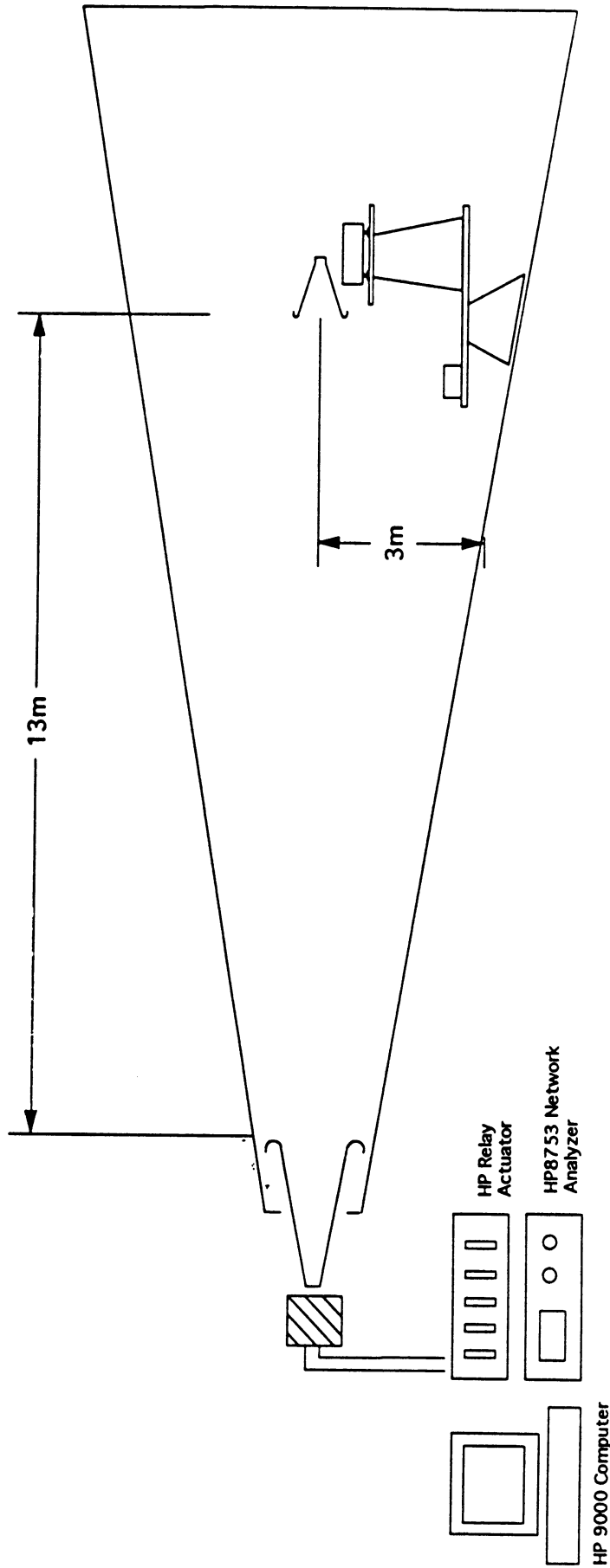


Figure 3.3: Anechoic Chamber Measurements at the University of Michigan's Radiation Laboratory

3.1.1 SAPARC Time Domain Response

Section 2.3 mentioned that a SAR calibration can be enhanced by time shifting the PARC's radar response so that it appears to originate over a dark background (refer to Figure 2.8). Recall that a 200 foot delay line is incorporated into the SAPARC design to accomplish such a feat. The effect of this delay is clearly shown in Figure 3.4, the time domain response of the L-band SAPARC system. As an addendum, Table 3.2 provides an identification of the five markers given in Figure 3.4.

<u>Marker</u>	<u>Identification</u>
1	Leakage from a circulator of the radar system
2	Leakage from the OMT and antenna unit of the radar system
3	Backscatter from the SAPARC's antenna and chassis (physical location of the SAPARC)
4	Primary time-delayed SAPARC response
5	Response due to the <i>ringing</i> of the SAPARC unit

Table 3.2: Marker Identification for Figure 3.4

Table 3.2 leads to a number of important conclusions. First, the electrical length of the delay line is found to be the difference between markers 3 and 4, namely 340 ns. This, in turn, corresponds to an electrical length of 102 m; hence, the SAPARC's SAR response has effectively been translated by 102 m (i.e. approximately 340 feet). Also note the ringing effect (marker 5) where a replica of the original SAR response is periodically repeated every 340 ns, or 102 m. The subsequent replicas are a product of the limited isolation of the OMT. During the transmission of the first SAR response, a small amount of leakage RF makes its way through the SAPARC loop where it is amplified, delayed, and re-transmitted as another SAR response. Figure 3.4 shows how each of the recurring responses will decay by approximately 15 dB; hence, this process continues until the net amount of leakage becomes negligible. When processing the imaging data, the ringing effect inherent with each SAPARC allows for easy identification and location of the calibration system, thus providing another advantage over passive calibration devices.

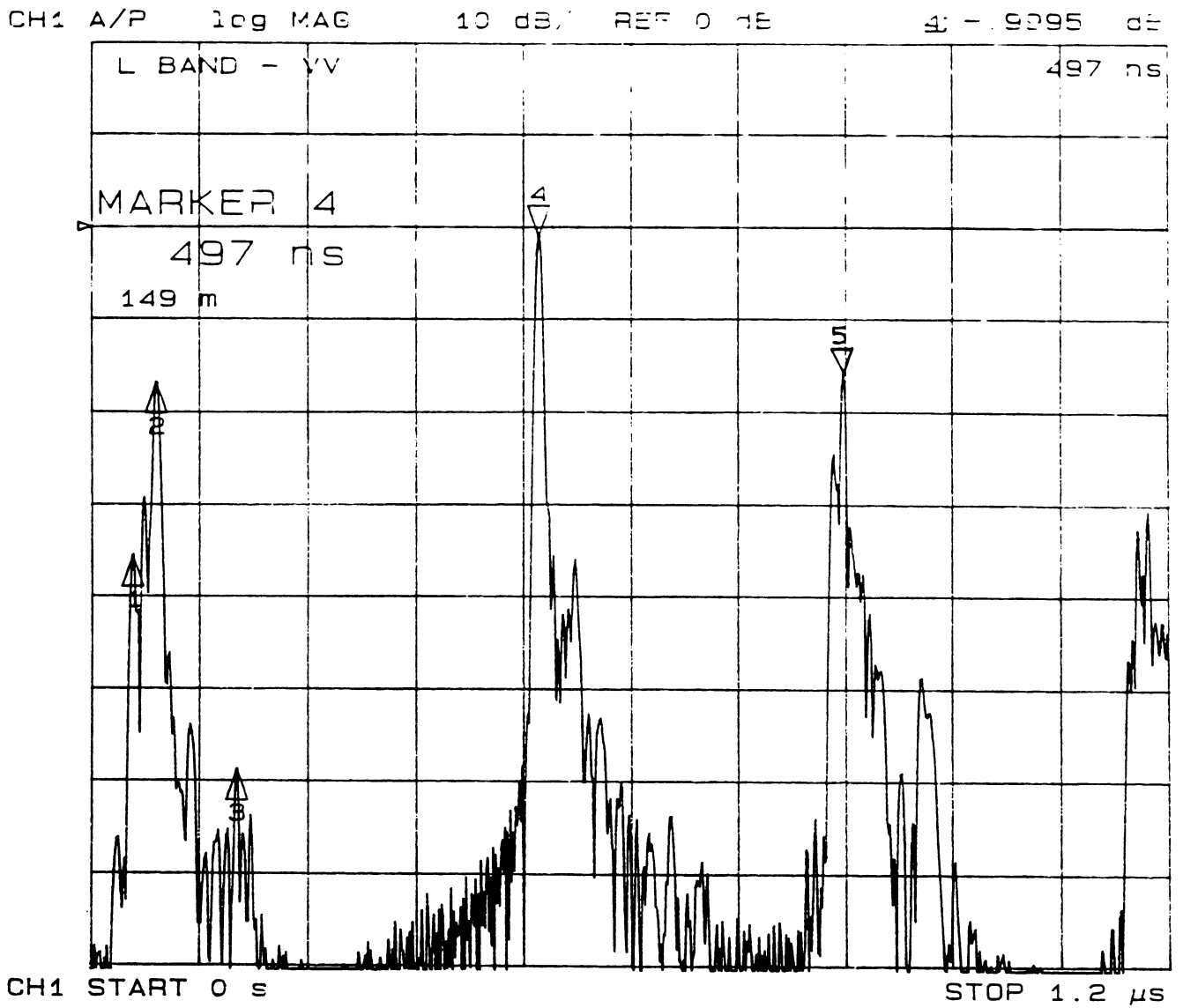


Figure 3.4: SAPARC Time Domain Response

As a final point, the SAPARC provides an exceptional signal to noise ratio (SNR). The difference between the SAR response (labeled as marker 4) and the anechoic chamber's noise floor is over 75 dB. A 55 dB signal to clutter ratio (i.e. the difference between markers 3 and 4) is also shown to be quite extraordinary. These relatively large values of SNR will prove to be very beneficial for actual SAR calibrations.

3.1.2 0° Orientation Test

The 0° orientation of a SAPARC refers to the case when there is no polarization mismatch between the radar's antenna and the SAPARC antenna. In this mode, the SAPARC provides a calibration of σ_{hv} , where a received vertically polarized signal is amplified, delayed, and transmitted back to the radar with a horizontal polarization. The phasor polarizations are given in Figure 3.5.

Figure 3.6 demonstrates the measured azimuthal pattern response for this orientation. As shown, the SAPARC yields a maximum RCS response of 42.6 dBsm with a 25° half-power beamwidth (for the σ_{hv} case). (Note that the traditional convention of listing the target's polarimetric RCS as σ_{xy} , where x and y refer to the received and transmitted polarizations, respectively, is used.) A cross polarization isolation of 32 dB exists between σ_{hv} and σ_{vv} , σ_{hh} , thereby giving credence to the excellent cross polarization isolation performance of the horn / OMT design described in section 2.2.

As a final point, the σ_{vh} response reveals the "noise floor" inherent with this measurement. This RCS response is characterized by a 100% polarization mismatch for both the radar and SAPARC antennas, and hence the extremely low RCS response of -40 to -60 dBsm is expected.

3.1.3 45° Orientation Test

The 45° orientation is accomplished by rotating the SAPARC horn as demonstrated in Figure 3.7. Doing so allows a complete calibration of the Scattering Matrix since each transmit and receive combination, namely σ_{vv} , σ_{hh} , σ_{hv} , and σ_{vh} , yields the same RCS azimuthal pattern response with a half-power beamwidth of 25°. Figure 3.8 depicts

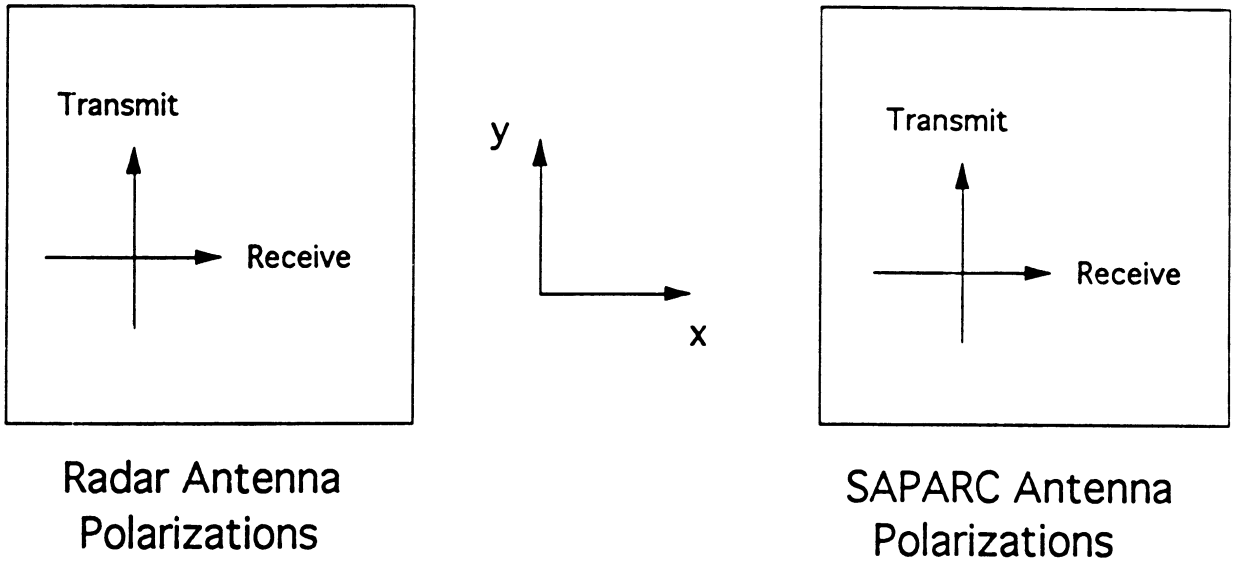


Figure 3.5: SAPARC 0° Orientation Phasor Polarizations

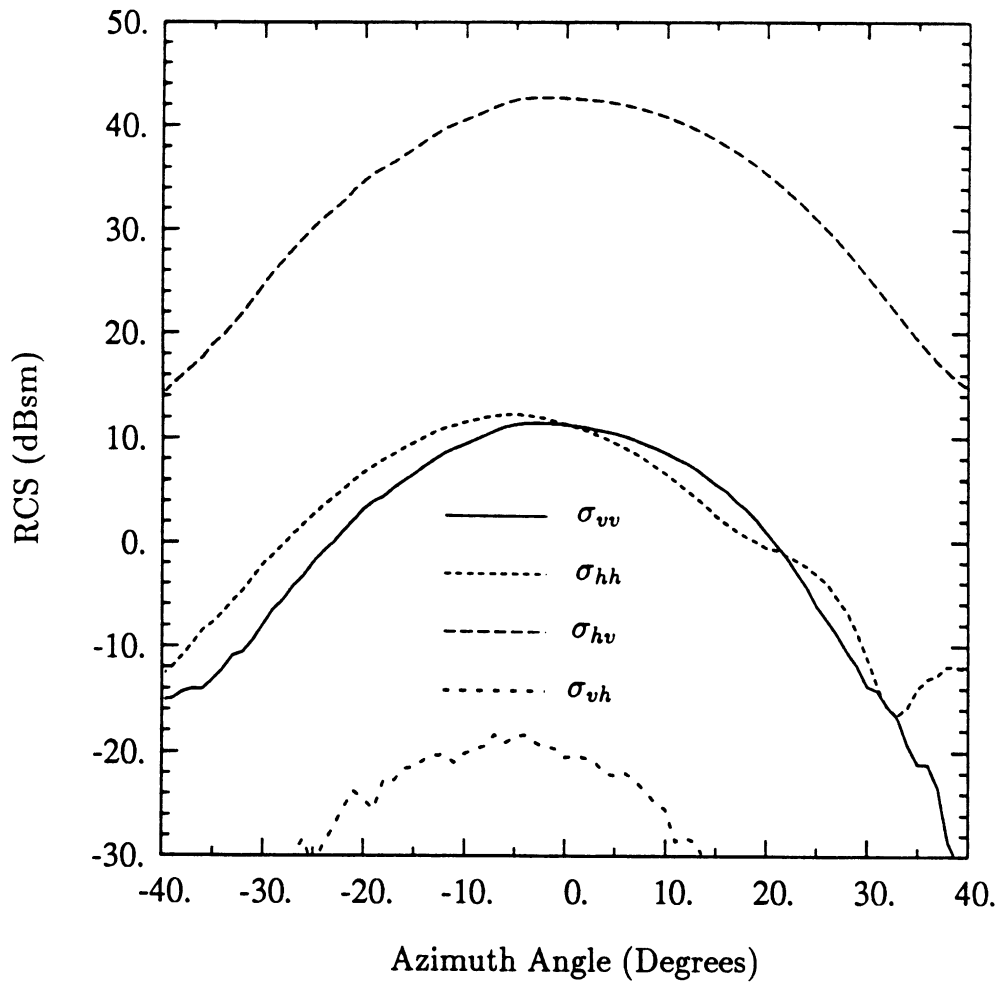
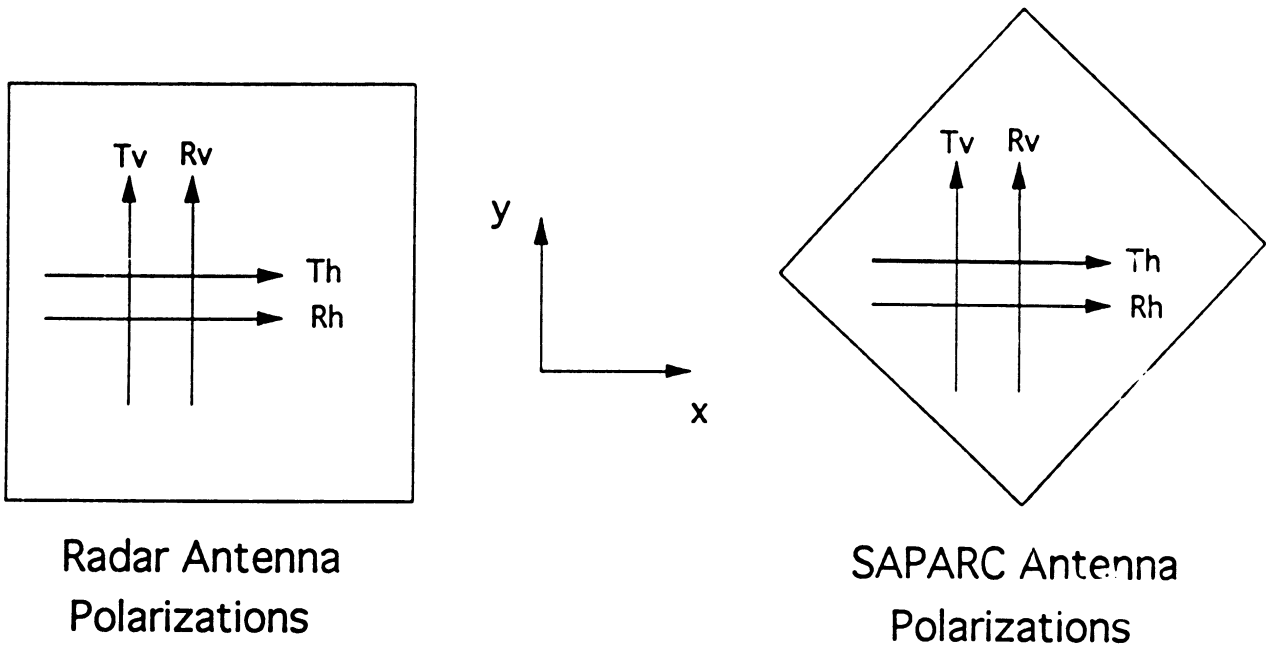


Figure 3.6: SAPARC 0° Orientation RCS Azimuthal Patterns at 20°C (SIR-C Mode)



Radar Antenna
Polarizations

SAPARC Antenna
Polarizations

- T_v : Transmit Vertically Polarized Wave Component**
- R_v : Receive Vertically Polarized Wave Component**
- T_h : Transmit Horizontally Polarized Wave Component**
- R_h : Receive Horizontally Polarized Wave Component**

Figure 3.7: SAPARC 45° Orientation Phasor Polarizations

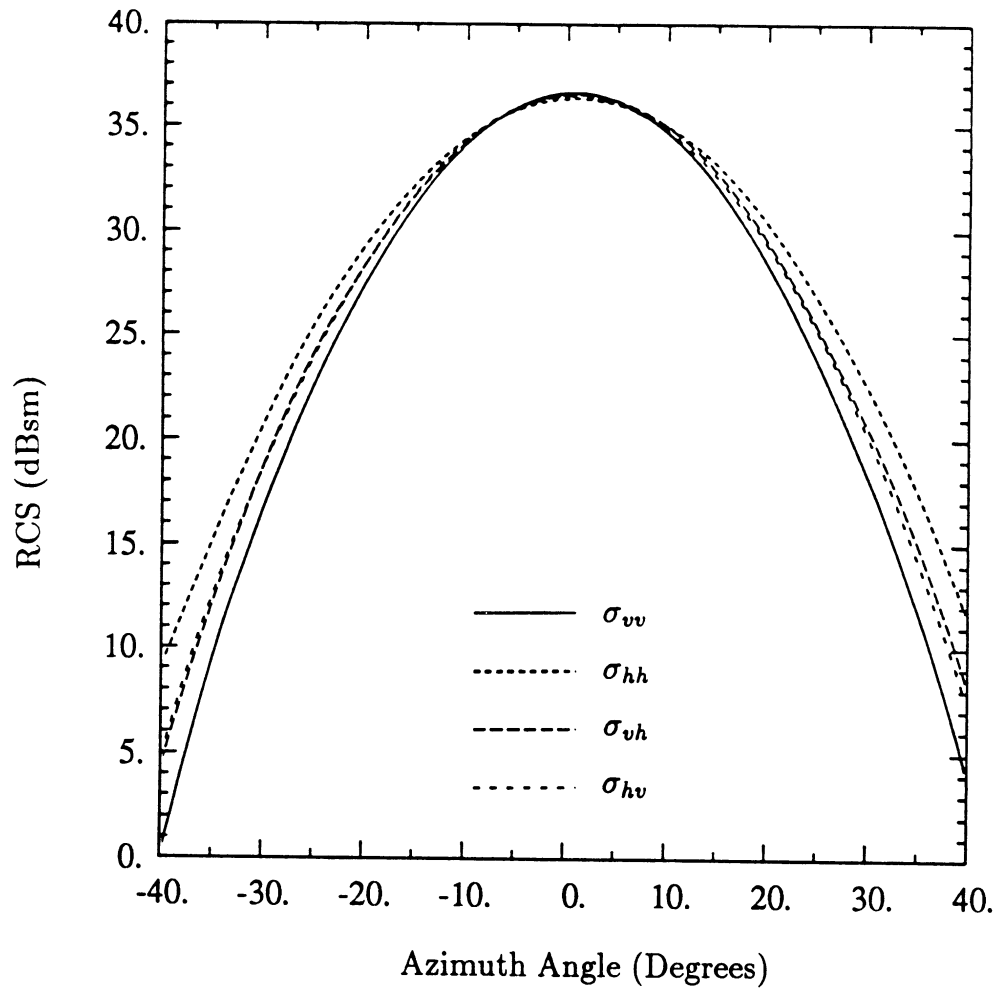


Figure 3.8: SAPARC 45° Orientation RCS Azimuthal Patterns at 20°C (SIR-C Mode)

the RCS azimuthal pattern response for the 45° orientation. Note how each trace is symmetric and virtually equal over a 40° beamwidth, as expected. Also note how the peak RCS of 36.6 dBsm is exactly 6 dB below the 0° orientation response of 42.6 dBsm. Again, this result is in excellent agreement with the theoretical expectations (the two 45° polarization mismatches, one for transmit and the second for receive, correspond to a total loss in power of $1/2 \cdot 1/2 = 1/4 = 6$ dB).

The phase responses shown in Figure 3.9 are also noteworthy. Theoretically, we expect

$$\phi_{hv} - \phi_{vv} = 0^\circ$$

$$\phi_{hh} - \phi_{vv} = \phi_{vh} - \phi_{vv} = 180^\circ$$

over an 80° beamwidth. The phase diagrams in Figure 3.10 help to explain these results.

Section 2.2 referred to the drawbacks encountered when using a two-antenna PARC system; more specifically, these problems include pattern asymmetry and ripples in the phase and magnitude responses. Figure 2.3 is an example of one two-antenna system tested by Sarabandi and Oh [1]. By comparing Figure 2.3 with those in Figures 3.6, 3.8, and 3.9, one can easily see the notable SAPARC improvements in magnitude and phase performance.

3.3 Thermal Gain Testing

Section 2.5 alluded to the fact that PARC's are susceptible to gain variations due to changes in the ambient temperature. Countering these thermal gain variations is formidable task; therefore, it is much easier to compensate for the changes in the SAPARC's RCS by mapping the G_{Loop} dependency on ambient temperature.

Figure 3.11 reflects the results of the experiment whereby G_{Loop} is plotted over a temperature range of -10°C to 40°C.

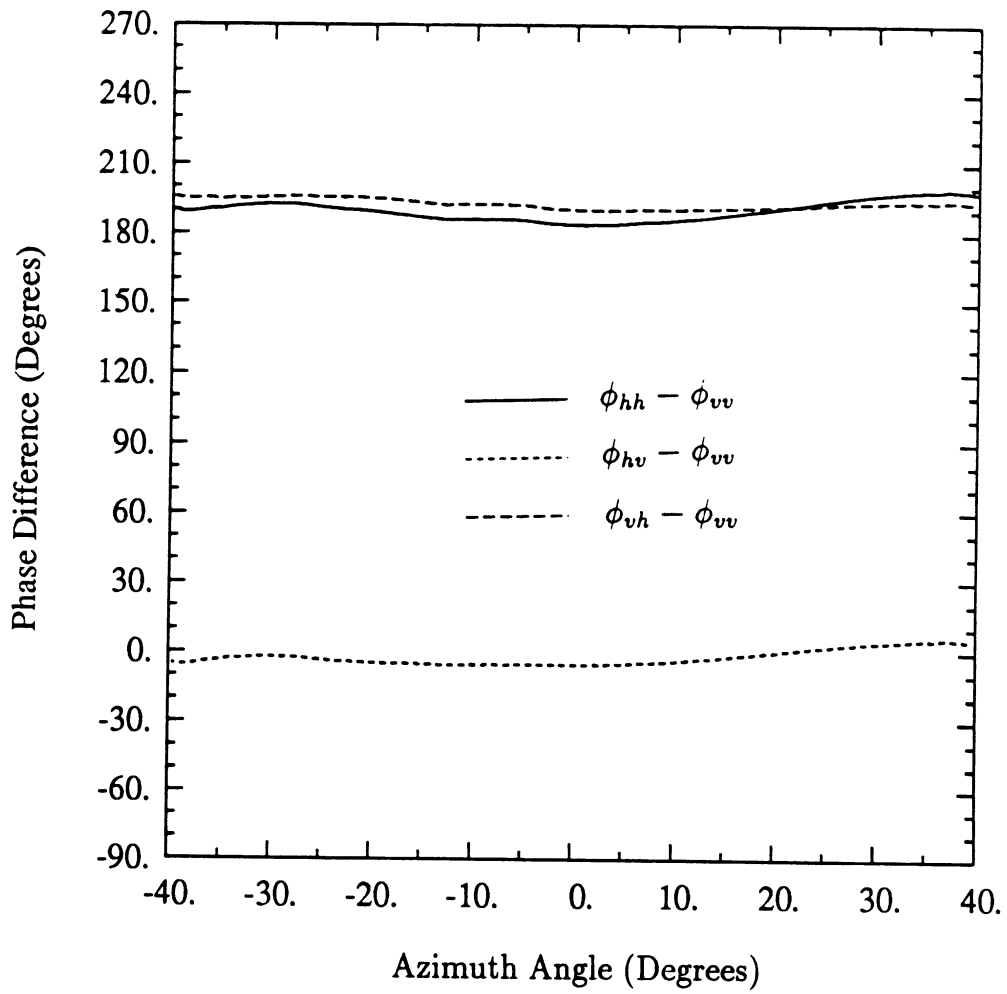


Figure 3.9: SAPARC 45° Orientation Phase Patterns at 20°C (SIR-C Mode)

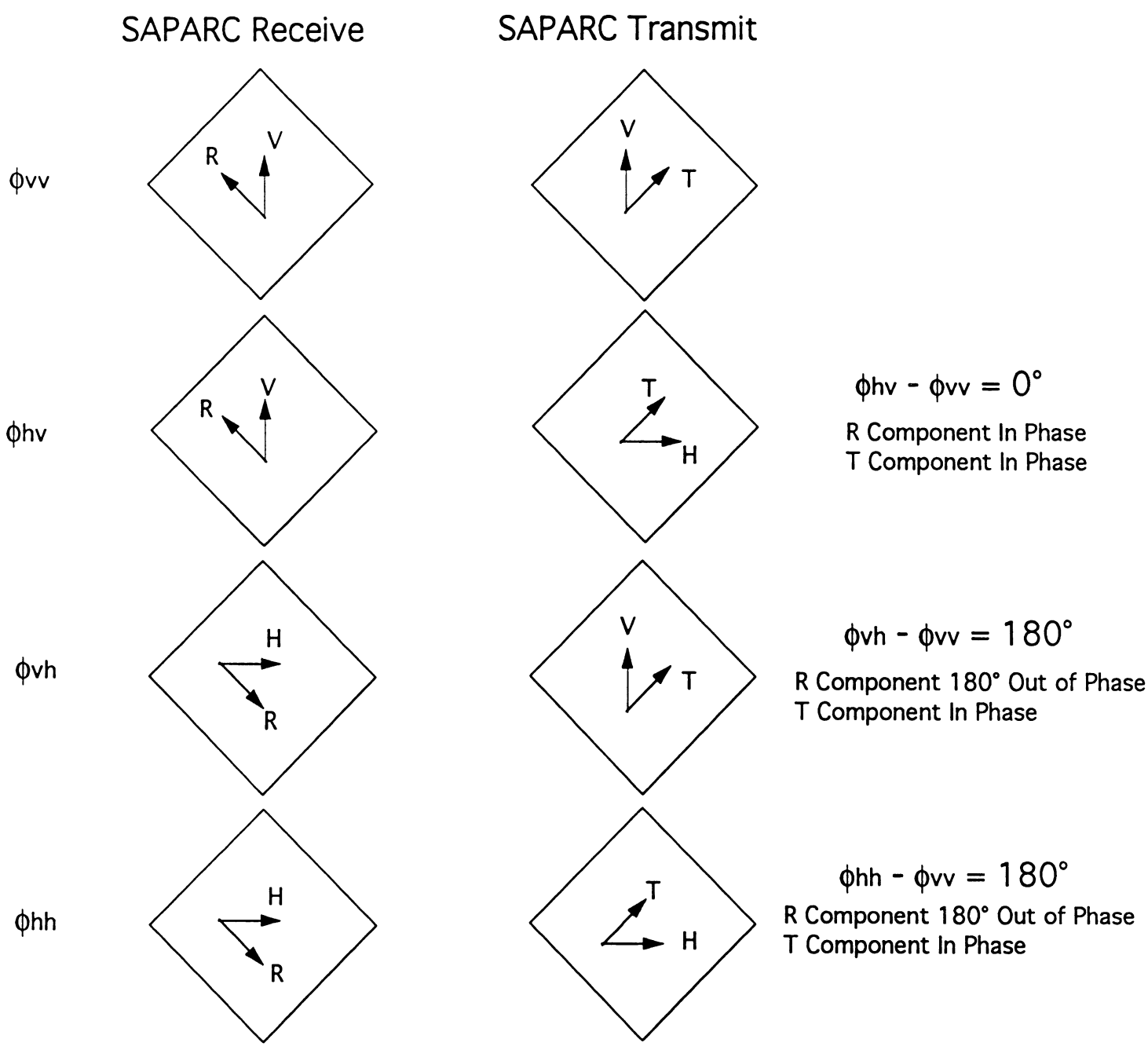
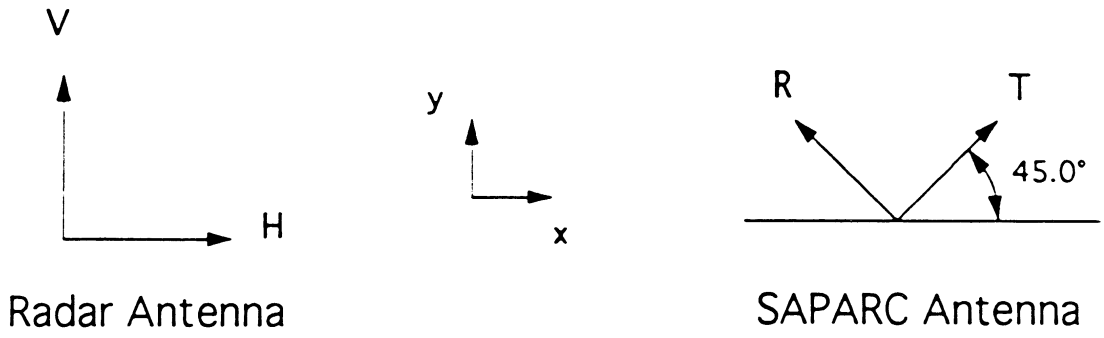


Figure 3.10: Phasor Diagram for the 45° Orientation

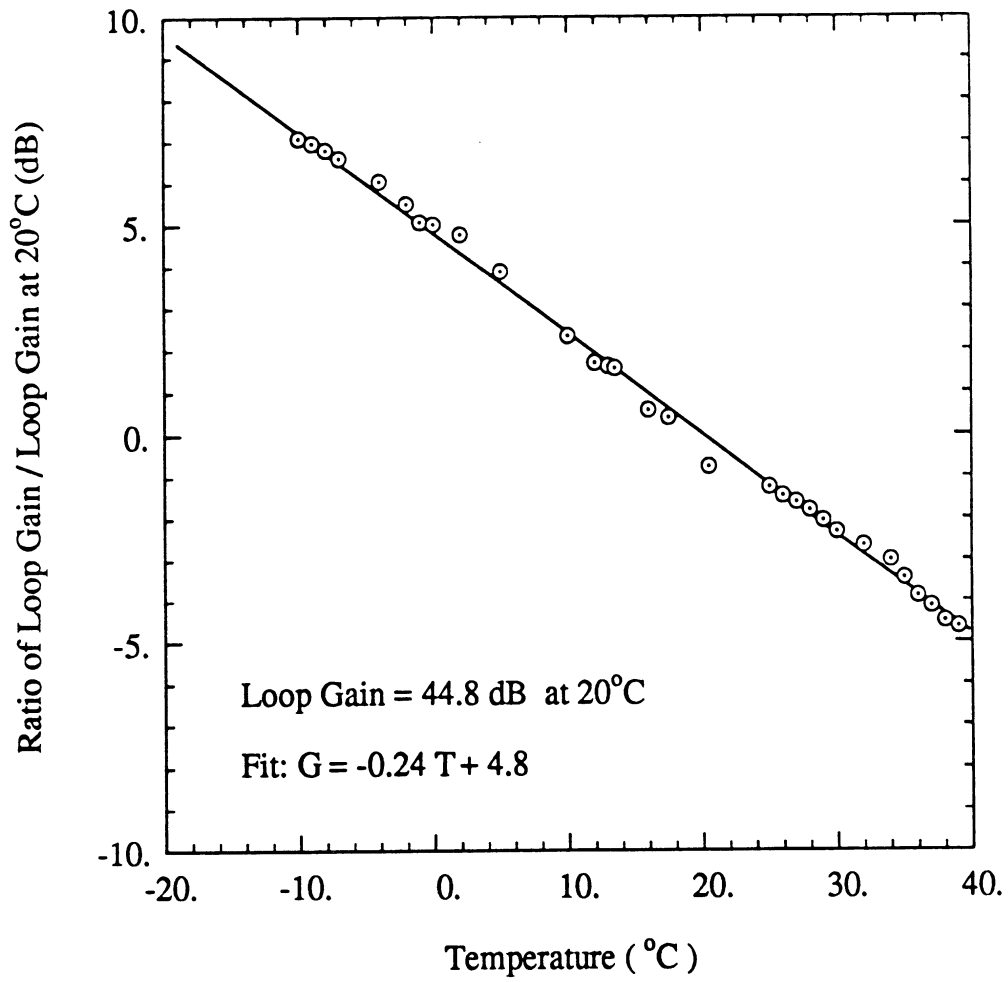


Figure 3.11: L-band SAPARC Thermal Gain Variations

The user of the device must remember, however, that component aging may alter the overall performance of G_{Loop} . Therefore, periodic calibrations of G_{Loop} vs. temperature is recommended.

As a final note, special precautions must be taken when operating the SAPARC in cold weather scenarios. Currently, the system is configured to provide the maximum allowable RCS for temperatures of 20°C or greater (see section 2.3.3). However, Figure 3.11 clearly shows how G_{Loop} can increase by as much as 7 dB for temperatures below 20°C. Therefore, the user is encouraged to add a 10 dB attenuator between microwave switches (see Fig. 2.2) whenever cold operating temperatures are anticipated.

3.4 Field Deployment Conditions

3.4.1 Battery Capacity

The SAPARC units developed through this project require two 12V, 7 Amp•H lead acid batteries. The power demands on Supply 2 (see Appendix C, pg. C-1) is given as follows:

<u>SAPARC Operating Condition</u>	<u>Current Draw</u>	<u>Power Demand</u>
Timing Circuitry On	0.37 A	4.44 W
System Active	1.09 A	13.08 W
System Active with LED Display On	1.20 A	14.40 W

Table 3.3: Power Demands on Supply 2

Figure 3.12 (1 A case) depicts the capacity performance of the Yuasa 12V battery used in the SAPARC design. Figure 3.13 shows the results for the full load case (i.e. a current draw of 1.2 A). Under full load conditions, the SAPARC can operate (at temperatures above 20°C) for up to 5.5 hours; longer operating times are achievable when using the Activation Timers.

Figure 3.14 shows the marked decrease in capacity during cold weather operation. During this test, the Yuasa 12V battery was subjected to a temperature of -10°C while providing a current of 1.2 amps. Under these conditions, the SAPARC's full load operating time is reduced by one hour; therefore, the user must take special precautions when planning to operate the SAPARC in cold climates.

3.4.2 All-Weather Performance

Ideally, the SAPARC can be used in all types of weather; of course, there are a number of practical limitations which concern the aperture on the horn antenna. Obviously, rain and snow can accumulate inside the horn / OMT, and thus the calibration would be ruined. In order to compensate for this occurrence, a polyethylene film (e.g. Saran Wrap) was placed over the aperture to serve as a radome. This film was very effective in keeping water out of the horn / OMT combination; however, an accumulation of water droplets on the radome eventually lead to a feedback oscillation scenario (see Sections 2.3.2.2 and 2.4.2). Therefore, applying a thin-filmed polyethylene radome is suggested for weatherproofing the horn, OMT, and waveguide adapters. Yet, do not expect the SAPARC to operate correctly in adverse weather conditions.

As a sidenote, if the rainfall ceases and the radome is allowed to dry, the SAPARC will "break-out" of its oscillation mode and return to its normal operating condition. The only notable change is that the detection circuitry will be triggered prematurely. Finally, the chassis of the SAPARC unit should be shrouded with a rain tarp to prevent excess exposure to the elements.

Capacity Test: Yuasa 7.0 AH

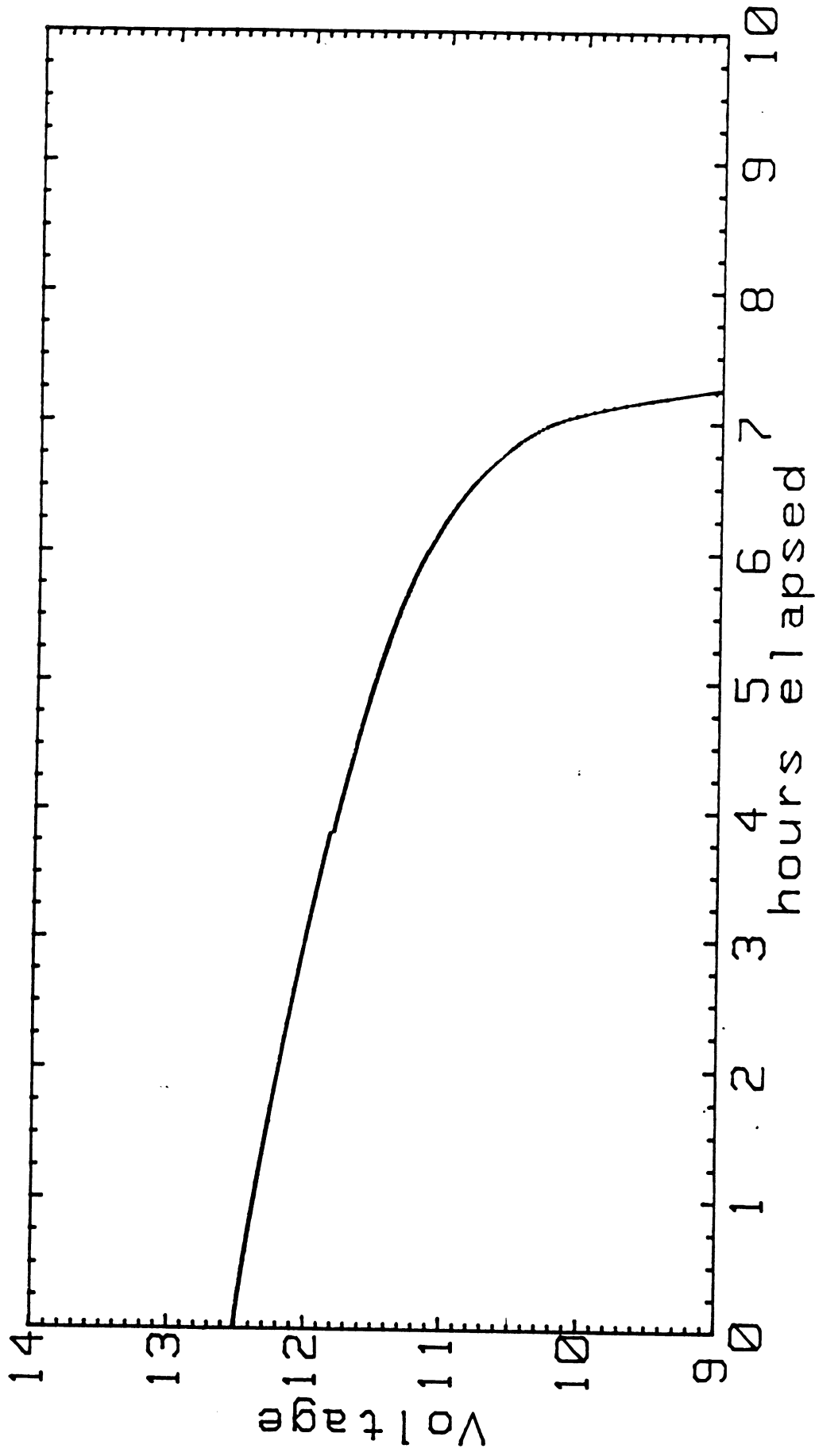


Figure 3.12: Battery Capacity Test (1.0A Load, 22°C)

Capacity Test: Yuasa 7.0 AH

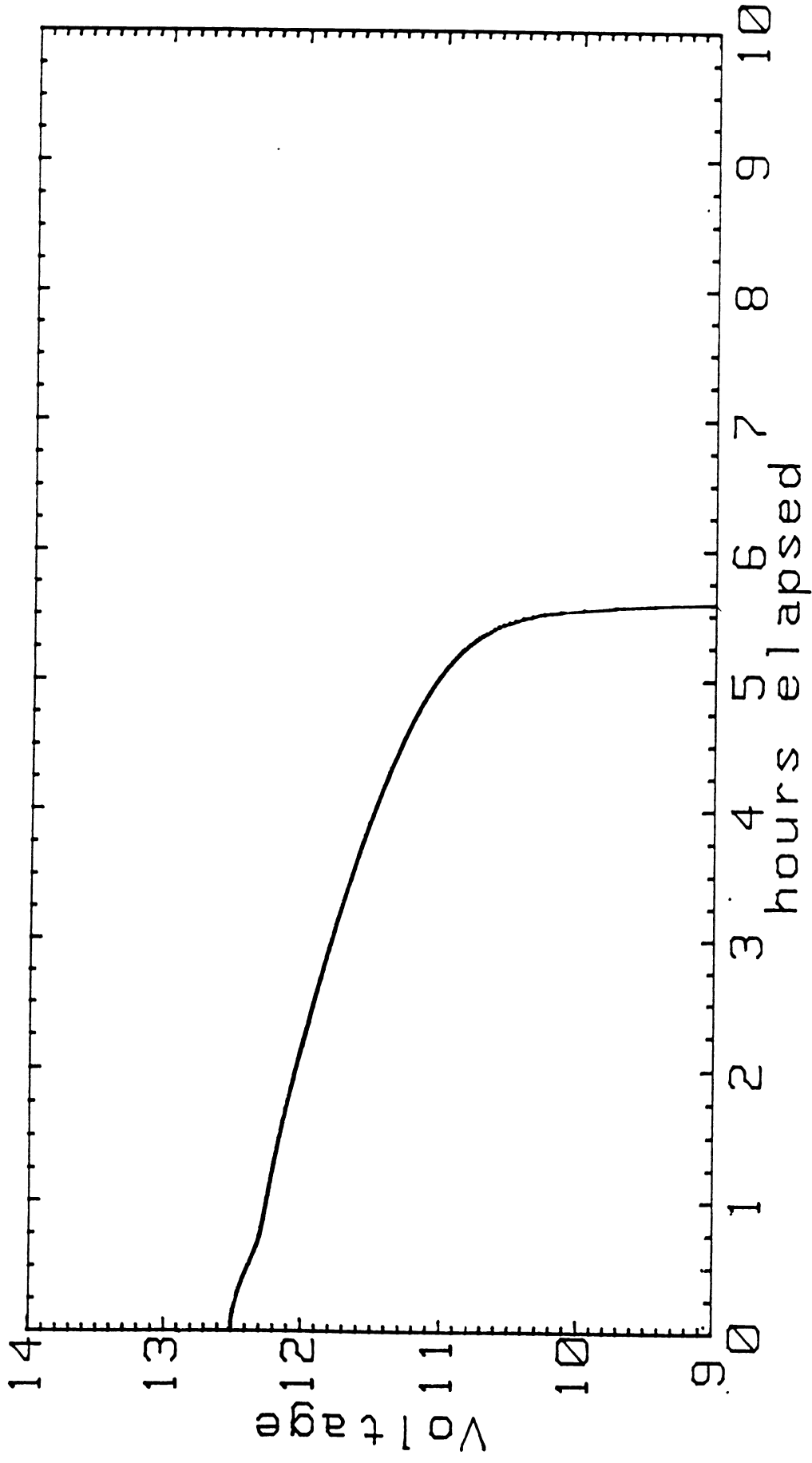


Figure 3.13: Battery Capacity Test (1.2A Load, 22°C)

Capacity Test: Yuasa 7.0 AH

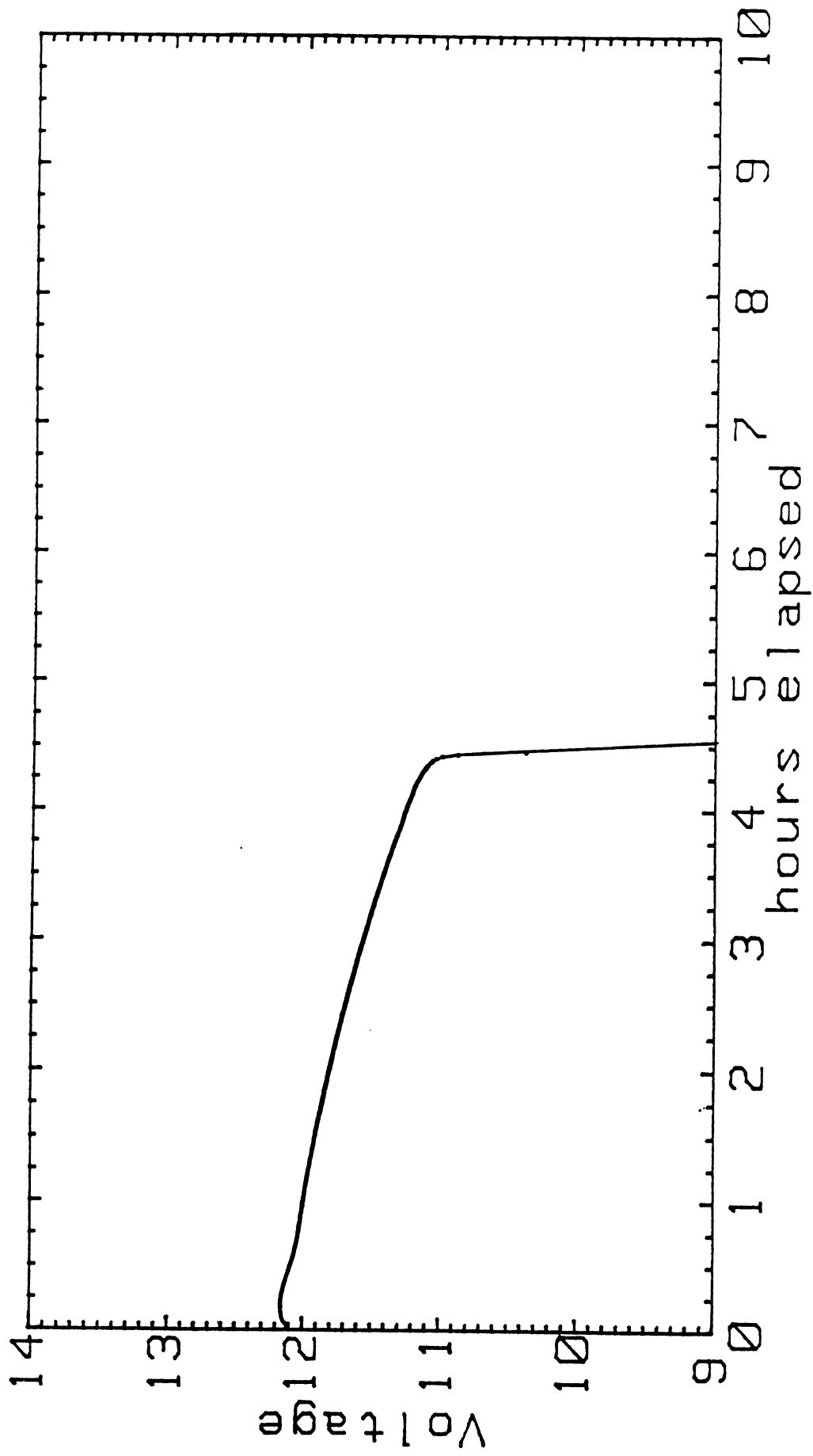


Figure 3.14: Battery Capacity Test (1.2A Load, -10°C)

CHAPTER IV

CONCLUDING REMARKS

The report outlines the design and performance characteristics of the first single antenna polarimetric active radar calibrator (SAPARC) prototype developed for NASA's SIR-C mission at the University of Michigan's Radiation Laboratory. In addition to this specific unit, a second L-band and two C-band versions are currently being constructed as part of a continuation of this project.

This L-band SAPARC possesses a nominal RCS of 36.6 dBsm with a 3 dB beamwidth of 25°. One of its best attributes, however, is the fact that it can outperform conventional PARCs through its implementation of a single dual-polarized antenna. More specifically, the pattern asymmetry and phase and magnitude ripples are eliminated through the use of this design.

In addition to these RF characteristics, the prototype is also noteworthy in that it provides a number of features which accommodate prolonged operation intervals and useful system status updates. In the future, subsequent modifications to this basic design will hopefully lead to more accurate and convenient calibrations of SAR platforms.

REFERENCES

- [1] Sarabandi, Kamal, and Yisok Oh "RCS Measurement of Polarimetric Active Radar Calibrators", *Radiation Laboratory Report No. 027165-1-T*, The University of Michigan, June 1990.
- [2] Sarabandi, Kamal, Yisok Oh, and Fawaaz T. Ulaby, "Performance Characterization of Polarimetric Active Radar Calibrators and a New Single Antenna Design", *IEEE Transactions on Antennas and Propagation*, Vol. 40, No. 10, October 1992.
- [3] Burnside, Walter D. "An Aperture-Matched Horn Design", *IEEE Transactions on Antennas and Propagation*, Vol. AP-30, No. 4, July 1982.
- [4] Balanis, Constantine A. *Antenna Theory: Analysis and Design*. New York: John Wiley and Sons, 1982.
- [5] Sarabandi, Kamal and Fawaaz T. Ulaby, "A Convenient Technique for Polarimetric Calibration of Radar Systems," *IEEE Transactions on Geoscience and Remote Sensing*, Vol. 28, pp. 1022-1033, 1990.
- [6] Ahne, James, Kamal Sarabandi, and Fawaaz T. Ulaby, "Design and Implementation of a C-band Single Antenna Polarimetric Active Radar Calibrator", *Radiation Laboratory Report No. 027587-1-T*, The University of Michigan, July 1993.

APPENDIX A

OMT SPECIFICATIONS

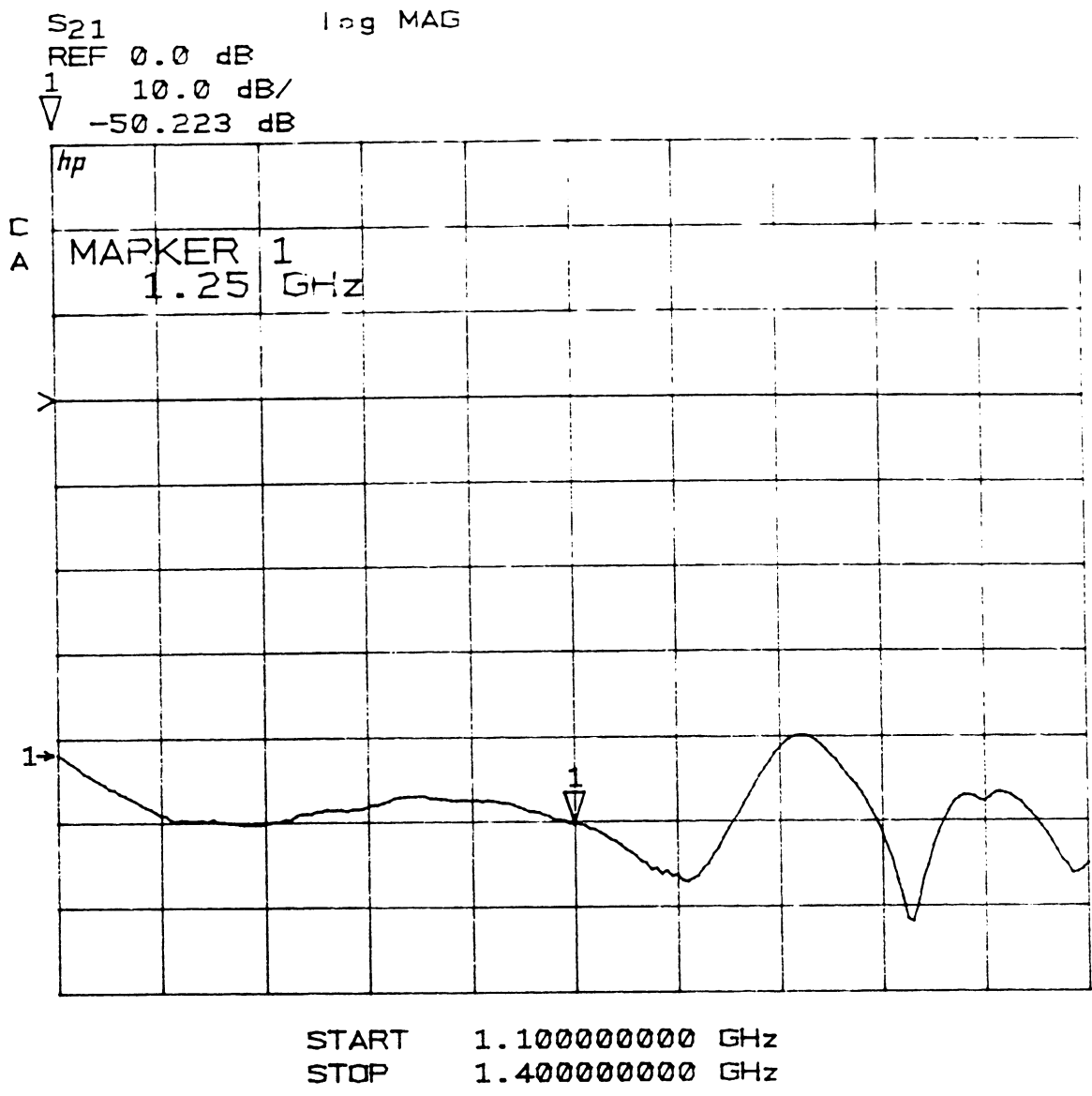


Figure A-1: Isolation of L-band OMT

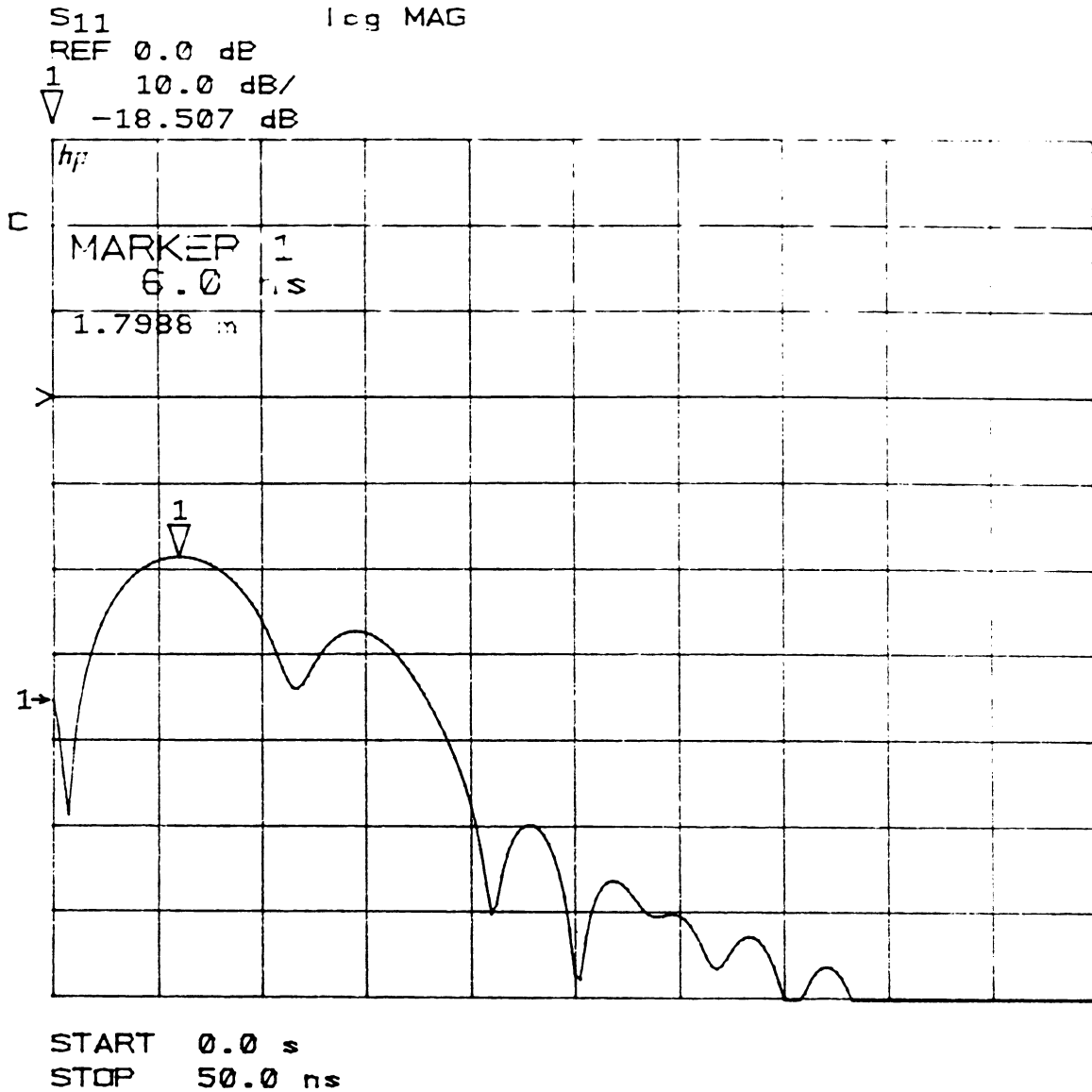


Figure A-2: Return Loss of L-band OMT (Side Arm)
(1.1 - 1.4 GHz)

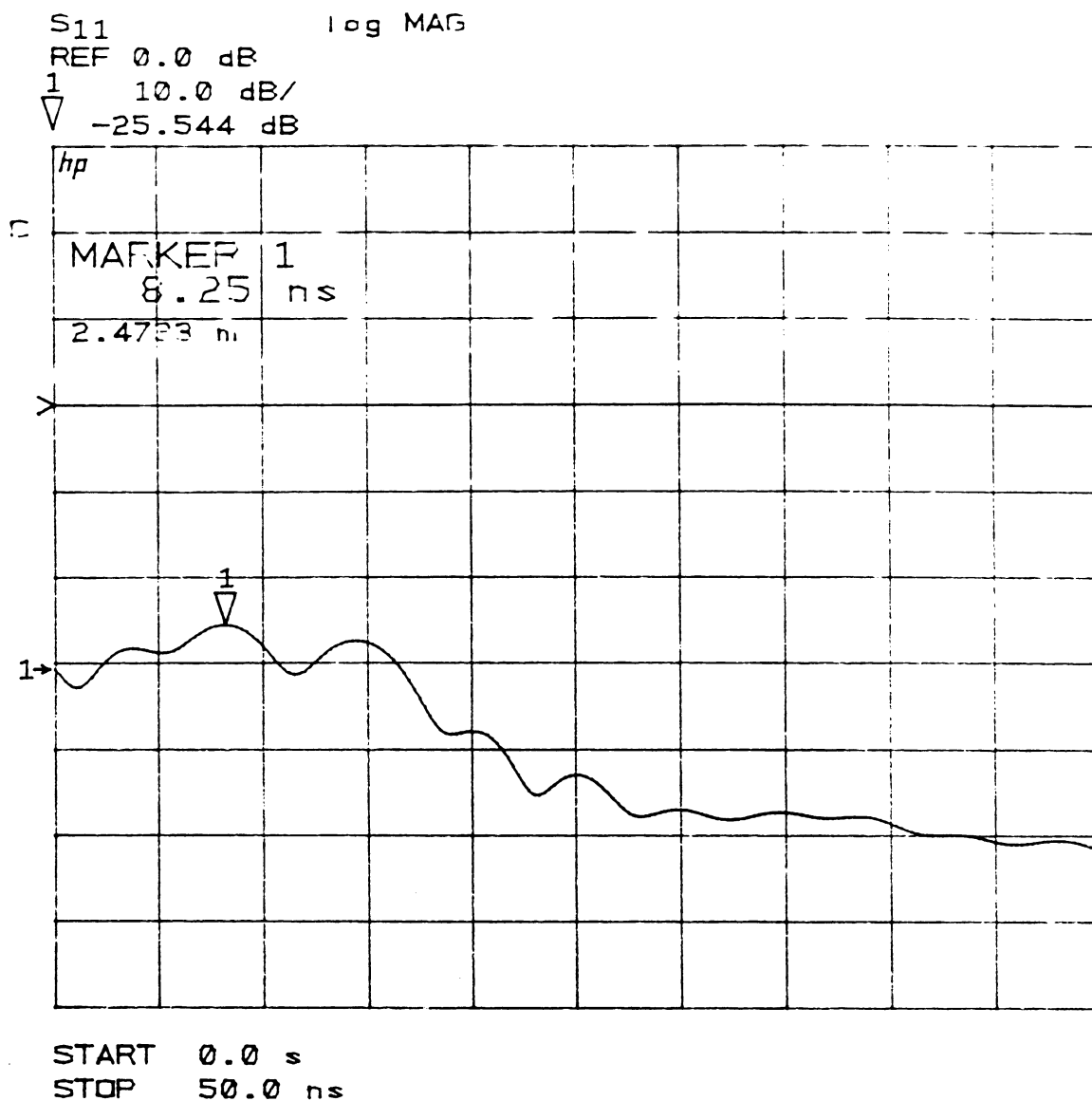
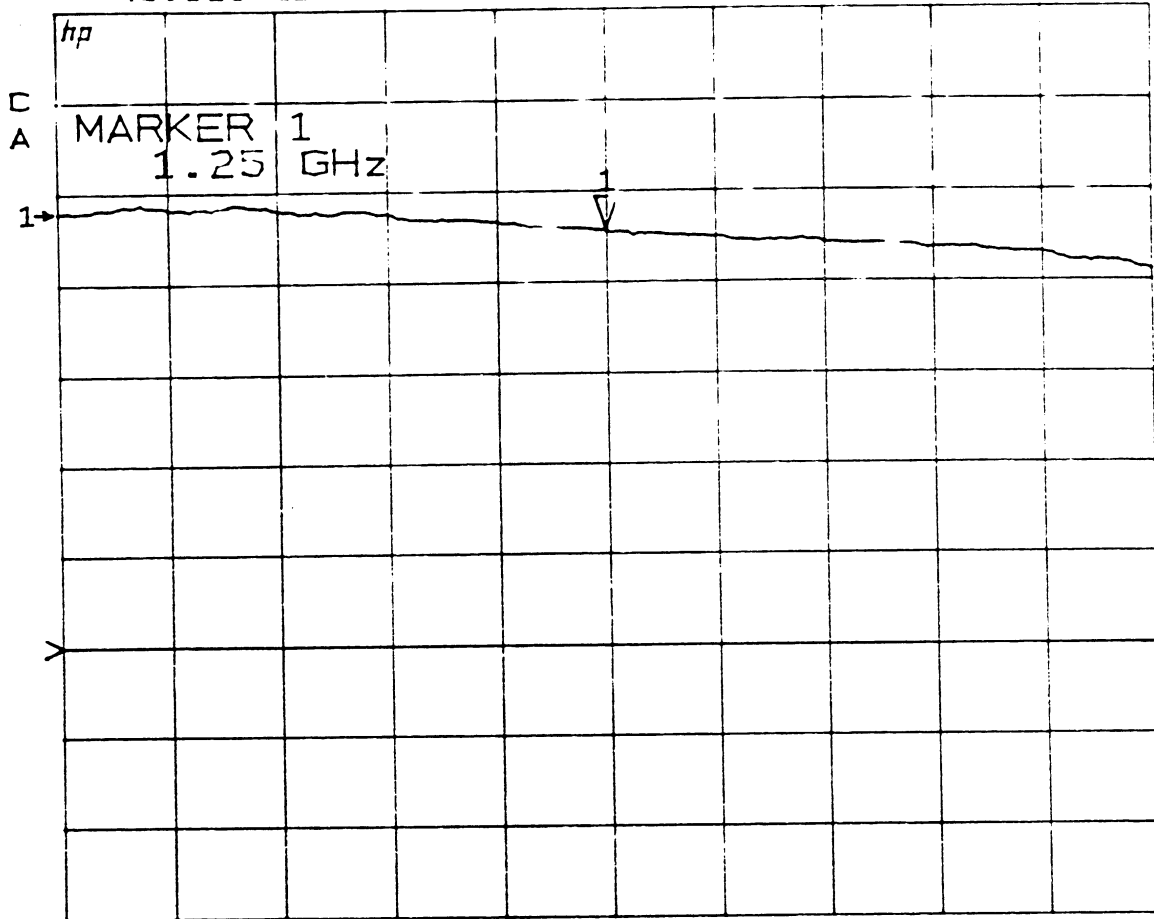


Figure A-3: Return Loss of L-band OMT (Streight Arm)
 (1.1 - 1.4 GHz)

APPENDIX B

AMPLIFIER SPECIFICATIONS

S21 log MAG
REF 0.0 dB
1 10.0 dB/
▽ 45.619 dB



CENTER 1.250000000 GHz
SPAN 0.500000000 GHz

Figure B-1: Gain of the Pre-amplifier at 24°C

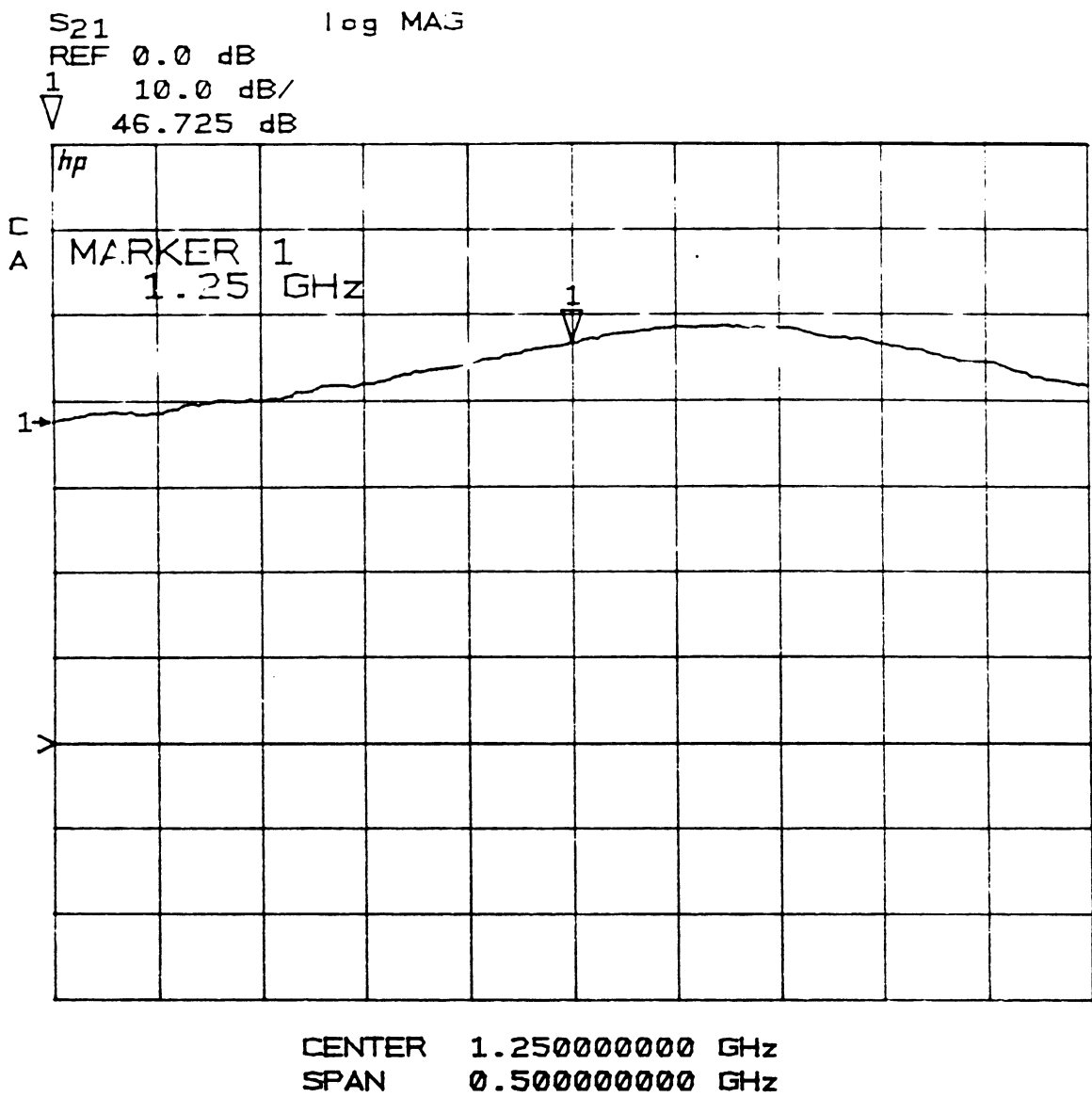
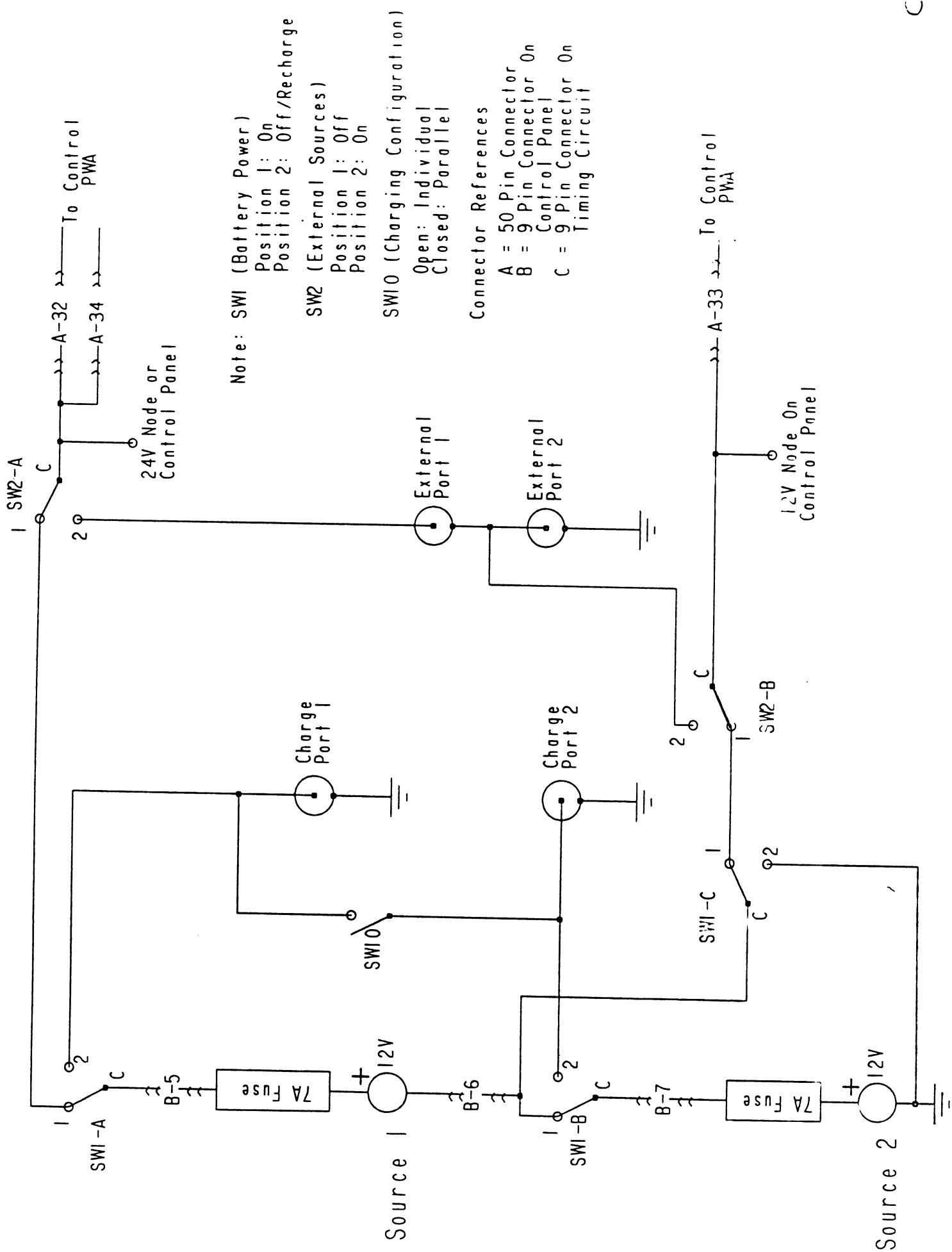


Figure B-2: Gain of the Power Amplifier at 24°C

APPENDIX C

CONTROL CIRCUITRY SCHEMATICS

Control Panel Power Connections



Note: SWI (Battery Power)
 Position 1: On
 Position 2: Off/Recharge

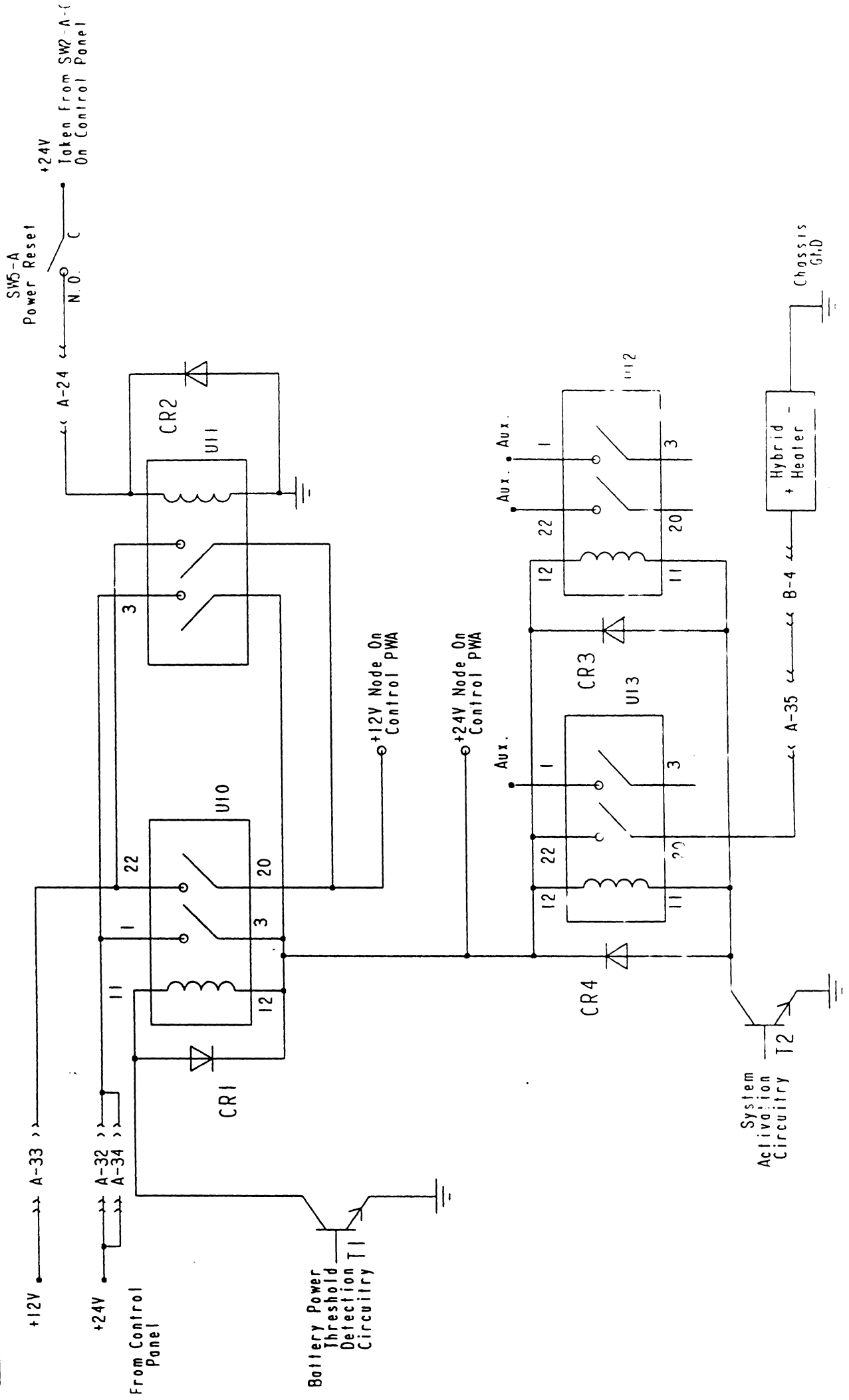
SW2 (External Sources)
 Position 1: Off
 Position 2: On

SWI0 (Charging Configuration)
 Open: Individual
 Closed: Parallel

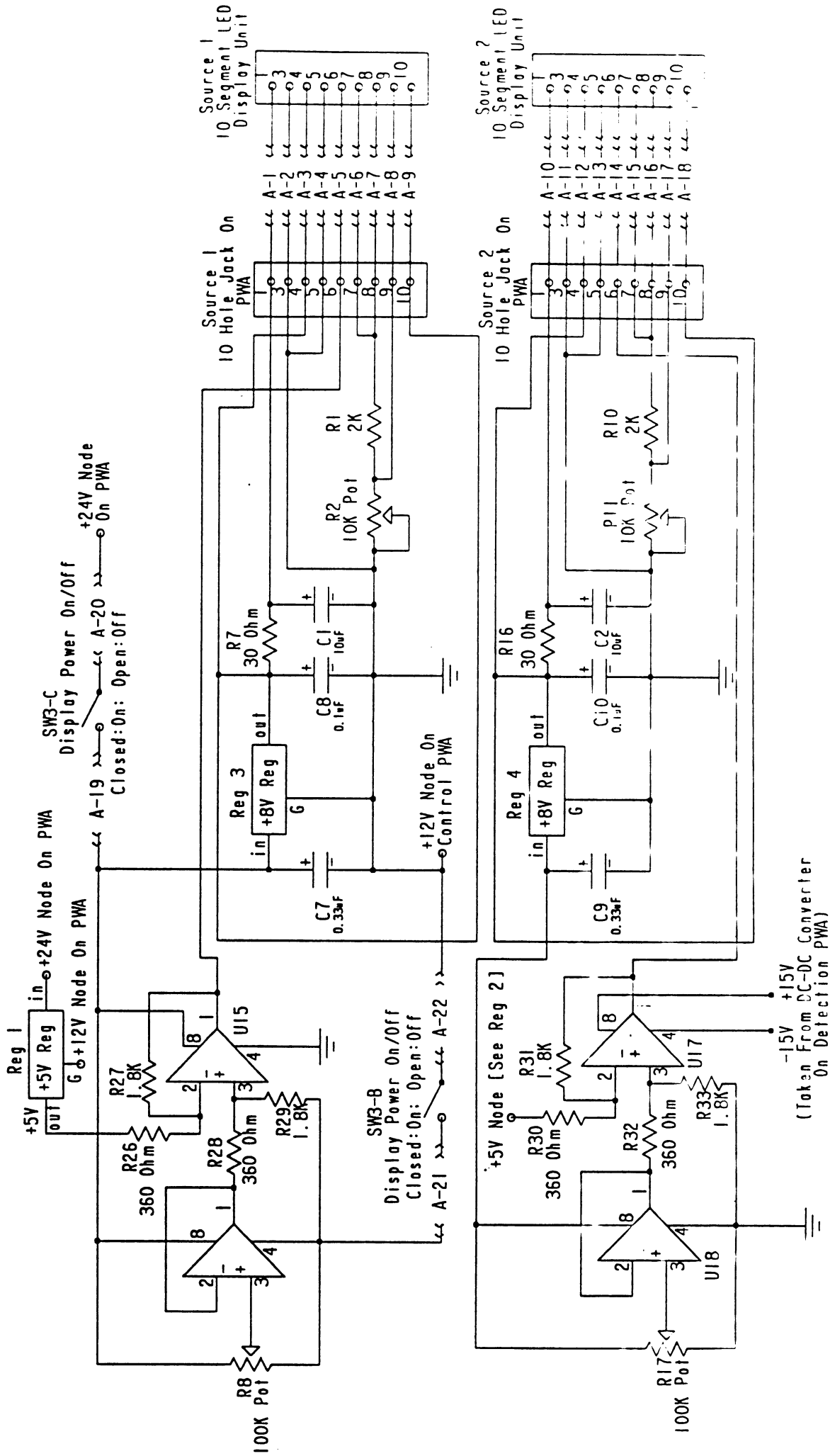
Connector References

- A = 50 Pin Connector
- B = 9 Pin Connector On Control Panel
- C = 9 Pin Connector On Timing Circuit

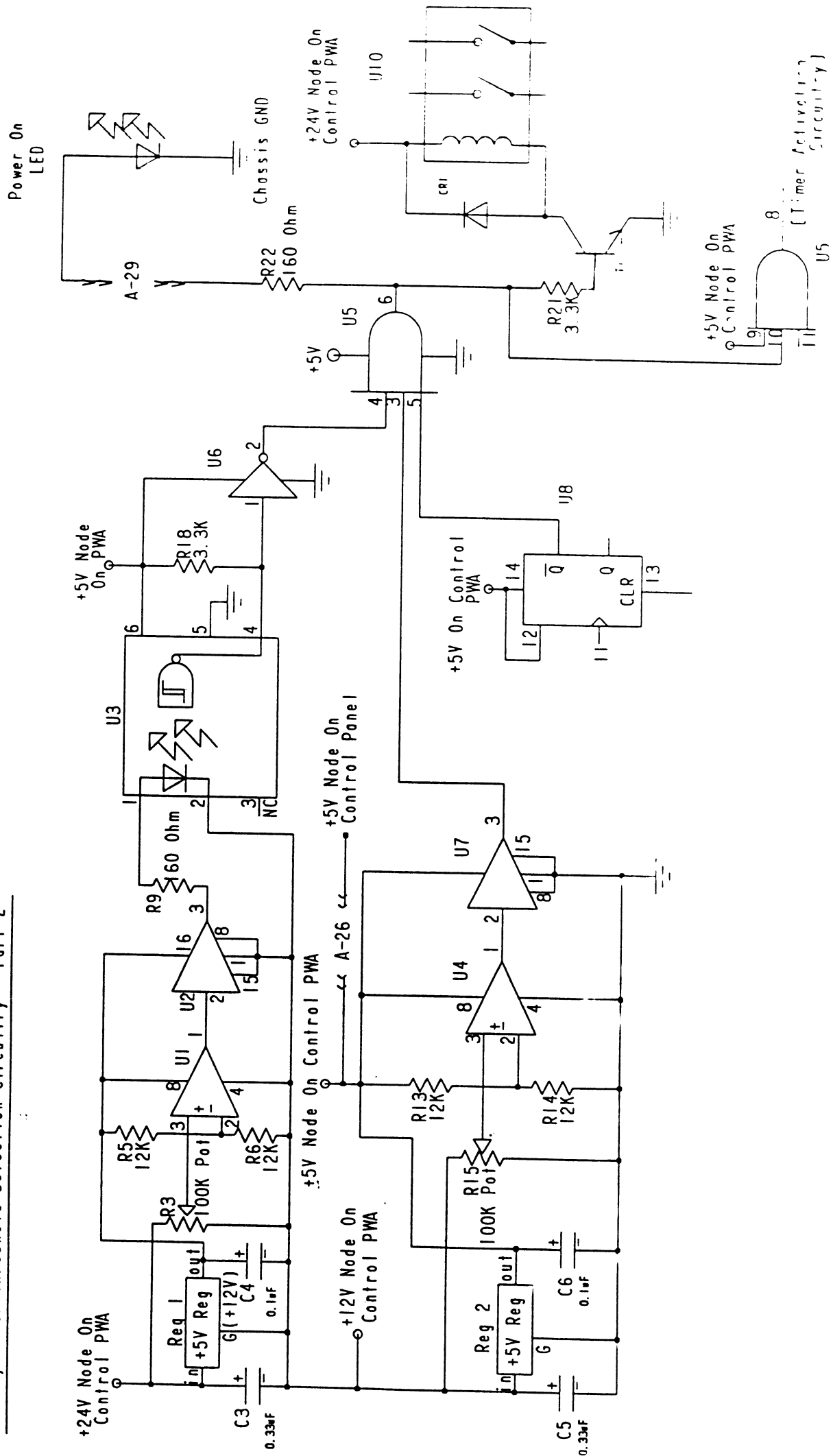
Relay Circuitry



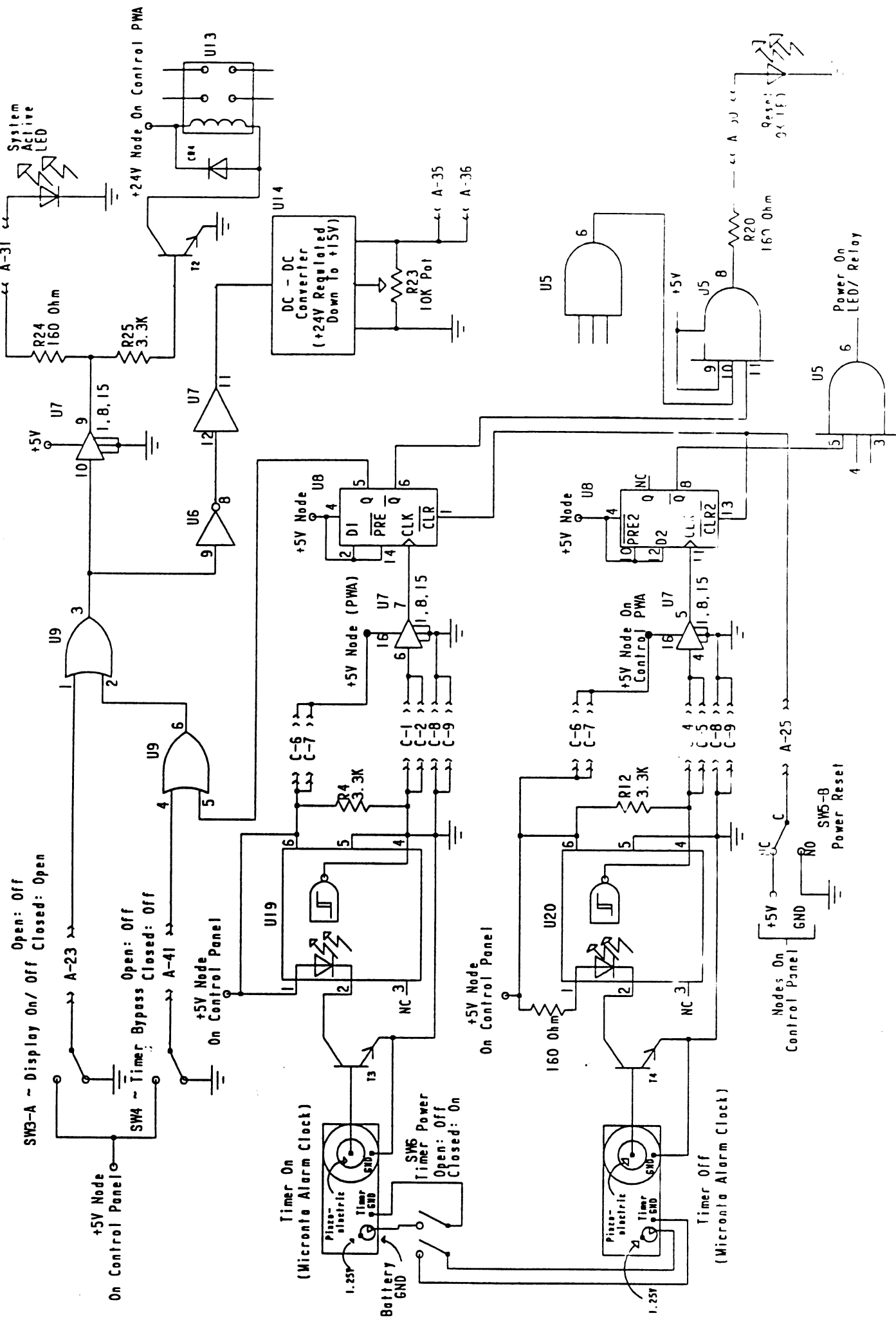
Battery Power Threshold Detection Circuitry



Battery Power Threshold Detection Circuitry - Part 2

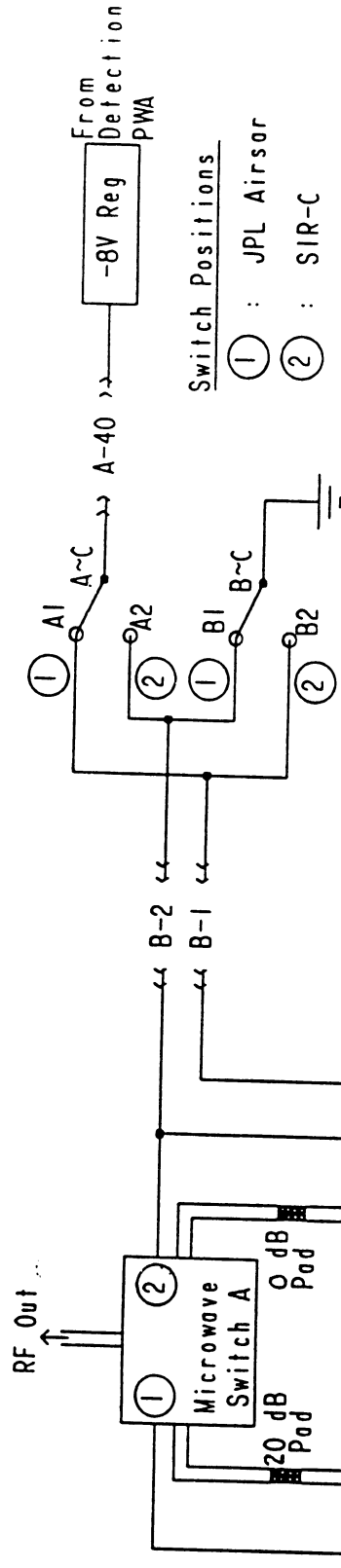


Timer Activation Circuitry



Microwave Switch Connections

SW7 ~ SAR Application



RF Amps/ Heater Connections

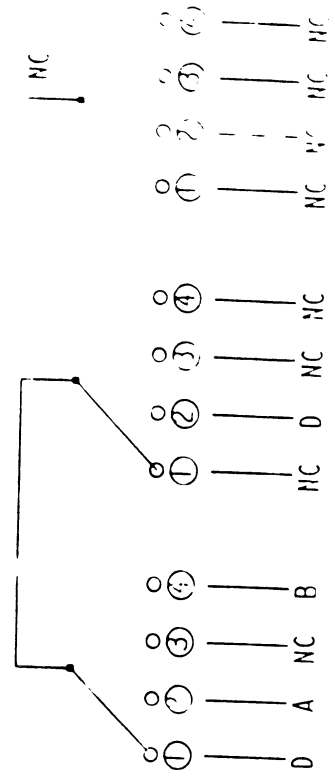
From PWA ——— A-35 ←—— B-4 →—— To Heater (+24V Node)

From PWA ——— A-36 ←—— B-3 →—— To Amplifiers (RF)
(+15V Node)

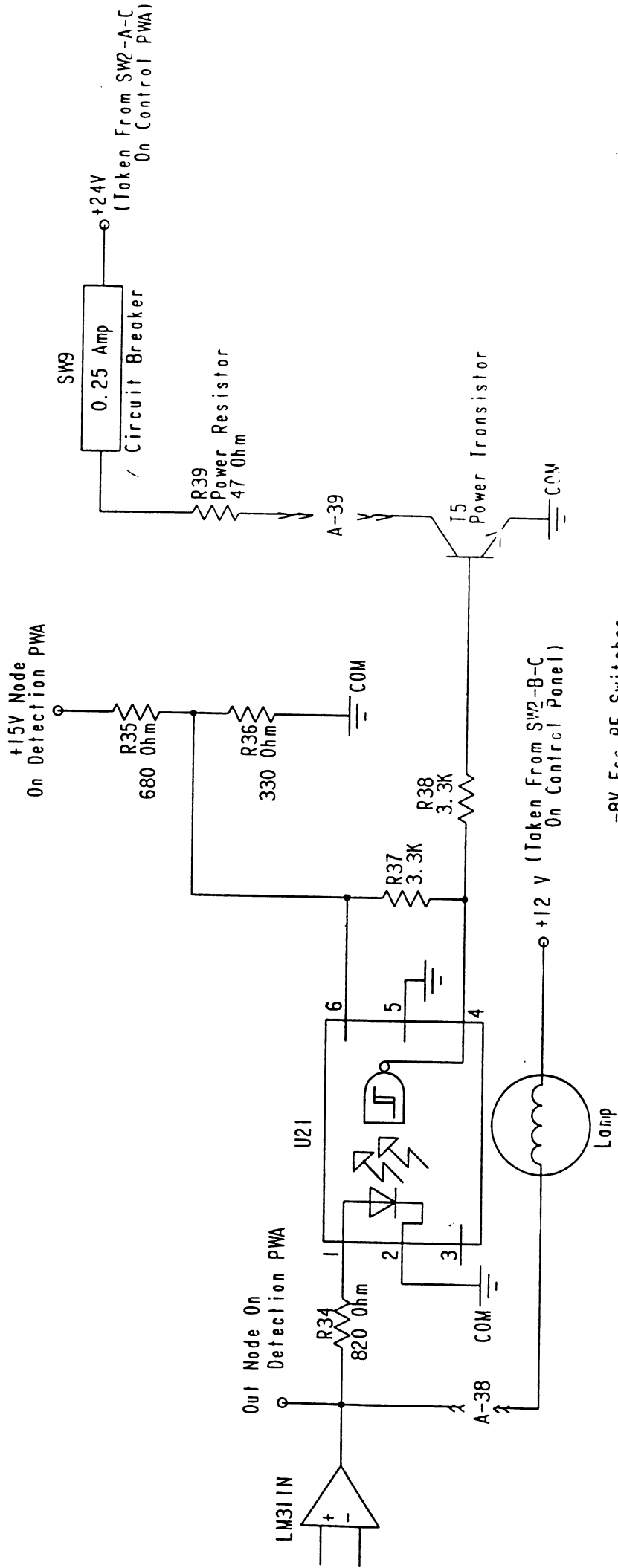
Timer Switch Replacement

Connection Pads Inside Of Timer	Positions	Function	Connected Pads	Position
A	1	Time Set	C, D	1
B	2	Alarm Set	A, C, D	2
C	3	Run - Alarm On	C	3
D	4	Run - Alarm Off	B, C	4

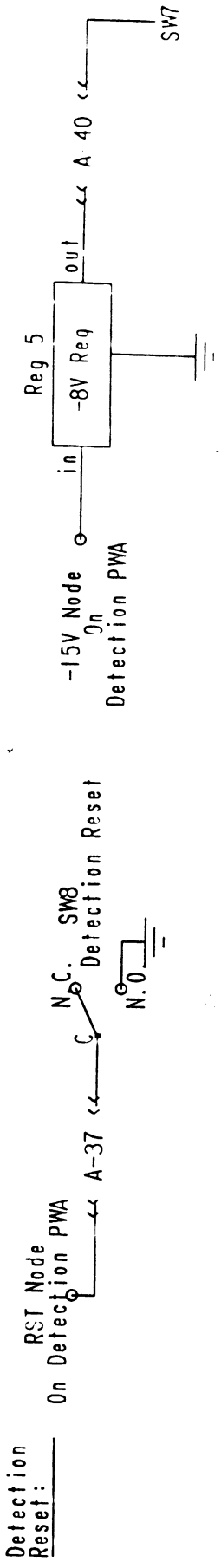
SW11 & SW12 (Timer Controls)
3 Pole - 4 Position Rotary Switch



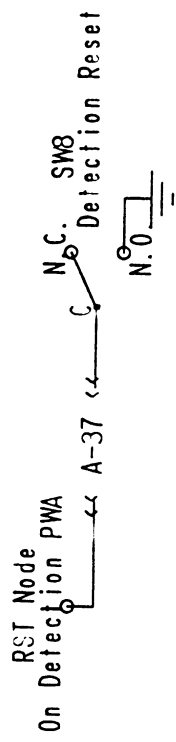
Modifications Made To Applied Microwave's Detection Circuitry



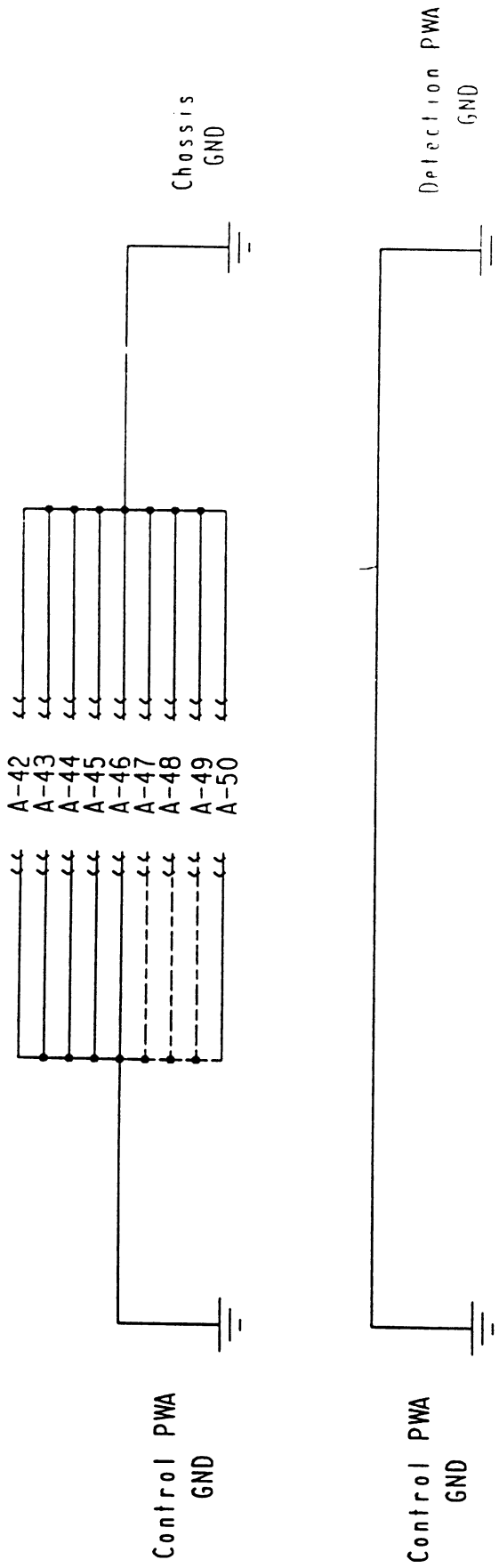
-8V For RF Switches



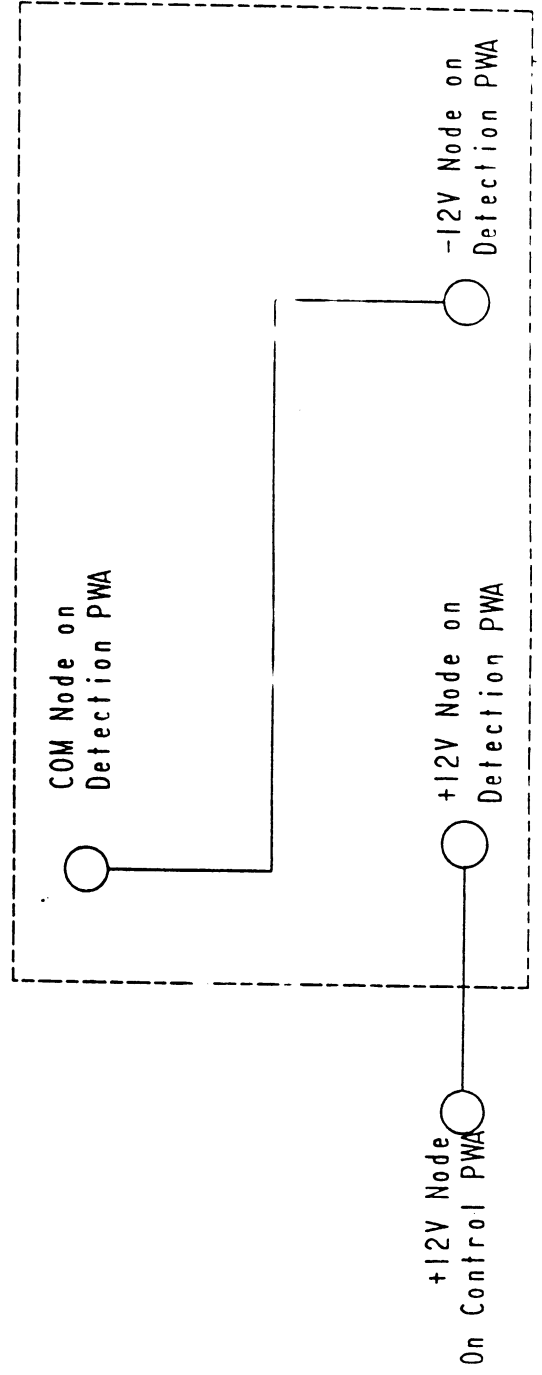
Detection Reset:



GROUND CONNECTIONS



POWER CONNECTIONS



APPENDIX D

MEASUREMENT AND CALIBRATION PROGRAMS


```
sig22=s11(itr,i)*sin(psi)**2+s21(itr,i)*cos(psi)**2
      +s21(itr,i)+s22(itr,i)*cos(psi)**2
sig12=sin(psi)*cos(psi)*(s11(itr,i)-s22(itr,i))-sin(psi)**2
      +s21(itr,i)+cos(psi)**2*s12(itr,i)
sig21=sin(psi)*cos(psi)*(s11(itr,i)-s22(itr,i))-sin(psi)**2
      +s12(itr,i)+cos(psi)**2*s21(itr,i)
s11(itr,i)=sig11
s22(itr,i)=sig22
s12(itr,i)=sig12
s21(itr,i)=sig21

WRITE(15,*)ANG,10.*ALOG10(4.*PI*cabs(S11(ITR,I))**2)
      ,10.*ALOG10(4.*PI*cabs(S22(ITR,I))**2)
      ,10.*ALOG10(4.*PI*cabs(S12(ITR,I))**2)
      ,10.*ALOG10(4.*PI*cabs(S21(ITR,I))**2)
WRITE(16,*)ANG,PHASE(S22(ITR,I)/S11(ITR,I))
      ,PHASE(S12(ITR,I)/S11(ITR,I))
      ,PHASE(S21(ITR,I)/S11(ITR,I))
ENDDO
STOP
END
C*****
C
C FUNCTION PHASE (2)
C*****
COMPLEX Z
PI=4.*ATAN(1.)
X=REAL(Z)
Y=AIMAG(Z)
PHASE=(180./PI)*ATAN2(Y,X)
if(phase.lt.-150.0) phase=phase+360
RETURN
END
```



```

1130 ON KEY 6 LABEL " # OF TRACES ",FNTRAP_level GOSUB Set_traces
1140 ON KEY 7 LABEL " # OF POINTS ",FNTRAP_level GOSUB Set_points
1150 ON KEY 8 LABEL " # OF AVERAGES ",FNTRAP_level GOSUB Set_average
1160 ON KEY 9 LABEL " QUIT ",FNTRAP_level GOTO Quit_fast_acq
1170 GOSUB Allocate_matrix
1180 LOOP
1190 EXIT IF Exit_flag=1
1200 END LOOP
1210 GOSUB Deallocate_mtxr
1220 Exit_flag=0
1230 GOTO Start_loop
1240 !
1250 Null: RETURN
1260 !
1270 !-----
1280 !
1290 Ref_target: ! Acquire a reference target data set.
1300
1310 OFF KEY
1320 Clear crt
1330 OUTPUT @Nwa;"TIMDTRANON; LOGM; GATEOFF;";
1340 OUTPUT @Nwa;"AUTO; ELED 100NS; STAR 0NS; STOP 300NS;";
1350 PRINT TABXY(1,10);"Please point scatterometer assembly to reference target."
1360 PRINT TABXY(1,12);"Press CONTINUE when ready..."
1370 PAUSE
1380 GOSUB Set_gates
1390 OUTPUT @Nwa;"TIMDTRANOFF; POLA; AVERFACT";VAL$(Average_factor);";";
1400 OUTPUT @Nwa;"AVEROON"
1410 INPUT "Enter the reference target angle: ",Ref_angle
1420 !
1430 ! Get the reference target response.
1440 !
1450 FOR T=1 TO Ntrace
1460 FOR F=1 TO 3
1470 IF Meas_flag(F) THEN
1480 Freq_sw(F)
1490 Freq_sw(F)
1500 OUTPUT @Nwa;"GATEOFF;";
1510 OUTPUT @Nwa;"GATECENT";VAL$(Gate_cent(F));"S;";
1520 OUTPUT @Nwa;"GATESPAN";VAL$(Gate_span(F));"S;";
1530 OUTPUT @Nwa;"GATEON;";
1540 OUTPUT @Nwa;"TIMDTRANOFF; POLA;";
1550 FOR P=1 TO 4
1560 Pol_sw(F,P)
1570 OUTPUT @Nwa;"FORM3;NUMG";VAL$(Average_factor+1);";";WAIT"
1580 OUTPUT @Nwa;"WAIT; OUTPFORM;";
1590 ENTER @Nwa data1;Preamble,Bytes,Trace(*)
1600 MAT Target_response(P,*)= Trace
1610 NEXT P
1620 FOR P=1 TO 4
1630 FOR Nt=Nskh TO Npts STEP Nskip
1640 Nst=INT(Nt/Nskip)
1650 Target_data(T,P,Nst)=Target_response(P,Nt)
1660 NEXT Nt
1670 NEXT P
1680 NEXT IF
1690 NEXT F
1700 NEXT T
1710 Store_file(Target_data(*),"REF",FNTime_stamp$,F)
1720 !
1730 ! Get the reference target mount response.
1740 !
1750 BEEP
1760

```

```

1770 PRINT TABXY(1,10);"Please remove the reference target from its mount."
1780 PRINT TABXY(1,12);"Press CONTINUE when ready..."
1790 PAUSE
1800 Clear crt
1810 PRINT TABXY(1,14);"Data for the mount is being collected .... "
1820 FOR T=1 TO Ntrace
1830 FOR P=1 TO 3
1840 IF Meas_flag(F) THEN
1850 Freq_set(F)
1860 Freq_sw(F)
1870 OUTPUT @Nwa;"GATEOFF;";
1880 OUTPUT @Nwa;"GATECENT";VAL$(Gate_cent(F));"S;";
1890 OUTPUT @Nwa;"GATESPAN";VAL$(Gate_span(F));"S;";
1900 OUTPUT @Nwa;"GATEON;";
1910 FOR P=1 TO 4
1920 Pol_sw(F,P)
1930 OUTPUT @Nwa;"FORM3;NUMG";VAL$(Average_factor+1);";";WAIT"
1940 OUTPUT @Nwa;"WAIT; OUTPFORM;";
1950 ENTER @Nwa data1;Preamble,Bytes,Trace(*)
1960 MAT Target_response(P,*)= Trace
1970 NEXT P
1980 Nskh=Nskip+1
1990 FOR P=1 TO 4
2000 FOR Nt=Nskh TO Npts STEP Nskip
2010 Nst=INT(Nt/Nskip)
2020 Target_data(T,P,Nst)=Target_response(P,Nt)
2030 NEXT Nt
2040 NEXT P
2050 END IF
2060 NEXT F
2070 NEXT T
2080 Store_file(Target_data(*),"MNT",FNTime_stamp$,F)
2090 Pol_sw(F_disp,P_disp)
2100 DISP "Reference target mount response saved."
2110 Exit_flag=1
2120 RETURN
2130 !
2140 !
2150 !
2160 Acq_target: !
2170 !
2180 OFF KEY
2190 Clear crt
2200 OUTPUT @Nwa;"TIMDTRANON; LOGM; GATEOFF;";
2210 OUTPUT @Nwa;"ELED 100NS; STAR 0NS; STOP 300NS;";
2220 PRINT TABXY(1,10);"Please point scatterometer assembly at surface target."
2230 PRINT TABXY(1,12);"Press CONTINUE when ready..."
2240 PAUSE
2250 GOSUB Set_gates
2260 OUTPUT @Nwa;"TIMDTRANOFF; POLA; AVERFACT";VAL$(Average_factor);";";
2270 OUTPUT @Nwa;"GATEOFF;AVEROON;";
2280 !
2290 ! Get the target response.
2300 !
2310 FOR T=1 TO Ntrace
2320 !
2330 ! Get angles
2340 !
2350 IF T=1 THEN
2360 Rotation_state=-1
2370 ELSE
2380 Rotation_state=2
2390 END IF
2400 SELECT Rotation_state

```

```

2410 CASE =0
2420   Clear crt
2430   PRINT TABXY(1,4);"When ready for measurement, press CONTINUE."
2440   BEEP
2450   PAUSE
2460   Clear crt(3,16)
2470   PRINT TABXY(1,4);"Collecting data..."
2480   CASE ELSE
2490     PRINT TABXY(1,4);"Current angle is ";Current_angle;" degrees."
2500     Rotate_target
2510     WAIT 1
2520     Clear crt(3,16)
2530     PRINT TABXY(1,4);"Collecting data ..."
2540     END SELECT
2550     FOR F=1 TO 3
2560       IF Meas_flag(F) THEN
2570         Freq_set(F)
2580         Freq_sw(F)
2590         OUTPUT @Nwa;"GATEOFF;"
2600         OUTPUT @Nwa;"GATECENT";VAL$(Gate_cent(F));"S;"
2610         OUTPUT @Nwa;"GATESPAN";VAL$(Gate_span(F));"S;"
2620         OUTPUT @Nwa;"GATEON";WAIT;"
2630         PRINT Npts,Ntrace,Ndata,Nskip
2640         FOR P=1 TO 4
2650           Pol_sw(F,P)
2660           OUTPUT @Nwa;"NUMG";VAL$(Average_factor);";WAIT; FORM3; OUTPFORM;"
2670           ENTER @Nwa_data1;Preamble,Bytes,Trace(*)
2680           MAT Target_response(P,*)= Trace
2690           NEXT P
2700           Nskh=Nskip+1
2710           FOR P=1 TO 4
2720             FOR Nt=Nskh TO Npts STEP Nskip
2730               Nst=INT(Nt/Nskip)
2740               Target_data(T,P,Nst)=Target_response(P,Nt)
2750               NEXT Nt
2760               NEXT P
2770               END IF
2780             NEXT F
2790             PRINT "# OF TRACES LEFT=";Ntrace-T
2800             NEXT T
2810             Store_file(Target_data(*),"GND",FNTime_stamp$,F)
2820             DISP "Surface target data saved."
2830             BEEP
2840             Rotation_state=4
2850             Rotate_target
2860             WAIT 5
2870             BEEP
2880             OUTPUT @Nwa;"CONT;"
2890             Exit_flag=1
2900             RETURN
2910             !
2920             !-----
2930             !
2940             Freq_set: GOSUB Deallocate_mtrx
2950             OFF KEY
2960             MAT Meas_flag_old= Meas_flag
2970             MAT Meas_flag= (0)
2980             !
2990             !
3000             ! ON KEY 0 LABEL " L BAND ",FNTrap_level GOSUB Set_1
3010             ! ON KEY 1 LABEL " C BAND ",FNTrap_level GOSUB Set_c
3020             ! ON KEY 2 LABEL " X BAND ",FNTrap_level GOSUB Set_x
3030             ! ON KEY 4 LABEL " STORE ",FNTrap_level GOTO Store_band
3040             ! ON KEY 5 LABEL " ",FNTrap_level GOSUB Null
3050             ! ON KEY 6 LABEL " ",FNTrap_level GOSUB Null
3060             !
3070             !
3080             !
3090             !
3100             !
3110             !
3120             !
3130             RETURN
3140             Set_1:
3150             Meas_flag(1)=1
3160             F_disp=1
3170             RETURN
3180             Set_c:
3190             Meas_flag(2)=1
3200             F_disp=2
3210             RETURN
3220             Set_x:
3230             Meas_flag(3)=1
3240             F_disp=3
3250             RETURN
3260             Store_band: Print_banner4
3270             Exit_flag=1
3280             GOSUB Allocate_matrix
3290             RETURN
3300             Cancel_band: !
3310             MAT Meas_flag= Meas_flag_old
3320             Exit_flag=1
3330             GOSUB Allocate_matrix
3340             RETURN
3350             !
3360             !-----
3370             !
3380             Set_angle: !
3390             INPUT "Enter measurement angle: ",Angle
3400             Angles=VAL$(Angle)&CHR$(179)&" " ! Degree sign.
3410             Print_banner4
3420             RETURN
3430             !
3440             !-----
3450             !
3460             Set_target: !
3470             LINPUT "Enter target type or name: ",Targets
3480             Target$=TRIMS(Target$)
3490             Target$=Target&RPTS(" ",30-LEN(Target$))
3500             Print_banner4
3510             RETURN
3520             !
3530             !-----
3540             !
3550             Set_traces: !
3560             INPUT "Enter the number of traces (or angles) desired( >-1) : ",Ntraces
3570             GOSUB Deallocate_mtrx
3580             GOSUB Allocate_matrix
3590             Print_banner4
3600             RETURN
3610             !
3620             !-----
3630             Set_points: !
3640             INPUT "Enter the number of sample points (Npts,201) : ",Npts
3650             OUTPUT @Nwa;"POIN ";$VAL$(Npts)&";"
3660             INPUT "Enter the data points to be stored (Ndata,10) : ",Ndata
3670             Nskip=INT(Npts/Ndata)
3680             Bytes=16*Ndata

```

```

3690 Print_banner4
3700 GOSUB Deallocate_mtrx
3710 GOSUB Allocate_matrix
3720 RETURN
3730 !
3740 !-----
3750 !
3760 Set_average: !
3770 INPUT "Enter averaging factor: ",Average_factor
3780 Print_banner4
3790 RETURN
3800 !
3810 !-----
3820 !
3830 Allocate_matrix: ! Allocate storage space for data.
3840
3850 System_memory=VAL(SYSTEMS("AVAILABLE MEMORY"))
3860 Avail_traces=MIN(Ntrace,INT(System_memory/50000-3*4*16.*Npts)/(3*4*16.*Ndata))
3870 IF Avail_traces<Ntrace THEN
3880 BEEP
3890 PRINT TABX(1,16);"Memory has capacity for only ";Avail_traces;" traces."
3900 PRINT "Press CONTINUE key to continue"
3910 PAUSE
3920 Ntrace=Avail_traces
3930 END IF
3940 ALLOCATE COMPLEX Trace(Npts),Target_response(4,Npts)
3950 ALLOCATE COMPLEX Target_data(Ntrace,4,Ndata)
3960 RETURN
3970 Deallocate_mtrx: ! Return to main program.
3980 !
3990 DEALLOCATE Target_response(*),Trace(*)
4000 DEALLOCATE Target_data(*)
4010 RETURN
4020 !
4030 !-----
4040 !
4050 Set_gates: ! Set gate centers and spans.
4060 !
4070 FOR F=1 TO 3
4080 IF Meas_flag(F) THEN
4090 Freq_set(F)
4100 Freq_sw(F)
4110 P=3
4120 Pol_sw(F,P)
4130 OUTPUT @Nwa;"TIMTRANON; LOGM;"
4140 OUTPUT @Nwa;"ELED 100NS; STAR 0NS; STOP 300NS; WAIT;"
4150 OUTPUT @Nwa;"FORM3; OUTPACTI;"
4160 ENTER @Nwa;Gate cent(F)
4170 OUTPUT @Nwa;"MARKOFF;"
4180 OUTPUT @Nwa;"CONT;"
4190 OUTPUT @Nwa;"GATESPAN";VAL$(Gate_span(F));"S;"
4200 OUTPUT @Nwa;"GATECENT";VAL$(Gate cent(F));"S;"
4210 OUTPUT @Nwa;"KEY41; KEY59; KEY58; KEY59;"
4220 LOCAL @Nwa
4230 DISP "Adjust gate center to suit, and press CONTINUE."
4240 PAUSE
4250 OUTPUT @Nwa;"OUTPACTI;"
4260 ENTER @Nwa;Gate cent(F)
4270 OUTPUT @Nwa;"GATESPAN";VAL$(Gate span(F));";"
4280 OUTPUT @Nwa;"KEY41; KEY59; KEY58; KEY4;"
4290 LOCAL @Nwa
4300 DISP "Adjust gate span to suit, and press CONTINUE."
4310 PAUSE
4320 OUTPUT @Nwa;"OUTPACTI;"
4330
4340 ENTER @Nwa;Gate_span(F)
4350 END IF
4360 NEXT F
4370 RETURN
4380 !-----
4390 !
4400 Quit_fast_acq: ! End of program
4410 DISP "PROGRAM EXIT"
4420 GOSUB Deallocate_mtrx
4430 LOAD KEY "EDITKEY:MEMORY,0,1"
4440 STOP
4450 END
4460 !
4470 !-----
4480 !
4490 DEF FNask(Prompt$)
4500 OFF KEY
4510 DISP Prompt$;
4520 INPUT "",Yn$
4530 Yn$=UPC$(Yn$(1,1))
4540 SELECT Yn$
4550 CASE ="Y"
4560 RETURN 1
4570 CASE ="N",=""
4580 RETURN 0
4590 CASE ELSE
4600 RETURN 0
4610 END SELECT
4620 FNEND
4630 !
4640 !-----
4650 !
4660 DEF FNfileloc$(File$,Dir$)
4670 INTEGER C ! for the location of the ':' in Dir$ (minus 1)
4680 LET C=POS(Dir$,":")-1
4690 IF C<=0 THEN
4700 RETURN TRIMS(File$&Dir$)
4710 ELSE
4720 RETURN Dir$(1,C)&RPTS("/",Dir$(C,C)<>"/")&File$&Dir$(C+1,LEN(Dir$))
4730 END IF
4740 FNEND ! Fileloc
4750 !
4760 !-----
4770 !
4780 DEF FNTIME_stamp$(OPTIONAL Time_format)
4790 !
4800 DIM Time_digits$(4),Year_digits$(6)
4810 DIM Machine_times$(8),Machine_dates$(11)
4820 REAL TImedate_now
4830 !
4840 TImedate_now=TIMEDATE
4850 Machine_date$=DATES(TImedate_now)
4860 Machine_times$=TIMES(TImedate_now)
4870 Time_digits$=Machine_times$(1,2)&Machine_time$(4,5)
4880 Year_digits$(1,2)=Machine_dates$(10,11)
4890 IF Machine_dates$(1,1)=" " THEN Machine_date$(1,1)="0"
4900 !
4910 SELECT Machine_date$(4,6)
4920 CASE ="Jan"
4930 Year_digits$(3,4)="01"
4940 CASE ="Feb"
4950 Year_digits$(3,4)="02"
4960 CASE ="Mar"

```



```
4970 Year_digits$[3,4]="03"
4980 CASE ="Apr"
4990 Year_digits$[3,4]="04"
5000 CASE ="May"
5010 Year_digits$[3,4]="05"
5020 CASE ="Jun"
5030 Year_digits$[3,4]="06"
5040 CASE ="Jul"
5050 Year_digits$[3,4]="07"
5060 CASE ="Aug"
5070 Year_digits$[3,4]="08"
5080 CASE ="Sep"
5090 Year_digits$[3,4]="09"
5100 CASE ="Oct"
5110 Year_digits$[3,4]="10"
5120 CASE ="Nov"
5130 Year_digits$[3,4]="11"
5140 CASE ="Dec"
5150 Year_digits$[3,4]="12"
5160 END SELECT
5170 !
5180 Year_digits$[5,6]=Machine_date$[1,2]
5190 SELECT NPAP
5200 CASE =0
5210 RETURN Year_digits$[5,6]&Time_digits$
5220 CASE =1
5230 IF Time_format=1 THEN
5240 RETURN Year_digits$&Time_digits$
5250 END IF
5260 IF Time_format=2 THEN
5270 RETURN Year_digits$[3,6]&Time_digits$
5280 END IF
5290 END SELECT
5300 FNEND
5310 !
5320 !
5330 !
5340 DEF FNTrap_level
5350 RETURN VAL(SYSTEM$("SYSTEM PRIORITY"))+1
5360 FNEND
5370 !
5380 !
5390 !
5400 SUB Config and poll
5410 COM /Paths/ @Nwa,@Nwa_data1,@Nwa_data2,Network_analyzer,@Hpiib,@Relay
5420 COM /System/ System_memory
5430 !
5440 ! Find out what's out there.
5450 !
5460 ALLOCATE Device_list$(0:31) [20]
5470 ALPHA PEN 4
5480 KBD LINE PEN 3
5490 KEY LABELS PEN 5
5500 Clear_crt
5510 Network_analyzer=0
5520 ALLOCATE Na_ident$(80)
5530 System_memory=VAL(SYSTEM$("AVAILABLE MEMORY")) ! How much memory for RAM-DISK
5540 PRINT "AVAILABLE MEMORY: ";System_memory;" BYTES"
5550 ON TIMEOUT 7,4 GOTO No_na ! In case there is no network analyzer
5560 Is_na: OUTPUT @Nwa;"FORM4"; OUTPIDEN;"
5570 ENTER @Nwa_data2;Na_ident$
5580 IF POS(Na_ident$,"8510A") THEN Network_analyzer=1
5590 IF POS(Na_ident$,"8510B") THEN Network_analyzer=2
5600 IF POS(Na_ident$,"8720A") THEN Network_analyzer=3
5610 IF POS(Na_ident$,"8720B") THEN Network_analyzer=4
5620 IF POS(Na_ident$,"8753A") THEN Network_analyzer=5
5630 IF POS(Na_ident$,"8753B") THEN Network_analyzer=6
5640 LOCAL @Nwa
5650 PRINT
5660 PRINT Na_ident$
5670 PRINT Network_analyzer
5680 ! Clear_crt
5690 PRINT
5700 PRINT
5710 IF Network_analyzer=0 THEN
5720 !
5730 !
5740 No_na: BEEP
5750 OFF CYCLE
5760 PRINT TABXY(1,5);"There is no active network analyzer on the HPIB bus."
5770 PRINT TABXY(1,6);"Please check connections, and press the RUN key."
5780 PRINT
5790 PRINT TABXY(1,7);"If you DO NOT want to use a network analyzer, press th
CONTINUE key."
5800 PAUSE
5810 END IF
5820 !
5830 !
5840 Check_hpiib: ! Check the rest of the bus
5850 ON TIMEOUT 7,.01 GOTO Nothing
5860 !
5870 FOR Device=700 TO 731
5880 DISP "Checking for device at address: ";Device
5890 Device_list$(Device-700)="NOTHING"
5900 ASSIGN @What_is_it TO Device
5910 Outcome=SPOLL(@What_is_it)
5920 Device_list$(Device-700)="SOMETHING"
5930 PRINT Device,"SOMETHING HERE", "spoll: ";Outcome
5940 ASSIGN @What_is_it TO *
5950 Nothing: ! Skip to next device
5960 NEXT Device
5970 !
5980 OFF TIMEOUT 7
5990 ASSIGN @What_is_it TO *
6000 IF Device_list$(1)="SOMETHING" THEN
6010 DISP "Position the printer to Top-Of-Form and press CONTINUE..."
6020 PAUSE
6030 PRINTER IS PRT
6040 PRINT CHR$(27)&"lll"; ! Set Page Breaks
6050 Printer_flag=1
6060 PRINTER IS CRT
6070 END IF
6080 DEALLOCATE Na_ident$
6090 DEALLOCATE Device_list$(*)
6100 ABORT @Hpiib
6110 SUBEXIT
6120 SUBEND
6130 !
6140 !
6150 !
6160 SUB Hp_bus_init
6170 COM /Paths/ @Nwa,@Nwa_data1,@Nwa_data2,Network_analyzer,@Hpiib,@Relay
6180 COM /Sys_1/ Freq$(*),Freq_cent(*),Freq_span(*),Gate_cent(*),Gate_span(*)
6190 COM /Sys_2/ Pol$(*),Polsw$(*)
6200 COM /System config/ INTEGER Printer_flag,Debug flag,Version2,Mode2,Out Type2,50
6210 d$,Bell$,Target$,Ref_target$
6220 !
! This subroutine configures the HPIB bus and connects the printer.
```

```

6230 !
6240 ASSIGN @Hpb TO 7
6250 ASSIGN @Nwa TO 716
6260 ASSIGN @Nwa_data1 TO 716;FORMAT OFF
6270 ASSIGN @Nwa_data2 TO 716;FORMAT ON
6280 ASSIGN @Relay TO 710
6290 REMOTE @Hpb
6300 ABORT @Hpb
6310 CLEAR @Nwa
6320 IF Debug_flag=1 THEN OUTPUT @Nwa;"DEBUON:"
6330 IF Debug_flag=0 THEN
6340 OUTPUT @Nwa;"DEBUOFF;"
6350 OUTPUT @Nwa;"TITL ""&Freq$(2) &" BAND ""
6360 END IF
6370 SUBEND
6380 !
6390 !*****
6400 !
6410 SUB Series_init
6420 COM /system_config/ INTEGER Printer_flag,Debug_flag,Version$,Mode$,Out_types,Sound
$,Bell$,Target$,Ref_target$
6430 DIM Input$(80)
6440 !
6450 ! This subroutine prints a header for the printout and sets the system
6460 ! date and time.
6470 !
6480 IF Printer_flag=1 THEN PRINTER IS PRT
6490 PRINT CHR$(12)
6500 Set clock
6510 ! LINPUT "ENTER MEASUREMENT SERIES TITLE",Input$
6520 ! Preface$="&RPT$( " ,9)
6530 ! PRINT RPT$( " ,70)
6540 ! PRINT Preface$&Input$
6550 ! LINPUT "ENTER OPERATOR NAME",Input$
6560 ! PRINT Preface$&Input$
6570 PRINTER IS CRT
6580 PRINT
6590 PRINT
6600 PRINT Preface$&"MEASUREMENT SERIES STARTED AT "&TIMES(TIMEDATE)
6610 PRINTER IS CRT
6620 SUBEND
6630 !
6640 !*****
6650 !
6660 SUB Set_clock
6670 OPTION BASE 1
6680 INTEGER I
6690 DIM Chrono$(12),Months(12)(3)
6700 Exec_key$=CHR$(255)&CHRS(88)
6710 READ Months(*)
6720 DATA "JAN","FEB","MAR","APR","MAY","JUN","JUL","AUG","SEP","OCT","NOV","DEC"
6730 OUTPUT KBD;"SCRATCH KEY "&Exec_key$;
6740 Clear_crt
6750 PRINT "
6760 PRINT " Current system date: ";DATES(TIMEDATE)
6770 PRINT " Current system time: ";TIMES(TIMEDATE)
6780 Ask: LINPUT "Enter date and time (YYMMDDHHMSS) ":";Chrono$
6790 IF Chrono$="" AND DATES(TIMEDATE)<" 1 Mar 1900" THEN
6800 Clear_crt
6810 SUBEXIT
6820 END IF
6830 Year$=VAL$(1900+VAL(Chrono$(1,2)))
6840 IF (VAL(Chrono$(3,4))<=0 OR VAL(Chrono$(3,4))>12) THEN
6850 BEEP

```

```

6860 PRINT "Incorrect month value."
6870 GOTO Ask
6880 END IF
6890 Year$=Month$(VAL(Chrono$(3,4)))&" "&Year$
6900 Year$=Chrono$(5,6)&" "&Year$
6910 SET TIMEDATE (DATE(Year$))
6920 IF (VAL(Chrono$(7,8)))>23 THEN
6930 BEEP
6940 PRINT "Incorrect hour value."
6950 GOTO Ask
6960 END IF
6970 Day$=Chrono$(7,8)&" ":"
6980 IF VAL(Chrono$(9,10))>59 THEN
6990 BEEP
7000 PRINT "Incorrect minute value."
7010 GOTO Ask
7020 END IF
7030 Day$=Day$&Chrono$(9,10)&" ":"
7040 IF (LEN(Chrono$(9,10))>10 AND LEN(Chrono$(9,10))=12) THEN
7050 IF VAL(Chrono$(11,12))>59 THEN
7060 BEEP
7070 PRINT "Incorrect seconds value."
7080 GOTO Ask
7090 END IF
7100 Day$=Day$&Chrono$(11,12)
7110 ELSE
7120 Day$=Day$&"00"
7130 END IF
7140 SET TIME TIME (Day$)
7150 Clear_crt
7160 SUBEXIT
7170 SUBEND
7180 !
7190 !*****
7200 !
7210 SUB Fix_errr
7220 SELECT ERRN
7230 CASE ELSE
7240 PRINTER IS CRT
7250 PRINT "ERROR ";ERRN
7260 PRINT ERRMS
7270 PRINT " PROGRAM IS PAUSED. FIX ERROR, IF POSSIBLE, AND CONTINUE."
7280 PAUSE
7290 END SELECT
7300 SUBEND
7310 !
7320 !*****
7330 !
7340 SUB Clear_crt(OPTIONAL INTEGER Start_line,Num_of_lines)
7350 !
7360 INTEGER I
7370 DIM Clear_line$(80)
7380 Clear_line$=""
7390 IF NPAR=0 THEN
7400 OUTPUT KBD;CHRS(255)&CHRS(75);
7410 ELSE
7420 PRINT TABXY(1,Start_line);"";RPTS(Clear_line$,Num_of_lines)
7430 PRINT TABXY(1,Start_line);"";
7440 SUBEXIT
7450 END IF
7460 SUBEND
7470 !
7480 !*****
7490 !

```

```
7500 SUB Print_banner1
7510 Clear_crt
7520 PRINT
7530 PRINT
7540 PRINT TABXY(3,16);"*****"
7550 PRINT TABXY(4,16);"*****"
7560 PRINT TABXY(5,16);"*****"
7570 PRINT TABXY(6,16);"*****"
7580 PRINT TABXY(7,16);"*****"
7590 PRINT TABXY(8,16);"*****"
7600 PRINT TABXY(9,16);"*****"
7610 PRINT TABXY(10,16);"*****"
7620 PRINT TABXY(11,16);"*****"
7630 PRINT TABXY(12,16);"*****"
7640 SUBEXIT
7650 SUBEND
7660 !
7670 !
7680 !
7690 SUB Print_banner2
7700 PRINT "Don't use Print_banner2."
7710 SUBEND
7720 !
7730 !
7740 !
7750 SUB Print_banner3
7760 PRINT "Don't use Print_banner3."
7770 SUBEND
7780 !
7790 !
7800 !
7810 SUB Print_banner4
7820 COM /Paths/ @Nwa,@Nwa_data1,@Nwa_data2,Network_analyzer,@Hpb,@Relay
7830 COM /Constants/ Vel_zero(*),Exec_key$
7840 COM /System config/ INTEGER Printer_flag,Debug_flag,Version$,Mode$,Out_type$,Soun
d$,Bell$,Target$,Ref_target$
7850 COM /Sys_1/ Freq$(*),Freq_cent(*),Freq_span(*),Gate_cent(*),Gate_span(*)
7860 COM /Sys_2/ Pol$(*),Polsw$(*)
7870 COM /Sys_3/ INTEGER F_disp,P_disp
7880 COM /Sys_4/ Drive_a$,Drive_b$,Drive_c$,INTEGER Preamble,Bytes
7890 COM /Sys_5/ INTEGER Nskip,Ndata
7900 COM /Sys_6/ Ref_angle,Angle$,Beam(*),INTEGER Npts,Ntrace,Average_factor
7910 COM /Sys_7/ INTEGER Meas_flag(*)
7920 !
7930 !
7940 OFF KEY
7950 Clear_crt
7960 PRINT
7970 PRINT
7980 PRINT
7990 PRINT
8000 PRINT
8010 FOR F=1 TO 3
8020 IF Meas_flag(F) THEN PRINT Freq$(F) & " ";
8030 NEXT F
8040 PRINT
8050 PRINT
8060 PRINT
8070 PRINT
8080 PRINT
8090 ! PRINT
!sp);
8100 PRINT
8110 PRINT

8120 PRINT " # OF SAMPLE POINTS ";Npts
8130 PRINT " # OF DATA POINTS ";Ndata
8140 PRINT " (to be stored)"
8150 PRINT " # OF AVERAGES ";Average_factor
8160 SUBEXIT
8170 SUBEND
8180 !
8190 !
8200 !
8210 SUB Store_file(COMPLEX Matrix(*),File_type$,Filename$,INTEGER F)
!
COM /Sys_1/ Freq$(*),Freq_cent(*),Freq_span(*),Gate_cent(*),Gate_span(*)
COM /Sys_2/ Pol$(*),Polsw$(*)
COM /Sys_5/ INTEGER Nskip,Ndata
COM /Sys_6/ Ref_angle,Angle$,Beam(*),INTEGER Npts,Ntrace,Average_factor
COM /Sys_7/ INTEGER Meas_flag(*)
COM /System config/ INTEGER Printer_flag,Debug_flag,Version$,Mode$,Out_type$,S
und$,Bell$,Target$,Ref_target$
8290 !
8300 !
8310 INTEGER Records_per_set,I
8320 REAL Bytes_per_set
8330 DIM Suffix$(2)
8340 ALLOCATE COMPLEX Trace(Ndata)
8350 !
8360 !
8370 DISP "Saving file."
8380 SELECT File_type$
CASE ="SKY" ! Sky data.
Bytes_per_set=16*Ndata
Records_per_set=4*SUM(Meas_flag)*Ntrace
IF SUM(Meas_flag)=3 THEN
Suffix$="SA"
ELSE
FOR F=1 TO 3
IF Meas_flag(F)=1 THEN
Mf=F
END IF
NEXT F
Suffix$=S&FREQ$(Mf)
END IF
GOSUB Save_hpux
GOSUB Save_traces
!
!
CASE ="REF"
Bytes_per_set=16*Ndata
Records_per_set=4*SUM(Meas_flag)*Ntrace
IF SUM(Meas_flag)=3 THEN
Suffix$="RA"
ELSE
FOR F=1 TO 3
IF Meas_flag(F)=1 THEN
Mf=F
END IF
NEXT F
Suffix$="R"&FREQ$(Mf)
END IF
GOSUB Save_hpux
GOSUB Save_traces
!
!
CASE ="MNT"
Bytes_per_set=16*Ndata
8740
```

```

8750 Records_per_set=4*SUM(Meas_flag)*Ntrace
8760 IF SUM(Meas_flag)=3 THEN
8770   Suffix$="MA"
8780 ELSE
8790   FOR F=1 TO 3
8800     IF Meas_flag(F)=1 THEN
8810       Mf=F
8820     END IF
8830   NEXT F
8840   Suffix$="M"&Freq$(Mf)
8850 END IF
8860 GOSUB Save_hpux
8870   GOSUB Save_traces
8880   !
8890   !
8900 CASE ="GND"
8910   Bytes_per_set=16*Ndata
8920   Records_per_set=Ntrace*4*SUM(Meas_flag)
8930   IF SUM(Meas_flag)=3 THEN
8940     Suffix$="GA"
8950   ELSE
8960     FOR F=1 TO 3
8970       IF Meas_flag(F)=1 THEN
8980         Mf=F
8990       END IF
9000     NEXT F
9010     Suffix$="G"&Freq$(Mf)
9020   END IF
9030   GOSUB Save_hpux
9040   GOSUB Save_traces
9050 END SELECT
9060 DEALLOCATE Trace(*)
9070 SUBEXIT
9080   !
9090   !
9100 Save_averaged: ! Save the reference data file.
9110   !
9120   !
9130 IF NOT Debug_flag THEN
9140   CREATE BDAT Filename$&Suffix$&Drive_c$,Records_per_set,Bytes_per_set
9150 END IF
9160 Base_record=0
9170 FOR F=1 TO 3
9180   IF Meas_flag(F)=1 THEN
9190     IF Debug_flag THEN
9200       ASSIGN @Disc TO PRT
9210       OUTPUT @Disc;"FILE: ",Filename$,Suffix$
9220       OUTPUT @Disc USING Image_1;Versions$,Freq_cent(F),Freq_span(F)
9230       OUTPUT @Disc USING Image_2;Ndata,Average_factor
9240       OUTPUT @Disc USING Image_3;Ref_target$,T
9250       FOR P=1 TO 4
9260         OUTPUT @Disc USING Image_4;Pol$(P),Gate_cent(F),Gate_span(F)
9270         MAT Trace= Matrix(1,P,*)
9280         OUTPUT @Disc;Trace(*)
9290       NEXT P
9300     ELSE
9310       ASSIGN @Disc TO Filename$&Suffix$&Drive_c$;FORMAT OFF
9320       OUTPUT @Disc,Base_record+1;Versions$,Freq_cent(F),Freq_span(F)
9330       OUTPUT @Disc,Base_record+1;Ndata,Average_factor
9340       OUTPUT @Disc,Base_record+1;Ref_target$,T
9350       FOR P=1 TO 4
9360         OUTPUT @Disc,Base_record+P;Pol$(P),Gate_cent(F),Gate_span(F)
9370         MAT Trace= Matrix(1,P,*)
9380         OUTPUT @Disc,Base_record+P;Trace(*)

```

```

9390 NEXT P
9400   Base_record=Base_record+4
9410 END IF
9420 END IF
9430 NEXT F
9440 ASSIGN @Disc TO *
9450 RETURN
9460 !
9470 !-----
9480 !
9490 Save_hpux: ! Save data in HP-UX format.
9500   !
9510   !
9520   IF NOT Debug_flag THEN
9530     CREATE Filename$&Suffix$&Drive_c$,240000
9540   END IF
9550   IF Debug_flag THEN
9560     ASSIGN @Disc TO PRT
9570     FOR T=1 TO Ntrace
9580       FOR F=1 TO 3
9590         IF Meas_flag(F)=1 THEN
9600           FOR P=1 TO 4
9610             MAT Trace= Matrix(T,P,*)
9620             OUTPUT @Disc;Trace(*)
9630           NEXT P
9640         END IF
9650       NEXT F
9660     NEXT T
9670   ELSE
9680     ASSIGN @Disc TO Filename$&Suffix$&Drive_c$;FORMAT ON
9690     FOR T=1 TO Ntrace
9700       FOR F=1 TO 3
9710         IF Meas_flag(F)=1 THEN
9720           FOR P=1 TO 4
9730             MAT Trace= Matrix(T,P,*)
9740             OUTPUT @Disc;Trace(*)
9750           NEXT P
9760         END IF
9770       NEXT F
9780     NEXT T
9790   END IF
9800   ASSIGN @Disc TO *
9810   RETURN
9820 !
9830 !-----
9840 !
9850 Save_traces: ! Save the ground target data file.
9860   !
9870   !
9880   IF NOT Debug_flag THEN
9890     CREATE BDAT Filename$&Suffix$&Drive_c$,Records_per_set,Bytes_per_set
9900   END IF
9910   !
9920   !
9930   IF Debug_flag THEN
9940     ASSIGN @Disc TO PRT
9950     OUTPUT @Disc;"FILE: ",Filename$,Suffix$
9960     OUTPUT @Disc USING Image_5;Ndata,Ntrace
9970     OUTPUT @Disc USING Image_3;Target$
9980     FOR T=1 TO Ntrace
9990       FOR F=1 TO 3
10000         IF Meas_flag(F)=1 THEN
10010           OUTPUT @Disc USING Image_1;Versions$,Freq_cent(F),Freq_span(F)
10020           FOR P=1 TO 4
10030             OUTPUT @Disc USING Image_4;Pol$(P),Gate_cent(F),Gate_span(F),T

```

```
10030 MAT Trace= Matrix(T,P,*)
10040 OUTPUT @Disc;Trace(*)
10050 NEXT P
10060 END IF
10070 NEXT F
10080 NEXT T
10090 ELSE
10100 ASSIGN @Disc TO Filename&Suffix&Drive_c$;FORMAT OFF
10110 OUTPUT @Disc,1;Ndata,Ntrace
10120 OUTPUT @Disc,1;Targets$
10130 FOR T=1 TO Ntrace
10140   FOR F=1 TO 3
10150     IF Meas_flag(F)=1 THEN
10160       OUTPUT @Disc,Base_record+1;Versions,Freq_cent(F),Freq_span(F)
10170       FOR P=1 TO 4
10180         OUTPUT @Disc,Base_record+P;Poi$(P),Gate_cent(F),Gate_span(F),T
10190         MAT Trace= Matrix(T,P,*)
10200         OUTPUT @Disc,Base_record+P;Trace(*)
10210       NEXT P
10220       Base_record=Base_record+4
10230     END IF
10240     NEXT F
10250   NEXT T
10260 END IF
10270 ASSIGN @Disc TO *
10280 RETURN
10290 !
10300 !-----
10310 !
10320 Image_1:IMAGE (1X,12A,5X,"FREQ CENTER: ",2D,4D,5X,"FREQ SPAN: ",2D,4D)
10330 Image_2:IMAGE ("NUMBER OF POINTS: ",5D,5X,"NUMBER OF AVERAGES: ",5D)
10340 Image_3:IMAGE ("TARGET: ",30A,"GATING TARGET TYPE: ",2D)
10350 Image_4:IMAGE ("POLARIZATION: ",2A,5X,"GATE CENTER: ",SD,14DE,/,5X,"GATE SPAN: ",S
D,14DE,"TRACE: ",3D)
10360 Image_5:IMAGE ("NUMBER OF POINTS: ",5D,5X,"NUMBER OF TRACES: ",5D)
10370 Image_6:IMAGE (5X,SD,14DE,5X,SD,14DE)
10380 SUBEND
10390 !
10400 !*****
10410 !
10420 SUB Freq_set(INTEGER Ifreq)
10430 COM /Paths/ @Nwa,@Nwa_data1,@Nwa_data2,Netwrk_analyzer,@Hplb,@Relay
10440 COM /Sys_1/ Freq$(*),Freq_cent(*),Freq_span(*),Gate_cent(*),Gate_span(*)
10450 !
10460 ! This subroutine sets the transmit frequency for the HP8753.
10470 !
10480 IF Ifreq=1 THEN
10490   OUTPUT @Nwa;"POWER0"
10500 ELSE
10510   OUTPUT @Nwa;"POWER-10"
10520 END IF
10530 SELECT Netwrk_analyzer
10540   CASE -3,-4,-5,-6
10550     OUTPUT @Nwa;"TIMDTRANOFF;"
10560   CASE -1,-2
10570     OUTPUT @Nwa;"FREQ;"
10580 END SELECT
10590 OUTPUT @Nwa;"CENT "&VAL$(Freq_cent(Ifreq))&" GHZ;"
10600 OUTPUT @Nwa;"SPAN "&VAL$(Freq_span(Ifreq))&" GHZ;"
10610 SUBEND
10620 !
10630 !*****
10640 !
10650 SUB Freq_sw(INTEGER Ifreq)
10660 COM /Paths/ @Nwa,@Nwa_data1,@Nwa_data2,Netwrk_analyzer,@Hplb,@Relay
10670 SELECT Ifreq
10680 CASE 1
10690   OUTPUT @Relay;"?A2B1"
10700 CASE 2
10710   OUTPUT @Relay;"?A1B2"
10720 CASE 3
10730   OUTPUT @Relay;"?B12"
10740 END SELECT
10750 WAIT .1
10760 SUBEND
10770 !
10780 !*****
10790 !
10800 SUB Pol_sw(INTEGER Ifreq,Ipol)
10810 COM /Paths/ @Nwa,@Nwa_data1,@Nwa_data2,Netwrk_analyzer,@Hplb,@Relay
10820 COM /Sys_1/ Freq$(*),Freq_cent(*),Freq_span(*),Gate_cent(*),Gate_span(*)
10830 COM /Sys_2/ Poi$(*),PoiSw$(*)
10840 !
10850 ! This subroutine sets the transmit and receive polarization by
10860 ! sending the proper command over the HP1B to the polarization
10870 ! relays.
10880 !
10890 OUTPUT @Relay;PoiSw$(Ifreq,Ipol)
10900 OUTPUT @Nwa;"ITTL " " &Freq$(Ifreq)&" BAND - "&Poi$(Ipol)&"****
10910 WAIT .1
10920 SUBEND
10930 !
10940 !*****
10950 !
10960 SUB Rotate_target
10970 OPTON BASE 1
10980 COM /Com4/ INTEGER Rotation_state,REAL Inc_angle,Current_angle,Start_angle,Stop_angle,Old_home_angle,INTEGER Sets_per_pos
le,Old_home_angle,INTEGER Sets_per_pos
10990 COM /Status/ INTEGER Sc,Connect_flg,E_flg,Debug_flg,Response$(80)
11000 INTEGER Fs_flag,Ss_flag,Speed,Imc_status,Confirm_answer
11010 !
11020 !
11030 Confirm_answer=1
11040 Imc_status=0
11050 Debug_flg=0
11060 Fs_flag=1
11070 Ss_flag=1
11080 Clear_crt(3,16)
11090 !
11100 !
11110 SELECT Rotation_state
11120 CASE =-1
11130   IF FNASK("Do you wish to use the rotator?") THEN
11140     Connect_flg=0
11150     GOSUB Init_Imc
11160     GOSUB Init_graph_pos
11170     GOSUB Manual_loop
11180     PRINT "Set Auto Mode Please....."
11190   ELSE
11200     Rotation_state=0
11210     GCLEAR
11220     GRAPHICS OFF
11230   END IF
11240 CASE =0
11250   SUBEXIT
11260 CASE =1
11270   GOSUB Check_position
11280   GOSUB Print_angles
```

```

11290 GOSUB Manual_loop
11300 CASE =2
11310 GOSUB Check_position
11320 GOSUB Auto
11330 CASE =3
11340 GOSUB Check_position
11350 GOSUB Manual_loop
11360 GOSUB Auto
11370 CASE =4
11380 GOSUB Check_position
11390 GOSUB Go_home
11400 CASE =5
11410 GOSUB Check_position
11420 Rotation_state=1 ! Switch to manual mode.
11430 END SELECT
11440 SUBEXIT
11450 !
11460 !
11470 Init_imc: ! Initialize the IMC unit.
11480 GOSUB Check_4_fault
11490 PRINT TABXY(1,3);"INITIALIZING IMC"
11500 Clear_crt(4,15)
11510 Comm("4WB") ! Set warm boot (clear flags).
11520 PRINT TABXY(1,4);"WB"
11530 Comm("4EB") ! Clear IMC buffer.
11540 PRINT TABXY(1,4);"EB"
11550 Encoder_ratio=4096 ! 32000
11560 Comm("4ER"&VAL$(Encoder_ratio)) ! Load encoder ratio.
11570 PRINT TABXY(1,4);"ER"&VAL$(Encoder_ratio)
11580 IF FNAask("Do you wish to set home at the current position?") THEN
11590 Comm("4RS",Confirm_answer)
11600 ENTER Responses;Old_home_angle
11610 Old_home_angle=Old_home_angle/93.3
11620 Comm("4PIZ0") ! Set IMC at 0.
11630 PRINT TABXY(1,4);"PIZ"&RPT$( " ",LEN(VAL$(Encoder_ratio)))
11640 Comm("4PIA0") ! Set IMC at 0.
11650 PRINT TABXY(1,4);"PIA"
11660 Current_angle=0
11670 END IF
11680 Comm("4SP100") ! Set speed to (50pps) .
11690 PRINT TABXY(1,4);"SP "&RPT$( " ",LEN(VAL$(Encoder_ratio)))
11700 Comm("4AC500") ! Set acceleration (500pps^2).
11710 PRINT TABXY(1,4);"AC "
11720 Comm("4DC500") ! Set deceleration (500pps^2).
11730 PRINT TABXY(1,4);"DC "
11740 GOSUB Check_position
11750 Rotation_state=1
11760 Clear_crt
11770 !
11780 !
11790 PRINT TABXY(1,4);"DONE INITIALIZING IMC"
11800 PRINT TABXY(1,5);"Turntable currently in manual mode."
11810 PRINT TABXY(1,6)
11820 Print_angles: !
11830 PRINT TABXY(1,7);"Current angle is: ";Current_angle;" degrees."
11840 PRINT TABXY(1,8);"Starting angle is: ";Start_angle;" degrees."
11850 PRINT TABXY(1,9);"Stopping angle is: ";Stop_angle;" degrees."
11860 RETURN
11870 !
11880 !
11890 Manual_loop: ! Main activation loop.
11900 LOOP
11910 ON KEY 0 LABEL "FAST SLEW CW ",FNTrap_level GOSUB Fs_cw
11920 ON KEY 1 LABEL "FAST SLEW CCW ",FNTrap_level GOSUB Fs_ccw

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11930 ON KEY 5 LABEL "SLOW SLEW CW ",FNTrap_level GOSUB Ss_cw
11940 ON KEY 6 LABEL "SLOW SLEW CCW ",FNTrap_level GOSUB Ss_ccw
11950 ON KEY 2 LABEL "MANUAL CONTROL",FNTrap_level GOSUB Manual
11960 ON KEY 3 LABEL "TARGET GO HOME",FNTrap_level GOSUB Go_home
11970 ON KEY 4 LABEL "STOP ROTATION ",FNTrap_level GOSUB Stop_turn
11980 ON KEY 7 LABEL "SET AUTO MODE ",FNTrap_level GOSUB Set_auto
11990 ON KEY 8 LABEL "SET TARGET HOME",FNTrap_level GOSUB Set_home
12000 ON KEY 9 LABEL "RETURN ",FNTrap_level GOTO Quit
12010 GOSUB Check_position
12020 END LOOP
12030 !
12040 !
12050 !
12060 Fs_cw: ! Fast slew clockwise.
12070 IF Fs_flag<0 THEN
12080 Comm("4SP500")
12090 Comm("4SFN")
12100 Fs_flag=-1*Fs_flag
12110 Clear_crt(3,15)
12120 PRINT TABXY(1,15);"ROTATING CW (FAST) "
12130 ELSE
12140 Comm("4ST")
12150 Fs_flag=-1*Fs_flag
12160 Clear_crt(3,15)
12170 PRINT TABXY(1,15);"ROTATION STOPPED"
12180 GOSUB Check_position
12190 END IF
12200 RETURN
12210 !
12220 !
12230 !
12240 Fs_ccw: ! Fast slew counterclockwise.
12250 IF Fs_flag<0 THEN
12260 Comm("4ST")
12270 Comm("4SP500")
12280 Comm("4SRN")
12290 Fs_flag=-1*Fs_flag
12300 Clear_crt(3,10)
12310 PRINT TABXY(1,15);"ROTATING CCW (FAST) "
12320 ELSE
12330 Comm("4ST")
12340 Fs_flag=-1*Fs_flag
12350 Clear_crt(3,15)
12360 PRINT TABXY(1,15);"ROTATION STOPPED"
12370 GOSUB Check_position
12380 END IF
12390 RETURN
12400 !
12410 !
12420 !
12430 Ss_cw: ! Slow slew clockwise.
12440 IF Ss_flag<0 THEN
12450 Comm("4ST")
12460 INPUT "Speed? ",Sp
12470 Comm("4SP"&VAL$(INT(Sp)))
12480 Comm("4SFN")
12490 Ss_flag=-1*Ss_flag
12500 Clear_crt(3,15)
12510 PRINT TABXY(1,15);"ROTATING CW (SLOW) "
12520 ELSE
12530 Comm("4ST")
12540 Ss_flag=-1*Ss_flag
12550 Clear_crt(3,15)
12560 PRINT TABXY(1,15);"ROTATION STOPPED"

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12570 GOSUB Check_position
12580 END IF
12590 RETURN
12600 !-----
12610 !
12620 !
12630 Ss_ccw:; Slow slew counterclockwise.
12640 IF Ss_flag<0 THEN
12650 INPUT "Speed?" ,Sp
12660 Comm("4SP"&VAL$(INT(Sp)))
12670 Comm("4SRN")
12680 Ss_flag=-1*Ss_flag
12690 Clear crt(3,15)
12700 PRINT TABXY(1,15);"ROTATING CCW (SLOW)"
12710 ELSE
12720 Comm("4ST")
12730 Ss_flag=-1*Ss_flag
12740 Clear crt(3,15)
12750 PRINT TABXY(1,15);"ROTATION STOPPED"
12760 GOSUB Check_position
12770 END IF
12780 RETURN
12790 !-----
12800 !
12810 !
12820 Manual: INPUT "ANGLE (IN DEGREES)=?",Inc_angle
12830 INPUT "SPEED? (-100--500 RECOMMENDED) ",Speed
12840 Comm("4SP"&VAL$(Speed))
12850 SELECT Rotation_state
12860 CASE =4
12870 GOSUB Go_home
12880 Rotation_state=2
12890 GOTO Auto
12900 CASE ELSE
12910 Angl2=Inc_angle*93.3
12920 Angl1=INT(Angl2)
12930 IF Angl2-Angl1>=.5 THEN Angl1=Angl1+1
12940 Current_angle=Current_angle+Inc_angle
12950 Inc_angle$=VAL$(Angl1)
12960 Comm("4IM"&Inc_angle$)
12970 Comm("4RFI")
12980 END SELECT
12990 Imc_status=0
13000 Clear crt(3,7)
13010 PRINT TABXY(1,14);"ROTATING TARGET, PLEASE WAIT."
13020 !-----
13030 !
13040 WHILE NOT BIT(Imc_status,0)
13050 Comm("4RS",Confirm_answer)
13060 ENTER Responses;Imc_status
13070 PRINT TABXY(1,15);DVAL$(Imc_status,2)
13080 GOSUB Check_position
13090 WAIT 1
13100 END WHILE
13110 Imc_status=0
13120 !-----
13130 !
13140 Clear crt(3,16)
13150 PRINT TABXY(1,16);"CURRENT TARGET POSITION IS ";Current_angle;" DEGREES."
13160 WAIT 2 ! Wait for target settling.
13170 RETURN
13180 !-----
13190 !
12570 !
12580 Stop_turn:Comm("4ST")
12590 WHILE NOT BIT(Imc_status,0)
12600 Comm("4RS",Confirm_answer)
12610 ENTER Responses;Imc_status
12620 WAIT .1
12630 END WHILE
12640 Clear crt(3,16)
12650 PRINT TABXY(1,15);"ROTATION STOPPED"
12660 GOSUB Check_position
12670 Imc_status=0
12680 RETURN
12690 !-----
12700 !
12710 !
12720 Set_auto: Comm("4SP500")
12730 GOSUB Check_position
12740 Clear crt(3,16)
12750 PRINT TABXY(1,3);"Current starting angle: ";Start_angle;" degrees"
12760 PRINT TABXY(1,4);"Current increment angle: ";Inc_angle;" degrees"
12770 PRINT TABXY(1,5);"Current stopping angle: ";Stop_angle;" degrees"
12780 PRINT TABXY(1,6);"Current rotation speed: ";Speed
12790 PRINT TABXY(1,7);RPTS(" ",80)
12800 PRINT TABXY(1,8);"Rotator positioned at: ";Current_angle;" degrees"
12810 INPUT "Enter starting angle value (degrees): ",Start_angle
12820 INPUT "Enter increment angle (degrees): ",Inc_angle
12830 INPUT "Enter stopping angle (degrees): ",Stop_angle
12840 INPUT "Enter rotation speed of target (-500 recommended): ",Speed
12850 Speed=INT(Speed)
12860 Comm("4SP"&VAL$(Speed))
12870 IF ABS(Start_angle-Current_angle)>.1 THEN
12880 PRINT TABXY(1,9);RPTS(" ",80)
12890 PRINT TABXY(1,10);"Rotating target to starting angle..."
12900 Temp_angle=Inc_angle
12910 Inc_angle=Start_angle-Current_angle
12920 GOSUB Auto
12930 Inc_angle=Temp_angle
12940 END IF
12950 Rotation_state=2
12960 Clear crt
12970 PRINT TABXY(1,20);"Turntable is in automatic mode. (press the RETURN eof
12980 RETURN
12990 !-----
13000 !
13010 Set_position:INPUT "LOCK IN CURRENT TARGET POSITION AS REFERENCE POSITION?",Yn$
13020 IF Yn$="y" OR Yn$="Y" THEN
13030 Comm("4RS",Confirm_answer)
13040 ENTER Responses;Old_home_angle
13050 Old_home_angle=Old_home_angle/93.3
13060 Comm("4PIA0") ! Set absolute position to zero.
13070 Comm("4PI20") ! Set incremental position to zero.
13080 Current_angle=0
13090 ELSE
13100 PRINT "POSITION WAS NOT SET."
13110 END IF
13120 RETURN
13130 !-----
13140 !
13150 Go_home: IF Speed<200 THEN Speed=200
13160 Comm("4SP"&VAL$(Speed))
13170 Comm("4AM0") ! Move to zero absolute position.
13180 RETURN
13190 !-----

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13830 Comm("4RAN") ! Initiate movement.
13840 Comm("4MW") ! Make sure the move is completed.
13850 Imc_status=0
13860 Clear_crt(3,15)
13870 PRINT TABXY(1,14);"ROTATING TARGET TO HOME POSITION, PLEASE WAIT."
13880 WHILE NOT (BIT(Imc_status,0) AND BIT(Imc_status,5))
13890 GOSUB Check_status
13900 PRINT TABXY(1,15);"CURRENT STATUS: ";DVAL$(Imc_status,2)
13910 GOSUB Check_position
13920 WAIT .1
13930 END WHILE
13940 Clear_crt(3,16)
13950 PRINT TABXY(1,15);"TARGET AT HOME POSITION."
13960 GOSUB Check_position
13970 Imc_status=0
13980 RETURN
13990 ! -----
14000 ! -----
14010 ! -----
14020 Check_status: ! Keep an eye on the Whedco controller status.
14030 Comm("4RS",Confirm_answer)
14040 ENTER Response$;Imc_status
14050 RETURN
14060 ! -----
14070 ! -----
14080 ! -----
14090 Check_position: ! Get the current turnstile position in degrees.
14100 Comm("4RP",Confirm_answer)
14110 ENTER Response$;Motor_position
14120 Current_angle=Motor_position/93.3
14130 ! Current_angle=Current_angle+inc_angle
14140 PRINT TABXY(1,16);"CURRENT TARGET POSITION IS ";Current_angle;" DEGREES."
14150 GOSUB Draw_positions
14160 RETURN
14170 ! -----
14180 ! -----
14190 ! -----
14200 Check_4_fault: ! Check the IMC for a fault condition and correct or
14210 ! notify the user if necessary.
14220 !
14230 Comm("4FC",Confirm_answer)
14240 ENTER Response$;Fault$
14250 SELECT Fault$
14260 CASE ="Power failure" ! Loss of power
14270 RETURN
14280 CASE ="Force DAC" ! Force DAC command was given
14290 BEEP
14300 PRINT "Force DAC command was given..."
14310 DISP "Press CONTINUE to resume..."
14320 PAUSE
14330 RETURN
14340 CASE ="Over-current" ! Over-current condition exists.
14350 BEEP
14360 PRINT "An over-current condition has been detected on the IMC."
14370 PRINT
14380 PRINT "Cycle the power to the IMC until the OV-CUR LED goes out"
14390 DISP "Press CONTINUE to reinitialize the IMC"
14400 PAUSE
14410 GOSUB Init_imc
14420 RETURN
14430 END SELECT
14440 RETURN
14450 ! -----

```

```

14460 ! -----
14470 ! -----
14480 Init_graph_pos: ! Creates a graphical depiction of where the target is.
14490 GINIT
14500 GCLEAR
14510 GRAPHICS ON
14520 SHOW 0,100,0,100
14530 PENUP
14540 MOVE 90,70
14550 PEN 1 ! Draw circle
14560 POLYGON 12,360,360
14570 PENUP
14580 MOVE 90,70 ! Draw old home orientation.
14590 PEN 2
14600 DRAW 90+11*COS(Old_home_angle),70-11*SIN(Old_home_angle)
14610 PENUP
14620 MOVE 90,70 ! Draw current home orientation.
14630 PEN 4
14640 DRAW 90,58
14650 PENUP
14660 MOVE 90,70 ! Draw current target orientation.
14670 PEN 3
14680 X_pos=90+11*COS(Current_angle)
14690 Y_pos=70-11*SIN(Current_angle)
14700 DRAW X_pos,Y_pos
14710 RETURN
14720 ! -----
14730 ! -----
14740 ! -----
14750 ! -----
14760 Draw_positions: ! Draws out the angular orientations.
14770 MOVE 90,70 ! Draw old home orientation.
14780 PEN 2
14790 DRAW 90-11*SIN(Old_home_angle),70-11*COS(Old_home_angle)
14800 PENUP
14810 MOVE 90,70 ! Draw current home orientation.
14820 PEN 4
14830 DRAW 90,58
14840 PENUP
14850 DISABLE
14860 MOVE 90,70 ! Draw current target orientation.
14870 PEN -3
14880 DRAW X_pos,Y_pos
14890 MOVE 90,70
14900 PEN 3
14910 X_pos=90-11*SIN(Current_angle)
14920 Y_pos=70-11*COS(Current_angle)
14930 DRAW X_pos,Y_pos
14940 PENUP
14950 ENABLE
14960 RETURN
14970 ! -----
14980 ! -----
14990 ! -----
15000 Quit: !
15010 SUBEXIT
15020 SUBEND
15030 ! -----
15040 ! *****
15050 ! -----
15060 SUB Comm(C$,OPTIONAL INTEGER Confirm_answer)
15070 !
15080 ! PROGRAM MODULE: Comm
15090 !

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15100 !
15110 ! Modified version of the Comm module to be used
15120 ! for direct two way communication with the WHEDCO
15130 ! IMC stepping motor controller.
15140 !
15150 ! UPDATE: 3.0 Version 3.0 checks to see if the card being used
15160 ! is the HP98628A (Datacomm) or the HP98626A (Serial).
15170 ! Depending on which card is used, the appropriate
15180 ! registers are selected.
15190 !
15200 ! OPTION BASE 1
15210 ! COM /Status/ INTEGER Sc,Connect_flg,E_flg,Debug_flg,Responses$
15220 ! INTEGER Baud_rate,B,Num_chars,Response_flg,Index1
15230 ! DIM Input$(256),Term$(256),In$(256),Buf$,From_232$(256)
15240 ! DIM Num_chars$(6),Num_ltrss$(6),Out$(256) BUFFER
15250 ! DIM White_print$(1),CrLf$(2)
15260 ! IF Debug_flg THEN PRINT TABXY(1,1);"ENTERING Comm "
15270 ! ON ERROR GOSUB Error
15280 !
15290 !
15300 ! IF Connect_flg THEN After_init
15310 ! Sc=30
15320 ! ASSIGN @Find_it TO Sc;RETURN Outcome
15330 ! IF Outcome=0 THEN
15340 ! ASSIGN @Find_it TO *
15350 ! CONTROL Sc,0;1
15360 ! CONTROL Sc,3;1
15370 ! CONTROL Sc,0;1
15380 ! CONTROL Sc,8;1+2
15390 ! CONTROL Sc,16;0
15400 ! CONTROL Sc,1;0
15410 ! CONTROL Sc,18;0
15420 ! CONTROL Sc,19;0
15430 ! CONTROL Sc,20;14
15440 ! CONTROL Sc,21;14
15450 ! CONTROL Sc,22;0
15460 ! CONTROL Sc,23;0
15470 ! CONTROL Sc,34;2
15480 ! CONTROL Sc,35;0
15490 ! CONTROL Sc,36;1
15500 ! Connect_flg=1
15510 ! ELSE
15520 ! Sc=8
15530 ! ASSIGN @Find_it TO *
15540 ! ASSIGN @Find_it TO Sc;RETURN Outcome
15550 ! IF Outcome<>0 THEN
15560 ! PRINT "RS-232 card not installed. Please install and reboot."
15570 ! ASSIGN @Find_it TO *
15580 ! STOP
15590 ! END IF
15600 ! ASSIGN @Find_it TO *
15610 ! RESET Sc
15620 ! CONTROL Sc,0;1
15630 ! CONTROL Sc,3;Baud_rate
15640 ! CONTROL Sc,4;8+2
15650 ! CONTROL Sc,5;3
15660 ! CONTROL Sc,12;128+32+16
15670 ! STATUS Sc,3;B
15680 ! Connect_flg=1
15690 ! END IF
15700 ! After_init:
15710 ! White_print$=CHR$(136)
15720 ! CrLf$=CHR$(13)&CHR$(10)
15730 ! PRINT CHR$(128)&CHR$(136);
! Set up the screen.
15740 !
15750 ! ASSIGN @Screen TO CRT
15760 ! ASSIGN @Kbd TO KBD
15770 ! ASSIGN @Rx TO BUFFER In$
15780 ! ASSIGN @Tx TO BUFFER Out$
15790 ! ASSIGN @Uart_out TO Sc
15800 ! ASSIGN @Uart_in TO Sc
15810 ! Response_flg=0
15820 ! Response$=""
15830 !
15840 ! ENABLE_INTR Sc
15850 ! TRANSFER @Tx TO @Uart_out;CONT
15860 ! TRANSFER @Uart_in TO @Rx
15870 ! ON_INTR Sc,FNTrap_level GOSUB Read_loop
15880 ! IF C$<>" THEN
15890 ! GOSUB Send_com
15900 ! ELSE
15910 ! GOTO Quit
15920 ! END IF
15930 !
15940 !
15950 !
15960 ! Wait_for_it:WHILE NOT Response_flg
15970 ! GOSUB Read_loop
15980 ! IF NPAR=2 THEN
15990 ! LOOP
16000 ! GOSUB Read_loop
16010 ! IF (POS(Response$,"**")) THEN
16020 ! Response$=Response$(POS(Response$,"**"),LEN(Response$))
16030 ! )
16040 ! Response_flg=1
16050 ! END IF
16060 ! EXIT IF ((Response_flg=1) AND (POS(Response$,CrLf$)))
16070 ! END LOOP
16080 ! ELSE
16090 ! WHILE NOT ((POS(Response$,"**")) OR (POS(Response$,"?")))
16100 ! GOSUB Read_loop
16110 ! END WHILE
16120 ! Index1=POS(Response$,"**")
16130 ! IF Index1=0 THEN
16140 ! Must be a "?" (Whedco command error).
16150 ! E_flg=1
16160 ! Response_flg=1
16170 ! ELSE
16180 ! Normal command interpretation.
16190 ! E_flg=0
16200 ! Response_flg=1
16210 ! END IF
16220 ! END IF
16230 ! END WHILE
16240 ! GOTO Quit
16250 !
16260 !
16270 ! Read_loop: Read in serial data from Whedco.
16280 !
16290 ! STATUS @Rx,4;Num_chars
16300 ! IF Num_chars=0 THEN RETURN
16310 ! Num_chars$=#,%VAL$(Num_chars),%A
16320 ! ENTER @Rx USING Num_chars$;From_232$
16330 ! Response$=Response$&From_232$
16340 ! RETURN
16350 !
16360 !

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16370 Send_com:Term$=CrLf$(1,1)&CS&CrLf$
16380 Num_ltr$=#,&VAL$(LEN(Term$))&"A"
16390 OUTPUT @Tx USING Num_ltr$$;Term$
16400 Term$=""
16410 RETURN
16420 !
16430 !
16440 Quit: OFF ERROR
16450 STATUS @Tx,10;Stat
16460 STATUS @Rx,4;Num_bytes
16470 ABORTIO @Uart_out
16480 ASSIGN @Tx TO *
16490 CONTROL @Rx,8;0
16500 STATUS @Rx,10;Stat
16510 STATUS @Rx,4;Num_bytes
16520 ABORTIO @Uart_in
16530 ASSIGN @Rx TO *
16540 DISABLE INTR Sc
16550 SUBEXIT
16560 !
16570 !
16580 Error:PRINT "HANDLING Comm ERROR"
16590 IF ERRN<>167 THEN Other error
16600 IF Sc=8 THEN ! Process the simple card.
16610 STATUS Sc,10;Uart_error
16620 IF BIT(Uart_error,1) THEN Overrun
16630 IF BIT(Uart_error,2) THEN Parity
16640 IF BIT(Uart_error,4) THEN Break1
16650 IF BIT(Uart_error,3) THEN Framing
16660 E_flg=1
16670 PAUSE
16680 RETURN
16690 ELSE
16700 PRINT ERRMS
16710 E_flg=1
16720 PAUSE
16730 RETURN
16740 END IF
16750 !
16760 !
16770 Other: PRINT "UART error status: ";Uart_error
16780 E_flg=1
16790 RETURN
16800 !
16810 !
16820 Overrun:PRINT "Overrun"
16830 E_flg=1
16840 RETURN
16850 !
16860 !
16870 Parity: PRINT "Parity"
16880 E_flg=1
16890 RETURN
16900 !
16910 !
16920 Break1: PRINT "Break"
16930 E_flg=1
16940 RETURN
16950 !
16960 !
16970 Framing:PRINT "Framing"
16980 E_flg=1
16990 RETURN
17000 !
17010 !
17020 Other_error:PRINT "Error message: ";ERRMS
17030 PAUSE
17040 E_flg=1
17050 SUBEXIT
17060 !
17070 !
17080 SUBEND
17090 !
17100 !*****
17110 !

```