ENGINEERING RESEARCH INSTITUTE THE UNIVERSITY OF MICHIGAN ANN ARBOR

CONDENSATION OF FREON-12 IN 11-FINS-PER-INCH AND 19-FINS-PER-INCH COAXIAL COILS

Report No. 46

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OBJECTIVE

The objective of this investigation was to determine the relative performance of a series of six coaxial finned tube coils with Freon-12 condensing in the annulus of the coils.

ABSTRACT

The relative performance of three ll-fin-per-inch coaxial coils of various lengths and three 19-fin-per-inch coils of various lengths were individually determined in a five ton refrigeration system charged with Freon-12. Heat transfer and pressure performance curves are presented for 85, 115, and 135 psig. condensing pressures as a function of various condensing water flow rates.

I. SCOPE OF INVESTIGATION

The object of this investigation was to determine the relative performance of various finned tube coaxial coils when condensing Freon-12 in a five ton refrigeration application. The geometrical and physical features of these coils are described in Section II of this report.

The following aspects of comparison were considered:

- 1. Rates of heat removal with Freon-12 condensing in the annulus of the coils with variation in:
 - a. cooling water flow rate,
 - b. Freon-12 condensing pressures, and
 - c. length of coil.
 - 2. Pressure drop on freon side, and
 - 3. Pressure drop on water side.

The experimentation was conducted in the condensing section of a five ton refrigeration system. Saturated or slightly superheated Freon-12 vapor was fed to the annulus of the coil where it was condensed on the finned side of the inner tube by means of water flowing inside the inner tube.

Many other factors which play an important role in the performance of the coils were not studied in this investigation. These are:

- 1. Outside shape of the coil (i.e., helical, spiral, slope per foot of length), and
- 2. Annulus cross sectional area, internal tube geometry, and external tube geometry.

A quantitative consideration of these factors was beyond the scope of the present study, since it would require a great number of different coils and more elaborate experimental equipment.

II. DESCRIPTION OF COILS

Coaxial coils fabricated with ll-fin-per-inch tubes and 19-fin-per-inch tubes inside of 18 gage 1-1/8 inch bare copper tube approximately twenty-five feet long were originally provided by Wolverine Tube. Pre-liminary studies indicated that the coils would have to be shortened in order to undertake the investigation. The coils were returned to Wolverine Tube for modification. Subsequently coils approximately 4 feet, 6 feet, and 12 feet long were received for investigation. Table I presents detailed information concerning the coils tested.

Figures 1, 2, and 3 show the 4 ft.-7 inch 5 ft.-ll $\frac{1}{2}$ inch, and ll ft.-l0 $\frac{1}{2}$ inch long 19-fin-per-inch coils. Figures 4, 5, and 6 show the 3 ft.-6 $\frac{1}{2}$ inch, 6 ft.-0 inch, and 12 ft.-8 inch long 11-fin-per-inch coils studied in this investigation. Figures 7 and 8 show cross sections of the ll-fin-per-inch and 19-fin-per-inch coils.

III. DESCRIPTION OF APPARATUS

The equipment used in this investigation was originally fabricated by D. R. Robinson as a Trufin Fellow for his doctoral dissertation in finned tube heat transfer in 1949. The same equipment was later used by J. E. Myers in his doctoral dissertation research also as a Trufin Fellow. This apparatus, consisting essentially of a five ton compressor, a condenser, and an evaporator together with considerable auxiliary equipment, had to be modified in many ways to fit the investigation of the performance of the coaxial coils. In essence the coils studied replaced the original condenser used by Robinson and Myers. Figures 9, 10, and 11 show the equipment as modified for this investigation.

Three stream circuits were necessary for the measurements of the heat loads. The first and main circuit contained and handled the Freon-12. The other two circuits consisted of the evaporator water circulation system and the desuperheating and condensing water systems.

A. Freon Circuit.

The Freon circuit flow sheet is shown in Figure 12. The system consisted of the following units: the evaporator, the compressor and its accessories, the vapor liquid separator, the liquid Freon seal, the finned tube coaxial coils and an auxiliary condenser.

The Freon gas leaving the evaporator flowed through valve V_2 (see Figure 12) to the suction side of the compressor. The inlet suction pressure was measured by gage P_2 . The Freon in passing through the compressor became contaminated with lubricating oil. The compressed gas was therefore passed through an oil separator. The oil separator was an Aminco Refrigeration Products Company type 820 F separator.

The compressed Freon gas after passing through the oil separator could be admitted through valve V_3 to the coaxial coil condensing system or through valve V_4 to the auxiliary condenser. The auxiliary condenser was seldom used. The vapor was desuperheated in a concentric pipe heat exchanger to a predetermined level.

All of the runs at a given inlet coil pressure were conducted at a constant inlet Freon temperature. At the inlet and outlet of the coil the temperature and pressure T_1 , P_4 and T_2 , P_5 were measured. The condensed Freon then passed to a liquid seal unit. This liquid seal was fabricated from a piece of 4 in. pipe about 14 in. long. It was fitted with a vent valve through which noncondensibles could be bled and a sight glass tube was provided along the side of the unit. The condensate then returned through a vapor liquid separator back to the evaporator.

The compressor used was a five ton carrier type 5F-30 model, operating three cylinders at 1750 rpm from a 5 hp drive. The unit was equipped with an automatic low and high pressure shut off switch, and an automatic oil safety switch which shut off the compressor whenever the difference between the oil pressure and suction pressure became less than about 45 psig.

The evaporator had a rectangular cross sectional shape. It measured 17-3/8 in. high by 7-14 in. wide by 39 in. long inside and was fabricated of 1/2 in. steel plate. It was fitted with a safety valve set to relieve at 150 psig, a pressure gage P_1 , and three bull's eye sight glasses welded into the sides at three different levels. These windows were used to observe the Freon liquid level. A tube bundle of 16 gage 3/4 in. copper tubes was used in the evaporator. Through these tubes water was circulated to provide the necessary latent heat of evaporation and keep the evaporator pressure at a predetermined level. The auxiliary condenser was a water cooled multipass unit containing finned tubes.

Figure 9 shows the following units:

- A. Coaxial Coil
- B. Five Ton Compressor
- C. Auxiliary Condenser
- D. Vapor-Liquid Separation

Figure 10 shows the following units:

- E. The Evaporator
- F. Hot Water Surge Tank
- G. Evaporator Water Recirculation Pump
- H. Evaporator Tube Bank Exit Section
- M. Evaporator Water Preheater

Figure 11 shows the following units:

- I. Liquid Seal Unit
- J. Condensing Water Pre-Heater
- K. Oil Separator
- L. Freon Vapor Desuperheater

B. Auxiliary Circuits

1. Evaporator Water Circuit.

The evaporator water circuit is shown in Figure 10. The heat of evaporation was provided by recirculated warm water. The circuit consists of a surge tank F, a pump G, and a pre-heater M.

The discharge from the pump was divided into two streams, one going to the evaporator and the other bypassed to the suction side of the pump for capacity control. The water was then returned to the surge tank. The pump took suction from the storage tank through a small stream heater.

2. Condenser Cooling Water Circuit.

Cooling water for the condensing coil was admitted from the main to a vertical heat exchanger (Unit J of Fig. 11) where it was preheated by means of steam to a constant temperature of 22°C. It was then admitted to the coil. Both the inlet and outlet temperatures were measured (T_1 and T_2 of Fig. 12). The rate of flow was determined by collecting and weighing the water in a weigh barrel for a certain period of time.

3. Freon Desuperheating Circuit.

Part of the Freon line at the inlet of the coil was jacketed and cooled by water coming from the water main. The flow rate of water required for the desired desuperheating was manually controlled by means of valves.

IV. PROCEDURE

A typical run consisted of operating the system under predetermined conditions such that the inlet Freon to the coaxial coil was entering at either 85, 115, or 135 psig. At the same time the condensing water flow rate was set at a predetermined value, always adjusting and holding the inlet water temperature at 22°C. The Freon was partially desuperheated before entering the coaxial coil.

In starting up, both water circuits were turned on and the co-axial coil inlet condensing water was adjusted to 22°C. The next step consisted of setting all valves in the Freon circuit following a sequence. The prescribed sequence prevented any liquid Freon from accumulating in the compressor crankcase and also prevented loss of oil from the crankcase into the Freon circuit. The compressor was started up and the pressure of the

Freon at the inlet of the coil was set at the prescribed level by valve $\rm V_2$ of Figure 12. The pressure in the evaporator was held close to 50 psig by controlling the temperature and flow rate of the evaporator tube side water.

Measurements:

When the inlet water temperature to the coil read 22°C for the given water flow rate the following steps were taken.

The amount of superheat of the Freon vapor was reduced to approximately 5°C by controlling the rate of water flow in the desuperheater.

The water rate flowing through the coaxial coil was then measured using a weigh barrel. The inlet and outlet Freon and water temperatures and pressures were read. The pressure at the evaporator and the compressor outlet pressure were also recorded.

For a given water flow rate a series of runs at different condensing Freon pressures were taken. For these runs no adjustment of the inlet water temperature was needed. It was necessary, however, to readjust the Freon inlet temperature, and the pressure at the evaporator.

The condensing water flow rate was then changed and a new series of runs at different inlet Freon condensing pressures was taken.

V. RESULTS AND DISCUSSION OF RESULTS

The experimental method used followed closely, but not exactly for reasons mentioned below, the condenser water method described in Section 26 of the A.S.R.E. Standard Methods for Testing Mechanical Condensing Units, prepared and approved by the A.S.R.E. Council June 11, 1940 (A.S.R.E. Standard 14-41).

The following measurements were taken for each run:

- 1. Pressure of vapor refrigerant entering condenser coil,
- 2. Temperature of vapor refrigerant entering condenser coil,
- 3. Pressure of liquid refrigerant leaving condenser coil,
- 4. Temperature of liquid refrigerant leaving condenser coil,
- 5. Temperature of water entering condenser,
- 6. Temperature of water leaving condenser,
- 7. Weight of condenser cooling water per unit time.
- 8. Evaporator pressure.

Three or four consecutive measurements were taken after equilibrium was reached. Not all runs are listed in this report. As indicated earlier in this report, at the beginning of the experimentation period, runs were taken

on smaple coaxial coils whose capacity exceeded the available capacity and load limit of the compressor. These coils were sent back and by request were cut to shorter lengths. Only the runs taken on these shortened coils are recorded in Table No. II. Only the arithmetic average of the four measurements of each run is recorded. The recorded pressures and temperatures include the necessary corrections determined by calibration of the thermometers and pressure gages.

The formula for calculation of the capacity of a condensing unit proposed by A.S.R.E. Standard 14-41 is

$$Q = \frac{(h_{g1} - h_{f1})}{(h_{g3} - h_{f3})} \left[W(t_2 - t_1) + Q_n \right]$$
 (1)

where:

h = heat content of refrigerant liquid leaving condensing unit, in Btu. per lb.

h = heat content of refrigerant liquid leaving the condenser,
in Btu. per lb.

h = heat content of refrigerant vapor entering condensing unit, under the conditions specified in the A.S.R.E. Standard Method of Rating Mechanical Condensing Units, in Btu. per lb.

h_{g3} = heat content of refrigerant vapor entering condenser, in Btu. per lb.

Q = condensing unit capacity, in Btu. per hr.

 Q_n = heat loss from condenser to surrounding air, in Btu. per hr., S $U_a(t_c - t_a)$ approximately.

S = outside surface of condenser, in sq. ft.

U_a = air film heat transfer coefficient, in Btu. per hr. per sq. ft. per *F.

ta = ambient temperature, in °F.

t_c = external surface temperature of condenser, in °F.

t = condenser entering water temperature, in °F.

t₂ = condenser leaving water temperature, in °F.

W = flow of condenser cooling water, in lb. per hr.

The nomenclature used above in formula (1) follows exactly that specified in A.S.R.E. Standard 14-41. This formula was not used in calculating Q. Instead the heat load handled by the coil was calculated as follows:

$$Q = W(t_2 - t_1)$$
 (2)

The reason for this is that Equation 1 applies to the testing of a complete condensing unit. The correction coefficient factor in Equation 1 takes into account the difference in enthalpy of the liquid refrigerant leaving the condenser unit and that of the liquid refrigerant leaving the condenser proper. The investigation described in this report was concerned with the performance of coaxial coils. The results should be independent of the overall setup in which the coaxial coils may be used. This correction factor was therefore not required in this investigation.

It should be noted that the term Q_n was also not used. This term represents the rate of heat loss to the ambient air by convection and radiation from the outside surface of the coil. It can be estimated that under the most unfavorable conditions that could be encountered in the course of the experimentation, this heat loss represented at most 3 percent of the total heat capacity Q. As explained below, other factors affect the performance to a greater degree.

Figures 13 through 18 are plots of heat loads Q, in Btu per hour, versus condensing water flow rates, in pounds per hour, with Freon condensing pressure as the parameter. It should be noted that sometime during the experimentation the pressure gages measuring the inlet and outlet Freon pressures deviated from their original calibrations. The exact time at which this deviation developed could not be exactly determined. All of the coils were therefore tested again. Both the original and final data are tabulated in this report. The filled circles in the figures referred to above represent the original data while the unfilled circles represent the final data. The pressure parameters indicated on the final data curves is that measured after recalibrating the pressure gages. The old data curves are labeled with pressures obtained from the cross-plot curves, Q versus P, Figures 19 through 24, with parameters of water flow rate. This latter group of figures was prepared using only the final data. The dash lined curves on Figures 13 through 18 and 25 through 27 were obtained from reading values from the Q versus P cross plots (Fig. 19 through 25). Figures 25 through 25 are comparison curves for the short, medium, and long coils. The Freon pressure drop plots (Figs. 31 through 33) are also based exclusively on the final data.

In the summary of results Table II the outlet Freon pressure column was left blank in the case of the original data. The inlet Freon pressure column for the old data lists the pressures read off from the Q vs P curves by locating the measured Q and the corresponding measured flow rate curve and reading the inlet pressure on the abscissa.

A separate set of isothermal runs was taken to determine the pressure drop of the condenser water at different water flow rates. For low water rates the pressure drop was measured by means of a mercury manometer. For the higher water flow rates the inlet and outlet pressures were measured by means of calibrated pressure gages. Corrections were made for the static head difference. The data is tabulated in Table III. The pressure drop is plotted versus the water flow rates in Figs. 34 through 39.

Three particularly interesting and indicative plots are given in Figs. 28, 29, and 30. In these figures the heat loads Q are plotted versus

the length of the six coaxial coils at what are considered to be representative water flow rates (50, 100, and 150 lbs. per minute) with Freon condensing pressure as the parameter.

Figure 25 indicates that the 19 fin-per-inch short coil is superior to the 11 fin-per-inch short coil. It should be noted, however, that the 19 fin-per-inch short coil is more than one foot longer than the 11 fin-per-inch coil. This figure must therefore be used with caution. The medium length coils are comparable in length. For high Freon condensing pressures the 11 fin-per-inch coil indicates superior performance. At high condensing water flow rates, however, the slope of the 11 fin-per-inch performance curve decreases faster than the corresponding 19 fin-per-inch curve and the curves cross. It is believed that differences in the Freon side cross sectional free flow area, geometrical deformations of the coil cross sections as a result of coiling of the tubes (Figures 7 and 8), finned tube geometry differences, and to some extent the shape of the coils all influenced the resulting performances of the coils. The precise mechanism which caused the curves to cross is unknown.

Figures 28, 29, and 30 indicate that there are definite coil length limitations beyond which the added length is not effective in condensing. It should be noted that any added length results mostly in supercooling of the condensate.

Figures 31, 32, and 33 indicate that there is no significant difference in the Freon pressure drops between 11 fin-per-inch and 19 fin-per-inch coils of the same length.

DESCRIPTION OF COAXIAL COILS

Coil No.	Length ft.	Tube No.	Material of Tube	Fins Per Inch	В _О	$\mathtt{D}_{_{\Sigma}}$	I.D.	A _o ft²/ft	$ m A_{i}$ $ m ft^{2}/ft$
73	4 ft 7 in.	196047-01	Copper	19	0.824	0.711	0.611	0.556	0.160
47	5 ft 11½ in.	196047-01	Copper	19	0.824	0.711	0.611	0.556	0,160
22	11 ft $10\frac{1}{2}$ in.	196047-01	Copper	19	0.824	0.711	0.611	0.556	0,160
62	3 ft $6\frac{1}{2}$ in.	60-115032-01	Copper	11	406.0	0.679	0.598	0.762	0.1565
777	12 ft 8 in.	60-115032-01	Copper	1	406.0	629.0	0.598	0.762	0.1565
7/8	6 ft 0 in.	60-115032-01	Copper	11	406.0	629.0	0.598	0.762	0.1565

		G,	Btu/hr.		34,400	21,450 32,800	27 , 900 18,150	28,300	15,850	6,100	15,750	17,170	17,550	32 , 600	25,100	21,850	29,300	4,230	3,720	3,800
		Rate	#/min.		182 182															
		Water Rate	# Sec.		50 16.5 50 16.5															
		Evap. Pres.	Psi		크다(66	72 74	222	37.5	77 36	27	22	0.	5.2	37	34	38	38.5	32	28.5
		Freon ΔP	Psi		0 M	20 12	w w M	9										Н		11 7
		Freon Pressure In Out	Psi		125	125	걸	130										78	700	83.5
H	TEST DATA	Freon F In	Psi		134	134.5	134. 111.	136	107	101 101	707	104 104	104	134 128	128	128	128	8 7 7	ጽ የረ	86
TABLE	SUMMARY OF	Freon Temperature In Out	೦೦	• $6\frac{1}{2}$ in•	38.0	37.8	40°0 35°0	41.00 30.8	37.8	32•2	31.6	32.0 33.55	34.0	39 . 05	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	40°6	39.4	25.8	26.5 - 26.5	25.7
		Freon Te In	೦೦	nch, 3 ft.	58 50 50 6	54°0 56°0	0.09 178.0	25 5 6 6	以 了 。	1,6.8	16.5	50°53°	الم الم الم	76. 76. 76. 76.	, E.	57•7 [].	53.5	39.8	10.2	41.3
		H ₂ OAT Corr.	೦೦	, 11 fin/inch,	1.75	1.36 2.08	3.37 2.32	3.35	1,15	3. ሚኒ ሊኒ	1.07	1.23 0.95	0.95	ار 96	2.52	. 3 . 28	1.76	0,85	ר 28 72	0.80
		Water AT	೦೦	115032-01	1.55	1.16 1.88	3.17 2.12	3.15	0.95	3.25	0 18,0 18,0	1.03	0.75	1.40	2.32	ლ - - - - -	1. 52.	0. 64.	ч. 6 6	9.0
		Temperature Out	೦ಂ	79, Wolverine 60-115032-01,	23.55	23 . 13 23.85	25.20 24.17	25.20 01.49	22.97	25.27	22.90	23.03	22.70	23°58	24.18	25.03	23,36	22.53	22,95	22.70
		Water Tem In	೦ಂ	No. 79, Wol	22.00 21.95	21 . 97 21 . 97	22.03 22.05	22.05 01.09	22.02	22.02 00.10	22.05	22 . 00	21.95	21.90	21.86	21.95	21.80	21.88	21.87	22,10
		Run No•		Coil No	479 480	783 183	184 185	186 116	177	245 245	148	1.50 1.50 1.51	152	ស្តិច	12,	156	122	160	191	163

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			•••		
	œ	Btu/hr.		27,750 28,200 23,950 23,950 23,950 20,500 20	
	Water Rate	#/min.		13. 13. 13. 13. 13. 13. 13. 13. 13. 13.	
	ater	Sec.		110 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
	×	#		22222222222222222222222222222222222222	
	Evap. Pres.	Psi		2555685888888888885858565885858585858585	
	Freon $\Delta extstyle{P}$	Psi		122 122 122 123 145 166 176 177 177 178 178 178 178 178 178 178 178	
q)	Freon Pressure In Out	Psi		113 109 109 109 109 109 109	
(Continued)	Freon	Psi		108 108 108 108 108 108 108 108 108 108	
TABLE II	Tempe ra ture Out	ပ			
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	Water ∆r	၁၀	60-115032-01,		
	Temperature Out	ပ ဝ	Wolverine 60.	22200000000000000000000000000000000000	
	Water Te In	ರಿಂ	L No. 78, Wo	28222222222222222222222222222222222222	

	œ	Btu/hr.		35,200	30, 800	24,900	000.67	78,900	15,700	40,800	29,800	19,200	9,000	19,700	1,8,800	13,600	17,400	35,600	002,67	7,600	34,400	14,300
	Water Rate	#/min.		157																		
	Water	Sec.		19.1	7. E.	57.1	26.0	29.9	34.7	31.4	42.6	18.4	33.3	20.3	24.5	19.0	20.3	20.0	20.5	26.2	26.4	20.2
		#		S &	35	9	2	8	₿	2	20	及	20	S S	.요	요	,	요	S S	及	ያያ	አ
	Evap. Pres.	Psi		47.5	2462	: 🖪	.	147	38	31	70	20	79	36	32	72	67	55	5,5 5,5	છ	6)	017
	Freon &P	Psi														8 7	8	35.5	23	굯	ر ال ال	۰ د•
	Pressure Out	Psi														76.5	77	78	82	81	, 3 8	(·)
Continued	Freon P In	Psi		בן זיי	11 7.7	115	135	135	135	135	135	135	135	135	135	8 7	85	113.5	135	135	115.5	00
TABLE II (Continued)	Freon Temperature In Out	೦೦	t. 8 in.	25.05	26.5 26.5	28.1	24.65	25.4	26.2	28.2	32.8	25.2	25.15	25.1	25.3	24.0	23.9	24.9	25.0	25.3	25.4	0.42
	Freon Ter In	೦°	inch, 12 ft.	20° 1-0° 1-0°	۲. د ه	ج 8. 12.	53.75	57.1	53.2	55.2	57.5	54.3	54.45	59.6	63.0	39.2	38.7	52.0	54.2	55.0	50°5	47.C
	H2OAT Corr.	ပ္စ	, 11 fin/in	2.08	3.79	5.48	2.81	3.75	7•30	9. 9	9.80	2.80	3.60	3.12	3.70	0.80	0.00	2.20	3.15	3.85	2 . 80	CT•T
	Water ∆T	೦°	115032-01	1.88	55°	5.28	2.61	3.55	4.70	0 [†] 09	8°6	2.60	3.40	2.92	3.50 2.00	9.0	0.70	2•00	2.95	3.65	8 9 8	0.75
	Water Temperature In Out	೦೦	No. 77, Wolverine 60-115032-01,	23.98	25.70	27.19	24.61	25.50	26.61	28.52	31.65	24.93	25.30	24.92	25.50	22,60	22.65	24.10	25.00	25.65	24•58	73.00
	Water Te	ဝ	Io. 77, Wo.	22.10	22,13	21.91	22,00	21.95	21.91	22,12	20.05	22.33	21.90	22,00	22,00	25.00	21.95	22.10	22.05	22.00	21.98	CO.22
	Run No.		Coil N	259	262	263	264	265	566	267	268	569	270	278	279	398	366	007	403	707	7 7 7 7	400

	ď	Btu/hr.		43,600 29,000 37,200 26,100 31,900	22, 500 33, 500 23, 500 23, 500 24, 500 26, 500	
	Rate	#/min.		192.5 191.5 127.7 127.2 87.0	88 887.0 887.0 887.0 887.0 71.0 71.0 71.0 71.0 71.0 71.0 71.0 7	\ \ !
	Water	Sec.		12275 12275 12275	13.8 21.0 21.0 21.0 19.6 27.2 27.2 27.0 38.0 38.0 19.6 6.1 19.6 6.1 19.6 6.1 19.6 6.1 19.6 6.1 19.6 19.6	Ì
		#		2222	22222222222222222222222222222222222222	\
	Evap. Pres.	Psi		28252 28252	E2%50%2028%30%20%50%	
	Freon AP	Psi		2. 4. 4. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6.	0 FV FOOOOHVO @ 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	,
	Freon Pressure In Out	Psi		116.5 97 121 110 126	110 122 122 126 126 130 130 100 100 111 120 120 120 120	, i
ntinued)	Freon P In	Psi		135 1114.5 1114.5 135.45	111 130 100 100 100 100 100 100 100 100	ì
TABLE II (Continued)	Temperature Out	೦೦	, in.	200 t 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	% & & & & & & & & & & & & & & & & & & &	1
T	Freon Te In	ರಿ	1, 4 ft. 7	877878 00700	587777875EEEEEE8888788788) •)
	H ₂ OAT Corr.	ာ္၀	19 fin/inch	2°10 1°40 1°40 3°40	00 00 00 00 00 00 00 00 00 00 00 00 00) J
	Water ∆T	೦ಂ		1.50 1.20 1.70 3.20) •
	nperature Out	೦೦	Wolverine 196049-01,	23.65 23.65 24.66 25.80 25.80 25.80 25.80	00000000000000000000000000000000000000))
	Water Temperature In Out	೦೦	No. 73, Wol	21.75 22.10 22.10 22.10		00 - 77
	Run No•		Coil N	7 777 777 777 777 777 777 777 777 777	,	5

	G*	Btu/hr.		29,300 28,050 27,400	17,850 9,300	39,400 44,800 42,200	36,300 29,000	4,900 6,860 320	8,640 000,004	35,400 50,400	25,100 50,500	32,000 23,550 17,750	39,600 27,700 19,800
	late	#/min.		171.5	17.6	115 171.5 139.5	88. 5 5. 6	37.9 70.6 110	123	164	166	22.00	96.99 96.99 96.99
	Water Rate	# Sec.		50 17.5 50 20.8 50 24.5									
	Evap. Pres.	Psi		38 36 5 7	1,74 1,74 1,00 1,00 1,00 1,00 1,00 1,00 1,00 1,0	26 27 27	72.25 72.25 72.25	7 0 T	767	26.7	.£&;	2 S &	17 8 27 1 17 8 27 1
	Freon ΔP	Psi							21.5	12.5	24.5	10 7 7 F	17
	Freon Pressure In Out	Psi							113.5	102	97	125	121 97 100
(Continued)	Freon P In	Psi		108 108 108	108	128 128 128	128 128 128	က က က က က က က က က		10	10		
TABLE II (Temperature Out	೦೦	11 <u>‡</u> in.	31.5	33.8	35 35 35 35 35 35	36.95 38.6 10.0	257 257 107 107	96.0 96.0 96.0	, 0 w	37.0	377° 377° 30° 30° 30° 30° 30° 30° 30° 30° 30° 30	33.0 30.1 23.7
	Freon Ter In	ರಿಂ	5 ft.	17.77.02.02 0.02.02	20 20 20 20 20 20 20 20 20 20 20 20 20 2	57.03 56.4 56.1	57.75 5.35.75 5.35.75	32.6 11.35 38.42	77 C	2000	56.0	77.00 77.00 77.00	56.0 148.0 34.0
	H ₂ OAT Corr.	ರಿಂ	9 fin/inch,	1.58 1.80 2.07	3.40	3.17 2.42 2.80	3.82 4.79 6.25	0.00	3.10	800.0	1.40	3.65 2.65 2.65	3.80 2.65 1.90
	Water AT	ರಿಂ	196049-01, 19	1.38	3.20	2.97 2.22 2.60	3.62 4.59 6.05	H00	3.00	1.90	1,30	0 7 7 67 7 67 7	3.70 1.80 1.80
	Temperature Out	೨೦	Wolverine 196	23.40 23.60 23.87	25.18	25.07 24.12 24.50	25.52 26.67 28.15	23.10 22.70 22.50	22.45 25.00 25.00	54°50 54°00 57°50	23.20	26.97 25.62 21.62	25.80 24.65 23.90
	Water Tem] In	ರಿಂ	No. 74, Woly	22.00 22.00 22.00	21.98	22.10 21.90 21.90	21.90 22.08	22.00 22.00 22.00	22.00	22.10 21.90	21.90	22.07 22.07 21.98	22.10 22.10 22.10
	Run No.		Coil N	227 228 229	231 232	233 234 234 234 237	236	239	242 466 1.67	704 1708 1709	470 471	473 474 125	724 724 7438 7438

	œ	Btu/hr.		700,600	29,500	11,020	12,000	32,800	14,400	23,550	25,700	35,400	46,500	46,700	47,300	35,900	26,900	20,100	13,400	6,560	25,900	13,800							
	Rate	#/min.		58.7	57.2	57.4	8.95	97.8	8.96	8.96	138	136	135	192	192	192	24.4	24.1	24.1	23.3	192	191							
	Water	Sec.		30.7	31.5	31.4	31.0	30.7	31.0	31.0	21.7	22.0	22.2	15,0	15.6	15.6	24.6	24.9	24.9	25.7	15.6	15.7							
		##		9	8	9	2	옸	S,	S	ß	汉	3	S,	汉	S	10	10	10	10	옸	S							
	Evap. Pres.	Psi		52	52	56	52.5	43.5	39	42	775	39	34	32.5	877	79	65	99	89	23	62	45							
	Fre on ΔP	Psi		38	23	八	rV	28	917	16.5	18.5	28.5	52	52.5	53	34	19	10.5	7	Μ	20	7							
<u> </u>	Pressure Out	Psi		25	92	80	80	98	89	87	81.5	98	85	82	82	81	911	105	93	82	80	78							
[ABLE II (Concluded)	Freon P In	Psi		135	115	8 77	85	, לובנ	135	100.5	100	114.5	135	134.5	135	115	135	115.5	100	85	100	85							
TABLE II	Freon Temperature In Out	^ပ ဝ	10 <u>1</u> in.	31.1	29.1	25.1	24.4	26.8	28.1	25.8	25.4	26.2	26.7	25.9	25.8	25.6	37.2	34.0	30•3	25.7	24.7	24.2							
	Freon Te In	೦ಂ	1, 11 ft.	59.0	51.0	0.44	43.0	55.0	57.8	9.74	7.57	52.0	56.6	59.5	58°3	53.5	54.8	6•67	57.0	0.87	50.7	9.81							
	H ₂ OAT Corr.	ပ္ပ	fin/inch	07°9	4.75	1.78	1.15	3.10	4.25	2.25	1.72	2.40	3.18	2.25	2.28	1.73	10.20	7.73	5.15	2.60	1.25	29.0							
	Water AT	೦೦	60,49-01, 19	6049-01, 19	,6049-01, 19	6049-01, 19	,6049-01, 19	,6049-01, 19	,6049-01, 15	5049-01, 19	6.20	4.55	1.58	0.95	2.90	4.05	2.05	1.52	2.20	2.98	2.05	2.08	1.53	10.00	7.53	4.95	2.40	1.05	24.0
	Water Temperature In Out	ဝွ	No. 75, Wolverine 196049-01, 19	28.24	26.50	23.56	23,00	24.85	26.05	24.07	23.50	24.25	25.03	24.10	24.05	23.55	32.00	29.53	26.90	24.45	23.00	22.47							
	Water Te In	၀	10. 75, WC	22.04	21.95	21.98	22.05	21.95	22.00	22.02	21,98	22.05	22.05	25.05	21.97	22.02	25,00	22.00	21.95	22.05	21,95	25,00							
	Run No.		Coil 1	704	708	607	770	117	412	413	177	415	716	417	47.8	419	750	421	422	423	757	425							

TABLE III. CONDENSING WATER PRESSURE DROP Water Pressure Gauge Manometer ΔP Water Rate Temp. Reading Reading Corr. outlet inlet left right OC Psi Psi in. Hg in. Hg Psi # Sec. #/min. Coil No. 73, Wolverine 196049-01, 19 fin/inch, 4 ft. 7 in. 7.8 45.9 30.8 13.9 15.3 50 196 7.8 46.2 31.3 50 13.7 15.4 195 48.5 57.0 7.8 7.3 50 22.1 136 12.6 7.6 30.3 50 16.2 185 7.6 24.3 13.4 9.8 50 18.0 166.5 7.6 + 4.3 **-** 3.8 3.69 50 30.9 97 7.65 - 8.4 + 8.6 7.75 50 20.5 146.5 7.65 -10.0 +10.1 9.15 50 19.0 158 7.65 - 5.6 + 6.0 50 5.28 25.7 117 7.65 - 2.0 + 2.5 50 2.05 42.6 70.4 - 1.2 7.7 + 1.75 1.34 50 53.9 55.6 Coil No. 74, Wolverine 196049-01, 19 fin/inch, 5 ft. $11\frac{1}{2}$ in. 8.2 37.0 20.6 15.2 50 14.4 208 8.1 32.1 17.8 13.2 50 15.4 195 8.05 24.4 13.6 9.7 50 18.0 167 8.0 26.3 14.5 10.7 50 17.1 175.5 8.0 21.5 11.9 8.5 50 18.5 162 8.0 - 9.0 50 + 9.2 8.31 19.9 151 0.8 + 8.0 - 7.7 7.17 50 21.9 137 7.8 - 5.95 + 6.35 5.62 50 24.9 120.5 7.8 - 4.6 + 5.1 28.3 4.44 50 106 7.7 - 3.1 + 3.65 50 3.1 34.2 87.7 0.8 - 2.0 + 2.6 50 2.12 42.3 70.9 8.05 - 1.1 + 1.7 50 1.3 55.5 54 Coil No. 77, Wolverine 60-115032-01, 11 fin/inch, 12 ft. 8 in. 8.5 13.2 41.1 50 17.9 167.5 53.5 8.4 11.3 41.0 50 19.5 154 44.8 10.5 8.4 33.1 50 20.1 149 44.3 8.35 9.1 34.0 50 21.6 139 8.35 32.5 7.6 23.8 50 23.8 126 8.4 25.4 5.9 18.4 50 26.9 111.5 8.5 50 50 18.6 4.3 13.2 31.7 94.6 8.5 - 9.7 +10.8 38.7 9.37 77.5 8.55 - 7.1 45.5 + 7.9 6.86 50 66 8.6 5.17 + 6.05 - 5.25 50 57.5 52.1 8.7 + 4.6 - 3.8 3.85 50 62.0 48.4

16

Water Temp.	Pressur Read inlet	re Gauge ling outlet	Mano	II (Contin meter ding right	ΔP Corr.	• Water Rate						
o _C	Psi	Psi	in. Hg	in. Hg	Psi	#	Sec.	#/min.				
Coil No. 75, Wolverine 196049-01, 19 fin/inch, 11 ft. $10\frac{1}{2}$ in.												
7.4 7.5 7.5 7.7 7.65 7.7 7.7 7.7 7.7 7.8 7.8 7.8	42.5 31.5 36.0 30.2 25.2 22.2	17.0 12.5 14.4 12.0 10.2 9.0	-11.3 - 9.2 - 7.3 - 4.8 - 3.8 - 2.35 - 1.45	+ 5.3	24.3 17.9 20.5 17.1 13.9 12.1 10.4 8.55 6.81 4.58 3.71 2.39 1.62	50 50 50 50 50 50 50 50 50 50 50 50 50 5	15.7 18.6 17.2 19.0 20.8 22.2 24.5 27.5 31.1 39.0 43.7 77.8 68.5	191 161 174 158 144 135 122.5 109 96.5 77 68.6 54				
Coil No. 78, Wolverine 60-115032-01, 11 fin/inch, 6 ft.												
7.9 7.85 7.85 7.8 7.8 7.8 7.85 7.9 7.9 8.0 8.0 8.1 8.1 8.3 8.5	45.5 46.5 46.5 42.7 40.5 35.0 30.0 21.7	16.5 16.8 17.0 15.4 14.7 12.6 10.9 8.2	-11.3 - 7.0 - 8.7 - 5.7 - 3.2 - 4.0 - 2.2 - 1.25	+11.4 + 7.4 + 9.0 + 6.2 + 3.8 + 4.5 + 2.8 + 1.9	27.8 28.5 28.3 26.1 24.6 21.3 18.0 12.4 10.3 6.6 8.1 5.45 3.21 3.9 2.3 1.46	50 50 50 50 50 50 50 50 50 50 50 50 50 5	15.8 16.5 15.8 16.5 17.0 18.0 20.0 23.5 26.3 33.5 37.1 48.8 44.0 57.9 74.8	190 182 190 182 176.5 167 150 128 114 89.5 99.2 80.9 61.5 68.1 51.9 40.1				

TABLE III (Concluded)

Water Temp.	Manometer Reading left right		ΔP Corr.		Water Rate						
°C	in. Hg	in. Hg	Psi	#	Sec.	#/min.					
Coil No. 79, Wolverine 60-115032-01, ll fin/inch, 3 ft. $6\frac{1}{2}$ in.											
7.8 7.7 7.7 7.7 7.7 7.7 7.75 7.8	-13.8 -11.7 -10.4 - 8.0 - 6.2 - 4.4 - 2.9 - 1.8	+13.9 +11.9 +10.7 + 8.4 + 6.7 + 5.0 + 3.6 + 2.5	12.6 10.75 9.6 7.46 5.88 4.28 2.96 1.96	50 50 50 50 50 50 50	19.5 20.5 22.4 25.0 28.6 33.7 40.9 50.8	134 120 104 89 73•4 59					
7.9 8.0	- 1.15 - 0.6	+ 1.95 + 1.4	1.41 0.91	50 50	60.1 76.6	49.9 39.2					

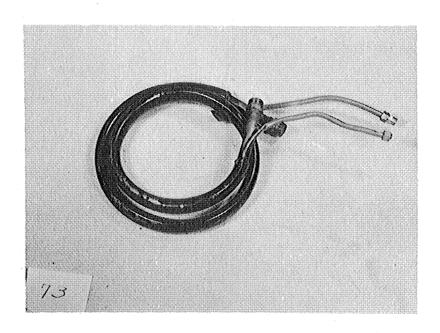


Fig. 1. 4'-7" long 19-fin-per-inch coaxial coil.

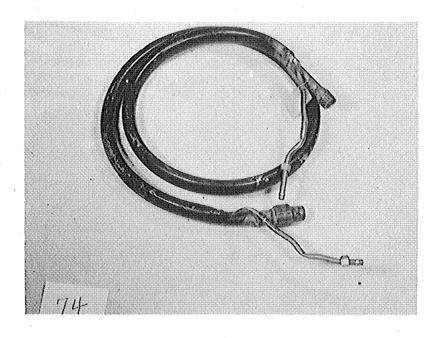


Fig. 2. 5'-11-1/2" long 19-fin-per-inch coaxial coil.

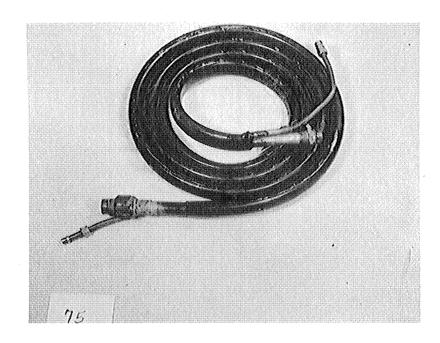


Fig. 3. $11^{4}-10-1/2^{11}$ long 19-fin-per-inch coaxial coil.

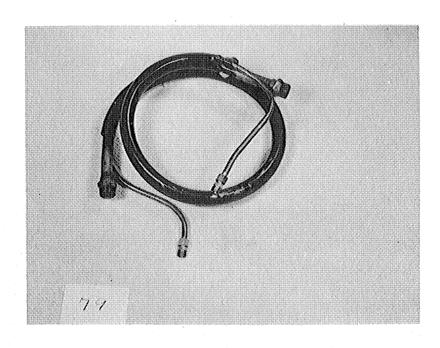


Fig. 4. 3'-6-1/2" long 11-fin-per-inch coaxial coil.

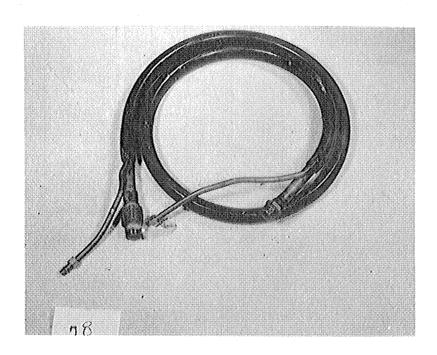


Fig. 5. 6'-0" long ll-fin-per-inch coaxial coil.

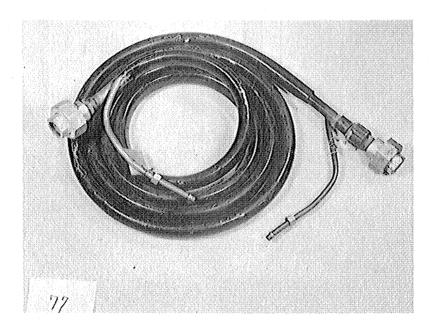


Fig. 6. 12'-8" long 11-fin-per-inch coaxial coil.

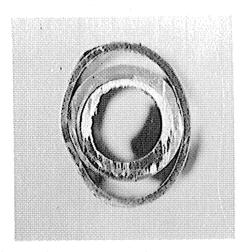


Fig. 7. Cross-sectional view of the 11-fin-per-inch coil.

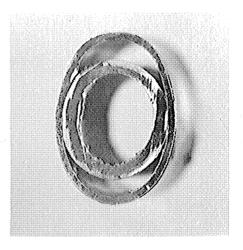


Fig. 8. Cross-sectional view of the 19-fin-per-inch coil.

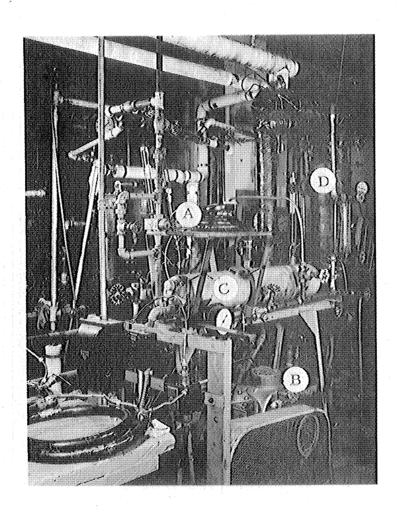


Fig. 9. Compressor and condensing section.

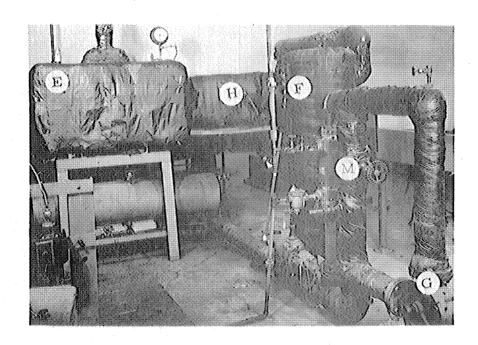


Fig. 10. Freon-12 evaporator and evaporator water system.

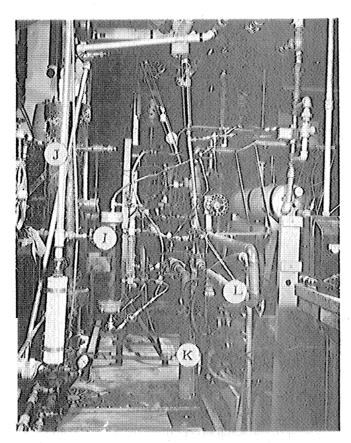
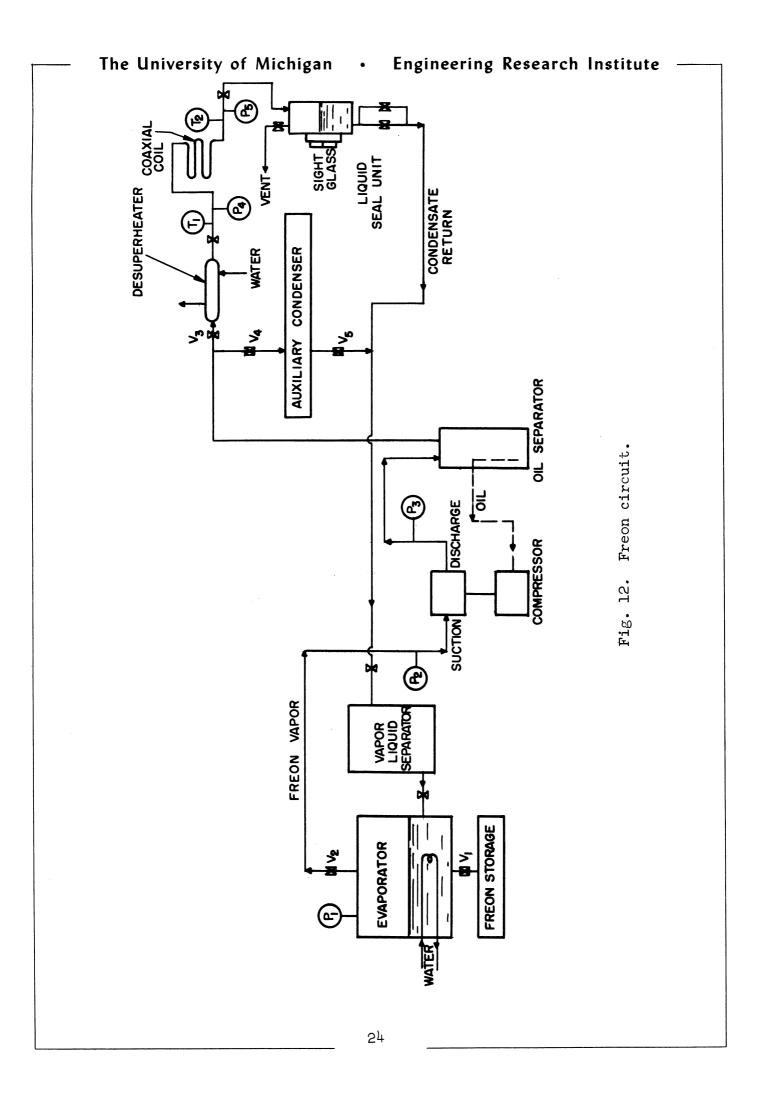
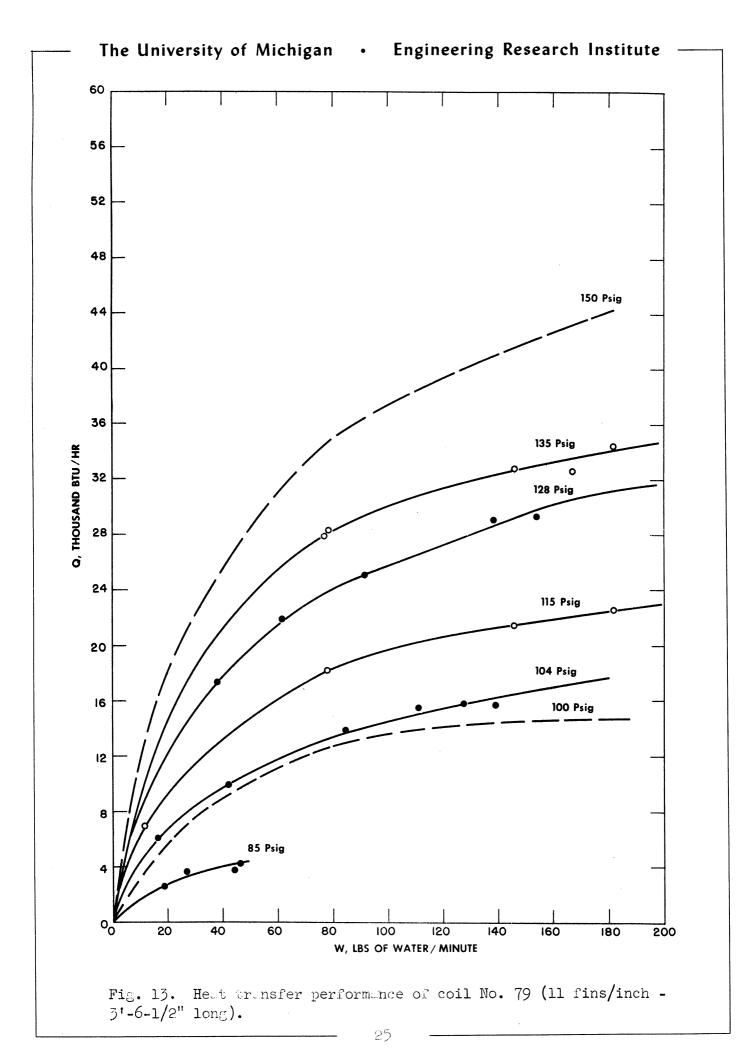


Fig. 11. View of the liquid seal and the desuperheater.





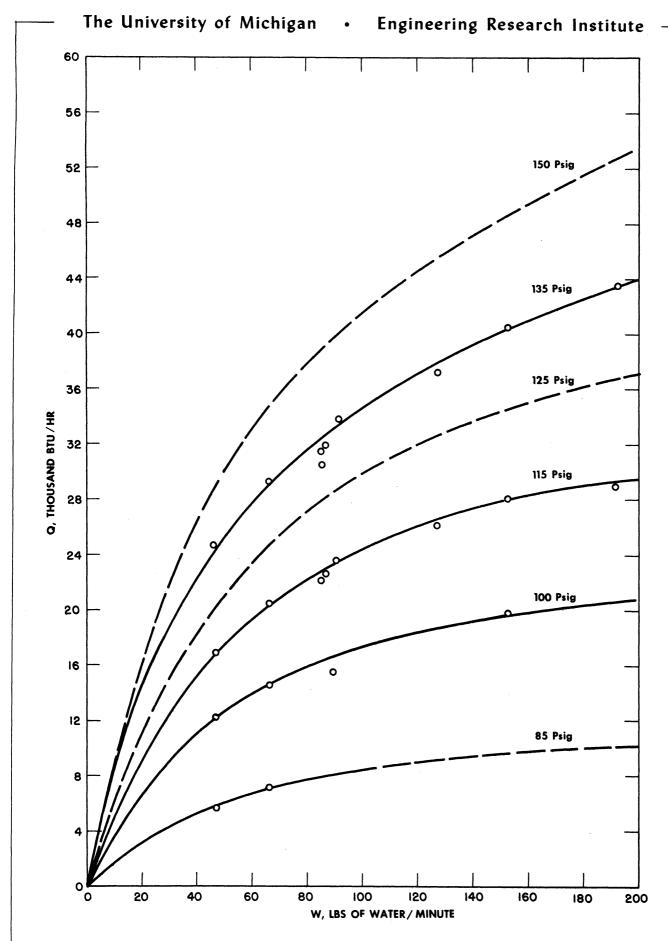
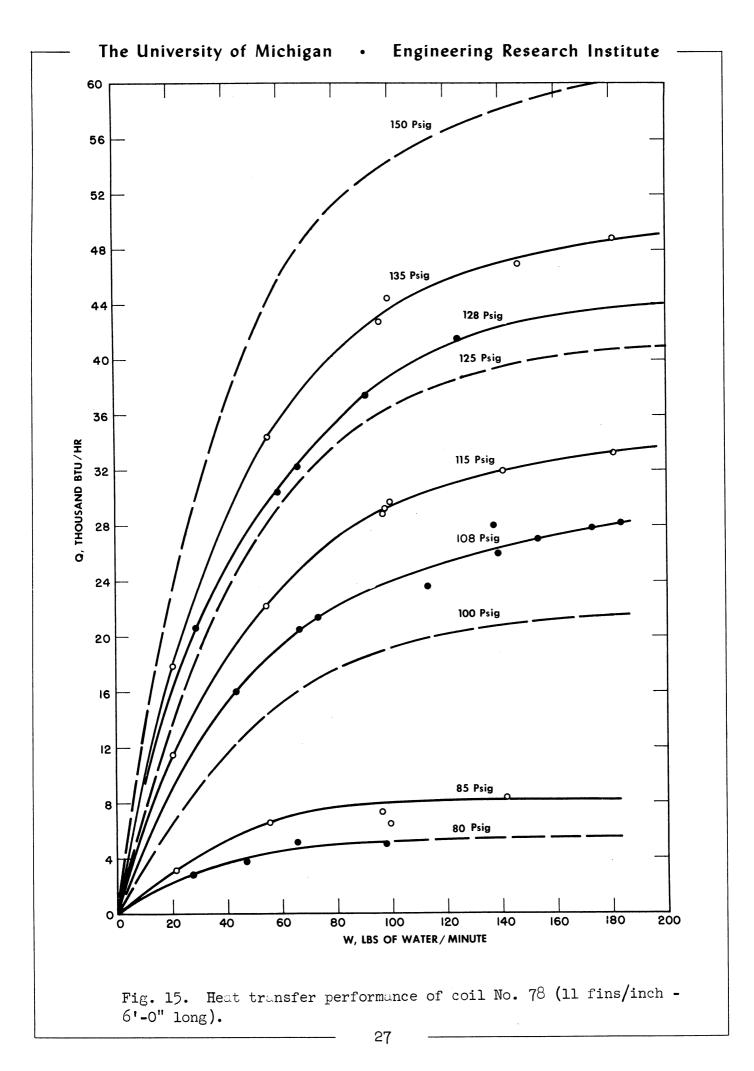


Fig. 14. Heat transfer performance of coil No. 73 (19 fins/inch - 4'-7" long).



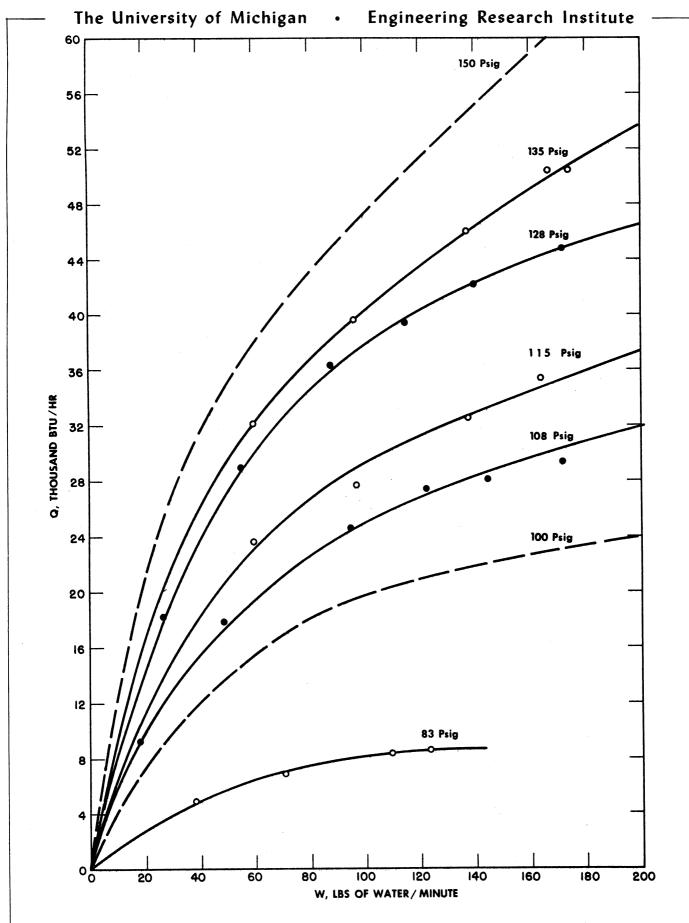
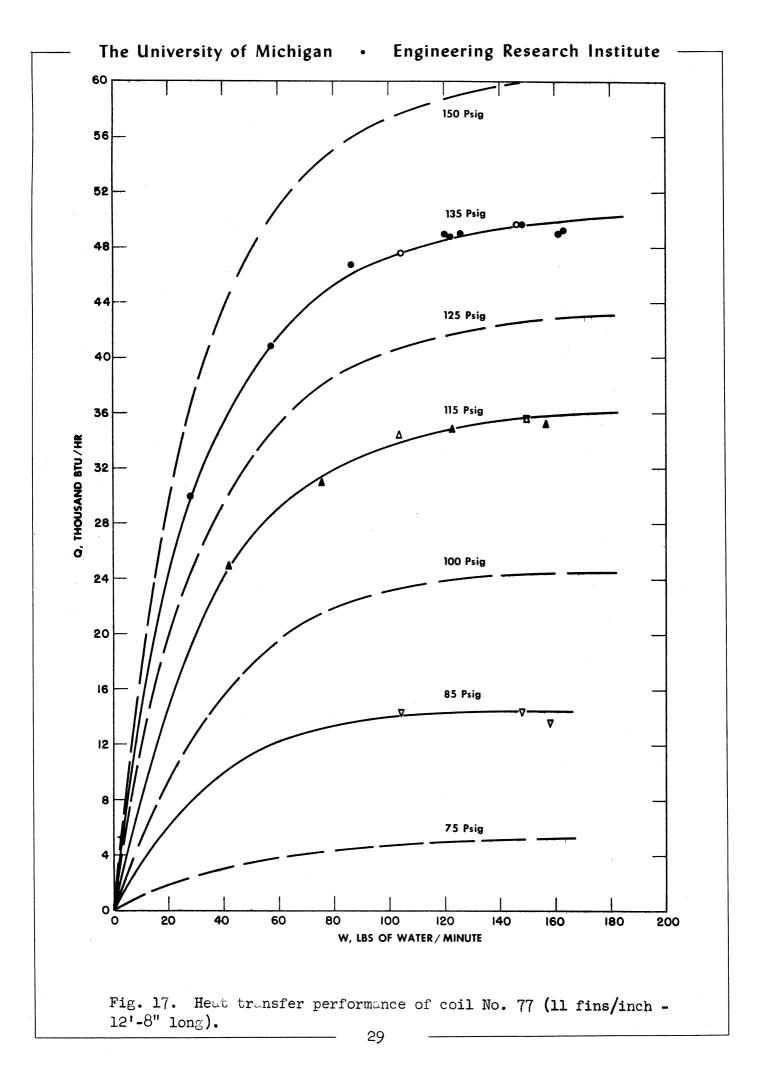


Fig. 16. Heat transfer performance of coil No. 74 (19 fins/inch - 5'-11-1/2" long).



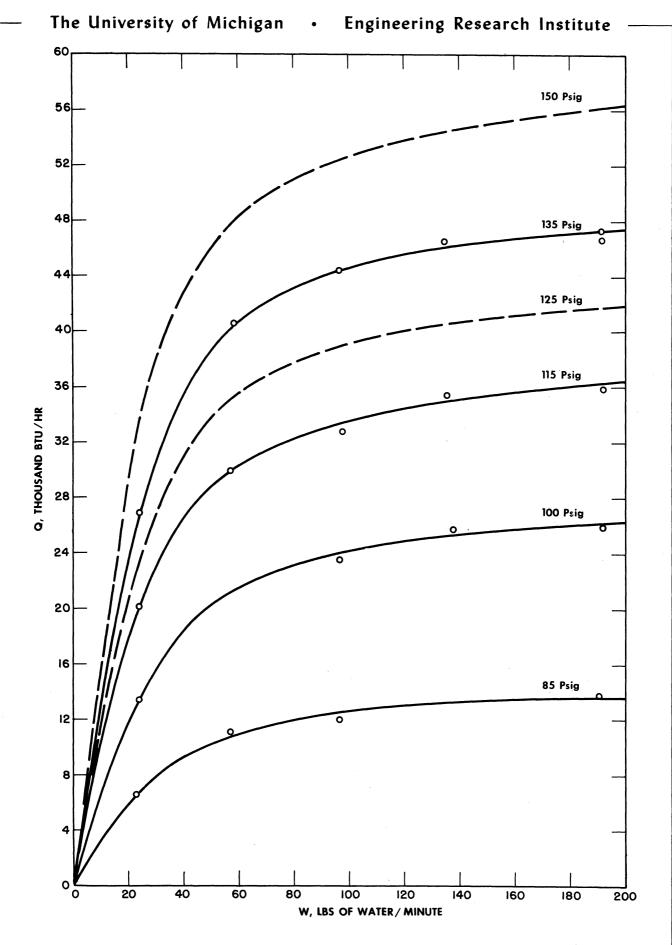


Fig. 18. Heat transfer performance of coil No. 75 (19 fins/inch - 11'-10-1/2" long).

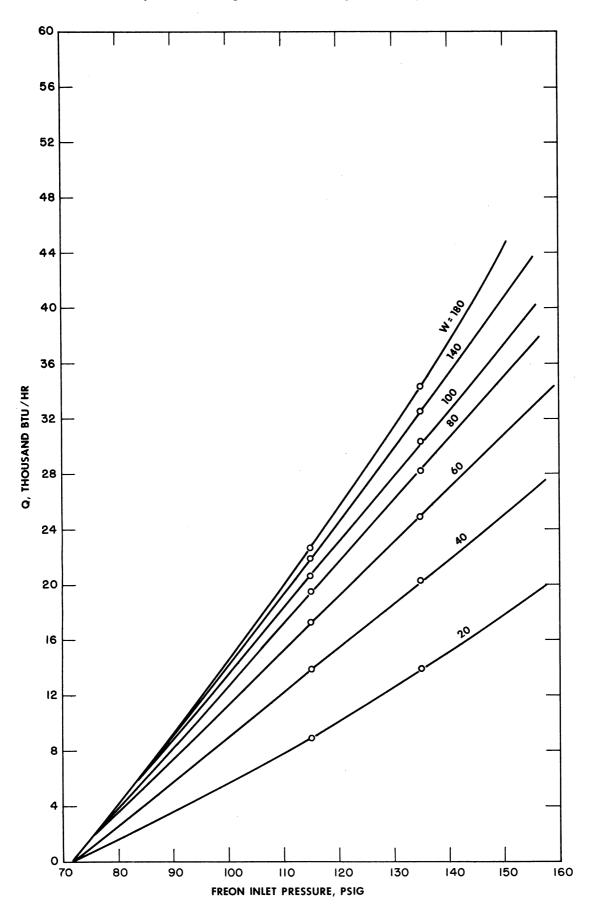


Fig. 19. Heat transfer performance cross-plot for coil No. 79.

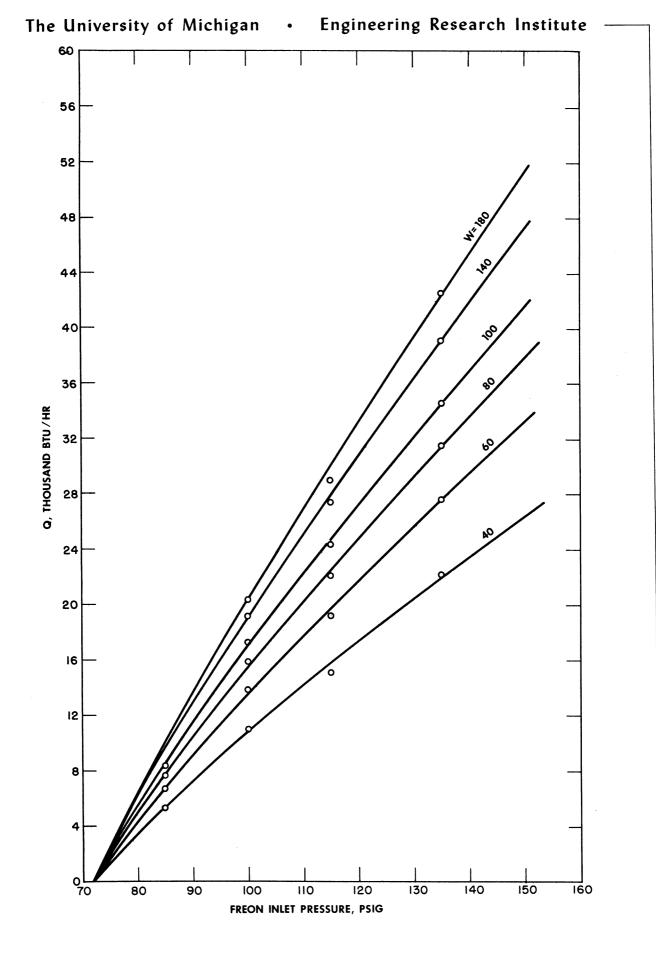


Fig. 20. Heat transfer performance cross-plot for coil No. 73.

Fig. 21. Heat transfer performance cross-plot for coil No. 78.

FREON INLET PRESSURE, PSIG

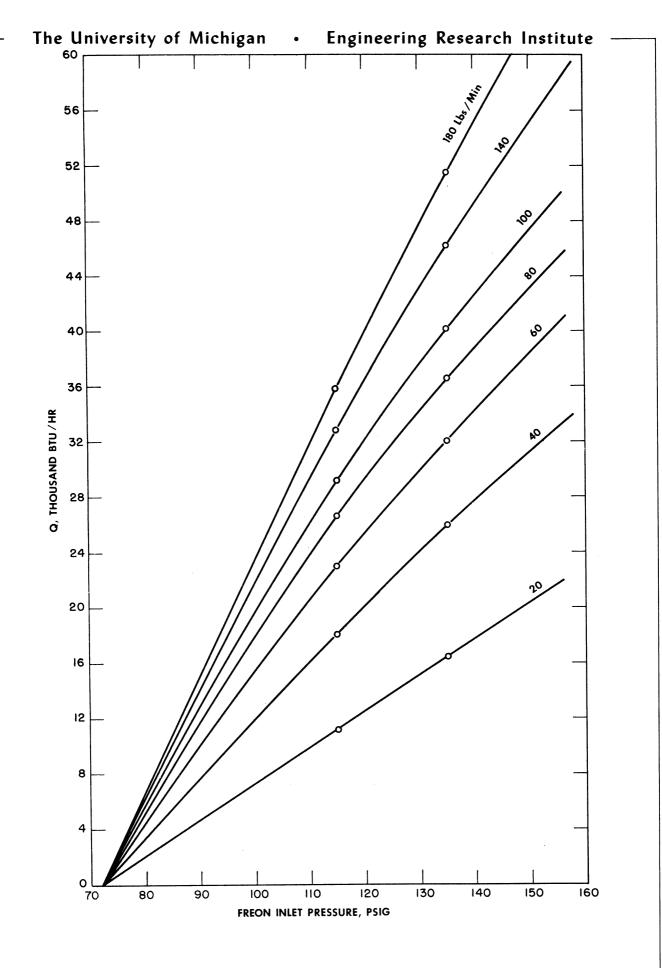
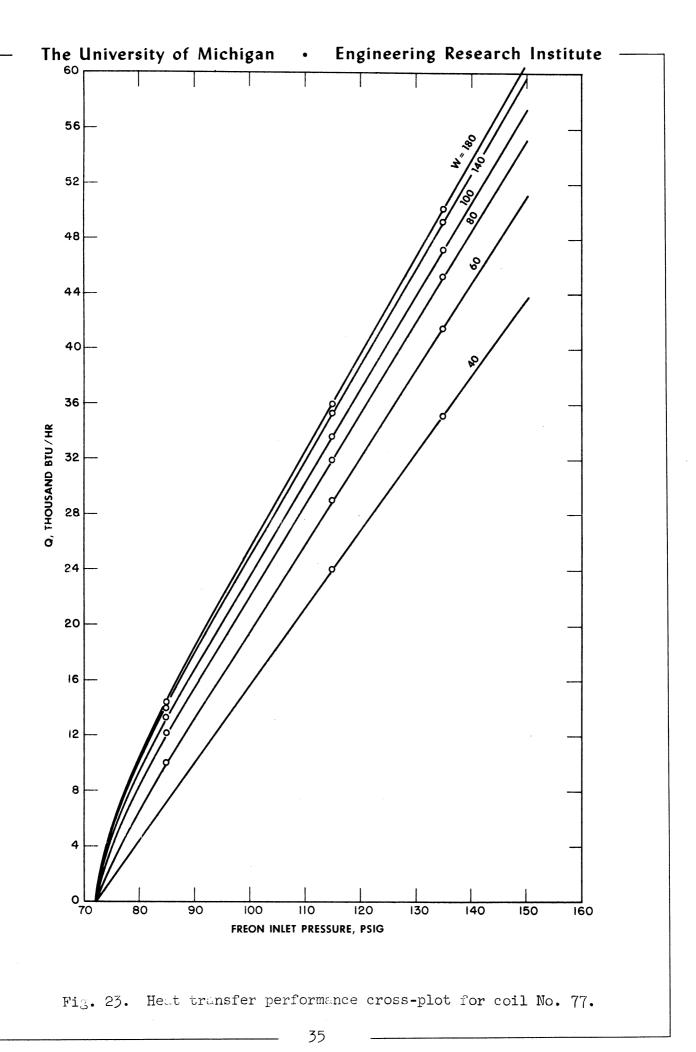
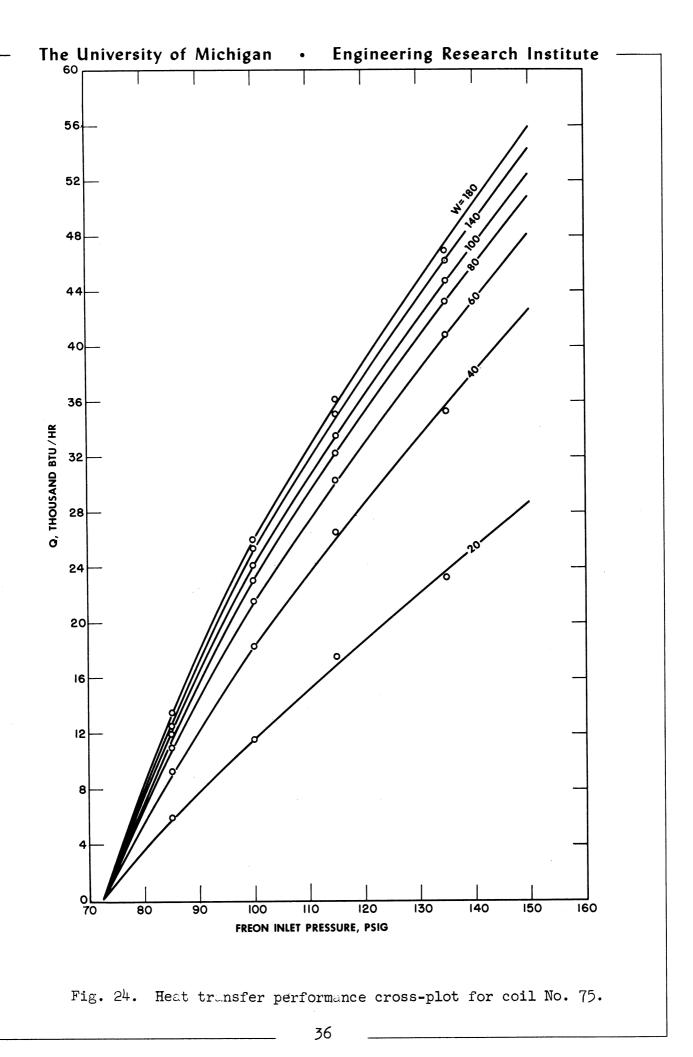
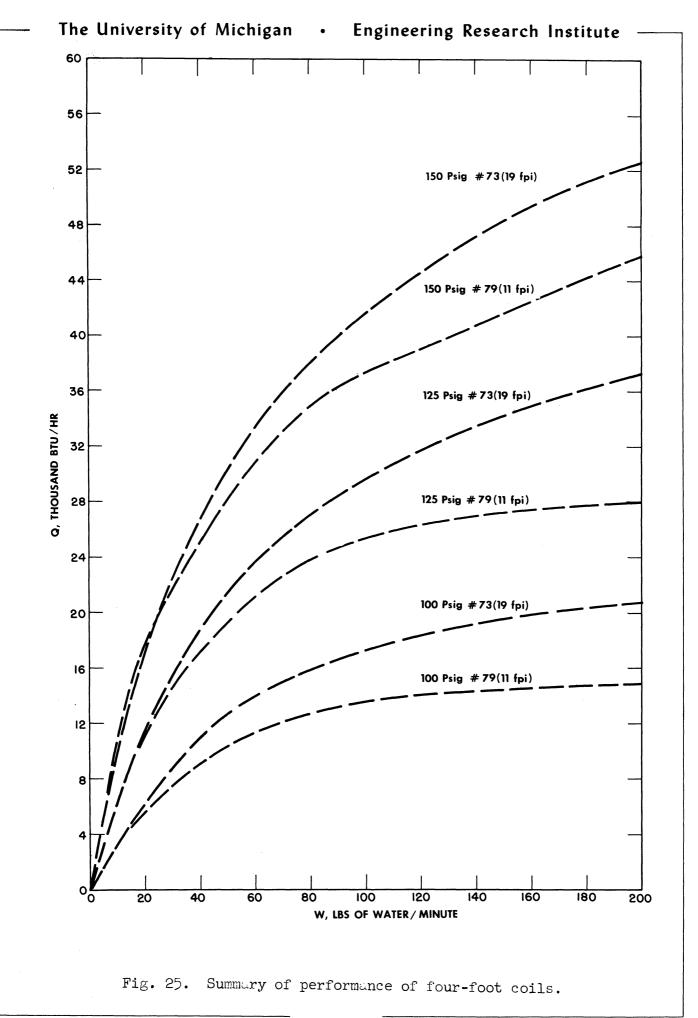


Fig. 22. Heat bransfer performance cross-plot for coil No. 74.







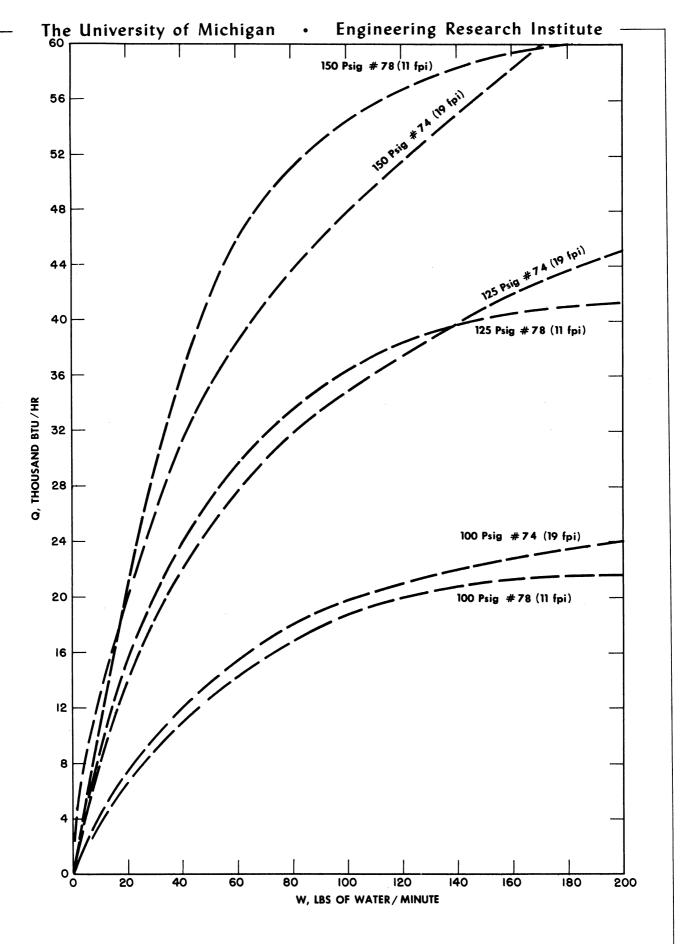
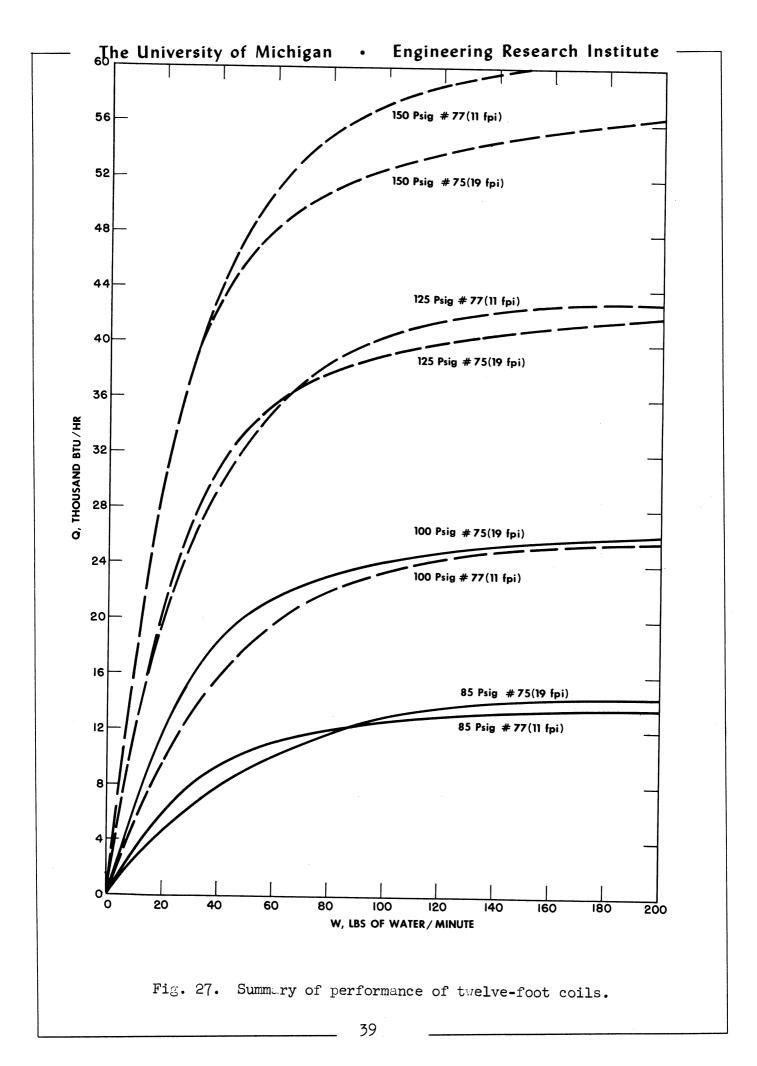


Fig. 26. Summary of performance of six-foot coils.



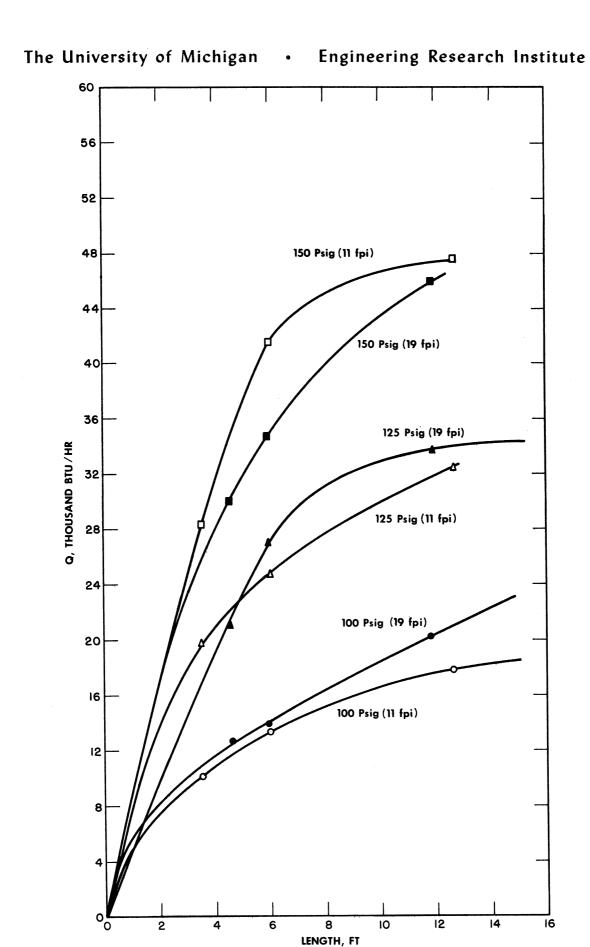


Fig. 28. Effect of length of coil on heat load with a constant water flow rate of 50 lbs. per minute.

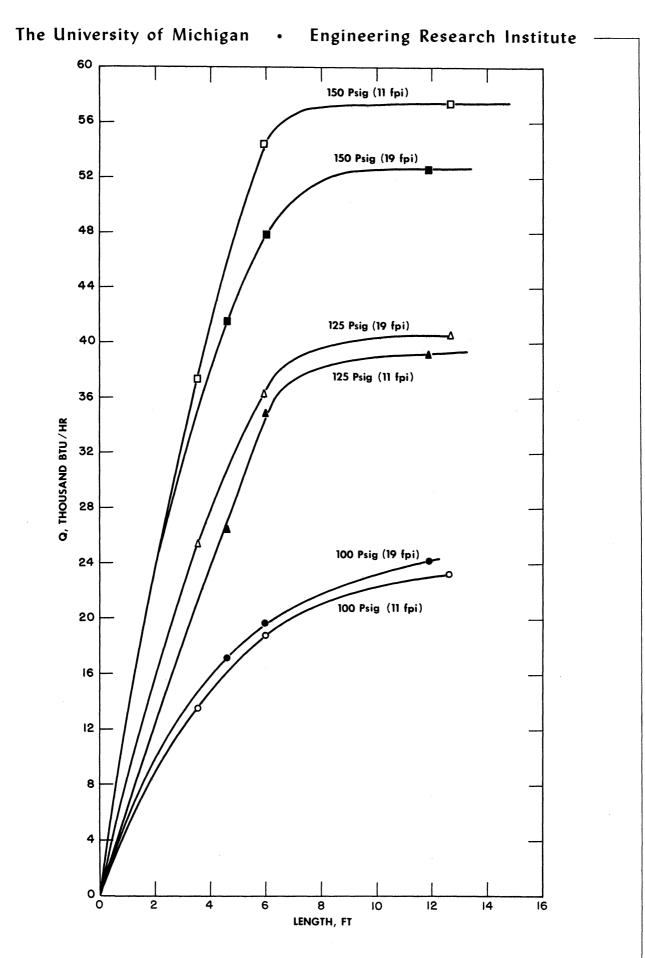


Fig. 29. Effect of length of coil on heat load with a constant water flow rate of 100 lbs. per minute.

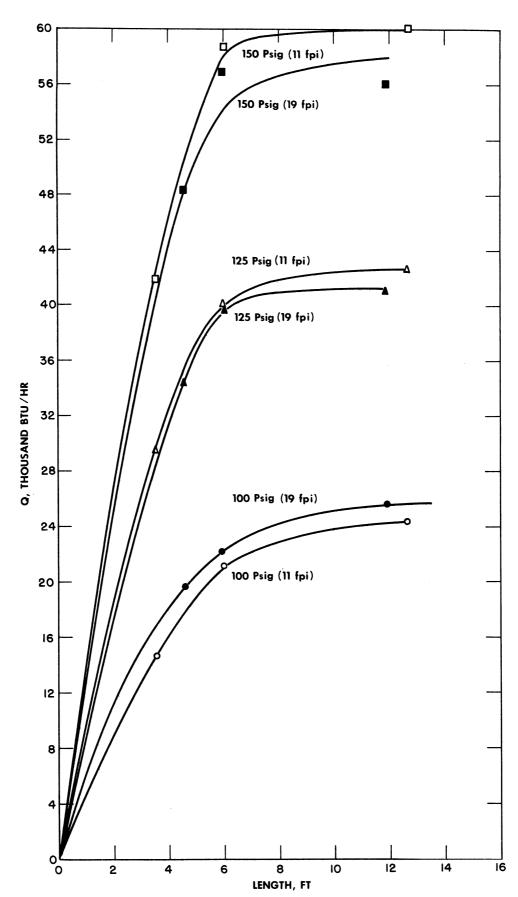
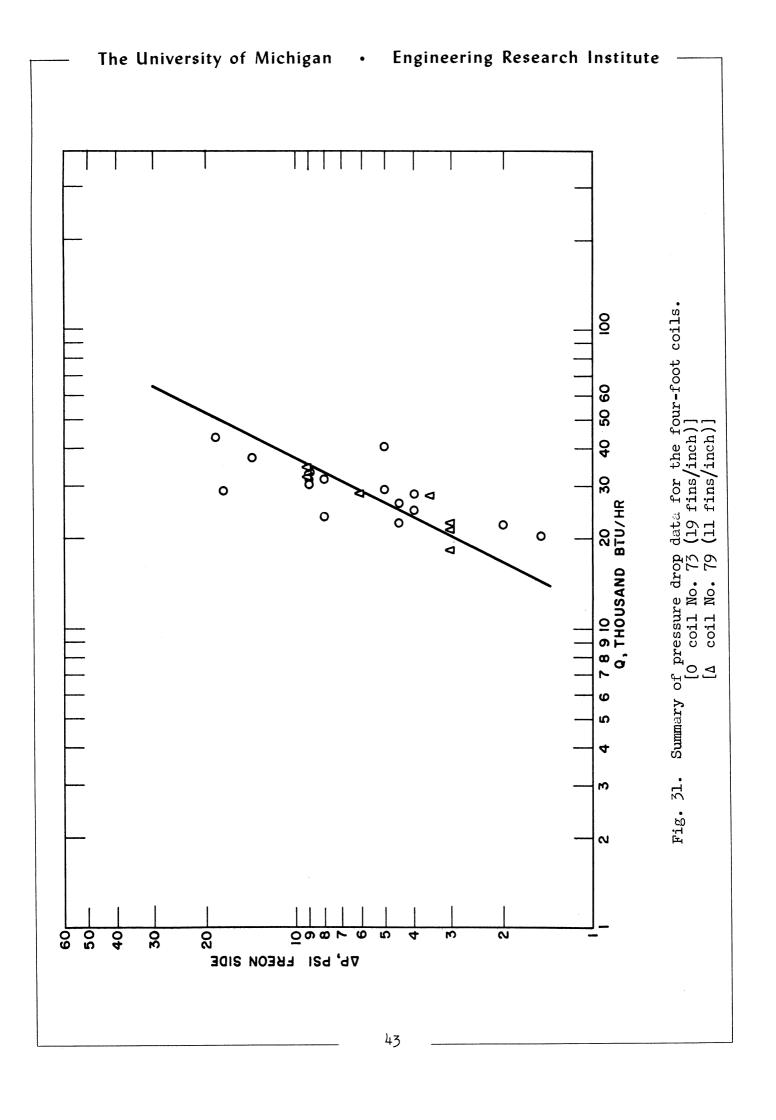
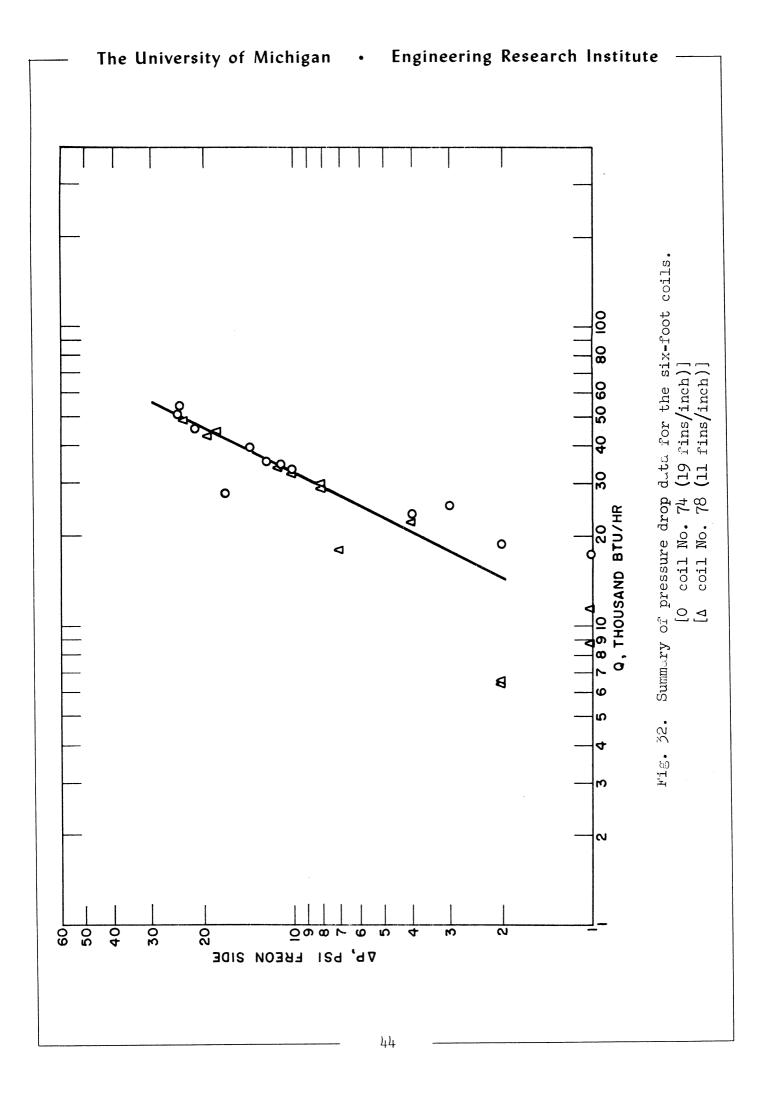
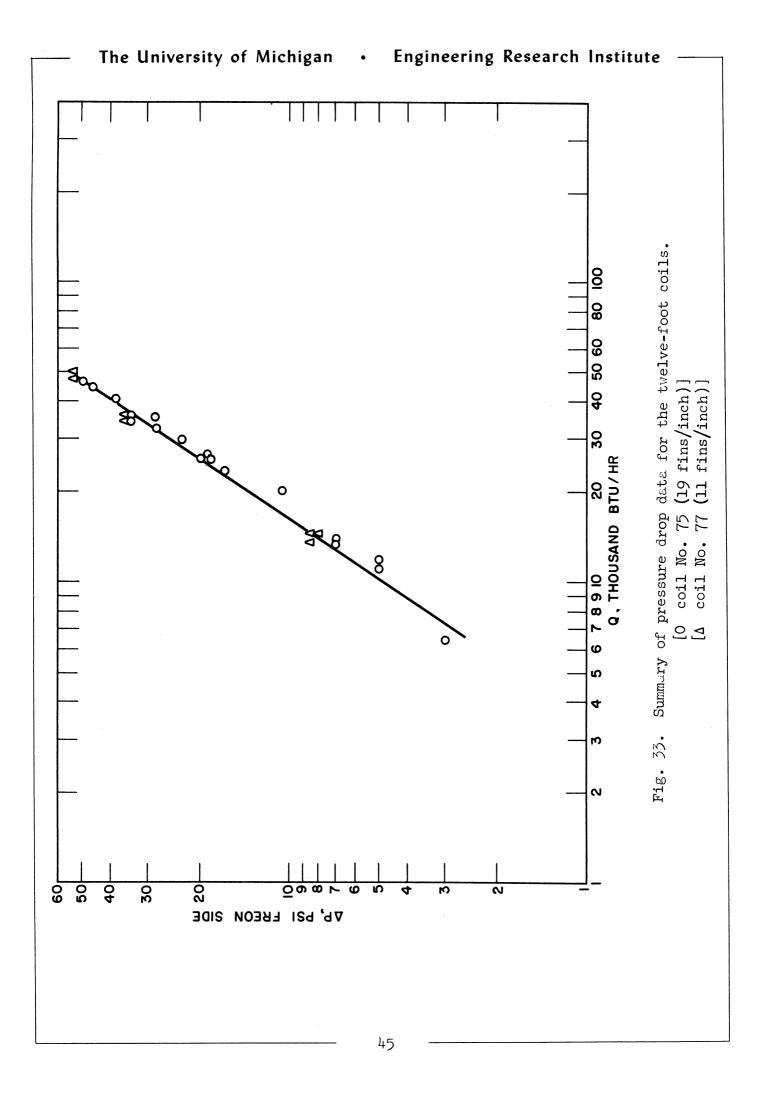


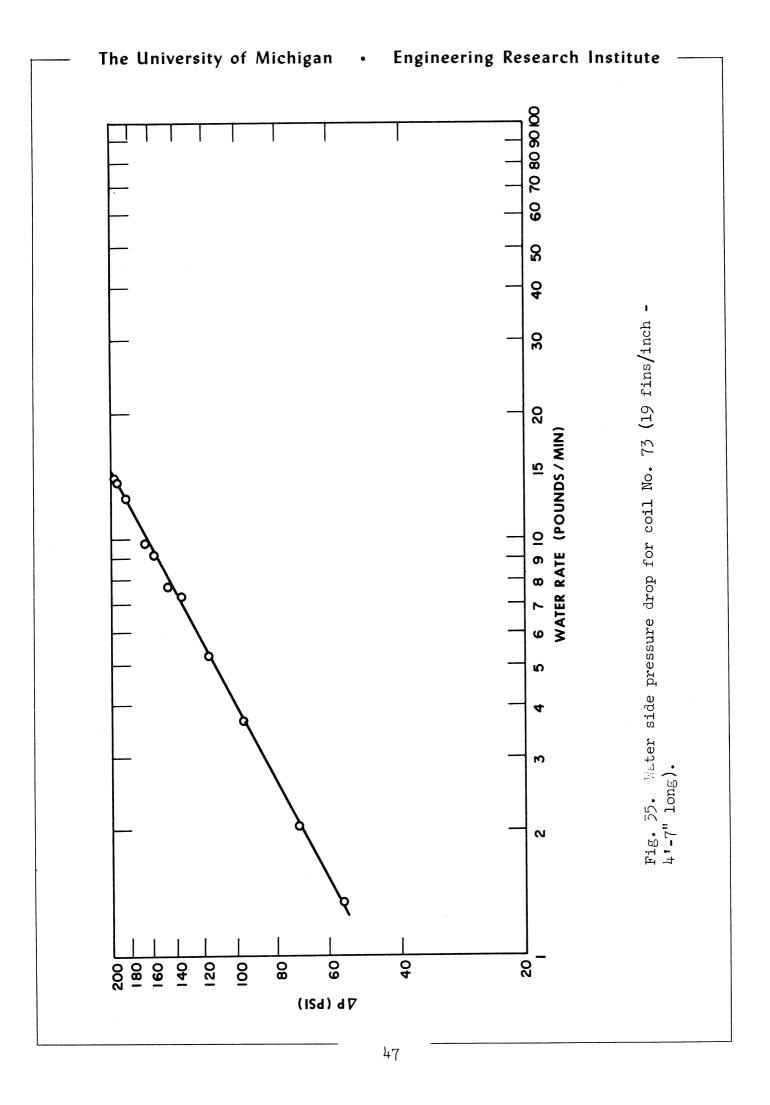
Fig. 30. Effect of length of coil on heat load with a constant water flow rate of 150 lbs. per minute.







(ISA) aV



(ISA) dV

200

140

120

8

49

